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IMPACLIB:  
A MATERIAL PROPERTY DATA LIBRARY FOR IMPACT ANALYSIS  
OF RADIOACTIVE MATERIAL TRANSPORT CASKS

December 1997

Takeshi IKUSHIMA

日本原子力研究所  
Japan Atomic Energy Research Institute

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IMPACLIB: A Material Property Data Library for Impact  
Analysis of Radioactive Material Transport Casks

Takeshi IKUSHIMA

Department of Fuel Cycle Safety Research  
Nuclear Safety Research Center  
Tokai Research Establishment  
Japan Atomic Energy Research Institute  
Tokai-mura, Naka-gun, Ibaraki-ken

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The paper describes the structural data library and graphical program for impact and stress analyses of radioactive material transport casks. Four kinds of material data, structure steels, stainless steels, leads and woods are compiled. These materials are main structural elements of casks. Structural data such as, coefficient of thermal expansion, modulus of longitudinal elasticity, modulus of transverse elasticity, Poisson's ratio and stress-strain relationship have been tabulated.

Main features of IMPACLIB are as follows:

- (1) data have been tabulated against temperature or strain rate,
- (2) thirteen kinds of polynominal fitting for stress-strain curve are available,
- (3) it is capable of graphical representations for structural data and
- (4) the IMPACLIB is able to be used on not only main frame computers but also work stations (OS UNIX) and personal computers (OS Windows 3.1).

In the paper, brief illustration of data library is presented in the first section. The second section presents descriptions of structural data. The third section provides a user's guide for computer program and input data for the IMPACLIB.

Keywords: Computer Program, Data library, Structural Data, Stress Analysis,  
Impact Analysis, Drop Impact, Transport Cask, Cask

IMPACLIB：放射性物質輸送容器の衝突解析用  
材料物性データライブラリー

日本原子力研究所東海研究所安全性試験研究センター燃料サイクル安全工学部  
幾島 肇

(1997年11月5日受理)

本報告書は放射性物質輸送容器の落下や衝突解析に必要な材料の衝撃特性データ、ならびに応力解析に必要なデータのライブラリーおよびその図形処理プログラム IMPACLIBについてまとめたものである。データライブラリーに含まれる材料の種類は、輸送容器の主要構成材料である構造用鋼、ステンレス鋼、鉛および木材である。材料データの種類は熱膨張率、綫弾性係数、横弾性係数、ポアソン比および応力-ひずみ特性である。

IMPACLIBの主要な特徴は次の通りである。

- (1) データは温度の関数あるいはひずみ速度の関数として与えられている。
- (2) 応力-ひずみ特性に関して13種類の近似式で表示できる。
- (3) データは図表で表示できる。
- (4) 大型計算機以外にもワークステーション (OS UNIX) およびパーソナルコンピュータ (OS Windows 3.1) によっても使用できる。

本報告書はデータライブラリーの説明、IMPACLIBプログラムおよび入力データ等のユーザガイドについて記述したものである。

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## 1 . Introduction

In the drop impact and stress analyses for radioactive transport casks, it has become possible to perform them in detail by using interaction evaluation, computer programs, such as DYNA2D<sup>(1)</sup>, DYNA3D<sup>(2)</sup>, NIKE2D<sup>(3)</sup>, NIKE3D<sup>(4)</sup>, PISCES<sup>(5)</sup> and HONDO<sup>(6)</sup>. Availability of these computer programs, makes it possible to accurately solve large numbers of problems involving a wide variety of material data provided that accurate input data are used. The structural properties of the materials, including coefficient of thermal expansion, modulus of longitudinal elasticity, modulus of transverse elasticity, Poisson's ratio and stress-strain relationship (temperature and/or strain rate dependent data) should be known as accurately as possible. Some of these properties are difficult to measure. In particular, stress-strain relationships may vary from data to data depending on test methods. Therefore, when used in calculations, the possible inaccuracy of variability of structural data should be accounted for to properly interpret the results. For this reason, we have made an effort to collect stress-strain data and make it available in a form convenient for handling by computer.

Four kinds of materials data, structure steels (mild steel or carbon steel), stainless steels, leads and woods have been compiled, and are summarized in this report. The structural data library IMPACLIB (one computer program of CASKET<sup>(7)-(19)</sup> code system as shown in Fig. 1.1) for impact and stress analyses has been developed.

Main features of the computer program IMPACLIB are as follows;

(1) data have been tabulated against temperature or strain rate,

(2) thirteen kinds of polynomial fitting functions for stress-strain curve are available,

(3) it is capable of graphical representations for structural data and

(4) the IMPACLIB is able to be used on not only main frame computers but also work stations (OS UNIX) and personal computers (OS Windows 3.1).

In the paper, brief illustration of data library is presented in the first section. The second section presents descriptions of structural data. The third section provides a user's guide for the IMPACLIB.

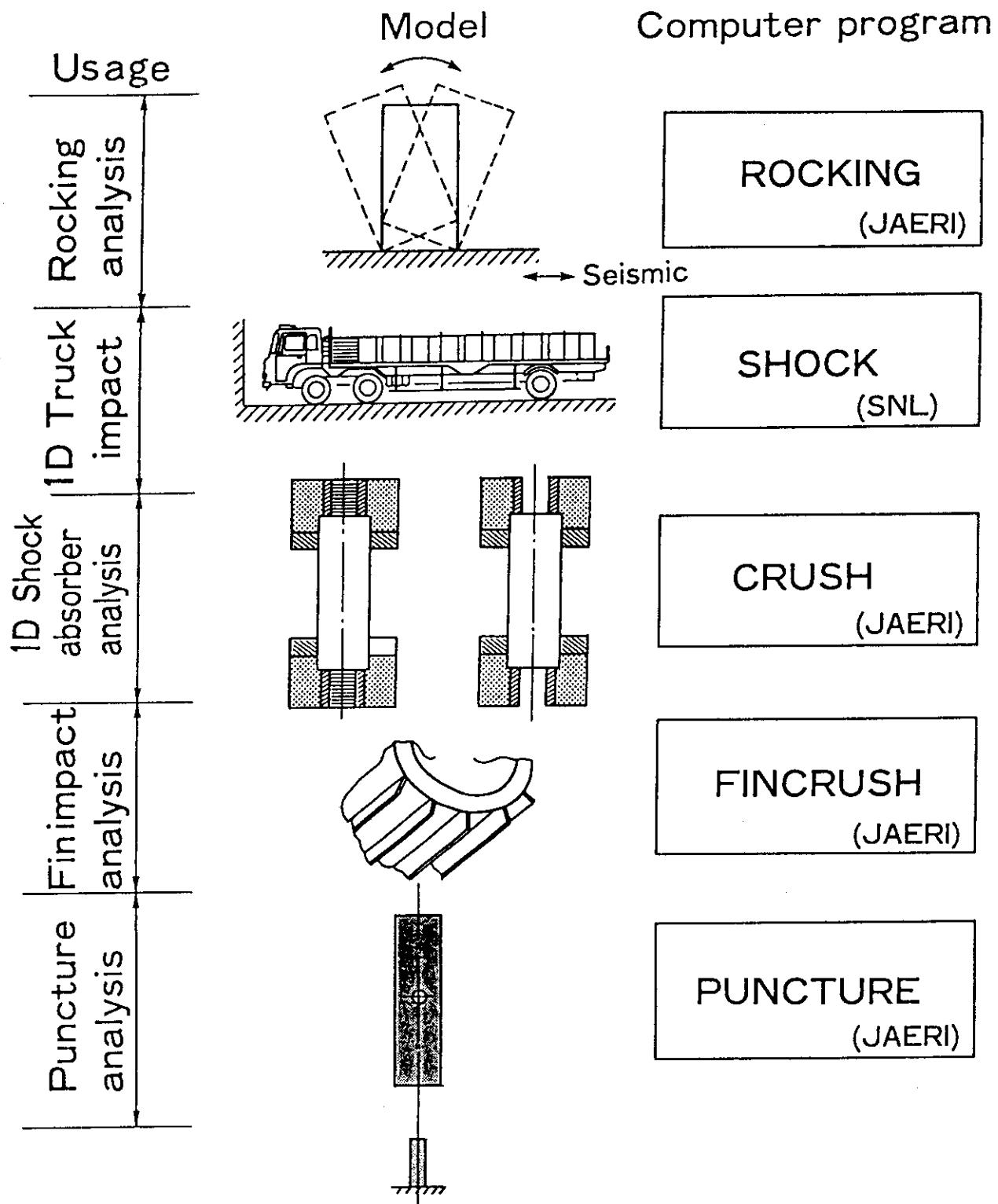


Fig. 1.1 Simplified analysis computer programs

## 2. Description of Structural Material Property Data

The structural property data are necessitated for impact analysis of casks using the computer programs such as DYNA2D, DYNA3D, NIKE2D, NIKE3D, PISCES, HONDO and so on. Therefore, the computer program IMPACLIB for a material property data library and data processing has been developed. Four kinds of materials data, structure steels (mild steel and carbon steel), stainless steels, leads and woods have been compiled and are summarized.

The structural property data including coefficient of thermal expansion, modulus of longitudinal elasticity, modulus of transverse elasticity, Poisson's ratio and stress-strain relationship have been tabulated against temperature and/or strain rate for more than 100 materials. These data have been collected from over 50 references. The data have been arranged in computer card image and stored in magnetic disks (hard or floppy disks) in a format suitable for computer processing, with the material identified numerically according to a general and flexible classification system. An accompanying numerical index, also in card image form, describes each material, assigns it an identification number, references the sources of the data by code number. The SI unit system is used for all data, and if desired, data can be converted to the MKS (meter-kilogram-second) unit system. In addition the data are obtained from a source list. The IMPACLIB has been written to search the material data list for specific material identification number.

### 3. Material Property Data Library

The computer program IMPACLIB has been developed. Four kinds of materials data, structure steels (mild steel and carbon steel), stainless steels, leads and woods have been compiled and are summarized.

(1) structure steels	(14 materials)
① carbon steel (JIS SS41)	(8 materials)
② mild steel (JIS SS4100)	(1 material)
③ structure steel (JIS S35C)	(1 material)
④ structure steel (JIS S45C)	(2 materials)
⑤ structure steel (JIS S55C)	(1 material)
⑥ mild steel (AISC 1020)	(1 material)
(2) stainless steels	(35 materials)
① stainless steel (JIS SUS302)	(1 material)
② stainless steel (JIS SUS303)	(1 material)
③ stainless steel (JIS SUS304)	(24 materials)
④ stainless steel (JIS SUS304L)	(1 material)
⑤ stainless steel (JIS SUS316)	(3 materials)
⑥ stainless steel (JIS SUS316L)	(2 materials)
⑦ stainless steel (AISC 1316L)	(1 material)
⑧ stainless steel (JIS SUS316H)	(1 material)
⑨ stainless steel (JIS SUS316)	(1 material)
(3) leads	(20 materials)
① pure lead	(17 materials)
② hard lead	(3 materials)
(4) woods	(24 materials)
① oak tree	(19 materials)
② playwood	(3 materials)
③ balsa wood	(2 materials)

The structural properties of materials, including coefficient of thermal expansion, modulus of longitudinal elasticity, modulus of transverse elasticity, Poisson's ratio and stress-strain relationship have been compiled and are summarized.

- (a) coefficient of thermal expansion (temperature dependent)
- (b) modulus of longitudinal elasticity (temperature dependent)
- (c) modulus of transverse elasticity (temperature dependent)
- (d) Poisson's ratio (temperature dependent)
- (e) stress-strain relationship (temperature dependent or strain rate dependent)

Table 3.1 shows relationships among material names, identification numbers, property data and reference numbers in the data library. Table 3.2 shows relationships between material identification numbers and reference numbers. Table 3.3 are listed constitutive equations in built in the computer program the IMPACLIB. The data formats of the structural property data are listed in Table 3.4. Table 3.5 shows the reference number for material property data in the library.

Table 3.1 Material name, identification number, reference and data in library

Category	Material name	ID number	Reference	Data
Structure steel	A I S C 1 0 2 0	1 0 0 1	R - 7	$\sigma - \epsilon$
	S 4 5 C	1 0 0 2	R - 2 4	$\sigma - \epsilon$
	STEEL	1 0 0 3	R - 3 6	$\sigma - \epsilon$
	STEEL	1 0 0 4	R - 3 6	$\sigma - \epsilon$
	STEEL	1 0 0 5	R - 5 2	$\sigma - \epsilon$
	STEEL	1 0 0 6	R - 5 2	$\sigma - \epsilon$
	STEEL	1 0 0 7	R - 5 3	$\sigma - \epsilon$
	STEEL	1 0 0 8	R - 5 5	$\sigma - \epsilon$
	STEEL	1 0 0 9	R - 5 6	$\sigma - \epsilon$
	S S 4 1	1 0 1 0	R - 8 6	$\sigma - \epsilon$
	S 3 5 C	1 0 1 1	R - 8 6	$\sigma - \epsilon$
	S 4 5 C	1 0 1 2	R - 8 6	$\sigma - \epsilon$
	S 5 5 C	1 0 1 3	R - 8 6	$\sigma - \epsilon$
	STEEL	1 1 0 0	—	$\alpha, E, G, \nu$
Stainless steel	S U S 3 0 2	2 0 0 1	R - 1	$\sigma - \epsilon$
	S U S 3 0 3	2 0 0 2	R - 1	$\sigma - \epsilon$
	S U S 3 0 4	2 0 0 3	R - 1	$\sigma - \epsilon$
	S U S 3 1 6 H	2 0 0 4	R - 1	$\sigma - \epsilon$
	S U S 3 0 4	2 0 0 5	R - 4 5	$\sigma - \epsilon$
	A I S I 3 1 6 L	2 0 0 6	R - 3	$\sigma - \epsilon$
	S U S 3 0 4 L	2 0 0 7	R - 7	$\sigma - \epsilon$
	S U S 3 0 4	2 0 0 8	R - 1 0	$\sigma - \epsilon$
	S U S 3 1 6	2 0 0 9	R - 1 0	$\sigma - \epsilon$
	S U S 3 0 4	2 0 1 0	R - 1 0	$\sigma - \epsilon$
	S U S 3 1 6	2 0 1 1	R - 1 0	$\sigma - \epsilon$
	S U S 3 1 6 L	2 0 1 2	R - 2 7	$\sigma - \epsilon$
	S U S 3 1 6 L	2 0 1 3	R - 2 7	$\sigma - \epsilon$
	S U S 3 0 4	2 0 1 4	R - 4	$\sigma - \epsilon$
	S U S ( 1 8 - 8 )	2 0 1 5	R - 4 6	$\sigma - \epsilon$
	S U S 3 0 4	2 0 1 6	R - 4 6	$\sigma - \epsilon$
	S U S 3 0 4	2 0 1 7	R - 4 8	$\sigma - \epsilon$
	S U S 3 0 4	2 0 1 8	R - 4 8	$\sigma - \epsilon$
	S U S 3 0 4	2 0 1 9	R - 4 8	$\sigma - \epsilon$
	S U S 3 0 4	2 0 2 0	R - 4 8	$\sigma - \epsilon$
	S U S 3 0 4	2 0 2 1	R - 4 8	$\sigma - \epsilon$
	S U S 3 0 4	2 0 2 2	R - 4 8	$\sigma - \epsilon$
	S U S 3 0 4	2 0 2 3	R - 4 8	$\sigma - \epsilon$
	S U S 3 0 4	2 0 2 4	R - 4 8	$\sigma - \epsilon$
	S U S 3 0 4	2 0 2 5	R - 4 8	$\sigma - \epsilon$
	S U S 3 0 4	2 0 2 6	R - 4 8	$\sigma - \epsilon$
	S U S 3 0 4	2 0 2 7	R - 4 8	$\sigma - \epsilon$
	S U S 3 0 4	2 0 2 8	R - 4 8	$\sigma - \epsilon$
	S U S 3 0 4	2 0 2 9	R - 4 8	$\sigma - \epsilon$
	S U S 3 0 4	2 0 3 0	R - 4 8	$\sigma - \epsilon$
	S U S 3 0 4	2 0 3 1	R - 4 8	$\sigma - \epsilon$
	S U S 3 0 4	2 0 3 2	R - 4 8	$\sigma - \epsilon$
	S U S 3 0 4	2 0 3 3	R - 5 1	$\sigma - \epsilon$
	S U S 3 0 4	2 1 0 0	—	$\alpha, E, G, \nu$
	S U S 3 1 6	2 2 0 0	—	$\alpha, E, G, \nu$
Lead	P U R E L E A D	3 0 0 1	R - 1	$\sigma - \epsilon$
	P U R E L E A D	3 0 0 2	R - 1	$\sigma - \epsilon$
	P U R E L E A D	3 0 0 3	R - 1	$\sigma - \epsilon$
	L E A D	3 0 0 4	R - 1	$\sigma - \epsilon$
	P U R E L E A D	3 0 0 5	R - 1 0	$\sigma - \epsilon$
	P U R E L E A D	3 0 0 6	R - 1 0	$\sigma - \epsilon$

Table 3.1 (Continued)

Category	Material name	ID number	Reference	Data
Lead	PURE LEAD	3 0 0 7	R-1	$\sigma - \epsilon$
	PURE LEAD	3 0 0 8	R-1	$\sigma - \epsilon$
	PURE LEAD	3 0 0 9	R-1	$\sigma - \epsilon$
	PURE LEAD	3 0 1 0	R-4	$\sigma - \epsilon$
	PURE LEAD	3 0 1 1	R-4	$\sigma - \epsilon$
	PURE LEAD	3 0 1 2	R-4	$\sigma - \epsilon$
	PURE LEAD	3 0 1 3	R-1 2	$\sigma - \epsilon$
	PURE LEAD	3 0 1 4	R-1 2	$\sigma - \epsilon$
	PURE LEAD	3 0 1 5	R-1 2	$\sigma - \epsilon$
	PB	3 0 1 6	R-8 5	$\sigma - \epsilon$
	PB 2	3 0 1 7	R-8 5	$\sigma - \epsilon$
	PB 4	3 0 1 8	R-8 5	$\sigma - \epsilon$
	PB 6	3 0 1 9	R-8 5	$\sigma - \epsilon$
	LEAD	3 1 0 0	-	$\alpha, E, G, \nu$
Wood	OAK	4 0 0 1	R-4 1	$\sigma - \epsilon$
	OAK	4 0 0 2	R-4 1	$\sigma - \epsilon$
	PLYWOOD	4 0 0 3	R-4 1	$\sigma - \epsilon$
	PLYWOOD	4 0 0 4	R-4 1	$\sigma - \epsilon$
	BALSA	4 0 0 5	R-4 2	$\sigma - \epsilon$
	BALSA	4 0 0 6	R-4 2	$\sigma - \epsilon$
	BALSA	4 0 0 7	R-4 2	$\sigma - \epsilon$
	BALSA	4 0 0 8	R-4 2	$\sigma - \epsilon$
	BALSA	4 0 0 9	R-4 2	$\sigma - \epsilon$
	BALSA	4 0 1 0	R-4 2	$\sigma - \epsilon$
	BALSA	4 0 1 1	R-4 2	$\sigma - \epsilon$
	BALSA	4 0 1 2	R-4 2	$\sigma - \epsilon$
	BALSA	4 0 1 3	R-4 2	$\sigma - \epsilon$
	BALSA	4 0 1 4	R-4 2	$\sigma - \epsilon$
	BALSA	4 0 1 5	R-4 4	$\sigma - \epsilon$
	BALSA	4 0 1 6	R-4 4	$\sigma - \epsilon$
	BALSA	4 0 1 7	R-4 4	$\sigma - \epsilon$
	BALSA	4 0 1 8	R-4 9	$\sigma - \epsilon$
	BALSA	4 0 1 9	R-4 9	$\sigma - \epsilon$
	BALSA	4 0 2 0	R-4 9	$\sigma - \epsilon$
	BALSA	4 0 2 1	R-4 9	$\sigma - \epsilon$
	BALSA	4 0 2 2	R-4 9	$\sigma - \epsilon$
	BALSA	4 0 2 3	R-4 9	$\sigma - \epsilon$
	PLYWOOD	4 1 0 0	-	$\alpha, E, G, \nu$

Table 3.2 Relationship between reference number and identification number

Reference	Identification number
R-7	1001, 2007
R-24	1002
R-25	1002
R-36	1003, 1004
R-52	1005, 1006
R-53	1007
R-55	1008
R-56	1009
R-1	2001, 2002, 2003, 2004, 3001, 3002, 3003, 3004, 3007, 3008
R-45	2005
R-3	2006
R-10	2008, 2009, 2011, 3003, 3005, 3006
R-27	2012, 2013
R-4	2014, 3009, 3010, 3011, 3012
R-46	2015, 2016
R-48	2017, 2018, 2019, 2020, 2021, 2022, 2023, 2024, 2025, 2026, 2027, 2028, 2029, 2030, 2031, 2032
R-51	2033
R-12	3013, 3014, 3015
R-41	4001, 4002, 4003, 4004
R-42	4005, 4006, 4008, 4009, 4010, 4011, 4012, 4013, 4014
R-44	4015, 4016, 4017
R-49	4018, 4019, 4021, 4022, 4023
R-85	3016, 3017, 3018, 3019
R-86	1001, 1011, 1012, 1013

Table 3.3 Constitutive equations built in IMPACLIB

Constitutive equations	Input parameters	Applied material
1. $\sigma_t = K \epsilon_t^n$	n, K	Lead
2. $\sigma_t = K (C + \epsilon_p)^n$	n, K, C, E	
3. $\sigma_t = \sigma_0 + K \epsilon_p^n$	n, K, $\sigma_0$ , E	
4. $\sigma_t = \sigma_c + K (\epsilon_t - \sigma_c/E)^n$	n, K, $\sigma_c$ , E	Stainless steel
6. $\sigma_t = \sigma_0 + A (1 - e^{-n\epsilon_p})$	n, A, $\sigma_0$ , E	Stainless steel
7. $\sigma_t = (\sigma_c - \sigma_\infty) e^{-\epsilon_p/m} + \sigma_\infty$	m, $\sigma_c$ , $\sigma_\infty$ , E	
8. $\sigma_t = A - B \epsilon_t^{-n}$	n, A, B	Stainless steel
10. $\sigma_t = \sum_{i=0}^n K_i \epsilon_t^i$	n, $K_0, K_1, K_2, K_3, K_4$	Stainless steel
11. $\sigma_t = A (1 + B \log \dot{\epsilon}) \epsilon_t^n$	n, A, B	Stainless steel Carbon steel
12. $\sigma_t = K (1 + C \dot{\epsilon}^m) \epsilon_t^n$	m, n, K, C	Lead
13. $\sigma_t = \sigma_y [1 + (\dot{\epsilon}/C)^{1/m}] \times [1 + (H/\sigma_y) \epsilon_p]$	m, C, H, $\sigma_y$ , E	Lead
14. $\sigma_t = K(\epsilon) + C \log \dot{\epsilon}$	K, C	
15. $\sigma_t = K \dot{\epsilon}^m \epsilon_t^n$	m, n, K	

$\sigma_t$  :True stress,       $\sigma_y$  :Yield stress,       $\sigma_0$  :Proportional limit of stress-strain,

$\epsilon_p$  :True plastic strain,  $\epsilon_t$  :True stress,       $\dot{\epsilon}$  :Strain rate,

E : Modulus of longitudinal elasticity,      e :Root of natural logarithm,

A, B, C, H, K, P, m, n, l,  $\sigma_c$ ,  $\sigma_\infty$ ,  $\epsilon_c$  :Constant.

Table 3.4 Format for material data

Data No.	Variables	Data type	Descriptions
Data set No.A-1 : MAT data set.			
1st data	NFLAG	Character	Flag for material data. 'MAT'.
2nd data	MTNAME	Character	Material name. Maximum characters are 16.
3rd data	MATNO	Integer	Material identification number. 1000 ~ 1999 : Structure steel. 2000 ~ 2999 : Stainless steel. 3000 ~ 3999 : Lead. 4000 ~ 4999 : Wood.
4th data	NALPHA	Integer	Number of data pairs listed in the table of coefficient of thermal expansion versus temperature.
5th data	NEMOD	Integer	Number of data pairs listed in the table of modulus of longitudinal elasticity versus temperature.
6th data	NSMOD	Integer	Number of data pairs listed in the table of modulus of transverse elasticity versus temperature.
7th data	NEMYU	Integer	Number of data pairs listed in the table of Poisson's ratio versus temperature.
8th data	NSSR	Integer	Number of data pairs listed in the table of stress-strain data versus temperature.
9th data	ALPHA0	Real	Coefficient of thermal expansion, if constant or if the temperature dependence is unknown.
10th data	EMOD0	Real	Modulus of longitudinal elasticity, if constant or if the temperature dependence is unknown.
11th data	SMOD0	Real	Modulus of transverse elasticity, if constant or if the temperature dependence is unknown.
12th data	EMYU0	Real	Poisson's ratio, if constant or if the temperature dependence is unknown.

Table 3.4 (Continued)

Data No.	Variables	Data type	Descriptions
Data set No.A-2 : MAT data set(continued).			
1st data	ALPHA(1)	Real	(Only included if at least two data pairs are listed.) Coefficient of thermal expansion at the temperature specified.
2nd data	TALPH(1)	Real	Temperature at which the material has the coefficient of thermal expansion specified.
3rd data	ALPHA(2)	Real	Coefficient of thermal expansion at the temperature specified.
4th data	TALPH(2)	Real	Temperature at which the material has the coefficient of thermal expansion specified.
.....	(ALPHA(I),TALPH(I)),I=1,NALPHA)		
.....			The thermal expansion table may list up to NALPHA pairs.
Data set No.A-3 : MAT data set(continued).			
1st data	EMOD(1)	Real	(Only included if at least two data pairs are listed.) Modulus of longitudinal elasticity at the temperature specified.
2nd data	TEMOD(1)	Real	Temperature at which the material has the modulus of longitudinal elasticity specified.
3rd data	EMOD(2)	Real	Modulus of longitudinal elasticity at the temperature specified.
4th data	TEMOD(2)	Real	Temperature at which the material has the modulus of longitudinal elasticity specified.
.....	(EMOD(I),TEMOD(I)),I=1,NEMOD)		
.....			The modulus of longitudinal elasticity table may list up to NEMOD pairs.

Table 3.4 (Continued)

Data No.	Variables	Data type	Descriptions
<b>Data set No.A-4 : MAT data set(continued).</b>			
1st data	SMOD(1)	Real	(Only included if at least two data pairs are listed.) Modulus of transverse elasticity at the temperature specified.
2nd data	TSMOD(1)	Real	Temperature at which the material has the modulus of transverse elasticity specified.
3rd data	SMOD(2)	Real	Modulus of transverse elasticity at the temperature specified.
4th data	TSMOD(2)	Real	Temperature at which the material has the modulus of transverse elasticity specified.
.....	(SMOD(I),TSMOD(I)),I=1,NSMOD)		
.....			The modulus of transverse elasticity table may list up to NSMOD pairs.
<b>Data set No.A-5 : MAT data set(continued).</b>			
1st data	EMYU(1)	Real	(Only included if at least two data pairs are listed.) Poisson's ratio at the temperature specified.
2nd data	TEMYU(1)	Real	Temperature at which the material has the Poisson's ratio specified.
3rd data	EMYU(2)	Real	Poisson's ratio at the temperature specified.
4th data	TEMYU(2)	Real	Temperature at which the material has the Poisson's ratio specified.
.....	(EMYU(I),TEMYU(I)),I=1,NEMYU)		
.....			The thermal expansion table data may list up to NEMYU pairs.

Table 3.4 (Continued)

Data No.	Variables	Data type	Descriptions
Data set No.B : REF data set.			
1st data	NFLAG	Character	Flag for reference number of original data. 'REF'.
2nd data	NREF	Integer	Number of references.
3rd data	REF(1)	Character	Reference number 1. Maximum characters of one reference are 8.
4th data	REF(2)	Character	Reference number 2.
.....	.....		.....
	(REF(I),I=1,NREF)		
Data set No.C : COM data set.			
1st data	NFLAG	Character	Flag for comment data. 'COM'.
2nd data	COMMEN	Character	Job description. Maximum characters are 72.
Data set No.D-1 : SSR data set.			
1st data	NFLAG	Character	Flag for material data. 'SSR'.
2nd data	TSSR	Real	Temperature specified for stress-strain data.
3rd data	DFTYPE	Character	Flag for material test method. 'C' : compression. 'T' : tension.
4th data	FIBDRC	Character	Flag for direction of force against wood fiber. 0 : 0 degree(parallel to wood fiber). 30 : 30 degrees. 45 : 45 degrees. 60 : 60 degrees. 90 : 90 degrees. NORM : Perpendicular to wood fiber.
5th data	NESPDT	Integer	Number of data for strain rate.
Data set No.D-2 : SSR data set(continued).			
1st data	EPSIDT(1)	Real	Strain rate.
2nd data	NSSD(1)	Integer	Number of stress strain data pairs.

Table 3.4 (Continued)

Data No.	Variables	Data type	Descriptions
3rd data	EPS(1,1)	Real	Strain.
4th data	STRESS(1,1)	Real	Stress.
5th data	EPS(1,2)	Real	Strain.
6th data	STRESS(1,2)	Real	Stress.
.....	.....	....	....
.....	.....	....	....
			[EPSIDT(I),NSSD(I),{EPS(I,J),STRESS(I,J)J=1,NSDD(I)},I=1,NEPSDT]
Data set No.E-1 : SSR2 data set.			
1st data	NFLAG	Character	Flag for material data. 'SSR2'.
2nd data	TSSR	Real	Temperature specified for stress-strain data.
3rd data	DFTYPE	Character	Flag for material test method. 'C' : compression. 'T' : tension.
4th data	FIBDRC	Character	Flag for direction of force against wood fiber. 0 : 0 degree(pallarel to wood fiber). 30 : 30 degrees. 45 : 45 degrees. 60 : 60 degrees. 90 : 90 degrees. NORM : Perpendicular to wood fiber.
5th data	NESPDT	Integer	Number of data for strain rate dependence data.
6th data	NEPSR	Integer	Number of data for strain dependence data.
Data set No.E-2 : SSR2 data set(continued).			
1rd data	EPS(1)	Real	Strain.
2th data	EPS(2)	Real	Strain.
.....	.....	....	....
	{EPS(J),J=1,NEPSR}		

Table 3.4 (Continued)

Data No.	Variables	Data type	Descriptions
Data set No.E-3 : SSR2 data set(continued).			
1st data	EPSDOT(1)	Real	Strain rate.
2nd data	NSIG(1)	Integer	Number of data for strain dependence. stress.
3rd data	STRESS(1,1)	Real	Stress.
4th data	STRESS(1,2)	Real	Stress.
.....	.....	...	....
.....	.....	...	....
[EPSDOT(I),NSIG(I),{STRESS(I,J)J=1,NSIG(I)},I=1,NEPSDT]			
Data set No.F : * data set.			
1st data	NFLAG	Character	Flag for comment. '*'.
2nd data	COMMEN	Character	Comment, maximum characters are 72.
Data set No.G : END data set.			
1st data	NFLAG	Character	Flag for data end. 'END'.

**Table 3.5 Reference Number for Material Property Data**

- R-1 : R. A. Robinson, W. J. Zielenbach and A. A. Lawrence, "A Survey of Strain-rate Effects for Some Common Structural Materials Used in Radioactive Material Packing and Transportation Systems", BMI-1954 (1976).
- R-2 : T. K. Hill and W. W. Joseph, "Energy-Absorbing Characteristics of Materials", SLA-74-0159 (1974).
- R-3 : C. Albertini, J. P. Halleux and M. Montagnani, "Material Behaviour and Modelling in Transient Dynamic Situations", Advanced Structural Dynamics, Applied Science Publishers Ltd., London (1978).
- R-4 : R. A. Robinson, J. A. Hadden and S. J. Basham, "Experinetal Studies of Dynamic Impact Response with Scale Models of Lead Shielded Radioactive Material Shipping Containers", BMI-2001 (1978).
- R-5 : D. Aquaro and G. Forasassi, "Plastic Deformation of Steel Shock Absorbing Structures", Trans. Int. Conf. SMiRT-6, L 9/6 (1981).
- R-6 : H. J. Rack and M. C. Cheresh, " Puncture Resistance of Type B Trasnport Systems", SAND-80-07620C (1980).
- R-7 : J. H. Evans, "Experimental Study of the Stress-Strain Properties of Cask Materials under Specified Impact Conditions", CONF-740901-6 (1974).
- R-8 : D. Meredith and K. N. Morman Jr., "Computer Simulation of Structural Energy Absorption by Collapse", Ford Motor Company.
- R-9 : B. J. Donham, "Prediction of Maximum Damage to Shielded Shipping Contaimers" LA-4649 (1971).
- R-10: H. J. Rack and G. A. Knorovsky, "An Assessment of Stress-Strain Data Suitable for Finite-Element Elastic-Plastic Analysis of Shipping Containers", SAND 77-1872 (1978).
- R-11: T. Ikushima, "Constitutive Equations of Lead for Impact Analysis", Letter to the RC-62 Sub-Committee in Japan Society of Mechanical Engineers (1982) (in Japanese).
- R-12: J. H. Evans, "Structural Analysis of Shipping Casks Vol. 8, Experimental Study of the Stress-Strain Properties of Lead under Specified Impact Conditions", ORNL-TM-1312 Vol. 8 (1970).
- R-13: T. Ikushima, "Structural Property Data for Impact Analysis of Shipping Casks", Letter to the RC-62 Sub-Committee in Japan Society of Mechanical Engineers (1982) (in Japanese).

Table 3.5 (Continued)

- R-14: Sandia National Labs., "A Comparison of Analytical Techniques for Analyzing a Nuclear-Spent-Fuel Shipping Cask Subjected to an End-on Impact", (1981).
- R-15: A. Chatani, "Review of Impact Testing Methods", Letter to the Sub-Committee in Japan Society of Mechanical Engineers (1982) (in Japanese).
- R-16: R. A. C. Slater, W. Johnson and S. Y. Aku, "Experiments in the Fast Upsetting of Short Pure Lead Cylinders and a Tentative Analysis", Int. J. Mech. Sci., 10, pp.169-186 (1968).
- R-17: C. H. Mok and J. Duffy, "The Dynamic Stress-strain Relation of Metals as Determined from Impact Tests with a Hard Ball", Int. J. Mech. Sci., 7, pp.355-371 (1965).
- R-18: K. Tanaka and T. Nojima, "Dynamic and Static Strength of Steels", Mechanical Properties at High Rates of Strain, ed. by J. Harding., The Institute of Pysics, pp.25-34 (1979).
- R-19: S. Sakai and T. Sakai, "The Effect of Strain Rate, Temperature and Grain Size on the Lower Yield Stress and Flow Stress of Polycrystalline Pure Iron", J. Iron and Steel Inst. Japan, 58, pp.1438-1455 (1972) (in Japanese).
- R-20: A. J. Holzer and R. H. Brown, "Mechanical Behavior of Metals in Dynamic Compression", Trans. ASME, J. Eng. Material Technol., 101, pp.238-247 (1979).
- R-21: K. Maekawa, T. Shirakashi and E. Usui, "Flow Stress of Low Carbon Steel at High Temperature and Strain Rate( 2nd Report - Flow Stress under Variable Temperature and Variable Strain Rate - )", J. Japan Socceity of Precision Machinary, 44, pp.1495-1500 (1978) (in Japanese).
- R-22: U. S. Lindholm, "Review of Dynamic Testing Techniques and Material Behavior", Conf. Mech. Prop. Material High Rate Strain, pp.3-21 (1974).
- R-23: S. Tanimura, "Practical Constitutive Equations for an Elastic/Viscoplastic Body Covering a Wide Range of Strain Rates", Proc. Jpan. Congr. Material Res., 25, pp.25-30 (1982).
- R-24: K. Kawata, "Three Topics in the Mechanics of High Velocity Deformation of Solids", Theory Appl. Mech., 30, pp.3-16 (1981).
- R-25: K. Kawata, "Micromechanical Study of High Velocity Deformation of Solids", Theory Appl. Mech., 29, pp.307-317 (1980).
- R-26: T. Vinh, M. Afzali and A. Roche, "Fast Fracture of Some Usual Metals at Combined High Strain and High Strain Rate", Mech. Behavior Material, 2, pp.633-642 (1979).
- R-27: C. Albertini, A. Del Grande and M. Montagnani, "Effects of Irradiation on the

Table 3.5 (Continued)

- Mechanical Properties of Austenitic Stainless Steels under Dynamic Loading", ASTM Spec. Tech. Publ. No. 683, pp.546-556 (1979).
- R-28: C. Albertini and M. Montagnani, "Experimental Determination of Material's Constitutive Laws and Design Criteria of Reactor Structures in Extreme Dynamic Loading Conditions", Trans. Int. Conf. SMiRT-6, L4/4, pp.1-10 (1981).
- R-29: D. Lee and F. Zaverl Jr., "The Influence of Material Parameters on Nonuniform Plastic Flow in Simple Tension", Acta Mat., 28, pp.1415-1426 (1980).
- R-30: A. Oda and H. Miyakawa, "X-ray Constant Measurement of 18Ni - 8Cr Austenitic Stainless Steel", J. Society of Materials Science, Japan, 27, pp.226-229 (1978) (in Japanese).
- R-31: H. Miyagawa and A. Oda, "X-ray Constant Measurement of Tensile Pre-Strained 18Ni - 8Cr Austenitic Stainless Steel", J. Society of Materials Science, Japan, pp.218-223 (1979) (in Japanese).
- R-32: J. P. Hammond, M. W. Moyer and C. R. Brinkman, "Effects of Materials and Test Variables on Elastic Constants of 2-1/4Cr - 1Mo Steel and Type 304 Stainless Steel", Int. Conf. Mech. Material, 2, pp.1037-1041 (1976).
- R-33: H. Nyuko, Y. Takeuchi, S. Zaima and N. Noda, "Temperature Dependence of Dynamic Moduli of Several Alloys", Symp. Mech. Behav. Mater., 2, pp.237-246 (1974).
- R-34: B. I. Verkin, V. Ya Illichev and I. N. Klimenko, "The Low-temperature Change of the Magnetic Structure and Plastic Properties of Fe-Cr-Ni Alloys", Adv. Cryog. Eng., 26, pp.120-125 (1980)
- R-35: H. M. Ledbetter, "Sound Velocities and Elastic Constants of Steels 304, 310 and 316", Mat. Sci., 14, p.595-596 (1980).
- R-36: M. Omori and Y. Yoshinaga, "Effects of Strain Rate on Deformation Behavior of Steels - 1st Report : Tensile and Compression Deformation", J. Plastic Working, Japan, 8, pp.297-306 (1980) (in Japanese).
- R-37: T. Sakuno and T. Goto, "Studies on the Impact Adhesives, IV, Estimation of Wood-Glue Joint by Impact Load(1)", J. Wood Research Society, Japan, 19, pp.533-537 (1973) (in Japanese).
- R-38: Y. Hamano and A. Matsumoto, "Studies on the Mechanism of Energy Absorption of Wood Subject to Impact Load, I)", J. Wood Research Society, Japan, 25, pp.567-572 (1979) (in Japanese).
- R-39: Y. Hamano and A. Matsumoto, "Studies on the Mechanism of Energy Study on Absorption of Wood Subject to Impact Load, II)", J. Wood Research Society,

Table 3.5 (Continued)

- Japan, 26, pp.658-663 (1980) (in Japanese).
- R-40: H. Miyakawa and M. Mori, "Impact Properties of Wood and wood Based Materials, IV, Effect of Impact Velocity on Shear Fracture of Wood Specimens)", J. Wood Research Society, Japan, 24, pp.857-864 (1978) (in Japanese).
- R-41: Kobe Steel Work Co., Ltd., "Charcteristics of Impact Energy Absorption on Woods", Letter to the RC-62 Sub-Committee in Japan Society of Mechanical Engineers (1983) (in Japanese).
- R-42: Nppon Steel Work Co., Ltd., "Crush Test of Balsa Woods", Letter to the RC-62 Sub-Committee in Japan Society of Mechanical Engineers (1983) (in Japanese).
- R-43: Nitta Playwood Co., Ltd., "Compression Characteristic Charts of Balsa Woods", Letter to the RC-62 Sub-Committee in Japan Society of Mechanical Engineers (1983) (in Japanese).
- R-44: Hitachi Ship and Dock Co., Ltd., "Compression Characteristics of Balsa Woods", Letter to the RC-62 Sub-Committee in Japan Society of Mechanical Engineers (1983) (in Japanese).
- R-45: U. Nishiyama and S. Tanimura, "Compressive Strength of Steels on High Strain Rates", Trans. Japan Society of Mechanical Enginerrs, 36-285, pp.714-722 (1970) (in Japanese).
- R-46: T. Hirano, M. Sudo and Y. Yutori, "Effect of Strain Rates and Pre-strains at Room Temperature on the Mechanical Properties of Austenitic Stainless Steels", Trans. Japan Inst. Metal, 33, pp.975-983 (1969) (in Japanese).
- R-47: J. P. Hammond and V. K. Sikka, "Predicted Strains in Austenitic Stainless Steels at Stresses above Yield", Winter Annual Meeting of ASME, Atlanta, USA (1977).
- R-48: A. Chatani, "Relationship of Compression Stress-Strain of SUS 304 Stainless Steel", Letter to the RC-62 Sub-Committee in Japan Society of Mechanical Engineers (1983) (in Japanese).
- R-49: Mitsui Ship and Dock Co., Ltd., "Drop Impact Test for Balsa Woods", (1983).
- R-50: H. M. Ledbettar, "Stainless-Steel Elastic Constants at Low Temperatures", Trans. ASME, J. Appl. Phys., 52, pp.1587-1589 (1981).
- R-51: T. Isozaki, T. Ooba and S. Ueda, "Impulse Tensile Test at High Temperature for Austenitic Stainless Steel", Trans. Japan Society of Mechanical Enginerrs, 42-359, pp.2034-2041 (1976) (in Japanese).
- R-52: C. J. Maiden and J. D. Cambell, "The Static and Dynamic Strength of Carbon

Table 3.5 (Continued)

- Steel at Low Temperatures", Phil. Mag., 3, pp.872-885 (1958).
- R-53: J. D. Cambell and J. Duby, "The Yield Behavior of Mild Steel in Dynamic Compression", Proc. Roy. Soc. A., 236, pp.24-40 (1956).
- R-54: A. B. Haberfield and M. W. Boyles, "The Tensile Properties of a Fully Aged Rimming Steel at High Strain Rates", PB Rep. No.226974 (1973).
- R-55: A. Hojo and A. Chatani, "The Effect of Strain Rate History on the Stress-Strain Curve", Research Report, Faculty of Technology, Kanazawa University, 13, pp.113-119 (1977) (in Japanese).
- R-56: A. Hojo and A. Chatani, "The Yield Stress on Combined Static Tension and Dynamic Torsion", Trans. Japan Society of Mechanical Engineers, 43-375, pp. 3994-4001 (1977) (in Japanese).
- R-57: A. Hoyo and A. Chatani, "The Yield Stress on Combined Static Tension and Dynamic Torsion", Trans. Japan Society of Mechanical Engineers, 48-429, pp. 633-640 (1982) (in Japanese).
- R-58: K. Kawata, S. Hashimoto, K. Kurokawa and N. Kanayama, "A New Testing Method for the Characterisation of Materials in High-Velocity Tension", Mechanical Properties at High Rates of Strain, ed. by J. Haring, The Institute of Physics (1979).
- R-59: L. W. Meyer, H. D. Kunze and K. Seifert, "Dynamic Behavior of High Strength Steels under Tension", Shock Waves and High-Strain-Rate Phenomena in Metals, ed. by M. A. Meyers and L. E. Murr, Plenum Press, pp.51-63 (1981).
- R-60: S. Shida, "Strain Rate Dependency for Resistance of Cold Deformation-Mathematical Model of Cold Tandem Mill (I)", J. Plastic Working, Japan, 13, p.935 (1972) (in Japanese).
- R-61: T. Kobayashi, "Ductility of Cast Irons", J. Iron and Forging, Japan, 30-7, pp.5-12 (1977) (in Japanese).
- R-62: T. Kobayashi, "Fracture Toughness of Irons - Concerning to Spheroidal Graphite Cast Irons", J. Society of Materials Science, Japan, 18, pp.512-517 (1979) (in Japanese).
- R-63: M. W. Schwartz and L. Boyce, "Ductile and Brittle Failure Design Criteria for Nodular Cast Iron Spent-Fuel Shipping Containers", UCRL-53046 (1983).
- R-64: T. Kobayashi and S. Nishi, "Fracture Characteristics of Spheroidal Graphite Cast Iron", J. Cast Iron, Japan, 52, pp.76-87 (1980).
- R-65: R. K. Nanstad, F. J. Worzala and C. R. Loper Jr., "The Fracture Characteristics of Nodular Cast Iron", Int. symp. Metall. Cast Iron, 2, pp.789-807 (1975).

Table 3.5 (Continued)

- R-66: R. K. Nanstad, F. J. Worzala and C. R. Loper Jr., "Static and Dynamic Toughness of Ductile Cast Iron", Trans. American Foundrymen Soc., 83, pp. 245-256 (1975).
- R-67: F. J. Worzala, R. W. Heine and Yi Wen Cheng, "Toughness of Malleable and Ductile Iron", Trans. American Foundrymen Soc., 84, pp.675-682 (1976).
- R-68: Yi Wen Cheng and F. J. Worzala, "Fracture Behavior of Cast Irons", Int. Conf. Mech. Behav. Mater., 2, pp.1223-1227 (1976).
- R-69: W. L. Bradley and H. E. Mead Jr., "Fracture Toughness Studies of Nodular Cast Iron Using a J-integral Approach", ASME MPC, 11, pp.69-87 (1979).
- R-70: W. L. Bradley, "Fracture Toughness Studies of Gray, Malleable and Ductile Cast Iron", Trans. American Foundrymen Soc., 89, pp.837-848 (1981).
- R-71: S. R. Holdsworth and G. Jolley, "The Influence of Graphite Nodule Number and Volume Fraction on the Fracture Toughness of Ferritic Nodular Cast Iron", Int. Symp. Metall. Cast Iron, pp.809-825 (1975).
- R-72: T. Luyendijk and H. Nieswaag, "Ductile Cast Iron Instrumented Impact Tests Made at Different Impact Speeds", Int. Foundry Congr., pp.1-13 (1982).
- R-73: A. LeDouaron, R. Lafont, D. Poulain and C. Cloitre, "Fracture Toughness of Ferritic Spheroidal Graphite Cast Irons", Adv. Fract. Res., 1, pp.252-262 (1982).
- R-74: R. Eisenstadt and G. H. Roulston, "A Low Temperature Brittle Fracture Investigation of Gray Iron and Nodular Iron on Machinery Castings", Pap. Am. Soc. Mech. Eng., pp.1-7 (1975).
- R-75: D. Frodl, W. Schmidt and H. Schoch, "Mechanische Eigenschaften von Stahl- und Gussqualitäten", VDI-Z, 125, pp.887-894 (1983).
- R-76: F. Henke, "Die Bruchzähigkeit von Gusseisen-Werkstoffen", Giesserei Prax., No. 9/10, pp.131-139 (1976).
- R-77: J. K. Mortz, C. Berger, G. Cohrt, E. K. Godehardt, K. Hüttebräucker, G. Kuhn, H. Reuter, D. Schock, M. shakshaft und D. Welter, "Bruchmechanische Eigenschaften in Grossen Wanddicken von Gussstücken aus Gusseisen mit Kugelgraphit", VDI-Z, 122, pp.883-898 (1980).
- R-78: C. Berger und W. Wiemann, "Bruchmechanische Eigenschaften in Dickwandigen Gussstücken aus Gusseisen mit Kugelgraphit als Kriterium für die Konstruktion", Ver. Dtsch. Ing. Ber., No. 469, pp. 47-58 (1983).
- R-79: J. Yajima, Y. Hirose, K. Tanaka and H. Ogawa, "X-ray Fractographic Study on Fracture Toughness of Ductile Cast Iron", J. Society of Materials Science, Japan, 32, pp.1345-1350 (1983) (in Japanese).

