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ROCKING : A COMPUTER PROGRAM FOR SEISMIC RESPONSE  
ANALYSIS OF RADIOACTIVE MATERIALS TRANSPORT  
AND/OR STORAGE CASKS

November 1995

Takeshi IKUSHIMA

日本原子力研究所  
Japan Atomic Energy Research Institute

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ROCKING : A Computer Program For Seismic Response Analysis of  
Radioactive Materials Transport AND/OR Storage Casks

Takeshi IKUSHIMA

Department of Fuel Cycle Safety Research  
Tokai Research Establishment  
Japan Atomic Energy Research Institute  
Tokai-mura, Naka-gun, Ibaraki-ken

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The computer program ROCKING has been developed for seismic response analysis, which includes rocking and sliding behavior, of radioactive materials transport and/or storage casks.

Main features of ROCKING are as follows;

- (1) Cask is treated as a rigid body.
- (2) Rocking and sliding behavior are considered.
- (3) Impact forces are represented by the spring dashpot model located at impact points.
- (4) Friction force is calculated at interface between a cask and a floor.
- (5) Forces of wire ropes against tip-over work only as tensile loads.

In the paper, the calculation model, the calculation equations, validity calculations and user's manual are shown.

Keywords: Computer Program, Seismic Response Analysis, Rocking Analysis,  
Structural Analysis, Cask, Transport Cask, Storage Cask

ROCKING：放射性物質輸送・貯蔵容器の地震応答解析プログラム

日本原子力研究所東海研究所燃料サイクル安全工学部

幾島 毅

(1995年10月5日受理)

放射性物質輸送・貯蔵容器の地震時のロッキングや滑り挙動を解析するために、計算プログラムROCKINGを開発した。

ROCKINGの主要な特徴は次のとおりである。

- (1) 輸送容器は剛体として取り扱う。
- (2) 輸送容器のロッキングおよび輸送容器と床面との間滑り挙動を考慮する。
- (3) 衝突力はばねとダッシュポットによって取り扱う。
- (4) 輸送容器と床面との間の摩擦力を考慮する。
- (5) 転倒防止用のワイヤーロープに加わる力は引張力のみを考慮する。

本報告書では、計算モデル、計算式、検証計算、計算プログラムの使用マニュアルについて記述されている。

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## 1. Introduction

In the stand point of seismic safety of transport and/or storage casks for spent fuels, it is necessary to evaluate integrity of casks against seismic loads. Therefore, it is important to clarify the tip-over behavior of casks during seismic loads using experimental and analytical methods.

Central Research Institute of Electric Power Industry(CRIEPI)<sup>(1)</sup>,<sup>(2)</sup> has studied seismic response behavior of casks experimentally and analytically. In this analysis the Distinct Element Method(DEM) was used for tip-over behavior of casks. However, the considerable cost and calculation time are necessitated to perform such analysis by the DEM.

Therefore, simplified computer programs which are capable of reducing cost and calculation time are needed to perform parametric calculation in designing casks and conducting safety analysis. To meet the above requirements, the computer program ROCKING<sup>(3)</sup> has been developed by Japan Atomic Energy Research Institute as shown in Fig.1.1.

In the program, a cask with (or without) tie-down wire ropes is modeled by a vertical cylindrical rigid body tied down with four non-linear springs having a certain tensile strength. An explicit or a semi-implicit numerical integration methods are adopted to predict whether a cask will tip-over or not, and tie-down ropes will break or not. Moreover, in the ROCKING program, sliding between a cask and a floor and vertical seismic load are treated.

The results of the ROCKING program are compared with experimental ones conducted by CRIEPI. Both analytical and experimental results fairly agree each others. The ROCKING program can accurately estimate tip-over behavior of casks during seismic loads.

In the paper, Chapter 2 presents an illustration of calculation model. Chapter 3 presents comparison between ROCKING and experimental results. Chapter 4 provides an user's guide for ROCKING.

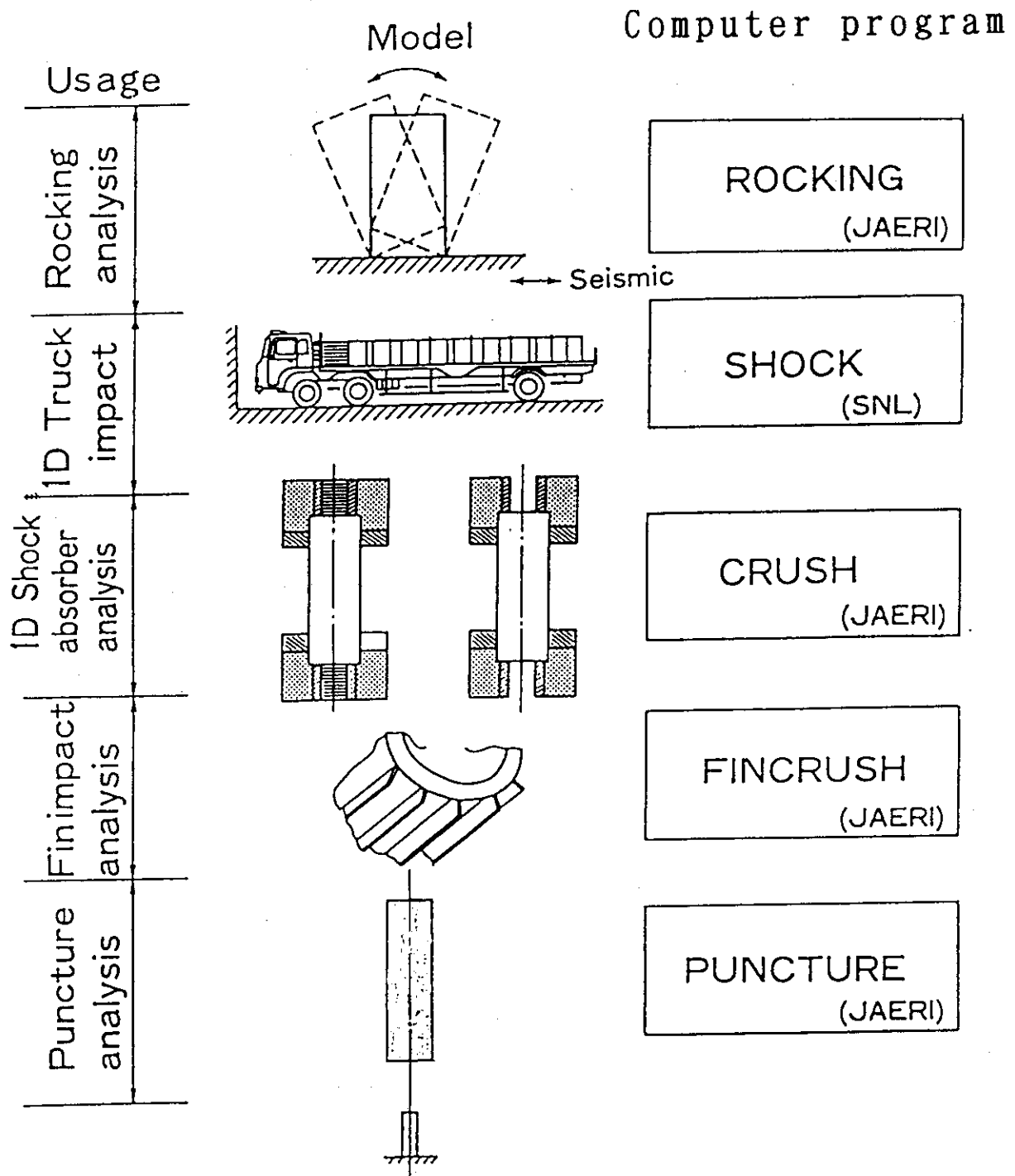


Fig. 1.1 Computer code



## 2. Calculation equation

### 2.1 Calculation model

In the computer program ROCKING, the following two-dimensional model is considered:

- (1) a cask is modeled as a rigid body,
- (2) the cask has three degrees-of-freedom, two translational displacements and one rotation around the cask center of gravity,
- (3) impact forces are represented by a spring and dashpot model located at impact points,
- (4) friction force due to surface sliding between the cask and a floor is represented by a nonlinear Coulomb element, and
- (5) forces of wire ropes work against only as tensile loads.

### 2.2 Equation of governing motion

Let the coordinate system be chosen as shown in Fig. 2.1. The cask has two translational coordinates,  $\xi$  and  $\eta$ , and one rotational coordinate  $\theta$ . Figure 2.2 shows the forces and moments that act upon the cask. The equations of motion may be written as:

$$m \ddot{\xi} = -m \alpha_{\xi} + F_{\xi A} + F_{\xi B} + F_{\xi C} + F_{\xi D} + R_{\xi} + F_F \quad (2.1)$$

$$F_{\eta A} + F_{\eta B} + F_{\eta C} + F_{\eta D} = 0 \quad (2.2)$$

$$m \ddot{z} = -m (\alpha_z + g) + F_{zA} + F_{zB} + F_{zC} + F_{zD} + R_z \quad (2.3)$$

$$M_{\xi A} + M_{\xi B} + M_{\xi C} + M_{\xi D} = 0 \quad (2.4)$$

$$I \ddot{\theta} = M_{\eta A} + M_{\eta B} + M_{\eta C} + M_{\eta D} + M_{R\xi} + M_{Rz} + M_F \quad (2.5)$$

$$M_{zA} + M_{zB} + M_{zC} + M_{zD} = 0 \quad (2.6)$$

where

- $a$  : cask rocking spring half width,
- $b$  : radius of cask bottom,
- $d$  : cask outer radius,
- $F_F$  : friction force between cask and floor,

$F_z$  : z -component of force,  
 $F_{zA}$  : z -component of force generated by wire rope A,  
 $F_{zB}$  : z -component of force generated by wire rope B,  
 $F_{zC}$  : z -component of force generated by wire rope C,  
 $F_{zD}$  : z -component of force generated by wire rope D,  
 $F_\eta$  :  $\eta$  -component of force,  
 $F_{\eta A}$  :  $\eta$  -component of force generated by wire rope A,  
 $F_{\eta B}$  :  $\eta$  -component of force generated by wire rope B,  
 $F_{\eta C}$  :  $\eta$  -component of force generated by wire rope C,  
 $F_{\eta D}$  :  $\eta$  -component of force generated by wire rope D,  
 $F_\xi$  :  $\xi$  -component of force,  
 $F_{\xi A}$  :  $\xi$  -component of force generated by wire rope A,  
 $F_{\xi B}$  :  $\xi$  -component of force generated by wire rope B,  
 $F_{\xi C}$  :  $\xi$  -component of force generated by wire rope C,  
 $F_{\xi D}$  :  $\xi$  -component of force generated by wire rope D,  
 $g$  : gravity constant,  
 $h$  : half height of cask,  
 $I$  : mass moment of inertia,  
 $m$  : mass of cask,  
 $M_F$  : moment generated by force  $F_F$ ,  
 $M_{Rz}$  : moment generated by force  $R_z$ .  
 $M_{R\xi}$  : moment generated by force  $R_\xi$ ,  
 $M_z$  : moment generated by force  $F_z$ ,  
 $M_{zA}$  : moment generated by force  $F_{zA}$ .  
 $M_{zB}$  : moment generated by force  $F_{zB}$ ,  
 $M_{zC}$  : moment generated by force  $F_{zC}$ ,  
 $M_{zD}$  : moment generated by force  $F_{zD}$ ,  
 $M_\eta$  : moment generated by force  $F_\eta$ ,  
 $M_{\eta A}$  : moment generated by force  $F_{\eta A}$ ,  
 $M_{\eta B}$  : moment generated by force  $F_{\eta B}$ ,

- $M_{\eta C}$  : moment generated by force  $F_{\eta C}$ ,  
 $M_{\eta D}$  : moment generated by force  $F_{\eta D}$ ,  
 $M_{\xi}$  : moment generated by force  $F_{\xi}$ ,  
 $M_{\xi A}$  : moment generated by force  $F_{\xi A}$ ,  
 $M_{\xi B}$  : moment generated by force  $F_{\xi B}$ ,  
 $M_{\xi C}$  : moment generated by force  $F_{\xi C}$ ,  
 $M_{\xi D}$  : moment generated by force  $F_{\xi D}$ ,  
 $R_z$  : impact force of z-direction,  
 $R_{\xi}$  : impact force of  $\xi$ -direction,  
 $z$  : z-coordinate or z-direction displacement,  
 $\dot{z}$  : z-component of velocity,  
 $\ddot{z}$  : z-component of acceleration,  
 $\alpha_z$  : vertical floor acceleration,  
 $\alpha_{\xi}$  : horizontal floor acceleration,  
 $\eta$  :  $\eta$ -coordinate or  $\eta$ -direction displacement,  
 $\theta$  : rotational angle,  
 $\dot{\theta}$  : angular velocity,  
 $\ddot{\theta}$  : angular acceleration,  
 $\nu$  : velocity,  
 $\xi$  :  $\xi$ -coordinate or  $\xi$ -direction displacement,  
 $\dot{\xi}$  :  $\xi$ -component of velocity,  
 $\ddot{\xi}$  :  $\xi$ -component of acceleration.

### 2.3 Friction force between cask and floor and its associated moment

The friction force due to surface sliding is represented by a nonlinear Coulomb element. The equations for the friction force  $F_F$  and its associated moment  $M_F$  acting on the cask are as follows.

$$F_F = -\text{sign}(\nu) F(\nu), \quad (2.7)$$

$$M_F = F_F(-h \cdot \cos\theta - b \cdot \sin\theta), \quad (2.8)$$

where

$$v = \dot{\xi} - (h \cdot \cos\theta + b \cdot \sin\theta) \dot{\theta} - \dot{\xi}_0. \quad (2.9)$$

Where  $\dot{\xi}$  and  $\dot{\xi}_0$  are horizontal velocity of the center of gravity and support floor, respectively.  $F(v)$  is a prescribed function for the friction characteristics which are related to the vertical contact force and the coefficients of both statical and dynamical friction.

$$F(v) = m \cdot g (\mu_d + \mu_s), \quad (2.10)$$

Where  $\mu_d$  and  $\mu_s$  are the coefficients of dynamical and statical frictions, respectively.

#### 2.4 Vertical impact force and its associated moment

The force acting on the interface between the cask and floor is derived in the term of deformation of a spring dashpot unit. When the gap is closing, the spring deformation  $\gamma$  and its time rate  $\dot{\gamma}$  are

$$\gamma = 0.5(z_0 - \{z + h(1 - \cos\theta) - b \cdot \sin\theta\}) \quad (2.11)$$

$$\dot{\gamma} = 0.5\{\dot{z}_0 - \{\dot{z} + h \cdot \sin\theta - b \cdot \cos\theta\} \dot{\theta}\} \quad (2.12)$$

where  $b$  is the cask rocking spring half width.  $z_0$  and  $\dot{z}_0$  are the vertical displacement and velocity of the floor, respectively. The vertical impact force  $R_z$  and its associated moment  $M_{Rz}$  acting on the cask are as follows. If  $\gamma > 0$

$$R_z = - (K_z \cdot \gamma + C_z \cdot \dot{\gamma}), \quad (2.13)$$

$$M_{Rz} = - R_z (h \cdot \cos\theta - a \cdot \sin\theta). \quad (2.14)$$

where  $K_z$  and  $C_z$  are the vertical boundary spring and damping coefficients, respectively. If  $\tau \leq 0$

If  $\gamma \leq 0$

$$R_z = 0, \quad (2.15)$$

$$M_{Rz} = 0. \quad (2.16)$$

#### 2.5 Lower corner impact force and its associated moment

The force acting on the cask lower corner as a results of the impact is derived by deformation of a spring dashpot unit which is

located on the lower corner of the cask. During impact against the lower corner, spring deformation  $\tau$  and its time rate  $\dot{\tau}$  of the cask are follows.

$$\tau = \xi + h \cdot \sin\theta - b (1 - \cos\theta) - \xi_0 - \delta, \quad (2.17)$$

$$\dot{\tau} = \dot{\xi} + (h \cdot \cos\theta - b \cdot \sin\theta) \dot{\theta} - \dot{\xi}_0, \quad (2.18)$$

where  $\delta$  is the gap between the cask and its lower boundary wall. The boundary wall impact force  $R_t$  and its associated moment  $M_{Rt}$  acting on the cask are as follows. If  $\tau > 0$

$$R_t = - (K_t \cdot \tau + C_t \cdot \dot{\tau}), \quad (2.19)$$

$$M_{Rt} = R_t (h \cdot \cos\theta - b \cdot \sin\theta), \quad (2.20)$$

where  $K_t$  and  $C_t$  are the horizontal boundary spring and damping coefficients, respectively. If  $\tau \leq 0$

$$R_t = 0, \quad (2.21)$$

$$M_{Rt} = 0. \quad (2.22)$$

## 2.6 Force due to wire rope

A tensile force due to a wire rope is as follows:

$$F = \sigma \cdot A, \quad (2.23)$$

where

$F$  : tensile force of wire rope,

$\sigma$  : tensile stress of wire rope,

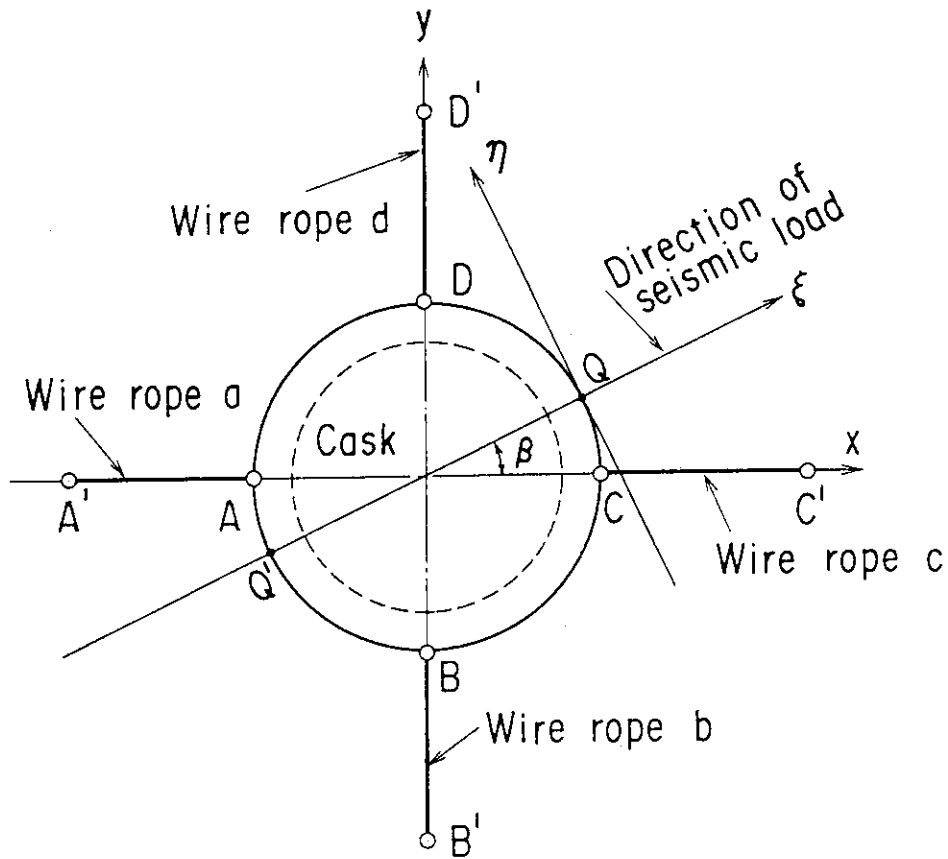
$$\sigma = E \cdot \Delta L / L, \quad (2.24)$$

