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照射履歴に従った燃料ペレット-被覆管ギャップ

熱伝達解析プログラムFREG-3の入力手引

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照射履歴に従った燃料ペレット-被覆管ギャップ
熱伝達解析プログラム FREG-3の入力手引

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この報告書は、プログラム FREG-3 のプログラム概要と使用手引である。FREG-3 を使用する場合に必要な入力の書式および出力形式について説明している。

FREG-3 は、燃料棒内の温度分布およびそれに基づく蓄積熱量の計算を行う。この計算は、通常運転状態下の温度分布の安全性評価を行うものであるが、燃料棒の照射履歴に従って温度分布を求めることができる。プログラムに必要な物性値およびモデルは、組みあるいは入力形式のオプションになっており、これらオプションは key word によって切換が可能になっている。オプションの選択によって、安全性評価用ばかりでなく最良推定値用プログラムとしても使用できると考える。

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User's guide for FREG-3: A computer program to analyze pellet-cladding gap conductance in accordance with fuel-rod irradiation history

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The present report describes user's manual for program FREG-3, and provides a general description of the program and instructions of input/output.

FREG-3 estimates the temperature distribution in a fuel rod and the stored energy based on the distribution. The temperature distribution is calculated in accordance with fuel-rod irradiation history.

Mechanical properties and models in handling specific problems, such as densification and relocation, are optional in the program. The options are to be given by key word. If appropriate options are selected, the program is used not only as a safety evaluation code, but also as a best evaluation code.

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1. はじめに

この報告書は、プログラム FREG-3 の使用手引である。FREG-3 の計算方法の詳細については、別の報告書にまとめる予定しているので、この報告書では FREG-3 を使用する場合に必要な入力の書式および出力型式等について説明する。⁶⁾

FREG-3 は燃料棒内の温度分布およびそれに基づく蓄積熱量の計算を行う。この計算は、通常運転状態下の温度分布を求めるものであるが、燃料棒の照射履歴（出力、冷却水温度と冷却水圧力の変化）に従って温度分布を求めることができる。

燃料棒の安全性を評価する場合、燃料ペレットの最高温度および燃料棒に蓄えられる蓄積熱量 (stored energy) が問題となる。

燃料ペレット温度が、ペレットの溶融温度 (UO_2 の場合約 2800°C) 以上になると、ペレットの相変化に伴う体積の膨張および温度上昇に伴う核分裂生成ガスの放出による燃料棒内圧の上昇のため燃料被覆管の破損が考えられる。このため、安全性上、燃料ペレットの最高温度が、ペレットの溶融温度以下になるよう燃料棒は設計、使用される。

LOCA (Loss of Coolant Accident: 冷却材喪失事故) 状態において、燃料棒からの熱除去能力が極端に低下する。核分裂生成物の崩壊熱および LOCA 直前に蓄えられていたペレットの蓄積熱量のため、被覆管の温度は上昇する。軽水炉に使用されるジルコニウム合金被覆管は、冷却材喪失事故時に、著しく変化して燃料棒がくずれ落ちるとかあるいは燃料棒内の内圧上昇によって被覆管が著しくふくれる等の現象を提すると考えられる。この現象は緊急炉心冷却系 (ECCS) から供給される冷却水の流れを防げる、すなわち coolable geometry (炉心の冷却可能な形状) の確保を困難にするおそれがある。

coolable geometry が保持できるか否かは、ECCS の性能によって支配される。しかし、事故発生直前における燃料棒の運転状態、とりわけ燃料棒内の温度分布（燃料棒内蓄積エネルギー）と燃料棒内ガス圧力は、事故の初期条件を与える重要な事項である。

事故後の被覆管温度上昇に寄与する被覆管表面熱伝達、崩壊熱と事故直前の温度分布等のうち燃料棒に関して、われわれが何らかの形である程度コントロールしうるものは蓄積熱量のみである。すなわち、ギャップ寸法の選択、出力の変更等によって蓄積熱量をコントロールすることが可能である。

したがって、燃料棒使用の安全性上ペレットの最高温度ならびに蓄積熱量を、出来る限り正確に評価することが望まれる。この最高温度および蓄積熱量の評価には、燃料棒内の温度分布の解析が必要不可欠である。さらに温度分布を決定する最大の要因は、ペレット表面と被覆管内面間のギャップ熱伝達である。温度分布を評価するということは、いかにギャップ熱伝達率を求めるかという作業にかゝっていると云つて過言ではない。

ギャップ熱伝達係数の評価を含めて、燃料棒内の温度分布を評価する目的の計算機用プログラムが種々開発された。特に、 UO_2 ペレットの温度上昇の安全性評価プログラムとして、¹⁾ GAPCON, ²⁾ GAPCON-THERMAL-1, ^{3),4)} GAPCON-THERMAL-2 が公開されている。

プログラム GAPCON, GAPCON-THERMAL-1 は、燃料棒の一定出力下での燃焼度の増加による温度分布の変化しか計算できない。GAPCON-THERMAL-2 は、出力の変化に

ついて照射履歴が追えるようになっているが、その他のパラメータ（冷却水圧力、温度）は一定値で変化させることができない。また、単位にインチ系、メートル系が混存したり、BWR燃料棒の計算を行うと最高温度が著しく高くなり非現実的過ぎる等の点がある。

プログラム FREG-3は、GAPCON-THERMAL-1を改造、修正したものである。主たる改造は、時間（あるいは燃焼度）に従う出力、冷却水温度、冷却水圧力の変化すなわち燃料棒の照射履歴に伴う燃料棒内温度分布を計算できるようにしたことである。また、主な修正は、単位系の整理、BWR燃料棒の計算を行っても妥当な結果がえられるようにしたことである。さらに、燃料ペレット、被覆管の物性値の計算式の追加、スウェーリング、ギャップに対するペレットクラックの効果、焼しまり等のモデルが追加されている。これらの計算式、モデルはすべてオプション形式となっていて、key wordにより使用者が選択できる。これらオプションを適切に選択することによって、FREG-3は安全性評価用としてばかりでなく、最良推定用プログラムとしても使用できると考える。