**Table 3.5 (Continued)**

- R-80: S. Komatsu, T. Shiota and K. Nakamura, "Influence of Silicon Content on Fracture Toughness of Ferritic Spheroidal Cast Iron", J. Japan Foundrymen's Society, 56, pp.170-175 (1984) (in Japanese).
- R-81: H. Sumitome and K. Nakamura, "Effects of Graphite on Low Temperature Impact Characteristics of Spheroidal Graphite Cast Irons", J. Japan Foundrymen's Society, 55, pp.609-614 (1983) (in Japanese).
- R-82: W. R. Holman and R. T. Langland, "Recommendations for Protecting Against Failure by Brittle Fracture in Ferritic Steel Shipping Containers Up to Four Inches Thick", UCRL-53013 (1981).
- R-83: M. W. Schwartz, "Protecting Against Failure by Brittle Fracture in Ferritic Steel Shipping Containers Greater Than Four Inches Thick", UCRL-53045 (1982).
- R-84: M. W. Schwartz, "Recommendations for Protecting Against Failure by Brittle Fracture in Ferritic Steel Shipping Containers Greater than Four Inches Thick", UCRL-53538 (1984).
- R-85: T. Ikushima, "A Compilation of Structural Property Data for Computer Impact Calculation (4/5), Volume 4 : Lead", JAERI-M 88-194 (1988) (in Japanese).
- R-86: T. Ikushima, "A Compilation of Structural Property Data for Computer Impact Calculation (2/5), Volume 2 : Mild Steel", JAERI-M 88-192 (1988) (in Japanese).
- R-87: T. Ikushima, "A Compilation of Structural Property Data for Computer Impact Calculation (3/5), Volume 3 : Stainless Steel", JAERI-M 88-193 (1988) (in Japanese).
- R-88: T. Ikushima, "A Compilation of Structural Property Data for Computer Impact Calculation (5/5), Volume 5 : Wood", JAERI-M 88-195 (1988) (in Japanese).
- R-89: T. Ikushima and T. Nagata, "A Compilation of Structural Property Data for Computer Impact Calculation (1/5), Volume 1 : Structural Property Data and Data Processing Computer Program", JAERI-M 88-191 (1988) (in Japanese).

## 4. Computer Program

### 4.1 Program Description

The computer program IMPACLIB consists of three parts. These are the material property library obtained by many research institutes, the data retrieval program and plotting program for the data used with DYNA2D, DYNA3D, NIKE2D, NIKE3D, PISCES, HONDO, CRUSH1<sup>(14)</sup>, CRUSH2<sup>(15)</sup>, FINCRUSH<sup>(16)</sup> and PUNCTURE<sup>(17)</sup> computer programs. The CRUSH1, CRUSH2, FINCRUSH and PUNCTURE are static calculation programs and the other are dynamic finite element programs capable of evaluating the maximum acceleration of the cask body, the maximum deformation and so on.

The computer program IMPACLIB consists of a main routine and thirty five subroutines. These are MAIN, BLOCKDATA, MLBST, MLBPT, RDSQF, RDCHS, ISBST, MLBEX, EXCOM, EXCOMQ, EXCOM1, EXCOM2, EXCOM3, EXQRY, EXDAT, MLBFD, GTPROP, GTEPSS, GTSIG, GTEMOD, EXUNI, EXUNI2, EXOUT, EXFIT, EXFIT1, EXFIT2, EXFIT3, EXMINX, EXLSTP, EXGRA, CURVE, AXFUN1, PLTAX2, PLTAXL, PLTLGV and DTLIST. Overall structure of the IMPACLIB is shown in Fig. 4.1. Functions of subroutines are as follows:

- MAIN : initializes start of run,
- BLOCKDATA : initializes data set,
- MLBST : prepares to read material data library(1),
- MLBPT : handling material data library,
- RDSQF : prepares to read material data library(2),
- RDCHS : sets input data parameters,
- ISBST : changes from character type data to integer type data,
- MLBEX : controls IMPACLIB program,
- EXCOM : reads input data(1),
- EXCOMQ : reads input data(2),
- EXCOM1 : reads input data(3),
- EXCOM2 : reads input data(4),
- EXCOM3 : reads input data(5),
- EXQRY : prints of output data,

EXDAT : prepares to print output data,  
 MLBFD : reads material data(1),  
 GTPROP : searches material property data,  
 GTEPSS : searches stress-strain data(1),  
 GTSIG : searches stress-strain data(2),  
 GTEMOD : reads material data(2),  
 EXUNI : changes data unit(1),  
 EXUNI2 : changes data unit(2),  
 EXOUT : prepares to print output data,  
 EXFIT : prepares data fitting output,  
 EXFIT1 : prepares data curve fitting(1),  
 EXFIT2 : prepares data curve fitting(2),  
 EXFIT3 : prepares data curve fitting(3),  
 EXMINX : searches maximum and minimum values,  
 EXLSTP : prepares to draw material property data,  
 EXGRA : prepares to draw stress-strain curves,  
 CURVE : draws stress-strain curves,  
 AXFUN1 : prepares to draw axis,  
 PLTAX2 : draws axis,  
 PLTAXL : draws grid lines,  
 PLTLGV : prepares to grid lines,  
 DTLIST : prints of input data.

A macroscopic flow chart of the IMPACLIB is shown in Fig. 4.2.

#### 4.2 Description of Input Data

This section describes the input data required by the IMPACLIB. The input data consist of a material title, the material selection, a data fitting curve selection and options for output plotting. The input instruction is simple and easy follow. The input data forms are presented in Tables 4.1, 4.2 and 4.3 and Fig. 4.3..

#### 4.3 Description of Output Data

This section describes the output data forms of the IMPACLIB. The contents of these various quantities are described in the followings.

(1) Input data

The input data are printed in two formats. The first print format is exactly the same as they were read. Second, the computer program lists the input data as interpreted by the IMPACLIB.

(2) Material property data

The material property data are compiled from the data library file and printed out on output sheets.

(3) Graphical output

The IMPACLIB provides users with the graphical output of the material property data.

Table 4.1 Input data for IMPACLIB

(1) ENTRY command

ENTRY command.

Function : Job entry.

Prompt : ENTRY? (0:1:2:3)

Input data :

- 0 : EXIT.
- 1 : QUERY.
- 2 : GRAPHICS.
- 3 : INPUT ECHO.

(2) QUERY command

QUERY command.

Function : Selection of job.

Prompt : QUERY? (0:1:2:3:4:5:6:7:8)

Input data :

- 0 : RETURN.
- 1 : MATERIAL NAME LIST.
- 2 : STRUCTURE STEEL NAME LIST.
- 3 : STAINLESS STEEL NAME LIST.
- 4 : LEAD NAME LIST.
- 5 : WOOD NAME LIST.
- 6 : REFERENCE LIST.
- 7 : MATERIAL DATA.
- 8 : MATERIAL INDEX.

(3) Graphic commands

(a) TITLE command

TITLE command.

Function : Job description.

Prompt : TITLE? ('.....')

Input data : '.....'

Table 4.1 (Continued)

## (b) MATERIALS command

MATERIALS command.
Function : Selection of material, number of materials and material index.
Prompt : MATERIALS? (PROP, NMAT, MATNO, ....)
Input data : PROP
<ul style="list-style-type: none"> <li>0 : RETURN.</li> <li>1 : COEFFICIENT OF THERMAL EXPANSION.</li> <li>2 : MODULUS OF LONGITUDINAL ELASTICITY.</li> <li>3 : MODULUS OF TRANSVERSE ELASTICITY.</li> <li>4 : POISSON'S RATIO.</li> <li>5 : STRESS-STRAIN CURVE.</li> <li>6 : STRESS-STRAIN CURVE DEPENDENT ON STRAIN RATE.</li> </ul>
NMAT : NUMBER OF MATERIALS.
MATNO : MATERIAL INDEX NUMBER.

## (c) PARAMETERS command

PARAMETERS command.
Function : Selection of data parameters, such as material test method, direction of compression or tensile force against wood fiber, temperature ranges, stress-strain curve and stress-strain curve dependent on strain rate.
Prompt : PARAMETERS? (0:1:2:3:4:5)
Input data :
<ul style="list-style-type: none"> <li>0 : RETURN.</li> <li>1 : DEFORMATION TYPE(material test method).</li> <li>2 : FIBER DIRECTION OF WOOD(direction of force against wood fiber).</li> <li>3 : TEMPERATURE(temperature range).</li> <li>4 : STRAIN RATE.</li> <li>5 : STRAIN.</li> </ul>

Table 4.1 (Continued)

(c-1) DEFORMATION TYPE subcommand

DEFORMATION TYPE subcommand.

Function : Selection of material test method.

Prompt : DEFORMATION TYPE? (0:1:2:3:)

Input data :

- 0 : RETURN.
- 1 : COMPRESSION.
- 2 : TENSION.
- 3 : COMPRESSION & TENSION.

(c-2) FIBER DIRECTION OF WOOD subcommand

FIBER DIRECTION OF WOOD subcommand.

Function : Selection of material test direction of compression or tensile force against wood fiber.

Prompt : FIBER DIRECTION OF WOOD? (0:1:2:3:4:5:6)

Input data :

- 0 : RETURN.
- 1 : 0 DEG.
- 2 : 30 DEG.
- 3 : 45 DEG.
- 4 : 60 DEG.
- 5 : 90 DEG.
- 6 : NORMAL.

(c-3) TEMPERATURE subcommand

TEMPERATURE subcommand.

Function : Selection of temperature ranges.

Prompt : TEMPERATURE? (NIN,MAX)

Input data :

- MIN : MINIMUM TEMPERATURE.
- MAX : MAXIMUM TEMPERATURE.

Table 4.1 (Continued)

(c-4) STRAIN RATE subcommand

STRAIN RATE subcommand.

Function : Selection of stress-strain curve dependent on strain rate.

Prompt : STRAIN RATE? (NIN,MAX)

Input data :

MIN : MINIMUM STRAIN RATE.

MAX : MAXIMUM STRAIN RATE.

(c-5) STRAIN subcommand

STRAIN RATE subcommand.

Function : Selection of strains.

Prompt : STRAIN ? (NSTRN, STRN1, STRN2, .....)

Input data :

NSTRN : NUMBER OF STRAINS(number of data dependent on strain).

STRN1 : STRAIN.

STRN2 : STRAIN.

..... : .....

(d) SYSTEM OF UNITS command

SYSTEM OF UNITS command.

Function : Selection of units.

Prompt : SYSTEM OF UNITS? (1:2)

Input data :

1 : SI (SI unit).

2 : MKS (MKS unit).

Table 4.1 (Continued)

(e) OUTPUT command

OUTPUT command.

Function : Selection of output forms.

Prompt : OUTPUT? (0:001:010:011:100:101:111)

Input data :

- 0 : RETURN.
- 001 : LISTING.
- 010 : PLOTTING.
- 011 : LISTING & PLOTTING.
- 100 : FITTING.
- 110 : FITTING & PLOTTING.
- 111 : FITTING & PLOTTING & LISTING.

(e-1) PLOT OPTIONS subcommand

PLOT OPTIONS subcommand.

Function : Selection of graphical output forms.

Prompt : PLOT OPTIONS? (0:1:2:3:4:5)

Input data :

- 0 : RETURN.
- 1 : DATA RANGES.
- 2 : TYPE OF AXES.
- 3 : STRING.
- 4 : MESH.
- 5 : COMMENT OF CURVES.

(e-2) DATA RANGES subcommand

DATA RANGES subcommand.

Function : Selection of data ranges for graphical plot.

Prompt : DATA RANGES? (XMIN, XMAX, YMIN, YMAX)

Input data :

- XMIN : MINIMUM VALUE ON X-AXIS.
- XMAX : MAXIMUM VALUE ON X-AXIS.
- YMIN : MINIMUM VALUE ON Y-AXIS.
- YMAX : MAXIMUM VALUE ON Y-AXIS.

Table 4.1 (Continued)

## (e-3) TYPE OF AXES subcommand

TYPE OF AXES subcommand.
Function : Selection of scale types for graphical plot axes.
Prompt : TYPE OF AXES? (1:2:3:4)
Input data :
<ul style="list-style-type: none"> <li>1 : BOTH X AND Y ARE LINEAR SCALE (both X- axis and Y-axis are linear scales).</li> <li>2 : X IS LOG SCALE, Y IS LINEAR SCALE (X-axis is log scale and Y-axis is linear scale).</li> <li>3 : X IS LINEAR SCALE, Y IS LOG SCALE (X-axis is linear scale and Y-axis is log scale).</li> <li>4 : BOTH X AND Y ARE LOG SCALE (both X-axis and Y-axis are log scales).</li> </ul>

## (e-4) STRING subcommand

STRING subcommand.
Function : Selection of string types.
Prompt : STRING? (0:1)
Input data :
<ul style="list-style-type: none"> <li>0 : NO (do not draws).</li> <li>1 : YES (draws line between plot marks).</li> </ul>

## (e-5) MESH subcommand

MESH subcommand.
Function : Selection of mesh drawing.
Prompt : MESH? (0:1:2)
Input data :
<ul style="list-style-type: none"> <li>0 : NONE (do not draws).</li> <li>1 : DASH LINE (draws straight line mesh).</li> <li>2 : LINE (draws dotted line mesh).</li> </ul>

Table 4.1 (Continued)

## (e-6) COMMENT OF CURVES subcommand

COMMENT OF CURVES subcommand.
-------------------------------

Function : Writes a comment on a curve.

Prompt : COMMENT OF CURVES? (CURVE-NO., '...COMMENT...')

Input data :

CURVE-NO.

0 : RETURN.

>1 : DEFINITION.

<20 : DEFINITION.

'...COMMENT...' (writes a comment on the curve).

## (f) FITTING commands

FITTING command.
------------------

Function : Selection of curve fitting.

Prompt : FITTING? (0:1:2:3)

Input data :

0 : RETURN.

1 : INPUT X-Y DATA (input X-Y data for fixed points).

2 : LINEAR REGRESSION (linear regression).

3 : BUILT IN EQUATIONS (use of built in equations).

## (f-1) X-Y DATA subcommand

X-Y DATA subcommand.
----------------------

Function : Read X-Y data for fixed points.

Prompt : X-Y DATA? (N, X1, Y1, ...., XN, YN))

Input data :

N : number of X and Y data for fixed points (maximum number is 50).

X1 : X DATA.

Y1 : Y DATA.

..... : .....

..... : .....

XN : X DATA.

YN : Y DATA.

Table 4.1 (Continued)

## (f-2) LINEAR REGRESSION subcommand

LINEAR REGRESSION subcommand.

Function : Seeks coefficient of linear regression.

Prompt : LINEAR REGRESSION? (A, B)

Input data :

A : coefficient of A.

B : coefficient of B.

$$Y = A \times X + B$$

## (f-3) EQUATION NUMBER subcommand

EQUATION NUMBER subcommand.

Function : Selection of equation number of built in function based on linear regression..

Prompt : EQUATION NUMBER? (1:2:3:.....:15)

Input data :

0 : RETURN.

1 : EQUATION NUMBER 1.

2 : EQUATION NUMBER 2.

... : .....

15 : EQUATION NUMBER 15.

## (4) EXIT/RESET command

EXIT/RESET command.

Function : Selection of job exit or reset.

Prompt : EXIT/RESET? (1:2:3:4:5:6)

Input data:

0 : EXIT.

1 : QUERY.

2 : TITLE,.....

3 : MATERIALS,.....

4 : PARAMETERS,.....

5 : SYSTEM OF UNITS.

6 : OUTPUT.

Table 4.2 Relationship between output plot selection and input data

X-axis	Y-axis	Input data(commands)					
		MATERIALS		PARAMETERS			
	PROP	MATNO	1:Direction of test force	2:Fiber direction of wood	3:Temperature	4:Strain rate	5:Strain
Temperature	Coefficient of thermal expansion	1	◎				
Temperature	Modulus of longitudinal elasticity	2	◎				
Temperature	Modulus of transverse elasticity	3	◎				
Temperature	Poisson's ratio	4	◎				
Strain	Stress	5	◎	○	○	○	
Strain rate	Stress	6	◎	○	○	○	◎

Legend : ◎ : Necessity  
 ○ : Option

Table 4.3 Commands for IMPACLIB

Commands/Subcommands	Functions
ENTRY	Job entry.
QUERY	Selection of job.
GRAPHICS	Graphic output.
MATERIALS	Job description.
PARAMETERS	Selection of material.
DEFORMATION TYPE	Selection of material test method.
FIBER DIRECTION OF WOOD	Selection of material test direction against wood fiber.
TEMPERATURE	Selection of temperature ranges.
STRAIN RATE	Selection of stress-strain curve dependent on strain rate.
STRAIN	Selection of strain.
SYSTEM OF UNITS	Selection of units
OUTPUT	Selection of output forms.
PLOT OPTIONS	Selection of graphical output forms.
DATA RANGES	Selection of data ranges for graphical plot.
TYPE OF AXES	Selection of scale types for graphical plot axes.
STRING	Selection of string types.
MESH	Selection of mesh drawing.
COMMENT OF CURVES	Write a comment on a curve.
FITTING	Selection of data fitting.
X-Y DATA	Read X-Y data for fixed points
LINEAR REGRESSION	Seeks coefficient of linear regression.
EQUATION NUMBER	Selection of equation number of built in function based on linear regression.
EXIT/RESET	Selection of job exit or reset.

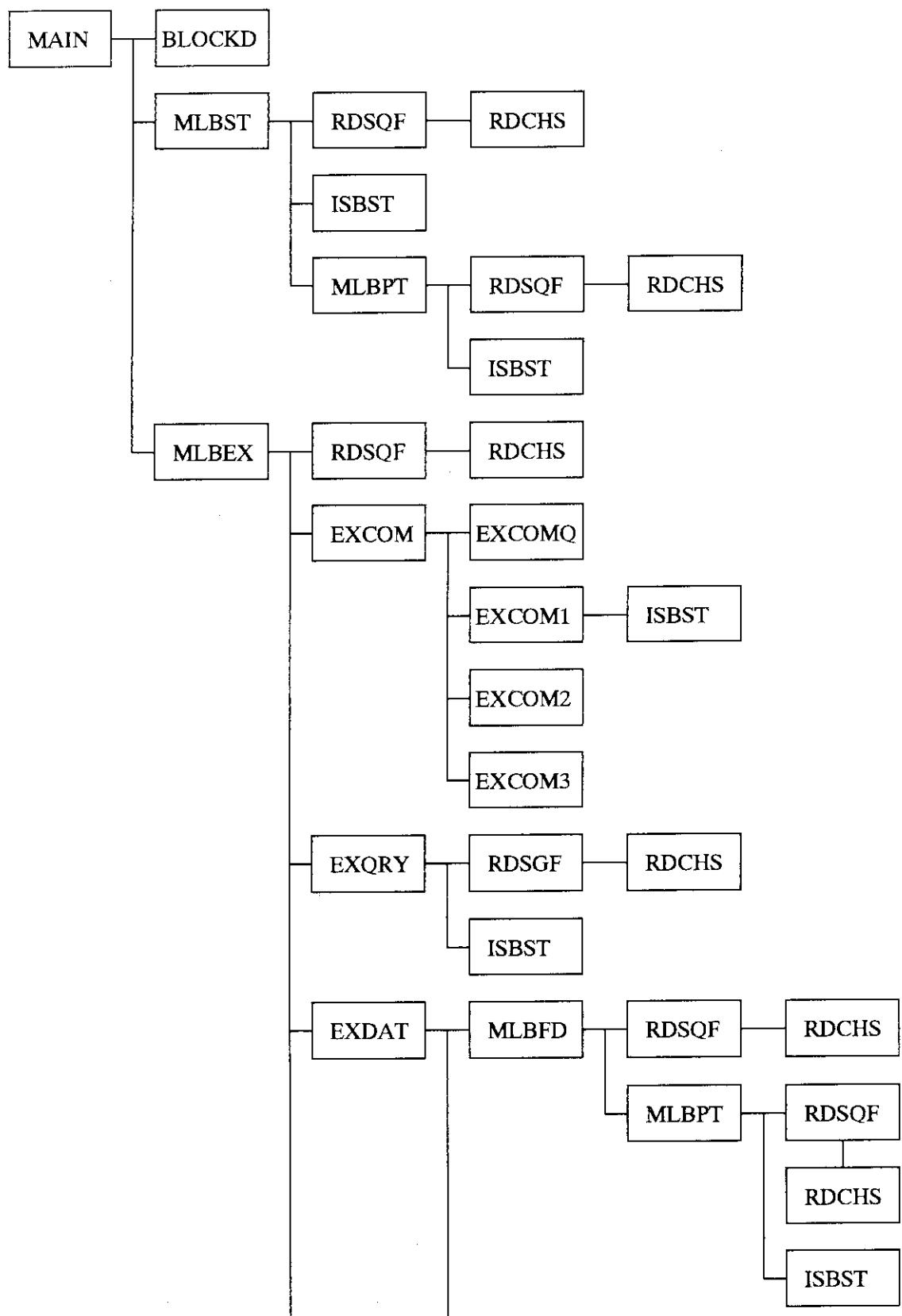


Fig. 4.1 Structure of computer program IMPACLIB(1/2)

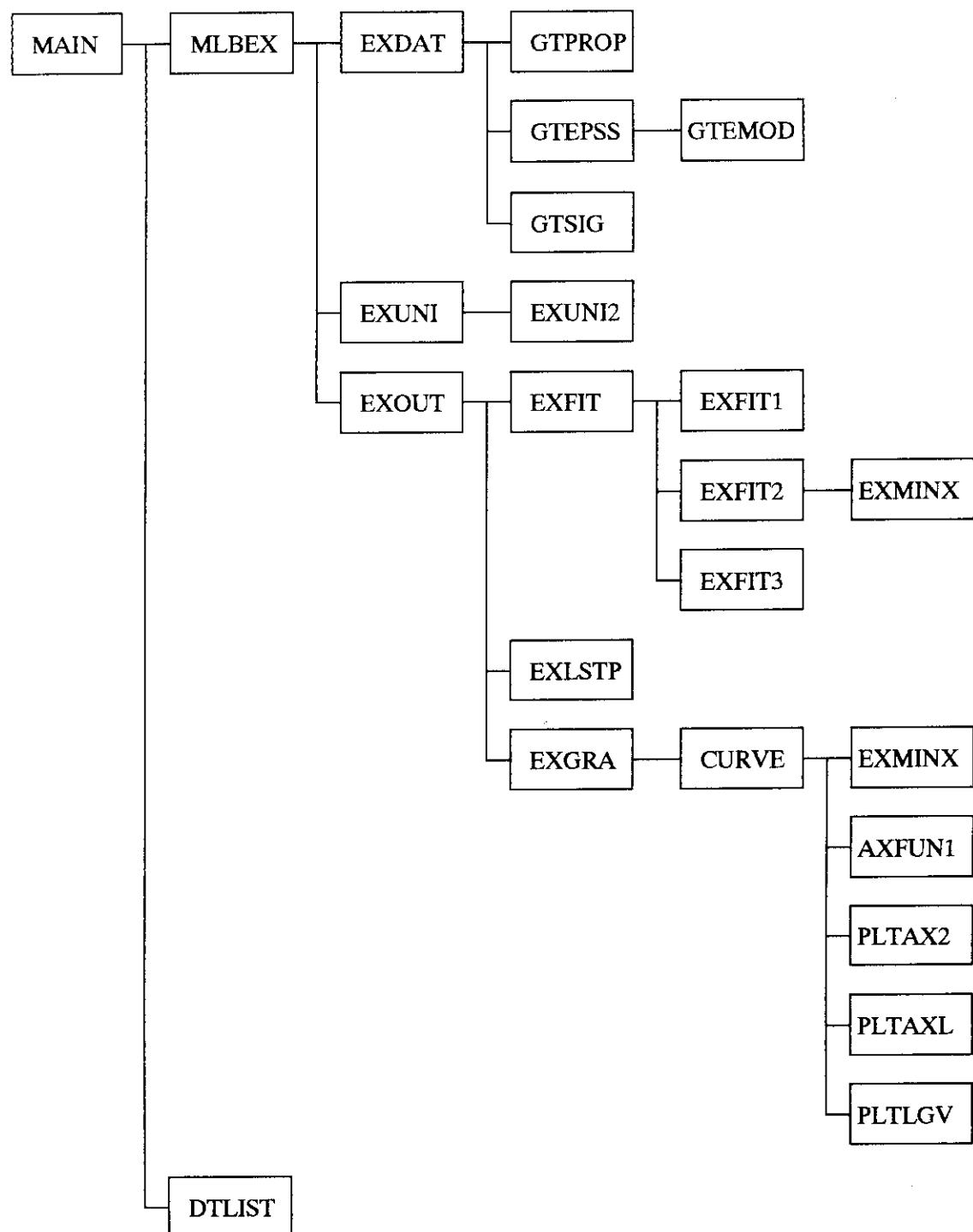


Fig. 4.1 Structure of computer program IMPACLIB(2/2)

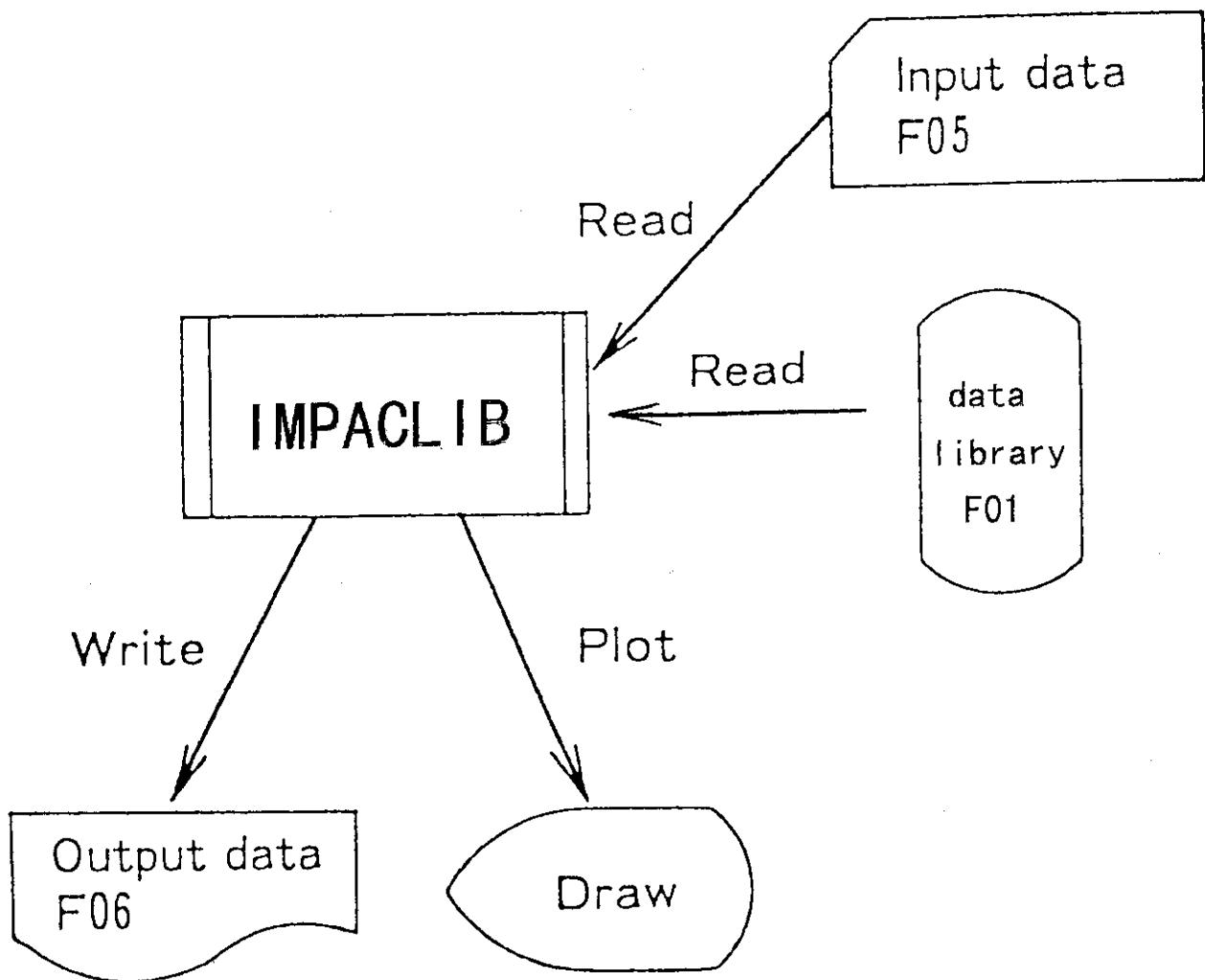


Fig. 4.2 Program flow

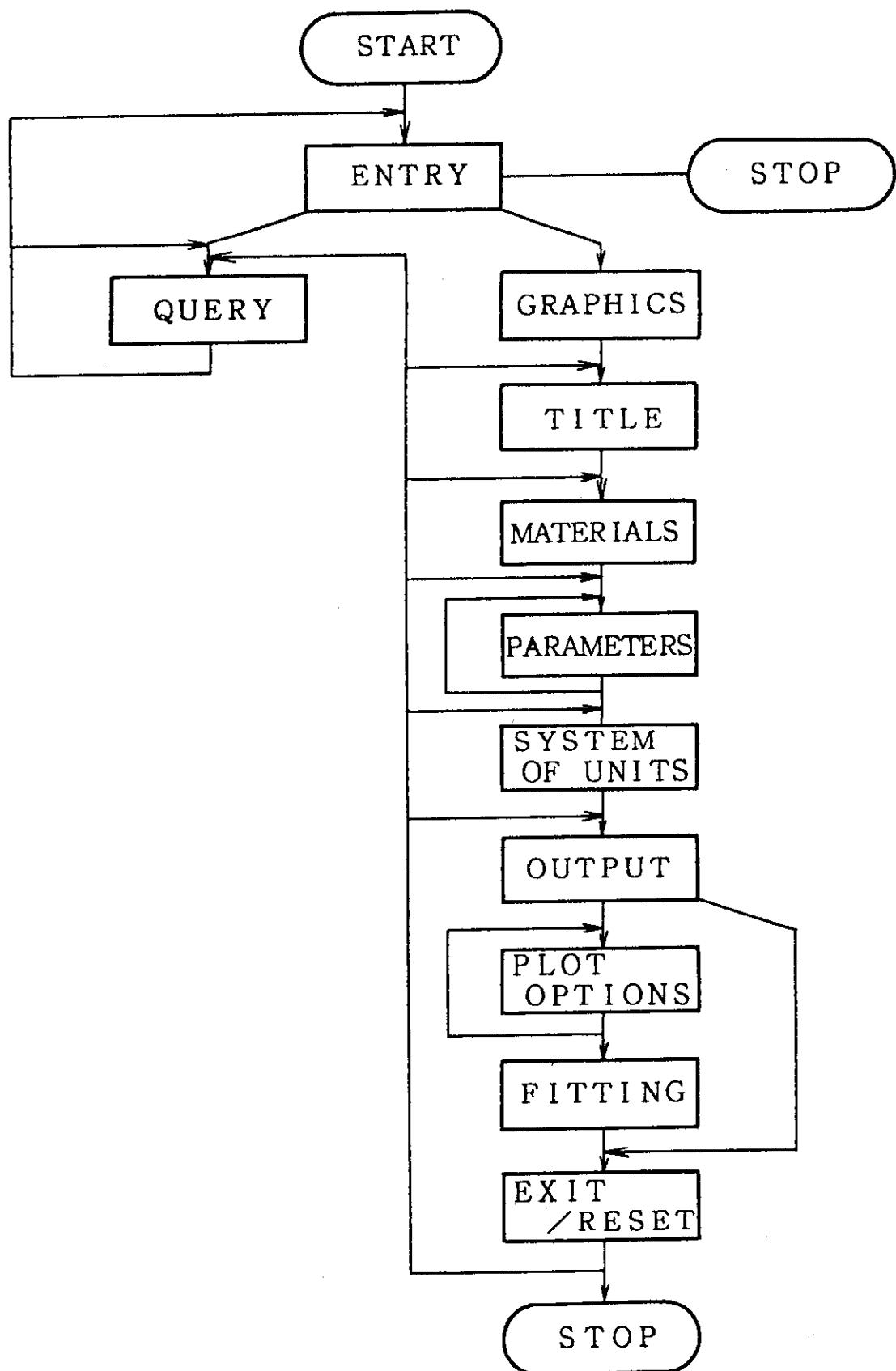


Fig. 4.3 Flow sheet of command

## 5. Conclusions

In regard to the evaluation of acceleration, deformation, stress and strain of casks in the case of drop impact, structural property data are necessary. A structural property data library IMPACLIB has developed for impact analysis programs such as DYNA2D, DYNA3D, NIKE2D, NIKE3D, PISCES, HONDO, CRUSH1, CRUSH2, FINCRUSH, PUNCTURE and so on. The IMPACLIB is further being utilized satisfactory for general purpose stress analysis programs.

## Acknowledgements

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## 5. Conclusions

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## Acknowledgements

The author is indebted Mrs. Junji Oshika and Takashi Ishiwata of CRC Research Institute, Inc. for assistance of making the computer program.

## References

- (1) Hallquist, J. O., "User's Manual for DYNA2D - Explicit Two-dimensional Hydro-dynamic Finite Element Code with Interactive Rezoning and Graphical Display", UCID-18756,Rev.3(1988).
- (2) Hallquist, J. O., "Use's Manual for DYNA3D(Nonlinear Dynamic Analysis of Structures in Three Dimensions)", UCID-18756,Rev.5(1989).
- (3) Hallquist, J. O., "NIKE2D: An Implicit, Finite-Deformation, Finite Element Code with Analyzing the Static and Dynamic Response of Two-Dimensional Solids", UCID-52678(1978).
- (4) Hallquist, J. O., "NIKE3D: An Implicit, Finite-Deformation, Finite Element Code with Analyzing the Static and Dynamic Response of Three-Dimensional Solids", UCID-18822(1981).
- (5) Trigg, M., et al., "PISCES user's Manual", Physics International(1980).
- (6) Key, S. W., Beisinger, Z. E. and Krieg, D., "HONDO-II - A Finite Element Computer Program for the Large Deformation Dynamic Response of Axisymmetric Solids", SAND 78-0442(1978).
- (7) Ikushima, T. et al., "Simplified Computer Codes for Cask Impact Analysis" , 10th Int. symposium on the Packaging and Transportation of Radioactive Materials, pp.1419-1426, Japan(Yokohama), (1992).
- (8) Ikushima, T., Oshika, J. and Ishiwata, T., "Computer Codes System for Structural Analysis of Radioactive Materials Transport" , 11th Int. symposium on the Packaging and Transportation of Radioactive Materials, pp.1174-1181, U.S.A(Las Vegas), (1995).
- (9) Ikushima, T. and Nagata, T., "A Compilation of Structural Property Data for Computer Impact Calculation (1/5), Volume 1 : Structural Property Data and Data Processing Computer Program", JAERI-M 88-191 (1988) (in Japanese).
- (10) Ikushima, T., "A Compilation of Structural Property Data for Computer Impact Calculation (2/5), Volume 2 : Mild Steel", JAERI-M 88-192 (1988) (in Japanese).
- (11) Ikushima, T., "A Compilation of Structural Property Data for Computer Impact Calculation (3/5), Volume 3 : Stainless Steel", JAERI-M 88-193 (1988) (in Japanese).
- (12) Ikushima, T., "A Compilation of Structural Property Data for Computer Impact Calculation (4/5), Volume 4 : Lead", JAERI-M 88-194 (1988) (in Japanese).

- (13) Ikushima, T., "A Compilation of Structural Property Data for Computer Impact Calculation (5/5), Volume 5 : Wood", JAERI-M 88-195 (1988) (in Japanese).
- (14) Ikushima, T., "CRUSH1 : A Simplified Computer Program for Impact Analysis of Radioactive Material Transport Casks", JAERI-Data/Code 96-025 (1996).
- (15) Ikushima, T., "CRUSH2 : A Simplified Computer Program for Impact Analysis of Radioactive Material Transport Casks", JAERI-Data/Code 97-001 (1997).
- (16) Ikushima, T., "FINCRUSH : A Computer Program for Impact Analysis of Radioactive Material Transport Cask with Fins", JAERI-Data/Code 97-018 (1997).
- (17) Ikushima, T., "PUNCTURE : A Computer Program for Puncture Analysis of Radioactive Material Transport Casks", JAERI-Data/Code 97-036 (1997).
- (18) Ikushima, T., "ROCKING : A Computer Program for Seismic Response Analysis of Radioactive Material Transport Casks", JAERI-Data/Code 95-017 (1995).
- (19) Ikushima, T., "FINLIB : A Fin Energy Absorption Data Library for Impact Analysis of Radioactive Material Transport Cask with Fins", JAERI-Data/Code 97-035 (1997).

Appendix A Sample Problem Input

```

INPUT DATA ECHO
      1   2   3   4   5   6   7   8
-----0---5---0---5---0---5---0---5---0---5---0
      2 'STRESS STRAIN CURVES OF STEEL TEMP.=293.0, *TITLE ? R-86
      5,1,1012 *MATERIALS ?
      3 290.0,295.0 *OPTION ?
      0           *TEMPERATURE RANGES ?
      1           *PARAMETERS ?
      11          *SYSTEM OF UNITS ?
      1           *OUTPUT ?
      0.0, 0.24, 0.0, 1600. *PLOT OPTIONS ?
      0           *DATA RANGES ?
      5           *PLOT OPTIONS ?
      1 'STRAIN RATE 2.1E-4 ! *CURVE NO. COMMENT
      2 'STRAIN RATE 2.1E-3 ! *CURVE NO. COMMENT
      3 'STRAIN RATE 2.1E-2 ! *CURVE NO. COMMENT
      4 'STRAIN RATE 2.1E-1 ! *CURVE NO. COMMENT
      5 'STRAIN RATE 9.9E-1 ! *CURVE NO. COMMENT
      6 'STRAIN RATE 1.3   ! *CURVE NO. COMMENT
      7 'STRAIN RATE 1.3E+1 ! *CURVE NO. COMMENT
      8 'STRAIN RATE 1.3E+2 ! *CURVE NO. COMMENT
      9 'STRAIN RATE 3.0E+2 ! *CURVE NO. COMMENT
      10 'STRAIN RATE 4.0E+2 ! *CURVE NO. COMMENT
      0 ,           *CURVE NO. COMMENT END
      0           *PLOT OPTIONS ?
      0           *END MARK
-----5---0---5---0---5---0---5---0---5---0
      1   2   3   4   5   6   7   8

```

## Appendix B Sample Problem Output

```

ENTRY? (0:1:2:3)
0; EXIT
1; QUERY
2; GRAPHICS
3; INPUT ECHO
>> 2
TITLE? ('')
>> STRESS STRAIN CURVES OF STEEL TEMP.=293.0
MATERIALS? (PROP,NMAT,MATNO,...)
PROPERTY
0; RETURN
1; COEFFICIENT OF THERMAL EXPANSION
2; MODULUS OF LONGITUDINAL ELASTICITY
3; MODULUS OF TRANSVERSE ELASTICITY
4; POISSON'S RATIO
5; STRESS-STRAIN
6; STRESS-STRAIN RATE
NMAT ; NUMBER OF MATERIALS
MATNO; MATERIAL NUMBER
>> 5 1 1012
PARAMETERS? (0:1:2:3:4:5)
0; RETURN
1; DEFORMATION TYPE
2; FIBRE DIRECTION OF WOOD
3; TEMPERATURE
4; STRAIN RATE
5; STRAIN
>> 3
TEMPERATURE? (MIN,MAX)
>> 290.000 295.000
PARAMETERS? (0:1:2:3:4:5)
0; RETURN
1; DEFORMATION TYPE
2; FIBRE DIRECTION OF WOOD
3; TEMPERATURE
4; STRAIN RATE
5; STRAIN
>> 0
SYSTEM OF UNITS? (1:2)
1; SI
2; MKS
>> 1
OUTPUT? (0:001:010:100)
0; RETURN
001; LISTING
010; PLOTTING
100; FITTING
>> 11
PLOT OPTIONS? (0:1:2:3:4:5)
0; RETURN
1; DATA RANGES
2; TYPE OF AXES
3; STRING
4; MESH
5; COMMENT OF CURVES
>> 1

```

## Appendix B (Continued)

```

DATA RANGES? (XMIN,XMAX,YMIN,YMAX)
XMIN; MINIMUM VALUE ON X-AXIS
XMAX; MAXIMUM VALUE ON X-AXIS
YMIN; MINIMUM VALUE ON Y-AXIS
YMAX; MAXIMUM VALUE ON Y-AXIS
>> 0.00 0.24 0.00 1600.00
PLOT OPTIONS? (0:1:2:3:4:5)
0; RETURN
1; DATA RANGES
2; TYPE OF AXES
3; STRING
4; MESH
5; COMMENT OF CURVES
>> 5
COMMENT OF CURVES? (CURVE-NO,'..COMMENT..')
CURVE-NO= 0; RETURN
> 0; DEFINITION
<11; DEFINITION
>> 1, STRAIN RATE 2.1E-4
COMMENT OF CURVES? (CURVE-NO,'..COMMENT..')
CURVE-NO= 0; RETURN
> 0; DEFINITION
<11; DEFINITION
>> 2, STRAIN RATE 2.1E-3
COMMENT OF CURVES? (CURVE-NO,'..COMMENT..')
CURVE-NO= 0; RETURN
> 0; DEFINITION
<11; DEFINITION
>> 3, STRAIN RATE 2.1E-2
COMMENT OF CURVES? (CURVE-NO,'..COMMENT..')
CURVE-NO= 0; RETURN
> 0; DEFINITION
<11; DEFINITION
>> 4, STRAIN RATE 2.1E-1
COMMENT OF CURVES? (CURVE-NO,'..COMMENT..')
CURVE-NO= 0; RETURN
> 0; DEFINITION
<11; DEFINITION
>> 5, STRAIN RATE 9.9E-1
COMMENT OF CURVES? (CURVE-NO,'..COMMENT..')
CURVE-NO= 0; RETURN
> 0; DEFINITION
<11; DEFINITION
>> 6, STRAIN RATE 1.3
COMMENT OF CURVES? (CURVE-NO,'..COMMENT..')
CURVE-NO= 0; RETURN
> 0; DEFINITION
<11; DEFINITION
>> 7, STRAIN RATE 1.3E+1
COMMENT OF CURVES? (CURVE-NO,'..COMMENT..')
CURVE-NO= 0; RETURN
> 0; DEFINITION
<11; DEFINITION
>> 8, STRAIN RATE 1.3E+2

```

## Appendix B (Continued)

```
COMMENT OF CURVES? (CURVE-NO?..COMMENT..')
  CURVE-NO= 0; RETURN
    > 0; DEFINITION
    <1> DEFINITION
  >> 9, STRAIN RATE 3.0E+2
COMMENT OF CURVES? (CURVE-NO?..COMMENT..')
  CURVE-NO= 0; RETURN
    > 0; DEFINITION
    <1> DEFINITION
  >> 10, STRAIN RATE 4.0E+2
COMMENT OF CURVES? (CURVE-NO?..COMMENT..')
  CURVE-NO= 0; RETURN
    > 0; DEFINITION
    <1> DEFINITION
  >> 0,
PLOT OPTIONS? (0:1:2:3:4:5)
  0; RETURN
  1; DATA RANGES
  2; TYPE OF AXES
  3; STRING
  4; MESH
  5; COMMENT OF CURVES
  >> 0
EXIT/RESET? (0:1:2:3:4:5:6)
  0; EXIT
  1; QUERY
  2; TITLE,...
  3; MATERIALS,...
  4; PARAMETERS,...
  5; SYSTEM OF UNITS
  6; OUTPUT
  >> 0
JWE0002I STOP EXIT
```

## Appendix C Graphical Output

MATERIAL (CURVE NO.1)	
NAME:	REFERENCES: R-86
NO.	1012
DEFORMATION TYPE	COMPRESSION
TEMPERATURE (K)	293.00
STRAIN RATE (1/S)	2.100E-04
STRAIN (-)	STRESS (MPA)
1.000E-02	3.530E+02
2.000E-02	4.020E+02
3.000E-02	4.610E+02
4.000E-02	5.050E+02
5.000E-02	5.390E+02
6.000E-02	5.640E+02
7.000E-02	5.880E+02
8.000E-02	6.080E+02
9.000E-02	6.220E+02
1.000E-01	6.370E+02
1.100E-01	6.520E+02
1.200E-01	6.620E+02
1.300E-01	6.760E+02
1.400E-01	6.820E+02
1.500E-01	6.910E+02
1.600E-01	6.960E+02
1.700E-01	7.060E+02
1.800E-01	7.150E+02
1.900E-01	7.250E+02
2.000E-01	7.300E+02

Fig. C.1 Graphical Output of IMPACLIB(1)

MATERIAL (CURVE NO.2)	
NAME:	REFERENCES: R-86
NO.	1012
DEFORMATION TYPE	COMPRESSION
TEMPERATURE (K)	293.00
STRAIN RATE (1/S)	2.100E-03
STRAIN (-)	STRESS (MPA)
1.000E-02	3.530E+02
2.000E-02	4.020E+02
3.000E-02	4.700E+02
4.000E-02	5.150E+02
5.000E-02	5.540E+02
6.000E-02	5.780E+02
7.000E-02	6.030E+02
8.000E-02	6.220E+02
9.000E-02	6.370E+02
1.000E-01	6.520E+02
1.100E-01	6.710E+02
1.200E-01	6.810E+02
1.300E-01	6.960E+02
1.400E-01	7.060E+02
1.500E-01	7.150E+02
1.600E-01	7.250E+02
1.700E-01	7.300E+02
1.800E-01	7.400E+02
1.900E-01	7.500E+02
2.000E-01	7.600E+02

Fig. C.2 Graphical Output of IMPACLIB(2)

## MATERIAL (CURVE NO.3)

NAME: S45C  
NO. 1012

REFERENCES: R-86

DEFORMATION TYPE	COMPRESSION
TEMPERATURE (K)	293.00
STRAIN RATE (1/S)	2.100E-02

STRAIN (-)	STRESS (MPA)
1.000E-02	3.720E+02
2.000E-02	4.170E+02
3.000E-02	4.800E+02
4.000E-02	5.240E+02
5.000E-02	5.640E+02
6.000E-02	5.980E+02
7.000E-02	6.170E+02
8.000E-02	6.370E+02
9.000E-02	6.570E+02
1.000E-01	6.710E+02
1.100E-01	6.820E+02
1.200E-01	6.960E+02
1.300E-01	7.110E+02
1.400E-01	7.200E+02
1.500E-01	7.250E+02
1.600E-01	7.350E+02
1.700E-01	7.450E+02
1.800E-01	7.500E+02
1.900E-01	7.600E+02
2.000E-01	7.690E+02

Fig. C.3 Graphical Output of IMPACLIB(3)