$A$  : sectional area of wire rope,

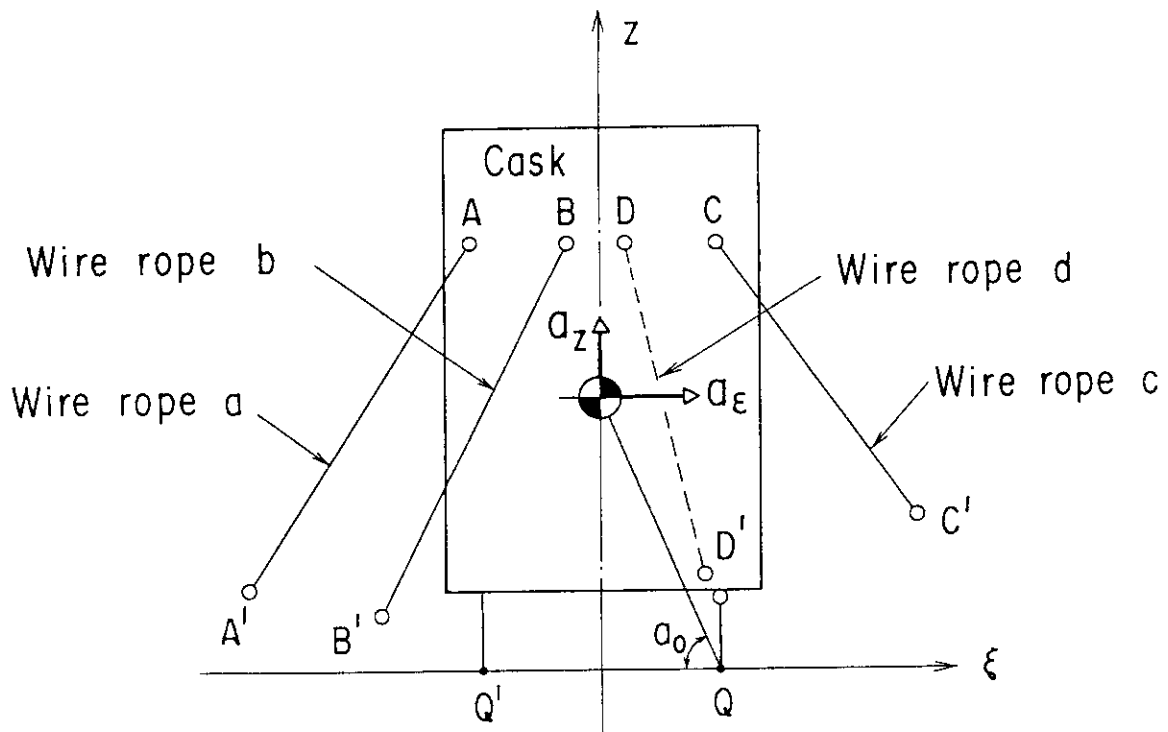
$E$  : Young's modulus,

$\Delta L$  : elongation of wire rope,

$L$  : wire rope length.

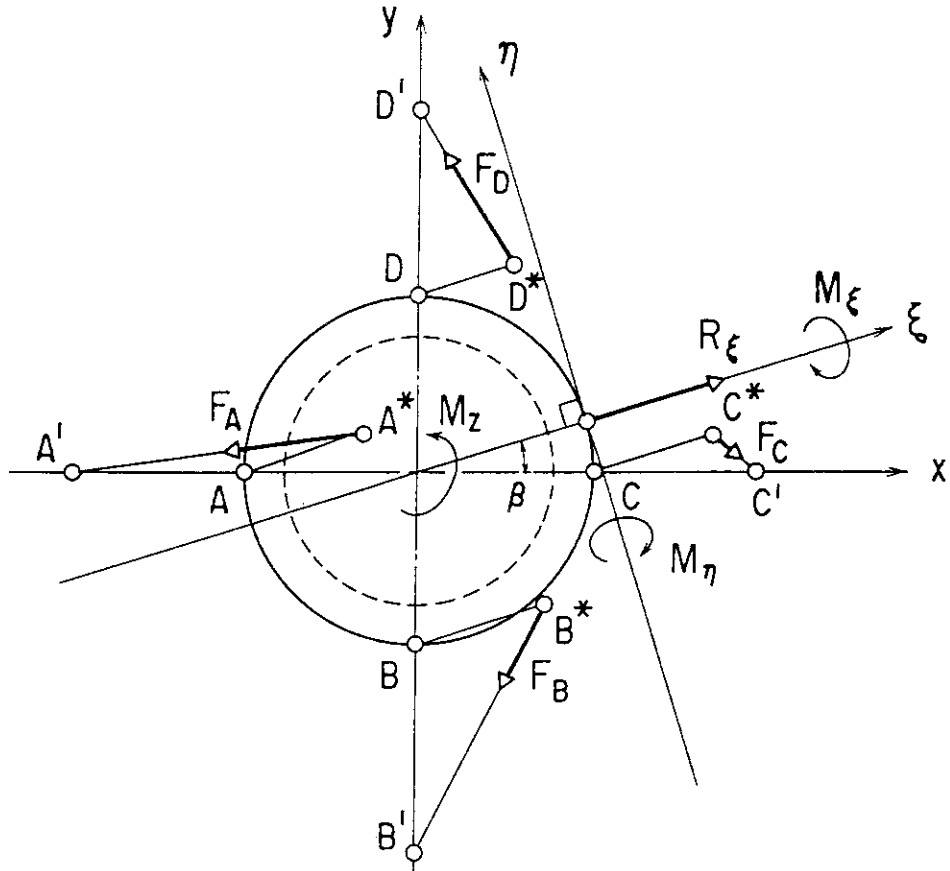


(b) Plane view

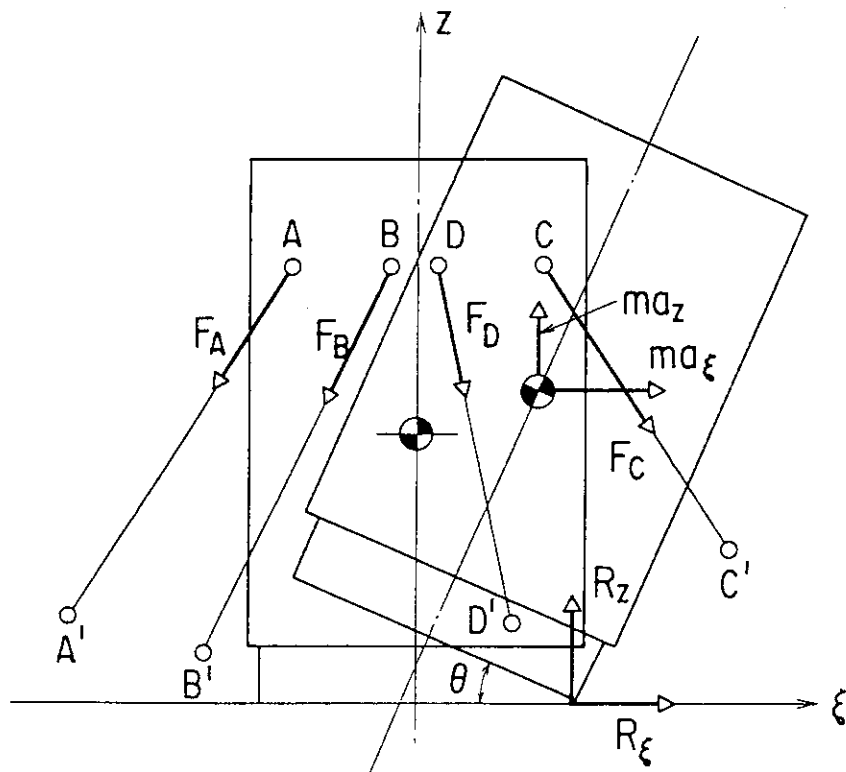


(a) Vertical view

Fig. 2.1 Coordinate system



(b) Plane view



(a) Vertical view

Fig. 2.2 Forces and moments acting on cask

### 3. Benchmark calculation

In order to demonstrate the adequacy of ROCKING, benchmark calculations using the CRIEPI experimental results of the 1/3 scale model of spent fuel cask as shown in Fig. 3.1 have been performed.

The rocking analysis of the model cask was performed under constant sinusoidal excitations. Figure 3.2 shows the maximum rotational angles in comparison with the experimental results. According to Fig.3.2 analytical results of ROCKING agree with the experimental ones.



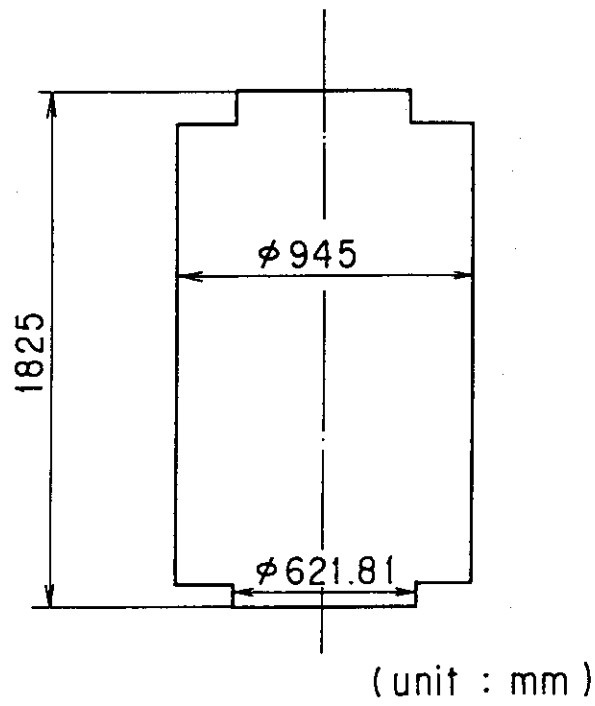


Fig. 3.1 Analysis model

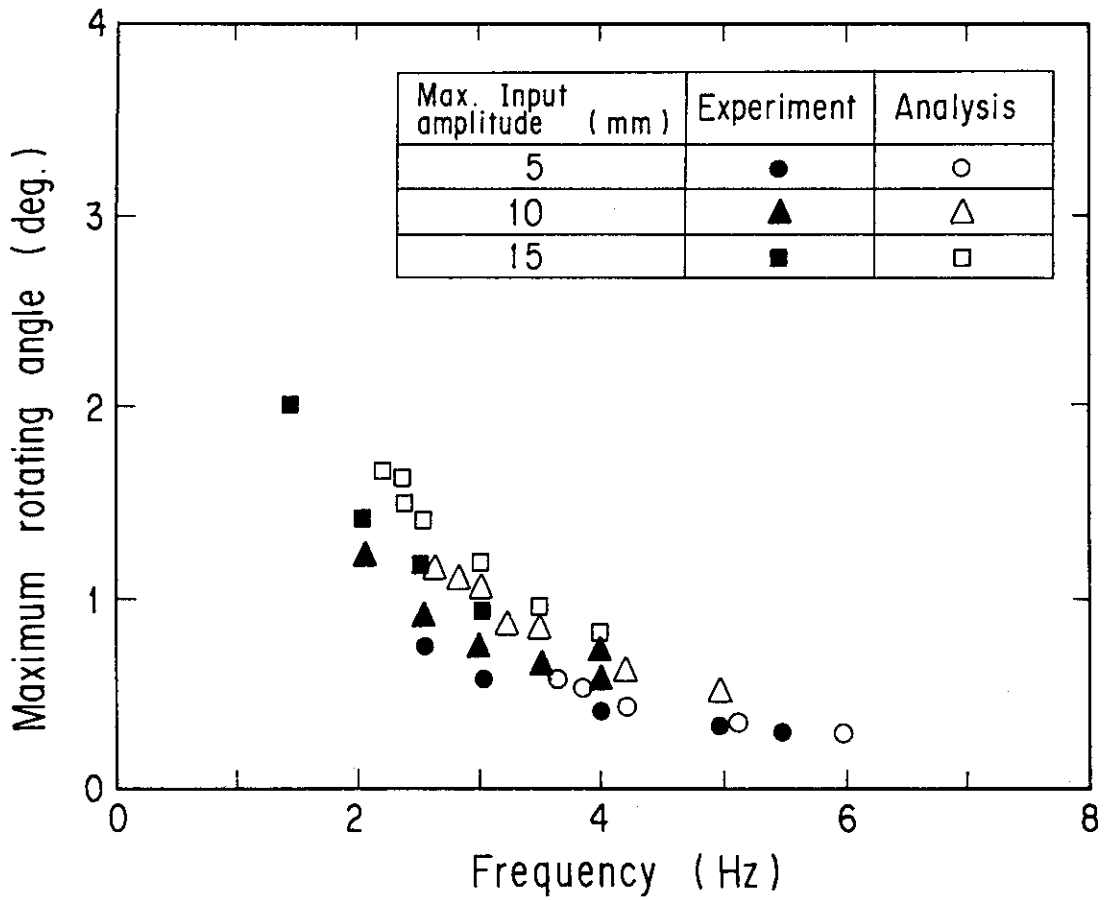


Fig. 3.2 Comparison between experiment and analysis

4. Computer program

4.1 Program description

The computer program ROCKING consists of a main routine and 26 subroutines. Overall structure of ROCKING is shown in Fig. 4.1.

Functions of the main routine and subroutines are as follows:

MAIN : initializes the start of run.  
 JULY31 : numerical integration using the Runge-Kutta method.  
 FUN : formation of calculation equations.  
 MOMENT : calculation of moments.  
 WIRDSP : calculation of wire rope lengths.  
 WIRINI : calculation of initial wire rope lengths.  
 GREATT : search of maximum values.  
 BIGLK : printout of maximum values.  
 DTVWST : store data for plotting.  
 DIPlot : plotting of cask displacements.  
 XYPlot : plotting of response values.  
 UWPlot : plotting of input wave.  
 BLKPLT : plotting of response values.  
 FRIC : calculation of friction force,  
 FUNUO : set of horizontal seismic wave,  
 FUNWO : set of vertical seismic wave,  
 FIT : calculation of amplitude of seismic wave,  
 SSIN : calculation of sine function,  
 GCOS : calculation of cosine function,  
 ZEROCL : clear memory,  
 MEMMAX : search of maximum values,  
 MEMMIN : search of minimum values,  
 UMMAX : search of maximum values,  
 UMMIN : search of minimum values,  
 DLOG : calculation of log-scale data,

RNUM : plot number,

DTLIST : printout of input data echo.

A macroscopic flowsheet of ROCKING is shown in Fig. 4.2.

#### 4.2 Description of input data

This section describes the input data required by ROCKING. The input data consists of the job description, analysis type such as with or without wire ropes for tip-over turn, geometries, the cask weight, initial conditions, boundary condition constants, the integral time step, strength data of wire ropes, seismic data and options for plottings. The input instructions are simple and easy to follow. The input data forms are presented in Table 4.1.

#### 4.3 Description of output data

This section describes the output data required by ROCKING. The contents of these various output quantities are described in the followings.

##### (1) Input data

Input data are printed in two formats. The first printout format is exactly the same as they are read. Second, the code lists the data as interpreted by the code.

##### (2) Calculation data

The calculation values; the maximum displacement, velocity, acceleration, forces and moments are printed.

##### (3) Graphical output

The computer code ROCKING provides users with graphical output of cask deflection and time history curves such as displacement, velocity, acceleration, forces and moments.

Table 4.1 Input data for ROCKING

Columns	Format	Variables	Descriptions
Data set No.1:Job description.			
1 - 5	5A1	-	'TITLE'.
6 - 10	5X	-	Blank.
11 - 72	62A1	ITI	Job description.
Data set No.2:Option data.			
1 - 7	7A1	-	'CONTROL'.
8 - 10	3X	-	Blank.
11 - 15	I5	IWIR	Option data for wire rope. =0:Without wire rope. =1:With wire rope.
Data set No.3:Geometry data.			
1 - 8	8A1	-	'GEOMETRY'.
9 - 10	2X	-	Blank.
11 - 20	F10.0	HH	Height of gravity center.
21 - 30	F10.0	BB	Upper radius.
31 - 40	F10.0	RCSK(2)	Lower radius.
41 - 50	F10.0	EI	Moment of inertia.
51 - 60	F10.0	EM	Mass.
61 - 70	F10.0	WI	Weight.
Data set No.4:Data for vertical impact.			
1 - 10	10A1	-	'V-SPRING-L'.
11 - 20	F10.0	XB	Radius of vertical impact point.
Data set No.5:Spring constant and damping coefficient of vertical impact.			
1 - 8	8A1	-	'VERTICAL'.
9 - 10	2X	-	Blank.
11 - 20	F10.0	V1K	Spring constant(1).
21 - 30	F10.0	V2K	Spring constant(2).

Table 4.1 (Continued)

Columns	Format	Variables	Descriptions
31 - 40	F10.0	V3K	Spring constant(3).
41 - 50	F10.0	V1C	Damping coefficient(1).
51 - 60	F10.0	V2C	Damping coefficient(2).
61 - 70	F10.0	V3C	Damping coefficient(3).
Resultant spring constant $K_z$ ;			
$K_z = V1K + V2K \cdot \gamma + V3K \cdot \gamma^2 .$			
Resultant damping coefficient $C_z$ ;			
$C_z = V1C + V2C \cdot \dot{\gamma} + V3C \cdot \dot{\gamma}^2 ,$			
where, $\gamma$ : Overlap vector of vertical spring,			
$\dot{\gamma}$ : Relative velocity between cask and floor.			
Data set No.6:Spring constant and damping coefficient of lower boundary horizontal impact.			
1 - 8	8A1	-	'HORIZONTAL'.
9 - 10	2X	-	Blank.
11 - 20	F10.0	B1K	Spring constant(1).
21 - 30	F10.0	B2K	Spring constant(2).
31 - 40	F10.0	B3K	Spring constant(3).
41 - 50	F10.0	B1C	Damping coefficient(1).
51 - 60	F10.0	B2C	Damping coefficient(2).
61 - 70	F10.0	B3C	Damping coefficient(3).
Resultant spring constant $K_t$ ;			
$K_t = B1K + B2K \cdot \tau + B3K \cdot \tau^2 .$			
Resultant damping coefficient $C_t$ ;			
$C_t = B1C + B2C \cdot \dot{\tau} + B3C \cdot \dot{\tau}^2 ,$			
where, $\tau$ : Overlap vector of horizontal spring,			
$\dot{\tau}$ : Relative velocity between cask and floor.			
Data set No.7;Friction coefficient.			
1 - 8	8A1	-	'FRICTION'.
9 - 10	2X	-	Blank.

