

JAEA-Data/Code 2014-001

Property Database of TRU Nitride Fuel

TRU窒化物燃料物性データベース

List of errata

正誤表

	Error (誤)	Correct (正)																																
p. 12	<p>Table 2-3-1 Coefficients a, b and c in Eq. (2-3-7) for (Zr<sub>0.61</sub>Pu<sub>0.39</sub>)N, (Zr<sub>0.58</sub>Pu<sub>0.21</sub>Am<sub>0.21</sub>)N and (Zr<sub>0.80</sub>Pu<sub>0.10</sub>Am<sub>0.10</sub>)N</p> <table border="1" style="width: 100%; text-align: center;"> <thead> <tr> <th></th> <th>(Zr<sub>0.61</sub>Pu<sub>0.39</sub>)N 298≤T(K)≤1100</th> <th>(Zr<sub>0.58</sub>Pu<sub>0.21</sub>Am<sub>0.21</sub>)N 298≤T(K)≤1082</th> <th>(Zr<sub>0.80</sub>Pu<sub>0.10</sub>Am<sub>0.10</sub>)N 298≤T(K)≤1067</th> </tr> </thead> <tbody> <tr> <td>a</td> <td>8.8807×10<sup>-3</sup></td> <td>7.6556×10<sup>-4</sup></td> <td>1.2836×10<sup>-3</sup></td> </tr> <tr> <td>b</td> <td>8.8807</td> <td>56.322</td> <td>42.542</td> </tr> <tr> <td>c</td> <td>-</td> <td>1.5865×10<sup>6</sup></td> <td>6.6356×10<sup>5</sup></td> </tr> </tbody> </table>		(Zr <sub>0.61</sub> Pu <sub>0.39</sub> )N 298≤T(K)≤1100	(Zr <sub>0.58</sub> Pu <sub>0.21</sub> Am <sub>0.21</sub> )N 298≤T(K)≤1082	(Zr <sub>0.80</sub> Pu <sub>0.10</sub> Am <sub>0.10</sub> )N 298≤T(K)≤1067	a	8.8807×10 <sup>-3</sup>	7.6556×10 <sup>-4</sup>	1.2836×10 <sup>-3</sup>	b	8.8807	56.322	42.542	c	-	1.5865×10 <sup>6</sup>	6.6356×10 <sup>5</sup>	<p>Table 2-3-1 Coefficients a, b and c in Eq. (2-3-7) for (Zr<sub>0.61</sub>Pu<sub>0.39</sub>)N, (Zr<sub>0.58</sub>Pu<sub>0.21</sub>Am<sub>0.21</sub>)N and (Zr<sub>0.80</sub>Pu<sub>0.10</sub>Am<sub>0.10</sub>)N</p> <table border="1" style="width: 100%; text-align: center;"> <thead> <tr> <th></th> <th>(Zr<sub>0.61</sub>Pu<sub>0.39</sub>)N 298≤T(K)≤1100</th> <th>(Zr<sub>0.58</sub>Pu<sub>0.21</sub>Am<sub>0.21</sub>)N 298≤T(K)≤1082</th> <th>(Zr<sub>0.80</sub>Pu<sub>0.10</sub>Am<sub>0.10</sub>)N 298≤T(K)≤1067</th> </tr> </thead> <tbody> <tr> <td>a</td> <td>8.8807×10<sup>-3</sup></td> <td>7.6556×10<sup>-4</sup></td> <td style="color: red;">1.7236×10<sup>-2</sup></td> </tr> <tr> <td>b</td> <td style="color: red;">46.507</td> <td>56.322</td> <td>42.542</td> </tr> <tr> <td>c</td> <td>-</td> <td>1.5865×10<sup>6</sup></td> <td>6.6356×10<sup>5</sup></td> </tr> </tbody> </table>		(Zr <sub>0.61</sub> Pu <sub>0.39</sub> )N 298≤T(K)≤1100	(Zr <sub>0.58</sub> Pu <sub>0.21</sub> Am <sub>0.21</sub> )N 298≤T(K)≤1082	(Zr <sub>0.80</sub> Pu <sub>0.10</sub> Am <sub>0.10</sub> )N 298≤T(K)≤1067	a	8.8807×10 <sup>-3</sup>	7.6556×10 <sup>-4</sup>	1.7236×10 <sup>-2</sup>	b	46.507	56.322	42.542	c	-	1.5865×10 <sup>6</sup>	6.6356×10 <sup>5</sup>
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p. 16	F = 64.58 - 0.2235 T - 0.0001812 T <sup>2</sup> - 0.00000004654 T <sup>3</sup>	F = 64.58 - 0.2235 T + 0.0001812 T <sup>2</sup> - 0.00000004654 T <sup>3</sup>																																
p. 17-18	<p>The thermal conductivity of (Zr<sub>x</sub>Pu<sub>(1-x)/2</sub>Am<sub>(1-x)/2</sub>)N (0.0 ≤ x ≤ 1.0) corrected for porosity to 100%TD is formulated by the following equation using the least squares method [26].</p> $K \text{ (Wm}^{-1}\text{K}^{-1}\text{)} = A + B \exp(x/C) \quad (2\text{-}4\text{-}4)$ $A = 4.7624 + 1.3937 \times 10^{-2} T - 1.4543 \times 10^{-5} T^2 + 5.6365 \times 10^{-9} T^3$ $B = -0.15962 - 4.2325 \times 10^{-4} T + 9.1965 \times 10^{-7} T^2$ $C = -9.8103 \times 10^{-3} + 2.3662 \times 10^{-4} T - 3.2471 \times 10^{-8} T^2$ <p>where x is the molar fraction of ZrN, and A, B and C are coefficients obtained by fitting. The temperature dependencies of the coefficients of A, B and C, obtained at each temperature above 873 K, are given as a polynomial equation of temperature. The predicted thermal conductivity of (Zr,Pu,Am)N is shown in Fig. 2-4-5. The uncertainty of</p>	<p>The thermal conductivity of (Zr<sub>x</sub>Pu<sub>(1-x)/2</sub>Am<sub>(1-x)/2</sub>)N (0.0 ≤ x ≤ 1.0) corrected for porosity to 100%TD is formulated by the following equation using the least squares method [26].</p> $K \text{ (Wm}^{-1}\text{K}^{-1}\text{)} = A + B \exp(x/C) \quad (2\text{-}4\text{-}4\text{-}1)$ $A = 4.7624 + 1.3937 \times 10^{-2} T - 1.4543 \times 10^{-5} T^2 + 5.6365 \times 10^{-9} T^3$ $B = -0.15962 - 4.2325 \times 10^{-4} T + 9.1965 \times 10^{-7} T^2$ $C = -9.8103 \times 10^{-3} + 2.3662 \times 10^{-4} T - 3.2471 \times 10^{-8} T^2$ <p>where x is the molar fraction of ZrN, and A, B and C are coefficients obtained by fitting. The temperature dependencies of the coefficients of A, B and C, obtained at each temperature above 873 K, are given as a polynomial equation of temperature. The predicted thermal conductivity of (Zr,Pu,Am)N is shown in Fig. 2-4-5. The uncertainty of</p>																																