FREG-3は、一定出力のもとで燃焼度増加の温度分布を計算するGAPCON-THERMAL-1を照射履歴に追従して計算するようにしたため、計算上かなり無理な点が生じた。そのような点（出力の半径と軸方向分布、プレナム温度等）については、照射履歴に追従して変更が可能ないようにオプションを追加した。また、長期間の照射によって変化すると考えられるパラメータ、例えば半径と軸方向の出力分布等を照射履歴に従って変更できるようになっている。

2. プログラム概要

FREG-3は、燃料棒のペレットスタックに相当する部分を軸方向に被覆管を含め最大20等分割、ペレット半径を50等分割して計算を進める。被覆管は、軸方向に上記の通り20等分割であるが、半径方向には1領域と考える。さらに、これら分割された領域の上部にプレナムがあると考えている。

温度分布を求めるにさいし、軸方向に分割された領域（FREG-3ではこの領域をセグメントと称する）では、軸方向の熱流を無視した定常熱伝導方程式が成立すると仮定する。

燃料棒内の温度を計算する場合、重要なkey parameterはギャップ熱伝達率である。⁵⁾ FREG-3のギャップ熱伝達評価の基本式は、修正されたLoss and Stoutの実験式である。Loss and Stoutのギャップ熱伝達率は、接触による熱伝達、ギャップに含まれるガスの熱伝導に基づく熱伝達および輻射による熱伝達から成ると考える。FREG-3は、ガスの熱伝導による熱伝達の評価に力点をおいている。そのため、ギャップに含まれるガスの種類と組成、ギャップ寸法の評価を行う。ガスの種類は、初期封入ガス、製造時にペレットに残留したガスおよび核分裂生成ガスを考慮する。特に、核分裂生成ガスは、Kr, Xeの各同位元素についてchainを考えてその生成量を近似計算で求めている。次に、ガスの組成が計算され混合ガスの熱伝導率が求められる。

一方、ギャップ熱伝達に影響を与えるギャップ寸法については、被覆管内径の変化とペレット外径の変化が考慮される。被覆管内径の変化には、内外圧力による弾性歪、クリープ歪および熱歪を考えている。ペレットの外径の変化には、熱歪およびスウェーリングによる歪を考える外、ペレット焼しまり、クラックおよびその再配置をモデル化してギャップ寸法の算出に入れている。しかし、これらによる変位および歪は、温度計算の目的のためにモデル化されて取入れているもので、これでえられた被覆管応力等については、なお検討を要する点が残っている。FREG-3の計算結果を使用する場合、上記の如き事項を充分念頭に入れて評価されることを希望する。

プログラム全体の流れをFig-1に示す。また、FREG-3に含まれている各Subroutineおよびfunctionの処理内容の概略をTable-1に示す。なおFREG-3のプログラムリストをAppendix-Aに収録しているので参照されたい。

プログラムの流れはFig-1に示す通りである。ギャップ熱伝達係数は、図中の番号16～28の箇所で計算される。この部分がプログラムの主要部分である。通常初期値を1000Btu/hr·ft²·F(0.567w/cm²°C)に設定し、一旦温度分布が求められる(19)，この温度分布に基き、ギャップ寸法およびギャップ熱伝達に影響する諸現象（熱膨張、FPガス放出量等：21～25）を計算し、ギャップ寸法等を評価する。このギャップ寸法、ガスの熱伝達率等を使ってギャップ熱伝達率の再評価が行なわれる(26)。これと仮定値の比較を行う(27)。この計算を収斂するまでくりかえす。

軸方向セグメントの温度計算が終了したら、燃料ペレットスタック全長についての体積平均温度を計算し、これが収斂していれば次のステップに移る。収斂していないければ、これはFPガスの放出量の評価が正しくないので、(22)で計算された放出量を各セグメントについて積