Table 4.1 (Continued)

Columns	Format	Variables	Descriptions
11 - 20	F10.0	F1	Coefficient of static friction.
21 - 30	F10.0	F2	Coefficient of kinetic friction.
Data set No.8;Initial values.			
1 - 7	7A1	-	'INITIAL'.
8 - 10	3X	-	Blank.
11 - 20	F10.0	X(1)	Initial angle.
21 - 30	F10.0	X(2)	Initial angular velocity.
31 - 40	F10.0	X(3)	Initial horizontal displacement.
41 - 50	F10.0	X(4)	Initial horizontal velocity.
51 - 60	F10.0	X(5)	Initial vertical displacement.
61 - 70	F10.0	X(6)	Initial vertical velocity.
Data set No.9;Timestep data.			
1 - 8	8A1	-	'TIMESTEP'.
9 - 10	2X	-	Blank.
11 - 20	F10.0	TINT	Initial problem time.
21 - 30	F10.0	TEND	Final problem time.
31 - 40	F10.0	DT	Integral time step size.
41 - 50	F10.0	TSTS	Time step size of plot data output for time history curve.
51 - 60	F10.0	TSTP	Time step size of plot data output for cask rocking.
Data set No.10A;Wire rope A data.			
1 - 10	10A1	-	'WIREROPE-A'.
11 - 20	F10.0	RWI(1)	Radius of attached wire rope of lower end.
21 - 30	F10.0	ZWI(1)	Height of attached wire rope of lower end.
31 - 40	F10.0	ZWCI(1)	Height of attached wire rope of upper end.
41 - 50	F10.0	WGEO(1,1)	Young's modulus of wire rope.
51 - 60	F10.0	WGEO(2,1)	Sectional area of wire rope.

Table 4.1 (Continued)

Columns	Format	Variables	Descriptions
61 - 70	F10.0	WGEO(3,1)	Ultimate strength of wire rope(default value is $10^{20}$ ).
Data set No.10B;Wire rope B data.			
1 - 10	10A1	-	'WIREROPE-B'.
11 - 20	F10.0	RWI(2)	Radius of attached wire rope of lower end.
21 - 30	F10.0	ZWI(2)	Height of attached wire rope of lower end.
31 - 40	F10.0	ZWCI(2)	Height of attached wire rope of upper end.
41 - 50	F10.0	WGEO(1,2)	Young's modulus of wire rope.
51 - 60	F10.0	WGEO(2,2)	Sectional area of wire rope.
61 - 70	F10.0	WGEO(3,2)	Ultimate strength of wire rope(default value is $10^{20}$ ).
Data set No.10C;Wire rope C data.			
1 - 10	10A1	-	'WIREROPE-C'.
11 - 20	F10.0	RWI(3)	Radius of attached wire rope of lower end.
21 - 30	F10.0	ZWI(3)	Height of attached wire rope of lower end.
31 - 40	F10.0	ZWCI(3)	Height of attached wire rope of upper end.
41 - 50	F10.0	WGEO(1,3)	Young's modulus of wire rope.
51 - 60	F10.0	WGEO(2,3)	Sectional area of wire rope.
61 - 70	F10.0	WGEO(3,3)	Ultimate strength of wire rope(default value is $10^{20}$ ).
Data set No.10D;Wire rope D data.			
1 - 10	10A1	-	'WIREROPE-D'.
11 - 20	F10.0	RWI(4)	Radius of attached wire rope of lower end.
21 - 30	F10.0	ZWI(4)	Height of attached wire rope of lower end.
31 - 40	F10.0	ZWCI(4)	Height of attached wire rope of upper end.
41 - 50	F10.0	WGEO(1,4)	Young's modulus of wire rope.
51 - 60	F10.0	WGEO(2,4)	Sectional area of wire rope.
61 - 70	F10.0	WGEO(3,4)	Ultimate strength of wire rope(default value

Table 4.1 (Continued)

Columns	Format	Variables	Descriptions
			is $10^{20}$ ).
Data set No.10E;Angle of seismic load.			
1 - 10	10A1	-	'INPUTANGLE'.
11 - 20	F10.0	BETA	Angle of seismic load.
Skip data set 10A - 10E if there are not wire ropes.			
Data set No.11A;Seismic data(I).			
1 - 10	10A1	-	'SINUSOIDAL'.
11 - 20	F10.0	G	Amplitude of input wave. KIK=0:Displacement amplitude. KIK=2:Acceleration amplitude.
21 - 30	F10.0	P	Circular frequency of input wave. KIK=0:Circular frequency(rad/s). KIK=2:Freauency(Hz).
Data set No.11B;Seismic data(II).			
1 - 9	9A1	-	'SEISMIC-1'.
10	1X	-	Blank.
11 - 15	I5	KIK	Option for seismic wave. KIK=0:Sinusoidal wave. KIK=2:Sinusoidal wave. KIK=3:Seismic wave.
Data set No.11C;Seismic data(III).			
1 - 9	9A1	-	'SEISMIC-2'.
10	1X	-	Blank.
11 - 15	I5	KXK(1)	Option for horizontal seismic wave. KXK(1)=0:No seismic wave. KIK(1)=1:Seismic wave.



Table 4.1 (Continued)

Columns	Format	Variables	Descriptions
16 - 20	5X	-	Blank.
21 - 25	I5	KXK(3)	Option for vertical seismic wave. KXK(3)=0:No seismic wave. KXK(3)=1:Seismic wave.
26 - 30	5X	-	Blank.
31 - 40	F10.0	ALP	Scale factor of displacement of horizontal seismic wave.
41 - 50	F10.0	BET	Scale factor of velocity of horizontal seismic wave.
Data set No.11D1:Seismic data(IVA:Option for displacement of horizontal seismic wave).			
1 - 10	10X	-	Blank.
11 - 14	I4	KXN(1,1)	Number of data.
15 - 30	16X	-	Blank.
31 - 40	F10.0	DDT(1,1)	Time step size of data.
Data set No.11D2:Seismic data(IVB:Displacement of horizontal seismic wave).			
1 - 10	10X	-	Blank.
11 - 20	F10.0	VX(1,1,1)	Horizontal displacement.
21 - 30	F10.0	VX(1,1,2)	.....
31 - 40	F10.0	VX(1,1,3)	.....
41 - 50	F10.0	VX(1,1,4)	.....
51 - 60	F10.0	VX(1,1,5)	Horizontal displacement.
Repeat data set No.11D2.			
Data set No.11E1:Seismic data(VA:Option for velocity of horizontal seismic wave).			
1 - 10	10X	-	Blank.
11 - 14	I4	KXN(1,2)	Number of data.
15 - 30	16X	-	Blank.

Table 4.1 (Continued)

Columns	Format	Variables	Descriptions
31 - 40	F10.0	DDT(1,2)	Time step size of data.
Data set No.11E2:Seismic data(VB:Velocity of horizontal seismic wave).			
1 - 10	10X	-	Blank.
11 - 20	F10.0	VX(1,2,1)	Horizontal velocity.
21 - 30	F10.0	VX(1,2,2)	.....
31 - 40	F10.0	VX(1,2,3)	.....
41 - 50	F10.0	VX(1,2,4)	.....
51 - 60	F10.0	VX(1,2,5)	Horizontal velocity.
Repeat data set No.11E2.			
Data set No.11F1:Seismic data(VIA:Option for displacement of vertical seismic wave).			
1 - 10	10X	-	Blank.
11 - 14	I4	KXN(3,1)	Number of data.
15 - 30	16X	-	Blank.
31 - 40	F10.0	DDT(3,1)	Time step size of data.
Data set No.11F2:Seismic data(VIB:Displacement of vertical seismic wave).			
1 - 10	10X	-	Blank.
11 - 20	F10.0	VX(3,1,1)	Vertical displacement.
21 - 30	F10.0	VX(3,1,2)	.....
31 - 40	F10.0	VX(3,1,3)	.....
41 - 50	F10.0	VX(3,1,4)	.....
51 - 60	F10.0	VX(3,1,5)	Vertical displacement.
Repeat data set No.11F2.			
Data set No.11G1:Seismic data(VIIA:Option for velocity of vertical seismic wave).			
1 - 10	10X	-	Blank.
11 - 14	I4	KXN(3,2)	Number of data.

Table 4.1 (Continued)

Columns	Format	Variables	Descriptions
15 - 30	16X	-	Blank.
31 - 40	F10.0	DDT(3,2)	Time step size of data.
Data set No.11G2:Seismic data(VIIB:Velocity of vertical seismic wave).			
1 - 10	10X	-	Blank.
11 - 20	F10.0	VX(3,2,1)	Vertical velocity.
21 - 30	F10.0	VX(3,2,2)	.....
31 - 40	F10.0	VX(3,2,3)	.....
41 - 50	F10.0	VX(3,2,4)	.....
51 - 60	F10.0	VX(3,2,5)	Vertical velocity.
Repeat data set No.11G2.			
Data set No.12:Plot data			
1 - 4	4A1	-	'PLOT'.
5 - 10	6X	-	Blank.
(11-70)	20I3	IPL0T(1) (I=1,20)	Option for time history plot. IPL0T(I)=0:No plot. IPL0T(I)=1:Plotting.
11 - 13	I3	IPL0T(1)	Angle(degree).
14 - 16	I3	IPL0T(2)	Angular velocity(rad/s).
17 - 19	I3	IPL0T(3)	Angular acceleration(rad/s <sup>2</sup> )
20 - 22	I3	IPL0T(4)	Horizontal displacement.
23 - 25	I3	IPL0T(5)	Horizontal velocity.
26 - 28	I3	IPL0T(6)	Horizontal acceleration.
29 - 31	I3	IPL0T(7)	Vertical displacement.
32 - 34	I3	IPL0T(8)	Vertical velocity.
35 - 37	I3	IPL0T(9)	Vertical acceleration.
38 - 40	I3	IPL0T(10)	Moment due to gravitational acceleration.
41 - 43	I3	IPL0T(11)	Frictional force.
44 - 46	I3	IPL0T(12)	Moment due to frictional force.
47 - 49	I3	IPL0T(13)	Vertical impact force.

Table 4.1 (Continued)

Columns	Format	Variables	Descriptions
50 - 52	I3	IPL0T(14)	Moment due to vertical impact force.
53 - 55	I3	IPL0T(15)	Horizontal impact force.
56 - 58	I3	IPL0T(16)	Moment due to horizontal impact force.
59 - 61	I3	IPL0T(17)	Tensile force of wire rope A.
62 - 64	I3	IPL0T(18)	Tensile force of wire rope B.
65 - 67	I3	IPL0T(19)	Tensile force of wire rope C.
68 - 70	I3	IPL0T(20)	Tensile force of wire rope D.

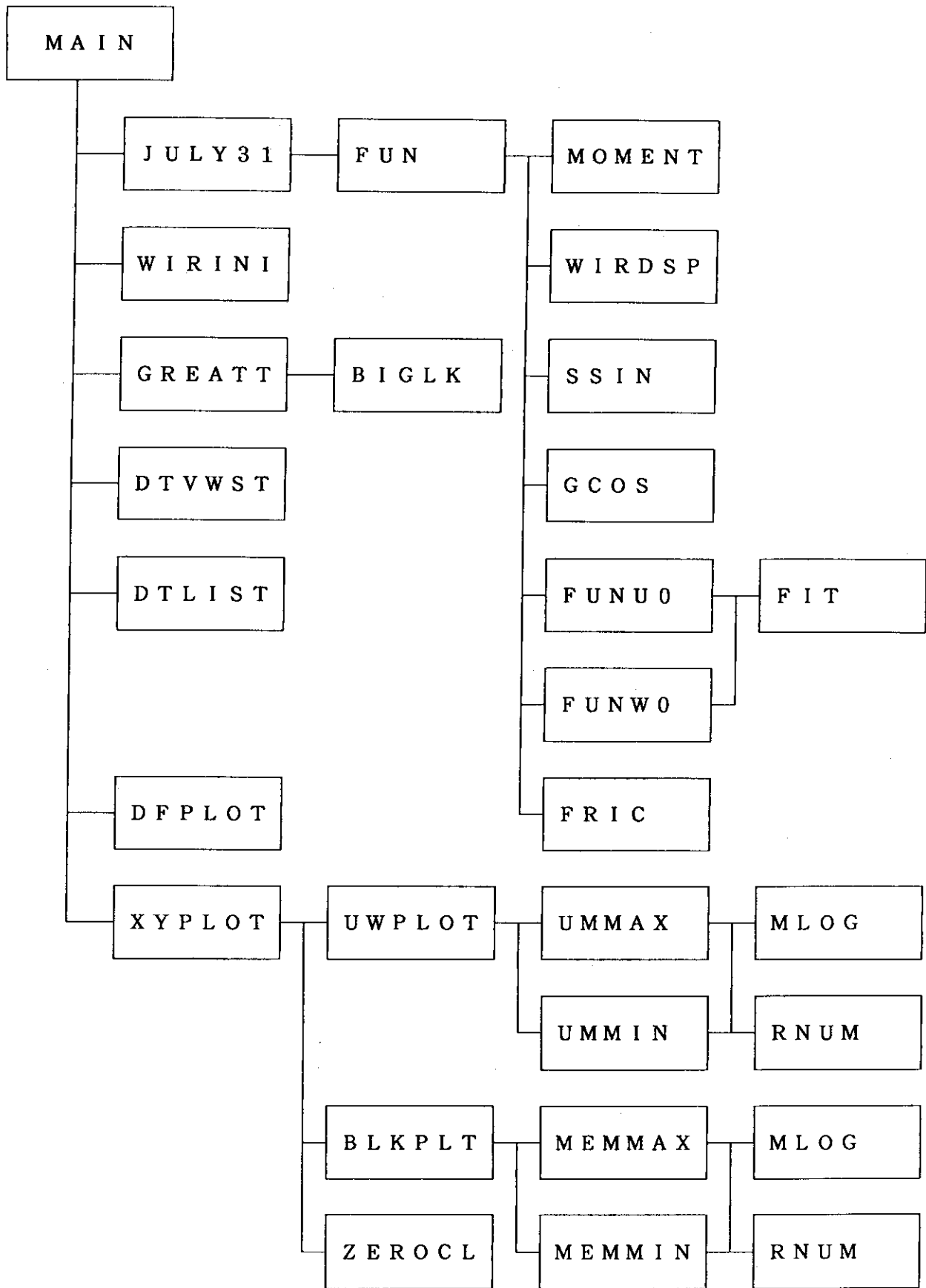


Fig. 4.1 Structure of ROCKING

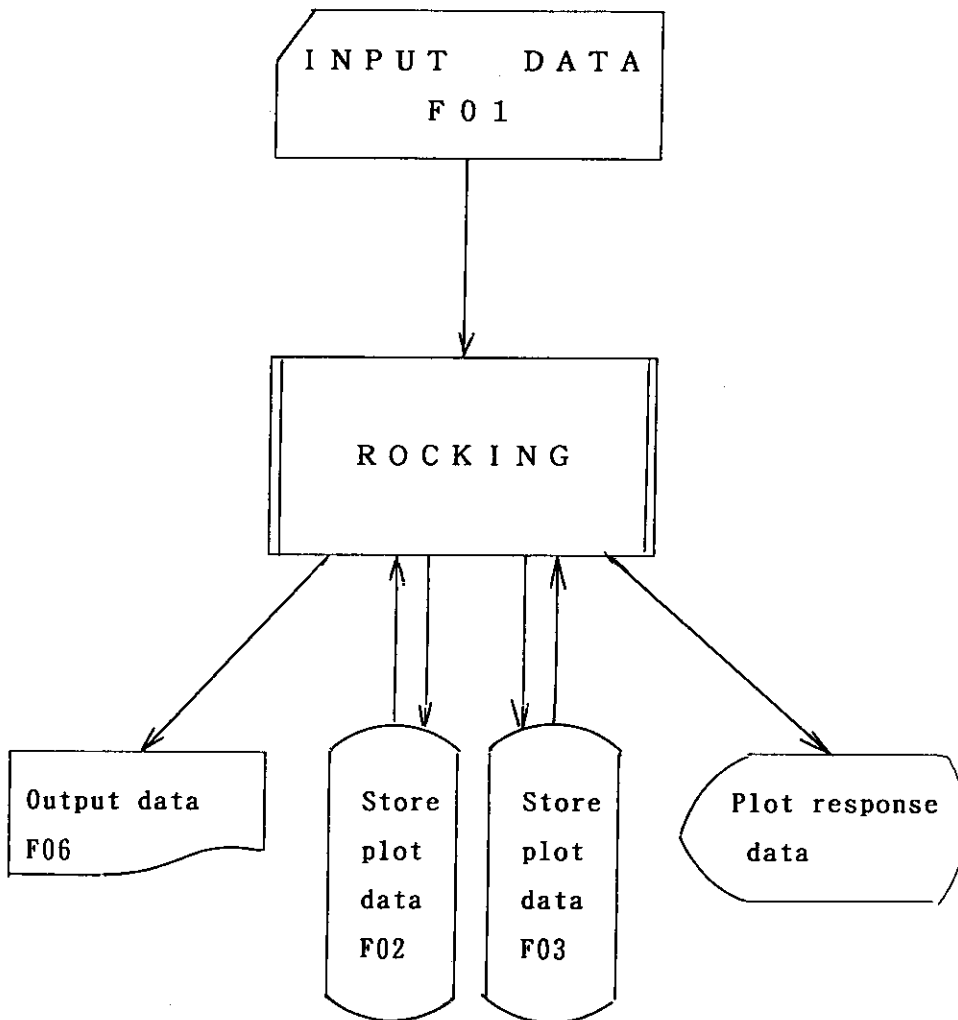


Fig. 4.2 Flowsheet of ROCKING

## 5. Conclusions

A computer program ROCKING for analysis of casks tip-over behavior has been developed. Validity tests for ROCKING have been performed using CRIEPI experimental results. Good agreement was obtained between analytical and experimental results.

In regard to evaluation of tip-over behavior of casks during sinusoidal and seismic excitations, the computer program ROCKING makes analysis economically shortening CPU time.