## MATERIAL (CURVE NO.4)

NAME: S45C  
NO. 1012

REFERENCES: R-86

DEFORMATION TYPE	COMPRESSION
TEMPERATURE (K)	293.00
STRAIN RATE (1/S)	2.100E-01

STRAIN (-)	STRESS (MPA)
1.000E-02	3.920E+02
2.000E-02	4.310E+02
3.000E-02	4.950E+02
4.000E-02	5.440E+02
5.000E-02	5.780E+02
6.000E-02	6.130E+02
7.000E-02	6.370E+02
8.000E-02	6.570E+02
9.000E-02	6.710E+02
1.000E-01	6.910E+02
1.100E-01	7.060E+02
1.200E-01	7.150E+02
1.300E-01	7.250E+02
1.400E-01	7.350E+02
1.500E-01	7.450E+02
1.600E-01	7.500E+02
1.700E-01	7.600E+02
1.800E-01	7.690E+02
1.900E-01	7.740E+02
2.000E-01	7.840E+02

Fig. C.4 Graphical Output of IMPACLIB(4)

## MATERIAL (CURVE NO.5)

NAME: S45C  
NO. 1012

REFERENCES: R-86

DEFORMATION TYPE	COMPRESSION
TEMPERATURE (K)	293.00
STRAIN RATE (1/S)	9.900E-01

STRAIN (-)	STRESS (MPA)
1.000E-02	4.610E+02
2.000E-02	4.410E+02
3.000E-02	4.900E+02
4.000E-02	5.390E+02
5.000E-02	5.780E+02
6.000E-02	6.080E+02
7.000E-02	6.370E+02
8.000E-02	6.570E+02
9.000E-02	6.760E+02
1.000E-01	6.910E+02
1.100E-01	7.060E+02
1.200E-01	7.200E+02
1.300E-01	7.300E+02
1.400E-01	7.350E+02
1.500E-01	7.450E+02

Fig. C.5 Graphical Output of IMPACLIB(5)

## MATERIAL (CURVE NO.6)

NAME: S45C  
NO. 1012

REFERENCES: R-86

DEFORMATION TYPE	COMPRESSION
TEMPERATURE (K)	293.00
STRAIN RATE (1/S)	1.300E+00

STRAIN (-)	STRESS (MPA)
1.000E-02	4.700E+02
2.000E-02	4.510E+02
3.000E-02	5.190E+02
4.000E-02	5.590E+02
5.000E-02	5.980E+02
6.000E-02	6.370E+02
7.000E-02	6.660E+02
8.000E-02	6.860E+02
9.000E-02	7.060E+02
1.000E-01	7.250E+02
1.100E-01	7.350E+02
1.200E-01	7.500E+02
1.300E-01	7.600E+02
1.400E-01	7.690E+02
1.500E-01	7.740E+02
1.600E-01	7.840E+02
1.700E-01	7.890E+02
1.800E-01	7.940E+02

Fig. C.6 Graphical Output of IMPACLIB(6)

MATERIAL (CURVE NO.7)

NAME: S45C REFERENCES: R-86  
NO. 1012

DEFORMATION TYPE	COMPRESSION
TEMPERATURE (K)	293.00
STRAIN RATE (1/S)	1.300E+01

STRAIN (-)	STRESS (MPA)
1.000E-02	4.900E+02
2.000E-02	5.000E+02
3.000E-02	5.190E+02
4.000E-02	5.980E+02
5.000E-02	6.370E+02
6.000E-02	6.650E+02
7.000E-02	6.960E+02
8.000E-02	7.150E+02
9.000E-02	7.250E+02
1.000E-01	7.350E+02
1.100E-01	7.450E+02

Fig. C.7 Graphical Output of IMPACLIB(7)

MATERIAL (CURVE NO.8)

NAME: S45C REFERENCES: R-86  
NO. 1012

DEFORMATION TYPE	COMPRESSION
TEMPERATURE (K)	293.00
STRAIN RATE (1/S)	1.500E+02

STRAIN (-)	STRESS (MPA)
1.000E-02	6.080E+02
2.000E-02	5.880E+02
3.000E-02	6.030E+02
4.000E-02	6.420E+02
5.000E-02	6.860E+02
6.000E-02	7.060E+02
7.000E-02	7.250E+02
8.000E-02	7.350E+02
9.000E-02	7.640E+02
1.000E-01	7.740E+02

Fig. C.8 Graphical Output of IMPACLIB(8)

MATERIAL (CURVE NO.9)  
 NAME: S45C  
 NO. 1012

REFERENCES: R-86

DEFORMATION TYPE	COMPRESSION
TEMPERATURE (K)	293.00
STRAIN RATE (1/S)	3.000E+02

STRAIN (-)	STRESS (MPA)
1.000E-02	5.980E+02
2.000E-02	5.880E+02
3.000E-02	6.270E+02
4.000E-02	6.660E+02
5.000E-02	6.950E+02
6.000E-02	7.250E+02
7.000E-02	7.500E+02
8.000E-02	7.740E+02
9.000E-02	8.040E+02
1.000E-01	8.230E+02
1.100E-01	8.330E+02
1.200E-01	8.430E+02
1.300E-01	8.470E+02
1.400E-01	8.520E+02

Fig. C.9 Graphical Output of IMPACLIB(9)

MATERIAL (CURVE NO.10)  
 NAME: S45C  
 NO. 1012

REFERENCES: R-86

DEFORMATION TYPE	COMPRESSION
TEMPERATURE (K)	293.00
STRAIN RATE (1/S)	4.000E+02

STRAIN (-)	STRESS (MPA)
1.000E-02	5.880E+02
2.000E-02	6.080E+02
3.000E-02	6.370E+02
4.000E-02	6.760E+02
5.000E-02	7.110E+02
6.000E-02	7.350E+02
7.000E-02	7.600E+02
8.000E-02	7.790E+02
9.000E-02	7.980E+02
1.000E-01	8.130E+02
1.100E-01	8.280E+02
1.200E-01	8.370E+02
1.300E-01	8.530E+02
1.400E-01	8.820E+02
1.500E-01	8.920E+02
1.600E-01	9.020E+02
1.700E-01	9.070E+02
1.800E-01	9.110E+02
1.900E-01	9.210E+02
2.000E-01	9.210E+02

Fig. C.10 Graphical Output of IMPACLIB(10)

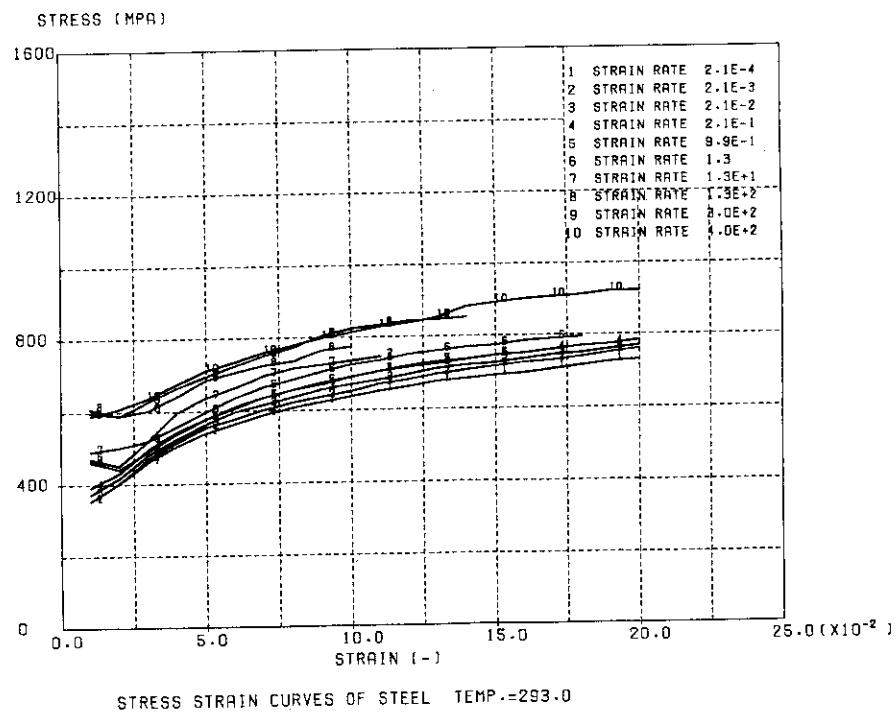


Fig. C.11 Graphical Output of IMPACLIB(11)

## Appendix D Job Control Data

The job control data for IMPACLIB execution on the computer FACOM M-780 in JAERI is as follows:

```

//JCLG JOB
// EXEC JCLG
//SYSIN DD DATA,DLM='++'
// JUSER XXXXXXXX.XX,XXXXXXXX,XXXX.XX,IMPLIB
// T.01 C.02 W.01 I.02 CLS GRP
// OOPTP MSGCLASS=A,MSGLEVEL=(2,0,1),CLASS=B,NOTIFY=JXXXX
// OOPTP PASSWORD=XXXXXXXX
// EXEC LMGOEX,LM=J2322.LMIMPLIB,PNM=IMPACLIB
// EXPAND GRNLP
//SYSIN      DD DSN=JXXXX.DTIMPLIN.DATA,DISP=SHR,LABEL=(,,IN)
//FT01F001 DD DSN=JXXXX.DTFINDAT.DATA,DISP=SHR
//FT02F001 DD DSN=SPACE=(TRK,(5,5)),UNIT=TSSWK
//FT20F001 DD DSN=JXXXX.DTIMPLIB.DATA,DISP=SHR
++
//

```

## Appendix E Program Abstract

1. Name :  
IMPLIB.
2. Computer for which the program is designed and others upon which it is possible:  
FACOM M-780, SUN4 or IBM-PC.
3. Nature of physical problem solved:  
Structural data at high speed test from USA and Japanese experimental data.
4. Method of solutions:
5. Restrictions on the complexity of the problem:  
None.
6. Typical running time:  
FACOM-M780 : 1 seconds.  
SUN4 : 2 seconds.  
IBM-PC : 3 seconds.
7. Unusual features of the program:  
None.
8. Related and auxiliary program:  
None.
9. Status:
10. References:
  - (1)Ikushima,T. and Hode S., "Simplified Analysis Computer Program and Their Adequacy for Radioactive Materials Shipping casks", PATRAM'89,pp.1202-1209, Washington DC, USA June 11-16,(1989).
  - (2)Ikushima,T. et al., "Simplified Computer Codes for Cask Impact Analysis", PATRAM'92, pp.1419-1426, Yokohama, Japan, September 13-18,(1992).
  - (3)Ikushima,T., Ohshika,J. and Ishiwata,T., "Computer Code System for Structural Analysis of Radioactive Materials Transport", PATRAM'95, pp.1174-1181, Las Vegas, USA, December 3-8,(1995).
  - (4)Ikushima,T., "FINCRUSH-A Computer Program for Impact Analysis of Radioactive Material Transport Cask with Fins", JAERI-Data/Code 97-018(1997).
11. Machine requirement:  
Required 1100 k bytes of core memory.
12. Program language used:  
FORTRAN-77.
13. Operating system or monitor under which the program is executed:  
FACOM M-780 : MSP.  
SUN4 : Solaris 2.1.  
IBM PC : Windows 3.1.
14. Any other programming or operating information or restrictions:  
The program is approximately 3800 source steps(including comment lines).  
The graphical programs are as follows:  
FACOM M-780 : CALCOMP plotter or the compatible ones.  
SUN4 : X-windows.  
IBM PC : windows 3.1.
15. Name and establishment of author:  
T. Ikushima  
Japan Atomic Energy Research Institute,  
Tokai Research Establishment,  
Department of Fuel Cycle Safety Research,  
Tokai-mura, Naka-gun, Ibaraki-ken, 319-11  
Japan
16. Material available:  
Program source and data library.

## Appendix F Program Source List

```

***** MAIN PROGRAM *****
C      MATERIAL DATA LIBRARY FOR 'CASKEITSS'
*****
COMMON /MLBALC/ LMLB, IMA1,IMA2,IMA3,IMA4,IMA5,IMA6,IMA7,IMA8
1      , IMA9,IMA10,IMA11,IMA12,IMA13,IMA14,IMA15,IMA16
2      , IMA17,IMA18
COMMON /MLBMAX/ MMLB, MMAT, MCS, MSS, MPB, MWD, MPTEMP, MWDFIB
1      , MTEMP, MEPSR, MEPSS, MREFF, MCOMM
COMMON /      / MLB(50000)
C
IADJST (IMA) = (IMA+2)/2+2-1
C
CALL DTLIST(5,6)
C* MEMORY ALLOCATION *
LMAT = 18+8*MPTEMP+(2+3*MEPSR)*MTEMP+MEPSS + 10
LMAT0 = 5*(MCS+MSS+MPB+MWD)+12*MMAT+4*MWDFIB+MWD+2*MREFF+20*MCOMM
MMLB = (MLB-LMAT)/LMAT
IF (MMLB.LE.0) THEN
LMAT = LMAT-LMAT0
WRITE(6,6100) LMAT, LMLB
6100 FORMAT( 22H0 **** ERROR ****
1   / 3H      INSUFFICIENT WORKING AREA
2   / 23H     NECESSARY ...IB
3   / 23H     GIVEN .....IB )
STOP 'QUIT'
ENDIF
C
IMA1 = 1
IMA2 = IMA1 +5*MCS
IMA3 = IMA2 +5*MSS
IMA4 = IMA3 +5*MPB
IMA5 = IMA4 +5*MWD
IMA6 = IMA5 +12*MMAT
IMA7 = IMA6 +MMLB*10
IMA7 = IADJST (IMA7)
IMA8 = IMA7 +MMLB*2
IMA9 = IMA8 +MMLB*MPTEMP*B
IMA10 = IMA9 +MMLB*4
IMA11 = IMA10+MWDFIB*MWD*2
IMA12 = IMA11+MWDFIB*MWD*2
IMA12 = IADJST (IMA12)
IMA13 = IMA12+MMAT*MTEMP
IMA14 = IMA13+MMLB*MTEMP
IMA14 = IADJST (IMA14)
IMA15 = IMA14+MMLB*MTEMP*MEPSR
IMA16 = IMA15+MMLB*MTEMP*MEPSR*2
IMA16 = IADJST (IMA16)
IMA17 = IMA16+MEPSS*MMLB
IMA18 = IMA17+MREFF*2
CALL MLBST ( MLB(IMA1), MLB(IMA2), MLB(IMA3), MLB(IMA4)
1      , MLB(IMA5), MLB(IMA6), MLB)
CALL MLBEX (MLB)
STOP 'EXIT'
END

```

## Appendix F (Continued)

```

BLOCK DATA
CHARACTER=8      AMAT1, ANAME, UNAME
CHARACTER=4      ATITLE, XXNAME, YYNAME, IEQCF, ICYNAME, CQRD
CHARACTER=4      CDA
CHARACTER      IRCCBF2=4
CHARACTER      IRCCBF1=1
COMMON /COMPL1/ ATITLE(18), XXNAME(10), YYNAME(10)
1      , XDATA( 50*20), YDATA( 50*20)
COMMON /COMPL2/ PMIN, PMAX, PYMIN, PYMAX, XL1, YL1, NPLOT
1      , NDATA, NDATA(20), NGRAPH
COMMON /COMPL3/ AMAT1(20), ANAME(20), UNAME(3)
COMMON /MLBALC/ LMLB, IMA1,IMA2,IMA3,IMA4,IMA5,IMA6,IMA7,IMA8
1      , IMA9,IMA10,IMA11,IMA12,IMA13,IMA14,IMA15,IMA16
2      , IMA17,IMA18
COMMON /MLBFND/ IFNC, IFNM, IFNP, IFNR
COMMON /MLBFT1/ KFIT, IEQFIT, NCDEF(16), COEF(6), COEFO(6/16)
1      , MXY, NYD(5), XYD(2*50,5), MXY, NYD
COMMON /MLBFT2/ NERCF(16), IEQCF(6/16)
COMMON /MLBIOX/ IMAT, IMAT, ICS, ISS, IPB, IND, JWDIB, JTEMP
1      , JEPSR, JREFF
COMMON /MLBMAX/ MMLB, MMAT, MCS, MSS, MPB, MWD, MPTEMP, MWDFIB
1      , MTEMP, MEPSR, MEPSS, MREFF, MCOMM
3      , MWD, NTMP, NEPSR, NEPS, NREFF, NCOMM
COMMON /MLBNUM/ MMAT, NMAT, NSS, NPB, NWD, NPROD(5), NDT
1      , NMDF, NTMP, NEPSR, NEPS, NREFF, NCOMM
COMMON /MLBPL1/ JAKES(2), KNESH, KCVNAM, JCVNAM(20), JCVNAM(5,20)
COMMON /MLBPR1/ KRFM1, KRFM2, KEYC, NRFM, NRM, IRFM(10), KARG(4)
COMMON /MLBPF1/ KRFC(8), IRFC(10-8), RRFC(2-10-8), KSYSU
COMMON /MLBPF2/ MRFX, MRFX, ICMD(8-20), RCND(8-20), NXEPS(20)
1      , XEPS(50,20), XSI(50-20), NRFXX, JRFXX(2,20)
COMMON /MLBPF3/ ICMD(8,20), RCND(8,20)
COMMON /MLBTCS/ ICPS, ITERM, ISCAL, XGO, YGO
COMMON /RDBUF1/ MDRF, IFMS(13), IFMBF2(100), ICBSBF(2,3)
1      , ICBCF1(80), IPDSR(3)
COMMON /RDBUF2/ IRCCBF2(4/30,3)
COMMON /RDBUF3/ CDA(10), IDA(10), RDA(50)
C
C* /COMPL1/ *
DATA ATITLE, XXNAME, YYNAME /
1 18*4H    10*4H    10*4H    /
C
C* /COMPL2/ *
DATA NPLOT,NDATA,NGRAPH /
1      0      0      0      /
C
C* /MLBALC/ *
DATA LMLB    / 50000 /
C* /MLBFND/ *
DATA IFNC,IFNM,IFNP,IFNR /
1      5, 11, 20, 10 /
C* /MLBFT1/ *
DATA KFIT,IEQFIT,NCDEF /
1      0, 0, 2*4,4,4,4,4,4,3*4,0,3*4,5*2,3*0 /
DATA COEF / 6*0.          /
DATA COEFO / 96*0.          /
DATA NYX,NYD, XYD,MXY,NKYD /
1      0, 5*0, 500*0., 5, 50 /
C* /MLBFT2/ *
DATA NERCF / 2*3,4,4,3*4,6,3*4*4,3*3,5*2,3*0 /
DATA IEQCF / 4*H, K, 4H ) ,
4*4H

```

```

Appendix F (Continued)

1   / 4HN, K, 4H, C,, 4H E ),          3*4H
2   / 4HN, K, 4H, S1, 4H-0,, 4H E ),    2*4H
3   / 4HN, K, 4H, S1, 4H-C,, 4H E ),    2*4H
4   / 4HL, M, 4H, N,, 4H K ),          3*4H
5   / 4HN, A, 4H, S1, 4H-0,, 4H E ),    2*4H
6   / 4HM, S, 4H-0-C, 4H, S1, 4H6-IN, 4HF, E, 4H ) 3*4H
7   / 4HN, A, 4H, B, > 4H) ,          3*4H
8   / 4HC, H, 4H, P,, 4H SIG, 4H-0 ),    2*4H
9   / 4HN, K, 4H0,..., 4H,, K, 4HN ) , 2*4H
*   / 4HN, A, 4H, B, > 4H) ,          3*4H
A   / 4HM, M, 4H, K,, 4H C ),          3*4H
B   / 4HM, C, 4H, H,, 4H SIG, 4H-Y, > 4HE ) , 4H
C   / 4HK, C, 4H ) ,                  4*4H
D   / 4HM, N, 4H, K, > 4H) ,          3*4H
E   /                                         6*4H  /
C* /MLBIDX/*      DATA JMAT,IMAT,ICS,ISS,IPB,IWD,JWDFIB,JTEMP,JEPSR,JREFF /
1   O, O / 100, 30, 50, 30, 30, 20, 6, 20, 20, 500 /
C* /MLBMAX/*      DATA NMMLB,NMMAT,NCS,NSS,NPB,NWD,NPROP,NOFT,NWDF,NTMP,NEPSR,NEPS /
1   O, O, O, O, O, O, 5*O, O, O, O, O, O, O / 100, 100 /
2   ,NREFF,NCOMM /
3   ,O, O /
C* /MLBNUM/*      DATA NMNLB,NMNT,NCS,NSS,NPB,NWD,NPROP,NOFT,NWDF,NTMP,NEPSR,NEPS /
1   O, O, O, O, O, O, 5*O, O, O, O, O, O, O / 100, 100 /
2   ,NREFF,NCOMM /
3   ,O, O /
C* /MLBPL1/*      DATA IAXES,KMESH /
1   2*O, 1 /
C* /MLBQR1/*      DATA KQR, IQRD, CQRD, JIQRD, JCQRD /
1   10*O, 10*O, 40*4H , 1, 1 /
C* /MLBRF1/*      DATA KRFM1,KRFM2,KECG,MRFM,NRFM,IRFM, KARG /
1   O, O, O, 10, 0,10*O, 3*O, 1 /
DATA NRFC, KSYSU /
1   8*O, 1 /
C* /MLBRF2/*      DATA MRFX, NRFX, NRFXX /
1   20, O, O /
C* /MLBTS/*       DATA ICPS, ITERM, ISCAL, X60, Y60 /
1   120, 3, 1024, 0, 0, 0 /
C* /RDBUF1/*      DATA MBF1,FBMF1, JFNBF2,ICMSBF,IPOSR /
1   3, 3*O, 100*O, 6*O, 3*O /
C* /RDBUF3/*      DATA CDA / 10*, * /
DATA IDA / 10*O, * /
DATA RDA / 50*O, * /
C* /COMPL2/*      DATA XL1 / 200, /
DATA YL1 / 160, /
END

```

Appendix F (Continued)

```

SUBROUTINE MLB8T ( NAMCS, NAMSS, NAMPB, NAMWD, NAMMAT, MATDIR
1      , MLB$ )
C
      INTEGER      NAMCS(5,1), NAMSS(5,1), NAMPB(5,1), NAMWD(5,1)
      INTEGER      NAMMAT(12,1), MATDIR(10-1)
      INTEGER      MLB(12)
COMMON /MLBLNO/ IFNC, IFNM, IFNP, IFMR
COMMON /MLB1DX/ JMAT, IMAT, ICS, ISS, IPB, IWD, JWDFIB, JTTEMP
1      , JEPSR, JREFF
COMMON /MLBALC/ LMBL, IMAI1,IMA2,IMA3,IMA4,IMA5,IMA6,IMA7,IMA8
1      , IMAI9,IMA10,IMA11,IMA12,IMA13,IMA14,IMA15,IMA16
2      , IMAI17,IMA18
COMMON /MLBMAX/ MMBL, NMAT, MCS, NSS, MFB, NWB, MPTEMP, MWDFIB
1      , MTEMP, MPESR, MEPSR, MREFF, MCMM
COMMON /MLBNUM/ NMBL, NMAT, MCS, NSS, NFB, NWB, NPROP(5), NDFT
1      , NWDF, NTMP, NEPSR, NEPS, NRFFF, NCMM
COMMON /MLBREF1/ KRFM1, KRFM2, KEXC, MRFM, NRFM, IRFM(30), KARG(4)
1      , NRC(30), IRFC(10-8), RRFC(2>10-8), KSYSU
COMMON /RDBUF3/ CDA(10), IDA(10), RDA(50)
CHARACTER*4 CDA
INTEGER      KMTYP(4), IFMT1(2,3)
CHARACTER*4 KEND, KMATE
C
      DATA KMTYP / 2000, 3000, 4000, 5000 /
      DATA IFMT1 / 101, 0, 104, 0, 201, 0 /
      DATA KEND / KMATE /
2      'END ', 'MAT ' /
C
      CALL RDSQF (0,IFNM, IFMT1 /0, KSTAT, CDA, IDA, RDA, JPOSR)
100    CONTINUE
      IFMT1(2,1) = 0
      CALL RDSQF (1,IFNM, IFMT1(1,1) /1, KSTAT, CDA(1), IDA, RDA
1      , JPOSR)
      IF ( CDA(1).EQ.KEND .OR. CDA(1).EQ.KMATE )      GOTO 140
C*  ERROR *
      WRITE(*,6120) CDA(1)
6120  FORMAT(2Z20) ***** ERROR *****
1      / 34H      INCORRECT HEADER LABEL ... ',A4,1H' )
      GOTO 100
C
      140 IF ( NMAT.GT.0 ) *
      *NMAT(2:NMAT) = JPOSR-NAMMAT(1,NMAT)-1
      IF ( CDA(1).EQ.KEND )      GOTO 400
      NMAT      = NMAT+1
      IMAT      = NMAT
      NMAT(1:NMAT) = JPOSR-1
      IFMT1(2,2) = 0
      IFMT1(2,3) = 0
      CALL RDSQF (1,IFNM, IFMT1(1,2) /2, KSTAT, CDA(1), IDA
1      , JPOSR)
C
      DO 160 I=1,4
      IF ( CDA(1).GE.KMTYP(I) )      GOTO 160
      IMTYP = I
      GOTO 200
160    CONTINUE
C*  ERROR *
      WRITE(*,6180) IDA(1)
6180  FORMAT(2Z20) ***** ERROR *****

```

```

        Appendix F (Continued)

      / 33H     MISSING MATERIAL NUMBER ...IB )
      GOTO 100

C   200 NAMMAT(5,NMAT) = ISBST(CDA(1))
      NAMMAT(6,NMAT) = ISBST(CDA(2))
      NAMMAT(7,NMAT) = ISBST(CDA(3))
      NAMMAT(8,NMAT) = ISBST(CDA(4))
      NAMMAT(9,NMAT) = ISBST(IDA(1))
      NAMMAT(10,NMAT)= 0
      NAMMAT(11,NMAT)= 0
      NAMMAT(12,NMAT)= 0
      IWD      = 0
      GOTO ( 210,220,230,240 ), INTYP
210 NCS      = NCS+1
      NXX      = NCS
      DO 215 I= 1,4
      NAMSS(1,NCS) = ISBST(CDA(1))
215 CONTINUE
      GOTO 300
220 NSS      = NSS+1
      NXX      = NSS
      DO 225 I= 1,4
      NAMSS(1,NSS) = ISBST(CDA(1))
225 CONTINUE
      GOTO 300
230 NPB      = NPB+1
      NXX      = NPB
      DO 235 I= 1,4
      NAMPB(1,NPB) = ISBST(CDA(1))
235 CONTINUE
      GOTO 300
240 NWD      = NWD+1
      NXX      = NWD
      IWD      = NWD
      DO 245 I= 1,4
      NAMWD(1,NWD) = ISBST(CDA(1))
245 CONTINUE
      300 IF ( .NMAT.LE..MMBLB ) THEN
          JMAT = NMAT
          NMLB = NMAT
          MATDIR(1,JMAT) = JMAT
          MATDIR(2,JMAT) = NMAT
          MATDIR(3,JMAT) = INTYP
          MATDIR(4,JMAT) = NAMMAT(9,NMAT)
          ELSE
              JMAT = 0
          ENDIF
          NAMMAT(3,NMAT) = JMAT
          NAMMAT(4,NMAT) = INTYP*1000+NXX
          CALL MLBPT ( NAMMAT(1,1), MLB(IMA6), MLB(IMA7), MLB(IMA8),
            , MLB(IMA9), MLB(IMA10), MLB(IMA11), MLB(IMA12),
            , MLB(IMA13), MLB(IMA14), MLB(IMA15), MLB(IMA16),
            , MLB(IMA17), MLB(IMA18),
            , MPTMP2,MWDFIB,MTEMP,MEPSR,MEPSS)
2        GOTO 100
400 KRFM1 = 1
      KRFM2 = NMLB
      CALL RDSQF ( 4,IFNM, IFMT1 >, KSTAT, CDA, IDA, RDA, JPSR)
      RETURN
      END

        Appendix F (Continued)

SUBROUTINE MLBPT (NAMMAT, MATDIR, PRDP1, PRDP2, IDFTYP, WDFIBR
1           , WDFIB, DTEMP, ITEMP, DEPSR, IEPSR, EPSS
2           , INEFF, ICOMM
3           , MPTMP2,MWDFIB,MTEMP,MEPSR,MEPSS)
C
      INTEGER   NAMMAT(12,1), MATDIR(10,1), IDFTYP(2,2,1)
      INTEGER   WDFIBR(2,MWDFIB,1)
      INTEGER   IWFIB(2,MWDFIB,1), ITEMP(MTEMP,1)
      INTEGER   IEPSR(2,MEPSR,MTEMP,1)
      INTEGER   IREF(2,1), ICOMM(20,1)
      REAL      PRDP1(4,1), PRDP2(MPTMP2,4,1)
      REAL      DTEMP(MTEMP,1), DEPSR(MEPSR,MTEMP,1)
      REAL      EPSS(MEPSS,1)
      COMMON /MLBNUM/ NMLB, NMAT, NCS, NSS, NPB, NWD, NPROP(5), NDIT
1      , NWDF, NTMP, NEPSR, NEPS, NREFF, NCOMM
      COMMON /MLBIDK/ JMAT, IMAT, IC5, ISS, IPB, IWD, JWDFIB, JTEMP
1      , JEPSR, JREF
      COMMON /MLBFNO/ IFNC, IFNM, IFNP, IFNR
      COMMON /RDBUF3/ CDA(10), IDA(10), RDA(50)
      CHARACTER*4 CDA
C
      CHARACTER*4 KSSR, KSSR2, KREF, KCOM, KDFTO, KWDFO, KBLNK
      CHARACTER*4 KDFTYP(4)
      INTEGER   IFMT1(2,15), IFMT2(2,10), IFMT3(2,4), IFMT4(2,3)
C
      DATA KSSR / 'SSR' /
      DATA KSSR2 / 'SSR2' /
      DATA KREF / 'REF' /
      DATA KCOM / 'COM' /
      DATA KDFTYP / 'C  ', 'T  ', 'C&T  ', 'CT  ' /
      DATA KDFTO / '  ' /
      DATA KWDFO / '  ' /
      DATA KBLNK / '  ' /
      DATA IFMT1 / 101, 0, 104, 0, 201, 0, 201, 0, 201, 0, 201, 0
1      , 201, 0, 201, 0, 301, 0, 301, 0, 301, 0, 301, 0
2      , 301, 0, 301, 0, -2, 0 /
      DATA IFMT2 / 101, 0, 301, 0, 101, 0, 101, 0, 201, 0, 301, 0
1      , 201, 0, 301, 0, 301, 0, -2, 0 /
      DATA IFMT3 / 101, 0, 201, 0, 102, 0, -1, 0 /
      DATA IFMT4 / 101, 0, 120, 0, -1, 0 /
      DATA MXEPSS / 0 /
C
      DO 10 I= 4,12
10 IFMT1(2,I) = 0
      CALL RDSQF ( 1,IFNM, IFMT1(1,4) >, KSTAT, CDA, IDA(1), RDA(1)
1           , JPSR)
      DO 20 J= 1,5
      NPROP(I)= IDA(I)
20 CONTINUE
C
      IF ( JMAT.GT.0 ) THEN
          MATDIR(2,JMAT) = IMAT
          MATDIR(3,JMAT) = NAMMAT(4,IMAT)/10000
          MATDIR(4,JMAT) = NAMMAT(9,IMAT)
          DO 40 I= 1,4
          MATDIR(1+I,JMAT) = NPROP(I)
          PRDP1(1,JMAT) = RDA(I)
40 CONTINUE
      ENDIF

```

```

Appendix F (Continued)

DO BO I= 1,4
IF ( NPROP(I).GT.0 ) THEN
NITM = NPROP(I)+NPROP(I)
CALL RDSQF (1,IFNM, IFMT1(1,13) ,NITM, KSTAT, CDA, IDA, RDA(1)
1 , JPOSR)
IF ( JMAT.GT.0 ) THEN
DO 60 J= 1,NITM
PROP2(J,I,JMAT) = RDA(J)
60 CONTINUE
ENDIF
ENDIF
BO CONTINUE
C CALL RDSQF (3,IFNM, IFMT3(1,1) ,1, KSTAT, CDA(1), IDA, RDA
1 , JPOSR)
IF ( CDA(1).EQ.KREF ) THEN
CALL RDSQF (1,IFNM, IFMT3(1,1) ,2, KSTAT, CDA(1), IDA(1), RDA
1 , JPOSR)
IF ( IDA(1).GT.0 ) THEN
JREFF = NREFF+1
NREFF = NREFF+IDA(1)
NAMAT(1,1,IMAT) = JREFF
NAMAT(1,2,IMAT) = IDA(1)
CALL RDSQF (1,IFNM, IFMT3(1,3) ,IDA(1), KSTAT, IREF(1,JREFF)
1 , IDA, RDA, JPOSR)
ENDIF
CALL RDSQF (3,IFNM, IFMT3(1,1) ,1, KSTAT, CDA(1), IDA, RDA
1 , JPOSR)
ENDIF
C IF ( CDA(1).EQ.KCOM ) THEN
NCOMM = NCOMM+1
CALL RDSQF (1,IFNM, IFMT4(1,1) ,1, KSTAT, CDA(1), IDA, RDA
1 , JPOSR)
C CALL RDSQF (1,IFNM, IFMT4(1,2) ,5, KSTAT, IC0MM(1,NCOMM), IDA
CALL RDSQF (1,IFNM, IFMT4(1,2) ,1, KSTAT, IC0MM(1,NCOMM), IDA
1 , RDA, JPOSR)
C IF ( JMAT.GT.0 )
*MATDIR(10,JMAT) = NCOMM
ENDIF
C IF ( NPROP(5).GT.0 ) THEN
NSSR = NPROP(5)
KDFTO = KBLNK
KWDFO = KBLNK
JWDFIB= 0
JTEMP = 1
JDFT = 1
JEPSS = 1
IF ( JMAT.GT.0 ) THEN
IDFTYP(1,1,JMAT) = 0
IDFTYP(2,1,JMAT) = 0
IDFTYP(1,2,JMAT) = 0
IDFTYP(2,2,JMAT) = 0
ENDIF
C DO 300 J= 1,NSSR
100 CONTINUE
IFMT2(2,1) = 0

```

```

Appendix F (Continued)

CALL RDSQF (1,IFNM, IFMT2(1,1) ,1, KSTAT, CDA(1), IDA, RDA
1 , JPOSR)
IF ( CDA(1).NE.KSSR )
*AND.CDA(1).NE.KSSR2) GOTO 100
IFMT2(2,4) = 0
IFMT2(2,5) = 0
IFMT2(2,6) = 0
IFMT2(2,7) = 0
CALL RDSQF (1,IFNM, IFMT2(1,2) ,4, KSTAT, CDA(2), IDA(1), RDA(1)
1 , JPOSR)
C IF ( JMAT.GT.0 ) THEN
IF ( MATDIR(3,JMAT).EQ.4 ) THEN
IF ( CDA(3).NE.KWDFD ) THEN
JWDFIB= JWDFIB+1
KWDFD = CDA(3)
WDFBRI(1,JWDFIB,IWD) = 15B5T(CDA(3))
IWDFIB(1,JWDFIB,IWD) = JTEMP
ENDIF
IWDFIB(2,JWDFIB,IWD) = JTEMP-IWDFIB(1,JWDFIB,IWD)+1
JTEMP = JWDFIB
ENDIF
C IF ( CDA(2).NE.KDFTO ) THEN
DD 120 J= 1,2
IF ( CDA(2).EQ.KDFTYP(J) ) THEN
JDFT = J
GOTO 140
ENDIF
120 CONTINUE
C 140 MATDIR(9,JMAT) = JDFT
IF ( KDFTO.NE.KBLNK )
*MATDIR(9,JMAT) = 5
KDFTO = CDA(2)
IF ( JDFT .EQ.4 )
*JDFT = 1
IDFTYP(1,JDFT,JMAT)= JTEMP
ENDIF
IDFTYP(2,JDFT,JMAT)= JTEMP-IDFTYP(1,JDFT,JMAT)+1
DTEMP(JTEMP,JMAT) = RDA(1)
ITEMP(JTEMP,JMAT) = IDA(1)
ENDIF
C IF ( CDA(1).EQ.KSSR )
IF ( JMAT.GT.0 )
*IEPSR(1,MEPSR,JTEMP,JMAT)= 1
ELSE
CALL RDSQF (1,IFNM, IFMT2(1,5) ,1, KSTAT, CDA, NEPSX, RDA
1 , JPOSR)
IF ( NEPSX.GT.0 ) THEN
CALL RDSQF (1,IFNM, IFMT2(1,9) ,NEPSX, KSTAT, CDA, IDA, RDA(1)
1 , JPOSR)
IF ( JMAT.GT.0 )
IEPSR(1,MEPSR,JTEMP,JMAT)= 2
IEPSR(2,MEPSR,JTEMP,JMAT)= JEPSS
DO 180 J=1,NEPSX
EPS(1,JEPSS,JMAT) = RDA(J)
JEPSS = JEPSS+1
180 CONTINUE

```

```

Appendix F (Continued)

      ENDIF
      ENDIF

C      NEPSR = IDA(1)
      IF (< NEPSR.GT.0 ) THEN
C      DO 240 J= 1,NEPSR
      CALL RDSQF (1,IFNM, IFMT2(1,6) ,2, KSTAT, CDA, IDA(1), RDA(1)
      1 , JPOSR)
      EPSR = RDA(1)
      NEPS = IDA(1)
      NEPSS = IDA(1)+IDA(1)
      IF (< CDA(1).EQ.KSSR2 ) *NEPSS = IDA(1)
      IF (< NEPSS.GT.0 ) THEN
      CALL RDSQF (1,IFNM, IFMT2(1,6) ,NEPSS, KSTAT, CDA, IDA, RDA(1)
      1 , JPOSR)
      IF (< JMAT.GT.0 ) THEN
      DEPSR(J,JTEMP,JMAT) = EPSR
      JEPSR(1,J,JTEMP,JMAT) = JEPSS
      JEPSR(2,J,JTEMP,JMAT) = NEPS
      DO 220 K= 1,NEPSS
      EPSS(JEPSS,JMAT) = RDA(K)
      JEPSS = JEPSS+1
      220 CONTINUE
      ENDIF
      240 CONTINUE
      ENDIF

C      CALL RDSQF (3,IFNM, IFMT4(1,1) ,1, KSTAT, CDA(1), IDA, RDA
      1 , JPOSR)
      IF (< CDA(1).EQ.KCOM ) THEN
      NCOMM = NCOMM+1
      CALL RDSQF (1,IFNM, IFMT4(1,1) ,1, KSTAT, CDA(1), IDA, RDA
      1 , JPOSR)
      C      CALL RDSQF (1,IFNM, IFMT4(1,2) ,5, KSTAT, ICOMM(1,NCOMM), IDA
      CALL RDSQF (1,IFNM, IFMT4(1,2) ,1, KSTAT, ICOMM(1,NCOMM), IDA
      1 , RDA, JPOSR)
      IF (< JMAT.GT.0 ) *ITEMP(JTEMP,JMAT) = 1000*NCOMM+ITEMP(JTEMP,JMAT)
      ENDIF
      JTEMP = JTEMP+1
      300 CONTINUE
      IF (< JEPSS.GT.MEPSS ) THEN
      WRITE(6,*510) JEPSS, MEPSS
      6310 FORMAT('0 ***** ERROR ***** '
      1 /' INSUFFICIENT WORKING AREA FOR STRESS-STRAIN DATA'
      2 /' NECESSARY ...',IB
      3 /' GIVEN .....',IB )
      STOP 'QUIT'
      ENDIF
      ENDIF
      RETURN
      END

```

```

Appendix F (Continued)

SUBROUTINE RDSQF (KFN,IFN, IFMT ,NITM, KSTAT, CDA, IDA, RDA
1 , JPOSR)
C      INTEGER   IFMT(2,1)
C      INTEGER   CDA(1)
C      INTEGER   IDA(1)
C      REAL      RDA(1)
C      COMMON /RDBUF1/ MBF, IFNBF1(3), IFNBF2(100), ICHSBF(2,3)
C      CHARACTER  IRCBF1#1
C      COMMON /RDBUF2/ IRCBF2(4,30,3)
C      CHARACTER  IRCBF2#4
C      CHARACTER#16 IRCD1, IRCD2, KRCD
C      INTEGER    JDA(3)
C      CHARACTER#1 KASTR
C      EQUIVALENCE ( JDA(1), JCDA ), ( JDA(2), JIDA ), ( JDA(3), JRDA )

C      DATA KASTR /'*' /
C      DATA MCHS / 30 /
C      DATA MCHBF / 16 /
C      DATA KRCD / ' ' /
C
C      JDA(1)= 0
C      JDA(2)= 0
C      JDA(3)= 0
C*  CHECK INPUT PARAMETERS *
      KSTAT = -1
      IF (< KFN.LE.-1 ) GOTO 800
      IF (< IFN.GT.1.4 ) GOTO 800
      IF (< IFN.LE.0 ) GOTO 800
      IF (< IFN.GT.99 ) GOTO 800
      IBF = IFNBF1(IFN)
      IF (< IBF.LE.0 ) GOTO 800
      *AND.KFN.NE.0 ) GOTO 800
      KSTAT = 0
C*  GET RECORR POSITION *
      IF (< KFN.NE.-1 ) GOTO 10
      JPOSR = IPDSR1(BF)
      GOTO 900
C*  OPEN/REWIND FILE *
      10 IF (< KFN.NE.0 ) GOTO 60
      IF (< IBF.NE.0 ) GOTO 40
      DO 20 I= 1,MBF
      IF (< IFNBF1(I).NE.0 ) GOTO 20
      IBF = I
      IFNBF1(IBF) = IFN
      IFNBF2(IFN) = IBF
      GOTO 40
      20 CONTINUE
      KSTAT = -4
      GOTO 900
C
      40 ICHSBF(1,IBF) = 0
      ICHSBF(2,IBF) = 0
      REWIND IFN
      JPOSR(IBF) = 0
      JPOSR = 0
      GOTO 900
C*  CLOSE FILE *
      60 IF (< KFN.NE.4 ) GOTO 70

```

## Appendix F (Continued)

```

JPOSR      = IPOSR(IBF)
IFNBF1(IBF) = 0
IFNBF2(IFN) = 0
GOTO 900
C* SKIP/BACK RECORDS *
70 IF ( KFN.NE.2 )           GOTO 80
    NRC      = NITM
    IF ( NRC.EQ.0 )           GOTO 900
    JPOSR   = IPOSR+NRC
    IPOSR(IBF) = JPOSR
    IF ( NRC.GT.0 )           THEN
        DO 72 I= 1,NRC
        READ(IFN,5140,END=74)
    72 CONTINUE
    GOTO 900
    74 KSTAT = -2
    ELSE
        NRC      = -NRC
        DO 76 I= 1,NRC
            BACK SPACE 1FN
    76 CONTINUE
        ENDIF
        GOTO 900
C* READ HEADER *
80 IF ( KFN.NE.3 )           GOTO 100
    NCNS     = 0
    JCNS     = 0
    GOTO 110
C* READ FILE *
100 IF ( KFN.NE.1 )           GOTO 800
    110 IF ( NITM.LT.1 )           GOTO 900
        NCNS     = ICHSBF(1,IBF)
        JCNS     = ICHSBF(2,IBF)
        JFMT     = 0
    C
        DO 300 I= 1,NITM
            IF ( JCNS.LT.NCNS )           GOTO 200
    120 CONTINUE
        READ(IFN,5140,END=160)  IRCBF1
    5140 FORMAT( 80A1 )
        IPOSR(IBF) = IPOSR(IBF)+1
        GOTO 180
    160 KSTAT = -2
        GOTO 900
    C
    180 IF ( IRCBF1(1).EQ.KASTR ) GOTO 120
        JCNS     = 0
        NCNS     = 0
        CALL RDCHS (IRCBF1(1),IRCBF2(1,1,IBF),NCNS,NCNS)
        IF ( NCNS.LT.1 )           GOTO 120
    C
    200 JCNS = JCNS+1
        JFMT = JFMT+1
        KSTAT = KSTAT+1
    C
    210 CONTINUE
        KFMT = IFMT(1,JFMT)
        IF ( KFMT.GT.0 )           GOTO 230
        IF ( KFMT.EQ.0 )           GOTO 320
        JFMT = JFMT+KFM
    C
        GOTO 210
    220 KFMT      = KFMT/100
        NWDS      = IFMT(1,JFMT)-KFMT*100
        JDAC(KFMT) = JDAC(KFMT)+1
        IFMT(2,JFMT)= JDAC(KFMT)
    C
        J2      = 0
        DO 230 J= 1,4
            J1      = J2+1
            J2      = J2+4
            IRCD1(J1:J2) = IRCBF2(J,JCNS,IBF)
    230 CONTINUE
C* CHARACTERS *
    240 IF ( KFMT.GT.1 )           GOTO 260
        DO 245 J= 1,NWDS
            READ(IRCBF2(J,JCNS,IBF),'(A4)')  CDA(JCDA)
            JCDA = JCDA+1
    245 CONTINUE
        JCDA      = JCDA-1
        IF ( NWDS.EQ.20 )           NCNS = JCNS*4
        *JCNS = JCNS*4
        IF ( KFN.EQ.3 )           NCNS = 0
        GOTO 300
    C
    260 J1      = MCHBF
        DO 265 J= 1,MCHBF
            IF ( IRCD1(J1:J1).NE.' ' ) GOTO 270
            J1      = J1-1
    265 CONTINUE
        IDA(JIDA) = 0
        GOTO 300
    270 J2      = MCHBF-J1+1
        IRCD2 = KRC
        IRCD2(J2:MCHBF) = IRCD1(1:J1)
C* INTEGER *
    280 IF ( KFMT.NE.2 )           GOTO 280
        READ(IRCD2,'(I16)')  IDA(JIDA)
        GOTO 300
C* REAL *
    280 IF ( KFMT.EQ.3 )
        *READ(IRCD2,'(E16.0)')  RDA(JRDA)
    300 CONTINUE
C
    320 ICHSBF(1,IBF) = NCNS
        ICHSBF(2,IBF) = JCNS
        JPOSR      = IPOSR(IBF)
        GOTO 900
C* ERROR *
    6820 WRITE(6,6820) KFN, IFN
    6820 FORMAT( 36H0 **** ERROR **** SUB. RDSCF
    1      / 22H      INPUT PARAMETERS
    2      / 17H      KFN ...16
    3      / 17H      IFN ...18 )
    900 CONTINUE
    RETURN
    END