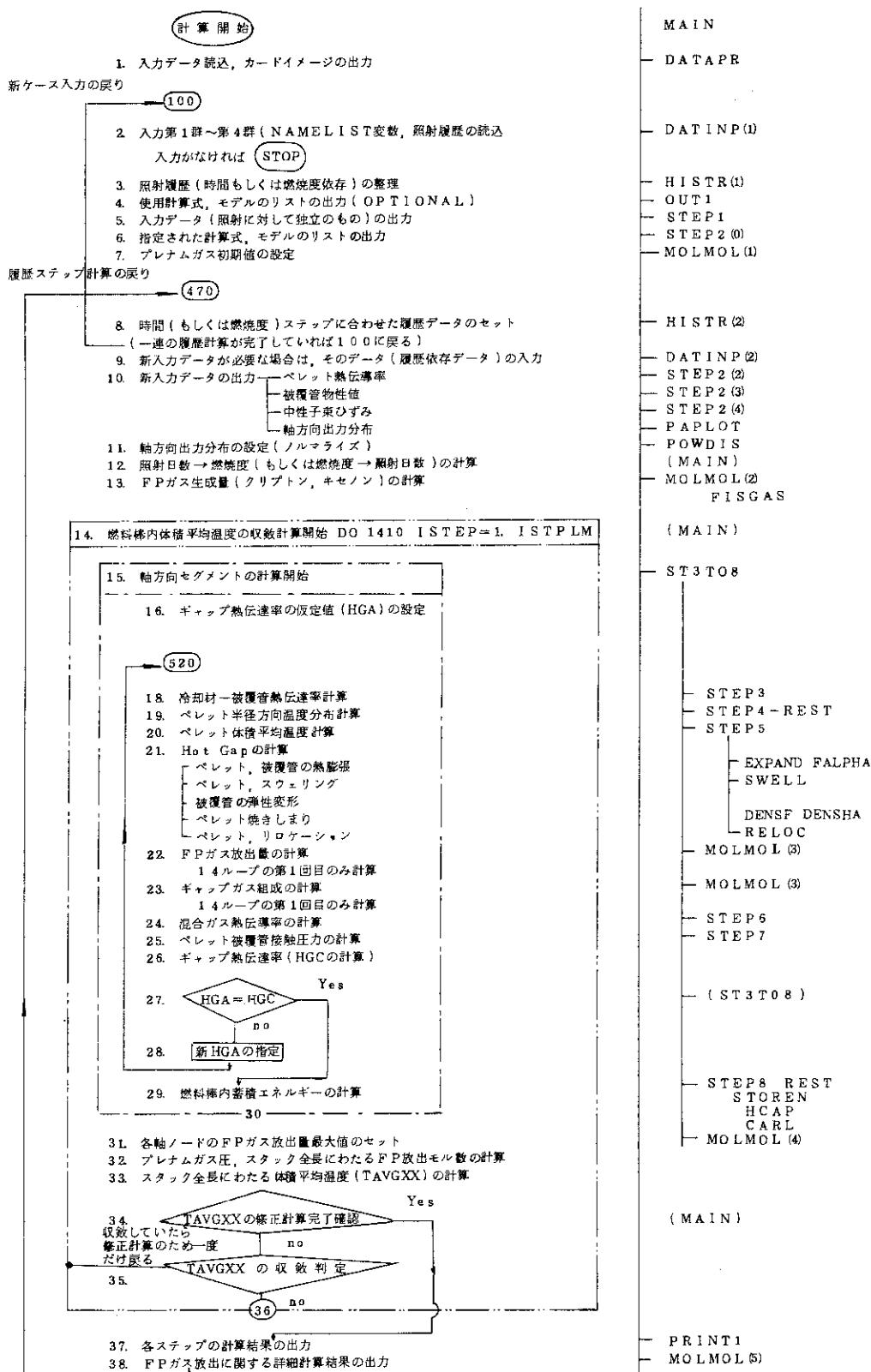


Fig. - 1 FREG-3 計算流れ図

Table-1 FREG-3に含まれる subroutine およびその処理概要

MAIN	プログラム全体を制御する。
CARL	蓄積エネルギーの計算
CHECK(KS)	K S = 1, 2 入力データ相互間の一貫性を調べる。
CREEP	被覆管クリープ変形量計算。 K S = 1 F. P. ガスの Radio - Activity を計算する為の初期値セット K S = 2 Radio - Activity を計算する
DATAPR	入力カードの 80 カラム・イメージをプリントする。
DATA1	計算に必要な定数及び熱的、機械的物性値を設定する。
DATINP(KS)	K S = 1 タイトル、運転履歴に依存しない入力値及び運転履歴データの入力。必要ならばその単位変換をする。 K S = 2 運転履歴に依存するデータを必要に応じ入力する。
DENSF	ペレット Densification 量計算。
DENSHA	HALDEN Densification Model。
DENSGT	GAPCON - THERMAL - 2 Densification Model.
DEPRES	ペレット内熱中性子束歪をベッセル I_0 近似により算出。
ERROR	直線内挿の際、表からはずれたパラメータが与えられたときの警告。
EXPAND	ペレット熱膨張モデル。
FALPHA	ペレット熱膨張係数計算式。
FCOND	ペレット熱伝導率計算式。
F1SGAS	K_r, X_e について核分裂・崩壊 Chain 計算を行ない原子数を求める。
FYIELD	被覆管温度依存 Yield Stress を計算する。
GAPRO	繰返し収斂計算中の Gap Conductance 収斂状況を Line Printer でグラフ化する。打切り回数を越え未収束の場合、必ずプリントされる。
HCAP	UO_2 の比熱計算(温度依存)
HEAD	アウト・プットの各頁のタイトルなどをプリントする。
HISTR(KS)	K S = 1 入力で与えられた運転履歴データを調べ、妥当な出力変動で計算が行なえるよう(定常条件)、履歴を再分割する。 K S = 2 時間ステップが変る度に、必要なパラメータを再設定する。
HICLM	液体金属 - 被覆管 熱伝達係数計算。
HTCW	Dittus - Boelter の式による熱伝達係数計算。
HYOSHI	出力用紙の表紙を作る。
MOLMOL(KS)	K S = 1 初期プレナム・ガスのモル数を計算 K S = 2 各軸方向セグメント毎の F. P. ガス生成量を計算。 照射量の積算。 K S = 3 各軸方向セグメント毎のガス放出率を体積平均温度を用いて表より求め、ガスマル分率計算。

	K S = 4	燃料棒平均温度を求める繰返し計算中の最も妥当なガス・モル分率を求める。
	K S = 5	次のタイム・ステップのF.P. ガス計算初期値セット。軸方向 Elongation によるプレナム圧力計算。
MOLMO4		改良ガス放出モデル（プレナム温度計算を詳細に行なう）
OUT1		このプログラムに用意されている計算式、モデルの一覧表をプリントする。
PAPLOT		入力された軸方向出力分布をライン・プリンターによって図示する。
POWDIS		入力された軸方向出力分布を規格化し、他に入力された平均又はピーク出力に合せる。
PRINT1		計算結果の出力（詳細）
PRINT2		計算結果の出力（簡略）
PROF		半径方向温度分布をライン・プリンタ・によって図示する。
RELOC		ペレット Relocation Model。
STEP 0		計算を行なった日付、時刻をシステムより得る。
STEP 1		計算の初期値を決め、選ばれたオプションに従い入力値をプリントする。
STEP 2 (KS)	K S = 0	主にギャップ・ガスに関する初期状態を決め、他にモデルに関するオプションをプリントする。
	K S = 1	使用していない。
	K S = 2	ペレット熱伝導率の表を変更の指示のある度に出力。
	K S = 3	被覆管物性値の表を "
	K S = 4	ペレット内中性子束歪の表を "
STEP 3		冷却材一被覆管熱伝達係数の計算及び被覆管内温度分布、ペレット外表面温度計算。
STEP 4		ペレット内温度分布、中心孔径（再組織化）の計算
STEP 5 } (STEP5A)		被覆管の弾性変形、熱変形、クリープ変化量、ペレットの熱膨張、Swelling, Densification, Relocationを計算、ホット・ギャップの計算。
STEP 6		ギャップ中のガス伝導率計算。
STEP 7 } (STEP7A)		ギャップ・コンダクタンスの計算。もし接触していれば、その接触圧力の計算。
STEP 8		蓄積エネルギー、燃料棒体積平均温度の計算。
ST3 TO8 (KS)	K S = 1, 2	各軸方向セグメント毎のx方向一次元温度分布、及びギャップ・コンダクタンスを繰返し収斂法により求める。
STOREN		蓄積エネルギー計算。
SWELL } (SWELLA)		Revised Gap Clousier Model.
TEPP		2 - Array 間の直線内挿。
TERP		複数個 Array 間の直線内挿。