## Acknowledgments

The author is indebted to Dr. C. Ito and his colleagues of Central Research Institute of Electric Power Industries for providing the experimental data. The author also indebted to Mr. J. Oshika of Century Research Center Ltd., for assistance of making the computer program.

## References

- (1) T. Saegusa, C. Ito, H. Imaeda, et al., "Cask Storage of Spent Fuel at Reactors", CRIEPI U27(1993).
- (2) K. Sirai, C. Ito, H. Ryu, "Development of Seismic Response Analysis Code of Cask", PATRAM 91(1991-Japan).
- (3) T. Ikushima, "CASKETSS-2: A Computer Code System for Thermal and Structural Analysis of Nuclear Fuel Shipping Casks (Version 2)", JAERI-M 91-129(1991).

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- (3) T. Ikushima, "CASKETSS-2: A Computer Code System for Thermal and Structural Analysis of Nuclear Fuel Shipping Casks (Version 2)", JAERI-M 91-129(1991).

Appendix A Sample problem input

INPUT DATA ECHO

```

      1      2      3      4      5      6      7      8
-----5-----0-----5-----0-----5-----0-----5-----0-----5-----0-----5-----0-----5-----0
TITLE: SAMPLE PROBLEM SINE 3.0 HZ 1.0CM WITH BASE FRICTION WITH WIRE
CONTROL      1
GEOMETRY      91.25      32.90      29.00      3.000E+5      12.86      1.260E+4
V-SPRING-L    25.00      -25.00
VERTICAL      5.600E+5      0.0      0.0      4.500E-4      0.0      0.0
HORIZONTAL    5.600E+5      0.0      0.0      4.500E-4      0.0      0.0
FRICTION      0.3      0.0
INITIAL      0.0      0.0      0.0      0.0      0.0      0.0
TIMESTEP      0.0      2.0      0.0001      0.002      0.2
WIREROPE-A    250.0      0.0      384.5      2.100E+6      2.19      3.000E+4
WIREROPE-B    250.0      0.0      384.5      2.100E+6      2.19      3.000E+4
WIREROPE-C    250.0      0.0      384.5      2.100E+6      2.19      3.000E+4
WIREROPE-D    250.0      0.0      384.5      2.100E+6      2.19      3.000E+4
INPUTANGLE    0.0
SINUSOIDAL    1.0      3.0      0.0
SEISMIC-1     3
SEISMIC-2     0      0      0
PLOT          1      1      1      1      1      1      0      0      0      0      1      0      1      0      1      0      1      1      1      1      0
-----5-----0-----5-----0-----5-----0-----5-----0-----5-----0-----5-----0-----5-----0
      1      2      3      4      5      6      7      8

```

\*\*\* INPUT DATA END \*\*\*

Appendix B Sample problem output

ROCKING TITLE: SAMPLE PROBLEM SINE 3.0 HZ 1.0CM WITH BASE FRICTION WITH WIRE

1. CALCULATION SYSTEM

NO. OF MASS	1
START TIME	0.000000
END TIME	2.000000
TIME STEP	0.000100
TIME STEP FOR TIME HISTORY DATA STORE	0.002000
TIME STEP FOR DISPLACEMENT DATA STORE	0.200000

2. DIMENSION

NO.	BLOCK		VERTICAL SPRING	
	HEIGHT	WIDTH	DISTANCE LEFT	DISTANCE RIGHT
1	91.2500	32.9000	-25.0000	25.0000

3. MASS

NO. OF MASS	MASS(KG.SEC**2/CM)	WEIGHT(KG)	ROTATION OF INERTIA
1	0.128600E+02	0.126000E+05	0.300000E+06

4. STIFFNESS

4.1 VERTICAL				
NO.	KV(1)	KV(2)	KV(3)	
1	0.560000E+06	0.000000E+00	0.000000E+00	

4.2 HORIZONTAL				
NO.	KB(1)	KB(2)	KB(3)	
1	0.560000E+06	0.000000E+00	0.000000E+00	

5. DAMPING

5.1 VERTICAL				
NO.	CV(1)	CV(2)	CV(3)	
1	0.450000E-03	0.000000E+00	0.000000E+00	

5.2 HORIZONTAL				
NO.	CB(1)	CB(2)	CB(3)	
1	0.450000E-03	0.000000E+00	0.000000E+00	

6. FRICTION

INTERFACE	F(1)	F(2)
1	0.378000E+04	0.000000E+00

7. INITIAL STATE

NO.	THETA	D-THETA/D-T	U	D-U/D-T	W	D-W/D-T
1	0.000000E+00	0.000000E+00	0.000000E+00	0.000000E+00	0.000000E+00	0.000000E+00

Appendix B (Continued)

8. PLOTTING DATA

THETA - (DEGREE)  
 THETA - VELOCITY  
 THETA - ACCELERATION  
 U - DISPLACEMENT  
 U - VELOCITY  
 U - ACCELERATION  
 FORCE BY FRICTION  
 FORCE BY V.SPRING  
 FORCE BY B.WALL  
 FORCE BY WIRE-A  
 FORCE BY WIRE-B  
 FORCE BY WIRE-C  
 FORCE BY WIRE-D

9. CALCULATION RESULTS (MAXIMUM VALUES)

9.1 DISPLACEMENT

THETA(DEGREE)	U	W
6.60696E+00	1.03609E+01	3.85642E+00

9.2 VELOCITY

D-THETA/D-T	D-U/D-T	D-W/D-T
8.99792E-01	7.88946E+01	9.65527E+01

9.3 ACCELERATION

D2THETA/DT2	D2U/DT2	D2W/DT2
2.36095E+01	4.84425E+03	1.37748E+04

9.4 FORCE AND MOMENT

MOMENT BY GRAVITY	FORCE BY FRICTION	MOMENT BY FRICTION	FORCE BY V.SPRING	MOMENT BY V.SPRING	FORCE BY H.SPRING	MOMENT BY H.SPRING
4.14540E+05	3.78000E+03	3.56938E+05	2.02397E+05	3.99026E+06	5.79090E+04	5.35245E+06

9.5 WIRE FORCE

FORCE BY WIRE-A	FORCE BY WIRE-B	FORCE BY WIRE-C	FORCE BY WIRE-D
6.56596E+04	3.97098E+04	6.56506E+04	6.56944E+04

Appendix C Graphical output

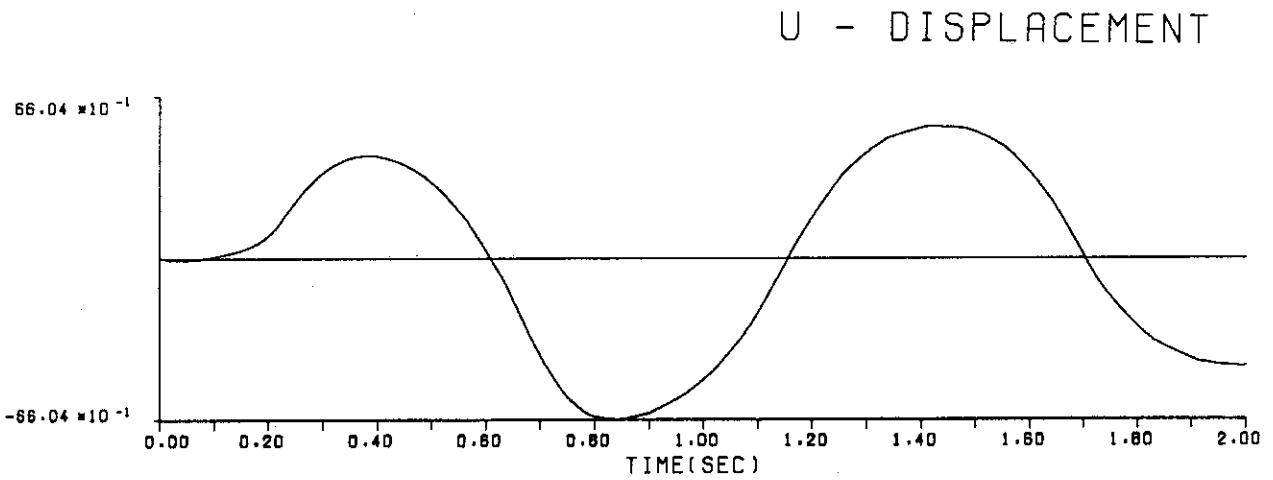
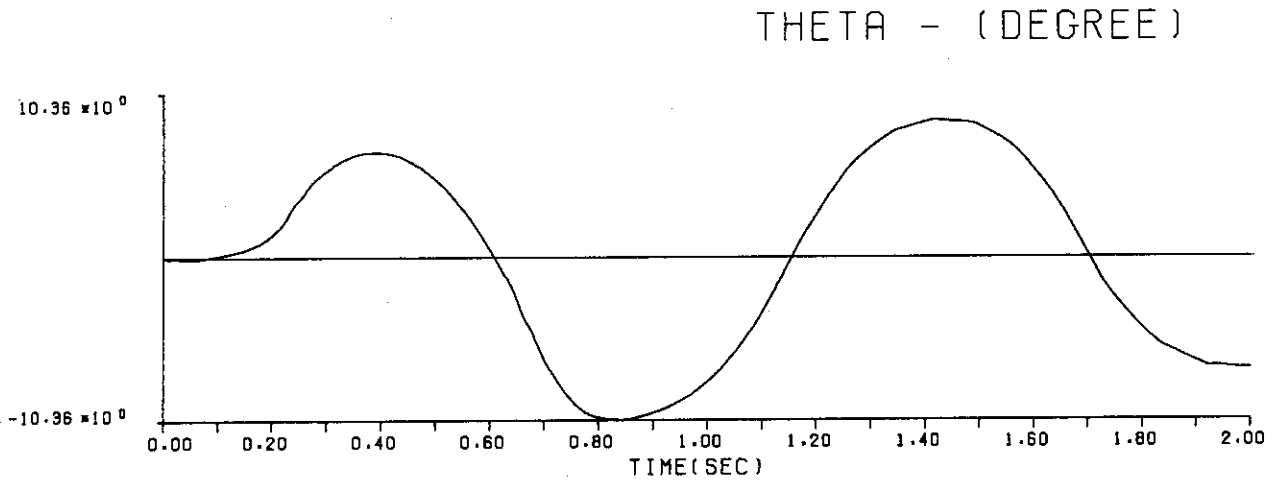


Fig. C.1 Graphical output of ROCKING(1)

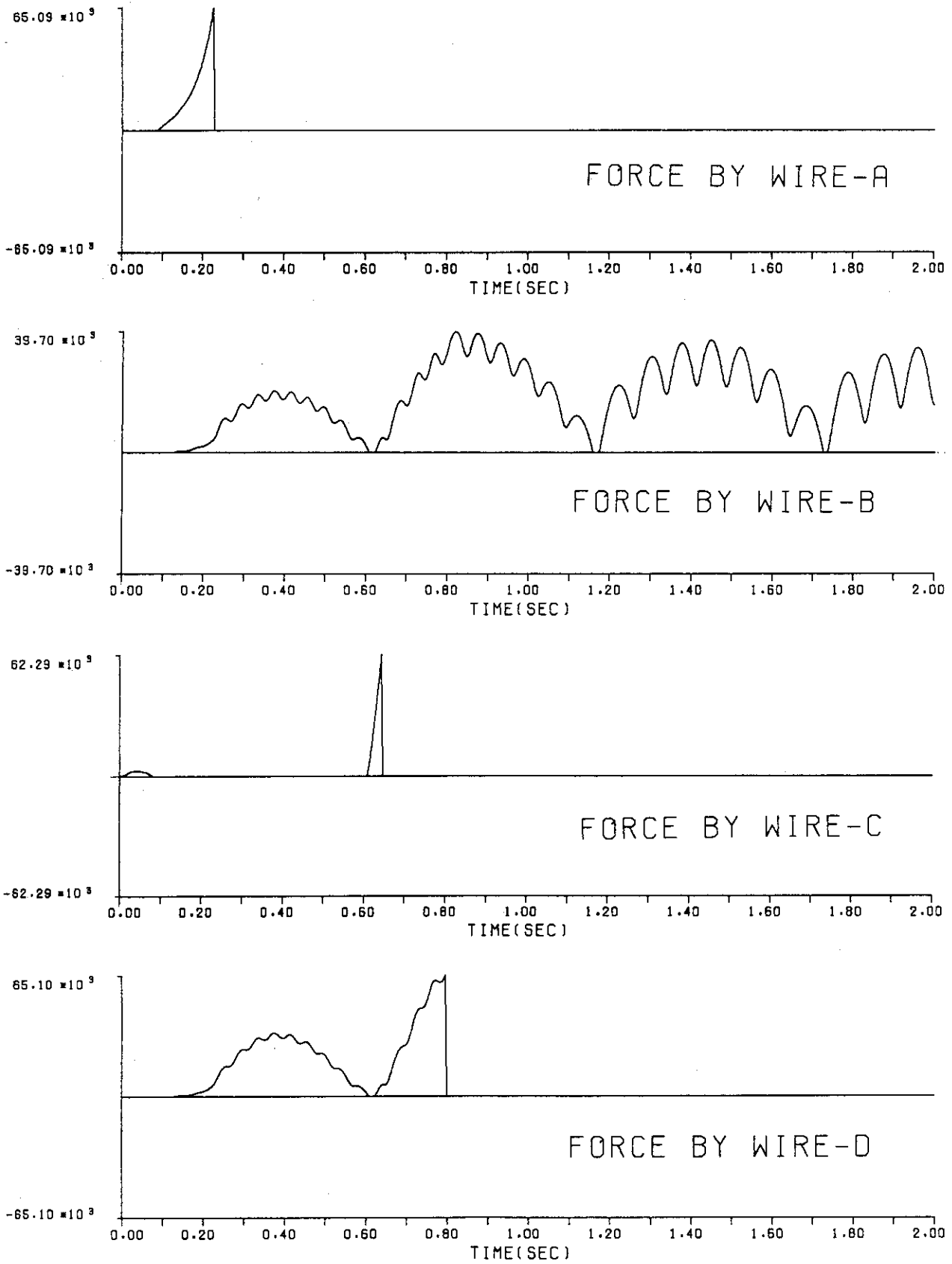


Fig. C.2 Graphical output of ROCKING(2)

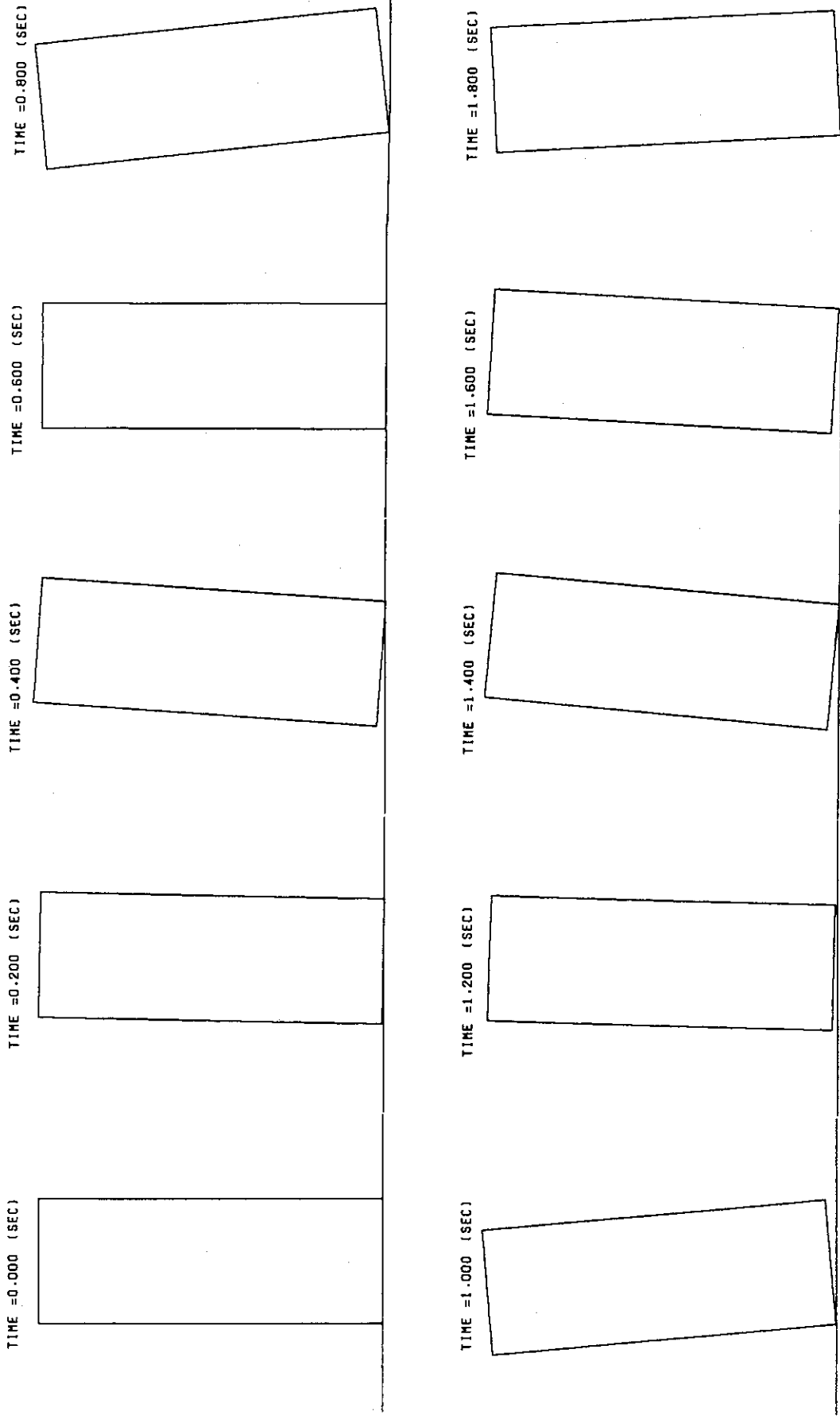


Fig. C.3 Graphical output of ROCKING(3)

## Appendix D Job control data

The job control data for ROCKING execution on the computer FACOM M-780 in JAERI is as follows:

```
//JCLG JOB
// EXEC JCLG
//SYSIN DD DATA,DLM='++'
// JUSER XXXXXXXX.XX,XXXXXXXX,XXXX.XX,ROCKING
    T.03 C.02 W.01 I.02 CLS GRP
    OPTP MSGCLASS=A,MSGLEVEL=(2,0,1),CLASS=B,NOTIFY=JXXXX
    OPTP PASSWORD=XXXXXXXX
//RUN EXEC LMGOEX,LM=J2322.LMROCKIN,PNM=ROCKING
// EXPAND GRNLP
//FT01F001 DD DSN=JXXXX.DTROCKIN.DATA,DISP=SHR
//FT02F001 DD SPACE=(TRK,(5,5)),UNIT=TSSWK
//FT03F001 DD SPACE=(TRK,(5,5)),UNIT=TSSWK
++
//
```



Appendix E Program abstract

1. Name :  
ROCKING
2. Computer for which the program is designed and others upon which it is possible:  
FACOM M-780, SUN4, IBM-PC
3. Nature of physical problem solved:  
Drop impact analysis of radioactive material transport casks.
4. Method of solutions:  
One-dimensional dynamic analysis.
5. Restrictions on the complexity of the problem:  
None.
6. Typical running time:  
FACOM M-780 : 1 minute.  
SUN4 : 2 minutes.  
IBM PC : 5 minutes.
7. Unusual features of the program:  
None.
8. Related and auxiliary program:  
None.
9. Status  
-
10. References:  
"CASKETSS-2:Computer Code System for Thermal and Structural Analysis of Nuclear Fuel Shipping Casks(Version2)",  
JAERI-M 91-129(1991).