```

```

          Appendix F (Continued)

SUBROUTINE RDCHS (JCHR, ICHS, NCHS, MCHS)
C
CHARACTER ICHR(1)*1
CHARACTER ICHS(4,1)*4
CHARACTER CBLNK#4
CHARACTER*1 ICHBF(16)
LOGICAL ISTRG, IBLNK
DIMENSION KCHR(4)
CHARACTER*1 KCHR, KCOMA, KBLNK
EQUIVALENCE ( KCHR(5), KCOMA ), ( KCHR(4), KBLNK )

C
DATA CBLNK / ' ' /
DATA KCHR / 'H', 'H', 'H', 'H' /
DATA MCHR / 80 /
DATA MCHBF / 16 /

C
NCHS = 0
JCHR = 0
JCHR1 = 1

C 100 CONTINUE
JSTR1 = 0
JSTR2 = 0
IQUOT = 0
ISTRG = .FALSE.
IBLNK = .FALSE.
DO 300 I= JCHR1,MCHR
IF ( IQUOT.NE.0 ) GOTO 200
IF ( ICHR(I).NE.KCOMA ) GOTO 110
IF ( ISTRG .AND. JSTR2.EQ.0 )
*JSTR2 = I-1
JCHR = I
ISTRG = .TRUE.
GOTO 400
110 IF ( ICHR(I).NE.KBLNK ) GOTO 130
IF ( .NOT.ISTRG .OR. IBLNK ) GOTO 300
IBLNK = .TRUE.
JSTR2 = I-1
JCHR = I
GOTO 300
130 IF ( ISTRG ) GOTO 170
ISTRG = .TRUE.
DO 150 J= 1,2
IF ( ICHR(I).NE.KCHR(J) ) GOTO 150
IQUOT = J
JQUOT = I
JSTR1 = I+1
GOTO 300
150 CONTINUE
JSTR1 = 1
170 IF ( .NOT.IBLNK ) GOTO 300
JCHR = I-1
GOTO 400
200 DO 220 J= 1,2
IF ( ICHR(I).NE.KCHR(J) ) GOTO 220
IF ( IQUOT.NE.J ) GOTO 300
ICHRS(I) = KBLNK
ICHRS(JQUOT) = KBLNK
IQUOT = 0
JQUOT = 0
IQUOT = 0

          Appendix F (Continued)

JSTR2 = I-1
GOTO 300
220 CONTINUE
300 IF ( .NOT.ISTRG ) GOTO 900
IF ( NCHS.GE.MCHS ) GOTO 900
IF ( JSTR1.NE.0 ) THEN
MCHBF = JSTR2-JSTR1
NCHSX = (NCCHBF+MCHBF)/MCHBF
IF ( NCHS+NCHSX.GT.NCHS )
*MCHSX = NCHS-NCHS
J2 = JSTR1-1
IF ( NCCHBF.GE.16 )
*NCHSX = 5
DO 450 I= 1,NCHSX
NCHS = NCHS+1
J1 = J2+1
J2 = J2+MCHBF
IF ( J2.GT.JSTR2 )
*J2 = JSTR2
IF ( J1.LE.J2 ) THEN
K = 1
DO 430 J= J1,J2
ICHBF(K)= ICHR(J)
K = K+1
410 CONTINUE
IF ( K.LE.MCHBF ) THEN
DO 420 J= K,MCHBF
ICHBF(J)= KBLNK
420 CONTINUE
430 CONTINUE
ELSE
DO 430 J= 1,MCHBF
ICHBF(J)= KBLNK
430 CONTINUE
ENDIF
ELSE
DO 430 J= 1,MCHBF
ICHBF(J)= KBLNK
430 CONTINUE
ENDIF
K1 = 1
K2 = 4
K3 = 0
DO 440 J= 1,MCHBF/4
K3 = K3+1
WRITE(ICHRS(K3,NCHS),'(4A1)') (ICHBF(K),K=K1,K2)
K1 = K2+1
K2 = K2+4
440 CONTINUE
450 CONTINUE
ELSE
NCHS = NCHS+1
DO 470 I= 1,4
ICHRS(I,NCHS) = CBLNK
470 CONTINUE
ENDIF
IF ( JCHR.GE.MCHR ) GOTO 900
JCHR1 = JCHR+1
GOTO 100
900 RETURN
END

```

## Appendix F (Continued)

```

FUNCTION ISBST (CHAR)
C
CHARACTER CHAR*4
CHARACTER CHARX*4
C
CHARX = CHAR
READ(CHARX,'(A4)') ISBST
RETURN
END

SUBROUTINE MLBEX (MLB)
C
INTEGER MLB(1)
COMMON /MLBRF1/ KRFM1, KRFM2, KEXC, MRFM, IRFM(10), KARG(4)
1      NRFC(8), IRFC(10,8), RRFC(2,10,8), KSYSU
COMMON /MLBAL1/ LMLB, IMA1, IMA2, IMA3, IMA4, IMA5, IMA6, IMA7, IMA8
1      IMA9, IMA10, IMA11, IMA12, IMA13, IMA14, IMA15, IMA16
2      IMA17, IMA18
COMMON /MLBFND/ IFNC, IFNM, IFNP, IFNR
COMMON /RDBUF3/ CDA(10), IDA(10), RDA(50)
CHARACTER*4 CDA
C
CALL RDGF (0,IFNM, IFMT >0, KSTAT, CDA, IDA, RDA, JPOSR)
100   CONTINUE
C
CALL EXCOM (MLB(IMA5), KLST, KPLT, KFIT)
C
IF ( KEXC.LE.0 )      GOTO 200
IF ( KEXC.EQ.1 )      THEN
CALL EXQRY (MLB(IMA5),MLB(IMA1),MLB(IMA2),MLB(IMA3),MLB(IMA4)
1           ,MLB(IMA17))
1           ELSE
C
CALL EXDAT (MLB(IMA5), MLB )
C
CALL EXUNI
C
CALL EXOUT (KLST,KPLT,KFIT,MLB(IMA17))
ENDIF
C
GOTO 100
C
200 CALL PLDT (0.,0.,999)
C
RETURN
END

```

## Appendix F (Continued)

```

SUBROUTINE EXCOM (NAMMAT, KLST, KPLT, KFIT)
C
INTEGER NAMMAT(12,1)
COMMON /MLBNOM/ NMLB, NMAT, MCS, NSS, NPB, NWD, NPROPS5, NDFT
1      NWDF, NTMP, NEPSR, NEPS, NREFF, NCDMH
COMMON /MLBFR1/ KRFM1, KRFM2, KEXC, MRFM, IRFM(10), KARG(4)
1      NRFC(8), IRFC(10,8), RRFC(2,10,8), KSYSU
COMMON /MLBLP1/ IXAMES(2), KMESEL, KCUNAM, JCUNAM(20), ICVNAM(5,20)
CHARACTER*4 ICMNAME
COMMON /MLBFT1/ XIT, IERFIT, COEF(16), COEF(6), COEOF(6,16)
1      MXY, MXYD(5), XYD(2,50,5), MXY, MXYD
COMMON /COMPL1/ ATITLE(10), XNAME(10), YNAME(10)
1      XDATA(50,20), YDATA(50,20)
1      XDATA(50,20), YDATA(50,20)
INTEGER ATITLE, XNAME, YNAME
COMMON /COMPL2/ PXMIN, PXMAX, PYMIN, PYMAX, XL1, YL1, NPLOT
1      NDATA, NDATA(20), NGRAPH
COMMON /RDBUF3/ CDA(10), IDA(10), RDA(50)
CHARACTER*72 CTITLE, CBLNK
DATA CBLNK    /
1      DATA KEXC1, KEXC2 / 2#0 /
DATA KECHO    / 1 /
C
KLST = 0
KPLT = 0
KFIT = 0
IF ( KEXC.GT.1 )      GOTO 100
IF ( KEXC.LE.1 )      GOTO 150
70   CONTINUE
WRITE(6,6080)
6080 FORMAT(' ENTRY? (0:1:2:3):'
1      / ' 0; EXIT '
2      / ' 1; QUERY '
3      / ' 2; GRAPHICS '
4      / ' 3; INPUT ECHO')
READ(5,*) KEXC
IF ( KECHO.NE.0 ) WRITE(6,6125) KEXC
IF ( KEXC.LE.0 )      GOTO 900
IF ( KEXC.EQ.1 )      GOTO 150
IF ( KEXC.EQ.2 )      GOTO 250
IF ( KEXC.EQ.3 )      THEN
WRITE(6,6090)
6090 FORMAT(' INPUT ECHO? (0:1)'
1      / ' 0; DFF '
2      / ' 1; ON '
READ(5,*) KEXC1
IF ( KECHO.NE.0 ) WRITE(6,6125) KEXC1
KECHO = KEXC1
ENDIF
GOTO 70
C
100   CONTINUE
WRITE(6,6120)
6120 FORMAT(' EXIT/RESET? (0:1:2:3:4:5:6) '
1      / ' 0; EXIT '
2      / ' 1; QUERY '
3      / ' 2; TITLE,...'
4      / ' 3; MATERIALS,...'
5      / ' 4; PARAMETERS,...'

```

## Appendix F (Continued)

```

6      /'   5; SYSTEM OF UNITS'
7      /'   6; OUTPUT
READ(S,*)
      KEXC
      IF ( KECHO.NE.0 ) WRITE(6,6125) KEXC
6125 FORMAT(' >>,I3')
      IF ( KEXC.LE.0 )          GOTO 900
      IF ( KEXC.GT.1 )          GOTO 100
      IF ( KEXC.GT.-1 )         GOTO 240
150 CALL EXCDM0 ( KEXC1,KECHO )
      IF ( KEXC1.LE.0 )          GOTO 70
      GOTO 900
C
200 KEXC = KEXC+KEXC1*KEXC2
      KEXC1 = 0
      KEXC2 = 0
      IF ( KEXC.LT.0 )          GOTO 900
C
220 KEXC = KEXC+1
240 IF ( KEXC.NE.2 )          GOTO 280
250 CTITLE= CBLNK
      WRITE(6,6260)
6260 FORMAT(15H TITLE? ('...'))
      READ(S,*;END=900) CTITLE
      IF ( KECHO.NE.0 ) WRITE(6,6265) CTITLE
6265 FORMAT(' >> ('AS0 )
      READ(CTITLE,'(18A4)') (ATITLE(I),I=1,18)
      GOTO 220
C
280 IF ( KEXC.NE.3 )          GOTO 400
300 WRITE(6,6320)
6320 FORMAT( ' MATERIALS? (PROP,NMAT,MATNO,...)')
      1      /' PROPERTY
      2      /'   0; RETURN
      3      /'   12; COEFFICIENT OF THERMAL EXPANSION
      4      /'   23; MODULUS OF LONGITUDINAL ELASTICITY
      5      /'   34; MODULUS OF TRANSVERSE ELASTICITY
      6      /'   42; POISSON'S RATIO
      7      /'   51; STRESS-STRAIN
      8      /'   62; STRESS-STRAIN RATE
      9      /'   NMAT; NUMBER OF MATERIALS
      A      /'   MATNO; MATERIAL NUMBER
      READ(S,*)
      KEXC1, NMATS, (IDA(I),I=1,NMATS)
      IF ( KECHO.NE.0 ) WRITE(6,6325) KEXC1, NMATS, (IDA(I),I=1,NMATS)
5325 FORMAT(' >>,213,10I5 : ( 10X,10I5 )')
      IF ( KEXC1.NE.-9 )          GOTO 330
      KECHO
      IDA(1)
      GOTO 300
330 IF ( KEXC1.LE.0 )          GOTO 200
      IF ( KEXC1.GT.6 )          GOTO 300
      IF ( NMATS.GT.NMAT )       GOTO 300
      KARG(1) = 0
      KARG(2) = KEXC1
      KARG(3) = KEXC1
      IF ( KEXC1.EQ.5 )         THEN
      KARG(1) = 9
      KARG(2) = 10
      ELSE
      IF ( KEXC1.EQ.6 )         THEN
      KARG(1) = 8
      KARG(2) = 10

```

## Appendix F (Continued)

```

      ENDIF
      ENDIF
      NRFM = 0
      DO 360 I = 1,NMATS
      DO 340 J = 1-NMAT
      IF ( IDA(I).NE.WMMAT(P,J) ) GOTO 340
      IF ( NRFM.GE.NRFM )          GOTO 380
      NRFM = NRFM+1
      IRFM(NRFM) = IDA(I)
      GOTO 360
340 CONTINUE
360 CONTINUE
380 KEXC = KEXC+1
      IF ( KARG(3).NE.5 .AND. KARG(3).NE.6 ) GO TO 220
      GOTO 420
400 IF ( KEXC.NE.4 )          GOTO 450
      IF ( KARG(3).NE.5 .AND. KARG(3).NE.6 ) GO TO 100
C* PROPERTY *
420 CALL EXCDM0 ( KEXC1, KEXC2,KECHO )
      IF ( KEXC1.LE.0 .OR. KEXC2.LE.0 ) GO TO 200
450 IF ( KEXC.NE.5 )          GOTO 500
460 WRITE(6,6470)
6470 FORMAT( ' SYSTEM OF UNITS? (1:2)'
      1      /'   1; SI
      2      /'   2; MKS
      READ(S,*)
      KEXC1
      IF ( KECHO.NE.0 ) WRITE(6,6125) KEXC1
      IF ( KEXC1.LT.0 )          GOTO 200
      IF ( KEXC1.LE.1 .AND. KEXC1.NE.2 ) GO TO 460
      KSYSU = KEXC1
      KEXC = KEXC1
500 IF ( KEXC.LT.6 )          GOTO 100
520 WRITE(6,6540)
6540 FORMAT( ' OUTPUT? (0:001:010:100) '
      1      /'   0; RETURN
      2      /'   001; LISTING
      3      /'   010; PLOTTING
      4      /'   100; FITTING
      READ(S,*)
      KEXC1
      IF ( KECHO.NE.0 ) WRITE(6,6125) KEXC1
      IF ( KEXC1.EQ.0 .OR. KEXC1.LT.-5 ) GO TO 100
      IF ( KEXC1.NE. 1 .AND. KEXC1.NE.-1 .AND. KEXC1.NE.11
      1.AND.KEXC1.NE.100 .AND. KEXC1.NE.101 .AND. KEXC1.NE.110
      2.AND.KEXC1.NE.111 )         GOTO 520
      KLST = 0
      IF ( KEXC1-KEXC1/10*10.NE.0 ) KLST = 1
      KEXC1 = KEXC1-KLST
      KPLT = KEXC1-KEXC1/100*100
      KFITT =(KEXC1-KPLT)/100
      KPLT = KPLT/10
      KEXC1 = KLST*KPLT
      KEXC = KEXC-KEXC1
      IF ( KPLT.NE.0 ) CALL EXCDM2 ( KEXC1, KECHO )
      IF ( KFITT.NE.0 )           THEN
      CALL EXCDM3 ( KEXC1,KECHO )
      KFITT = KFITT
      ENDIF
900 CONTINUE
      RETURN
      END

```

## Appendix F (Continued)

```

SUBROUTINE EXCOMQ ( KEXC1,KECHD)
COMMON /MLBQR1/ KQR(10), JQRD(10), JCQRD, JCQRD
CHARACTER*4      CQRD
CHARACTER*17 MNAM1, BLNK1
CHARACTER*17 MNAM2(17), BLNK2
DATA   BLNK1 / '          ' /
DATA   BLNK2 / '          ' /
120    CONTINUE
      WRITE(6,6140)
6140 FORMAT(1X, QUERY? (0:1:2:3:4:5:6:7:8:9) )
1      / ' 0: RETURN '
2      / ' 1: MATERIAL NAME LIST '
3      / ' 2: CARBON STEEL NAME LIST '
4      / ' 3: STAINLESS STEEL NAME LIST '
5      / ' 4: LEAD NAME LIST '
6      / ' 5: WOOD NAME LIST '
7      / ' 6: REFERENCE LIST '
8      / ' 7: MATERIAL DATA '
9      / ' 8: MATERIAL NO. BY NAME '
*      / ' 9: MATERIAL NO. BY REFERENCE '
*      READ(5,*), KEXC1
*      IF ( KECHD.NE.0 ) WRITE(6,6145) KEXC1
6145 FORMAT( ' >> ',13 )
      IF ( KEXC1.LE.0 )      GOTO 900
      IF ( KEXC1.GT.9 )      GOTO 120
      KQR(1) = KEXC1
      IF ( KEXC1.EQ.7 )      THEN
      WRITE(6,6220)
6220 FORMAT(1X, MATERIAL DATA? (MAT-NO.) )
      READ(5,*), KEXC2
      IF ( KECHD.NE.0 ) WRITE(6,6225) KEXC2
6225 FORMAT( ' >> ',15 )
      KQR(2) = JCQRD
      JCQRD(J1QRD)= KEXC2
      JCQRD = JCQRD+1
      IF ( JCQRD.GT.10 ) JCQRD = 1
      ELSE
      IF ( KEXC1.GE.8 )      THEN
      IF ( KEXC1.EQ.8 ) WRITE(6,6240)
6240 FORMAT(2H MATERIAL NO.? ('MAT-NAME') )
      IF ( KEXC1.EQ.9 ) WRITE(6,6242)
6242 FORMAT(2H MATERIAL NO.? ('REFERENCE') )
      MNAM1 = BLNK1
      READ(5,*), MNAM1
      IF ( KECHD.NE.0 ) WRITE(6,6245) MNAM1
6245 FORMAT( ' >> ',17 )
      READ(MNAM1,'(17A17)',(MNAM2(I),I=1,17)
      260 WRITE(MNAM1,'(6A1)',(MNAM2(I),I=1,16)
      READ (MNAM1,'(4A4)',(CQRD(I,JCQRD),I=1,4)
      KQR(2) = JCQRD
      JCQRD = JCQRD+1
      IF ( JCQRD.GT.10 ) JCQRD = 1
      ENDIF
      ENDIF
900 RETURN
END

```

## Appendix F (Continued)

```

SUBROUTINE EXCOM1 ( KEXC1, KEXC2,KECHD)
C
COMMON /MLBRF1/ KRFM1, KRFM2, KEXC, MRFM, NRFM, IRFM(10), KARG(4)
1      NRFC(10), IRFC(10,B), RRFCC(2*10,B), KSYSU
COMMON /RDBUF3/ CDA(10), IDA(10), RDA(50)
CHARACTER*4      CDA
CHARACTER*4 KFIBR(B)
C
      DATA      KFIBR / '0', '30', '45', '60', /
1      / '90', 'NDRM', ' ', ' ', ' ' /
C
      DO 100 I= 1,B
      NRFC(I)= 0
100 CONTINUE
C
120 KEXC2 = 0
      WRITE(6,6140)
6140 FORMAT(1X, PARAMETERS? (0:1:2:3:4:5) )
1      / ' 0: RETURN '
2      / ' 1: DEFORMATION TYPE '
3      / ' 2: FIBRE DIRECTION OF WOOD '
4      / ' 3: TEMPERATURE '
5      / ' 4: STRAIN RATE '
6      / ' 5: STRAIN '
*      READ(5,*), KEXC1
*      IF ( KECHD.NE.0 ) WRITE(6,6145) KEXC1
6145 FORMAT( ' >> ',13 )
      IF ( KEXC1.LE.0 )      GOTO 900
      IF ( KEXC1.GT.5 )      GOTO 120
      IF ( KEXC1.NE.1 )      GOTO 300
C
200 WRITE(6,6220)
6220 FORMAT(1X, DEFORMATION TYPE? (0:1:2:3) )
1      / ' 0: RETURN '
2      / ' 1: COMPRESSION '
3      / ' 2: TENSION '
4      / ' 3: COMPRESSION & TENSION '
*      READ(5,*), KEXC2
*      IF ( KECHD.NE.0 ) WRITE(6,6145) KEXC2
      IF ( KEXC2.LT.0 )      GOTO 900
      IF ( KEXC2.EQ.0 )      GOTO 120
      IF ( KEXC2.GT.3 )      GOTO 200
      NRFC(KEXC1) = (KEXC2+1)/2
      IRFC(1,KEXC1) = KEXC2
      IF ( KEXC2.LE.2 )      GOTO 120
      IRFC(1,KEXC1) = 1
      IRFC(2,KEXC1) = 2
      GOTO 120
C
300 IF ( KEXC1.NE.2 )      GOTO 400
320 WRITE(6,6340)
6340 FORMAT(1X, FIBRE DIRECTION OF WOOD? (0:1:2:3:4:5:6) )
1      / ' 0: RETURN '
2      / ' 1: 0 DEG '
3      / ' 2: 30 DEG '
4      / ' 3: 45 DEG '
5      / ' 4: 60 DEG '
6      / ' 5: 90 DEG '
7      / ' 6: NORMAL '
*      READ(5,*), KEXC2

```

```

        Appendix F (Continued)

1 IF ( KECHO.NE.0 ) WRITE(6,6145) KEXC2
1 IF ( KEXC2.LT.0 ) GOTO 900
1 IF ( KEXC2.EQ.0 ) GOTO 120
1 IF ( KEXC2.GT.6 ) GOTO 320
1 NRFC(KEXC1) = NRFC(KEXC1)+1
1 J = NRFC(KEXC1)
1 IRFC(J,KEXC1) = ISBT(KFIBR(KEXC2))
1 GOTO 120
C
400 IF ( KEXC1.NE.3 ) GOTO 500
420 WRITE(6,6440)
440 FORMAT(' TEMPERATURE? (MIN,MAX) ')
440 READ(5,*), RMIN, RMAX
440 IF ( KECHO.NE.0 ) WRITE(6,6445) RMIN, RMAX
445 FORMAT(' >>2F10.3 ')
445 IF ( RMIN.GT.-9999. ) GOTO 460
460 KEXC2 = -9
460 GOTO 900
460 IF ( RMIN.GT.RMAX ) GOTO 420
460 NRFC(KEXC1) = NRFC(KEXC1)+1
460 J = NRFC(KEXC1)
460 RRFc(1,J,KEXC1)= RMIN
460 RRFc(2,J,KEXC1)= RMAX
460 GOTO 120
500 IF ( KEXC1.NE.4 ) GOTO 600
500 IF ( KARG(1).EQ.8 ) GOTO 120
520 WRITE(6,6540)
540 FORMAT(' STRAIN RATE? (MIN,MAX) ')
540 READ(5,*), RMIN, RMAX
540 IF ( KECHO.NE.0 ) WRITE(6,6445) RMIN, RMAX
540 IF ( RMIN.GT.-9999. ) GOTO 560
540 KEXC2 = -9
540 GOTO 900
560 IF ( RMIN.GT.RMAX ) GOTO 520
560 NRFC(KEXC1) = NRFC(KEXC1)+1
560 J = NRFC(KEXC1)
560 RRFc(1,J,KEXC1)= RMIN
560 RRFc(2,J,KEXC1)= RMAX
560 GOTO 120
600 IF ( KEXC1.NE.5 ) GOTO 120
600 IF ( KARG(1).EQ.9 ) GOTO 120
620 WRITE(6,6640)
640 FORMAT(' STRAIN? (NSTRM,STRN,...) '
1      /' NSTRM: NUMBER OF STRAINS '
2      /' STRN : STRAIN '
1      READ(5,*), KEXC2, (RDA(I),I=1,KEXC2)
1      IF ( KECHO.NE.0 ) WRITE(6,6645) KEXC2, (RDA(I),I=1,KEXC2)
645 FORMAT(' >>13.5F10.4 : ( 7X,5F10.4 ) ')
645 IF ( KEXC2.LT.0 ) GOTO 900
645 IF ( KEXC2.EQ.0 ) GOTO 120
645 J = NRFC(KEXC1)
645 NRFC(KEXC1) = NRFC(KEXC1)+KEXC2
660 DO 660 I=1,KEXC2
660 J = J+1
660 RRFc(1,J,KEXC1) = RDA(I)
660 RRFc(2,J,KEXC1) = RDA(I)
660 CONTINUE
660 GOTO 120
900 RETURN
END

```

```

        Appendix F (Continued)

SUBROUTINE EXCOM2 ( KEXC1,KECHO )
C
COMMON /COMPL2/ PXMIN, Pymax, PYMIN, PYMAX, XL1, YL1, NPLDT
1 COMMON /NDATA/ NDATA, NDATAX(20), NGRAPH
1 COMMON /MLBPL1/ IAXES(2), KMESH, KCVNAM, JCVNAM(20), ICVNAM(5,20)
CHARACTER*4 KCVNAM
COMMON /MLBRF1/ KRFM1, KRFM2, KEXC, MRFM, NRFP, IRFM(10), KARG(4)
1 , NRFC(8), IRFC(10,8), RRFC(2,10,8), KSYSU
1 CHARACTER*22 CVNAM1, BLNK1
CHARACTER*21 CVNAM2(22), BLNK2
C
C
DATA BLNK1 / ' ' /
DATA BLNK2 / ' ' /
C
C
120 WRITE(6,6140)
6140 FORMAT(' PLOT OPTIONS? (0:1:2:3:4:5) '
1      /' 0: RETURN '
2      /' 1: DATA RANGES '
3      /' 2: TYPE OF AXES '
4      /' 3: STRING '
5      /' 4: MESH '
6      /' 5: COMMENT OF CURVES ')
6140 READ(5,*), KEXC1
IF ( KECHO.NE.0 ) WRITE(6,6145) KEXC1
6145 FORMAT(' >>13 ')
IF ( KEXC1.LE.0 ) GOTO 900
IF ( KEXC1.GT.5 ) GOTO 120
C
C
IF ( KEXC1.NE.1 ) GOTO 250
200 WRITE(6,6220)
6220 FORMAT(' DATA RANGES? (XMIN,XMAX,YMIN,YMAX) '
1      /' XMIN: MINIMUM VALUE ON X-AXIS '
2      /' XMAX: MAXIMUM VALUE ON X-AXIS '
3      /' YMIN: MINIMUM VALUE ON Y-AXIS '
4      /' YMAX: MAXIMUM VALUE ON Y-AXIS ')
6220 READ(5,*), PXMIN, Pymax, PYMIN, PYMAX
IF ( KECHO.NE.0 ) WRITE(6,6225) PXMIN, Pymax, PYMIN, PYMAX
6225 FORMAT(' >>13.10. ')
IF ( PXMIN.GT.Pymax .OR. PYMIN.GT.PYMAX ) GO TO 200
GOTO 120
C
C
250 IF ( KEXC1.NE.2 ) GOTO 300
260 WRITE(6,6280)
6280 FORMAT(' TYPE OF AXES? (1:2:3:4) '
1      /' 1: BOTH X AND Y ARE LINEAR SCALE '
2      /' 2: X IS LOG SCALE, Y IS LINEAR SCALE '
3      /' 3: X IS LINEAR SCALE, Y IS LOG SCALE '
4      /' 4: BOTH X AND Y ARE LOG SCALE ')
6280 READ(5,*), KEXC2
IF ( KECHO.NE.0 ) WRITE(6,6145) KEXC2
IF ( KEXC2.LT.1 .OR. KEXC2.GT.4 ) GO TO 260
KEXC2 = KEXC2-1
IAXES(2)= KEXC2/2
IAXES(1)= KEXC2-2*IAXES(2)

```

## Appendix F (Continued)

```

      GOTO 120
C
C
  300 IF ( KEXC1.NE.3 )      GOTO 350
  320 WRITE(6,6340)
6340 FORMAT( ' STRING2 (0:1) '
  1   / ' 02 NO '
  2   / ' 12 YES ' )
  READ(5,*), KEXC2
  IF ( KECHO.NE.0 ) WRITE(6,6145) KEXC2
  IF ( KEXC2.LT.0 .OR. KEXC2.GT.1 ) GO TO 320
  KARG(4) = KEXC2
  GOTO 120
C
C
  350 IF ( KEXC1.NE.4 )      GOTO 400
  360 WRITE(6,6380)
6380 FORMAT( ' MESH? (0:1:2) '
  1   / ' 02 NONE '
  2   / ' 12 DASH LINE'
  3   / ' 22 LINE ' )
  READ(5,*), KEXC2
  IF ( KECHO.NE.0 ) WRITE(6,6145) KEXC2
  IF ( KEXC2.LT.0 .OR. KEXC2.GT.2 ) GO TO 360
  KMESH = KEXC2
  GOTO 120
C
C
  400 IF ( KEXC1.NE.5 )      GOTO 120
  IF ( KCVNAM.NE.0 )      THEN
  KCVNAM = 0
  DO 410 I=1,20
  JCVNAM(I) = 0
  410 CONTINUE
  ENDIF
  420 WRITE(6,6440)
6440 FORMAT( ' COMMENT OF CURVES? (CURVE-ND,..COMMENT..)'
  1   / ' 02 RETURN '
  2   / ' > 02 DEFINITION '
  3   / ' <12 DEFINITION ' )
  CVNAM1= BLNK1
  READ(5,*), KEXC2, CVNAM1
  IF ( KECHO.NE.0 ) WRITE(6,6450) KEXC2, CVNAM1
6450 FORMAT( ' >>'13.2H, /A22 )
  IF ( KEXC2.EQ.0 )      GOTO 120
  IF ( KEXC2.LT.0 .OR. KEXC2.GT.20 ) GO TO 420
  JCVN = KEXC2
  JCVNAM(JCVN)= JCVN
  READ(CVNAM1,'(22A1)') (CVNAM2(I),I=1,22)
  470 WRITE(CVNAM1,'(20A1)') (CVNAM2(I),I=1,20)
  READ(CVNAM1,'(5A4)') (CVNAM(I,JCVN),I=1,5)
  KCVNAM= KCVNAM+1
  GOTO 420
  900 CONTINUE
  RETURN
END

```

## Appendix F (Continued)

```

SUBROUTINE EXCOM3 ( KEXC1,KECHO )
C
COMMON /MLBFT1/ KFIT, IEQFIT, NCDEF(16), COEF(6), COEOF(6,16)
1      , NXY, NXFD(5), XYD(2,50,5), MXY, MXFD
COMMON /MLBFT2/ NEACFC(16), IEQCF(6,16)
CHARACTER4 IEQCF
COMMON /MLBRF1/ KRFM1, KRFM2, KEXC, MRFM, NRFM, IRFM(10), KARG(4)
1      , NRFC(8), IRFC(10,8), RRFC(2,10,8), KSYSU
C
  120 WRITE(6,6140)
6140 FORMAT( ' FITTING? (0:1:2:3) '
  1   / ' 02 RETURN '
  2   / ' 12 INPUT X-Y DATA '
  3   / ' 22 LINEAR REGRESSION '
  4   / ' 32 BUILD IN EQUATIONS ' )
C
C
  READ(5,*), KEXC1
  IF ( KECHO.NE.0 ) WRITE(6,6145) KEXC1
6145 FORMAT( ' >>'13 )
  IF ( KEXC1.LE.0 )      GOTO 900
  IF ( KEXC1.GT.3 )      GOTO 120
C
C
  IF ( KARG(4).EQ.0 ) KARG(4) = -1
  KFIT = KEXC1
  IF ( KEXC1.NE.1 )      GOTO 250
  NXY = 0
  200 NXY = NXY+1
  WRITE(6,6220)
6220 FORMAT( ' X-Y DATA? (N,X1,Y1,...,XN,YN) '
  1   / ' N; NUMBER OF X-Y DATA (<51) '
  2   / ' X; X DATA '
  3   / ' Y; Y DATA ' )
C
C
  READ(5,*), KEXC2, ((XYD(I,J,NXY),(I=1,2),J=1,KEXC2))
  IF ( KECHO.NE.0 )
  *WRITE(6,6225)KEXC2, ((XYD(I,J,NXY),(I=1,2),J=1,KEXC2)
6225 FORMAT( ' >>'14.1P6E11.3: / ( BX,6E11.3 ) )
  IF ( KEXC2.GT.0 )      GOTO 240
  NXY = NXY-1
  GOTO 900
C
C
  240 IF ( KEXC2.GT.MXYD ) KEXC2 = MXYD
  MXYD(NXY)= KEXC2
  GOTO 200
C
C
  250 IF ( KEXC1.NE.2 )      GOTO 300
  WRITE(6,6260)
6260 FORMAT( ' LINEAR REGRESSION? (A,B) '
  1   / ' Y = A*X + B ' )
C

```

## Appendix F (Continued)

```

C
C
      READ(5,*), A, B
      IF ( KECFO.NE.0 ) WRITE(6,6270) A, B
6270 FORMAT(' >> ',2F10.2)
      COEF(1)= A
      COEF(2)= B
      GOTO 900
C
C
      300 IF ( KEXC1.LE.3 )      GOTO 120
      IEQFIT= 0
      310 WRITE(6,6320)
6320 FORMAT(' EQUATION NUMBER? (0:1,...,15) '
           1   '/ * RETURN '
           2   '/ * 1; EQUATION NUMBER 1 '
           3   '/ * ... '
           4   '/ * 15; EQUATION NUMBER 15 ')
C
C
      READ(5,*), KEXC2
      IF ( KECFO.NE.0 ) WRITE(6,6145) KEXC2
      IF ( KEXC2.LE.0 )      GOTO 900
      IF ( KEXC2.GT.15 )      GOTO 300
C
C
      IEQFIT = KEXC2
      NEQC = NEQCF(IEQFIT)
      NCOE = NCOEF(IEQFIT)
      WRITE(6,6340) IEQFIT, (IEQCF(I),IEQFIT), I=1,NEQC
6340 FORMAT(' COEFFICIENT OF THE EQUATION',13,' ? ( ',6A4')
C
C
      IF ( IEQFIT.EQ.10 )      THEN
      READ(5,*), NCOE, COEF(2), (COEF(I+2),I=1,NCOE)
      COEF(1)= NCOE
      IF ( KECFO.NE.0 )
      *WRITE(6,6345) NCOE, COEF(2), (COEF(I+2),I=1,NCOE)
6345 FORMAT(' >>',1Z,8F9.3)
      NCOEF(10) = NCOE+2
C
C
      ELSE
      READ(5,*), (COEF(I),I=1,NCOE)
      IF ( KECFO.NE.0 )
      *WRITE(6,6347) (COEF(I),I=1,NCOE)
6347 FORMAT(' >>',1Z,8F9.3)
      ENDIF
C
C
      900 RETURN
      END

```

## Appendix F (Continued)

```

SUBROUTINE EXQRY (NAMMAT,NAMCS,NAMSS,NAMPB,NAMWD,IREFF)
C
      DIMENSION NAMMAT(12,1)
      DIMENSION NAMCS(5,1), NAMSS(5,1), NAMPB(5,1), NAMWD(5,1)
      DIMENSION IREFF(2,1)
      INTEGER ICORD(2)
      COMMON /LBFNO/ IFNC, IFNM, IFNP, IFNR
      COMMON /LBQR1/ KRR(10), IQRD(10), JQRD, JCQRD
      CHARACTER*4 CDRD
      COMMON /LBNUM/ NMLB, NMAT, NSS, NPP, NWD, NPROP(5), NDFT
      COMMON /RDBUF3/ CDA(10), IDA(10), RDA(50)
      CHARACTER CDA*4
      CHARACTER CDAX(20)*4
      EQUIVALENCE ( CDR(1), CDAX(1) )
C
      KQR1 = KRR(1)
      IF ( KQR1.LT.1 )
      *OR. KQR1.GT.9 )      GOTO 900
      GOTO ( 110,120,130,140,150,160,170,180,190 ), KQR1
C*
      MATERIAL NAME
      110 WRITE(6,6112) ((NAMMAT(J,1),J=5,9),I=1,NMAT)
      6112 FORMAT( 27H0* MATERIAL NAME * NO. * /
           1          ( 3X,4A4,14 ) )
      GOTO 900
C*
      CARBON STEEL NAME
      120 IF ( NSS.GT.0 )      THEN
      WRITE(6,6122) ((NAMCS(J,1),J=1,4),I=1,NCS)
      6122 FORMAT( 23H0* CARBON STEEL NAME * /
           1          ( 3X,4A4 ) )
      ELSE
      WRITE(6,6124)
      6124 FORMAT( 23H0* NONE CARBON STEEL * )
      ENDIF
      GOTO 900
C*
      STAINLESS STEEL NAME
      130 IF ( NSS.GT.0 )      THEN
      WRITE(6,6132) ((NAMSS(J,1),J=1,4),I=1,NSS)
      6132 FORMAT( 25H0* STAINLESS STEEL NAME * /
           1          ( 3X,4A4 ) )
      ELSE
      WRITE(6,6134)
      6134 FORMAT( 25H0* NONE STAINLESS STEEL * )
      ENDIF
      GOTO 900
C*
      LEAD NAME
      140 IF ( NPB.GT.0 )      THEN
      WRITE(6,6142) ((NAMPB(J,1),J=1,4),I=1,NPB)
      6142 FORMAT( 14H0* LEAD NAME * /
           1          ( 3X,4A4 ) )
      ELSE
      WRITE(6,6144)
      6144 FORMAT( 14H0* NONE LEAD * )
      ENDIF
      GOTO 900
C

```

## Appendix F (Continued)

```

C*   WOOD NAME
150 IF ( NWD.GT.0 )          THEN
    WRITE(6,6152)  ((NAMWD(J,I),J=1,4),I=1,NWD)
152 FORMAT(14H0* WOOD NAME * /
1      ( 3X,4A4 ) )
    ELSE
    WRITE(6,6154)
154 FORMAT(14H0* NONE WOOD * )
    ENDIF
    GOTO 900
C*
C*   REFERENCE LIST
160 IF ( NREFF.GT.0 )          THEN
    DO 167 I=1,NREFF
    IF ( I.EQ.1 )              THEN
    WRITE(6,6162)  (IREFF(J,I),J=1,2)
162 FORMAT(16H0* REFERENCES * /
1      ( 3X,2A4 ) )
    ELSE
    I1 = I-2
    DO 164 J=I,1
    IF ( IREFF(I,J).NE.IREFF(1,I) )  GOTO 166
    IF ( IREFF(2,J).EQ.IREFF(2,I) )  GOTO 166
164 CONTINUE
    WRITE(6,6165)  (IREFF(J,I),J=1,2)
165 FORMAT(14H0* 3X,2A4 )
166 CONTINUE
    ENDIF
167 CONTINUE
    ELSE
    WRITE(6,6168)
168 FORMAT(20H0* NONE REFERENCE * )
    ENDIF
    GOTO 900
C*
C*   MATERIAL DATA
170 JCIRD = KQR(2)
    MATNO = IORD(JCIRD)
    DO 172 I=1,NMAT
    IF ( NAMMAT(9,I).NE.MATNO )  GOTO 172
    IMAT = I
    GOTO 174
172 CONTINUE
    WRITE(6,6173)  MATNO
173 FORMAT(26H0* NONE MATERIAL DATA, NO.,15,2H * )
    GOTO 900
C*
174 JPOS = NAMMAT(1,I)
    NREC = NAMMAT(2,I)
    CALL RDSQF (<1,IFNM, IFMT ,0, KSTAT, CDA, IDA, RDA, JPOSR)
    NRCS = JPOS-JPOS
    IF ( NRCS.GE.0 )          THEN
    CALL RDSQF (2,IFNM, IFMT ,0, KSTAT, CDA, IDA, RDA, JPOSR)
    ELSE
    CALL RDSQF (0,IFNM, IFMT ,0, KSTAT, CDA, IDA, RDA, JPOSR)
    CALL RDSQF (2,IFNM, IFMT ,JPOS, KSTAT, CDA, IDA, RDA, JPOSR)
    ENDIF
    WRITE(6,6175)
175 FORMAT(18H0* MATERIAL DATA * )
    DO 178 I=1,NREC

```

## Appendix F (Continued)

```

READ(IFNM,5176)  (CDA(J),J=1,20)
5176 FORMAT( 20H0 )
C*AE WRITE(6,6177)  (CDAX(J),J=1,20)
WRITE(6,6177)  (CDRX(J),J=1,18)
6177 FORMAT( 1X,17A4,A3 )
178 CONTINUE
    CALL RDSQF (0,IFNM, IFMT ,0, KSTAT, CDA, IDA, RDA, JPOSR)
    GOTO 900
C*
C*   MATERIAL NO. BY NAME
180 JCQRD = KQR(2)
    DO 181 I=1,4
    ICQRD(I)= ISBST(CQRD(I,JCQRD))
181 CONTINUE
    KQ = 0
    DO 184 I=1,NMAT
    IF ( NAMMAT(5,I).NE.ICQRD(1) )  GOTO 184
    IF ( NAMMAT(6,I).NE.ICQRD(2) )  GOTO 184
    IF ( NAMMAT(7,I).NE.ICQRD(3) )  GOTO 184
    IF ( NAMMAT(8,I).NE.ICQRD(4) )  GOTO 184
    IF ( KQ.EQ.0 )
    *WRITE(6,6182)
6182 FORMAT(16H0* MATERIAL NO * )
    WRITE(6,6183)  NAMMAT(9,I)
6183 FORMAT( 1H ,I10 )
    KQ = KQ+1
184 CONTINUE
    IF ( KQ.EQ.0 )
    *WRITE(6,6185)  (CQRD(I,JCQRD),I=1,4)
6185 FORMAT(28H0* NONE MATERIAL NO., NAME: ,4A4,2H * )
    GOTO 900
C*
C*   MATERIAL NO. BY REFERENCE
190 JCQRD = KQR(2)
    DO 191 I=1,4
    ICQRD(I)= ISBST(CQRD(I,JCQRD))
191 CONTINUE
    KQ = 0
    DO 194 I=1,NMAT
    IF ( NAMMAT(12,I).LE.0 )          GOTO 194
    NRF = NAMMAT(12,I)
    JRF = NAMMAT(11,I)
    DO 193 J=1,NRF
    IF ( IREFF(1,JRF).NE.ICQRD(1) )  GOTO 192
    IF ( IREFF(2,JRF).NE.ICQRD(2) )  GOTO 192
    IF ( KQ.EQ.0 )
    *WRITE(6,6182)
    WRITE(6,6183)  NAMMAT(9,I)
    KQ = KQ+1
192 JRF = JRF+1
193 CONTINUE
194 CONTINUE
    IF ( KQ.EQ.0 )
    *WRITE(6,6195)  (CQRD(I,JCQRD),I=1,2)
6195 FORMAT(33H0* NONE MATERIAL NO., REFERENCE: ,2A4,2H * )
C
900 RETURN
END

```

Appendix F (Continued)

```

SUBROUTINE EXDAT (NAMMAT, MLB )
C
      INTEGER   NAMMAT(12,1), MLB(1)
      COMMON /MLBMAX/  MNLB, MMAT, MCS, MSS, MPB, MWD, MPTEMP, MWDFIB
      1          , MTEMP, MEPSR, MEPSB, MREFF, MCMM
      COMMON /MLBIDX/  JMAT, IMAT, ICS, ISS, IPB, IWD, JWDFIB, JTEMP
      1          , JEPSR, JREFF
      COMMON /MLBALC/  LNLB, IMAL, IMA2, IMA3, IMA4, IMA5, IMA6, IMA7, IMA8
      1          , IMA9, IMA10, IMA11, IMA12, IMA13, IMA14, IMA15, IMA16
      2          , IMA17, IMA18
      COMMON /MLBFR1/  KRFM1, KRFM2, KEXL, MRFM, IRFM(10), KARG(4)
      1          , NRFCB, IRFC(10,8), RRFL(2,10,8), KSYSU
      COMMON /MLBFR2/  MRFX, NRFX, ICND(8,20), RCND(8,20), NKEPS(20)
      1          , XEPS(50,20), XSIG(50,20), NRFMX, JRFXX(2,20)
      COMMON /MLBFR3/  ICNDP(8,20), RCNDP(8,20)
      COMMON /COMPL1/  ICNDP(8,20), RCNDP(8,20)
      COMMON /COMPL2/  ATITLE(18), XXNAME(10), YYNAME(10)
      1          , XDATA(50,20), YDATA(50,20)
      COMMON /COMPL3/  XMIN, PXMAX, PYMIN, PYMAX, XL1, YL1, NPLOT
      1          , NDATA(20), NGRAPH
      COMMON /COMPL4/  AMAT1(20), ANAME(20), UNAME(3)
      CHARACTER*8     AMAT1   , ANAME   , UNAME
      CHARACTER*8     RRDATA, AMATIX  , ANAMEX
      CHARACTER*8     CDATA
      CHARACTER*4     ATITLE, XXNAME, YYNAME
      CHARACTER*4     IDATA(2)
      CHARACTER*4     KBLNK
      EQUIVALENCE    ( IDATA(1) , RRDATA )

C       DATA      KBLNK / 0 /
C
      NPLOT = 0
      IF ( NRFM.LE.0 )      GOTO 900
C
C
      DO 200 I= 1,NRFX
      CALL MLBFD (IRFM(I), MLB(IMA5), MLB(IMA6), MLB
      IF ( IMAT.LE.0 )      GOTO 200
      WRITE(ANAMEX,'(2A4)')  (NAMMAT(J,IMAT),J=5,6)
      WRITE(CDATA,'(1A4)')   NAMMAT(9,IMAT)
      READ (CDATA,'(A4)')   IDATA(1)
      READ (KBLNK,'(A4)')   IDATA(2)
      AMATIX = RRDATA
C
C
      IF ( NPLOT.LT.20 )      GOTO 110
      WRITE(6,610B)  (NAMMAT(J,IMAT),J=5,6), NAMMAT(9,IMAT)
      610B FORMAT(' *** OVERFLOW *** TOO MANY CURVES TO PLOT ( ', 
      1        '2A4,' , '15, ' )'
      GOTO 200
C
C
      110 IF ( KARG(3).GE.1 .AND. KARG(3).LE.4 ) THEN
      NPLOT = NPLOT+1
      CALL GTPROP ( NDATA(NPLOT), YDATA(1,NPLOT), XDATA(1,NPLOT)
      1          , MLB(IMA6), MLB(IMA7), MLB(IMA8), MPTEMP
      ANAME(NPLOT)  = ANAMEX
      AMAT1(NPLOT) = AMATIX
      ELSE
      CALL GTEPS (MLB(IMA6),MLB(IMA7),MLB(IMA8),MLB(IMA9),
      1          ,MLB(IMA11),MLB(IMA12),MLB(IMA13),MLB(IMA14)
      2          ,MLB(IMA15),MLB(IMA16),MPTEMP,MWDFIB,MTEMP,MEPSR
      3          ,MEPSB)
      IF ( NRFX.GT.0 )      THEN
      IF ( KARG(3).EQ.5 )      THEN
C
C
      DO 140 J= 1,NRFX
      IF ( NPLOT.LT.20 )      GOTO 115
      WRITE(6,610B)  (NAMMAT(K,IMAT),K=5,6), NAMMAT(9,IMAT)
      GOTO 140
C
C
      115 NPLOT      = NPLOT+1
      ANAME(NPLOT) = ANAMEX
      AMAT1(NPLOT) = AMATIX
      NDATAX(NPLOT)= NXEPS(J)
      NDATA      = NXEPS(J)
      DO 120 K= 1,NDATA
      XDATA(K,NPLOT)= XEPS(K,J)
      YDATA(K,NPLOT)= XSIG(K,J)
      120 CONTINUE
C
C
      ICNDP(1,NPLOT) = NAMMAT(9,IMAT)
      ICNDP(2,NPLOT) = ICND(2,J)
      ICNDP(3,NPLOT) = ICND(3,J)
      ICNDP(4,NPLOT) = 100+NAMMAT(11,IMAT)+NAMMAT(12,IMAT)
      ICNDP(5,NPLOT) = NAMMAT(5,IMAT)
      ICNDP(6,NPLOT) = NAMMAT(6,IMAT)
      ICNDP(7,NPLOT) = NAMMAT(7,IMAT)
      ICNDP(8,NPLOT) = NAMMAT(8,IMAT)
      RCNDP(4,NPLOT) = RCND(4,J)
      RCNDP(5,NPLOT) = RCND(5,J)
      RCNDP(6,NPLOT) = RCND(6,J)
      RCNDP(7,NPLOT) = RCND(7,J)
      140 CONTINUE
C
C
      ELSE
      IF ( KARG(3).EQ.6 ) CALL GTSIG ( NAMMAT(1,IMAT) )
      ENDIF
      ENDIF
      ENDIF
      200 CONTINUE
      900 RETURN
      END