the thermal conductivities obtained by above equation is estimated as  $\pm 15\%$ , from analytical and experimental errors.

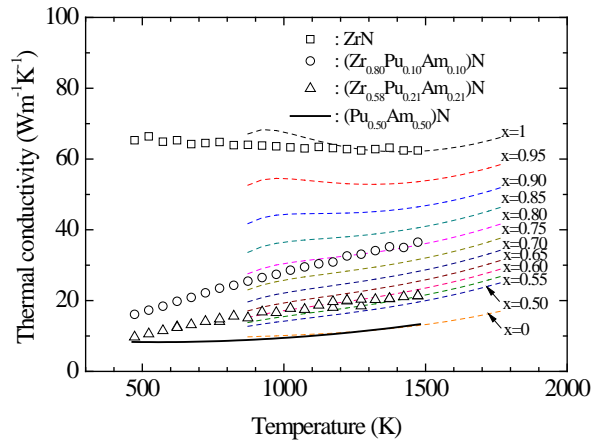


Fig. 2-4-5 Predicted thermal conductivity of  $(Zr_xPu_{(1-x)/2}Am_{(1-x)/2})N$

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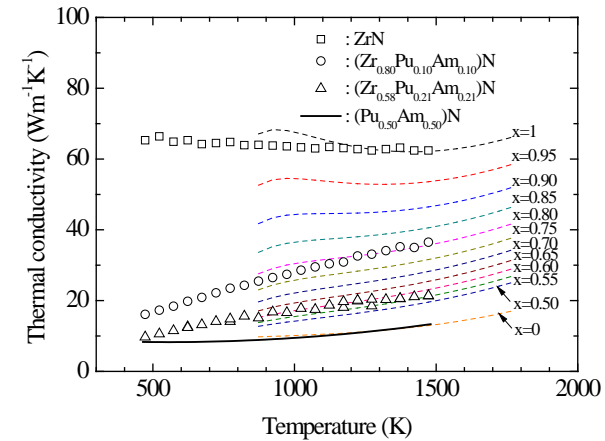