算した量を新たな guess としてくりかえし計算を行う。

FREG-3 は、現在 GAPCON-THERMAL-1 と同様各セグメントの体積平均温度によつて FP ガスの放出量を定めている。一方、ギャップ熱伝達がギャップにおけるガスの組成によって変動するので、上記の収斂計算を必要とする。

1～9までは主として入力に関する部分であり、37, 38は出力に関する部分である。

Fig-1 には、左側の計算処理を行つてある subroutine 名を右側に示している。

FREG-3 の入力は、ノートル系とインチ系の両方が使用できる。これは、3.2節で述べる key word KUNIT で切換え使用が可能である。ただし、プログラム内の諸計算は、メートル系に統一されている。

3. 入力手引

FREG-3 の入力データは、カード入力形式で、その第1枚目のカードは、タイトルカードである。FREG-3 は連続計算が可能で、入力カードでタイトルカードから次のタイトルカードまでの計算を“ケース”と呼ぶ。1 計算ケースの中で照射履歴に従って時間あるいは燃焼度を計算に適するように分割した分割点を“ステップ”と云う。ステップは、入力された照射履歴の最初の点を第1ステップとしたシリーズナンバーになる。

3.1 入力データの構成

FREG-3 の入力データは次の8群で構成される。入力データカードの順序もここで記述する順序に従う。Fig-2 にデータ構成および順序を示すので、以下の説明に参照されたい。入力データには最初に読み込まれて初期値の設定に使われるものと計算の進行に伴って読み込まれるものとがある。

また、FREG-3 の入力データをまとめるときのデータシートをTable-2 に示す。このシートは入力計画を作成する場合便利なはずである。

1) TITLE and END card (第1群入力)

このカードは、各計算ケースの入力カード群の最初に必要なTITLEカードである。すべての入力カード群の最後に特定のシグナルをパンチしたカードを付けるとEND cardになる。

このカードは、1枚のカードであり、20A4 のFORMAT形式で読まれる。TITLEカードとして使用する場合は、1～80コラム内に任意の文字をパンチしてよい。ただし、次に述べるENDカードになるシグナルを入れてはならない。TITLEカードの内容は、出力の各頁の第1行に印刷される。

ENDカードとして使用するときのシグナルは、

- i) コラム1～4に“STOP”
- ii) ブランクカード

の2種がある。FREG-3 の入力カードは第1群のTITLEカードから始り第8群で終るいくつかの計算ケースの入力カード群と最後のENDカードによって構成される。

2) MAIN NAMELIST DATA card (第2群入力)

b \$ INPUT………\$で区切られているNAMELIST形式の入力cardである。入力内容については、3.2節参照のこと。ここで入力されるデータがFREG-3 の主要入力データである。

3) HISTORY DATA card (第3群入力)

計算する燃料棒の照射履歴のdataを入力する。照射履歴は、出力、冷却水温度、冷却水圧力の変動のある時点における時間（または燃焼度）を入力する。ただし、1ステップ以上50ステップまでにしなければならない。入力型式は7F1.0.1, 5I2のFormat形式である。この入力の中の5I2は5)～8)群の入力群を制御するsignalの入力である。詳しくは、3.3節参照のこと。このHistory dataの最後にはデータ終了を表すカードを入れなければならない。この終了シグナルは-1.0でコラム1～10にパンチする。