```

## Appendix F (Continued)

```

SUBROUTINE MLBF0 (KMAT, NAMMAT, MATDIR, MLB)
C
      INTEGER      NAMMAT(12,1), MATDIR(10,1), MLB(1)
      COMMON /MLBALC/  MLB0, IMA1,IMA2,IMA3,IMA4,IMA5,IMA6,IMA7,IMA8
      ,IMA9,IMA10,IMA11,IMA12,IMA13,IMA14,IMA15,IMA16
      ,IMA17,IMA18
      COMMON /MLBMAX/  MLB0, MMAT, MCS, NSS, MPB, NWD, MTEMP, MWDFIB
      ,MTEMP, MEPSR, MEPS, MREF, MCOMM
      COMMON /MLBNUM/  MLB0, NMAT, MCS, NSS, NPB, NWD, NPROP(5), NDFT
      ,NWDF, NTMP, NEPSR, NEPS, NREFF, NCOMM
      COMMON /MLBIDX/  JMAT, IMAT, ICS, ISS, IPB, IWD, JWDFIB, JTEMP
      ,JEPSR, JREF
      COMMON /MLBRF1/  KRFM1, KRFM2, KEXC, MRFM, NRFM, IRFM(10), KARG(4)
      ,NRFC(8), IRFC(10,8), RRFC(2,10,8), KSYSU
      COMMON /MLBFNO/  IFNC, IFNM, IFNP, IFNR
      COMMON /RDBUF3/  CDA(10), IDA(10), RDA(50)
      CHARACTER*4     CDA
      INTEGER         JFMT1(2,3)
      CHARACTER*4     KMATE
C
      DATA  JFMT1 / 101, 0, 104, 0, 201, 0 /
      DATA  KMATE / 'MAT' /
C
      DO 20 I= 1,NMAT
      IF ( KMATE.NE.NAMMAT(9,I) )  GOTO 20
      IMAT = 1
      GOTO 40
      20 CONTINUE
      GOTO 800
C
      40 IWD = 0
      IF ( NAMMAT(4,IMAT).GE.40000 )  THEN
      IWD = NAMMAT(4,IMAT)/40000
      IWD = NAMMAT(4,IMAT)-40000*IWD
      ENDIF
C
      JMAT = NAMMAT(3,IMAT)
      IF ( JMAT.LE.0 )  THEN
      DO 60 I= 1,MLB
      IF ( KRFM1.LT.MATDIR(1,I) )  GOTO 60
      JMAT = I
      GOTO 100
      60 CONTINUE
      JMAT = 1
C
      100 KRFM1 = KRFM1+1
      IMATX = MATDIR(2,JMAT)
      NAMMAT(3,IMATX)= 0
      NAMMAT(3,IMAT) = JMAT
      JPOSRM = NAMMAT(1,IMAT)
C
      CALL RDGF (<1,IFNM, JFMT1,0, KSTAT, CDA, IDA, RDA, JPOSR)
C
      IF ( JPOSRM.NE.JPOSR )  THEN
      CALL RDGF (0,IFNM, JFMT1,0, KSTAT, CDA, IDA, RDA, JPOSR)
C
      IF ( JPOSRM.GT.0 )  THEN
      CALL RDGF (2,IFNM, JFMT1, JPOSRM, KSTAT, CDA, IDA, RDA, JPOSR)
      ENDIF
      ENDIF

```

## Appendix F (Continued)

```

C
      CALL RDGF (1,IFNM, JFMT1(1,1), 3, KSTAT, CDA(1), IDA(1), RDA
      , JPOSR)
C
      IF ( CDA(1).NE.KMAT )  GOTO 800
      CALL MLBP (NAMMAT(1,1), MLB(IMA6), MLB(IMA7), MLB(IMA8)
      ,MLB(IMA9), MLB(IMA10), MLB(IMA11), MLB(IMA12)
      ,MLB(IMA13), MLB(IMA14), MLB(IMA15), MLB(IMA16)
      ,MTEMP+PTEMP+MWDFIB,MTEMP,MEPSR,MEPS)
      ENDIF
C
      KRFM2 = KRFM2+1
      MATDIR(1,JMAT) = KRFM2
      GOTO 900
C
      800 IMAT = 0
C
      900 RETURN
      END

```

```

SUBROUTINE GTPROP (NPTEMP, PROP, PTEMP, MATDIR, PROP1, PROP2
1          ,PTEMP2)
C
      REAL      PROP(1), PTEMP(1)
      INTEGER   MATDIR(10,1)
      REAL      PROP1(4,1), PROP2(2,NPTEMP,4,1)
      COMMON /MLBIDX/  JMAT, IMAT, ICS, ISS, IPB, IWD, JWDFIB, JTEMP
      ,JEPSR, JREF
      COMMON /MLBRF1/  KRFM1, KRFM2, KEXC, MRFM, NRFM, IRFM(10), KARG(4)
      ,NRFC(8), IRFC(10,8), RRFC(2,10,8), KSYSU
C
      JARG1 = KARG(3)
      JARG2 = JARG1*4
      NPTEMP= MATDIR(JARG2,JMAT)
      IF ( NPTEMP.LE.0 )  THEN
      NPTEMP = 0
      PROP(1) = PROP1(JARG1,JMAT)
      PROP(2) = PROP1(JARG1,JMAT)
      PTEMP(1)= 0.
      PTEMP(2)= 1.
      ELSE
      DD 110 I= 1,NPTEMP
      PROP(1) = PROP2(1,I,JARG1,JMAT)
      PTEMP(1)= PROP2(2,I,JARG1,JMAT)
      110 CONTINUE
      ENDIF
C
      RETURN
      END

```

```

        Appendix F (Continued)

      SUBROUTINE GTEPSS (MATDIR,PROP1,PROP2,IDFTYP,WDFIBR,IWDFIB
1      ,DTEMP,JTEMP,DEPSR,IEPSR,EPSS,MPTEMP,MWDFIB
2      ,MTEMP,MEPSR,MEPSS)
      INTEGER MATDIR(0-1), IDFTYP(2,2,1)
      INTEGER WDFIBR(2,MWDFIB-1)
      INTEGER IWDFIB(2,MWDFIB-1)
      INTEGER ITEMP(MTEMP-1), IEPSR(2,MEPSR,MTEMP-1)
      REAL PROP1(1), PROP2(1)
      REAL DTEMP(MTEMP-1), DEPSR< MEPSR-MTEMP-1>
      REAL EPSS(MEPSS-1)
      COMMON /MLBNUM/ NMLB, NMAT, NC5, NSS, NPB, NWD, NPROP(5), NDFT
      COMMON /MLBIDX/ NUDF, NTMP, NEPSR, NEPS, NREFE, NCOMM
      COMMON /MLBRF1/ KRCM1, KRCM2, KEXC, MRFM, NRFM, IRFM(10), KARG(4)
      COMMON /MLBRF2/ NRFC(8), IRFC(10,8), RRFC(2-10,8), KSYSU
      COMMON /MLBRF3/ MRFX, NRFX, ICND(8,20), RCND(8,20), NXEPS(20)
      COMMON /MLBRF4/ XEPS(50,20), XSIG(50,20), NRFXX, JRFXX(2,20)
      DATA TOLE / 1.E-10 /
      NRFX = 0
      NRFXX = 0
      IDF1 = MATDIR(9,JMAT)
      IF ( IDF1.EQ.4 ) IDF1 = 1
      IDF2 = IDF1
      IF ( IDF1.EQ.3 ) THEN
      IDF1 = 1
      IDF2 = 2
      ENDIF
      DO 700 1= IDF1,IDF2
C* DEFORMATION TYPE *
      IF ( NRFC(1).LE.0 ) GOTO 140
      NRFCX = NRFC(1)
      DO 120 J= 1,NRFCX
      IF ( IRFC(J).EQ.1 ) GOTO 140
      120 CONTINUE
      GOTO 700
      140 JTMP1 = IDFTYP(1,J,JMAT)
      JTMP2 = IDFTYP(2,J,JMAT)+JTMP1-1
      JWDF1 = JTMP1
      JWDF2 = JTMP2
      IF ( IWD.LE.0 ) THEN
      JWDF1 = 1
      JWDF2 = 1
      ENDIF
      DO 600 J= JWDF1,JWDF2
      IF ( IWD.GT.0 ) THEN
      JTMP1 = IWDFIB(1,J,IWD)
      JTMP2 = IWDFIB(2,J,IWD)+JTMP1-1
      C* FIBRE DIRECTION OF WOOD *
      IF ( NRFC(2).LE.0 ) GOTO 170
      NRFCX = NRFC(2)
      DO 160 K= 1,NRFCX
      IF ( WDFIBR(1,J,IWD).EQ.IRFC(K) ) GOTO 170
      160 CONTINUE
      GOTO 600
      ENDIF
      170 DO 500 K= JTMP1,JTMP2
C* TEMPERATURE *
      IF ( NRFC(3).LE.0 ) GOTO 200
      NRFCX = NRFC(3)

      Appendix F (Continued)

      DO 180 L= 1,NRFCX
      IF ( DTEMP(K,JMAT).GE.RRFC(1,L-3)-TOLER
      * .AND.DTEMP(K,JMAT).LE.RRFC(2,L-3)+TOLER ) GOTO 200
      180 CONTINUE
      GOTO 500
      200 IF ( NRFXX.GE.MRFX ) GOTO 500
      NRFXX = NRFXX+1
      JRFXX(1,NRFXX) = NRFX +1
      NEPSR = ITEMP(K,JMAT)
      DO 400 L= 1,NEPSR
C* STRAIN RATE *
      IF ( NRFC(4).LE.0 ) GOTO 300
      NRFCX = NRFC(4)
      DO 220 M= 1,NRFCX
      IF ( DEPSR(L,K,JMAT).GE.RRFC(1,M-4)-TOLER
      * .AND.DEPSR(L,K,JMAT).LE.RRFC(2,M-4)+TOLER ) GOTO 300
      220 CONTINUE
      GOTO 400
      300 IF ( NRFX.GE.MRFX ) GOTO 400
      NRFX = NRFX+1
      JEPSS = IEPSR(1,L,K,JMAT)
      NEPS = IEPSR(2,L,K,JMAT)
      ISSR = IEPSR(1,MEPSR,K,JMAT)
      JEPS = IEPSR(2,MEPSR,K,JMAT)
      IF ( ISSR.EQ.1 ) THEN
      DO 320 M= 1,NEPS
      XEPS(M,NRFX) = EPSS(JEPSS ,JMAT)
      XSIG(M,NRFX) = EPSS(JEPSS+1,JMAT)
      JEPSS = JEPSS+2
      320 CONTINUE
      ELSE
      IF ( ISSR.EQ.2 ) THEN
      DO 340 M=1,NEPS
      XEPS(M,NRFX) = EPSS(JEPS ,JMAT)
      XSIG(M,NRFX) = EPSS(JEPSS,JMAT)
      JEPS = JEPS +1
      JEPSS = JEPSS+1
      340 CONTINUE
      ENDIF
      ICND(1,NRFX) = MATDIR(4,JMAT)
      ICND(2,NRFX) = 1
      IF ( MATDIR(2,JMAT).EQ.4 ) ICND(2,NRFX) = 3
      ICND(3,NRFX) = 0
      IF ( IWD.GT.0 ) ICND(3,NRFX) = WDFIBR(1,J,IWD)
      RCND(4,NRFX) = DTEMP(K,JMAT)
      RCND(5,NRFX) = DEPSR(L,K,JMAT)
      NXEPS(NRFX) = NEPS
      CALL GTEMOD (DTEMP(K,JMAT),MATDIR(1,1),PROP1(1),PROP2(1),MPTEMP
      1      ,RCND(7,NRFX))
      400 CONTINUE
      JRFXX(2,NRFXX) = NRFX
      500 CONTINUE
      600 CONTINUE
      700 CONTINUE
      RETURN
      END

```

Appendix F (Continued)

```

SUBROUTINE GTSIG (NAMMAT)
C
      INTEGER   NAMMAT(12)
      COMMON /MLBFR1/ KRFM1, KRFM2, KEXC, MRFM, NRFM, IRFM(10), KARG(4)
      COMMON /MLBFR2/ NRFC(10,8), RRFC(2,10,8), KSYSU
      COMMON /MLBFR3/ MRFX, NRFX, ICND(8,20), RCND(8,20), NXEPS(20)
      COMMON /MLBFR4/ XEPS(50,20), XSIG(50,20), NRFXX, JRFXX(2,20)
      COMMON /COMPL1/ ATITLE(18), XXNAME(10), YYNAME(10)
      COMMON /COMPL2/ XDATA(50,20), YDATA(50,20)
      COMMON /COMPL3/ XMIN, XMAX, YMINT, YMINT, XL1, YL1, MPLOT
      COMMON /COMPL4/ NDATA, NDATAX(20), NGRAPH
      CHARACTER*8  AMAT(20), ANAME(20), UNAME(3)
      CHARACTER*8  AMAT1, ANAME1, UNAME1
      CHARACTER*8  CDATA
      CHARACTER*4  ATITLE, XXNAME, YYNAME
      CHARACTER*4  IDATA(2) , KSTRA(2)
      EQUIVALENCE ( IDATA(1) , AMAT1X )
      EQUIVALENCE ( KSTRA(1) , ANAME1X )

C     DATA      KSTRA / 'STRA', 'IN =' /
C
C
C     NRFEPS = NRFC(5)
C     IF ( NRFEPS.LT.1 )      GOTO 900
C
C
C     DO 210 I= 1,NRFEPS
C     EPS = RRFC(1,I,5)
C     WRITE(CDATA,'(FB.4)') EPS
C     READ (CDATA,'(2A4)') (IDATA(J),J=1,2)
C
C
C     DO 190 J= 1,NRFXX
C     IF ( MPLOT.LT.20 )      GOTO 109
C     WRITE(6,6108) (NAMMAT(K),K=5,6), NAMMAT(9)
C     6108 FORMAT( ' **** OVERFLOW **** TOO MANY CURVES TO PLDT (',
C     1        2A4,'.',1S,.' )')
C     GOTO 190
C
C
C     109 NPLOT = NPLOT+1
C     AMAT1(NPLOT) = AMAT1X
C     ANAME(NPLOT) = ANAMEX
C     NDATAX(NPLOT) = 0
C     XDATA(1,NPLOT)= 0.
C     XDATA(2,NPLOT)= 1.
C     YDATA(1,NPLOT)= 0.
C
C
C     JEPSR1= JRFXX(1,J)
C     JEPSR2= JRFXX(2,J)
C
C

```

Appendix F (Continued)

```

C
C     IF ( JEPSR1.LE.JEPSR2 ) THEN
C       NDATA = 0
C
C
C     DO 170 K= JEPSR1,JEPSR2
C     NEPS = NXEPS(K)
C     IF ( NEPS.LE.0 )      GOTO 170
C     EPS2 = 0.
C     SIG2 = 0.
C
C
C     DO 110 L= 1,NEPS
C     EPS1 = EPS2
C     SIG1 = SIG2
C     EPS2 = XEPS(L,K)
C     SIG2 = XSIG(L,K)
C     IF ( EPS1.LE.EPS1 .AND. EPS2.LE.EPS2 ) GO TO 130
C     110 CONTINUE
C
C
C     130 NDATA = NDATA+1
C     XDATA(NDATA,NPLOT)= RCND(5,K)
C     YDATA(NDATA,NPLOT)= SIG2
C     IF ( EPS1.NE.EPS2 )
C     *YDATA(NDATA,NPLOT)= ((SIG2-SIG1)/(EPS2-EPS1))* (EPS-EPS1)+SIG1
C     170 CONTINUE
C
C
C     NDATAX(NPLOT) = NDATA
C     IF ( NDATA.EQ.1 )      THEN
C       NDATAX(NPLOT) = 0
C       XDATA(1,NPLOT)= 0.
C     ENDIF
C
C     ICNDP(1,NPLOT)= NAMMAT(9)
C     ICNDP(2,NPLOT)= ICND(2,JEPSR1)
C     ICNDP(3,NPLOT)= ICND(5,JEPSR1)
C     ICNDP(4,NPLOT)= 100*NAMMAT(11)+NAMMAT(12)
C     ICNDP(5,NPLOT)= NAMMAT(5)
C
C
C     ICNDP(6,NPLOT)= NAMMAT(6)
C     ICNDP(7,NPLOT)= NAMMAT(7)
C     ICNDP(8,NPLOT)= NAMMAT(8)
C     RCNDP(4,NPLOT)= RCND(4,JEPSR1)
C     RCNDP(6,NPLOT)= EPS
C
C     190 CONTINUE
C     210 CONTINUE
C
C
C     900 RETURN
C

```

```

        Appendix F (Continued)

SUBROUTINE GTEMOD (TEMP,MATDIR,PROP1,PROP2,MPTEMP, EMOD)
C
      INTEGER MATDIR(10,1)
      REAL PROP1(4,1), PROP2(2,MPTEMP,4,1)
      COMMON /MLBIDX/ JMAT, IMAT, ICS, ISS, IPB, IWD, JWDFIB, JTEMP
      1           , JEPSR, JREFF
C
      EMOD = PROP1(2,JMAT)
      NTMP = MATDIR(6,JMAT)
      IF ( NTMP.LT.2 ) GOTO 300
C
      DO 200 I=2,NTMP
      IF ( TEMP.LT.PROP2(2,I-1,2,JMAT) .OR. TEMP.GT.PROP2(2,I+2,JMAT) ) GOTO 200
      EMD1 = PROP2(1,I-1,2,JMAT)
      TMP1 = PROP2(2,I-1,2,JMAT)
      EMD2 = PROP2(1,I+2,JMAT)
      TMP2 = PROP2(2,I+2,JMAT)
      IF ( TMP1.EQ.TMP2 ) THEN
      EMOD = EMD1
      ELSE
      EMOD = (EMD2-EMD1)/(TMP2-TMP1)*(TEMP-TMP1)+EMD1
      ENDIF
      GOTO 300
200 CONTINUE
300 IF ( EMOD.LE.0. )
      *EMOD = 1.E+50
      RETURN
      END

SUBROUTINE EXUNI
C
      COMMON /MLBRF1/ KRFM1, KRFM2, KENC, MRFM, IRFM(10), KARG(4)
      1           , NRFC(8), IRFC(10,8), RRFC(2,10,8), KSYSU
      1           /COMPL1/ ATITLE(18), XXNAME(10), YYNAME(10)
      1           , XDATA(50,20), YDATA(50,20)
      CHARACTER*4 ATITLE, XXNAME, YYNAME
      COMMON /COMPL2/ PXMIN, PXMAX, PYMIN, PYMAX, XL1, YL1, NPLOT
      1           , NDATA, NDATAX(20), NGRAPH
      1
      IF ( KSYSU.NE.2 .OR. NPLOT.LE.0 ) GOTO 900
C
      DO 200 I=1,NPLOT
      NDAT = JABS (NDATAX(I))
      IF ( NDAT.EQ.0 ) NDAT = 2
C
      CALL EXUNI2 (KARG(1), XDATA(1,I), NDATA)
      CALL EXUNI2 (KARG(2), YDATA(1,I), NDATA)
200 CONTINUE
C
      900 RETURN
      END

```

```

        Appendix F (Continued)

SUBROUTINE EXUNI2 (KDTYP, DATA, NDATA)
C
      DIMENSION DATA(1)
C
      IF ( KDTYP.LT.1
      *.OR. KDTYP.GT.10 ) GOTO 900
C
      GOTO ( 110,120,130,140,150,160,170,180,190,200 ), KDTYP
C
C* COEF. OF THERMAL EXPANSION
      110 CONTINUE
      GOTO 900
C
C* YOUNG'S MODULUS
      120 DO 125 I=1,NDATA
      DATA(I) = 0.101972*DATA(I)
      125 CONTINUE
      GOTO 900
C
C* SHEAR MODULUS
      130 DO 135 I=1,NDATA
      DATA(I) = 0.101972*DATA(I)
      135 CONTINUE
      GOTO 900
C
C* POISSON'S RATIO
      140 CONTINUE
      GOTO 900
C
C* DEFORMATION TYPE
      150 CONTINUE
      GOTO 900
C
C* FIBRE DIRECTION OF WOOD
      160 CONTINUE
      GOTO 900
C
C* TEMPERATURE
      170 DO 175 I=1,NDATA
      DATA(I) = DATA(I)-273.
      175 CONTINUE
      GOTO 900
C
C* STRAIN RATE
      180 CONTINUE
      GOTO 900
C
C* STRAIN
      190 CONTINUE
      GOTO 900
C
C* STRESS
      200 DO 205 I=1,NDATA
      DATA(I) = 0.101972*DATA(I)
      205 CONTINUE
C
      900 RETURN
      END

```

## Appendix F (Continued)

```

SUBROUTINE EXOUT (KLST,KPLT,KFIT,IREFF)
C
      INTEGER IREFF()
      COMMON /MLBFNO/ IFNC, IFNM, IFNP, IFNR
      COMMON /MLBRF1/ KRFM1, KRFM2, KEXC, MRFM, NRFM, IRFM(10), KARG(4)
      1   HRCG(8), IRFC(10-8), RRFC(2-10-8), KSYSU
      1   COMMON /COMPL1/ ATITLE(18), XXNAME(10), YYNAME(10)
      1   XDATA(50,20), YDATA(50,20)
      1   COMMON /COMPL2/ PXMIN, PMAX, PYMIN, PYMAX, XL1, YL1, NPLOT
      1   NDATA, NDATA(20), NSGRAPH
      1   COMMON /COMPL3/ AMAT1(20), ANAME(20), UNAME(3)
      CHARACTER*B AMAT1, ANAME, UNAME
      CHARACTER*B KBLNK
      CHARACTER#4 ATITLE, XXNAME, YYNAME
      CHARACTER#4 TITLES(6,11)
      CHARACTER#4 TITLEM(6,11)
C
C
      DATA TITLES / 4HTHER, 4HMAL, 4HEXPA, 4HNSID, 4HN (1, 4H/K)
      2   , 4H E, 4H MOD, 4HULUS, 4H (MP, 4HA) , 4H
      3   , 4H G, 4H MOD, 4HULUS, 4H (MP, 4HA) , 4H
      4   , 4HPOIS, 4HSN, 4HS RA, 4HTIO , 4H(-) , 4H
      5   , 4HDEFD, 4HRMAT, 4HION, 4HTYPE, 4H , 4H
      6   , 4HFIBR, 4HE DI, 4HRECT, 4HION , 4HOF W, 4HOOD
      7   , 4HTEMP, 4HERAT, 4HURE , 4H(K, 4H) , 4H
      8   , 4HSTR, 4HIN R, 4HATE , 4H(1/5, 4H) , 4H
      9   , 4H , 4H STR, 4HAIN , 4H(-) , 4H , 4H
      A   , 4H , 4H STR, 4HESS , 4H(MPA, 4H) , 4H
      B   , 4H /, 4H/C
      DATA TITLEM / 4HTHER, 4HMAL, 4HEXPA, 4HNSID, 4HN (1, 4H/C)
      2   , 4H E, 4H MOD, 4HULUS, 4H (KG, 4HF/MM, 4H#2)
      3   , 4H G, 4H MOD, 4HULUS, 4H (KG, 4HF/MM, 4H#2)
      4   , 4HPOIS, 4HSN, 4HS RA, 4HTIO , 4H(-) , 4H
      5   , 4HDEFD, 4HRMAT, 4HION, 4HTYPE, 4H , 4H
      6   , 4HFIBR, 4HE DI, 4HRECT, 4HION , 4HOF W, 4HOOD
      7   , 4HTEMP, 4HERAT, 4HURE , 4H(C) , 4H , 4H
      8   , 4HSTR, 4HIN R, 4HATE , 4H(1/5, 4H) , 4H
      9   , 4H , 4H STR, 4HAIN , 4H(-) , 4H , 4H
      A   , 4H , 4H STR, 4HESS , 4H(KGF, 4H/MM#, 4H#2)
      B   , 4H /, 4H
      DATA KBLNK / 4H /
C
C
      IF ( KFIT.NE.0 ) CALL EXFIT
C
C
      CALL NEWPEN (2)
      IF ( KLST.NE.0 .OR. KPLT.NE.0 ) NSGRAPH = NSGRAPH + 1
      IF ( NSGRAPH.EQ.1 ) THEN
      C (1) CALL PLOTS (0.,0.,0.)
      C (2) CALL PLOT (0.,0.,-3)
      ENDIF
      J = KARG(1)
      IF ( J.LT.1 .OR. J.GT.10 ) J = 11
      IF ( KSYSU .EQ. 2 ) GOTO 200

```

## Appendix F (Continued)

```

C
C
      UNIT IS SI
C
      DO 120 I= 1,6
      XXNAME(I) = TITLES(I,J)
      120 CONTINUE
C
C
      J = KARG(2)
      IF ( J.LT.1 .OR. J.GT.10 ) J = 11
      DO 140 I= 3,6
      YYNAME(I) = TITLES(I,J)
      140 CONTINUE
C
C
      DO 160 I= 1,3
      UNAME(I)= KBLNK
      160 CONTINUE
      GO TO 300
C
C
      UNIT IS MKS
C
      200 CONTINUE
      DO 220 I= 1,6
      XXNAME(I) = TITLEM(I,J)
      220 CONTINUE
C
C
      J = KARG(2)
      IF ( J.LT.1 .OR. J.GT.10 ) J = 11
      DO 240 I= 1,6
      YYNAME(I) = TITLEM(I,J)
      240 CONTINUE
C
C
      DO 260 I= 1,3
      UNAME(I)= KBLNK
      260 CONTINUE
      300 CONTINUE
C
C
      IF ( KLST.NE.0 ) THEN
      CALL EXLSTP (IREFF(1))
      ENDIF
      IF ( KPLT.NE.0 ) CALL EXGRAP (IREFF(1))
      CALL NEWPEN (1)
      RETURN
END

```

```

        Appendix F (Continued)

SUBROUTINE EXFIT
C
COMMON /MLBFT1/ KFIT, IEQFIT, CODEF(16), COEFO(6,16)
1      MXY, MXYD(5), XYD(2,50,5), MXY, MXYD
COMMON /MLBRF3/ ICNDP(8,20), RCNDP(8,20)
COMMON /CDMPL1/ ATITLE(10), XXNAME(10), YYNAME(10)
1      XDATA(50,20), YDATA(50,20)
CHARACTER*4 ATITLE, XXNAME, YYNAME
COMMON /CDMPL2/ PMIN, PMAX, PYMIN, PYMAX, XL1, YL1, NPLOT
1      NDATA, NDATAX(200), NGRAPH
COMMON /CDMPL3/ AMAT1(20), ANAME(20), UNAME(3)
CHARACTER*8 AMAT1, ANAME, UNAME
CHARACTER*8 AMAT1X, ANAMEX
INTEGER IFITXY(16)
CHARACTER*4 IDATA(4)
EQUIVALENCE ( IDATA(1),AMAT1X ), (IDATA(3),ANAMEX )
C
DATA IFITXY / 2+1,2+2,1+1,2+2,2+2,1+2,2+2 /
DATA IDATA / 'PRE.', 'DATA', 'FITT', 'ING' /
C
IF ( KFIT.NE.1 ) GOTO 200
CALL EXFIT1
GOTO 900
200 IF ( NPLOT.LE.0 ) GOTO 900
IF ( NPLOT.LE.20) GOTO 210
WRITE(6,6208)
6208 FORMAT( ' **** OVERFLOW **** TOO MANY CURVES TO PLOT ' )
NPLOT = 20
210 NPLOT = NPLOT
NPLOT = NPLOT+NPLOT
JPLT1 = NPLOT
JPLT2 = NPLOT
DO 500 I= 1,NPLOT
ANAME(JPLT2) = ANAMEX
AMAT1(JPLT2) = AMAT1X
NDATA = NDATAX(JPLT1)
IF ( NDATA.EQ.0 ) THEN
NDATAX(JPLT2) = 0
DO 220 J= 1,2
XDATA(J,JPLT2) = XDATA(J,JPLT1)
YDATA(J,JPLT2) = YDATA(J,JPLT1)
220 CONTINUE
DO 230 J= 1,8
ICNDP(J,JPLT2) = ICNDP(J,JPLT1)
RCNDP(J,JPLT2) = RCNDP(J,JPLT1)
230 CONTINUE
ELSE
IF ( KFIT.EQ.2 ) THEN
IF ( COEF(1).EQ.0 .AND. COEF(2).EQ.0. ) THEN
CALL EXFIT2 (XDATA(1,JPLT1),YDATA(1,JPLT1),NDATA, A, B)
ELSE
A = COEF(1)
B = COEF(2)
ENDIF
NDATAX(JPLT2) = -2
XDATA(1,JPLT2) = PMIN
XDATA(2,JPLT2) = PMAX
XDATA(9,JPLT2) = -9999.
XDATA(8,JPLT2) = A
XDATA(7,JPLT2) = B
ENDIF
500 CONTINUE

```

```

Appendix F (Continued)

DO 240 J= 1,2
YDATA(J,JPLT2) = B*XDATA(J,JPLT2)+A
240 CONTINUE
WRITE(6,6250)
6250 FORMAT( / 12X,'X',15X,'Y',9X,'FITTING',5X,'PERCENT' / )
DO 270 J=1,NDATA
FIT = A*XDATA(J,JPLT1)+B
IF ( ABS (FIT) .LE.1.0E-50 ) THEN
ERR = YDATA(J,JPLT1)
ELSE
ERR = (YDATA(J,JPLT1)-FIT)/FIT*100.
ENDIF
WRITE(6,6260) XDATA(J,JPLT1), YDATA(J,JPLT1), FIT, ERR
6260 FORMAT( 1X,1P2E16.3,E13.5,OF10.1 )
270 CONTINUE
IF ( KFIT.EQ.3 ) THEN
CALL EXFIT3 (XDATA(1,JPLT1),YDATA(1,JPLT1),NDATAX(JPLT1),
,RCNDP(1,JPLT1), XDATA(1,JPLT2), YDATA(1,JPLT2),
,NDATAX(JPLT2))
1      WRITE(6,6250)
DO 275 J=1,NDATA
IF ( IFITXY(IEQFIT).EQ.1 ) THEN
FIT = XDATA(J,JPLT2)
IF ( ABS (FIT) .LE.1.0E-50 ) THEN
ERR = XDATA(J,JPLT1)
ELSE
ERR = (XDATA(J,JPLT1)-FIT)/FIT*100.
ENDIF
IF ( ABS (FIT) .LE.1.0E-50 ) THEN
ERR = YDATA(J,JPLT1)
ELSE
ERR = (YDATA(J,JPLT1)-FIT)/FIT*100.
ENDIF
ENDIF
WRITE(6,6260) XDATA(J,JPLT1), YDATA(J,JPLT1), FIT, ERR
275 CONTINUE
ENDIF
JPLT2 = JPLT2-1
ANAME(JPLT2) = ANAME(JPLT1)
AMAT1(JPLT2) = AMAT1(JPLT1)
NDATAX(JPLT2) = NDATAX(JPLT1)
NDATA = NDATAX(JPLT1)
IF ( NDATA.EQ.0 ) NDATA = -2
DO 280 J= 1,NDATA
XDATA(J,JPLT2) = XDATA(J,JPLT1)
YDATA(J,JPLT2) = YDATA(J,JPLT1)
280 CONTINUE
DO 290 J= 1,B
ICNDP(J,JPLT2) = ICNDP(J,JPLT1)
RCNDP(J,JPLT2) = RCNDP(J,JPLT1)
290 CONTINUE
JPLT2 = JPLT2-1
JPLT1 = JPLT1-1
500 CONTINUE
900 RETURN
END

```

Appendix F (Continued)

```

SUBROUTINE EXFIT1
C
COMMON /MLBFT1/ KFIT, IEGFIT, NCoeff(16), COEF(6), COEFO(6,16)
      , NXY, NXVD(5), XVD(2,50,5), MXY, MXYD
COMMON /CDMPL1/ ATITLE(18), XXNAME(10), YYNAME(10)
      , XDATA(50,20), YDATA(50,20)
CHARACTER*4 ATITLE, XXNAME, YYNAME
COMMON /COMPL2/ PXMIN, PXMAX, PYMIN, PYMAX, XL1, YL1, NPLOT
      , NDATA, NDATAX(20), NGRAPH
      , NDATA(NPLOT)-NDATA
C
C
C
      IF ( NXY.LE.0 )      GOTO 900
      DO 140 I=1,NXY
      NDATA = NXVD(I)
      IF ( NDATA.LE.0 )      GOTO 140
      NPLOT = NPLOT+1
      NDATA(NPLOT)=NDATA
C
C
C
      DO 120 J=1,NDATA
      XDATA(I,J,NPLOT)= XVD(1,J,I)
      YDATA(I,J,NPLOT)= XVD(2,J,I)
120 CONTINUE
140 CONTINUE
C
C
C
900 RETURN
END

```

```

SUBROUTINE EXMINX (DATA,MD1,NPLOT,NDATA, DMIN, DMAX)
C
DIMENSION DATA(MD1,1), NDATAX(1)
DATA DMIN, DMAX / 1.E70, -1.E70 /
C
DMIN = 0.
DMAX = 0.
IF ( NPLOT.LE.0 )      GOTO 900
DMIN = DMIN
DMAX = DMAX
C
DO 200 I= 1,NPLOT
NDATA = IABS (NDATAX(1))
IF ( NDATA.EQ.0 )      NDATA = 2
DO 100 J= 1,NDATA
DMIN = AMIN1 (DMIN,DATA(I,J))
DMAX = AMAX1 (DMAX,DATA(I,J))
100 CONTINUE
200 CONTINUE
C
900 RETURN
END

```

Appendix F (Continued)

```

SUBROUTINE EXFIT2 (XDATA,YDATA,NDATA, A, B)
DIMENSION XDATA(1), YDATA(1)
DIMENSION AA(2), BB(2), SE(2)
EQUIVALENCE ( AA(1),A1 ), ( BB(1),B1 ), ( SE(1),SE1 )
EQUIVALENCE ( AA(2),A2 ), ( BB(2),B2 ), ( SE(2),SE2 )
DATA EPS / 1.E-10 /
SE(1) = -1.
SE(2) = 0.
A1 = 0.
B1 = 0.
IF ( NDATA.LE.1 )      GOTO 80
XM = XDATA(1)
YM = YDATA(1)
DO 20 I= 2,NDATA
XM = XDATA(I)+XM
YM = YDATA(I)+YM
20 CONTINUE
XM = XM/NDATA
YM = YM/NDATA
SX = 0.
SY = 0.
SXY = 0.
DO 40 I= 1,NDATA
RX = XDATA(I)-XM
RY = YDATA(I)-YM
SX = RX*RX-SX
SY = RY*RY-SY
SXY = RX*RY+SXY
40 CONTINUE
C
C
      IF ( SX.LT.EPS )      GOTO 60
      B1 = SXY/SX
      A1 = YM-B1*XM
      SE1 = SY-B1*SXY
60 IF ( SY.LT.EPS )      GOTO 80
      B2 = SXY/SY
      A2 = XM-B2*YM
      SE2 = SX-B2*SXY
      C = ABS (B2)
      IF ( C.LT.EPS )      GOTO 80
      B2 = B2/C
      A2 = 1.0/C
      A2 = -A2/C
      GOTO 100
C
C
      80 A = 0.
      B = 0.
100 I = 1
      IF ( SE(1).GT.SE(2) ) I = 2
      IF ( SE(1).LT.0. ) I = I + 1
      IF ( I.GT.2 ) I = 1
      B = BB(I)
      A = AA(I)
      RETURN
END

```

```

          Appendix F (Continued)
SUBROUTINE EXFIT3 (XDATA1,YDATA1,NDATA1,RCND1, XDATA, YDATA
1           , NDATAX)
C
DIMENSION XDATA1(1), YDATA1(1), RCND1(B), XDATA(1), YDATA(1)
COMMON /MLBFT1/ KFIT, IEQFIT, COEFC(16), COEOF(6-16)
1           , NXY, NYXD(5), XYD(2,50,5), MXY, MXYD
COMMON /MLBFT2/ NEQCF(16), IEQCF(6-16)
CHARACTER*4 IEQCF
COMMON /MLBRF1/ KRFM1, KRFM2, KEXC, MRFM, NRFM, IRFM(10),
1           , MRFC(8), IRFC(10,B), RRFC(2,10,B), KSYSU
C
DATA EE   / 2.71828 /
DATA NXX  / 50      /
DATA TOLLE / 1.0E-10 /
C
C
CALL EXMINX (XDATA1(1)-NDATA1/1-NDATA1, XMN1, XMX1)
DX   = XMN1-XMX1
IF ( DX.GT.TOLLE ) GOTO 120
NDATAX = 0
XDATA(1)= XDATA1(1)
XDATA(2)= XDATA1(1)
YDATA(1)= YDATA1(1)
YDATA(2)= YDATA1(1)
GOTO 900
120 DX   = DX/NXX
XMN   = XMN1-DX
C
IF ( IEQFIT .LT. 1 .OR. IEQFIT.GT.15 ) GO TO 700
IF ( KARG(2).NE.10 ) GOTO 800
IF ( KARG(1).EQ. 9 .AND. ( IEQFIT.LE.13 .OR. IEQFIT.EQ.15 ) )
1   GO TO 200
IF ( KARG(1).EQ. 8 .AND. IEQFIT.GE.11 ) GO TO 200
C
200 GOTO ( 210,220,230,240,250,260,270,280,290,300
1   , 310,320,330,340,350 ), IEQFIT
C
C
210 N    = COEFC(1)+0.01
XK   = COEFC(2)
NDATAX = -NDATA1
NDATA  = NDATA1
DO 212 I=1,NDATA
XDATA(I)= XDATA1(I)
YDATA(I)= (XDATA(I)==N)*XK
212 CONTINUE
GOTO 900
C
C
220 DVN   = 1./COEFC(1)
XK   = COEFC(2)
C   = COEFC(3)
E   = COEFC(4)
IF ( E.LE.0. ) E = RCND1(7)
NDATAX = -NDATA1
NDATA  = NDATA1
DO 222 I=1,NDATA
XDATA(I)= YDATA1(I)/E+((YDATA1(I)-SIG0)/XK)**DVN
YDATA(I)= YDATA1(I)
222 CONTINUE
GOTO 900
C
C
230 DVN   = 1./COEFC(1)
XK   = COEFC(2)
SIG0  = COEFC(3)
E   = COEFC(4)
IF ( E.LE.0. ) E = RCND1(7)
NDATAX = -NDATA1
NDATA  = NDATA1
DO 232 I=1,NDATA
YDATA(I)= YDATA1(I)/E+((YDATA1(I)-SIG0)/XK)**DVN
YDATA(I)= YDATA1(I)
232 CONTINUE
GOTO 900
C
C
240 N    = COEFC(1)+0.01
XK   = COEFC(2)
SIG0  = COEFC(3)
E   = COEFC(4)
IF ( E.LE.0. ) E = RCND1(7)
EPSC  = SIG0/E
NDATAX = -NDATA1
NDATA  = NDATA1
DO 242 I=1,NDATA
XDATA(I)= XDATA1(I)
YDATA(I)= ((XDATA1(I)-EPSC)**N)*XK+SIG0
242 CONTINUE
GOTO 900
C
C
250 L    = COEFC(1)+0.01
M   = COEFC(2)+0.01
N   = COEFC(3)+0.01
EL   = EE**L
EM   = EE**M
NDATAX = -NDATA1
NDATA  = NDATA1
DO 252 I=1,NDATA
EPSL  = XDATA1(I)
XDATA(I)= EPSL
YDATA(I)= COEFC(4)*EPSL**N+EL*EM**EPSL
252 CONTINUE
GOTO 900
C
C
260 DVN   = 1./COEFC(1)
A   = COEFC(2)
SIG0  = COEFC(3)
E   = COEFC(4)
IF ( E.LE.0. ) E = RCND1(7)
NDATAX = -NDATA1
NDATA  = NDATA1
DO 262 I=1,NDATA
XX1  = 1.-(YDATA1(I)-SIG0)/A
IF ( XX1.LE.0. ) XX1 = 1.
XDATA(I)= YDATA1(I)/E-DVN*ALOG(XX1)

```

## Appendix F (Continued)

```

YDATA(I)= YDATA1(I)
262 CONTINUE
GOTO 900
C
270 DVM    = 1./COEF(1)
XM     = COEF(2)
SIGC   = COEF(2)
SIG1   = COEF(3)
E      = COEF(4)
IF ( E.LE.0. ) E = RCND1(7)
XX1   = XM*SIG1
XX2   = 1. / (SIGC-SIG1)
NDATAX = -NDATA1
NDATA  = NDATA1
DO 272 I=1,NDATA
XX3   = YDATA1(I)*XX2
IF ( XX3.LE.0. ) XX3 = 1.
XDATA(I)= YDATA1(I)/E+XX1-XM*ALDG(XX3)
YDATA(I)= YDATA1(I)
272 CONTINUE
GOTO 900
C
280 N      = COEF(1)+0.01
N      = -N
A      = COEF(2)
B      = COEF(3)
NDATAX = -NDATA1
NDATA  = NDATA1
DO 282 I=1,NDATA
XDATA(I)= XDATA1(I)
YDATA(I)= A-B*XDATA1(I)**N
282 CONTINUE
GOTO 900
C
290 C      = COEF(1)
H      = COEF(2)
P      = COEF(3)
SIG0   = COEF(4)
CP     = C*P
NDATAX = -NDATA1
NDATA  = NDATA1
DO 292 I=1,NDATA
EPSN  = XDATA1(I)
XDATA(I)= EPSP
YDATA(I)= SIG0+CP*EPSP/(1.+P*EPSP)+H*EPSP
292 CONTINUE
GOTO 900
C
300 K      = COEF(1)+0.01
K2    = N+2
NDATAX = -NDATA1
NDATA  = NDATA1
DO 304 I=1,NDATA
XDATA(I)= XDATA1(I)
YDATA(I)= COEF(2)
DO 302 J=3,N2

```

## Appendix F (Continued)

```

YDATA(I)= YDATA(I)+ COEF(J)*(XDATA(I)**(J-2))
302 CONTINUE
304 CONTINUE
GOTO 900
C
310 N      = COEF(1)+0.01
A      = COEF(2)
B      = COEF(3)
NDATAX = -NDATA1
NDATA  = NDATA1
IF ( KAR0(I).EQ.8 ) THEN
EPSN  = RCND1(6)**N
DO 312 I=1,NDATA
XDATA(I)= XDATA1(I)
YDATA(I)= A*(1.+B*ALDG(XDATA1(I)))*EPSN
312 CONTINUE
ELSE
EPSR  = RCND1(5)
XX1   = A*(1.+B*ALDG(EPSR))
DO 314 I=1,NDATA
XDATA(I)= XDATA1(I)
YDATA(I)= XX1*(XDATA1(I)**N)
314 CONTINUE
ENDIF
GOTO 900
C
320 M      = COEF(1)+0.01
N      = COEF(2)+0.01
XX    = COEF(3)
C      = COEF(4)
NDATAX = -NDATA1
NDATA  = NDATA1
IF ( KAR0(I).EQ.8 ) THEN
EPSN  = RCND1(6)**N
DO 322 I=1,NDATA
XDATA(I)= XDATA1(I)
YDATA(I)= XX*(1.+C*(XDATA1(I)**M))*EPSN
322 CONTINUE
ELSE
EPSR  = RCND1(5)
XX1   = XX*(1.+C*(EPSR**M))
DO 324 I=1,NDATA
XDATA(I)= XDATA1(I)
YDATA(I)= XX1*(XDATA1(I)**N)
324 CONTINUE
ENDIF
GOTO 900
C
330 DVM    = 1./COEF(1)
M      = COEF(1)+0.01
C      = COEF(2)
H      = COEF(3)
SIGY   = COEF(4)
E      = COEF(5)
IF ( E.LE.0. ) E = RCND1(7)
HSIGY  = H*SIGY
NDATAX = -NDATA1

```

```

        Appendix F (Continued)

      NDATA = NDATA1
      IF ( KARG(1).EQ.8 ) THEN
      EPS = RCND1(6)
      XX1 = SIGY*(1.+HSIGY*EPS)
      DO 332 I=1,NDATA
      EPS = EPS-YDATA1(I)/E
      XDATA1(I) = C*(YDATA1(I)/(H*EPS+SIGY)-1.)*M
      YDATA1(I) = YDATA1(I)
332 CONTINUE
      ELSE
      EPSR = RCND1(5)
      XX1 = SIGY/H
      XX2 = 1. / (SIGY*(1.+(EPSR/C)*DVM))
      DO 334 I=1,NDATA
      EPS = EPS-YDATA1(I)/E+XX1*(YDATA1(I)*XX2-1.)
      XDATA1(I) = YDATA1(I)
334 CONTINUE
      ENDIF
      GOTO 900
C
C
      340 XK = CDEF(1)
      C = CDEF(2)
      NDATAX = -NDATA1
      NDATA = NDATA1
      DO 342 I=1,NDATA
      XDATA1(I) = XDATA1(I)
      YDATA1(I) = XK+C*ALOG(XDATA1(I))
342 CONTINUE
      GOTO 900
C
C
      350 M = CDEF(1)+0.01
      N = CDEF(2)+0.01
      XK = CDEF(3)
      NDATAX = -NDATA1
      NDATA = NDATA1
      IF ( KARG(1).EQ.8 ) THEN
      EPSN = RCND1(6)
      XX1 = XK*(EPSN**N)
      DO 352 I=1,NDATA
      XDATA1(I) = XDATA1(I)
      YDATA1(I) = XX1*(XDATA1(I)**M)
352 CONTINUE
      ELSE
      EPSR = RCND1(5)
      XX1 = XK*(EPSR**M)
      DO 354 I=1,NDATA
      XDATA1(I) = XDATA1(I)
      YDATA1(I) = XX1*(XDATA1(I)**N)
354 CONTINUE
      ENDIF
      GOTO 900
700 WRITE(6,6710) IEQFIT
6710 FORMAT(15HO* EQUATION NO.,I3,19H IS NOT AVAILABLE * )
      GOTO 900
800 WRITE(6,6810)
6810 FORMAT(3OH* UNMATCH DATA AND EQUATION * )
900 RETURN
END

```

```

        Appendix F (Continued)

SUBROUTINE EXLSTP (IREFF)
C
      INTEGER IREFF(2,1)
      COMMON /MLBIDX/ JMAT, IMAT, ICS, ISS, IPB, IWD, JWDFIB, JTEMP
      COMMON /MLBRF1/ JEPSR, JREFF
      COMMON /MLBRF2/ KRFM1, KRFM2, KEXC, MRFM, NRFM, IRFM(10), KARG(4)
      COMMON /MLBRF3/ NRFC(10), IRFC(10,B), RRFC(2,10,B), KSYSU
      COMMON /MLBRF5/ ICNDP(8,20), RCNDP(8,20)
      COMMON /COMPL1/ ATITLE(18), XXNAME(10), YYNAME(10)
      COMMON /COMPL2/ XDATA(50,20), YDATA(50,20)
      COMMON /COMPL2/ PXMIN, PXMAX, PYMIN, PYMAX, XL1, YL1, NPLOT
      COMMON /COMPL2/ NDATA, NDATA(20), NGRAPH
      DATA CBLNK / ' ' /
C
      DATA KDFTYP / 4HCOMP,4HRESS,4HION
      1 / 4HTENS,4HION ,4H
      2 / 4H ,4H ,4H ,4H /
      DATA IXVSY / 4H THE,4H RHMAL,4H EXP,4HANSI,4HON ,4H1/K)
      1 / 4HYDN,4H'S,4HMODU,4HLUS ,4H(CPA,4H)
      2 / 4H SHE,4HAR M,4HODUL,4HUS ,4H(CMPA),4H
      3 / 4H POI,4HSSON,4H'S R,4HATIO,4H (-),4H
      4 / 12*4H
      5 / 4H T,4HEMPE,4HRATU,4HRE ,4H(K), ,4H
      6 / 4H ST,4HRAIN,4H RAT,4HE (1,4H/S) ,4H
      7 / 4H ,4H STR,4HAIN ,4H(-),4H ,4H
      8 / 4H ,4HSTRE,4HSS ,4H(CMPA),4H ,4H
      9 / 4H THE,4H RHMAL,4H EXP,4HANSI,4HON ,4H1/C)
      A / 4H ,4H MOD,4HLUS,4H (KG,4HF/MM,4H**2)
      B / 4H G,4H MOD,4HLUS,4H (KG,4HF/MM,4H**2)
      C / 4H POI,4HSSON,4H'S R,4HATIO,4H (-),4H
      D / 12*4H
      E / 4H T,4HEMPE,4HRATU,4HRE ,4H
      F / 4H ST,4HRAIN,4H RAT,4HE (1,4H/S) ,4H
      G / 4H ,4H STR,4HAIN ,4H(-),4H ,4H
      H / 4H ST,4HRESS,4H (KG,4HF/MM,4H**2),4H /
C
C* PLOT MATERIAL DATA *
C
C* TITLE =
      CALL PLOT (0.,0.,666)
      CALL NEWPEN (1)
      WRITE(CTITLE,'(18A4)') (ATITLE(I),I=1,18)
      READ (CTITLE,'(72A1)') (CTITLE2(I),I=1,72)
      DO 500 I=1,NPLOT
      CALL SYMBOL ( 5.0,190.,3.,'TABLE' , ' ',0.,13)
      JK = 73
      DO 100 IK=2,72
      JK = JK-1
      IF ( CTITLE2(JK).EQ.CBLNK ) GOTO 100
      CALL SYMBOL (50.,190.,3.,CTITLE2(I),0.,JK)
      GOTO 110
100 CONTINUE
110 CONTINUE