11. Machine requirement:

1100 k bytes of core memory.

12. Program language used:

FORTRAN-77

13. Operating system or monitor under the program is executed:

FACOM M-780 : MSP

SUN4 : Solaris 2.1

IBM PC : Windows 3.1

14. Any other program or operating information or restrictions:

The program is approximately 1700 source steps. The plotting programs are used as follows:

FACOM M-780 : CALCOMP plotter or the compatible ones.

SUN4 : X-windows

IBM PC : Windows 3.1

15. Name and establishment of author:

T. Ikushima

Japan Atomic Energy Research Institute,  
Tokai Research Establishment.

Department of Fuel Cycle Safety Research,  
Tokai-mura, Naka-gun, Ibaraki-ken, 319-11  
Japan

16. Material available:

Source.

Appendix F Program source list

```

C*****
C
C          ROCKING ---  MAIN PROGRAM
C
C*****
      IMPLICIT REAL*8 (A-H,O-Z)
      REAL*4 HHHH, BBBB
      COMMON/IRIR/ XB(10),VK,VC,DK,DC,BK,BC,HH,BB,EI,EM,WI,NB,ITI(18)
      COMMON/COEF/ F1, F2,
1          V1K, V2K, V3K, B1K, B2K, B3K,
2          V1C, V2C, V3C, B1C, B2C, B3C, UD
      COMMON/FIG/ TIM,STEP,TSTP,GHOST(1024)
      COMMON/AAWWPP/ G, W, P
      COMMON/XXD/ A(6)
      COMMON/FMFMFM/ FGM, FRI, FRM, VFZ, VYM, BWF, BWM,
1          FWF(4), FWM(4)
      COMMON/GRETTT/ GFGMG, GFRIG, GFRMG, GVFZG, GVYMG, GBWFG, GBWMG,
1          GMXX(6), GMAA(6), GFWF(4)
      COMMON/XDSDSX/ XDIS(6), UB
      COMMON/FRIFRI/ FPAI
      COMMON/CXXCXX/ CXX
      COMMON/KIKKIK/ Z1, Z2, Z3, Z4, Z5, Z6, KIK
      COMMON/KXXKK/ DDT(3,2),VX(3,2,1100), KXX(3), KXN(3,2)
      COMMON/PDPXPD/ PX,PD,PD2,PXX,PDD,PDW2
      COMMON/ALPBET/ ALP,BET
      COMMON/XX/ X(6),Q(6),T1(6),XN(6),N6,NMAX
      COMMON/BC/ EE,TC,NCONTC
      COMMON/UIDID/ UIDO,UID1
      COMMON /WIRE/ RWI(4), ZWI(4), ZWCI(4), WGEO(3,4), WDISP(3,2,4),
1          WCORDO(3,2,4), WCORD(3,2,4), WLENGO(4), WLENG(4),
2          WFORC(4),WFCMP(3,4), WMCMP(3,4), IWSTAT(4),NWIRE
      COMMON /CASK/ RCSK(2), ZCSK, WCSK, CSKI, BETA
      COMMON /LUNITL/ LUCD, LUHT, LUDP, LUPR

      DIMENSION XWRIT(21),IPLLOT(21),E(6),JPLLOT(5,21)
      CHARACTER*26 PARM(3)
      DATA ((JPLLOT(I,J),I=1,5),J=1,9)
1          /'THET','A - ','(DEG','REE)',' '
2          /'THET','A - ','VELO','CITY',' '
3          /'THET','A - ','ACCE','LERA','TION'
4          /' ','U - ','DISP','LACE','MENT'
6          /' ','U - ','VELO','CITY',' '
7          /' ','U - ','ACCE','LERA','TION'
8          /' ','W - ','DISP','LACE','MENT'
9          /' ','W - ','VELO','CITY',' '
+          /' ','W - ','ACCE','LERA','TION'/
      DATA ((JPLLOT(I,J),I=1,5),J=10,21)
1          /'MOME','NT B','Y GR','AVIT','Y '
2          /'FORC','E BY',' FRI','CTIO','N '
3          /'MOME','NT B','Y FR','ICTI','ON '
4          /'FORC','E BY',' V.S','PRIN','G '
5          /'MOME','NT B','Y V.','SPRI','NG '
6          /'FORC','E BY',' B.W','ALL ',' '
7          /'MOME','NT B','Y B.','WALL',' '
8          /'FORC','E BY',' WIR','E-A ',' '
9          /'FORC','E BY',' WIR','E-B ',' '
+          /'FORC','E BY',' WIR','E-C ',' '
1         /'FORC','E BY',' WIR','E-D ',' '
    
```

## Appendix F (Continued)

```

2      , '      ' , '      ' , '      ' , '      ' , '      ' , '      ' /
C
CJR  CALL  OSPARM( PARM )
CJR  OPEN(UNIT=LUCD,FILE=PARAM(1),FORM='FORMATTED',STATUS='OLD')
CJR  OPEN(UNIT=LUHT,FILE=PARAM(2),FORM='UNFORMATTED',STATUS='UNKNOWN')
CJR  OPEN(UNIT=LUDP,FILE=PARAM(3),FORM='UNFORMATTED',STATUS='UNKNOWN')
C
    PAIPAI = 3.1415926535900
    MAXD = 21
    LUCD = 1
    LUHT = 2
    LUDP = 3
    LUPR = 6
    GFGMG = 0.
    GFRIG = 0.
    GFRMG = 0.
    GVFGZG = 0.
    GVYMG = 0.
    GBWFG = 0.
    GBWMG = 0.
    DO 50 N=1,4
50  GFWF(N) = 0.
    DO 60 N=1,6
    GMXX(N) = 0.
60  GMAA(N) = 0.
    DO 70 I=1,6
    A(I) = 0.E0
    X(I) = 0.0
    Q(I) = 0.0
    T1(I) = 0.0
70  XN(I) = 0.0
    DO 80 I=1,3
    DO 80 J=1,4
80  WFCMP(I,J) = 0.0
    DO 90 N=1,21
    IPLOT(N) = 0
90  XWRIT(N) = 0.0
    UD = 0.
C
    CALL DTLIST( LUCD, LUPR)
C
C  INPUT DATA
C
    READ(LUCD,6000,END=300)  ITI
    READ(LUCD,6010)  NWIRE
    NN = 1
    N6 = 6
    NMAX = N6
    NB = 2
    NBND = 0
C
C  CALCULATION DATA
C
    READ(LUCD,6020)  HH, BB, RCSK(2), EI, EM, WI
    READ(LUCD,6020)  XB(1)
    XB(2) = - XB(1)
    READ(LUCD,6020)  V1K ,V2K ,V3K ,V1C ,V2C ,V3C
    READ(LUCD,6020)  B1K ,B2K ,B3K ,B1C ,B2C ,B3C

```

## Appendix F (Continued)

```

READ(LUCD,6020) F1 , F2 , CXX
READ(LUCD,6020) (X(I),I=1,N6)
READ(LUCD,6020) TINT, TEND, DT, TSTS, TSTP

```

C  
C  
C

PLOTTING DATA INTERVAL

```

IF ( TSTS .LT. DT ) GO TO 100
ITHTMX = ( TEND - TINT ) / TSTS
IF ( ITHTMX .GT. 2048 ) ITHTMX = 2048
TSTS = ( TEND - TINT ) / DFLOAT( ITHTMX )
100 CONTINUE
IF ( TSTP .LT. DT ) GO TO 105
ITDPMX = ( TEND - TINT ) / TSTP
IF ( ITDPMX .GT. 2048 ) ITDPMX = 2048
TSTP = ( TEND - TINT ) / DFLOAT( ITDPMX )
105 CONTINUE

```

C  
C-----

READ WIRE PROPERTY AND GEOMETRY

```

IF( NWIRE .EQ. 0 ) GO TO 115
DO 110 I=1,4
READ(LUCD,6020) RWI(I), ZWI(I), ZWCI(I), (WGEO(J,I),J=1,3)
IF(WGEO(3,I) .EQ. 0.0 ) WGEO(3,I) = 1.0D20
110 CONTINUE
RCSK(1) = BB
WCSK = WI
CSKI = EI
ZCSK = HH
READ(LUCD,6020) BETA

```

C  
C-----

WIRE GEOM INITIAL SET

```

CALL WIRINI( 4, WCORDO, WLENGO, RWI, ZWI, ZWCI, RCSK(2), BETA)

```

C  
C  
C  
C  
C  
C

115 CONTINUE

SEISMIC DATA

```

READ(LUCD,6020) G, W, P, DIFDF, CHECK
READ(LUCD,6025) KIK, Z1, Z2, Z3, Z4, Z5, Z6
READ(LUCD,6230) (KXK(I),I=1,3),ALP,BET
IF ( DIFDF .EQ. 0.0 ) DIFDF = 1.E-5
IF ( CHECK .EQ. 0.0 ) CHECK = 0.1
IF (ALP.EQ.0.0) ALP=1.0
IF (BET.EQ.0.0) BET=1.0
DO 120 I=1,3
IF(KXK(I).EQ.0) GO TO 120
DO 125 J=1,2
READ(LUCD,6240) KXN(I,J),IWAVE,DDT(I,J)
JXN = KXN(I,J)
READ(LUCD,6250) (VX(I,J,MM),MM=1,JXN)
125 CONTINUE
120 CONTINUE

```

C  
C  
C

PLOTTING DATA

```

IF ( TSTS .LT. DT ) GO TO 130
READ(LUCD,6005) IPLOT

```

## Appendix F (Continued)

```

130 CONTINUE
C
C   FRICITION FORCE
C
C   F1 = WI * F1
C
C   PRINT INPUT DATA
C
WRITE(LUPR,6030) ITI,NN,TINT,TEND,DT,TSTS,TSTP
WRITE(LUPR,6040)
WRITE(LUPR,6310) NN, HH , BB, XB(2), XB(1)
WRITE(LUPR,6060)
WRITE(LUPR,6070) NN, EM ,WI      ,EI
WRITE(LUPR,6080)
WRITE(LUPR,6090) NN, V1K ,V2K    ,V3K
WRITE(LUPR,6110)
WRITE(LUPR,6090) NN, B1K ,B2K    ,B3K
WRITE(LUPR,6120)
WRITE(LUPR,6090) NN, V1C ,V2C    ,V3C
WRITE(LUPR,6140)
WRITE(LUPR,6090) NN, B1C ,B2C    ,B3C
WRITE(LUPR,6150) NN, F1 ,F2
WRITE(LUPR,6160)
WRITE(LUPR,6170) NN,(X(J),J=1,6)
WRITE(LUPR,6320)

C
IF ( TSTS .LT. DT ) GO TO 145
NDATA = 0
DO 140 I=1,21
IF ( IPLOT(I) .EQ. 0 ) GO TO 140
WRITE(LUPR,6330) (JPLOT(J,I),J=1,5)
NDATA = NDATA + 1
140 CONTINUE
145 CONTINUE
TIM = TINT
TPLT = TSTS
TPTP = TSTP

C
C   BLOCK DISPLACEMENT PLOT DATA
C
C
HHHH = HH
BBBB = BB
IF ( TSTP .GE. DT ) WRITE( LUDP ) HHHH, BBBB

C
E(1) = FUNU0(TIM)
E(2) = FUNU1(TIM)
E(1) = PXX
E(2) = PDD
E2D = FUNU1(TIM+0.01)
E2D = PDD
E(3) = 100.*(E2D-E(2))
E(4) = FUNW0(TIM)
E(5) = FUNW1(TIM)
E(4) = UUID0
E(5) = UUID1
E5D = FUNW1(TIM+0.01)
E5D = UUID1
E(6) = 100.*(E5D-E(5))

```

## Appendix F (Continued)

```

      UB = PXX
C
C   TIME HISTORY CURVE PLOT DATA
C
      IF( TSTS .LT. DT ) GO TO 150
      WRITE(LUHT)  NN,TINT,TEND
      WRITE(LUHT)  IPLOT
      WRITE(LUHT)  TIM,E,(XWRIT(I),I=1,NDATA)
150 CONTINUE
C
C   DISPLACEMENT PLOT DATA
C
      IF( TSTP .LT. DT ) GO TO 160
      CALL DTVWST ( TIM, UB, XN, HH, BB )
160 CONTINUE
C
170 NZR = 0
      E(1) = FUNUO(TIM)
      E(2) = FUNU1(TIM)
      E(1) = PXX
      E(2) = PDD
      E2D = FUNU1(TIM+0.01)
      E2D = PDD
      E(3) = 100.*(E2D-E(2))
      E(4) = FUNWO(TIM)
      E(5) = FUNW1(TIM)
      E(4) = UUIDO
      E(5) = UUID1
      E5D = FUNW1(TIM+0.01)
      E5D = UUID1
      E(6) = 100.*(E5D-E(5))
      UB = PXX
C
      DT1 = DT
180 CALL JULY31(TIM,DT1,X,XN,N6,Q,T1)
      XDIS(3) = XN(3) - UB
      XDIS(1) = XN(1)
      XDIS(2) = XN(2)
      XDIS(4) = XN(4)
      XDIS(5) = XN(5)
      XDIS(6) = XN(6)
C
      N1 = 0
      IF(NZR.EQ.0.AND.X(1)*XN(1).LT.0.) THEN
          DT2 = DABS(X(1))/(DABS(X(1))+DABS(XN(1)))
          IF(DT2.LT.CHECK) GO TO 190
          DTXXDT=DT
          DT2 = DTXXDT *DT2
          IF(DT2.GE.DT1) GO TO 190
          DT1 = DT2
          N1 = 1
      ENDIF
190 CONTINUE
C
      IF(NZR .EQ. 1) GO TO 200
      IF(N1 .EQ. 0) GO TO 200
      N2=N1

```

## Appendix F (Continued)

```

NZR = 1
GO TO 180
C
200 CONTINUE
TIM = TIM + DT1
IF(NZR.EQ.0) GO TO 205
IF(N2.EQ.1) XN(6*N2-5) = 0.
C
205 NDATA = 0
C
C MAXIMUM VALUE SEARCH
C
CALL GREATT ( XDIS, A, WFORC )
C
IF( TSTS .LT. DT ) GO TO 210
IF( TIM .LT. TPLT ) GO TO 210
TPLT = TPLT + TSTS
DO 550 I=1,21
IF(IPLT(I).EQ.0) GO TO 550
NDATA = NDATA + 1
IF ( NDATA .GT. MAXD ) GO TO 560
IF ( I .LE. 9 ) GO TO 500
IMS9 = I-9
GO TO (601,602,603,604,605,606,607,608,609,610,611),IMS9
601 CONTINUE
XWRIT(NDATA) = FGM
GO TO 550
602 CONTINUE
XWRIT(NDATA) = FRI
GO TO 550
603 CONTINUE
XWRIT(NDATA) = FRM
GO TO 550
604 CONTINUE
XWRIT(NDATA) = VFZ
GO TO 550
605 CONTINUE
XWRIT(NDATA) = VYM
GO TO 550
606 CONTINUE
XWRIT(NDATA) = BWF
GO TO 550
607 CONTINUE
XWRIT(NDATA) = BWM
GO TO 550
608 CONTINUE
XWRIT(NDATA) = -WFORC(1)
GO TO 550
609 CONTINUE
XWRIT(NDATA) = -WFORC(2)
GO TO 550
610 CONTINUE
XWRIT(NDATA) = -WFORC(3)
GO TO 550
611 CONTINUE
XWRIT(NDATA) = -WFORC(4)
GO TO 550
C

```



## Appendix F (Continued)

```

500 CONTINUE
    THANGF = 1.0
    GO TO (501,502,521,540,503,522,504,505,523),I
501 I1 = 1
    THANGF = 180.0 / PAIPAI
                                         GO TO 510
502 I1 = 2
                                         GO TO 510
503 I1 = 4
                                         GO TO 510
504 I1 = 5
                                         GO TO 510
505 I1 = 6
510 CONTINUE
520 XWRIT(NDATA) = XN(I1) * THANGF
                                         GO TO 550
521 I1 = 2
                                         GO TO 530
522 I1 = 4
                                         GO TO 530
523 I1 = 6
530 CONTINUE
535 XWRIT(NDATA) = A(I1)
                                         GO TO 550
540 CONTINUE
545 XWRIT(NDATA) = XDIS(3)
550 CONTINUE
                                         GO TO 570
560 NDATA = MAXD
570 CONTINUE
C
C   TIME HISTORY CURVE PLOT DATA
C
C   WRITE(LUHT)  TIM,E,(XWRIT(I),I=1,NDATA)
C
CJR  WRITE(LUPR,6400) TIM
    6400 FORMAT(1H , 'TIME HISTORY DATA PLOT TIME= ', F12.5)
C
    210 CONTINUE
C
C   DISPLACEMENT PLOT DATA
C
    IF( TSTP .LT. DT ) GO TO 250
    IF( TIM .LT. TPTP ) GO TO 250
CJR  WRITE(LUPR,6410) TIM
    6410 FORMAT(1H , 'BLOCK DEFORMATION PLOT TIME= ', F12.5)
    CALL DTWST ( TIM, UB, XN, HH, BB )
    TPTP = TPTP + TSTP
    250 CONTINUE
C
    DO 260 I=1,N6
    260 X(I) = XN(I)
        UD   = X(4)
C
    IF(TIM.GT.TEND)   GO TO 300
    GO TO 170
    300 CONTINUE
C