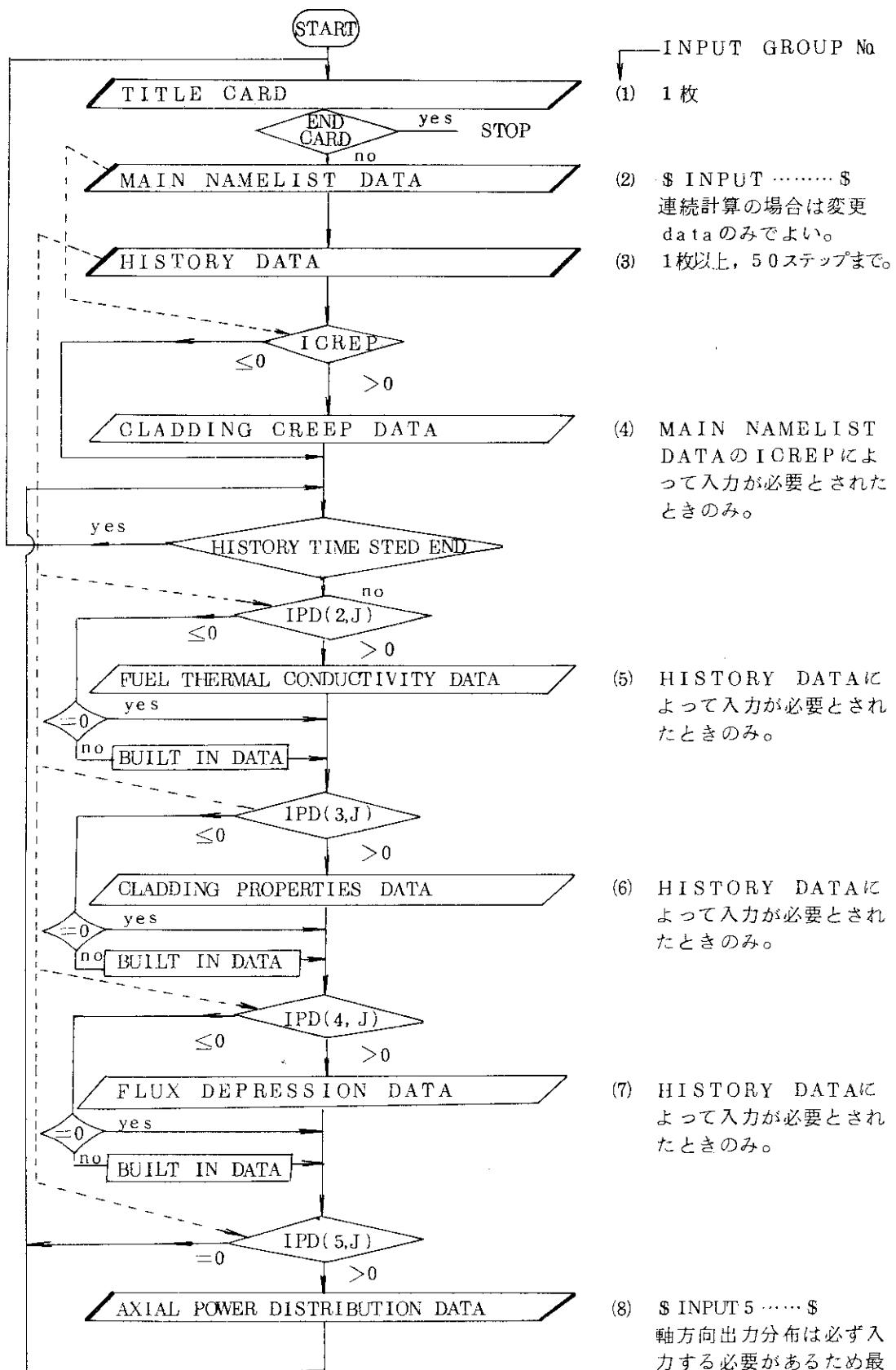


Fig.-2 FREG-3 入力 DATA の構成および順序

4) CLADDING CREEP DATA card (第4群入力)

第2群のNAMELIST DATA中のOPTION signal, key word ICREPによって必要($ICREP < 0$)とされるときのみ、入力される。入力データは、時間に対する被覆管外直徑変位値で、F10.0, E10.0のFormat形式で読み込まれ、20対まで許される。詳しくは3.6節参照のこと。このデータカード枚数は、key word ICREPと一致しなければならない。

5) FUEL THERMAL CONDUCTIVITY DATA card (第5群入力)

第3群のHISTORY DATAで入力を必要とされたときに読み込まれる。入力型式は\$INPUT2……\$のNAMELIST形式で、30対まで許される。詳しくは3.4節参照のこと。

6) CLADDING PROPERTIES DATA card (第6群入力)

第3群のHISTORY DATAで入力を必要とされたときに読み込まれる。入力型式は、\$INPUT3……\$のNAMELISTで、30対まで許される。詳しくは、3.4節参照のこと。

7) FLUX DEPRESSION DATA card (第7群入力)

このデータは、燃料ペレットの半径方向熱中性子束分布である。第3群のHISTORY DATAで入力を必要とされたときに読み込まれる。入力は、\$INPUT4……\$のNAMELIST形式で、20対まで許される。詳しくは、3.4節参照のこと。

8) AXIAL POWER DISTRIBUTION DATA card (第8群入力)

燃料の軸方向出力分布を与えるデータで、第2群入力のNPOW+1個のデータが必要である。照射履歴に従ってこの分布を変更することも可能である。そのかわり、最初のステップには必ず入力されねばならない。DATAは、\$INPUT5……\$のNAMELIST形式で入力される。詳しくは、3.4節参照のこと。

3.2 主入力データ

FREG-3の主な入力変数は、第2群の入力によって与えられる。この入力は、NAMELIST形式である。

もし、連続的に数ケースの計算を実行する場合、第2のケースからは、この入力群中の変更のあるデータのみを与えればよい。ただし、この場合、第2のケース以後のデータの単位系は、原則として最初に与えた単位系のkey word KUNITで決定される。

第2群の入力変数のFORTRAN SYMBOL NAMEとその定義をTable-3に示す。

3.3 照射履歴データの入力

3.3.1 まえおき

FREG-3は、時間(または燃焼度)に依存した照射履歴のパラメータを入力しなければならない。この照射履歴に関するデータは、第3群として入力される。この節において照射履歴データの入力法を説明する。このデータは、最大50ステップまで与えることが許される。