```

## Appendix F (Continued)

```

XX = 0.0
YY = 180.0
C
X = XX+5.0
Y = YY-4.0
CALL SYMBOL (X , Y, 3.0, 'MATERIAL', 0.0, 8)
CALL SYMBOL (X+39.0, Y, 3.0, 'CURVE NO.', 0.0, 10)
X = X+69.0
RI = 1
CALL NUMBER (X, Y, 3.0, RI, 0.0, -1)
IF ( I.GE.10 ) X = X + 3.0
CALL SYMBOL (X+3.0, Y, 3.0, ' ', 0.0, 1)
YY = Y
C
NDATA = IABS (NDATA(I))
IF ( XDATA(9,I).EQ.-9999.0 .AND. NDATA.EQ.2 ) THEN
X = XX+14.0
Y = YY- 7.0
CALL SYMBOL (X,Y,3.0, 'FITTING BY LINEAR REGRESSION', 0.0, 2B)
Y = Y-5.0
CALL SYMBOL (X,Y,3.0, ' Y = A * X + B ', 0.0, 18)
Y = Y-5.0
CALL SYMBOL (X,Y,3.0, ' A = ', 0.0, 7)
WRITE (ICCHAR, '(1PE10.3)') XDATA(7,I)
READ (ICCHAR, '(3A4)' ) (ICHA(J),J=1,3)
CALL SYMBOL (X+21.0, Y, 3.0, ICCHA(1), 0.0, 10)
Y = Y-5.0
CALL SYMBOL (X,Y,3.0, ' B = ', 0.0, 7)
WRITE (ICCHAR, '(1PE10.3)') XDATA(8,I)
READ (ICCHAR, '(3A4)' ) (ICHA(J),J=1,3)
CALL SYMBOL (X+21.0, Y, 3.0, ICCHA(1), 0.0, 10)
YY = Y
ELSE
C
IF ( NDRTAX(I).GT.0 ) THEN
X = XX+14.0
Y = YY- 7.0
CALL SYMBOL (X,Y,3.0, 'NAME:', 0.0, 5)
X1 = X+18.0
CALL SYMBOL (X1,Y,3.0, ICNDP(5,I), 0.0, 16)
C
JRF = ICNDP(4,I)/100
NRF = ICNDP(4,I)-100*JRF
IF ( NRF.LE.0 ) GOTO 160
X2 = X+74.0
CALL SYMBOL (X2,Y,3.0, 'REFERENCES:', 0.0, 11)
X2 = X+10.0
DO 155 J=1,NRF
CALL SYMBOL (X2,Y,3.0, IREFF(1,JRF), 0.0, 8)
X2 = X2-27.0
JRF = JRF+1
155 CONTINUE
C
160 Y = Y-5.0
CALL SYMBOL (X,Y,3.0, 'NO.', 0.0, 3)
RI = ICNDP(1,I)
CALL NUMBER (X+18.0, Y, 3.0, RI, 0.0, -1)
YY = Y
C

```

## Appendix F (Continued)

```

C
X = XX+10.0
Y = YY- 4.0
IF ( KARG(3).EQ.5 .OR. KARG(3).EQ.6 ) THEN
X1 = X+4.0
Y1 = Y-5.0
K = ICNDP(2,I)
CALL SYMBOL (X1,Y1,3.0, 'DEFORMATION TYPE', 0.0, 16)
X2 = X+61.0
CALL SYMBOL (X2,Y1,3.0, KDFTP(1,K), 0.0, 12)
X2 = X+61.0
CALL PLOT (X+98.0, Y1-2.0, 3)
CALL PLOT (X , Y1-2.0, 2)
C
IF ( IWD.GT.0 ) THEN
Y1 = Y1-7.0
CALL SYMBOL (X1,Y1,3.0, 'FIBRE DIRECTION', 0.0, 15)
CALL SYMBOL (X2,Y1,3.0, ICNDP(5,I), 0.0, 4)
CALL PLOT (X+98.0, Y1-2.0, 3)
CALL PLOT (X , Y1-2.0, 2)
ENDIF
C
Y1 = Y1-7.0
CALL SYMBOL (X1 , Y1, 3.0, 'TEMPERATURE (K)', 0.0, 15)
CALL NUMBER (X2+3.0, Y1, 3.0, RCNDP(4,I), 0.0, 2)
CALL PLOT (X+98.0, Y1-2.0, 3)
CALL PLOT (X , Y1-2.0, 2)
C
Y1 = Y1-7.0
IF ( KARG(3).EQ.5 ) THEN
WRITE (ICCHAR, '(1PE10.3)') RCNDP(5,I)
CALL SYMBOL (X1,Y1,3.0, 'STRAIN RATE (1/S)', 0.0, 17)
ELSE
WRITE (ICCHAR, '(1PE10.3)') RCNDP(6,I)
CALL SYMBOL (X1,Y1,3.0, 'STRAIN (-)', 0.0, 10)
ENDIF
READ (ICCHAR, '(3A4)' ) (ICHA(J),J=1,3)
CALL SYMBOL (X2,Y1,3.0, ICCHA(1), 0.0, 10)
C
YY = Y1-2.0
X1 = X+98.0
X2 = X+57.0
C
CALL PLOT (X , YY, 3)
CALL PLOT (X1,YY, 2)
CALL PLDT (X1,Y , 2)
CALL PLDT (X , Y , 2)
CALL PLDT (X , YY, 2)
CALL PLDT (X2,YY, 3)
CALL PLDT (X2,Y , 2)
ENDIF
ENDIF
ENDIF
C

```

```

        Appendix F (Continued)

Y      = YY- 4.0
X      = XX+10.0
XX3   = X - 4.0
DO 350 J=1,NDATA,30
JJ    = J+29
IF ( JJ.GT.NDATA ) JJ = NDATA
XX1   = XX3+ 4.0
XX2   = XX1+57.0
XX3   = XX2+57.0
X1    = XX1+ 2.0
YT    = Y - 4.25
C
C
DO 230 K=1,2
KVS   = KARG(K)
CSZ   = 2.5
IF ( KVS.EQ.1 ) CSZ = 2.2
CALL SYMBOL (XT,YT,CSZ,IKVSY(1,KVS,KSYSU),0.0,24)
XT    = XT+57.0
230 CONTINUE
C
C
Y2    = Y - 6.0
Y1    = Y2 - 0.5
X1    = XX1+17.5
X2    = XX2+17.5
C
C
DO 310 K=J,JJ
Y1    = Y1-4.0
WRITE(ICHAR,'(1PE10.3)') XDATA(K,1)
READ(ICHAR,'(3A4)',*) (ICHAL(L),L=1,3)
CALL SYMBOL (X1-Y1+2.5,ICHA(1),0.0,10)
WRITE(ICHAR,'(1PE10.3)') YDATA(K,1)
READ(ICHAR,'(3A4)',*) (ICHAL(L),L=1,3)
CALL SYMBOL (X2-Y1+2.5,ICHA(1),0.0,10)
310 CONTINUE
C
C
Y1    = Y1-2.0
CALL PLDT (XX1,Y1,3)
CALL PLDT (XX3,Y1,2)
CALL PLDT (XX3,Y ,2)
CALL PLDT (XX1,Y ,2)
CALL PLDT (XX1,Y1,2)
CALL PLDT (XX2,Y1,3)
CALL PLDT (XX2,Y ,2)
CALL PLDT (XX1,Y2,3)
CALL PLDT (XX3,Y2,2)
350 CONTINUE
C
CALL PLDT (300.,0.,-3)
C (3)
CALL PLDT (0.,0.,777)
CALL PLDT (0.,0.,666)
CALL PLDT (0.,0.,888)
500 CONTINUE
C
RETURN
END

```

```

        Appendix F (Continued)

SUBROUTINE EXGRA(IREFF)
C
INTEGER IREFF(2,1)
C
COMMON /MLBRF3/ ICNDF(8,20), RCNDF(8,20)
COMMON /MLBRF1/ KRFM1, KRFM2, KEXC, MRFM, NRFM, IRFM(10), KARG(4)
1     COMMON /MLBRF1/ KRFM1, KRFM2, KEXC, MRFM, NRFM, IRFM(10), KARG(4)
1     COMMON /MLBRF1/ NRFC(8), IRFC(10,8), RRFC(2,10,8), KSYSU
1     COMMON /COMPL1/ ATITLE(18), XXNAME(10), YYNAME(10)
1     COMMON /COMPL1/ XDATA(50,20), YDATA(50,20)
1     COMMON /COMPL2/ PXMIN, PXMAX, PYMIN, PYMAX, XL1, YL1, NPLOT
1     COMMON /COMPL2/ NDATA, NDATAX(20), NGRAPH
C
CHARACTER*72 CTITL1
CHARACTER*4 ATITLE, XXNAME, YYNAME
CHARACTER*1 CTITL2(72), CBLNK
C
DATA CBLNK '/ ' /
DATA XBOX, YBOX / 300., 210. /
C
C
IF ( NPLOT.LE.0 ) GOTO 900
C* BOX *
C
CALL NEWPEN (1)
XBOXX = XBOX-20.
XBST = -20.
C
CALL PLDT (0.,0.,666)
CALL PLDT (XBST,-5.0,3)
CALL PLDT (XBOXX,-5.0,2)
CALL PLDT (XBOXX,YBOX,2)
CALL PLDT (XBST ,YBOX,2)
CALL PLDT (XBST ,-5.0,2)
CALL PLDT (0.,0.,3)
CALL NEWPEN (1)
C* TITLE *
C
CALL SYMBOL ( 10.0,8.,3.,'FIG. ', '0.,11)
WRITE(CTITL1,'(18A4)') (ATITLE(I),I=1,18)
READ(CTITL1,'(72A1)') (CTITL2(I),I=1,72)
C
C
J    = 73
DO 220 I=2,J
J    = J-1
IF ( CTITL2(J).EQ.CBLNK) GOTO 220
CALL SYMBOL (50.,8.,3.,CTITL2(1),0.,J)
GOTO 300
220 CONTINUE
C
C
300 CONTINUE
X    = 50.0

```

## Appendix F (Continued)

```

Y      = 0.0
I      = 1
CALL SYMBOL (X,Y,3.0,'MATERIAL NAME:',0.0,14)
X1    = X+45.0
CALL SYMBOL (X1,Y,3.0,ICNDP(S,I),0.0,16)

C
C
JRF   = ICNDP(4,I)/100
NRF   = ICNDP(4,I)-100*JRF
C
C
X2   = X+74.0
CALL SYMBOL (X2,Y,3.0,'MATERIAL NO.:',0.0,13)
RI   = ICNDP(1,I)
CALL NUMBER (X2+42.0,Y,3.0,RI,0.0,-1)
C
C
IF ( NRF.LE.0 )      GOTO 160
X2   = X+143.0
CALL SYMBOL (X2,Y,3.0,'REFERENCE NO.:',0.0,14)
C
C
X2   = X+188.0
DO 155 J=1,NRF
CALL SYMBOL (X2,Y,3.0,IREFF(1,JRF),0.0,8)
X2   = X2+20.0
JRF   = JRF+1
155 CONTINUE
160 CONTINUE
C* PLOT CURVES *
C
CALL CURVE
C
C
CALL PLOT  (500.,0.,-3)
C
(3)
CALL PLDT  (0.,0.,777)
CALL PLOT  (0.,0.,666)
CALL PLOT  (0.,0.,888)
C
C
900 RETURN
END

```

## Appendix F (Continued)

```

SUBROUTINE CURVE
*****
PLOTTING PROGRAM
*****
INPUT DATA
  ATITLE (18)  = HEADING (MAX. 72 CHARS.)
  XTITLE (10)  = TITLE OF X-AXIS (MAX. 40 CHARS.)
  YTITLE (10)  = TITLE OF Y-AXIS (MAX. 40 CHARS.)
  IPARM       = PARM. =1 LINEAR, =2 SMOOTHING
  PXMIN,PXMAX = USER DEFINED MIN. AND MAX. VALUE OF X-AXIS
  IF PXMIN>PXMAX=0.0 THEN AUTOMATIC SCALE.
  PYMIN,PYMAX = USER DEFINED MIN. AND MAX. VALUE OF Y-AXIS
  IF PYMIN>PYMAX=0.0 THEN AUTOMATIC SCALE.
  NPLOT        = NUM. OF PLOTTING CURVE/GRAPH (MAX. 20)
  NDATA        = NUM. OF PLOTTING DATA/CURVE (MAX. 1000)
  XDATA (NDATA) = XDATA OF 1-ST CURVE
  YDATA (NDATA) = YDATA OF 1-ST CURVE
  XDATA (NDATA) = XDATA OF 2-ND CURVE
  YDATA (NDATA) = YDATA OF 2-ND CURVE
  END OR IF YOU WANT NEXT GRAPH THEN REPEAT FROM ATITLE DATA.
*****
COMMON /MLBRL1/ KRFM1, KRFM2, KEXC, MRFM, IRFM(10), KARG(4)
1      NRFC(8), IRFC(5,8), RRFC(2,10,8), KSYSU
COMMON /MLBPL1/ IAXES(2), KMESH, KCVNAME, JCNAME(20), JCVNAME(5,20)
CHARACTER*4   ICVNAME
COMMON /COMPL1/ ATITLE(18),XXNAME(10),YYNAME(10),
*                  XDATA(50,20),YDATA(50,20)
CHARACTER*4   ATITLE, XXNAME, YYNAME
COMMON /COMPL2/ PXMIN,PXMAX,PYMIN,PYMAX,XL1,YL1,NPLDT,NDATA
1      NDATAX(20), NGRAFH
COMMON /COMPL3/ AMAT1(20),ANAME(20),UNAME(3)
CHARACTER*8   AMAT1   , ANAME   , UNAME
COMMON /NAL/ NALPH
CHARACTER*2   CNUM1(20)
DATA CNUM1 /' 1',' 2',' 3',' 4',' 5',' 6',' 7',' 8',' 9',' 10',
1      '11','12','13','14','15','16','17','18','19','20'/ 
***** PLOT INITIAL VALUE SET
IPARM=1
C
C...PLOT INITIAL SET
C...PLOT MODE SYMBOL
XX1 = 178.5
YY1 = 182.0
DO 100 I=1,NPLDT
YY2 = YY1 - (I-1)*5.0
FPN1= I*0.005
IF ( I .GE. 10 ) GO TO 90
CALL NUMBER(XX1-2.0,YY2,2.4,FPN1   ,0.0,-1)
GO TO 95
90 CONTINUE
CALL NUMBER(XX1-3.5,YY2,2.4,FPN1   ,0.0,-1)
95 CONTINUE
JCVN= JCVNAME(I)
IF ( JCVN.EQ.0 )      THEN
CALL SYMBOL(XX1+ 5.0,YY2,2.4,ANAME(I),0.0, 8)
CALL SYMBOL(XX1+30.0,YY2,2.4,AMAT1(I),0.0, 8)
ELSE

```

```

Appendix F (Continued)
XX = XX1+5.0
CALL SYMBOL(XX,YY2,2.4,ICVNAM(1,I),0.0,20)
ENDIF
100 CONTINUE
C...SET INSIDE BOX ORIGIN
C
CALL PLOT(35.0,30.0,-3)
CALL PLOT( 0.0, 0.0, 3)
CALL PLOT( 0.0, YL1, 2)
CALL PLOT( XL1, YL1, 2)
CALL PLOT( XL1, 0.0, 2)
CALL PLOT( 0.0, 0.0, 2)
IF ( KMESH.NE.0 ) THEN
IF ( IAXES(2).EQ.0 ) THEN
CALL NEWPEN(1)
XXXL1=XL1
DO 150 I=1,7
YYHEIT= 20.0 * FLDAT(I)
IF ( I.GT.6 ) XXXL1=140.0
CALL PLOT( 0.0, YYHEIT, 3 )
IF ( KMESH.EQ.1 ) THEN
CALL DASHP ( XXXL1, YYHEIT, 1.1 )
ELSE
IF ( KMESH.EQ.2 ) THEN
CALL PLOT ( XXXL1, YYHEIT, 2 )
ENDIF
ENDIF
150 CONTINUE
IF ( IAXES(1).EQ.0 ) THEN
YYYL1=YL1
DO 200 I=1,9
XXWITH= 20.0 * FLOAT(I)
IF ( I.GT.7 ) YYYL1=120.0
CALL PLOT( XXXWITH, 0.0, 3 )
IF ( KMESH.EQ.1 ) THEN
CALL DASHP ( XXXWITH, YYYL1, 1.1 )
ELSE
IF ( KMESH.EQ.2 ) THEN
CALL PLOT ( XXXWITH, YYYL1, 2 )
ENDIF
ENDIF
200 CONTINUE
ENDIF
ENDIF
CALL NEWPEN(1)
VX= XL1
VY= YL1
C...PLOT TITLE
YTPNUM=-20.0
IF( NALPHA.EQ.4 ) YTPNUM=-22.5
IF( NALPHA.EQ.5 ) YTPNUM=-25.0
IF( NALPHA.EQ.6 ) YTPNUM=-27.5
CALL SYMBOL( 60.0,-11.0,3.0,XXNAME,0.,20)
CPLOT10(2)
CALL SYMBOL(YTPNUM,YL1+3.0,YYNAME, 0.,24)
C...MIN.,MAX.
C

```

```

Appendix F (Continued)
DO 450 I=1,NPLOT
IF (NDATA(1) .NE. 1) GOTO 450
NDATA(1) = 2
XDATA(2,I) = XDATA(1,I) * 1.01
YDATA(2,I) = YDATA(1,I)
450 CONTINUE
C
C
IF (PXMIN.NE.0.0 .OR. PXMAX.NE.0.0) GOTO 500
CALL EXMINX(XDATA(1,1), SD-NPLOT,NDATA(1), PXMIN, PXMAX)
500 CONTINUE
IF (PYMIN.NE.0.0 .OR. PYMAX.NE.0.0) GOTO 600
CALL EXMINX(YDATA(1,1), SD-NPLOT,NDATA(1), PYMIN, PYMAX)
C
C...DEFAULT YMINT = 0.0
C
IF (PYMIN.GE.0.0) PYMIN = 0.0
600 CONTINUE
C...PLOT AXIS
C... X-AXIS
C
IF ( IAXES(1).EQ.0 ) THEN
DX1 = (PXMAX-PXMIN)/5.0
CALL AXFUN1(DX1,SDX,ISUFX)
DX = SDX*5.0/VX
PXMAX1 = PXMIN + SDX*5.0
PXMIN1 = PXMIN
CALL PLTAX2(1,VX,PXMIN1,PXMAX1,SDX,ISUFX)
ELSE
IF ( IAXES(1).EQ.1 ) THEN
CALL PLTAXL(1,VX,PXMIN,PXMAX, PXMIN1, PXMAX1)
DX = (PXMAX1-PXMIN1)/VX
CALL PLTGVK( XDATA(1,1) , SD-NPLOT,NDATA(1))
ENDIF
ENDIF
C... Y-AXIS
C
IF ( IAXES(2).EQ.0 ) THEN
IF (PYMIN.GE.0.0) GO TO 650
TYM1 = -PYMIN
DY1 = PYMAX/3.0
IF (DY1.LT.TYM1) CALL AXFUN1(TYM1,SDY,ISUFY)
IF (DY1.GE.TYM1) CALL AXFUN1(DY1,SDY,ISUFY)
PYMAX1 = SDY*3.0
PYMIN1 = -SDY
GO TO 660
650 CONTINUE
DY1 = (PYMAX-PYMIN)/4.0
CALL AXFUN1(DY1,SDY,ISUFY)
PYMAX1 = PYMIN + SDY*4.0
PYMIN1 = PYMIN
660 CONTINUE
DY = SDY*4.0/VY
CALL PLTAX2(2,VY,PYMIN1,PYMAX1,SDY,ISUFY)
ELSE
IF ( IAXES(2).EQ.1 ) THEN
CALL PLTAXL(2,VY,PYMIN,PYMAX, PYMIN1, PYMAX1)
DY = (PYMAX1-PYMIN1)/VY

```

```

Appendix F (Continued)
CALL PLTLGV( YDATA(1,1) , 50,NPLOT,NDATAX(1))
      ENDIF
      ENDIF
C...PLOT CURVE
C
DO 800 I=1,NPLOT
  NDATA = IABS (NDATAX(I))
  IF (NDATA.EQ.0) GO TO 680
  XDATA(NDATA+1,I)=PXMIN1
  XDATA(NDATA+2,I)=DX
  YDATA(NDATA+1,I)=PYMIN1
  YDATA(NDATA+2,I)=DY
  GO TO 690
680 CONTINUE
C...CONSTANT VALUE
C
  XDATA(1,I) = PXMIN1
  XDATA(2,I) = PYMAX1
  XDATA(3,I) = PYMIN1
  XDATA(4,I) = DY
  YDATA(3,I) = PYMIN1
  YDATA(4,I) = DY
  NDATA = 2
690 CONTINUE
C (5)
C
  IF( ( NDATAX(I).GE.0 .AND. KARG(4).GT.0 )
*.OR. ( NDATAX(I).LT.0 .AND. KARG(4).NE.0 )
*.OR.( NDATA .EQ.2 .AND. XDATA(9,I).EQ.-9999. ) )
      THEN
    CALL NEWOPEN(2)
    CALL LINE(XDATA(1,I),YDATA(1,I),NDATA,1,O,1DMY)
    CALL NEWOPEN(1)
    TTMPI=NDATA/6
    TTMP2=TTMPI/NPLOT
    DO 700 KKK=1,NDATA-2
      TX=(XDATA(KKK,I)-XDATA(NDATA+1,I))/XDATA(NDATA+2,I)
      TY=(YDATA(KKK,I)-YDATA(NDATA+1,I))/YDATA(NDATA+2,I)
      CALL SYMBOL(TX,TY,2.0,CNUM1(I),0,2)
700 CONTINUE
C (3)
C
  ELSE
    CALL NEWOPEN(2)
    CALL LINE(XDATA(1,I),YDATA(1,I),NDATA,1,-1,I)
    CALL NEWOPEN(1)
  ENDIF
800 CONTINUE
9000 CONTINUE
C...RESET ORIGIN
C
  CALL PLOT(-35.0,-30.0,-3)
  RETURN
END

```

```

Appendix F (Continued)
SUBROUTINE AXFUN1(DXi,SDX,ISUFX)
*****
C   AXIS FUNCTION (ROUND N*10**ISUFX )
*****
C
  TX = ALOG10(DXi)
  IF (TX.LT.0.0) TX = TX-1.0
  KX1 = IFIX(TX)
  ISUFX = KX1
  SX1 = FLOAT(KX1)
  F = DX1/(10.0**KX1)
C...DX1 = F*10**KX1  ( 1<= F <10 )
C
  IF (F.GT.5.0) GO TO 100
  IF (F.GT.4.0) GO TO 200
  IF (F.GT.3.0) GO TO 300
  IF (F.GT.2.0) GO TO 400
  IF (F.GT.1.0) GO TO 500
C
C
  SDX = 10.0**SX1
  RETURN
C
C
  100 CONTINUE
  SDX = 10.0** (SX1+1.0)
  RETURN
C
C
  200 CONTINUE
  SDX = 5.0*10.0**SX1
  RETURN
C
C
  300 CONTINUE
  SDX = 4.0*10.0**SX1
  RETURN
C
C
  400 CONTINUE
  SDX = 3.0*10.0**SX1
  RETURN
C
C
  500 CONTINUE
  SDX = 2.0*10.0**SX1
  RETURN
END

```

```

Appendix F (Continued)

SUBROUTINE PLTAX2(IXY,ALEN,XMIN,XMAX,SD,ISUF)
C*****PLTAX2.C *****

C   PLOT AXIS   < ORIGIN=(0.0,0.0) >

C   INPUT
C     IXY    = 1 XAXIS / -2 YAXIS
C     ALEN   = LENGTH OF AXIS
C     XMIN   = MIN. OF AXIS
C     XMAX   = MAX. OF AXIS
C     SD     = 
C     ISUF   = 10.0** ISUF

C   COMMON /NAL/ NALPHA
C     IX1 = ISUF
C     KX1 = ISUF
C     KX2 = KX1-2

C
C
C     IF (KX1.EQ.0)  KX2 = KX1
C     IF (KX1.EQ.1)  KX2 = KX1 - 1
C...
C
C     DELX = SD
C     IF (IXY.EQ.2)      GOTO  400
C
C
C     DA = ALEN/5.0
C     DO 100 I=1,20
C       TX=DA*I
C       IF (TX.GE.ALEN)      GOTO  100
C       CALL PLDT(TX,1.0,3)
C       CALL PLDT(TX,-1.0,2)
C 100 CONTINUE

C
C
C     DC 200 I=1,20
C     TX=DA*(I-1)-3.0
C     TY=-5.0
C     IF ( TX .GT.ALEN)  GOTO  200
C     TN=XMIN+ DELX*(I-1)
C     IF (IX1.LE.-2)      TN=TN*10.**(-IX1)
C     CALL NUMBER(TX,TY,3.0,TN,0.0,-1)
C 200 CONTINUE

C
C
C     IF (IX1.GT.-2)      GOTO  300
C     CALL SYMBOL( ALEN +10.,-5.0,3.0,(X10 )',0.0,7)
C     TN=IX1
C     CALL NUMBER( ALEN +10.+12.,-3.0,2.0,TN,0.0,-1)
C
C     CPLOT10(1)

```

```

Appendix F (Continued)

C   300 CONTINUE      GOTO  700
C   400 CONTINUE      GOTO  700
C...PLOT Y-AXIS
C
C     DA = ALEN/4.0
C     DC 500 I=1,20
C     TY=DA*I
C     IF (TY.GE.ALEN)      GOTO  500
C     CALL PLDT(-1.0,TY,3)
C     CALL PLDT( 1.0,TY,2)
C 500 CONTINUE

C
C
C     MNUM=NALPHA
C     IF(NALPHA.EQ.0) MNUM=2
C     YPNUMB=-15.0
C     IF(NALPHA.EQ.3) YPNUMB=-17.0
C     IF(NALPHA.EQ.4) YPNUMB=-19.5
C     IF(NALPHA.EQ.5) YPNUMB=-22.5
C     IF(NALPHA.EQ.6) YPNUMB=-25.0

C
C
C     DO 600 I=1,20
C       TX=-12.0
C       TY=DA*(I-1)-1.0
C       IF (TY .GT.ALEN)  GOTO  600
C       TN=XMIN+ DELX*(I-1)
C       TN = TN*10.0 **(-KX2)
C       CALL NUMBER(TX,TY,3.0,TN,0.0,-1)
C     GOTO 600
C 550 CONTINUE

C...PLOT X.XX
C
C     CALL NUMBER(YPNUMB, TY,3.0,TN,0.0,MNUM )
C 600 CONTINUE
C     IF (KX2.EQ. 0)      GOTO  700
C     CALL SYMBOL(-20.0, ALEN +3.0,3.0,(X10 )',0.0,7)
C     TN=KX2
C     CALL NUMBER( -8.0, ALEN +5.0,2.0,TN,0.0,-1)
C
C     CPLOT10(1)
C
C   700 CONTINUE
C     WRITE(50,6010) IXY,ALEN,XMIN,XMAX
C     WRITE(50,6020) IX1,DELX,DA,KX1,KX2
C 6010 FORMAT('0',' *** PLTAX CHECK LIST *** ')
C 6010 FORMAT(' ',IXY=12,3X,'ALEN=',F10.3,3X,'MIN=',E12.4,
C           1      3X,'MAX=',E12.4)
C 6020 FORMAT(' ',          3X,'IX1=',15,3X,'DELX=',
C           1      E12.4,3X,'DA=',E12.4, ' KX1=',15,' KX2=',15 )
C
C     RETURN
C
C     END

```

```

Appendix F (Continued)
SUBROUTINE PLTAXL (XXY,AXLEN,XMIN,XMAX, XMIN1, XMAX1)
C
COMMON /COMPL2/ PXMIN, PXMAX, PYMIN, PYMAX, XL1, YL1, NPLOT
1      NDATA, WDATA(20), NGRAPH
COMMON /MLBPL1/ IAKES(2), KMESH, KCVNAM(20), ICVNAM(5,20)
CHARACTER*4 ICVNAM
C
      DATA XXL1, YYL1 / 140., 120. /
      DATA EPS0 / 1.E-50 /
C*
      LA
      IF ( XMIN.GE.1.0 )      THEN
      LA = ALOG10 (XMIN)      ELSE
      IF ( XMIN.LE.EPS0 )      THEN
      LA = 0                   ELSE
      LA = ALOG10 (1.0/XMIN)
      LA = -(LA+1)
      ENDIF
      ENDIF
C*
      LB
      IF ( XMAX.GE.1.0 )      THEN
      LB = ALOG10 (XMAX)
      D = 10.*#LB
      D = XMAX-D
      IF ( D.GT.EPS0 ) LB = LB + 1      ELSE
      LB = ALOG10 (1.0/XMAX)
      LB = -LB
      ENDIF
      ENDIF
C
      XMIN1 = LA
      XMAX1 = LB
      XD = XMAX1-XMIN1
      IF ( XD.LE.EPS0 ) GOTO 900
      XD = AXLEN/XD
      L = LA-1
      N = LB-L
      C
      GOTO ( 100,200 ), XXY
C*
      X AXIS
100   Y = YL1
      DO 140 I=1,N
      L = L+1
      X = L
      X10 = 10.*#L
      XN = (X-XMIN1)*XD
      CALL PLOT ( XN, 1.0, 3 )
      CALL PLOT ( XN, 1.0, 2 )
      CALL SYMBOL ( XN-4.5,-5.5,3.0,*10*,0., 2 )
      CPLOT10(1)
      CALL NUMBER ( XN, -3.5,2.0,X , 0.,-1 )
C
      IF ( I.EQ.1 .OR. I.EQ.N ) GOTO 110
      IF ( KMESH.NE.0 )      THEN
      IF ( XN.GT.XXL1 ) Y = YYL1
      CALL PLOT ( XN,Y,3 )
      IF ( KMESH.EQ.1 ) CALL DASHP ( XN, 0.0, 1.1 )
      IF ( KMESH.EQ.2 ) CALL PLOT ( XN, 0.0, 2 )
      ENDIF
      ENDIF
110   IF ( I.GE.N )      THEN
      GOTO 140
      DO 120 J=2,9
      XJ = J*X10
      XX = (ALOG10 (XJ) -XMIN1)*XD
      CALL PLOT ( XX,1.0,3 )
      CALL PLOT ( XX,0.0,2 )
      120 CONTINUE
      140 CONTINUE
C*
      IF ( KMESH.NE.0 )      THEN
      CALL PLOT ( XXL1,YL1,3 )
      IF ( KMESH.EQ.1 ) CALL DASHP ( XXL1, YYL1, 1.1 )
      IF ( KMESH.EQ.2 ) CALL PLOT ( XXL1, YYL1, 2 )
      ENDIF
      GOTO 900
C*
      Y AXIS
200   X = XL1
      DO 240 I=1,N
      L = L+1
      Y = L
      Y10 = 10.*#L
      LA = IAABS (L)
      AA = LA
      NA = ALOG10 (AA+0.1) +1.
      IF ( L.LT.0 ) NA = NA + 1
      C
      XN = -NA+2.0-8.5
      YN = (-XMIN1)*XD
      CALL PLOT ( 1.0,YN,3 )
      CALL PLOT ( -1.0,YN,2 )
      CALL SYMBOL ( XN ,YN-2.0,3.0,*10*,0., 2 )
      CPLOT10(1)
      CALL NUMBER ( XN+4.5,YN , 2.0,Y , 0.,-1 )
C
      IF ( I.EQ.1 .OR. I.EQ.N ) GOTO 210
      IF ( KMESH.NE.0 )      THEN
      IF ( YN.GT.YYL1 ) X = XXL1
      CALL PLOT ( X,YY,3 )
      IF ( KMESH.EQ.1 ) CALL DASHP ( 0.0, YN, 1.1 )
      IF ( KMESH.EQ.2 ) CALL PLOT ( 0.0, YN, 2 )
      ENDIF
      210 IF ( I.GE.N )      GOTO 240
      DO 220 J=2,9
      YJ = J*Y10
      YY = (ALOG10 (YJ) -XMIN1)*XD
      CALL PLOT ( 1.0,YY,3 )
      CALL PLOT ( 0.0,YY,2 )
      220 CONTINUE
      240 CONTINUE
C*
      IF ( KMESH.NE.0 )      THEN
      CALL PLOT ( XXL1,YYL1,3 )
      IF ( KMESH.EQ.1 ) CALL DASHP ( XXL1, YYL1, 1.1 )
      IF ( KMESH.EQ.2 ) CALL PLOT ( XXL1, YYL1, 2 )
      ENDIF
      900 RETURN
      END

```

## Appendix F (Continued)

```

SUBROUTINE PLTBV( PDATA ,MPD,NPLOT,NDATAP)
DIMENSION PDATA(MPD,1), NDATAP(1)
IF ( NPLOT.LE.0 ) GOTO 900
DO 200 I=1,NPLOT
NDATA = IABS (NDATAP(I))
IF ( NDATA.EQ.0 ) NDATA = 2
DO 150 J=1,NDATA
IF ( PDATA(J,I).LE.0. ) THEN
PDATA(J,I)= 0.
      ELSE
PDATA(J,I)= ALOG10 (PDATA(J,I))
      ENDIF
150 CONTINUE
200 CONTINUE
900 RETURN
END

SUBROUTINE DTLIST(LU1,LU2)
DIMENSION IA(20)
REWIND LU1
N = 1
L = 51
15 IF ( L .LE. 50 ) GO TO 30
20 WRITE(LU2,2)
WRITE(LU2,3) ( 1, I=1,8 )
WRITE(LU2,4)
L = 1
30 READ(LU1,1,END=50) ( IA(I),I=1,20 )
WRITE(LU2,5) ( N,(IA(I),I=1,20),N
IF ( L .NE. 50 ) GO TO 40
WRITE(LU2,6)
WRITE(LU2,10) ( 1, I=1,8 )
WRITE(LU2,7)
40 L = L + 1
N = N + 1
GO TO 15
50 CONTINUE
WRITE(LU2,6)
WRITE(LU2,10) ( 1, I=1,8 )
WRITE(LU2,8)
WRITE(LU2,9) LU1
REWIND LU1
1 FORMAT( 20A4 )
2 FORMAT( 1H1, //, 50X, ' INPUT DATA ECHO ' // )
3 FORMAT( 16X, 'DATA ', 4X, B'0X, 11' )
4 FORMAT( 14X, 'SEQ. NO.', 3X, 8('-----0'), / )
5 FORMAT( 16X, 14, 5X, 20A4, 2X, 14 )
6 FORMAT( 1H0, 24X, B'-----0' )
7 FORMAT( 1H0, 30X, ' * * * CONTINUE * * *' )
8 FORMAT( 1H0, 30X, ' * * * INPUT DATA END * * *' )
9 FORMAT( 1H0,30X,' * * * INPUT DATA FROM FILE NO. =',13,' * * *' )
10 FORMAT( 25X, 8(9X,11) )
11 FORMAT( 1H0)
RETURN
END

```

## Appendix G Data Library

DATA SEQ. NO.	1	2	3	4	5	6	7	8
1	MAT 'AISC1020'	1001	0	0	0	1		
2	0.	0.	0.					
3	REF 1 'R-7'							
4	SSR 293.,C,,1							
5	+1.E-2,10,0.01 223.,0.02 379.,0.05 611.,0.11 717.,0.16 767.,							
6	0.22 794.,0.29 840.,0.36 841.,0.51 836.,0.69 857.0							
7	*							
8	MAT 'S45C'	1002	0	0	0	1		
9	0.	0.	0.					
10	REF 2 'R-24','R-25'							
11	SSR 293.,T,,3							
12	6.3E-4, 9.0.003 374., 0.009 349., 0.03 525., 0.049 610.,							
13	0.095 711., 0.14 757., 0.18 784., 0.22 780.,							
14	0.26 724.							
15	4.2E+2,10,0.0061 591., 0.0096 900., 0.0156 659., 0.03 795.,							
16	0.049 861., 0.095 938., 0.14 955., 0.18 946.,							
17	0.22 903., 0.25 818.							
18	1.5E+3,10,0.0061 591.,0.0115 1100.,0.0185 726.,0.030 808.,							
19	0.049 884., 0.095 971., 0.14 1002., 0.18 990.,							
20	0.22 946., 0.26 815.							
21	*							
22	MAT 'STEEL'	1003	0	0	0	2		
23	0.	0.	0.					
24	REF 1 'R-36'							
25	COM 'C 0.14, SI 0.20, MN 0.49, P 0.008, S 0.013, NI 0.04 '							
26	SSR 293.,C,,5							
27	2.0E-4, 4.0.002 181., 0.1 430., 0.2 526., 0.3 593.							
28	5.0E-3,14,0.002 181., 0.02 228., 0.04 291., 0.06 341., 0.08 389.,							
29	0.10 427., 0.12 456., 0.14 481., 0.16 500., 0.18 515.,							
30	0.20 529., 0.25 558., 0.30 573., 0.35 583.							
31	3.0E-1,14,0.002 241., 0.02 286., 0.04 336., 0.06 385., 0.08 425.,							
32	0.10 458., 0.12 483., 0.14 506., 0.16 529., 0.18 545.,							
33	0.20 563., 0.25 593., 0.30 612., 0.35 625.							
34	4.3 , 4.0.002 310., 0.1 432., 0.20 570., 0.3 634.							
35	3.7E+2,14,0.002 431., 0.02 448., 0.04 469., 0.06 498., 0.08 507.,							
36	0.10 525., 0.12 544., 0.14 555., 0.16 572., 0.18 586.,							
37	0.20 599., 0.25 627., 0.30 647., 0.35 666.							
38	SSR 293.,T,,5							
39	1.0E-3, 3.0.002 228., 0.1 409., 0.2 499.							
40	1.2E-2,11,0.002 228., 0.02 261., 0.04 317., 0.06 354., 0.08 389.,							
41	0.10 412., 0.12 436., 0.14 456., 0.16 473., 0.18 492.,							
42	0.20 500.							
43	1.0E-1,11,0.002 232., 0.02 299., 0.04 350., 0.06 385., 0.08 419.,							
44	0.10 444., 0.12 466., 0.14 483., 0.16 498., 0.18 509.,							
45	0.20 522.							
46	1.2 , 3.0.002 294., 0.1 499., 0.2 537.							
47	1.1E+2,10,0.002 414., 0.02 448., 0.04 466., 0.06 483., 0.08 498.,							
48	0.10 515., 0.12 530., 0.14 541., 0.16 551., 0.18 555.							
49	*							
50	MAT 'STEEL'	1004	0	0	0	3		
	-----	1	2	3	4	5	6	7

## Appendix G (Continued)

DATA SEQ. NO.	1	2	3	4	5	6	7	8
51	0.	0.	0.	0.				
52	REF 1 'R-36'							
53	COM 'C 0.14, SI 0.20, MN 0.49, P 0.008, S 0.013, NI 0.04'							
54	SSR 373.,T,,3							
55	1.0E-3, 1.0.002 196.							
56	1.2 , 1.0.002 273.							
57	1.1E+2, 1.0.002 342.							
58	SSR 473.,T,,5							
59	1.0E-3, 1.0.002 206.							
60	1.2E-2, 1.0.002 195.							
61	1.0E-1, 1.0.002 185.							
62	1.2 , 1.0.002 226.							
63	1.1E+2, 1.0.002 294.							
64	SSR2 195.,C,,3,5							
65	0.002, 0.05, 0.10, 0.15, 0.20							
66	5.0E-3, 5, 238. 373. 481. 537. 578.							
67	3.0E-1, 5, 327. 425. 502. 556. 595.							
68	3.7E+2, 5, 521. 555. 591. 621. 647.							
69	*							
70	MAT 'STEEL'	1005	0	0	0	3		
71	0.	0.	0.	0.				
72	REF 1 'R-52'							
73	COM 'C 0.32, SI 0.24, MN 0.62, S 0.037, P 0.025 : PRESSURE TEST MACHINE'							
74	SSR 189.,C,,1							
75	1.0E-6, 6.0.002 344., 0.015 388., 0.02 430., 0.025 467.,							
76	0.03 499., 0.035 528.							
77	SSR 232.,C,,1							
78	1.0E-6, 7.0.002 310., 0.01 328., 0.015 360., 0.02 396.,							
79	0.025 433., 0.03 460., 0.035 486.							
80	SSR 288.,C,,1							
81	1.0E-6, 7.0.002 276., 0.01 298., 0.015 335., 0.02 367.,							
82	0.025 399., 0.03 428., 0.035 452.							
83	*							
84	MAT 'STEEL'	1006	0	0	0	3		
85	0.	0.	0.	0.				
86	REF 1 'R-52'							
87	COM 'C 0.32, SI 0.24, MN 0.62, S 0.037, P 0.025 : FALL'							
88	SSR 189.,C,,2							
89	260. , 1.0.002 827.							
90	350. , 1.0.002 827.							
91	SSR 232.,C,,3							
92	260. , 1.0.002 717.							
93	360. , 1.0.002 723.							
94	470. , 1.0.002 737.							
95	SSR 288.,C,,3							
96	440. , 1.0.002 634.							
97	570. , 1.0.002 641.							
98	670. , 1.0.002 648.							
99	*							
100	MAT 'STEEL'	1007	0	0	0	3		
	-----	1	2	3	4	5	6	7

## Appendix G (Continued)

DATA SEQ. NO.	1	2	3	4	5	6	7	8	
101	0.	0.	0.	0.					
102	REF 1	'R-53'							
103	COM 'C 0.24, S1 0.07, MN 0.72, S 0.02, P 0.03, MO 0.016'								
104	SSR 293.,C,,7								
105	1.0E-4, 8./0.002 256., 0.002 244., 0.01 249., 0.02 305., 0.03 350.,								
106	0.04 385., 0.05 412., 0.06 437.								
107	135., 1./0.002 695.								
108	455., 1./0.03 553.								
109	474., 1./0.04 580.								
110	683., 1./0.02 545.								
111	860., 1./0.01 552.								
112	944., 1./0.0111 540.								
113	*								
114	MAT 'STEEL' 100B,0,0,0,0,1								
115	0. 0. 0. 0.								
116	REF 1	'R-55'							
117	COM 'C 0.19, MN 0.6, P 0.013, S 0.017'								
118	SSR 293.,C,,4								
119	3.8E-4, 6./0.002 224., 0.02 251., 0.04 324., 0.08 415., 0.12 465.,								
120	0.16 503.								
121	1.5E-2, 4./0.002 243., 0.04 339., 0.08 430., 0.12 483.								
122	4.3E-1, 4./0.002 308., 0.04 383., 0.08 481., 0.12 542.								
123	3.8E+2, 6./0.002 518., 0.02 520., 0.04 574., 0.08 624., 0.12 662.,								
124	0.16 683.								
125	*								
126	MAT 'STEEL' 1009,0,0,0,0,1								
127	0. 0. 0. 0.								
128	REF 1	'R-56'							
129	COM 'C 0.20, MN 0.73, P 0.020, S 0.018'								
130	SSR2 293.,C,,2,7								
131	0.01, 0.02, 0.03, 0.04, 0.05, 0.06, 0.07, 0.08, 0.09, 0.10,								
132	1.0E-4, 7./203. 260. 318. 351. 379. 405. 424.								
133	90., 7./494. 465. 481. 507. 539. 561. 576.								
134	*								
135	MAT 'SS41' 1010,0,0,0,0,5								
136	0. 0. 0. 0.								
137	REF 1	'R-86'							
138	COM 'KANAZAWA UNIVERSITY TEST DATA'								
139	SSR2 293.,C,,10,20								
140	0.01, 0.02, 0.03, 0.04, 0.05, 0.06, 0.07, 0.08, 0.09, 0.10,								
141	0.11, 0.12, 0.13, 0.14, 0.15, 0.16, 0.17, 0.18, 0.19, 0.20								
142	2.0E-4, 20, 259. 276. 318. 350. 376. 395. 415. 430. 447. 456.								
143	467. 478. 489. 498. 508. 512. 522. 527. 531. 539.								
144	2.0E-3, 20, 270. 278. 319. 353. 378. 402. 424. 439. 459. 470.								
145	481. 493. 505. 511. 525. 532. 539. 543. 547. 557.								
146	2.0E-2, 20, 298. 295. 321. 360. 392. 413. 431. 453. 468. 480.								
147	493. 504. 514. 525. 534. 542. 550. 559. 566. 570.								
148	2.0E-1, 20, 319. 312. 330. 368. 400. 424. 450. 467. 481. 496.								
149	510. 521. 531. 542. 550. 561. 567. 575. 580. 586.								
150	1.1 ,20, 366. 343. 343. 371. 398. 421. 443. 464. 484. 500.								
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## Appendix G (Continued)

DATA SEQ. NO.	1	2	3	4	5	6	7	8	
151	512. 527. 536. 545. 553. 561. 567. 574. 578. 585.								
152	1.4 ,20, 392. 352. 356. 386. 416. 446. 470. 489. 506. 525.								
153	546. 553. 567. 576. 585. 591. 600. 602. 608. 609.								
154	15. ,12, 465. 444. 416. 427. 444. 465. 487. 509. 520. 526.								
155	537. 541.								
156	280. ,15, 459. 455. 474. 493. 519. 535. 551. 566. 576. 600.								
157	610. 628. 637. 639. 640.								
158	420. ,13, 488. 471. 494. 513. 536. 556. 574. 587. 603. 613.								
159	622. 632. 631.								
160	500. ,20, 470. 479. 497. 522. 542. 562. 573. 588. 600. 612.								
161	623. 632. 640. 648. 664. 676. 676. 712. 720. 727.								
162	SSR2 473.,C,,4,20								
163	0.01, 0.02, 0.03, 0.04, 0.05, 0.06, 0.07, 0.08, 0.09, 0.10,								
164	0.11, 0.12, 0.13, 0.14, 0.15, 0.16, 0.17, 0.18, 0.19, 0.20								
165	2.1E-4, 13, 242. 296. 354. 390. 410. 435. 451. 471. 491. 504.								
166	515. 528. 537.								
167	4.2E-2, 16, 251. 262. 292. 325. 345. 360. 379. 390. 400. 412.								
168	421. 431. 434. 440. 446. 448.								
169	0.63 ,20, 261. 281. 314. 339. 364. 381. 397. 410. 422. 434.								
170	443. 449. 456. 465. 472. 480. 483. 491. 500. 500.								
171	400. ,12, 368. 381. 413. 439. 465. 484. 502. 522. 538. 555.								
172	565. 579.								
173	SSR2 373.,C,,4,14								
174	0.01, 0.02, 0.03, 0.04, 0.05, 0.06, 0.07, 0.08, 0.09, 0.10,								
175	0.11, 0.12, 0.13, 0.14								
176	2.1E-4, 13, 268. 299. 339. 364. 390. 408. 424. 438. 453. 462.								
177	473. 483. 490.								
178	4.2E-2, 14, 272. 286. 324. 357. 381. 402. 417. 431. 445. 457.								
179	462. 474. 483. 495.								
180	0.63 ,13, 297. 368. 415. 446. 470. 492. 511. 522. 531. 547.								
181	556. 567. 569.								
182	370. ,11, 409. 422. 437. 467. 488. 507. 526. 543. 562. 568.								
183	576.								
184	SSR2 273.,C,,4,15								
185	0.01, 0.02, 0.03, 0.04, 0.05, 0.06, 0.07, 0.08, 0.09, 0.10,								
186	0.11, 0.12, 0.13, 0.14, 0.15								
187	2.1E-4, 14, 242. 259. 295. 328. 348. 371. 391. 404. 418. 427.								
188	440. 445. 456. 459.								
189	4.2E-2, 13, 311. 315. 350. 382. 423. 441. 468. 484. 500. 519.								
190	527. 547. 555.								
191	0.63 ,15, 305. 298. 322. 355. 382. 399. 426. 441. 457. 471.								
192	484. 493. 499. 509. 509.								
193	300. ,15, 487. 484. 509. 528. 546. 568. 583. 595. 600. 639.								
194	649. 659. 664. 677. 678.								
195	SSR2 223.,C,,4,17								
196	0.01, 0.02, 0.03, 0.04, 0.05, 0.06, 0.07, 0.08, 0.09, 0.10,								
197	0.11, 0.12, 0.13, 0.14, 0.15, 0.16, 0.17								
198	2.0E-4, 15, 267. 276. 316. 351. 383. 405. 423. 441. 454. 468.								
199	485. 493. 506. 521. 536.								
200	4.1E-2, 14, 303. 304. 341. 375. 404. 431. 459. 469. 488. 507.								
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## Appendix G (Continued)