Fig. 2-4-5-1 Predicted thermal conductivity of  $(Zr_xPu_{(1-x)/2}Am_{(1-x)/2})N$

$$873 \leq T(K) \leq 1673$$

It is necessary to obtain the thermal conductivity above 473 K for the fuel design of ADS. Although the ZrN composition range is limited from 0.58 to 0.80, the thermal conductivity is expressed as the following equation.

$$K \text{ (Wm}^{-1}\text{K}^{-1}\text{)} = D + E x \quad (2-4-4-2)$$

$$D = -4.766 - 2.718 \times 10^{-4} T - 6.115 \times 10^{-6} T^2$$

$$E = 8.558 + 0.04059 T$$

The temperature dependencies of the coefficients of D and E, obtained at each temperature above 473 K, are given as a polynomial equation of

temperature. The predicted thermal conductivity of (Zr,Pu,Am)N is shown in Fig. 2-4-5-2. The uncertainty of the thermal conductivities obtained by above equation is estimated as  $\pm 10\%$ , from analytical and experimental errors.

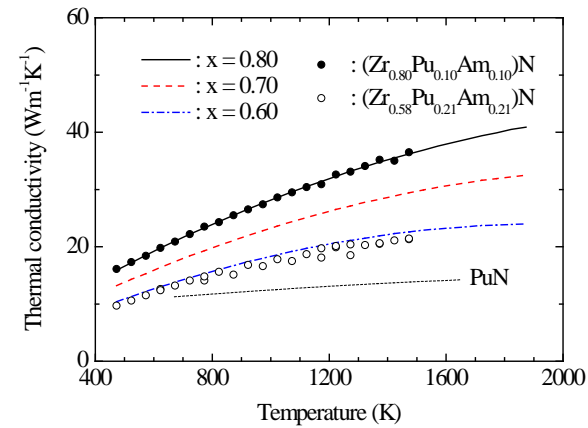


Fig. 2-4-5-2 Predicted thermal conductivity of  $(Zr_xPu_{(1-x)/2}Am_{(1-x)/2})N$   
 $473 \leq T(K) \leq 1673$ ,  $0.58 \leq x(\text{mol}\%) \leq 0.80$

p. 21

Table 2-4-6 Coefficients A, B, and C in Eq. (2-4-2) for  $(Np_{1-x}Am_x)N$   
 and  $(Pu_{1-x}Am_x)N$

	$(Np_{1-x}Am_x)N$			$(Pu_{1-x}Am_x)N$		
	x	0.25	0.50	0.75	0.25	0.50
A		7.18	6.49	3.45	12.81	10.03
B		$8.75 \times 10^{-3}$	$5.49 \times 10^{-3}$	$7.88 \times 10^{-3}$	$8.16 \times 10^{-3}$	$-6.39 \times 10^{-3}$
C		$-1.90 \times 10^{-6}$	$-6.07 \times 10^{-7}$	$-1.47 \times 10^{-6}$	$6.29 \times 10^{-6}$	$5.82 \times 10^{-6}$

Table 2-4-6 Coefficients A, B, and C in Eq. (2-4-2) for  $(Np_{1-x}Am_x)N$   
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<p><b>p. 28</b></p>	$\Delta_f G_{\text{UN}} \text{ (J/mol)} = -2.941 \times 10^5 + 80.98 T - 0.04640 T^2 + 3.085 \times 10^{-6} T^3$ $- 1.710 \times 10^6 / T \quad (298 < T(\text{K}) < 2628) \quad (2-9-1)$ $\Delta_f G_{\text{PuN}} \text{ (J/mol)} = -3.384 \times 10^5 + 152.0 T - 0.03146 T^2 - 5.998 \times 10^{-6} T^3$ $+ 6.844 \times 10^6 / T \quad (298 < T(\text{K}) < 3000) \quad (2-9-3)$	$\Delta_f G_{\text{UN}} \text{ (J/mol)} = -2.941 \times 10^5 + 80.98 T - 0.004640 T^2 + 3.085 \times 10^{-6} T^3$ $+ 1.710 \times 10^6 / T \quad (298 < T(\text{K}) < 2628) \quad (2-9-1)$ $\Delta_f G_{\text{PuN}} \text{ (J/mol)} = -3.384 \times 10^5 + 152.0 T - 0.03146 T^2 + 5.998 \times 10^{-6} T^3$ $+ 6.844 \times 10^6 / T \quad (298 < T(\text{K}) < 3000) \quad (2-9-3)$
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