計算の1ステップに関する情報は1枚のカードに納められる。

1枚のカード上のデータ構成、形式をFig-3に示す。この節の説明にさいし、図中に示す

Table-3 Fortran symbol name and definition for 2nd input group

番号	FORTRAN NAME	単位		説明	SAMPLE DATA
		cm-kg系	Ft-lb系		
1	FRPUO2			重量比 $PuO_2 / (PuO_2 + UO_2)$	
2	FR35			重量比 $U^{235} / (U^{235} + U^{238})$	0.0254
3	FR40			重量比 $Pu^{240} / (\text{Total Pu})$	
4	FR41			重量比 $Pu^{241} / (\text{Total Pu})$	
5	FRDEN			ペレット密度／理論密度	0.935
6	FRSIN			組織変化した燃料の密度／理論密度	
7	DFS(S)	CM	INCH	ペレット直径	0.365
8	DC1	CM	INCH	被覆管内径	0.3735
9	DC0	CM	INCH	被覆管外径	0.422
10	LFUEL	CM	INCH	燃料柱長さ	132.0
11	DSINZ	CM	INCH	組織変化している部分の外直径	
12	DVOIDZ	CM	INCH	ペレットの初期中心孔径	
13	LVOIDZ	CM	INCH	ペレットの初期中心孔長さ(燃料棒全体)	
14	VPLENZ	CM ³	INCH ³	プレナム体積	0.5
15	ATMOS	ATMOS-PHERES	ATMOS-PHERES	初期封入ガス圧	20
16	TM	°C	°C	ペレット融点	2790.
17	ROUF(S)	CM	INCH	ペレット表面粗さ(算術平均値)	0.00004
18	ROUC(S)	CM	INCH	被覆管内表面粗さ(算術平均値)	0.00002
19	SIGHF(S)	$\frac{\text{Watt}}{\text{CM}^2 - \text{°C}}$	$\frac{\text{BTU}}{\text{HR-FT}^2 \text{°F}}$	冷却材-被覆管熱伝達係数 > 0 SIGHFの値を熱伝達係数とする。 = 0 冷却材をナトリウムとして熱伝達係数を計算する。 冷却材を水として DITTUS-BEOLTER の式で計算する。 = -2 冷却材を水として JENS-LOTTES の式で計算する。 = -3 鮫和温度を境として -1, -2 の双方を用いる。	
20	DE	CM	INCH	冷却材流路の相当直径 (SIGHF = -1, -3 のときのみ)	
21	V	$\frac{\text{M}}{\text{SEC}}$	$\frac{\text{FT}}{\text{SEC}}$	冷却材速度(〃)	
22	DTEMP(S)	°C	°C	炉心を通過する冷却材の軸方向温度差 (T _{OUTLET} - T _{INLET})	100.

番号	FORTRAN NAME	単位		説明	SAMPLE DATA
		cm - kg系	Ft - lb系		
23	SINTEM	°C	°F	ペレット焼結温度 (MDEN=1 のときのみ入力)	
24	DDISH	CM	INCH	ペレット・ディッシュの外直径	
25	HDI SH	CM	INCH	" 深さ	
26	FRACHE			初期封入ガスの組成 ヘリウム / 初期封入ガス	
27	FRACAR			" アルゴン / "	
28	FRACH			" 水素 / "	
29	FRACN			" 窒素 / "	
30	FRACKR			" クリプトン / "	
31	FRACXE			" キセノン / "	
32	S	CC gr(FUEL)	CC gr(FUEL)	燃料に吸着されているガスの量 (H ₂ , N ₂ のみ)	
33	XX			吸着ガスの組成 H ₂ / (H ₂ + N ₂)	
34	NOH			吸着ガス中の水素の挙動を指定するシグナル (注) 原プログラム(GAPCON-THERMAL-1) 内では常に NOH = 1 とする。すなわち水素は 被覆管と反応、又は被覆管よりもれ出てしま い、混合ガスの組成とはならないとしている。 このため、この入力変数は無意味となってい る。	
35					
36					
37					
38					
39					
40	IFLUX			= 0 高速中性子照射 > 0 熱中性子照射	1
41	KOOL			1 以上の整数値を指定すると冷却材の温度を被覆 管内面温度とする。冷却材 - 被覆管熱伝達係数、 被覆管温度計算は行なわない。	
42	NPOW			計算を行なう燃料柱セグメント数 (最大 20等分割)	10
43	IPEAK			与えられた線出力密度(履歴 data 参照)が平 均出力かピーク出力かを指定するシグナル。 > 0 平均出力を入力 ≤ 0 ピーク出力を入力	0

番号	FORTRAN NAME	単位		説明	SAMPLE DATA
		cm - kg系	Ft - lb系		
44	ICDF			内外圧力の差による被覆管の弾性変形を考慮するシグナル <0 被覆管の弾性変形が考慮される。 ≥0 考慮されない。 (注) ICREP > 0 のとき、この弾性変形も考慮して、DATAが作られているならば ≥ 0 としなければならない。	
45	ICREP			被覆管クリープ変形を計算する OPTION >0 時間対クリープ変形による半径(内半径の変位(CM OR / INCH))の表をICREP 枚入力する。(最大 20) =0 クリープしない。 =-2 ATR設計使用の式 =-3 Pressure tube設計の式 =-4 プログラム FIGRO使用の式 =-5 新ATR設計使用のモデル	
46	IYIELD			被覆管耐力の計算を指定するシグナル =0 プログラム GAPCON-THERMAL-1に用意された値を用いる。	
47	NEXP			ベレットの線熱膨張係数の計算式を指定するシグナル。 =0 熱膨張は考慮しない。 =1 ROTH & HALEMANの式を用いる。 (GAPCON) =2 CONWAY FINCEL & HAINの式を用いる。(GAPCON-THERMAL-1)	
48	MEXP			ベレットの熱膨張による変位量を計算する MODELを指定する シグナル。 =1 HALF CRACK MODEL (GAPCON-THERMAL-1 MODEL) =2 PLASTIC MODEL (面積バランス) =3 2領域モデル (BRITTLE MODEL + PLASTIC MODEL)	
49	ISWELL			ベレットの SWELLING 量を計算する MODELを指定する。 =0 SWELLINGを考慮しない。	