DATA SEQ. NO.	1	2	3	4	5	6	7	B
201	519.	530.	543.	565.				
202	0.61	,17.	338.	337.	343.	371.	397.	427.
203			508.	519.	539.	548.	563.	571.
204			230.	,14.	624.	595.	595.	604.
205					629.	649.	664.	705.
206					732.	741.	748.	749.
207	MAT 'S35C'							
208	0.	0.	0.	0.				
209	REF 1 'R-86'							
210	COM 'KANAZAWA UNIVERSITY TEST DATA'							
211	SSR2 293.,C.,10,20							
212	0.01,0.02,0.03,0.04,0.05,0.06,0.07,0.08,0.09,0.10,							
213	0.11,0.12,0.13,0.14,0.15,0.16,0.17,0.18,0.19,0.20,							
214	2.1E-4,20,	388.	347.	408.	451.	485.	514.	537.
215	600.	609.	623.	633.	640.	649.	657.	662.
216	662.	672.	676.	682.	691.	696.	699.	699.
217	706.	710.	720.	734.	741.	746.	750.	750.
218	754.	760.	764.	768.	772.	776.	780.	780.
219	784.	788.	792.	796.	799.	803.	807.	807.
220	811.	813.	817.	821.	825.	829.	833.	833.
221	837.	841.	845.	849.	853.	857.	861.	861.
222	865.	869.	870.	879.	890.	897.	903.	903.
223	917.	918.	923.	928.	934.	938.	943.	943.
224	947.	951.	955.	959.	963.	967.	971.	971.
225	975.	979.	983.	987.	991.	995.	999.	999.
226	1.3.	,20.	435.	412.	445.	496.	537.	571.
227	604.	619.	691.	700.	709.	715.	722.	728.
228	730.	734.	741.	777.	791.	792.	796.	796.
229	800.	,15.	554.	562.	581.	618.	646.	670.
230	670.	680.	691.	700.	709.	715.	722.	730.
231	733.	745.	761.	777.	791.	792.	796.	796.
232	800.	,20.	539.	552.	598.	630.	657.	683.
233	683.	696.	700.	709.	715.	721.	735.	752.
234	760.	771.	784.	785.	823.	841.	843.	858.
235	869.	870.	879.	890.	899.	903.	907.	920.
236	MAT 'S45C'							
237	0.	0.	0.	0.				
238	REF 1 'R-86'							
239	COM 'KANAZAWA UNIVERSITY TEST DATA'							
240	SSR2 293.,C.,10,20							
241	0.01,0.02,0.03,0.04,0.05,0.06,0.07,0.08,0.09,0.10,							
242	0.11,0.12,0.13,0.14,0.15,0.16,0.17,0.18,0.19,0.20,							
243	2.1E-4,20,	353.	402.	461.	505.	539.	564.	588.
244	608.	622.	676.	682.	691.	696.	706.	715.
245	725.	730.	736.	741.	746.	750.	755.	760.
246	760.	764.	770.	775.	780.	785.	790.	795.
247	794.	798.	802.	806.	810.	814.	818.	823.
248	828.	837.	853.	882.	892.	902.	907.	911.
249	911.	921.						
250	0.99	,15.	461.	441.	490.	539.	578.	608.
251	637.	637.	637.	637.	637.	637.	637.	637.
252	637.	637.	637.	637.	637.	637.	637.	637.
253	637.	637.	637.	637.	637.	637.	637.	637.
254	637.	637.	637.	637.	637.	637.	637.	637.
255	637.	637.	637.	637.	637.	637.	637.	637.
256	637.	637.	637.	637.	637.	637.	637.	637.
257	637.	637.	637.	637.	637.	637.	637.	637.
258	637.	637.	637.	637.	637.	637.	637.	637.
259	637.	637.	637.	637.	637.	637.	637.	637.
260	637.	637.	637.	637.	637.	637.	637.	637.
261	SSR2 473.,C.,4,15							
262	0.01,0.02,0.03,0.04,0.05,0.06,0.07,0.08,0.09,0.10,							
263	0.11,0.12,0.13,0.14,0.15,							
264	2.1E-4,11,	304.	392.	446.	485.	519.	549.	568.
265	598.	617.						
266	4.1E-2,12,	314.	372.	421.	461.	495.	519.	534.
267	549.	597.						
268	0.62	,15.	343.	392.	441.	480.	510.	529.
269	549.	568.	608.	637.	676.	711.	735.	760.
270	779.	798.	813.	828.	837.	853.	882.	902.
271	907.	911.	921.					
272	SSR2 373.,C.,4,14							
273	0.01,0.02,0.03,0.04,0.05,0.06,0.07,0.08,0.09,0.10,							
274	0.11,0.12,0.13,0.14,							
275	2.1E-4,13,	343.	392.	441.	480.	515.	539.	559.
276	573.	593.						
277	603.	613.	627.	632.				
278	632.	642.	652.	662.				
279	672.	682.	692.	702.				
280	712.	722.	732.	742.				
281	752.	762.	772.	782.				
282	SSR2 273.,C.,4,15							
283	0.01,0.02,0.03,0.04,0.05,0.06,0.07,0.08,0.09,0.10,							
284	0.11,0.12,0.13,0.14,0.15,							
285	2.1E-4,12,	343.	363.	417.	480.	505.	529.	554.
286	568.	587.						
287	4.2E-2,14,	402.	397.	470.	524.	563.	598.	627.
288	652.	676.	725.	740.	750.	774.	790.	816.
289	833.	843.	847.	857.				
290	853.	868.	872.	882.				
291	892.	902.	907.	911.				
292	SSR2 223.,C.,4,16							
293	0.01,0.02,0.03,0.04,0.05,0.06,0.07,0.08,0.09,0.10,							
294	0.11,0.12,0.13,0.14,0.15,0.16,							
295	2.2E-4,14,	343.	392.	451.	490.	529.	559.	578.
296	603.	637.	657.	666.	671.			
297	681.	701.	711.	725.	735.	740.		
298	749.	761.	771.	781.	791.	801.		
299	811.	810.	755.	760.	764.	774.	784.	
300	833.	835.	838.	841.	843.	846.	854.	

1	2	3	4	5	6	7	B
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## Appendix G (Continued)

DATA SEQ. NO.	1	2	3	4	5	6	7	8
301	*							
302	MAT 'SSSC'	1013.	0.	0.	0.			
303	0.	0.	0.	0.				
304	REF 1 'R-86'							
305	CDM 'KANAZAWA UNIVERSITY TEST DATA'							
306	SSR2 293.,C,,10,20							
307	0.01,0.02,0.03,0.04,0.05,0.06,0.07,0.08,0.09,0.10,							
308	0.11,0.12,0.13,0.14,0.15,0.16,0.17,0.18,0.19,0.20,							
309	2.0E-4,18,372,470,539,593,637,671,696,715,730,745,							
310	755,769,784,794,804,809,818,823,							
311	2.0E-3,18,373,471,544,603,647,676,706,725,740,755,							
312	770,779,794,804,813,823,828,833,							
313	2.0E-2,20,358,436,524,588,642,676,711,730,750,769,							
314	789,799,809,818,828,838,848,853,862,862,							
315	2.0E-1,20,402,446,529,598,652,696,720,750,769,784,							
316	799,813,823,833,848,853,862,872,877,882,							
317	0.99,-13,470,490,559,613,662,706,725,750,774,789,							
318	804,813,823,							
319	1.3,-17,490,480,568,647,696,735,764,794,813,823,							
320	843,862,872,877,882,882,887,							
321	10.5,-9,510,558,627,686,725,764,784,794,794,							
322	140,-9,627,637,686,740,774,794,809,818,818,							
323	260,-12,637,647,686,735,774,804,828,858,867,877,							
324	887,892,							
325	350,-18,696,676,725,774,813,833,858,887,907,921,							
326	941,960,970,985,990,1000,1005,1010							
327	*							
328	MAT 'STEEL'	1100,6,6,0,0,0,0						
329	12.1E-6, 211400., 81600., 0.293							
330	12.1E-6, 293., 12.1E-6, 373., 12.9E-6, 473., 13.8E-6, 673.,							
331	14.5E-6, 873., 14.6E-6, 1073.							
332	192000., 294.1, 191000., 366.3, 186000., 477.4, 178000., 588.6,							
333	162000., 699.7, 106000., 810.8							
334	*							
335	MAT 'SUS302'	2001,0,0,0,0,3						
336	0. 0. 0. 0.							
337	REF 1 'R-1'							
338	SSR 273.,C,,3							
339	4.0E-1, 1.0,69 513,							
340	2.0E+1, 1.0,69 555,							
341	2.0E+2, 1.0,69 596,							
342	SSR 473.,C,,3							
343	4.0E-1, 1.0,69 345,							
344	7.0,-, 1.0,69 353,							
345	6.0E+1, 1.0,69 373,							
346	SSR 673.,C,,6							
347	4.0E-1, 1.0,69 237,							
348	1.6,-, 1.0,69 245,							
349	7.0,-, 1.0,69 256,							
350	2.0E+1, 1.0,69 266,							
351	*							
352	6.0E+1, 1.0,69 290,							
353	2.0E+2, 1.0,69 309,							
354	*							
355	MAT 'SUS303'	2002,0,0,0,1						
356	0. 0. 0. 0.							
357	REF 1 'R-1'							
358	SSR 273.0,T,,9							
359	1.2E+2, 4, 0.41 1047., 0.44 1198., 0.45 1156., 0.46 1283.							
360	2.6E+2, 1, 0.46 1129.							
361	2.7E+2, 2, 0.43 1105., 0.44 1145.							
362	4.5E+2, 1, 0.47 1240.							
363	4.6E+2, 1, 0.45 1156.							
364	4.7E+2, 1, 0.44 1190.							
365	6.8E+2, 1, 0.47 1165.							
366	6.9E+2, 1, 0.44 1191.							
367	9.1E+2, 2, 0.45 1292., 0.46 1210.							
368	*							
369	MAT 'SUS304'	2003,0,0,0,0,10						
370	0. 0. 0. 0.							
371	REF 1 'R-1'							
372	SSR 294.,C,,B,3							
373	0.01, 0.02, 0.04							
374	1.0E-4, 3, 255, 293, 359,							
375	1.0E-1, 3, 307, 348, 414,							
376	1.0,-, 3, 331, 372, 434,							
377	1.0E+1, 3, 365, 410, 472,							
378	1.0E+2, 3, 403, 452, 510,							
379	398.1, 3, 441, 483, 538,							
380	630.96, 3, 441, 483, 538,							
381	1.0E+3, 3, 441, 483, 538,							
382	SSR 294.,T,,3							
383	4.0E-5, 3, 0.54 994., 0.57 956., 0.62 1000.							
384	4.15E-5, 4, 0.57 1032., 0.59 1037., 0.60 1033., 0.62 1022.							
385	4.0E-4, 1, 0.50 860.							
386	SSR 366.,T,,2							
387	4.2E-5, 1, 0.47 747.							
388	4.5E-4, 1, 0.47 706.							
389	SSR 373.,T,,2							
390	4.2E-5, 1, 0.47 747.							
391	4.5E-4, 1, 0.47 706.							
392	SSR 473.,T,,2							
393	4.8E-5, 1, 0.34 590.							
394	5.0E-4, 1, 0.38 583.							
395	SSR 477.,T,,2							
396	4.8E-5, 1, 0.34 590.							
397	5.0E-4, 1, 0.38 583.							
398	SSR 533.,T,,3							
399	4.7E-5, 2, 0.36 555., 0.39 604.							
400	4.6E-4, 1, 0.39 581.							
401	4.6E-3, 1, 0.38 565.							
402	*							

1	2	3	4	5	6	7	8
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## Appendix G (Continued)

DATA SEQ. NO.	1	2	3	4	5	6	7	8
401	SSR 589.,T,,1							
402	5.9E-5, 1, 0.33	606.						
403	4.7E-5, 1,	0.35	614.					
404	SSR 623.,T,,1							
405	4.7E-4, 1,	0.36	661.					
406	SSR 700.,T,,5							
407	6.0E-5, 1,	0.32	590.					
408	4.8E-5, 1,	0.33	595.					
409	4.6E-5, 1,	0.38	605.					
410	4.6E-4, 1,	0.38	574.					
411	4.6E-3, 1,	0.38	560.					
412	*							
413	MAT 'SUS316H'	2004,0,0,0,0,2						
414	0. 0. 0. 0.							
415	REF 1 'R-1'							
416	SSR 295.,T,,1							
417	2.0E-5, 4,	0.35	860., 0.37	912., 0.39	923., 0.40	918.		
418	SSR 371.,T,,1							
419	2.0E-5, 1,	0.34	767.					
420	*							
421	MAT 'SUS304'	2005,0,0,0,0,1						
422	0. 0. 0. 0.							
423	REF 1 'R-45'							
424	COM 'C 0.05, SI 0.48, MN 1.83, P 0.040, S 0.006, NI 9.10, CR 18.40'							
425	SSR 300.,L,,1							
426	5.5E+3, 6,	0.018	456., 0.030	519., 0.047	580., 0.069	631.,		
427	0.086 673., 0.108	722.						
428	*							
429	MAT 'AISI1316L'	2006,0,0,0,0,1						
430	0. 0. 0. 0.							
431	REF 1 'R-3'							
432	SSR2 293.,T,,4,7							
433	0.02, 0.05, 0.10,	0.15, 0.20,	0.30, 0.40					
434	3.0E-3, 7,	381. 445.	541. 625.	703. 841.	953.			
435	12., 6,	517. 567.	647. 721.	790. 894.				
436	36., 6,	567. 629.	708. 790.	845. 967.				
437	360., 5,	604. 669.	757. 842.	911.				
438	*							
439	MAT 'SUS304L'	2007,0,0,0,0,1						
440	0. 0. 0. 0.							
441	REF 1 'R-7'							
442	SSR 293.,L,,1							
443	+1.E-2, 9,	0.01 63., 0.02	150., 0.05	483., 0.11	896.,			
444	0.16 878., 0.22	938., 0.29	1080., 0.36	1190.,				
445	0.43 1210.							
446	*							
447	MAT 'SUS304'	2008,0,0,0,0,8						
448	0. 0. 0. 0.							
449	REF 1 'R-10'							
450	COM 'C 0.08,MN 2.0,SI 1.0,P 0.045,S 0.03,CR 18.0-20.0,NI 8.0-10.5,MO 2.0-3.0'							
1	2	3	4	5	6	7	8	

## Appendix G (Continued)

DATA SEQ. NO.	1	2	3	4	5	6	7	8
451	SSR 223.,T,,1							
452	1.0E-4, 4,	0.0002	170., 0.0005	198., 0.0010	233., 0.0020	237.		
453	SSR 253.,T,,1							
454	1.0E-4, 4,	0.0002	193., 0.0005	216., 0.0010	229., 0.0020	241.		
455	SSR 273.,T,,1							
456	1.0E-4, 4,	0.0002	198., 0.0005	219., 0.0010	232., 0.0020	243.		
457	SSR 293.,T,,1							
458	1.0E-4, 4,	0.0002	194., 0.0005	207., 0.0010	217., 0.0020	226.		
459	SSR 373.,T,,1							
460	1.0E-4, 4,	0.0002	136., 0.0005	148., 0.0010	157., 0.0020	167.		
461	SSR 473.,T,,1							
462	1.0E-4, 4,	0.0002	105., 0.0005	123., 0.0010	131., 0.0020	139.		
463	SSR 573.,T,,1							
464	1.0E-4, 4,	0.0002	98.5,	0.0005 114., 0.0010	122., 0.0020	130.		
465	SSR 673.,T,,1							
466	1.0E-4, 4,	0.0002	88.2,	0.0005 107., 0.0010	114., 0.0020	121.		
467	*							
468	MAT 'SUS316'	2009,0,0,0,0,8						
469	0. 0. 0. 0.							
470	REF 1 'R-10'							
471	COM 'C 0.08,MN 2.0,SI 1.0,P 0.045,S 0.03,CR 16.0-18.0,NI 10.0-14.0,MO 2.0-3.0'							
472	SSR 223.,T,,1							
473	1.0E-4, 4,	0.0002	256., 0.0005	292., 0.0010	312., 0.0020	337.		
474	SSR 253.,T,,1							
475	1.0E-4, 4,	0.0002	232., 0.0005	259., 0.0010	275., 0.0020	288.		
476	SSR 273.,T,,1							
477	1.0E-4, 4,	0.0002	208., 0.0005	233., 0.0010	253., 0.0020	262.		
478	SSR 293.,T,,1							
479	1.0E-4, 4,	0.0002	198., 0.0005	213., 0.0010	223., 0.0020	235.		
480	SSR 373.,T,,1							
481	1.0E-4, 4,	0.0002	152., 0.0005	165., 0.0010	176., 0.0020	184.		
482	SSR 473.,T,,1							
483	1.0E-4, 4,	0.0002	128., 0.0005	137., 0.0010	143., 0.0020	152.		
484	SSR 573.,T,,1							
485	1.0E-4, 4,	0.0002	121., 0.0005	127., 0.0010	131., 0.0020	139.		
486	SSR 673.,T,,1							
487	1.0E-4, 4,	0.0002	111., 0.0005	117., 0.0010	122., 0.0020	130.		
488	*							
489	MAT 'SUS304'	2010,0,0,0,0,4						
490	0. 0. 0. 0.							
491	REF 1 'R-10'							
492	SSR 297.,T,,1							
493	1.0E-4, 7,	0.002	235.5,	0.005 276.5,	0.010 295. ,	0.015 306. ,		
494	0.020 317. ,	0.030 336.5,	0.040 405. ,					
495	SSR 366.,T,,1							
496	1.0E-4, 7,	0.002	198. ,	0.005 228.5,	0.010 251.5,	0.015 263.5,		
497	0.020 271.5,	0.030 283.5,	0.040 296.5					
498	SSR 477.,T,,1							
499	1.0E-4, 7,	0.002	169. ,	0.005 194. ,	0.010 216. ,	0.015 229.5,		
500	0.020 243.5,	0.030 267. ,	0.040 290.5					
1	2	3	4	5	6	7	8	

## Appendix G (Continued)

DATA SEQ. NO.	1	2	3	4	5	6	7	8
501	SSR	589.,T,,1						
502		1.0E-4, 7,	0.002 149.5, 0.005 172., 0.010 190., 0.015 201.5,					
503			0.020 211.5, 0.030 231., 0.040 248.					
504	*							
505	MAT	'SUS316'	2011,0,0,0,0,4					
506		0. 0. 0. 0.						
507	REF	1 'R-10'						
508	SSR	297.,T,,1						
509		1.0E-4, 7,	0.002 264., 0.005 308., 0.010 330., 0.015 344.5,					
510			0.020 371.5, 0.030 393., 0.040 418.					
511	SSR	366.,T,,1						
512		1.0E-4, 7,	0.002 233.5, 0.005 276.5, 0.010 299.5, 0.015 315.5,					
513			0.020 338.5, 0.030 354.5, 0.040 351.					
514	SSR	477.,T,,1						
515		1.0E-4, 7,	0.002 200.5, 0.005 232.5, 0.010 255., 0.015 269.,					
516			0.020 292.5, 0.030 308., 0.040 327.					
517	SSR	589.,T,,1						
518		1.0E-4, 7,	0.002 192.5, 0.005 216., 0.010 234., 0.015 250.5,					
519			0.020 273., 0.030 294., 0.040 319.5					
520	*							
521	MAT	'SUS316L'	2012,0,0,0,2					
522		0. 0. 0. 0.						
523	REF	1 'R-27'						
524	SSR2	293.,T,,4,9						
525		0.02, 0.05, 0.10, 0.14, 0.18, 0.22, 0.26, 0.34, 0.41						
526		3.9E-3, 9, 383. 450. 538. 612. 680. 743. 797. 892. 965.						
527		1.5E+1, 8, 515. 571. 642. 708. 768. 818. 863. 952.						
528		4.3E+1, 8, 567. 626. 691. 768. 827. 873. 919. 1001.						
529		4.1E+2, 7, 605. 691. 755. 827. 890. 936. 971.						
530	SSR2	673.,T,,4,7						
531		0.02, 0.05, 0.10, 0.14, 0.18, 0.22, 0.26						
532		2.9E-3, 7, 309. 362. 433. 494. 547. 594. 623.						
533		4.4E+1, 6, 368. 416. 473. 531. 561. 589.						
534		6.9E+1, 6, 403. 452. 505. 550. 579. 599.						
535		4.6E+2, 5, 367. 435. 496. 551. 574.						
536	*							
537	MAT	'SUS316L'	2013,0,0,0,2					
538		0. 0. 0. 0.						
539	REF	1 'R-27'						
540	SSR	293.,T,,5						
541		1.0E-2, 1, 0.002 314.						
542		1.0E-1, 1, 0.002 356.						
543		1.0, 1, 0.002 394.						
544		1.0E+2, 1, 0.002 437.						
545		1.0E+2, 1, 0.002 481.						
546	SSR	673.,T,,5						
547		1.0E-2, 1, 0.002 242.						
548		1.0E-1, 1, 0.002 255.						
549		1.0, 1, 0.002 270.						
550		1.0E+1, 1, 0.002 286.						
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## Appendix G (Continued)

DATA SEQ. NO.	1	2	3	4	5	6	7	8
551	1.0E+2, 1, 0.002 331.							
552	*							
553	MAT	'SUS304'	2014,0,0,0,1					
554		0. 0. 0. 0.						
555	REF	1 'R-4'						
556	SSR	293.,T,,10						
557		1.00E-3, 1, 0.002 237.						
558		1.001E-3, 1, 0.002 250.						
559		1.002E-3, 1, 0.002 336.						
560		1.003E-3, 1, 0.002 272.						
561		1.004E-3, 1, 0.002 273.						
562		1.005E-3, 1, 0.002 344.						
563		1.006E-3, 1, 0.002 270.						
564		1.007E-3, 1, 0.002 255.						
565		1.008E-3, 1, 0.002 320.						
566		1.009E-3, 1, 0.002 344.						
567	*	SUS 18-B						
568	MAT	'SUS 18-B'	2015,0,0,0,2					
569		0. 0. 0. 0.						
570	REF	1 'R-6'						
571	COM	'N1 9.15.CR 18.27.C 0.06,MN 1.62,S 0.01,N 0.019,S1 0.39,P 0.026,CU 0.01'						
572	SSR2	206.,T,,3,9						
573		0.026,0.052,0.078,0.104,0.154,0.208,0.260,0.313,0.365						
574		5.45E-4,8, 366. 446. 555. 664. 869. 1087. 1281. 1396.						
575		4.99E-2,9, 431. 494. 555. 621. 784. 969. 1132. 1311. 1426.						
576		4.8E+1,9, 364. 462. 719. 784. 913. 1034. 1176. 1258. 1278.						
577	SSR	293.,T,,3						
578		5.05E-4,9, 0.026 315., 0.053 362., 0.077 407., 0.102 446.,						
579		0.147 514., 0.202 597., 0.230 668., 0.303 733.						
580		0.351 801.						
581		6.26E-2,9, 0.026 335., 0.053 382., 0.077 428., 0.102 467.,						
582		0.147 538., 0.202 614., 0.250 691., 0.303 746.						
583		0.351 814.						
584		5.48E+1,9, 0.027 457., 0.053 499., 0.077 534., 0.102 573.,						
585		0.152 641., 0.202 727., 0.250 792., 0.303 861.,						
586		0.351 920.						
587	*							
588	MAT	'SUS304'	2016,0,0,0,2					
589		0. 0. 0. 0.						
590	REF	1 'R-46'						
591	COM	'N 9.15.CR 18.27.C 0.06,S1 0.39,MN 1.62,P 0.026,S 0.010'						
592	SSR	207.,T,,3						
593		5.45E-4,9, 0. 273., 0.024 360., 0.049 447., 0.076 556.,						
594		0.104 665., 0.152 866., 0.200 1085., 0.251 1272.,						
595		0.300 1400.						
596		4.99E-2,9, 0. 337., 0.024 435., 0.049 490.,						
597		0.104 621., 0.152 790., 0.200 964., 0.251 1143.,						
598		0.300 1309., 0.352 1428.						
599		4.8E+1,10, 0. 463., 0.024 553., 0.049 643., 0.076 714.,						
600		0.104 785., 0.152 904., 0.200 1037., 0.251 1177.,						
		-----0-----5-----0-----5-----0-----5-----0-----5-----0						
		1 2 3 4 5 6 7 8						

## Appendix G (Continued)

DATA SEQ. NO.	1	2	3	4	5	6	7	8
601								
602	SSR2 293.,7.,3,10							
603	0.	.026,0.052,0.078,0.104,0.154,0.206,0.257,0.308,0.358						
604	5.05E-4,10, 249, 313, 362, 408, 446, 519, 596, 671, 734, 804,							
605	6.26E-2,10, 257, 335, 388, 428, 471, 541, 612, 694, 749, 812,							
606	5.48E+1,10, 392, 458, 500, 538, 576, 638, 730, 792, 867, 926,							
607	*							
608	MAT 'SUS304'	2017,0,0,0,1						
609	0. 0. 0.							
610	REF 1 'R-48'							
611	COM 'C 0.079,SI 0.360,MN 1.660,CR 18.350,NI 10.030,MD 0.060'							
612	SSR2 293.,7.,4,8							
613	0.0253,0.0513,0.0780,0.1054,0.1335,0.1625,0.1924,0.2231							
614	1.1E-4, 6, 413, 466, 508, 556, 622, 687,							
615	1.1E-2, 8, 413, 475, 535, 591, 652, 716, 784, 855,							
616	1.3E+2, 4, 586, 624, 662, 697,							
617	3.1E+2, 6, 599, 642, 710, 773, 831, 894.							
618	*							
619	MAT 'SUS304'	2018,0,0,0,1						
620	0. 0. 0.							
621	REF 1 'R-48'							
622	COM 'C 0.079,SI 0.360,MN 1.660,CR 18.350,NI 10.030,MD 0.060'							
623	SSR2 293.,7.,4,7							
624	0.0253,0.0513,0.0780,0.1054,0.1335,0.1625,0.1924							
625	1.2E-4, 5, 387, 439, 505, 562, 623,							
626	1.2E-2, 6, 400, 473, 540, 607, 683, 759,							
627	2.1E+2, 5, 584, 646, 700, 755, 814,							
628	3.9E+2, 7, 584, 646, 712, 775, 839, 902, 963.							
629	*							
630	MAT 'SUS304'	2019,0,0,0,1						
631	0. 0. 0.							
632	REF 1 'R-48'							
633	COM 'C 0.077,SI 0.280,MN 1.730,CR 18.490,NI 8.920,MD 0.050'							
634	SSR2 293.,7.,4,8							
635	0.0253,0.0513,0.0780,0.1054,0.1335,0.1625,0.1924,0.2233							
636	1.1E-4, 4, 413, 466, 521, 591,							
637	1.1E-2, 8, 423, 484, 553, 613, 682, 758, 841, 925,							
638	1.5E+2, 4, 595, 653, 675, 697,							
639	2.8E+2, 6, 624, 680, 734, 785, 840, 875.							
640	*							
641	MAT 'SUS304'	2020,0,0,0,1						
642	0. 0. 0.							
643	REF 1 'R-48'							
644	COM 'C 0.077,SI 0.280,MN 1.730,CR 18.490,NI 8.920,MD 0.050'							
645	SSR2 293.,7.,4,8							
646	0.0253,0.0513,0.0780,0.1054,0.1335,0.1625,0.1924,0.2231							
647	1.2E-4, 5, 375, 433, 490, 560, 639,							
648	1.2E-2, 8, 394, 461, 512, 573, 639, 708, 784, 870,							
649	2.7E+2, 5, 538, 587, 639, 692, 750,							
650	3.8E+2, 8, 605, 661, 725, 785, 849, 908, 962, 996.							
651	*							
652	MAT 'SUS304'	2021,0,0,0,1						
653	0. 0. 0.							
654	REF 1 'R-48'							
655	COM 'C 0.080,SI 0.280,MN 1.710,CR 18.050,NI 7.890,MD 0.050'							
656	SSR2 293.,7.,4,7							
657	0.0253,0.0513,0.0780,0.1054,0.1335,0.1625,0.1924							
658	1.0E-4, 4, 408, 475, 539, 609,							
659	1.0E-2, 7, 442, 498, 567, 639, 716, 791, 885,							
660	6.3E+1, 4, 592, 653, 721, 775,							
661	3.4E+2, 6, 643, 698, 752, 807, 866, 908,							
662	*							
663	MAT 'SUS304'	2022,0,0,0,1						
664	0. 0. 0.							
665	REF 1 'R-48'							
666	COM 'C 0.080,SI 0.280,MN 1.710,CR 18.050,NI 7.890,MD 0.050'							
667	SSR2 293.,7.,4,6							
668	0.0253,0.0513,0.0780,0.1054,0.1335,0.1625							
669	1.2E-4, 5, 389, 448, 502, 558, 613,							
670	1.2E-2, 6, 401, 471, 534, 603, 673, 738,							
671	1.9E+2, 4, 547, 601, 649, 709,							
672	3.9E+2, 6, 577, 637, 694, 758, 814, 876,							
673	*							
674	MAT 'SUS304'	2023,0,0,0,1						
675	0. 0. 0.							
676	REF 1 'R-48'							
677	COM 'C 0.069,SI 0.380,MN 1.800,CR 18.580,NI 10.350,MD 0.020'							
678	SSR2 293.,7.,4,8							
679	0.0253,0.0513,0.0780,0.1054,0.1335,0.1625,0.1924,0.2231							
680	1.0E-4, 5, 331, 386, 435, 494, 562,							
681	1.0E-2, 8, 355, 400, 449, 507, 557, 612, 671, 733,							
682	1.9E+2, 4, 475, 521, 576, 626,							
683	3.8E+2, 7, 499, 545, 594, 644, 699, 762, 809,							
684	*							
685	MAT 'SUS304'	2024,0,0,0,1						
686	0. 0. 0.							
687	REF 1 'R-48'							
688	COM 'C 0.069,SI 0.380,MN 1.800,CR 18.580,NI 10.350,MD 0.020'							
689	SSR2 293.,7.,4,8							
690	0.0253,0.0513,0.0780,0.1054,0.1335,0.1625,0.1924,0.2231							
691	1.2E-4, 5, 307, 363, 412, 467, 536,							
692	1.2E-2, 8, 312, 368, 422, 476, 540, 608, 679, 753,							
693	2.8E+2, 6, 456, 507, 571, 631, 690, 758,							
694	5.3E+2, 8, 461, 521, 580, 635, 699, 762, 825, 886,							
695	*							
696	MAT 'SUS304'	2025,0,0,0,1						
697	0. 0. 0.							
698	REF 1 'R-48'							
699	COM 'C 0.079,SI 0.320,MN 1.660,CR 18.160,NI 10.140,MD 0.060'							
700	SSR2 293.,7.,4,8							

DATA SEQ. NO.	1	2	3	4	5	6	7	8
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## Appendix G (Continued)

DATA	1	2	3	4	5	6	7	8
SEQ. NO.	-----5-----0-----5-----0-----5-----0-----5-----0-----5-----0-----5-----0-----5-----0							
701	0.0253,0.0513,0.0780,0.1054,0.1335,0.1625,0.1924,0.2231							
702	1.1E-4, 6, 451.	512.	553.	613.	677.	733.		
703	1.1E-2, 8, 466.	535.	589.	655.	737.	808.	889.	964.
704	7.8E+1, 3, 668.	709.	751.					
705	2.4E+2, 5, 730.	768.	807.	842.	858.			
706	*							
707	MAT 'SUS304'	2026,0,0,0,0,1						
708	0. 0. 0. 0.							
709	REF 1 'R-48'							
710	COM 'C 0.079, SI 0.320,MN 1.660,CR 18.160,NI 10.140,MD 0.060'							
711	SSR2 293.,C,,4,8							
712	0.0253,0.0513,0.0780,0.1054,0.1335,0.1625,0.1924,0.2231							
713	1.2E-4, 4, 366.	405.	453.	520.				
714	1.2E-2, 8, 375.	433.	485.	538.	600.	662.	728.	804.
715	1.6E+2, 4, 634.	679.	722.	751.				
716	3.0E+2, 5, 668.	724.	769.	813.	846.			
717	*							
718	MAT 'SUS304'	2027,0,0,0,0,1						
719	0. 0. 0. 0.							
720	REF 1 'R-48'							
721	COM 'C 0.016, SI 0.310,MN 1.830,CR 18.300,NI 10.330,MD 0.030'							
722	SSR2 293.,C,,4,6							
723	0.0253,0.0513,0.0780,0.1054,0.1335,0.1625							
724	1.1E-4, 5, 370.	419.	467.	520.	579.			
725	1.1E-2, 6, 394.	452.	512.	551.	609.	675.		
726	1.7E+2, 4, 562.	605.	648.	675.				
727	3.5E+2, 6, 576.	638.	684.	741.	793.	841.		
728	*							
729	MAT 'SUS304'	2028,0,0,0,0,1						
730	0. 0. 0. 0.							
731	REF 1 'R-48'							
732	COM 'C 0.016, SI 0.310,MN 1.830,CR 18.300,NI 10.330,MD 0.030'							
733	SSR2 293.,C,,4,7							
734	0.0253,0.0513,0.0780,0.1054,0.1335,0.1625,0.1924							
735	1.2E-4, 5, 334.	389.	448.	503.	558.			
736	1.2E-2, 6, 370.	429.	484.	542.	598.	654.		
737	2.4E+2, 5, 543.	591.	648.	706.	755.			
738	4.8E+2, 7, 567.	614.	675.	723.	789.	825.	861.	
739	*							
740	MAT 'SUS304'	2029,0,0,0,0,1						
741	0. 0. 0. 0.							
742	REF 1 'R-48'							
743	COM 'C 0.047, SI 0.320,MN 1.720,CR 18.470,NI 10.060,MD 0.060'							
744	SSR2 293.,C,,4,6							
745	0.0253,0.0513,0.0780,0.1054,0.1335,0.1625							
746	1.1E-4, 5, 394.	442.	503.	551.	609.			
747	1.1E-2, 6, 420.	478.	532.	588.	642.	683.		
748	1.5E+2, 4, 567.	605.	655.	662.				
749	3.1E+2, 6, 595.	642.	703.	754.	802.	841.		
750	*							

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## Appendix G (Continued)

DATA	1	2	3	4	5	6	7	8
SEQ. NO.	-----5-----0-----5-----0-----5-----0-----5-----0-----5-----0-----5-----0							
751	MAT 'SUS304'	2030,0,0,0,0,1						
752	0. 0. 0. 0.							
753	REF 1 'R-48'							
754	COM 'C 0.047, SI 0.320,MN 1.720,CR 18.470,NI 10.060,MD 0.060'							
755	SSR2 293.,C,,4,8							
756	0.0253,0.0513,0.0780,0.1054,0.1335,0.1625,0.1924,0.2231							
757	1.2E-4, 6, 365.	419.	480.	529.	587.	658.		
758	1.2E-2, 8, 384.	438.	490.	556.	609.	671.	744.	808.
759	2.2E+2, 5, 571.	624.	671.	714.	746.			
760	4.3E+2, 7, 576.	633.	680.	750.	815.	875.	938.	
761	*							
762	MAT 'SUS304'	2031,0,0,0,0,1						
763	0. 0. 0. 0.							
764	REF 1 'R-48'							
765	COM 'C 0.073, SI 0.570,MN 1.600,CR 18.760,NI 8.370,MD 0.210'							
766	SSR2 293.,C,,4,7							
767	0.0253,0.0513,0.0780,0.1054,0.1335,0.1625,0.1924							
768	1.1E-4, 4, 384.	447.	521.	604.				
769	1.1E-2, 7, 399.	461.	521.	600.	673.	754.	845.	
770	1.7E+2, 4, 538.	587.	621.	662.				
771	3.5E+2, 5, 547.	605.	671.	745.	815.			
772	*							
773	MAT 'SUS304'	2032,0,0,0,0,1						
774	0. 0. 0. 0.							
775	REF 1 'R-48'							
776	COM 'C 0.073, SI 0.570,MN 1.600,CR 18.760,NI 8.370,MD 0.210'							
777	SSR2 293.,C,,4,7							
778	0.0253,0.0513,0.0780,0.1054,0.1335,0.1625,0.1924							
779	1.2E-4, 5, 341.	410.	490.	564.	656.			
780	1.2E-2, 7, 360.	438.	512.	591.	669.	758.	857.	
781	2.4E+2, 5, 509.	577.	644.	710.	750.			
782	4.8E+2, 7, 499.	568.	640.	708.	755.	816.	873.	
783	*							
784	MAT 'SUS304'	2033,0,0,0,0,2						
785	0. 0. 0. 0.							
786	REF 1 'R-51'							
787	COM 'NI 8.90,CR 18.63,C 0.08,SI 0.71,MN 1.67,P 0.028,S 0.008'							
788	SSR 293.,T,,10							
789	1.010E-4 /1, 0.009 375.							
790	9.8 /1, 0.019 453.							
791	5.8E+1 /1, 0.028 504.							
792	1.7E+2 /1, 0.058 572.							
793	3.5E+2 /1, 0.110 674.							
794	4.0E+2 /1, 0.162 763.							
795	4.95E+2 /1, 0.209 845.							
796	5.81E+2 /1, 0.295 1000.							
797	5.92E+2 /1, 0.418 1165.							
798	8.29E+2 /1, 0.450 1203.							
799	SSR 673.,T,,6							
800	1.000E-4, 1, 0.110 379.							

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1 2 3 4 5 6 7 8

## Appendix G (Continued)

DATA SEQ. NO.	1	2	3	4	5	6	7	8
801	1.001E-4,	1,	0.162	437.				
802	1.002E-4,	1,	0.209	493.				
803	7.4	,	1,	0.295	561.			
804	7.5	,	1,	0.063	295.			
805	9.3	,	1,	0.256	528.			
806	*							
807	MAT	'SUS304'		2034.0.0.0.0.1				
808	0.	0.	0.	0.				
809	REF	1	'R-51'					
810	COM	'NI 8.90,CR 18.63,C 0.08,SI 0.71,MN 1.67,P 0.028,S 0.008'						
811	SSR	293.,T,,1						
812	2.0E+1,	6,	0.0016	294.,	0.0027	354.,	0.0102	423.,
813							0.0131	438.,
814								0.0161
815	MAT	'SUS304'		2100.7.7.7.7.0				
816	14.3E-6,	194000.,	767000.,	0.266				
817	14.3E-6	293.,	15.1E-6	373.,	16.1E-6	473.,	16.9E-6	573.,
818	17.3E-6	673.,	17.9E-6	773.,	18.3E-6	873.,		
819	194000.	293.,	190000.	373.,	184000.	473.,	177000.	573.,
820	169000.	673.,	159000.	773.,	149000.	873.,		
821	76700.	293.,	74800.	373.,	72100.	473.,	68600.	573.,
822	65100.	673.,	61000.	773.,	56900.	873.,		
823	0.266	293.,	0.272	373.,	0.279	473.,	0.287	573.,
824	0.295	673.,	0.302	773.,	0.310	873.,		
825	*							
826	MAT	'SUS316'		2200.7.7.7.7.0				
827	15.2E-6,	194000.,	767000.,	0.266				
828	15.2E-6	293.,	15.8E-6	373.,	16.5E-6	473.,	17.2E-6	573.,
829	17.7E-6	673.,	18.1E-6	773.,	18.6E-6	873.,		
830	194000.	293.,	190000.	373.,	184000.	473.,	177000.	573.,
831	169000.	673.,	159000.	773.,	149000.	873.,		
832	76700.	293.,	74800.	373.,	72100.	473.,	68600.	573.,
833	65100.	673.,	61000.	773.,	56900.	873.,		
834	0.266	293.,	0.272	373.,	0.279	473.,	0.287	573.,
835	0.295	673.,	0.302	773.,	0.310	873.,		
836	*							
837	MAT	'PURE LEAD'		3001.0.0.0.0.5				
838	0.	0.	0.	0.				
839	REF	1	'R-1'					
840	SSR2	295.,C,,4,7						
841	0.1,	0.2,	0.3,	0.5,	1.0,	1.5,	2.0	
842	0.4	,	11.0	16.5	20.7	26.2	32.4	34.4
843	9.0	,	7,	15.2	21.4	25.5	31.0	37.9
844	10.1	,	7,	18.6	24.1	27.6	33.1	40.0
845	311.	,	7,	21.4	26.2	29.6	35.1	41.3
846	SSR2	383.,C,,4,7						
847	0.1,	0.2,	0.3,	0.5,	1.0,	1.5,	2.0	
848	0.4	,	7,	12.4	15.8	16.8	15.3	13.1
849	9.0	,	7,	17.2	20.0	22.6	22.0	19.8
850	10.1	,	7,	19.3	26.0	29.5	29.8	27.6
851	SSR2	443.,C,,4,7						
852	0.1,	0.2,	0.3,	0.5,	1.0,	1.5,	2.0	
853	0.4	,	7,	11.0	13.8	12.4	11.0	10.5
854	9.0	,	7,	13.8	17.8	17.9	15.0	13.5
855	10.1	,	7,	18.3	21.4	24.0	24.7	21.5
856	311.	,	7,	23.4	28.0	29.8	30.2	26.9
857	SSR2	533.,C,,4,7						
858	0.1,	0.2,	0.3,	0.5,	1.0,	1.5,	2.0	
859	0.4	,	7,	4.1	5.2	3.9	3.2	2.8
860	9.0	,	7,	8.8	9.9	10.5	9.2	8.3
861	10.1	,	7,	12.1	14.1	14.9	14.7	13.8
862	311.	,	7,	14.9	16.8	18.1	18.9	17.9
863	SSR2	573.,C,,4,8						
864	0.05,	0.1,	0.2,	0.3,	0.5,	1.0,	1.5,	2.0
865	0.4	,	8,	3.10	3.65	3.65	3.10	2.48
866	9.0	,	8,	5.51	6.82	7.58	7.72	7.44
867	10.1	,	8,	10.0	10.7	11.9	12.7	13.0
868	311.	,	8,	12.4	13.2	14.8	15.6	16.0
869	SSR2	573.,C,,4,8						
870	*							
871	MAT	'PURE LEAD'		3002.0.0.0.0.1				
872	0.	0.	0.	0.				
873	REF	1	'R-1'					
874	SSR2	275.,C,,2,6						
875	0.02,	0.04,	0.08,	0.16,	0.24,	0.32		
876	3.33E-4,	6,	8.96	11.7	13.8	17.2	19.3	21.4
877	2.0E+3	,	6,	13.8	17.9	25.4	28.9	33.1
878	*							
879	MAT	'PURE LEAD'		3003.0.0.0.0.3				
880	0.	0.	0.	0.				
881	REF	2	'R-1','R-10'					
882	SSR2	273.,C,,2,5						
883	0.11,	0.22,	0.36,	0.51,	0.69			
884	0.8	,	5,	19.6	25.8	28.8	32.6	32.6
885	10.0	,	5,	21.2	28.0	33.3	36.4	39.4
886	SSR2	293.,C,,2,5						
887	0.11,	0.22,	0.36,	0.51,	0.69			
888	0.8	,	5,	19.6	25.8	28.8	31.8	31.8
889	10.0	,	5,	19.6	26.5	31.1	34.1	36.4
890	SSR	383.,C,,2						
891	0.8	,	5,	0.11	15.2	0.22	18.2	0.36
892								16.7
893								0.51
894	MAT	'LEAD'		3004.0.0.0.0.1				
895	0.	0.	0.	0.				
896	REF	1	'R-1'					
897	SSR	295.,C,,1						
898	5.0E+4,	8,	0.012	55.1	0.020	89.6	0.025	117.1
899								0.032
900	*							137.8,
901								68.9
902								

1	2	3	4	5	6	7	8
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## Appendix G (Continued)

DATA SEQ. NO.	1	2	3	4	5	6	7	8
901	MAT 'PURE LEAD'	3005	0.0,0,0,0,4					
902	0. 0. 0. 0.							
903	REF 1 'R-10'							
904	SSR2 311.,T,,2,8							
905	0.01, 0.03, 0.05, 0.10, 0.18, 0.26, 0.34, 0.41							
906	8.3E-5, 5, 2.16 2.98 3.69 5.15 7.52							
907	1.0E-3, 8, 2.82 5.54 7.74 10.91 14.68 16.00 11.58 0.31							
908	SSR2 332.,T,,2,9							
909	0.01, 0.03, 0.05, 0.10, 0.18, 0.26, 0.34, 0.41, 0.47							
910	8.3E-5, 5, 1.95 2.66 3.22 4.28 5.79							
911	1.0E-3, 9, 2.80 5.04 6.51 8.72 9.43 8.15 7.23 5.58 2.15							
912	SSR2 393.,T,,2,9							
913	0.01, 0.03, 0.05, 0.10, 0.18, 0.26, 0.34, 0.41, 0.47							
914	8.3E-5, 5, 1.57 1.99 2.32 2.99 4.05							
915	1.0E-3, 9, 2.37 3.90 4.77 5.87 5.21 5.02 4.92 4.86 4.30							
916	SSR2 436.,T,,2,9							
917	0.01, 0.03, 0.05, 0.10, 0.18, 0.26, 0.34, 0.41, 0.47							
918	8.3E-5, 5, 1.18 1.42 1.63 1.97 2.56							
919	1.0E-3, 9, 1.74 2.63 3.18 3.68 3.22 3.18 3.09 3.05 2.98							
920	*							
921	MAT 'PURE LEAD'	3006	0.0,0,0,0,6					
922	0. 0. 0. 0.							
923	REF 1 'R-10'							
924	SSR2 311.,T,,2,6							
925	0.02, 0.05, 0.10, 0.18, 0.26, 0.34							
926	8.3E-5, 6, 3.80 6.37 8.94 11.12 6.94 2.12							
927	8.3E-4, 6, 3.80 6.95 10.61 14.55 15.94 11.09							
928	SSR2 393.,T,,2,8							
929	0.02, 0.05, 0.10, 0.18, 0.26, 0.34, 0.41, 0.47							
930	8.3E-5, 8, 2.53 3.65 3.79 5.21 3.58 3.47 3.10 1.38							
931	8.3E-4, 8, 3.37 4.70 5.84 5.29 5.02 4.82 4.81 4.41							
932	SSR2 311.,C,,1,6							
933	0.002,0.005,0.01, 0.02, 0.03, 0.04							
934	2.5E-4, 6, 2.24 4.64 5.94 7.59 8.94 10.14							
935	SSR2 352.,C,,1,6							
936	0.002,0.005,0.01, 0.02, 0.03, 0.04							
937	2.5E-4, 6, 1.17 3.15 4.21 5.48 6.39 7.04							
938	SSR2 393.,C,,1,6							
939	0.002,0.005,0.01, 0.02, 0.03, 0.04							
940	2.5E-4, 6, 1.17 2.67 3.24 4.01 4.47 4.12							
941	SSR2 436.,C,,1,6							
942	0.002,0.005,0.01, 0.02, 0.03, 0.04							
943	2.5E-4, 6, 0.76 1.90 2.23 2.67 3.09 3.08							
944	*							
945	MAT 'PURE LEAD'	3007	0.0,0,0,0,3					
946	0. 0. 0. 0.							
947	REF 1 'R-1'							
948	SSR2 295.,C,,9,4							
949	0.03, 0.10, 0.30, 0.50							
950	1.0E-4, 4, 8.89 12.1 16.3 16.3							
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	1	2	3	4	5	6	7	8