```

## Appendix F (Continued)

```

C      TIME HISTORY CURVE PLOT DATA
C
      IF ( TSTS .LT. DT ) GO TO 310
      WRITE(LUHT)  TIM,E,(XWRIT(I),I=1,NDATA)
310  CONTINUE
C
C      DISPLACEMENT PLOT DATA
C
      IF( TSTP .LT. DT ) GO TO 320
      CALL  DTVWST ( TIM, UB, XN, HH, BB )
320  CONTINUE
C
C      PLOTTER ROUTINE
C
      CALL  BIGLK ( XDIS, A, WFORC )
      IF ( TSTS .LT. DT ) GO TO 330
      IF ( TSTP .LT. DT ) GO TO 330
      CALL  PLOTS(GHOST,1024)
      CALL  FACTOR(1.0)
C      CALL  FACTOR(0.8)
C      CALL  FACTOR(0.4)
      CALL  SYMBOL(0.0, 200.0, 4.0, ITI, 0.0, 72 )
      CALL  PLOT( 300.0, 0.0, -3 )
      CALL  PLOT( 0.0, 0.0, 666 )
      CALL  PLOT( 0.0, 0.0, 777 )
      CALL  PLOT( 0.0, 0.0, 888 )
      IF ( TSTS .GE. DT ) CALL  XYPLOT
      IF ( TSTP .GE. DT ) CALL  DFPLLOT
      CALL  PLOT( 0.0, 0.0, 999 )
330  CONTINUE
C
      WRITE(LUPR,6340)
      STOP
C
6000  FORMAT(18A4)
6005  FORMAT(10X,21I3)
6010  FORMAT(10X,10I5)
6020  FORMAT(10X,7E10.5)
6025  FORMAT(10X,I5,5X,6F10.0 )
C
6030  FORMAT(1H1,10X,'ROCKING  ',5X,18A4//5X,
1 21H1. CALCULATION SYSTEM //10X,
2 37HNO. OF MASS ,3X,I12/ 10X,
3 37HSTART TIME ,3X,F12.6/ 10X,
4 37HEND TIME ,3X,F12.6/ 10X,
5 37HTIME STEP ,3X,F12.6/ 10X,
6 37HTIME STEP FOR TIME HISTORY DATA STORE,3X,F12.6/ 10X,
7 37HTIME STEP FOR DISPLACEMENT DATA STORE,3X,F12.6 )
6040  FORMAT(1H0,///5X,12H2. DIMENSION//20X, 32HB L O C K VERTICAL
1 SPRING / 7X, 3HNO., 10X, 7HH A L H, 10X, 15HD I S T A N C E, /
2 11X, 11HH E I G H T, 2X, 9HW I D T H, 3X, 7HL E F T, 2X,
3 9HR I G H T )
6060  FORMAT(///5X,7H3. MASS//10X,11HNO. OF MASS,5X,18HMASS(KG.SEC**2/C
1M),13X,10HWEIGHT(KG),4X,19HROTATION OF INERTIA )
6070  FORMAT(I20,3E23.6)
6080  FORMAT(1H0,///,4X,12H4. STIFFNESS//7X,12H4.1 VERTICAL/10X,3HNO.,
1 11X,5HKV(1),11X,5HKV(2),11X,5HKV(3))
6090  FORMAT(I13,3E16.6)

```

## Appendix F (Continued)

```

6110 FORMAT(//7X,14H4.2 HORIZONTAL/10X,3HNO.,11X,5HKB(1),
1 11X,5HKB(2),11X,5HKB(3))
6120 FORMAT(1H0,///,4X,10H5. DAMPING//7X,12H5.1 VERTICAL/10X,3HNO.,
1 11X,5HCV(1),11X,5HCV(2),11X,5HCV(3))
6140 FORMAT(//7X,14H5.2 HORIZONTAL/10X,3HNO.,11X,5HCB(1),
1 11X,5HCB(2),11X,5HCB(3))
6150 FORMAT(1H1,4X,11H6. FRICTION//10X,9HINTERFACE,12X,4HF(1),12X,
1 4HF(2)/(I15,4X,2E16.6))
6160 FORMAT(1H0,///,4X,17H7. INITIAL STATE //10X,3HNO.,11X,5HTHETA,
1 5X,11HD-THETA/D-T,15X,1HU,9X,7HD-U/D-T,15X,1HW,9X,7HD-W/D-T)
6170 FORMAT(I13,7E16.6)
6220 FORMAT( I5, 2X, 5( 3X, 1PE11.4 ) , OP )
6230 FORMAT(10X,3I5,5X,3F10.5)
6240 FORMAT(10X,I4,6X,I1,9X,F10.0)
6250 FORMAT(10X,5F10.3)
6310 FORMAT( I10, 4(1X,F10.4) )
6320 FORMAT(1H0,///,4X,17H8. PLOTTING DATA )
6330 FORMAT(/10X,10A4)
6340 FORMAT(1H0,//////, 4X,38H*** CALCULATION NORMALLY FINISHED. ***)
END

```

```

SUBROUTINE JULY31(T,DT,XO,XN,NMAX,Q,T1)
IMPLICIT REAL*8(A-H,O-Z)
DIMENSION XO(1),XN(1),Q(1),T1(1)
COMMON/RK/ IGO,IAG,IVSG(10),IMG980(2)

```

C

```

    IGO = 0
    IAG = 0
    DO 100 I=1,10
100  IVSG(I) = 0
    DO 102 I=1,2
102  IMG980(I) = 0

```

C

```

    DO 110 N=1,NMAX
    T1(N) = DT*FUN(N,T,XO)
    XN(N) = XO(N) + 0.5*T1(N)
110  Q (N) = T1(N)
    IGO = 1
    T9 = T + DT/2.0
    DO 120 N=1,NMAX
120  T1(N) = DT*FUN(N,T9,XN)
    DO 130 N=1,NMAX
    XN(N) = XO(N) + 0.5*T1(N)
130  Q (N) = Q (N) + 2.0*T1(N)
    DO 140 N=1,NMAX
140  T1(N) = DT*FUN(N,T9,XN)
    DO 150 N=1,NMAX
    XN(N) = XO(N) + T1(N)
150  Q (N) = Q (N) + 2.0*T1(N)
    T9 = T + DT
    DO 160 N=1,NMAX
160  T1(N) = DT*FUN(N,T9,XN)
    DO 170 N=1,NMAX
170  XN(N) = XO(N) + ( T1(N) + Q(N) )/6.0
    RETURN
END

```

## Appendix F (Continued)

```

FUNCTION FUN(N,T,X)
IMPLICIT REAL*8(A-H,O-Z)
COMMON/IRIR/ XB(10),VK,VC,DK,DC,BK,BC,HH,BB,EI,EM,WI,NB,ITI(18)
COMMON/COEF/ F1, F2,
1          V1K, V2K, V3K, B1K, B2K, B3K,
2          V1C, V2C, V3C, B1C, B2C, B3C, UV
COMMON /FMFMFM/ FGM, FRI, FRM, VFZ, VYM, BWF, BWM,
1          FWF(4), FWM(4)
COMMON/RK/ IGO,IAG,IVSG(10),IMG980(2)
COMMON/XXD/A(6)
COMMON/XSDSX/ XDIS(6), UB
COMMON/CXXCXX/ CXX
COMMON /WIRE/ RWI(4), ZWI(4), ZWCI(4), WGEO(3,4), WDISP(3,2,4),
1          WCORD(3,2,4), WCORD(3,2,4), WLENGO(4), WLENG(4),
2          WFORC(4),WFCMP(3,4), WMCMP(3,4), IWSTAT(4),NWIRE
COMMON /CASK/ RCSK(2), ZCSK, WCSK, CSKI, BETA
DIMENSION X(1)
CBA = 1.0EO
IF( N .NE. 1 ) GO TO 400
BWF = 0.0
BWM = 0.0
FGM = 0.0
FRI = 0.0
FRM = 0.0
VFZ = 0.0
VYM = 0.0

C
DO 100 I=1,4
DO 100 J=1,3
WFCMP(J,I) = 0.0
WMCMP(J,I) = 0.0
100 CONTINUE

C
C      FGM MOMENT BY G
C      FRI FRICTION FORCE, VFZ V-SPRING FORCE,
C      FRM FRICTION MOMENT, VYM V-SPRING MOMENT,
C*** FRICTION FORCE
C
ALPHA = X(1)
SN1 =SSIN( X(1) )
CS1 =GCOS( X(1) )
IF(IGO.EQ.0.AND.ALPHA.LT.0.) IAG = 1
IF(IAG.EQ.1) GO TO 110
V = X(4) - ( HH*CS1 + BB*SN1 ) * X(2) - FUNU1(T)
FF =-DSIGN(CBA,V)*FRIC(F1, F2, EM, UV)
FM =-FF * ( HH*CS1 + BB*SN1 )
GO TO 120

110 CONTINUE
V = X(4) - ( HH*CS1 - BB*SN1 ) * X(2) - FUNU1(T)
FF =-DSIGN(CBA,V)*FRIC(F1, F2, EM, UV)
FM =-FF * ( HH*CS1 - BB*SN1 )

120 CONTINUE
FRI = FRI + FF
FRM = FRM + FM

C
C*** VERTICAL SPRING
C
DO 130 IV=1,NB

```

## Appendix F (Continued)

```

ETA = 0.5*( FUNWO(T) - ( X(5) - HH*( 1. - CS1 ) - XB(IV)*SN1))
IF(IGD.EQ.0.AND.ETA.LE.0.)  IVSG(IV) = 1
IF(IVSG(IV).EQ.1)  GO TO 130
ETD = 0.5*( FUNW1(T) - ( X(6) + ( HH*SN1 - XB(IV)*CS1 ) * X(2)))
VC = V1C + ETD*( V2C + ETD*V3C )
VK = V1K + ETA*( V2K + ETA*V3K )
FN = -VK*ETA - VC*ETD
IF(FN.GE.0.0)  FN = 0.0
FM = FN * ( -HH*SN1 + XB(IV)*CS1 )
VFZ = VFZ + FN
VYM = VYM + FM
130 CONTINUE
C
C*** MOMENT
C
CALL MOMNT(FGM,X)
C
C  UB = FUNBO(T)
C  UB = FUNUO(T)
C  UD = FUNB1(T)
C  UD = FUNU1(T)
CONTINUE
NFB = 0
NFR = 0
NFL = 0
VJB = 0.0
VJR = 0.0
VJL = 0.0
SN1 = SSIN( X(1) )
CS1 = GCOS( X(1) )
C
C *** LOWER RIGHT
C
XI = X(3) + BB*( CS1 - 1.0 ) - HH*SN1 - UB
IF(XI.LE.0.0)  GO TO 200
XT = X(4) - ( BB*SN1 + HH*CS1 ) * X(2) - UD
BK = B1K + XI*( B2K + XI*B3K )
BC = B1C + XT*( B2C + XT*B3C )
FB = BK*XI + BC*XT
IF(FB.LE.0.)  FB = 0.
BWF = BWF - FB
BWM = BWM + FB*( HH*CS1 + BB*SN1 )
C
C *** LOWER LEFT
C
200 XI = -( X(3) - BB*( CS1 - 1.0 ) - HH*SN1 ) + UB
IF(XI.LE.0.)  GO TO 300
XT = -X(4) - ( BB*SN1 - HH*CS1 ) * X(2) + UD
BK = B1K + XI*( B2K + XI*B3K )
BC = B1C + XT*( B2C + XT*B3C )
FB = BK*XI + BC*XT
IF(FB.LE.0.)  FB = 0.
BWF = BWF + FB
BWM = BWM - FB*( HH*CS1 - BB*SN1 )
300 CONTINUE
C
C*** WIRE DISP , FORCE
C

```

## Appendix F (Continued)

```

IF( NWIRE .EQ. 0 ) GO TO 350
CALL WIRDSP( 4, T, X, ZWCI, RCSK, ZCSK, BETA, WGEO, WDISP, WCORD,
1          WCORDO, WLENG, WLENGO, IWSTAT, WFORC, WFCMP, WMCMP,
2          IGO)
350 CONTINUE
400 CONTINUE
C
FCX = CXX*X(4)
C
C*** DERIVATIVE
C
IF(N .EQ.1) FUN = X(2)
IF(N .EQ.2) THEN
FUN = (FGM +FRM +VYM +BWM )/EI
FUN1 = 0.0
DO 500 I=1,4
FUN1= FUN1+WMCMP(2,I)/EI
500 CONTINUE
FUN = FUN + FUN1
ENDIF
IF(N .EQ.3) FUN = X(4)
IF(N .EQ.4) THEN
FUN = (FRI +BWF )/EM - FCX/EM
FUN1 = 0.0
DO 600 I=1,4
FUN1= FUN1+WFCMP(1,I)/EM
600 CONTINUE
FUN = FUN + FUN1
ENDIF
IF(N .EQ.5) FUN = X(N+1)
IF(N .EQ.6) THEN
FUN = -(VFZ +WI )/EM
FUN1 = 0.0
DO 700 I=1,4
FUN1= FUN1+WFCMP(3,I)/EM
700 CONTINUE
FUN = FUN + FUN1
ENDIF
A(N) = FUN
RETURN
END
SUBROUTINE MOMNT(FXS,X)
IMPLICIT REAL*8(A-H,O-Z)
COMMON/IRIR/ XB(10),VK(6),HH,BB,EI,EM,WI,NB,ITI(18)
DIMENSION X(1)
COMMON/RK/ IGO,IAG,IVSG(10),IMG980(2)
REAL IMG980
ALPHA = X(1)
IF(IGO.EQ.0) GO TO 180
170 IMG980(2) = ALPHA
180 IF(IMG980(2)) 190, 200, 210
190 FXS = FXS + WI * ( BB * DCOS(X(1)) + HH * DSIN(X(1)))
GO TO 220
200 FXS = FXS + WI * HH * DSIN(X(1))
GO TO 220
210 FXS = FXS - WI * ( BB * DCOS(X(1)) - HH * DSIN(X(1)))
220 CONTINUE
RETURN
END

```

## Appendix F (Continued)

```

SUBROUTINE WIRDSP
1      ( NW, T, X, ZWCI, RCSK, ZCSK, BETA, WGEO, WDISP, WCORD
2      WCORDO, WLENG, WLENGO, IWSTAT, WFORC, WFCMP, WMCMP,
3      IGO)
IMPLICIT REAL*8(A-H,O-Z)

C
DIMENSION X(1), ZWCI(1), WDISP(3,2,1), WCORDO(3,2,1), WLENGO(1),
1      WCORD(3,2,1), WLENG(1), WFORC(1), WFCMP(3,1),
2      WMCMP(3,1), WGEO(3,1), DCMP(3), IWSTAT(1),
3      SW(4), SANG(4), ALCMP(3)

C
DATA SW /          1.0,          1.0, -1.0,          -1.0 /
DATA SANG/         0.0,  1.57079632, 0.0,  1.57079632 /
DATA EPSL/         0.0/

C
SN = DSIN(X(1))
DO 10 I=1,NW
IF( IWSTAT(I) .EQ. 3 ) GO TO 10
YM = WGEO(1,I)
AR = WGEO(2,I)
SIGB = WGEO(3,I)
ZZ = ZWCI(I) - ZCSK
BANG = DABS(SANG(I) - BETA)
R2BT = RCSK*DCOS( BANG )
CS = SW(I) * (1.0-DCOS(X(1)))
DCMP(1) = ZZ*SN + R2BT*CS
DCMP(2) = 0.0
DCMP(3) = - ZZ*CS + R2BT*SN*SW(I)
WDISP(1,1,I) = X(3) + DCMP(1)
WDISP(2,1,I) = 0.0
WDISP(3,1,I) = X(5) + DCMP(3)
WDISP(1,2,I) = FUNUO(T)
WDISP(2,2,I) = 0.0
WDISP(3,2,I) = FUNWO(T)

C
AL = 0.0
DO 20 J=1,3
WCORD(J,1,I) = WCORDO(J,1,I)+WDISP(J,1,I)
WCORD(J,2,I) = WCORDO(J,2,I)+WDISP(J,2,I)
ALCMP(J) = WCORD(J,1,I) - WCORD(J,2,I)
AL = AL + ALCMP(J)**2
20 CONTINUE

C
WLENG(I) = DSQRT( AL )
DLENG = WLENG(I) - WLENGO(I)
IF( IGO .EQ. 1 .AND. IWSTAT(I) .EQ. 2 ) THEN
WFORC(I) = 0.0
IWSTAT(I) = 2
GO TO 30

ENDIF
IF( DLENG .LE. EPSL ) THEN
WFORC(I) = 0.0
IWSTAT(I) = 2
GO TO 30

ELSE
WFORC(I) = DLENG/WLENGO(I) * YM
IF( WFORC(I) .GT. SIGB ) THEN
WFORC(I) = 0.0

```

## Appendix F (Continued)

```

        IWSTAT(I) = 3
        GO TO 30
    ENDIF
    WFORC(I) = WFORC(I) * AR * (-1.0)
    IWSTAT(I) = 1
ENDIF
30 CONTINUE
    DO 40 J=1,3
        ALCMP(J) = ALCMP(J)/WLENG(I)
        WFCMP(J,I) = WFORC(I)*ALCMP(J)
40 CONTINUE
        WMCMP(1,I) = 0.0
        WMCMP(2,I) = -(WFCMP(1,I)*(WCORD(3,1,I)-(ZCSK+X(5))))
1        - WFCMP(3,I)*(WCORD(1,1,I)-X(3)))
        WMCMP(3,I) = 0.0
10 CONTINUE
    RETURN
    END

SUBROUTINE WIRINI
1        ( NW, WCORDO, WLENGO, RWI, ZWI, ZWCI, RCU, BETA)
    IMPLICIT REAL*8(A-H,O-Z)
C
    DIMENSION WCORDO(3,2,1), WLENGO(1), RWI(1), ZWI(1), ZWCI(1),
1        SFANG(4)
C
    DATA SFANG/ 3.14159265, -1.57079632, 0.0, 1.57079632 /
C
    DO 10 I=1,NW
        TH = SFANG(I) - BETA
        CS = DCOS( TH )
        SN = DSIN( TH )
        WCORDO(1,2,I) = RWI(I)* CS
        WCORDO(2,2,I) = RWI(I)* SN
        WCORDO(3,2,I) = ZWI(I)
        WCORDO(1,1,I) = RCU * CS
        WCORDO(2,1,I) = RCU * SN
        WCORDO(3,1,I) = ZWCI(I)
        AL = 0.0
        DO 20 J=1,3
            AL = AL + ( WCORDO(J,1,I) - WCORDO(J,2,I) )**2
20 CONTINUE
        WLENGO(I) = DSQRT(AL)
10 CONTINUE
    RETURN
    END

FUNCTION FRIC(F1, F2, EM, UV)
    IMPLICIT REAL*8(A-H,O-Z)
    T = UV * UV
    FRIC = F1 + 0.5 * F2 * EM * T
    RETURN
    END

```



## Appendix F (Continued)

```

FUNCTION FUNUO(T)
IMPLICIT REAL*8 (A-H,O-Z)
COMMON /AAWPPP/ A, W, P
COMMON /KIKKIK/ Z1, Z2, Z3, Z4, Z5, Z6, KIK
COMMON /FRIFRI/ FPAI
COMMON /KXKXK/ DDT(3,2), VX(3,2,1100), KXK(3), KXN(3,2)
COMMON /PDPXPD/ PX, PD, PD2, PXX, PDD, PDW2
COMMON /ALPBET/ ALP, BET