番号	FORTRAN NAME	単位		説明	SAMPLE DATA
		cm + kg系	Ft - lb系		
				= 1 GEITHOFF, et.al. MODEL (GAPCON ORIGINAL) を用いる。 = 2 REVISED GAP CLOSURE MODEL (GAPCON-THERMAL-1 に追加された MODEL) を用いる。	
50	MREST			ペレットの再組織化による計算を行なうシグナル = 0 再組織化を行なわない。 ≥ 0 再組織化を考慮し、寸法変化を計算して次の Time-Step の初期値とする。	
51	MDEN			ペレットの DENSIFICATION による変位を計算するシグナル = 0 DENSIFICATION は行なわない。 = 1 * HALDEN DENSIFICATION MODEL を用いる。 = 2 * GAPCON-THERMAL-2 の MODEL を用いる。	
52	MRELOC			ペレットの RELOCATION による変位を計算するシグナル = 0 RELOCATION は行なわない。 = 1 GAPCON-THERMAL-2 使用モデルを用いる。	
53	LCREP			ペレットのクリープ変形を計算するシグナル。 = 0 クリープ変形しない。 (現プログラムでは、ペレットのクリープは考慮していない。将来、追加の予定)	
54	IIPROF			燃料温度分布を PRINT するシグナル。 = 0 プリントしない。 = 1 詳細温度分布をプリントする。 = 2 詳細温度分布とライン・プリンタによる温度分布の図をプリントする。	
55	MCONV			GAP-CONDUCTANCE の収束線返し計算の方法を指示する。 = 0 プログラム GAPCON-THERMAL-1 と同じであるが、収斂加速因子、及び体積平均温度収斂線返し計算の回数によって	

番号	FORTRAN NAME	単位		説明	SAMPLE DATA
		cm - kg系	Ft - lb系		
				の予測値の設定に改良がなされている。 = 1 NEWTON-RAPHSON法によって収斂させる。	
56	MREV1			GAP- CONDUCTANCEの計算法についての指示 ≥ 0 プログラム GAPCON-THERMAL-1と同じ。 = 1 ROSS & STOUTEの式において、ギャップ幅が支配的因素となるが、このギャップ幅を原プログラムより厳密に扱ったMODEL(特に接触後のギャップ幅)を用いる。 =-1 RESAR-41の式を使用する。	
57	IOUT1			プログラムに用意されたオプションの一覧表をプリント・アウトするシグナル。 = 0 プリント・アウトしない。 = 1 プリント・アウトする。	
58	NOCLEI			FISSION PRODUCT(ガス)のRADIO-ACTIVITYを計算しプリント・アウトするシグナル。 = 0 計算しない。 = 1 計算する。	
59	ISPA			運転履歴に依存させて、変化させたい入力パラメータ(本表中に(S)で示した入力変数のみ有効、詳細は以後に述べる)の数を示す。 最大1 caseにつき3個。	
60	NAMSP			ISPAによって指定された変化させたい入力変数名を指示する。変数名はコード化された番号によって与えなければならない。 ISPA = 0 のときこの入力は無効となる。	
61	NHIST			運転履歴の独立変数を指定する。 = 0 時間(DAY) = 1 燃焼度(MWD/MTM)	
62	KUNIT			入力データの単位系を指示する。 = 0 FT-LB-BTUを主とした単位系 = 1 CM-KG-KCAL "	

番号	FORTRAN NAME	単位		説明	SAMPLE DATA
		cm-kg系	Ft-lb系		
				ここで選ばれた単位系は以後に行なわれる入力についても、ほぼ共通している。以後の各入力 data の単位は各々の項で参照されたい。	

① 時間または燃焼度 密 度	② 線出力 度	③ 冷却材 入口温度	④ 冷却材 圧 力	⑤ <補助 DATA >	⑥ 助 DATA >	⑦ 入力コントロールデータ (IPD)
	kW/ft	°F	psi			
	W/cm	°C	kg/cm²			

- notes : 1. 単位の上段は KUNIT=0 のときの単位、下段は KUNIT=1 のときの単位
 2. FORMAT (7 E 1 0 . 0 , 5 I 2)

Fig. -3 Constitution of irradiation history data card

指示番号①、②～⑧を使用する。

以下、入力カードの①、②～⑧の順に従って説明する。⑤、⑥、⑦の補助データの使用法については別途 3.5 節に詳述する。

照射履歴データ入力の最後には、コラム 1 ～ 10 に -1.0 をパンチしたカードを追加しなければならない。これが照射履歴データ入力の終了シグナルになる。

3.3.2 照射履歴データ

① 独立変数：時間または燃焼度

照射履歴の最も基本となる変数で、時間または燃焼度である。入力は第 1 ステップを基準とした積算値で与える。時間で指定するか燃焼度で指定するかは、第 2 群入力のオプション選択の key word NHIST によって決定される。すなわち、NHIST = 0 ならば時間（単位 day）、NHIST = 1 ならば燃焼度（単位 MWd/MTM）である。

Fig-3 の②～⑧のデータは、この独立変数に対応した値が入力されねばならない。

時間を独立変数として選んだ場合、100 日を越える時間間隔 (ΔT) が履歴として与えられると、プログラムは自動的にその時間間隔を等分割して履歴を作成する。その分割数は、 $1 + \Delta T (\text{日}) / 100 (\text{日})$ の整数値とし、もし $\Delta T / 100$ が整数値ならば、その数に置きかえる。また、分割が行なわれた場合、②～⑦のパラメータは、①によって直線内挿した値とする。

燃焼度が独立変数として選ばれた場合には、上記のような分割は行なわない。

② 線出力密度

第2群入力で入力された IPEAK によって選択された燃料棒平均出力、あるいはピーク出力を与える。すなわち、 $IPEAK > 0$ ならば平均出力、 $IPEAK \leq 0$ ならばピーク出力を与えねばならない。これは、もし平均出力で与えたければ $IPEAK > 0$ 、ピーク出力で与えたければ $IPEAK \leq 0$ にすることである。

出力変化 (ΔP) が 100 w/cm を越えて与えられた場合には、時間間隔が $1 + \Delta P (\text{w/cm}) / 100 (\text{w/cm})$ で与えられる整数値個に等分割され、自動的に履歴データを作成する。計算は、(1), (2) によって作成された履歴に従って行なわれる。入力した点については必ず計算される (Fig-4 参照)。入力データは最大 50 ステップまで計算されるが、分割された場合、最大 100 ステップまで許される。