## Appendix G (Continued)

DATA SEQ. NO.	1	2	3	4	5	6	7	8
951	1.0E-3, 4, 9.85 13.8 19.6 19.6							
952	1.0E-2, 4, 10.8 15.6 22.6 23.5							
953	1.0E-1, 4, 11.8 17.4 25.3 27.0							
954	1.0, , 4, 12.7 19.2 28.0 30.9							
955	1.0E+1, 4, 13.9 20.7 31.0 34.8							
956	1.0E+2, 4, 14.7 22.7 33.8 38.5							
957	1.0E+3, 4, 15.8 24.4 36.5 42.3							
958	1.0E+4, 4, 16.7 25.4 39.3 46.0							
959	SSR 311.,C,,1							
960	1.0E-4, 2, 0.002 2.72 , -0. 6.13							
961	SSR 441.,C,,1							
962	1.0E-4, 2, 0.002 0.083, -0. 3.91							
963	*							
964	MAT 'PURE LEAD'	3008	0.0,0,0,0,3					
965	0. 0. 0. 0.							
966	REF 1 'R-1'							
967	SSR 293.,C,,9							
968	11. , , 1, 0.07 15.8							
969	12. , , 1, 0.13 21.4							
970	12.5 , , 1, 0.21 24.8							
971	14. , , 1, 0.29 28.2							
972	15. , , 1, 0.38 31.0							
973	16.5 , , 1, 0.47 33.8							
974	18. , , 1, 0.56 35.1							
975	21. , , 1, 0.70 36.5							
976	23.5 , , 1, 0.83 37.9							
977	SSR2 295.,C,,7,6							
978	0.03, 0.06, 0.12, 0.18, 0.24, 0.30							
979	1.0E-3, 6, 11.4 13.7 16.5 18.7 20.3 21.9							
980	1.0E-2, 6, 12.1 14.9 18.2 20.7 22.5 24.3							
981	1.0E-1, 6, 12.9 16.1 19.8 22.5 24.7 26.5							
982	1.0, , 6, 13.8 17.4 21.6 24.5 26.9 28.8							
983	1.0E+1, 6, 14.5 18.7 23.3 26.4 29.1 31.2							
984	1.0E+2, 6, 15.4 19.8 25.1 28.4 31.2 33.3							
985	1.0E+3, 6, 16.1 21.2 26.9 30.2 33.3 35.6							
986	SSR 503.,C,,5							
987	5.75 , , 1, 0.11 16.5							
988	6.5 , , 1, 0.22 21.4							
989	7.4 , , 1, 0.36 23.4							
990	8.75 , , 1, 0.51 23.4							
991	10.2 , , 1, 0.64 22.7							
992	*							
993	MAT 'PURE LEAD'	3009	0.0,0,0,0,3					
994	0. 0. 0. 0.							
995	REF 1 'R-4'							
996	SSR 233.,C,,1							
997	1.7E-5, 1, 0.002 8.9							
998	SSR2 293.,C,,1,5							
999	0.0020, 0.0021, 0.0022, 0.0023, 0.0024							
1000	1.7E-5, 5, 3.1 10.9 4.4 5.6 4.5							
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	1	2	3	4	5	6	7	8

## Appendix G (Continued)

DATA SEQ. NO.	1	2	3	4	5	6	7	8
1001	SSR	450.,C,,1						
1002		1.7E-5, 1, 0.002	1.3					
1003	*							
1004	MAT	'PURE LEAD'	3010,0,1,0,0,6					
1005		0.	1000.	0.	0.			
1006		1000.	293.					
1007	REF	1	'R-4'					
1008	SSR	233.,C,,1						
1009		1.0E-4, 1,	0.0020	2.08				
1010	SSR	233.,C,,1						
1011		1.001E-4, 1,	0.0020	9.02				
1012	SSR	293.,C,,1						
1013		1.00E-4, 1,	0.0020	3.23				
1014	SSR	293.,C,,1						
1015		1.001E-4, 1,	0.0020	1.45				
1016	SSR	293.,C,,1						
1017		1.002E-4, 1,	0.0020	11.1				
1018	SSR	450.,C,,1						
1019		1.0E-4, 1,	0.0020	1.27				
1020	*							
1021	MAT	'PURE LEAD'	3011,0,1,0,0,4					
1022		0.	0.	0.	0.			
1023		1000.	293.					
1024	REF	1	'R-4'					
1025	SSR	293.,C,,1						
1026		1.0E-4, 1,	0.0020	0.97				
1027	SSR	293.,C,,1						
1028		1.001E-4, 1,	0.0020	1.45				
1029	SSR	293.,C,,1						
1030		1.002E-4, 1,	0.0020	4.51				
1031	SSR	293.,C,,1						
1032		1.003E-4, 1,	0.0020	5.68				
1033	*							
1034	MAT	'PURE LEAD'	3012,0,1,0,0,2					
1035		0.	0.	0.	0.			
1036		1000.	293.					
1037	REF	1	'R-4'					
1038	SSR	293.,C,,1						
1039		1.0E-4, 1,	0.0020	1.24				
1040	SSR	293.,C,,1						
1041		1.001E-4, 1,	0.0020	4.61				
1042	*							
1043	MAT	'PURE LEAD'	3013,0,0,0,0,1					
1044		0.	0.	0.	0.			
1045	REF	1	'R-12'					
1046	SSR	293.,C,,3						
1047		2.66E-5, 7,	0.04	7.4,	0.10	10.8,	0.20	13.3,
1048			0.50	13.4,	0.70	12.9,		
1049		7.82E-3, 7,	0.04	11.7,	0.10	16.9,	0.20	20.4,
1050			0.50	22.6,	0.70	22.3,		
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	1	2	3	4	5	6	7	8

## Appendix G (Continued)

DATA SEQ. NO.	1	2	3	4	5	6	7	8
1051	2.31E-2, 7,	0.03	10.3,	0.10	16.9,	0.20	20.4,	0.30
1052		0.50	24.3,	0.70	24.3			
1053	*							
1054	MAT	'PURE LEAD'	3014,0,0,0,0,1					
1055		0.	0.	0.	0.			
1056	REF	1	'R-12'					
1057	SSR	293.,T,,4						
1058		1.02E-4, 6,	0.03	4.2,	0.05	6.9,	0.10	11.4,
1059			0.25	14.6				
1060		1.02E-3, 6,	0.03	4.2,	0.05	6.9,	0.10	12.6,
1061			0.25	16.5				
1062		1.02E-2, 5,	0.04	6.1,	0.10	15.3,	0.15	16.8,
1063			0.25	15.6				
1064	*							
1065	MAT	'PURE LEAD'	3015,0,0,0,0,1					
1066		0.	0.	0.	0.			
1067	REF	1	'R-12'					
1068	SSR	293.,C,,1,9						
1069		0.03,	0.05,	0.10,	0.20,	0.30,	0.40,	0.50,
1070		0.50	8.3,	14.5	22.3	29.4	33.2	35.7
1071	*							
1072	MAT	'Pb'	3016,0,0,0,0,4					
1073		0.	0.	0.	0.			
1074	REF	1	'R-B5'					
1075	COM	'KANAZAWA UNIVERSITY TEST DATA'						
1076	SSR2	423.,C,,4,20						
1077		0.01	0.02,	0.03,	0.04,	0.05,	0.06,	0.07,
1078		0.11	0.12,	0.13,	0.14,	0.15,	0.16,	0.17,
1079		0.31	0.32	0.33	0.34	0.35	0.36	0.37
1080		8.3E-4, 20,	5.4	7.4	9.2	10.3	11.2	12.0
1081			13.7	13.5	13.5	13.5	13.4	13.3
1082		1.7E-2, 20,	9.0	12.8	15.4	16.6	17.2	17.9
1083			19.9	20.0	20.2	20.3	20.3	20.4
1084		1.7E-1, 20,	10.3	13.7	15.8	17.2	18.3	19.4
1085			22.6	22.8	23.0	23.1	23.2	23.3
1086		650.,	7.2	13.8	18.2	20.8	22.8	24.2
1087			23.4	23.8	23.9	24.4	24.7	24.9
1088	SSR2	373.,C,,3,20						
1089		0.01	0.02	0.03	0.04	0.05	0.06	0.07
1090		0.11	0.12	0.13	0.14	0.15	0.16	0.17
1091		0.31	0.32	0.33	0.34	0.35	0.36	0.37
1092		8.3E-4, 15,	5.1	7.4	9.2	10.2	11.0	11.8
1093			12.6	12.5	12.3	12.3	12.3	12.3
1094		1.7E-2, 20,	9.6	14.2	16.5	17.7	18.8	19.3
1095			21.6	21.5	21.7	21.9	22.1	22.3
1096		1.7E-1, 20,	9.4	13.9	16.3	18.1	19.5	20.1
1097			23.4	23.8	23.9	24.4	24.7	24.9
1098	SSR2	293.,C,,8,20						
1099		0.01	0.02	0.03	0.04	0.05	0.06	0.07
1100		0.11	0.12	0.13	0.14	0.15	0.16	0.17
		0.31	0.32	0.33	0.34	0.35	0.36	0.37
		13.3	13.3	13.3	13.4	13.4	13.5	13.6
		13.7						
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	1	2	3	4	5	6	7	8

## Appendix G (Continued)

DATA SEQ. NO.	1	2	3	4	5	6	7	8
1101	3.2E-4,17,	6.5	7.6	9.0	10.4	11.7	12.4	13.2
1102		16.3	16.8	17.2	17.6	17.9	18.3	18.8
1103	9.7E-3,12,	6.8	8.6	10.0	11.6	12.5	13.4	14.4
1104		17.3	17.8					
1105	1.7E-2,20,	8.3	11.2	13.1	15.0	16.5	17.6	18.3
1106		19.2	21.6	21.9	22.4	22.6	22.6	22.7
1107	1.7E-1,20,	8.0	12.0	14.5	16.7	18.6	19.7	20.7
1108		21.1	21.6	21.9	22.4	22.6	22.6	22.7
1109	0.89 ,20,	7.7	8.6	10.0	11.5	12.3	13.8	14.9
1110		18.4	19.1	19.8	20.2	20.7	21.1	21.7
1111	400. ,13,	9.7	12.9	14.7	17.0	18.1	19.4	20.6
1112		22.6	23.2	23.6	23.7	24.0	24.1	24.3
1113	650. ,20,	11.8	16.5	19.4	21.9	24.4	26.2	27.9
1114		25.3	26.3	27.1				
1115	SSR2 223.,C,,4,20	33.1	34.1	34.8	35.4	36.3	36.8	37.6
1116		38.0	38.7	39.2				
1117	0.01,0.02,0.03,0.04,0.05,0.06,0.07,0.08,0.09,0.10,							
1118	0.11,0.12,0.13,0.14,0.15,0.16,0.17,0.18,0.19,0.20							
1119	8.3E-4,20,	6.4	8.9	10.5	12.1	13.4	14.6	15.5
1120		16.3	16.9	18.6	19.2	19.2	19.3	19.3
1121	1.7E-2,20,	9.4	12.2	14.5	16.1	17.3	18.3	19.0
1122		19.0	21.2	22.3	22.5	22.7	22.8	23.1
1123	1.7E-1,20,	10.6	13.8	16.0	17.7	19.3	20.6	21.8
1124		22.6	24.8	25.3	25.4	25.6	26.0	26.1
1125	650. ,20,	13.7	16.2	19.3	21.9	23.8	25.9	27.7
1126		29.7	30.2	30.4	31.1	32.8	33.5	34.2
1127	MAT 'PB2'	3017,0,0,0,0,4						
1128	0. 0. 0.							
1129	REF 1 'R-85'							
1130	CDM 'KANAZAWA UNIVERSITY TEST DATA'							
1131	SSR2 423.,C,,4,20							
1132	0.01,0.02,0.03,0.04,0.05,0.06,0.07,0.08,0.09,0.10,							
1133	0.11,0.12,0.13,0.14,0.15,0.16,0.17,0.18,0.19,0.20							
1134	8.3E-4,20,	12.7	15.1	16.4	16.9	17.5	18.1	18.4
1135		18.6	19.9	20.5	20.7	21.0	21.3	21.4
1136	1.7E-2,20,	18.1	20.2	21.7	23.1	24.2	24.9	25.5
1137		26.2	26.2	26.6	27.2	27.8	28.2	28.6
1138	1.7E-1,20,	27.3	27.8	28.1	28.2	28.6	28.8	28.8
1139		29.3	32.2	32.4	33.2	33.7	34.2	34.6
1140	650. ,20,	31.6	32.2	32.4	33.7	34.2	35.1	35.3
1141		35.4	35.4	35.5	35.5	35.5	37.5	38.9
1142	SSR2 373.,C,,3,20	40.2	41.1	41.8	42.4	43.1	43.7	44.1
1143		44.6	45.2	45.8				
1144	0.01,0.02,0.03,0.04,0.05,0.06,0.07,0.08,0.09,0.10,							
1145	0.11,0.12,0.13,0.14,0.15,0.16,0.17,0.18,0.19,0.20							
1146	8.3E-4,20,	13.9	16.5	17.6	18.2	19.0	19.3	19.5
1147		19.8	20.7	20.9	21.2	21.5	21.5	21.6
1148	1.7E-2,20,	20.7	21.6	23.3	24.7	26.2	26.8	27.4
1149		28.4	28.7	29.1	29.9	30.1	30.2	30.5
1150	1.7E-1,20,	31.6	32.2	32.4	33.7	34.2	34.6	35.1
		35.3	35.4	35.5	35.5	35.5	37.5	38.9
1151	SSR2 293.,C,,8,20	32.8	33.8	34.0	34.5	35.1	35.5	35.9
1152		36.3	36.7	37.1	37.5	38.1	38.5	39.0
1153	0.01,0.02,0.03,0.04,0.05,0.06,0.07,0.08,0.09,0.10,							
1154	0.11,0.12,0.13,0.14,0.15,0.16,0.17,0.18,0.19,0.20							
1155	1.7E-4,20,	13.4	16.1	17.8	19.2	20.5	21.4	22.6
1156		23.3	24.2	25.1	25.5	26.2	26.9	27.1
1157	3.2E-4,16,	16.3	19.7	21.9	22.6	23.3	24.2	25.1
1158		26.0	26.1	26.6	27.3	27.8	28.2	28.7
1159	1.5E-2,1B,	16.5	20.7	22.8	25.0	26.6	27.9	28.5
1160		29.6	31.8	32.0	32.3	32.7	33.2	33.8
1161	1.7E-2,20,	16.0	20.1	22.3	24.0	25.0	26.5	27.3
1162		27.1	28.2	29.5	30.7	31.9	32.5	33.4
1163	1.7E-1,20,	18.6	20.9	23.9	26.7	28.8	30.4	31.9
1164		31.4	32.5	32.9	33.7	34.3	34.8	35.3
1165	3.6E-2,20,	18.2	20.7	22.8	25.0	26.7	27.9	29.6
1166		30.5	31.2	31.5	31.8	32.1	32.4	33.2
1167	0.96 ,19,	17.9	20.2	23.8	25.9	27.9	29.5	30.9
1168		31.2	31.8	32.4	33.0	33.6	34.2	35.2
1169	430. ,16,	19.4	25.0	28.5	31.6	33.1	34.6	35.7
1170		35.7	36.0	36.5	37.8	39.6	41.1	42.8
1171	650. ,20,	40.0	40.7	41.6	42.6	42.8	43.2	45.6
1172		47.0	47.9	49.1	50.3	51.1	51.6	52.3
1173	SSR2 233.,C,,4,20	53.1	53.1	53.1	53.1	53.1	53.1	53.8
1174		54.2	54.7	55.0	55.3	55.6	56.0	56.3
1175	0.01,0.02,0.03,0.04,0.05,0.06,0.07,0.08,0.09,0.10,							
1176	0.11,0.12,0.13,0.14,0.15,0.16,0.17,0.18,0.19,0.20							
1177	8.3E-4,20,	12.4	15.9	18.1	20.5	22.0	23.5	24.4
1178		25.5	26.2	26.6	27.3	28.3	29.5	30.5
1179	1.7E-2,20,	18.6	22.8	25.6	27.3	28.3	29.5	30.5
1180		30.5	31.7	32.7	33.7	34.7	35.3	36.0
1181	34.2	35.0	35.5	36.0	36.8	37.4	38.1	39.7
1182	MAT 'PB4'	3018,0,0,0,0,4						
1183	0. 0. 0.							
1184	REF 1 'R-85'							
1185	CDM 'KANAZAWA UNIVERSITY TEST DATA'							
1186	SSR2 423.,C,,4,20							
1187	0.01,0.02,0.03,0.04,0.05,0.06,0.07,0.08,0.09,0.10,							
1188	0.11,0.12,0.13,0.14,0.15,0.16,0.17,0.18,0.19,0.20							
1189	8.3E-4,20,	15.5	17.9	19.2	19.9	20.6	21.0	21.7
1190		22.2	23.3	23.7	24.0	24.2	24.5	24.7
1191	1.7E-2,20,	21.9	25.8	27.3	28.7	29.3	29.6	30.3
1192		30.3	31.9	32.5	32.8	32.9	33.0	33.2
1193	31.8	32.1	32.5	32.8	32.9	33.0	33.2	33.8
1194	1.7E-1,20,	22.2	25.5	27.9	29.7	31.1	32.5	33.8
1195		33.2	34.2	34.6	35.1	35.6	36.1	36.6
1196	650. ,20,	15.6	24.3	30.9	34.9	38.0	40.4	42.6
1197		42.6	45.0	51.3	52.4	53.4	54.8	55.3
1198	49.0	50.9	51.9	52.6	53.8	54.3	55.7	56.3
1199	SSR2 373.,C,,3,20							
1200		56.3	57.1	57.9	58.7	59.5	59.9	59.9
		60.0	60.7	61.4	62.1	62.8	63.5	63.8
1201	0.01,0.02,0.03,0.04,0.05,0.06,0.07,0.08,0.09,0.10,							
1202	0.11,0.12,0.13,0.14,0.15,0.16,0.17,0.18,0.19,0.20							
1203	8.3E-4,20,	16.2	18.5	19.7	20.6	21.2	21.7	22.0
1204		22.5	22.5	22.5	22.5	22.5	22.5	22.9
1205								

1	2	3	4	5	6	7	8
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## Appendix G (Continued)

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DATA      1   2   3   4   5   6   7   8
SER. NO. ----5---0---5---0---5---0---5---0---5---0---5---0---5---0---5---0---5---0
1201          23.2 23.5 23.5 23.6 23.8 23.9 23.9 24.1 24.4 24.2
1202          1.7E-2,20, 21.5 24.2 26.0 27.5 28.7 29.6 30.5 31.3 31.9 32.5
1203          33.1 33.5 33.8 34.1 34.5 34.6 34.6 34.9 34.9 34.9
1204          1.7E-1,20, 22.2 25.3 27.6 29.6 31.2 32.4 33.3 34.4 35.3 36.2
1205          37.1 37.8 38.2 38.7 39.3 39.9 40.3 40.6 41.2 41.7
1206 SSR2 293.,C,,8,20
1207          0.01,0.02,0.03,0.04,0.05,0.06,0.07,0.08,0.09,0.10,
1208          0.11,0.12,0.13,0.14,0.15,0.16,0.17,0.18,0.19,0.20
1209          1.7E-4,20, 16.3 18.6 20.3 21.6 23.1 24.1 24.9 26.1 26.7 27.5
1210          28.2 29.0 29.3 29.6 30.2 30.4 30.8 31.3 31.6 31.8
1211          2.9E-4,16, 17.9 22.5 25.7 26.9 27.5 29.1 30.2 31.2 31.9 32.6
1212          33.3 35.9 34.4 34.9 35.2 35.5
1213          1.6E-2,18, 18.4 24.0 27.1 28.7 30.3 31.7 33.1 33.9 34.7 35.5
1214          36.0 36.5 37.0 37.5 37.9 38.4 38.9 39.1
1215          1.7E-2,20, 21.0 26.9 29.5 31.3 32.4 33.7 35.0 36.0 37.1 37.7
1216          38.5 39.2 39.5 40.1 40.9 41.3 41.6 42.3 42.7 42.9
1217          1.7E-1,20, 21.4 25.1 28.2 30.5 32.8 34.4 36.3 37.7 39.1 40.3
1218          41.4 42.1 43.2 44.2 45.3 46.0 46.9 47.5 48.3 48.9
1219          0.80 ,18, 22.6 26.1 29.5 32.2 34.3 36.0 37.7 38.4 39.4 40.1
1220          40.9 41.6 42.1 42.7 43.6 44.0 44.4 44.6
1221          42.0, ,15, 24.7 29.3 34.7 36.8 38.9 40.6 41.6 42.7 43.9 44.8
1222          45.3 45.9 46.5 46.8 47.2
1223          65.0, ,20, 32.8 38.1 42.0 45.9 48.7 50.9 53.1 54.7 56.1 57.3
1224          58.2 59.4 60.2 61.0 62.3 62.8 63.6 64.2 65.0 65.4
1225 SSR2 233.,C,,4,20
1226          0.01,0.02,0.03,0.04,0.05,0.06,0.07,0.08,0.09,0.10,
1227          0.11,0.12,0.13,0.14,0.15,0.16,0.17,0.18,0.19,0.20
1228          B.3E-4,20, 18.5 21.8 24.3 26.1 27.4 28.7 29.5 30.2 31.1 31.8
1229          32.5 33.1 33.7 34.2 34.8 35.5 35.8 36.3 36.5 36.9
1230          1.7E-2,20, 24.3 29.7 32.3 34.1 35.4 36.1 37.3 38.2 38.9 39.5
1231          40.2 40.8 41.1 41.7 42.1 42.4 42.7 43.5 43.8 44.0
1232          1.7E-1,20, 23.4 27.8 30.9 33.2 35.4 37.3 39.0 40.5 41.9 43.0
1233          44.1 45.3 46.5 47.6 48.7 49.4 50.2 51.1 51.6 52.5
1234          65.0, ,20, 33.7 38.2 42.3 46.0 49.0 51.6 54.0 55.4 57.1 58.7
1235          60.0 61.2 62.5 63.4 64.3 65.2 65.9 66.8 67.3 67.7
1236 *
1237 MAT 'PB6'          3019,0,0,0,0,4
1238 0. 0. 0. 0.
1239 REF 1 'R-85'
1240 COM 'KAHANAWA UNIVERSITY TEST DATA'
1241 SSR2 423.,C,,4,20
1242          0.01,0.02,0.03,0.04,0.05,0.06,0.07,0.08,0.09,0.10,
1243          0.11,0.12,0.13,0.14,0.15,0.16,0.17,0.18,0.19,0.20
1244          8.3E-4,20, 19.5 21.9 23.0 23.8 24.3 24.8 25.4 25.9 26.0 26.4
1245          26.7 27.0 27.0 27.3 27.4 27.6 27.7 27.8 27.8 27.8
1246          1.7E-2,20, 24.4 27.8 29.2 30.1 30.9 31.6 32.1 32.7 32.9 33.4
1247          33.5 33.9 34.2 34.5 34.6 34.8 34.7 34.9 34.8 34.8
1248          1.7E-1,20, 25.4 29.4 31.9 33.2 34.9 36.1 37.2 37.9 38.7 39.3
1249          40.2 41.1 41.7 42.3 43.1 43.5 43.7 44.2 44.4 44.7
1250          65.0, ,20, 26.8 33.7 38.1 41.7 44.3 46.8 48.7 50.6 52.1 53.0
-----5----0----5----0----5----0----5----0----5----0----5----0----5----0
1         2         3         4         5         6         7         8

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## Appendix G (Continued)

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DATA      1   2   3   4   5   6   7   8
SEQ. NO. ----5---0---5---0---5---0---5---0---5---0---5---0---5---0---5---0
1251          54.2 55.1 55.7 56.2 56.8 57.4 57.7 58.4 58.8 59.2
1252 SSR2 373.,C,,3,20
1253          0.01,0.02,0.03,0.04,0.05,0.06,0.07,0.08,0.09,0.10,
1254          0.11,0.12,0.13,0.14,0.15,0.16,0.17,0.18,0.19,0.20
1255          B.3E-4,20, 19.6 23.8 24.9 25.9 26.2 26.6 27.0 27.3 27.4
1256          27.6 28.0 28.1 28.3 28.7 28.9 29.0 29.3 29.4 29.5
1257          1.7E-2,20, 24.0 27.1 29.1 30.4 31.4 32.5 33.1 33.9 34.3 34.8
1258          35.1 35.6 35.9 36.1 36.3 36.3 36.9 36.8 37.2 37.1
1259          1.7E-1,20, 26.0 30.5 32.9 34.7 36.5 37.4 38.3 39.4 40.1 41.4
1260          42.1 42.8 43.4 43.9 44.5 45.0 45.5 45.9 46.5 46.8
1261 SSR2 293.,C,,8,20
1262          0.01,0.02,0.03,0.04,0.05,0.06,0.07,0.08,0.09,0.10,
1263          0.11,0.12,0.13,0.14,0.15,0.16,0.17,0.18,0.19,0.20
1264          1.7E-4,20, 18.2 21.0 23.2 24.4 25.6 26.6 27.7 28.7 29.3 30.3
1265          30.9 31.7 31.9 32.4 32.9 33.1 33.6 34.0 34.4 34.8
1266          3.0E-4,16, 19.7 22.1 25.2 26.4 27.4 28.1 28.8 29.4 30.0 30.6
1267          31.2 31.8 32.3 33.0 33.7 34.5
1268          1.7E-2,20, 21.9 26.9 29.0 31.1 32.6 33.7 34.7 35.8 36.8 37.4
1269          37.9 38.1 39.2 39.9 40.3 40.5 41.0 41.6 41.6 41.9
1270          1.7E-2,20, 26.3 30.1 32.2 34.0 35.6 36.8 37.1 39.0 40.1 41.0
1271          41.9 42.7 43.4 44.1 44.8 45.3 46.0 46.6 47.1 47.5
1272          1.7E-1,20, 28.4 33.3 36.5 38.0 39.4 40.7 42.2 43.7 44.6 45.8
1273          46.4 47.1 48.2 49.0 49.8 50.5 51.3 52.0 53.1 53.9
1274          0.89 ,20, 23.3 27.1 31.9 33.9 35.9 36.8 37.9 39.0 40.0 40.9
1275          41.6 42.1 42.9 43.7 44.1 44.7 44.9 45.3 45.4 45.6
1276          41.0, ,17, 25.2 31.7 36.7 39.3 41.9 43.1 44.8 46.2 47.2 48.3
1277          49.6 50.2 51.2 51.9 52.5 52.8 53.3
1278          65.9 67.1 67.9 68.9 70.1 70.7 71.6 72.5 73.3 74.1
1279 SSR2 233.,C,,4,20
1280          0.01,0.02,0.03,0.04,0.05,0.06,0.07,0.08,0.09,0.10,
1281          0.11,0.12,0.13,0.14,0.15,0.16,0.17,0.18,0.19,0.20
1282          B.3E-4,20, 24.3 27.4 30.2 32.0 33.5 34.6 35.9 36.6 37.3 38.1
1283          38.5 39.0 39.9 39.7 40.2 40.5 41.1 41.5 41.9 42.2
1284          1.7E-2,20, 30.1 34.5 37.7 39.8 41.2 42.6 43.5 44.2 45.1 46.0
1285          46.8 47.6 48.2 48.6 49.2 49.9 50.3 50.6 51.3 51.7
1286          1.7E-1,20, 33.2 37.9 40.5 43.0 45.2 46.8 48.5 49.6 50.8 51.7
1287          52.7 53.5 54.4 55.0 55.9 56.5 57.1 57.7 58.2 58.7
1288          65.0, ,20, 41.1 45.9 50.6 54.9 58.2 60.4 62.7 64.8 66.5 67.7
1289          69.1 70.2 71.0 72.0 72.9 73.7 74.2 75.0 75.6 75.7
1290
1291 *
1292 MAT 'LEAD'          3100,4,0,0,0,0
1293 29.0E-6, 16100, 5590, ,0.44
1294 29.0E-6, 291. ,29.1E-6, 373., 30.0E-6, 473., 31.3E-6, 573.
1295 *
1296 MAT 'DARK'          4001,0,0,0,0,3
1297 0. 0. 0. 0.
1298 REF 1 'R-41'
1299 SSR 293.,C,0,1
1300 1.0E-4,11, 0.01 9.8, 0.02 47.9, 0.03 49.8, 0.041 49.8
-----5----0----5----0----5----0----5----0----5----0----5----0----5----0
1         2         3         4         5         6         7         8

```

## Appendix G (Continued)

DATA SEQ. NO.	1	2	3	4	5	6	7	8
1301	0.051	49.8	0.105	50.7	0.163	52.3	0.223	53.9
1302	0.357	60.5	0.511	75.7	0.693	99.0		
1303	SSR	293.,C,45,1						
1304	1.0E-4,11,	0.01	0.78	0.02	3.53	0.03	9.22	0.041
1305		12.8		0.051	15.4	0.105	21.0	0.163
1306				0.24.5		0.223	28.4	
1307	SSR	293.,C,90,1						
1308	1.0E-4,12,	0.01	0.69	0.02	3.53	0.03	5.49	0.041
1309		6.28		0.051	6.77	0.105	8.43	0.163
1310				9.41		0.223	10.4	
1311	*							
1312	MAT	'OAK'	4002,0,0,0,0,3					
1313	0.	0.	0.	0.				
1314	REF	1	'R-41'					
1315	COM	'9 M FALL	,					
1316	SSR	293.,C,0,1						
1317	+1.E-2,11,	0.02	22.3	0.041	50.8	0.062	71.8	0.105
1318				69.5		0.288	80.2	0.357
1319					0.431	77.6	0.511	80.2
1320	SSR	293.,C,45,1						
1321	+1.E-2,12,	0.02	6.96	0.041	33.7	0.062	39.2	0.105
1322				31.7		0.288	34.3	0.357
1323					0.431	35.8	0.511	42.4
1324	SSR	293.,C,90,1						
1325	+1.E-2,13,	0.02	1.37	0.041	15.2	0.062	16.1	0.105
1326				14.2		0.288	16.1	0.357
1327					0.431	20.5	0.511	21.4
1328						0.693	28.5	0.92
1329	*							
1330	MAT	'PLYWOOD'	4003,0,0,0,0,3					
1331	0.	0.	0.	0.				
1332	REF	1	'R-41'					
1333	SSR	293.,C,0,1						
1334	1.0E-4,11,	0.01	0.294	0.02	0.588	0.03	2.45	0.041
1335				4.31		0.288	34.3	0.223
1336					0.357	19.6	0.511	32.2
1337	SSR	293.,C,45,1						
1338	1.0E-4,13,	0.01	2.45	0.02	10.9	0.03	19.6	0.041
1339				21.0		0.288	22.1	0.105
1340					0.357	25.6	0.511	27.9
1341						0.693	28.5	0.92
1342	SSR	293.,C,90,1						
1343	1.0E-4,13,	0.01	2.45	0.02	19.6	0.03	21.1	0.041
1344				20.7		0.288	22.1	0.105
1345					0.357	22.5	0.511	23.4
1346						0.693	27.1	0.92
1347	*							
1348	MAT	'PLYWOOD'	4004,0,0,0,0,3					
1349	0.	0.	0.	0.				
1350	REF	1	'R-41'					
1351								
1352								
1353								
1354								
1355								
1356	SSR	293.,C,45,1						
1357	+1.E-2,13,	0.02	1.96	0.041	4.9	0.062	10.7	0.083
1358				24.0		0.288	10.5	0.123
1359					0.357	22.1	0.511	27.9
1360						0.693	28.5	0.92
1361	SSR	293.,C,90,1						
1362	+1.E-2,13,	0.02	0.88	0.041	7.16	0.062	12.1	0.083
1363				17.4		0.288	12.3	0.123
1364					0.357	23.0	0.511	31.2
1365						0.693	32.2	0.92
1366	*							
1367	MAT	'BALSA'	4005,0,0,0,0,1					
1368	0.	0.	0.	0.				
1369	REF	1	'R-42'					
1370	COM	'SPECIFIC GRAVITY 0.17'						
1371	SSR	293.,C,90,1						
1372	1.0E-4, 4,	0.1	1.0	0.2	1.2	0.3	1.6	0.4
1373	*							
1374	MAT	'BALSA'	4006,0,0,0,0,1					
1375	0.	0.	0.	0.				
1376	REF	1	'R-42'					
1377	COM	'SPECIFIC GRAVITY 0.18'						
1378	SSR	293.,C,90,1						
1379	1.1E+2, 4,	0.1	3.3	0.2	2.9	0.3	2.8	0.4
1380	*							
1381	MAT	'BALSA'	4007,0,0,0,0,1					
1382	0.	0.	0.	0.				
1383	REF	1	'R-42'					
1384	COM	'SPECIFIC GRAVITY 0.18'						
1385	SSR	293.,C,90,1						
1386	1.1E+2, 4,	0.1	2.0	0.2	2.1	0.3	2.5	0.4
1387	*							
1388	MAT	'BALSA'	4008,0,0,0,0,2					
1389	0.	0.	0.	0.				
1390	REF	1	'R-42'					
1391	COM	'SPECIFIC GRAVITY 0.20'						
1392	SSR	293.,C,45,2						
1393	1.0E-4, 4,	0.1	3.2	0.2	3.6	0.3	4.0	0.4
1394				4.6		0.223	4.4	0.3
1395	SSR	293.,C,90,1						
1396	1.1E+2, 4,	0.1	5.5	0.2	6.4	0.3	7.4	0.4
1397	*							
1398	MAT	'BALSA'	4009,0,0,0,0,1					
1399	0.	0.	0.	0.				
1400	REF	1	'R-42'					
1401								

DATA SEQ. NO.	1	2	3	4	5	6	7	8
1351	COM	'9 M FALL	,					
1352	SSR	293.,C,0,1						
1353	+1.E-2,11,	0.02	2.26	0.041	5.79	0.062	9.81	0.083
1354			0.128	11.8	0.174	15.2	0.223	15.2
1355				0.357	30.3	0.511	46.4	0.693
1356	SSR	293.,C,45,1						
1357	+1.E-2,13,	0.02	1.96	0.041	4.9	0.062	10.7	0.083
1358			0.105	27.2	0.128	27.2	0.174	27.2
1359				0.357	32.3	0.511	33.0	0.693
1360					0.92	49.4	0.92	
1361	SSR	293.,C,90,1						
1362	+1.E-2,13,	0.02	0.88	0.041	7.16	0.062	12.1	0.083
1363			0.128	32.3	0.174	29.4	0.223	29.4
1364				0.357	25.0	0.511	31.2	0.693
1365					0.92	40.1	0.92	
1366	*							
1367	MAT	'BALSA'	4005,0,0,0,0,1					
1368	0.	0.	0.	0.				
1369	REF	1	'R-42'					
1370	COM	'SPECIFIC GRAVITY 0.17'						
1371	SSR	293.,C,90,1						
1372	1.0E-4, 4,	0.1	1.0	0.2	1.2	0.3	1.6	0.4
1373	*							
1374	MAT	'BALSA'	4006,0,0,0,0,1					
1375	0.	0.	0.	0.				
1376	REF	1	'R-42'					
1377	COM	'SPECIFIC GRAVITY 0.18'						
1378	SSR	293.,C,90,1						
1379	1.1E+2, 4,	0.1	3.3	0.2	2.9	0.3	2.8	0.4
1380	*							
1381	MAT	'BALSA'	4007,0,0,0,0,1					
1382	0.	0.	0.	0.				
1383	REF	1	'R-42'					
1384	COM	'SPECIFIC GRAVITY 0.18'						
1385	SSR	293.,C,90,1						
1386	1.1E+2, 4,	0.1	2.0	0.2	2.1	0.3	2.5	0.4
1387	*							
1388	MAT	'BALSA'	4008,0,0,0,0,2					
1389	0.	0.	0.	0.				
1390	REF	1	'R-42'					
1391	COM	'SPECIFIC GRAVITY 0.20'						
1392	SSR	293.,C,45,2						
1393	1.0E-4, 4,	0.1	3.2	0.2	3.6	0.3	4.0	0.4
1394			0.223	4.4	0.3	4.4	0.4	8.3
1395	SSR	293.,C,90,1						
1396	1.1E+2, 4,	0.1	5.5	0.2	6.4	0.3	7.4	0.4
1397	*							
1398	MAT	'BALSA'	4009,0,0,0,0,1					
1399	0.	0.	0.	0.				
1400	REF	1	'R-42'					
1401								

## Appendix G (Continued)

DATA SEQ. NO.	1	2	3	4	5	6	7	8
1401	COM 'SPECIFIC GRAVITY 0.21'							
1402	SSR 293.,C,0,1							
1403	1.0E-4, 4, 0.1 14.7, 0.2 14.9, 0.3 15.2, 0.4 15.7							
1404	*							
1405	MAT 'BALSA' 4010,0,0,0,1							
1406	0. 0. 0. 0.							
1407	REF 1 'R-42'							
1408	COM 'SPECIFIC GRAVITY 0.21'							
1409	SSR 293.,C,0,1							
1410	1.0E-4, 4, 0.1 14.0, 0.2 14.1, 0.3 14.4, 0.4 14.9							
1411	*							
1412	MAT 'BALSA' 4011,0,0,0,2							
1413	0. 0. 0. 0.							
1414	REF 1 'R-42'							
1415	COM 'SPECIFIC GRAVITY 0.25'							
1416	SSR 293.,C,0,1							
1417	1.1E+2, 4, 0.1 22.3, 0.2 22.1, 0.3 21.9, 0.4 21.7							
1418	SSR 293.,C,45,1							
1419	1.3E+2, 4, 0.1 8.1, 0.2 9.5, 0.3 10.9, 0.4 12.3							
1420	*							
1421	MAT 'BALSA' 4012,0,0,0,3							
1422	0. 0. 0. 0.							
1423	REF 1 'R-42'							
1424	COM 'SPECIFIC GRAVITY 0.26'							
1425	SSR 293.,C,90,2							
1426	1.0E-4, 4, 0.1 2.2, 0.2 2.8, 0.3 3.4, 0.4 4.5							
1427	1.3E+2, 4, 0.1 5.1, 0.2 5.9, 0.3 6.8, 0.4 7.8							
1428	SSR 293.,C,45,1							
1429	1.0E-4, 4, 0.1 4.9, 0.2 5.8, 0.3 6.7, 0.4 7.8							
1430	SSR 293.,C,0,1							
1431	1.0E-4, 4, 0.1 19.1, 0.2 20.1, 0.3 21.1, 0.4 22.2							
1432	*							
1433	MAT 'BALSA' 4013,0,0,0,1							
1434	0. 0. 0. 0.							
1435	REF 1 'R-42'							
1436	COM 'SPECIFIC GRAVITY 0.26'							
1437	SSR 293.,C,0,1							
1438	1.0E-4, 4, 0.1 22.3, 0.2 21.8, 0.3 21.5, 0.4 21.2							
1439	*							
1440	MAT 'BALSA' 4014,0,0,0,1							
1441	0. 0. 0. 0.							
1442	REF 1 'R-42'							
1443	COM 'SPECIFIC GRAVITY 0.26'							
1444	SSR 293.,C,45,1							
1445	1.0E-4, 4, 0.1 3.3, 0.2 5.6, 0.3 7.9, 0.4 10.4							
1446	*							
1447	MAT 'BALSA' 4015,0,0,0,4							
1448	0. 0. 0. 0.							
1449	REF 1 'R-44'							
1450	COM 'SPECIFIC GRAVITY 0.09'							

----5----0----5----0----5----0----5----0----5----0----5----0----5----0

DATA SEQ. NO.	1	2	3	4	5	6	7	8
1451	SSR 293.,C, 0,1							
1452	1.0E-4, 7, 0.02 4.16, 0.1 4.59, 0.2 4.60, 0.3 4.61, 0.4 4.60,							
1453	0.5 4.60, 0.6 4.56							
1454	SSR 293.,C,45,1							
1455	1.0E-4, 7, 0.02 0.54, 0.1 0.91, 0.2 0.99, 0.3 1.05, 0.4 1.13,							
1456	0.5 1.27, 0.6 1.51							
1457	SSR 293.,C,60,1							
1458	1.0E-4, 7, 0.02 0.38, 0.1 0.60, 0.2 0.66, 0.3 0.69, 0.4 0.77,							
1459	0.5 0.86, 0.6 1.01							
1460	SSR 293.,C,90,1							
1461	1.0E-4, 7, 0.02 0.25, 0.1 0.44, 0.2 0.47, 0.3 0.50, 0.4 0.55,							
1462	0.5 0.60, 0.6 0.66							
1463	*							
1464	MAT 'BALSA' 4016,0,0,0,1							
1465	0. 0. 0. 0.							
1466	REF 1 'R-44'							
1467	COM 'SPECIFIC GRAVITY 0.18'							
1468	SSR 293.,C, 0,1							
1469	1.0E-4, 7, 0.02 10.4, 0.1 10.9, 0.2 10.95, 0.3 10.94, 0.4 10.9,							
1470	0.5 10.7, 0.6 10.7							
1471	*							
1472	MAT 'BALSA' 4017,0,0,0,1							
1473	0. 0. 0. 0.							
1474	REF 1 'R-44'							
1475	COM 'SPECIFIC GRAVITY 0.31'							
1476	SSR 293.,C, 0,1							
1477	1.0E-4, 7, 0.02 22.19, 0.1 22.6, 0.2 22.5, 0.3 22.5, 0.4 22.4,							
1478	0.5 22.3, 0.6 21.3							
1479	*							
1480	MAT 'BALSA' 4018,0,0,0,1							
1481	0. 0. 0. 0.							
1482	REF 1 'R-49'							
1483	COM 'SPECIFIC GRAVITY 0.22'							
1484	SSR 293.,C,90,1							
1485	+1.E-2, 8, 0.01 0.776, 0.02 1.34, 0.05 2.05, 0.11 2.29, 0.22 2.35,							
1486	0.36 2.40, 0.51 2.35, 0.69 2.45, 0.92 2.67							
1487	*							
1488	MAT 'BALSA' 4019,0,0,0,1							
1489	0. 0. 0. 0.							
1490	REF 1 'R-49'							
1491	COM 'SPECIFIC GRAVITY 0.22'							
1492	SSR 293.,C, 0,1							
1493	+1.E-2, 8, 0.02 7.7, 0.04 15.1, 0.06 22.1, 0.08 27.4, 0.16 23.8,							
1494	0.29 20.2, 0.36 18.2, 0.43 14.1							
1495	*							
1496	MAT 'BALSA' 4020,0,0,0,1							
1497	0. 0. 0. 0.							
1498	REF 1 'R-49'							
1499	COM 'SPECIFIC GRAVITY 0.22'							
1500	SSR 293.,C, 0,1							

----5----0----5----0----5----0----5----0----5----0----5----0----5----0

## Appendix G (Continued)

DATA SEQ. NO.	1	2	3	4	5	6	7	8												
1501	1.0E-4,13,	0.02	7.7,	0.04	15.1,	0.06	22.1,	0.08	27.4,	0.16	23.8,									
1502											0.29	20.0,	0.36	18.4,	0.43	16.6,	0.51	14.1,	0.60	10.8,
1503											0.69	8.25,	0.74	7.54,	0.80	7.06				
1504	*																			
1505	MAT 'BALSA'																			
1506		4021,0,0,0,1																		
1507	O. O. O.																			
1508	REF 1 'R-49'																			
1509	COM 'SPECIFIC GRAVITY 0.22'																			
1510	SSR 293.,C,0,1																			
1511		+1.E-2,15,	0.02	7.7,	0.04	15.1,	0.06	22.1,	0.08	27.4,	0.16	23.2,								
1512																				
1513																				
1514	MAT 'BALSA'																			
1515		4022,0,0,0,1																		
1516	O. O. O.																			
1517	REF 1 'R-49'																			
1518	COM 'SPECIFIC GRAVITY 0.22'																			
1519	SSR 293.,C,90,1																			
1520		+1.E-2, 9,	0.01	0.776,	0.02	1.34,	0.05	2.05,	0.11	2.29,	0.22	2.20,								
1521																				
1522	MAT 'BALSA'																			
1523		4023,0,0,0,1																		
1524	O. O. O.																			
1525	REF 1 'R-49'																			
1526	COM 'SPECIFIC GRAVITY 0.22'																			
1527	SSR 293.,C,90,1																			
1528		+1.E-2, 9,	0.01	0.776,	0.02	1.34,	0.05	2.05,	0.11	2.29,	0.22	2.20,								
1529																				
1530	MAT 'PLYWOOD'																			
1531		4100,0,0,0,0																		
1532	1.0E-6,	18.0,	7.1,	0.26																
1533	*																			
1534	END																			
1535	MAT 'SUS304'																			
1536		2033,0,0,0,2																		
1537	O. O. O.																			
1538	REF 1 'R-51'																			
1539	COM 'NI B.90,CR 18.63,C 0.08,SI 0.71,MN 1.67,P 0.028,S 0.008'																			
1540	SSR 293.,T,,14																			
1541		1.000E-4 ,1,	0.002	196.																
1542		1.010E-4 ,1,	0.009	375.																
1543		9.8 ,1,	0.019	453.																
1544		5.8E+1 ,1,	0.028	504.																
1545		1.7E+2 ,1,	0.058	572.																
1546		3.5E+2 ,1,	0.110	674.																
1547		4.0E+2 ,1,	0.162	783.																
1548		4.95E+2,1,	0.209	845.																
1549		5.81E+2,1,	0.295	1000.																
1550		5.83E+2,1,	0.252	918.																
1551		5.92E+2,1,	0.418	1165.																
1552		5.95E+2,1,	0.380	1116.																
1553	*																			
1554	END																			
1555																				
1556																				
1557																				
1558																				
1559																				
1560																				
1561																				

DATA SEQ. NO.	1	2	3	4	5	6	7	8
1551	5.97E+2,1,	0.341	1067.					
1552	8.29E+2,1,	0.450	1203.					
1553	SSR 673.,T,,6							
1554	1.000E-4, 1,	0.110	379.					
1555	1.001E-4, 1,	0.162	457.					
1556	1.002E-4, 1,	0.209	493.					
1557	7.4 , 1,	0.295	561.					
1558	7.5 , 1,	0.063	295.					
1559	9.3 , 1,	0.256	528.					
1560	*							
1561	END							