```

C

```

PAI=3.14159265359D0
IF(KXK(1).NE.0) GO TO 15
IF ( KIK .EQ. 1 ) GO TO 10
IF (KIK.EQ.2) GOTO 12
IF(KIK.EQ.3) GO TO 13
FUNUO = A * DSIN( W * T - P )
PXX=FUNUO
RETURN
10 CONTINUE
CALL FIT ( FPAI, T )
PF = 2.0 * PAI * FPAI
PF2 = PF * PF
PXX = A / PF2 * DSIN( PF * T - P )
FUNUO = PXX
RETURN
12 CONTINUE
PF = 2.0*PAI*W
PF2=PF*PF
PXX=A/PF2*DSIN(PF*T-P)
FUNUO=PXX
RETURN
13 CONTINUE
CALL FIT(FPAI,T)
PF=2.0*PAI*FPAI
PXX=A*DSIN(PF*T-P)
FUNUO=PXX
RETURN
15 CONTINUE
N = T/DDT(1,1)
FUNUO = (T-DDT(1,1)*N)*(VX(1,1,N+2)-VX(1,1,N+1))
1 /DDT(1,1)+VX(1,1,N+1)
FUNUO=ALP*FUNUO
PXX=FUNUO
RETURN

```

C

```

ENTRY FUNU1(T)
PAI=3.14159265359D0
IF(KXK(1).NE.0) GO TO 25
IF ( KIK .EQ. 1 ) GO TO 20
IF(KIK.EQ.2) GO TO 22
IF(KIK.EQ.3) GO TO 23
FUNU1 = A * W * DCOS(W*T-P)
PDD=FUNU1
RETURN
20 CONTINUE
CALL FIT ( FPAI, T )
PF = 2.0 * PAI * FPAI
PDD = A / PF * DCOS( PF * T - P )
FUNU1 = PDD

```

## Appendix F (Continued)

```

RETURN
22 CONTINUE
PF=2.0*PAI*W
PDD=A/PF*DCOS(PF*T-P)
FUNU1=PDD
RETURN
23 CONTINUE
CALL FIT(FPAI,T)
PF=2.0*PAI*FPAI
PDD=A*DCOS(PF*T-P)*PF
FUNU1=PDD
RETURN
25 CONTINUE
N = T/DDT(1,2)
FUNU1 = (T-DDT(1,2)*N)*(VX(1,2,N+2)-VX(1,2,N+1))
1 /DDT(1,2)+VX(1,2,N+1)
PDD=FUNU1
NN=(T-0.01)/DDT(1,2)
TT=T-0.01
PDW2=(TT-DDT(1,2)*NN)*(VX(1,2,NN+2)-VX(1,2,NN+1))
1 /DDT(1,2)+VX(1,2,NN+1)
FUNU1=BET*FUNU1
PDD=FUNU1
RETURN
END

FUNCTION FUNWO(T)
IMPLICIT REAL*8(A-H,O-Z)
COMMON /KXKXK/ DDT(3,2),VX(3,2,1100), KXK(3), KXN(3,2)
COMMON /UUIIDID/ UUIIDO, UUIID1
IF(KXK(3).NE.0) GO TO 15
FUNWO = 0.0
UUIIDO=FUNWO
RETURN
15 CONTINUE
N = T/DDT(3,1)
FUNWO = (T-DDT(3,1)*N)*(VX(3,1,N+2)-VX(3,1,N+1))
1 /DDT(3,1)+VX(3,1,N+1)
UUIIDO=FUNWO
RETURN
ENTRY FUNW1(T)
IF(KXK(3).NE.0) GO TO 25
FUNW1 = 0.0
UUIID1=FUNW1
RETURN
25 CONTINUE
N = T/DDT(3,2)
FUNW1 = (T-DDT(3,2)*N)*(VX(3,2,N+2)-VX(3,2,N+1))
1 /DDT(3,2)+VX(3,2,N+1)
UUIID1=FUNW1
RETURN
END

```

## Appendix F (Continued)

```

SUBROUTINE GREATT( X, A, WFORC )
IMPLICIT REAL*8(A-H,O-Z)
COMMON / GRETIT/ GFGMG, GFRIG, GFRMG, GVZG, GVYMG, GBWFG, GBWMG,
1          GMXX(6), GMAA(6), GFWF(4)
COMMON /FMFMFM/ FGM, FRI, FRM, VFZ, VYM, BWF, BWM,
1          FWF(4), FWM(4)
DIMENSION X(1), A(1), WFORC(1)
DO 100 I=1,6
GMXX(I)= DMAX1(GMXX(I),DABS( X(I)) )
100 CONTINUE
GMAA(2)= DMAX1(GMAA(2),DABS( A(2)) )
GMAA(4)= DMAX1(GMAA(4),DABS( A(4)) )
GMAA(6)= DMAX1(GMAA(6),DABS( A(6)) )
GFGMG = DMAX1( GFGMG, DABS( FGM ) )
GFRIG = DMAX1( GFRIG, DABS( FRI ) )
GFRMG = DMAX1( GFRMG, DABS( FRM ) )
GVZG = DMAX1( GVZG, DABS( VFZ ) )
GVYMG = DMAX1( GVYMG, DABS( VYM ) )
GBWFG = DMAX1( GBWFG, DABS( BWF ) )
GBWMG = DMAX1( GBWMG, DABS( BWM ) )
GFWF(1)= DMAX1(GFWF(1),DABS(WFORC(1)))
GFWF(2)= DMAX1(GFWF(2),DABS(WFORC(2)))
GFWF(3)= DMAX1(GFWF(3),DABS(WFORC(3)))
GFWF(4)= DMAX1(GFWF(4),DABS(WFORC(4)))
RETURN
ENTRY BIGLK ( X, A, WFORC )
WRITE(6,610)
GMXX(1) = 180.0 / 3.14 * GMXX(1)
WRITE(6,660) GMXX(1), GMXX(3), GMXX(5)
WRITE(6,620)
WRITE(6,660) GMXX(2), GMXX(4), GMXX(6)
WRITE(6,630)
WRITE(6,660) GMAA(2), GMAA(4), GMAA(6)
WRITE(6,640)
WRITE(6,670) GFGMG, GFRIG, GFRMG, GVZG, GVYMG, GBWFG, GBWMG
WRITE(6,650)
WRITE(6,680) GFWF(1), GFWF(2), GFWF(3), GFWF(4)
DO 200 N=1,6
GMXX(N) = 0.00
200 GMAA(N) = 0.00
DO 300 N=1,4
300 GFWF(N) = 0.00
610 FORMAT(1H1,4X,39H9. CALCULATION RESULTS (MAXIMUM VALUES)//
1      8X,16H9.1 DISPLACEMENT// 16X,13HTHETA(DEGREE),
2      13X,1HU,13X,1HW )
620 FORMAT(1H0,///,8X,12H9.2 VELOCITY,///,18X,11HD-THETA/D-T,
1      7X, 7HD-U/D-T, 7X, 7HD-W/D-T )
630 FORMAT(1H0,///,8X,16H9.3 ACCELERATION,///,18X,11HD2THETA/DT2,
1      7X, 7HD2U/DT2, 7X, 7HD2W/DT2 )
640 FORMAT(1H0,///,8X,20H9.4 FORCE AND MOMENT //, 19X, 9HMOMENT BY,
1      6X,8HFORCE BY,5X,9HMOMENT BY,6X,8HFORCE BY,
2      5X,9HMOMENT BY,6X,8HFORCE BY,5X,9HMOMENT BY, /
3      21X,7HGRAVITY,6X,8HFRICTION,6X, 8HFRICTION,
4      2(6X,8HV.SPRING),2(6X,8HH.SPRING),)
650 FORMAT(1H0,///, 8X,14H9.5 WIRE FORCE,/// 20X, 8HFORCE BY,
1      6X,8HFORCE BY,6X,8HFORCE BY,6X,8HFORCE BY, / 22X,6HWIRE-A,
2      8X,6HWIRE-B,8X,6HWIRE-C,8X,6HWIRE-D)
660 FORMAT(15X, 3( 2X, 1PE12.5 ), OP )

```

## Appendix F (Continued)

```

670 FORMAT(15X, 7( 2X, 1PE12.5 ), OP )
680 FORMAT(15X, 4( 2X, 1PE12.5 ), OP )
RETURN
END

```

```

SUBROUTINE FIT ( F, T )
IMPLICIT REAL*8(A-H,O-Z)
COMMON /AAWWPP/ A, W, P
COMMON /KIKKIK/ Z1,Z2,Z3,Z4,Z5,Z6,KIK
F = W + Z1*T + Z2*T*T + Z3*T**3 + Z4*T**4 + Z5*T**5 + Z6*T**6
RETURN
END

```

```

FUNCTION SSIN(X)
IMPLICIT REAL*8(A-H,O-Z)
SSIN = X*(1.0-(1.0-X*X/20.0)*X*X/6.0)
RETURN
END

```

```

FUNCTION GCOS(X)
IMPLICIT REAL*8(A-H,O-Z)
GCOS = 1.0-X*X*(1.0-X*X/12.0)*0.5
RETURN
END

```

```

SUBROUTINE ZEROCL
COMMON /B/ BB(58940)
COMMON /C/ IUWT(3,2),IPLTT(21), CC(63)
CHARACTER*20 IPLTT
DO 10 N=1,58940
10 BB(N)=0.0
DO 20 N=1,63
20 CC(N)=0.0
RETURN
END

```

```

SUBROUTINE DTWST( TIM, UB, XN, HH, BB )
IMPLICIT REAL*8 (A-H,O-Z)
REAL*4 S,T,STEP,TMM,US,X(6)
COMMON/LUNITL/ LUCD, LUHT, LUDP, LUPR
DIMENSION XN(1)
TMM = TIM
US = UB
DO 100 N=1,6
100 X(N) = XN (N)
STEP = 12.0 + 20.0 * BB / HH
FACT = 80.0 / HH
S = 4.0 * STEP
T = FUNWO(TIM) * FACT
C UO = FUNBO(TIM)
UO = FUNUO(TIM)
WRITE(LUDP) TMM, US, S, T, (X(I),I=1,6)
RETURN
END

```

## Appendix F (Continued)

```

C*****C
C
C      SUBROUTINE DF PLOT
C
C      PROGRAM NAME - ROCKING-DISPLACEMENT-PLOT
C
C*****C
      DIMENSION X(6)
      DATA XORG, YORG/ 140.0, 20.0 /
      COMMON /LUNITL/ LUCD, LUHT, LUDP, LUPR
      REWIND LUDP
      READ(LUDP,END=200) HH, BB
      STEP = 12.0 + 20.0 * BB / HH
      FACT = 80.0 / HH
100  CONTINUE
      READ(LUDP,END=200) TIME, UB, S, T, (X(I),I=1,6)
      XXX = 100.0
      CALL SYMBOL( XXX, 190.0, 4.0, 6HTIME =, 0.0, 6 )
      XXX = XXX + 24.0
      CALL NUMBER( XXX, 190.0, 4.0, TIME, 0.0, 3 )
      XXX = XXX + 26.0
      CALL SYMBOL( XXX, 190.0, 4.0, 5H(SEC), 0.0, 5 )
      CALL PLOT(XORG-S,YORG+T,3)
      CALL PLOT(XORG+S,YORG+T,2)
C      CX = (X(3)-UB)*10.*FACT + XORG
C      CY = (HH + 10.*X(5))*FACT + YORG
C      ST = SIN(10.*X(1))
C      CT = COS(10.*X(1))
      CX = (X(3)-UB)* FACT + XORG
      CY = (HH + X(5))*FACT + YORG
      ST = SIN( X(1))
      CT = COS( X(1))
      X1 = HH*ST + BB*CT
      X2 = HH*ST - BB*CT
      Y1 = HH*CT - BB*ST
      Y2 = HH*CT + BB*ST
      SO = CX + X1*FACT
      TO = CY + Y1*FACT
      CALL PLOT(SO,TO,3)
      S1 = CX + X2*FACT
      T1 = CY + Y2*FACT
      CALL PLOT(S1,T1,2)
      S1 = CX - X1*FACT
      T1 = CY - Y1*FACT
      CALL PLOT(S1,T1,2)
      S1 = CX - X2*FACT
      T1 = CY - Y2*FACT
      CALL PLOT(S1,T1,2)
      CALL PLOT(SO,TO,2)
      CALL PLOT( 0.0, 0.0, 3 )
      CALL PLOT( 10.0*STEP, 0.0, -3 )
      CALL PLOT( 0.0,0.0, 666 )
      CALL PLOT( 0.0,0.0, 777 )
      CALL PLOT( 0.0,0.0, 888 )
      GO TO 100
200  CONTINUE
      RETURN
      END

```

Appendix F (Continued)

```

CCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCC
SUBROUTINE XYPLOT
C
C   ROCKING CODE TIME HISTORY CURVE PLOT
C
C   COMMON / A/ DATA RECORD 1.
C       N       - BLOCK SU.
C       TO      - TIME (FIRST).
C       T1      - TIME (LAST).
C       IPL     - PLOT SELECT POINT
C   COMMON / B/ DATA RECORD 2.
C       T       - TIME
C       U,U1,U2 - JISHIN-YOKO DISP , VELO , ACCELE .
C       W,W1,W2 - JISHIN-TATE - , - , - .
C       PLT1    - BLOCK PLOT DATA FIRST.
C       PLT2    - BLOCK PLOT DATA SECOND.
C       PLT3    - BLOCK PLOT DATA THIRD.
C   COMMON / C/
C       IUWT    - SUB.UWPLOT TITLE AREA.
C       IPLTT   - SUB.BLKPLOT TITLE AREA.
C       IDVA    - SUB.TITLE AREA.
C       P-MAX   - PLT-MAX
C       P-MIN   - PLT-MIN
C       P-WIDE  PLOT BLOCKS MAX WIDE.
C
C   DIMENSION AREA.
C       TEMP    PLT1 READ TEMPORARY AREA.
C       NPL     PLOT SELECT CONTROL AREA.
C
C   SUBROUTINE UWPLOT
C       TATE,YOKO JISIN PLOT.
C   SUBROUTINE BLKPLOT
C       BLOCKS MASS POINT YURE PLOT.
C
C   SUBROUTINE MEMOMIN
C       BLKPLOT Y-JIKUZAHYO MIN
C   SUBROUTINE MEMOMAX
C       BLKPLOT Y-JIKUZAHYO MAX
C   SUBROUTINE UMMIN
C       UWPLOT Y-JIKUZAHYO MIN
C   SUBROUTINE UMMAXIKUZAHYO MIN
C       UWPLOT Y-JIKUZAHYO MAX
C   SUBROUTINE MLOG
C       SHISU KEISAN
C   SUBROUTINE RNUMB
C       SUJI MIGIZUME PLOT
C
CCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCC
COMMON / A/ N,TO,T1,IPL(21)
COMMON / B/ T(2105),U(2105),U1(2105),U2(2105),W(2105),W1(2105),
1 W2(2105),PLT1(21,2105)
COMMON / C/ IUWT(3,2),IPLTT(21), P1MAX(21),
1 P1MIN(21),P1WIDE(21)
COMMON / D/ IPLT2,FIPLT2
COMMON /LUNITL/ LUCD, LUHT, LUDP, LUPR
CHARACTER*20 IPLTT
REAL*8 TDPO, TDP1, TDP, UDP, UDP1, UDP2, WDP, WDP1, WDP2, TEMP

```

## Appendix F (Continued)

```

DIMENSION TEMP(21),NPL(21)
DATA IUWT/'U  ','U1  ','U2  ','W  ','W1  ','W2  '/
DATA (IPLTT(J),J=1,9) /
1  'THETA - (DEGREE)      ',
2  'THETA - VELOCITY     ',
3  'THETA - ACCELERATION',
4  '  U - DISPLACEMENT',
5  '  U - VELOCITY       ',
6  '  U - ACCELERATION',
7  '  W - DISPLACEMENT',
8  '  W - VELOCITY       ',
9  '  W - ACCELERATION'//
DATA (IPLTT(J),J=10,21) /
1  'MOMENT BY GRAVITY     ',
2  'FORCE BY FRICTION    ',
3  'MOMENT BY FRICTION   ',
4  'FORCE BY V.SPRING    ',
5  'MOMENT BY V.SPRING   ',
6  'FORCE BY B.WALL      ',
7  'MOMENT BY B.WALL     ',
8  'FORCE BY WIRE-A      ',
9  'FORCE BY WIRE-B      ',
A  'FORCE BY WIRE-C      ',
B  'FORCE BY WIRE-D      ',
C  '                      '//

```

```

C
100 DO 100 I=1,21
    TEMP(I)=0.0
    CALL ZEROCL
    FIPLT2=200.0
    REWIND LUHT
    READ(LUHT,END=180) N, TDPO, TDP1
    READ(LUHT) NPL

```

```

C
C   - PLOT DATA SELECT POINT SET (IPL) -
C

```

```

J=1
DO 110 I=1,21
  IF(NPL(I).EQ.0) GO TO 110
  IPL(J)=I
  NDATA = J
  J=J+1
110 CONTINUE
  UMAX=0.
  UMIN=0.
  U1MAX=0.
  U1MIN=0.
  U2MAX=0.
  U2MIN=0.
  WMAX=0.
  WMIN=0.
  W1MAX=0.
  W1MIN=0.
  W2MAX=0.
  W2MIN=0.
  P1MAXX=0.

```

```

C
C   ... PLOT DATA READ ...

```

## Appendix F (Continued)

```

C
  II = 0
120 CONTINUE
  II = II + 1
  IF(II.EQ.2101) GO TO 180
  READ(LUHT,END=180) TDP, UDP, UDP1, UDP2, WDP, WDP1, WDP2 ,
1    (TEMP(I),I=1,NDATA)
  T(II) = TDP
  U(II) = UDP
  U1(II) = UDP1
  U2(II) = UDP2
  W(II) = WDP
  W1(II) = WDP1
  W2(II) = WDP2

C
C   - PLOT DATA MOVE -
C
  DO 140 I=1,NDATA
  PLT1(I,II)=TEMP(I)
140 CONTINUE

C
C   - MAX . MIN -
C
  IF( U(II).GT.UMAX )      UMAX=U(II)
  IF( U(II).LT.UMIN )      UMIN=U(II)
  IF( U1(II).GT.U1MAX )    U1MAX=U1(II)
  IF( U1(II).LT.U1MIN )    U1MIN=U1(II)
  IF( U2(II).GT.U2MAX )    U2MAX=U2(II)
  IF( U2(II).LT.U2MIN )    U2MIN=U2(II)
  IF( W(II).GT.WMAX )      WMAX=W(II)
  IF( W(II).LT.WMIN )      WMIN=W(II)
  IF( W1(II).GT.W1MAX )    W1MAX=W1(II)
  IF( W1(II).LT.W1MIN )    W1MIN=W1(II)
  IF( W2(II).GT.W2MAX )    W2MAX=W2(II)
  IF( W2(II).LT.W2MIN )    W2MIN=W2(II)

C
  DO 150 I=1,NDATA
  IF(PLT1(I,II).GT.P1MAX(I))      P1MAX(I)=PLT1(I,II)
  IF(PLT1(I,II).LT.P1MIN(I))      P1MIN(I)=PLT1(I,II)
150 CONTINUE

C
  IF ( T(II) .GE. TDP1 ) GO TO 180
  GO TO 120
180 CONTINUE

C
C   CHECK WRITE
C
  WRITE(LUPR,6000) UMAX, UMIN
  WRITE(LUPR,6100) U1MAX, U1MIN
  WRITE(LUPR,6200) U2MAX, U2MIN
  WRITE(LUPR,6300) WMAX, WMIN
  WRITE(LUPR,6400) W1MAX, W1MIN
  WRITE(LUPR,6500) W2MAX, W2MIN
6000 FORMAT(1H1,3X,17H10. PLOTTING DATA //
1    8X,25HHORIZONTAL DISPLACEMENT ,11H MAX ,MIN ,2E15.7,/)
6100 FORMAT(8X,25HHORIZONTAL VELOCITY ,11H MAX ,MIN ,2E15.7,/)
6200 FORMAT(8X,25HHORIZONTAL ACCELERATION ,11H MAX ,MIN ,2E15.7,/)
6300 FORMAT(8X,25HVERTICAL DISPLACEMENT ,11H MAX ,MIN ,2E15.7,/)

```



## Appendix F (Continued)

```

6400 FORMAT(8X,25HVERTICAL VELOCITY ,11H MAX ,MIN ,2E15.7,/)
6500 FORMAT(8X,25HVERTICAL ACCELERATION ,11H MAX ,MIN ,2E15.7,/)
C
C CHECK WRITE
C
CJR WRITE(LUPR,6600) II,T(II)
6600 FORMAT(1H , 5X, 7HCOUNT =, I4, 10X, 10HLASTTIME =, F10.5)
DO 190 I=1,NDATA
WRITE(LUPR,6700) IPLTT(IPL(I)),P1MAX(I),P1MIN(I)
190 CONTINUE
6700 FORMAT(11X,A20,2X,11H MAX ,MIN ,2E15.7,/)
DO 200 I=1,NDATA
PPP = ABS(P1MAX(I))
IF(PPP.LT.ABS(P1MIN(I))) PPP = ABS(P1MIN(I))
P1MAX(I) = PPP
P1MIN(I) = -PPP
200 CONTINUE
C
C - PLOTS -
C
CALL PLOT(0.0,0.0,-3)
C
C - DATA SCALING -
C .. T ..
C
T(II+2)=T(II+1)
III=II+2
C
CALL SCALE(T,FIPLT2,III,1,10.0)
DO 210 K=1,II
210 T(K)=T(K)/T(II+4)
C
C ... SUBROUTINE UWPLLOT SET AND CALL ...
C
UWIDE = ABS(UMAX - UMIN)
U1WIDE = ABS(U1MAX - U1MIN)
U2WIDE = ABS(U2MAX - U2MIN)
WWIDE = ABS(WMAX - WMIN)
W1WIDE = ABS(W1MAX - W1MIN)
W2WIDE = ABS(W2MAX - W2MIN)
C
UU=ABS(UMAX)+ABS(UMIN)+ABS(U1MAX)+ABS(U1MIN)+ABS(U2MAX)+ABS(U2MIN)
IF(UU.EQ.0.0) GO TO 400
C
C - DATA SCALING -
C .. U ..
C
IF(UWIDE.EQ.0.0) GO TO 230
TKK= 20.0/UWIDE
DO 240 I=1,II
240 U(I)= TKK* ABS(U(I)-UMIN)
GO TO 250
230 DO 260 I=1,II
260 U(I)= 10.0
250 IF(U1WIDE.EQ.0.0) GO TO 280
TKK= 20.0/U1WIDE
DO 270 I=1,II

```

## Appendix F (Continued)

```

270 U1(I)= TKK* ABS(U1(I)-U1MIN)
    GO TO 300
280 DO 290 I=1,II
290 U1(I)= 10.0
300 IF(U2WIDE.EQ.0.0) GO TO 310
    TKK= 20.0/U2WIDE
    DO 320 I=1,II
320 U2(I)= TKK* ABS(U2(I)-U2MIN)
    GO TO 340
310 DO 330 I=1,II
330 U2(I)= 10.0
340 CONTINUE
C
C   - U PLOT -
C
    IC=1
    CALL UWPLLOT(UMAX,UMIN,U1MAX,U1MIN,U2MAX,U2MIN,UWIDE,U1WIDE,U2WIDE,
1              IC,II)
C
400 WW=ABS(WMAX)+ABS(WMIN)+ABS(W1MAX)+ABS(W1MIN)+ABS(W2MAX)+ABS(W2MIN)
    IF(WW.EQ.0.0) GO TO 600
C   - DATA SCALING -
C   .. W ..
C
    IF(WWIDE.EQ.0.0) GO TO 420
    TKK= 20.0/WWIDE
    DO 410 I=1,II
410 W(I)= TKK* ABS(W(I)-WMIN)
    GO TO 440
420 DO 430 I=1,II
430 W(I)= 10.0
440 IF(W1WIDE.EQ.0.0) GO TO 460
    TKK= 20.0/W1WIDE
    DO 450 I=1,II
450 W1(I)=TKK* ABS(W1(I)-W1MIN)
    GO TO 480
460 DO 470 I=1,II
470 W1(I)= 10.0
480 IF(W2WIDE.EQ.0.0) GO TO 500
    TKK= 20.0/W2WIDE
    DO 490 I=1,II
490 W2(I)= TKK* ABS(W2(I)-W2MIN)
    GO TO 520
500 DO 510 I=1,II
510 W2(I)= 10.0
520 CONTINUE
C
C   - W PLOT -
C
    IC=2
    CALL UWPLLOT(WMAX,WMIN,W1MAX,W1MIN,W2MAX,W2MIN,WWIDE,W1WIDE,W2WIDE,
1              IC,II)
C
600 CONTINUE
C
C ... SUBROUTINE BLKPLOT SET AND CALL ...
C
    DO 650 I=1,NDATA

```

## Appendix F (Continued)

```

IC = IPL(I)
IF( IC .EQ. 0 ) GO TO 650
P1MAXX = 0.0
P1WIDE(I) = ABS(P1MAX(I) - P1MIN(I))
IF(P1WIDE(I).GT.P1MAXX) P1MAXX = P1WIDE(I)
CALL BLKPLT( I, P1MAXX, IC, II )
650 CONTINUE
RETURN
END

SUBROUTINE UWPLOT(VMAX,VMIN,V1MAX,V1MIN,V2MAX,V2MIN,
1 VWIDE,V1WIDE,V2WIDE,IC,II)
COMMON / A/ N,TO,T1,IPL(21)
COMMON / B/ T(2105),U(2105),U1(2105),U2(2105),W(2105),W1(2105),
1 W2(2105),PLT1(21,2105)
COMMON / C/ IUWT(3,2),IPLTT(21), P1MAX(21),
1 P1MIN(21),P1WIDE(21)
CHARACTER*20 IPLTT
COMMON / D/ IPLT2,FIPLT2

C
C - U.W TITLE PLOT -
C
YY=167.5
DO 100 I=1,3
YY=YY-30.0
CALL SYMBOL(10.0,YY,5.0,IUWT(I,IC),0.0,3)
100 CONTINUE

C
C - D.V.A PLOT -
C
YY=183.5
DO 200 I=4,6
YY=YY-30.0
CALL SYMBOL( 33.0,YY,3.0,IPLTT(I)(9:20),0.0,12)
200 CONTINUE

C
C X-AXIS PLOT
C
CALL AXIS(30.0,70.0,10HTIME(SEC) , -10,FIPLT2,0.0,T(II+3),
1 T(II+4),10.0)
YY=40.0
DO 300 I=1,3
YY=YY+30.0
CALL PLOT(29.0,YY,3)
CALL PLOT(30.0,YY,2)
CALL PLOT(30.0,YY+20.0,2)
CALL PLOT(29.0,YY+20.0,2)
CALL PLOT(30.0,YY+10.0,3)
CALL PLOT(FIPLT2+30.0,YY+10.0,2)
300 CONTINUE

C
C .. U2,W2 PLOT ..
C
IF(V2WIDE.EQ.0.0) GO TO 400
CALL UMIN(V2MIN,70.0)
CALL UMAX(V2MAX,87.0)
GO TO 450

```

## Appendix F (Continued)

```

400 CALL NUMBER(25.0,79.0,2.0,V2WIDE,0.0,-1)
450 CONTINUE
C
C   .. U1,W1 PLOT ..
C
IF(V1WIDE.EQ.0.0) GO TO 500
CALL UMMIN(V1MIN,100.0)
CALL UMMAX(V1MAX,117.0)
GO TO 550
500 CALL NUMBER(25.0,109.0,2.0,V1WIDE,0.0,-1)
550 CONTINUE
C
C   .. U,W PLOT ..
C
IF (VWIDE.EQ.0.0) GO TO 600
CALL UMMIN(VMIN,130.0)
CALL UMMAX(VMAX,147.0)
GO TO 650
600 CALL NUMBER(25.0,139.0,2.0,VWIDE,0.0,-1)
650 CONTINUE
C
C   - U.W PLOT SELECT -
C
IIKK=II-1
IF(IC.EQ.2) GO TO 760
C
CALL PLOT(30.0,80.0,3)
DO 700 I=1,IIKK
CALL PLOT(T(I+1)+30.0,70.0+U2(I),2)
700 CONTINUE
CALL PLOT(T(I+1)+30.0,70.0+U2(I),3)
CALL PLOT(30.0,110.0,3)
DO 720 I=1,IIKK
CALL PLOT(T(I+1)+30.0,100.0+U1(I),2)
720 CONTINUE
CALL PLOT(T(I+1)+30.0,100.0+U1(I),3)
CALL PLOT(30.0,140.0,3)
DO 740 I=1,IIKK
CALL PLOT(T(I+1)+30.0,130.0+U(I),2)
740 CONTINUE
CALL PLOT(T(I+1)+30.0,130.0+U(I),3)
GO TO 900
C
760 CONTINUE
C
C   .. W2 PLOT ..
C
CALL PLOT(30.0,80.0,3)
DO 800 I=1,IIKK
CALL PLOT(T(I+1)+30.0,70.0+W2(I),2)
800 CONTINUE
CALL PLOT(T(I+1)+30.0,70.0+W2(I),3)
CALL PLOT(30.0,110.0,3)
DO 820 I=1,IIKK
CALL PLOT(T(I+1)+30.0,100.0+W1(I),2)
820 CONTINUE
CALL PLOT(T(I+1)+30.0,100.0+W1(I),3)
CALL PLOT(30.0,140.0,3)

```

## Appendix F (Continued)

```

DO 840 I=1,IKK
CALL PLOT(T(I+1)+30.0,130.0+W(I),2)
840 CONTINUE
CALL PLOT(T(I+1)+30.0,130.0+W(I),3)
C
900 CONTINUE
C
CALL PLOT(400.0,0.0,-3)
CALL PLOT(0.0,0.0,666)
CALL PLOT(0.0,0.0,777)
CALL PLOT(0.0,0.0,888)
RETURN
END

SUBROUTINE BLKPLT(IJUN, PWMAX, IC, II )
COMMON / A/ N,TO,T1,IPL(21)
COMMON / B/ T(2105),U(2105),U1(2105),U2(2105),W(2105),W1(2105),
1 W2(2105),PLT1(21,2105)
COMMON / C/ IUWT(3,2),IPLTT(21), P1MAX(21),
1 P1MIN(21),P1WIDE(21)
CHARACTER*20 IPLTT
COMMON / D/ IPLT2,FIPLT2

C
C .. TITLE PLOT ..
C
XX=30.0
CALL SYMBOL(XX,200.0,5.0,IPLTT(IC),0.0,20)

C
C .. X-AXIS PLOT ..
C
CALL AXIS(30.0,30.0,10HTIME(SEC) , -10,FIPLT2,0.0,T(II+3),
1 T(II+4),10.0)
C
YY=30.0
ANN=60.0
ANH=60.0/2.0
AN= ANN
CALL PLOT(29.0,YY,3)
CALL PLOT(30.0,YY,2)
CALL PLOT(30.0,YY+AN,2)
CALL PLOT(29.0,YY+AN,2)
CALL PLOT(30.0,YY+ANH,3)
CALL PLOT(FIPLT2+30.0,YY+ANH,2)
YY=YY+ANN
CALL PLOT(30.0,YY,3)

C
C .. Y-AXIS PLOT ..
C
YY=30.0
TK=ANN/PWMAX
IF(P1WIDE(IJUN).EQ.0.0) GO TO 100
PMAN= (P1MIN(IJUN)+P1WIDE(IJUN)/2.0) - (PWMAX/2.0)
CALL MEMMIN( PMAN, YY )
PMAN= (P1MIN(IJUN)+P1WIDE(IJUN)/2.0) + (PWMAX/2.0)
CALL MEMMAX( PMAN, YY, ANN, ANH )
GO TO 200
100 CALL NUMBER(25.0,YY+ANH-1.0,2.0,P1WIDE(IJUN),0.0,-1)
200 CALL PLOT(30.0,YY+ANH,3)

```

## Appendix F (Continued)

```

C
C .. CURVE PLOT ..
C
      IIKK=II-1
      DO 300 J=1,IKK
      IF(P1WIDE(IJUN).EQ.0.0) GO TO 320
      WNN= ANN * P1WIDE(IJUN) / PWMAX
      IF( WNN.NE.ANN )      GO TO 340
      PN = 0.0
      GO TO 360
340  PN= (ANN-WNN) / 2.0
      GO TO 360
320  PN=ANH
360  PLT1(IJUN,J)=ABS(PLT1(IJUN,J)-P1MIN(IJUN))
      PLY= TK * PLT1(IJUN,J)
      CALL PLOT(T(J+1)+30.0,YY+PN+PLY,2)
300  CONTINUE
      YY=YY+ANN
      CALL PLOT(T(J+1)+30.0,YY+PN+PLY,3)
C
      CALL PLOT(400.0,0.0,-3)
      CALL PLOT(0.0,0.0,666)
      CALL PLOT(0.0,0.0,777)
      CALL PLOT(0.0,0.0,888)
      RETURN
      END

      SUBROUTINE UMMAX(VMAN,YY)
      CALL MLOG(VMAN,IMN)
      CALL RNUMB(12.0,YY,2.0,VMAN,0.0,2)
      CALL SYMBOL(15.0,YY,2.0,3H*10,0.0,3)
      CALL NUMBER(22.0,YY+1.0,1.5,FLOAT(IMN),0.0,-1)
      RETURN
      END

      SUBROUTINE UMMIN(VMAN,YY)
      CALL MLOG(VMAN,IMN)
      CALL RNUMB(12.0,YY,2.0,VMAN,0.0,2)
      CALL SYMBOL(15.0,YY,2.0,3H*10,0.0,3)
      CALL NUMBER(22.0,YY+1.0,1.5,FLOAT(IMN),0.0,-1)
      RETURN
      END

      SUBROUTINE MEMMAX(PMAN, YY, ANN, ANH )
      CALL MLOG(PMAN,IMN)
      CALL RNUMB(12.0,YY+ANN-3.0,2.0,PMAN,0.0,2)
      CALL SYMBOL(15.0,YY+ANN-3.0,2.0,3H*10,0.0,3)
      CALL NUMBER(22.0,YY+ANN-1.5,1.5,FLOAT(IMN),0.0,-1)
      CALL PLOT(30.0,YY+ANH,3)
      RETURN
      END

```

## Appendix F (Continued)

```

SUBROUTINE MEMMIN( PMAN, YY )
CALL MLOG(PMAN,IMN)
CALL RNUMB(12.0,YY,2.0,PMAN,0.0,2)
CALL SYMBOL(15.0,YY,2.0,3H*10,0.0,3)
CALL NUMBER(22.0,YY+1.0,1.5,FLOAT(IMN),0.0,-1)
RETURN
END

```

```

SUBROUTINE RNUMB(X,Y,H,PMAN,ANG,NC)
APP=ABS(PMAN)
IF(APP.GE.1) GO TO 100
IKK=2+NC
GO TO 200
100 IKK=INT(ALOG10(APP)+2.00001+NC)
200 IF(PMAN.LT.0.0) IKK=IKK+1
DST=IKK*H*6./7.
XN= X- DST*COS(ANG*0.01745)
YN= Y- DST*SIN(ANG*0.01745)
CALL NUMBER(XN,YN,H,PMAN,ANG,NC)
RETURN
END

```

```

SUBROUTINE DTLIST(LU1,LU2)
DIMENSION IA(20)
REWIND LU1
N = 1
L = 51
15 IF ( L .LE. 50 ) GO TO 30
20 WRITE(LU2,2)
WRITE(LU2,3) ( I, I=1,8 )
WRITE(LU2,4)
L = 1
30 READ(LU1,1,END=50) ( IA(I),I=1,20 )
WRITE(LU2,5) N,( IA(I),I=1,20 ),N
IF ( L .NE. 50 ) GO TO 40
WRITE(LU2,6)
WRITE(LU2,10) ( I, I=1,8 )
WRITE(LU2,7)
40 L = L + 1
N = N + 1
GO TO 15
50 CONTINUE
WRITE(LU2,6)
WRITE(LU2,10) ( I, I=1,8 )
WRITE(LU2,8)
WRITE(LU2,9) LU1
REWIND LU1
1 FORMAT( 20A4 )
2 FORMAT( 1H1, //, 50X, ' INPUT DATA ECHO ' / )
3 FORMAT( 16X, 'DATA ', 4X, 8( 9X, I1 ) )
4 FORMAT( 14X, 'SEQ. NO.', 3X, 8('----5----0'), / )
5 FORMAT( 16X, I4, 5X, 20A4, 2X, I4 )
6 FORMAT( 1H0, 24X, 8('----5----0') )

```

```
7 FORMAT(1H0, 30X, '* * * CONTINUE * * *' )
8 FORMAT(1H0, 30X, '* * * INPUT DATA END * * *' )
9 FORMAT(1H0,30X,'* * * INPUT DATA FROM FILE NO. =',I3,' * * *' )
10 FORMAT( 25X, 8(9X,I1) )
11 FORMAT(1H0)
RETURN
END
```