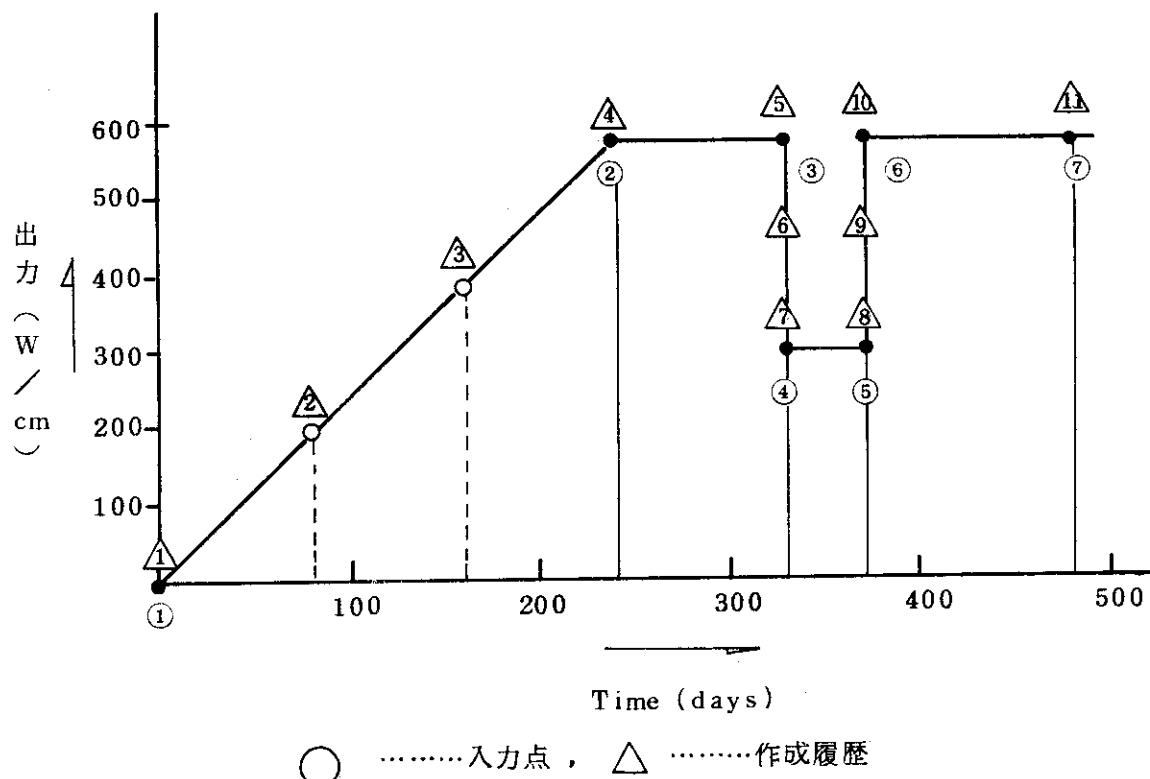


Fig - 4 時間による履歴の作成例

なお、時間および線出力密度の増加が大きく、両方共に分割が必要とされた場合、必要とする分割数の大きい方に従って分割され、履歴データが作成される。

③ 冷却材入口温度

冷却材の軸方向温度分布は、この値を基準として計算される。すなわち、冷却材軸方向温度分布は、第2群の入力 DTEMP (冷却材出口温度と入口温度の差) および後述の軸方向出力分布により計算される。入力値の単位は°Fまたは°Cである。この単位は、第2群入力の key word KUNIT によって°Fから°Cへあるいは°Cから°Fに変換される。

④ 冷却材圧力

FREG-3 では冷却材圧力の軸方向分布を考えない。當時、その履歴ステップ内では一定とする。入力値の単位は psi または kg/cm² である。この単位は第2群入力の key word

KUNIT によって psi から kg/cm² へあるいは kg/cm² から psi に変換される。

⑤～⑦ 補助データ

②～④以外に履歴をもつデータを選び変化させたい場合に使用する。選べるパラメータ、およびその使用方法は 3.5 節「補助照射履歴データ」を参照されたい。

⑧ 入力コントロールデータ

履歴データ中に 5 個のコントローラが用意されている。このコントローラは、各履歴ステップ毎に変更することが可能である。シンボル名は IPD(I, J) である (I : コントローラの種類, J : 計算ステップ No.) 。

1) 温度分布プリントアウトコントローラ, IPD(1, J)

このコントローラは、第 1 番目のコントローラで、この値を変えることにより次のような温度分布の出力をを行う。

0 : 軸方向各 section の半径方向温度分布はプリントされない。

1 : 軸方向各 section の半径方向温度分布を詳細にプリントアウトする。

2 : 上記 1 のプリントアウトの外、ラインプリンタによる温度分布図を出力する。

< 0 1 ステップの計算結果を 2 ページに要約してプリントする。

2) 燃料熱伝導率コントローラ, IPD(2, J)

このコントローラは、第 2 番目のコントローラで、この値を変えることにより、照射履歴に従って燃料熱伝導率の算出式を切換えることが可能である。このコントローラの値によって次のようなことが実行できる。

= 0 : 前ステップと同じ表または計算式を用いる。そのため計算の第 1 ステップで、0 を指定してはならない。

= N : 温度に対する熱伝導率の表を入力しなければならない。入力は N 一対のデータで、3.4 節に述べる方法によって入力されなければならない。N ≤ 30 である。

= - N : プログラムに組込まれた計算式が使用される。組込み計算式は次の通りである。

= - 2 : WARD Design equation

= - 3 : Godfrey equation

= - 4 : Lyons equation

3) 被覆管熱的、機械的物性値のコントローラ, IPD(3, J)

このコントローラは第 3 番目の制御数で、この値によって、被覆管に関する熱的、機械的物性値が選択される。

= 0 : 前ステップで使用されたと同じ値(表)が用いられる。そのため、計算の第 1 ステップでは 0 を指定することは許されない。

= N : 温度に対する各パラメータの表を入力する。入力は N 一対のデータで、3.4 節に述べる方法によって入力されなければならない。
N ≤ 30 である。

= - N : プログラムに組込まれている表を用いる。

= - 2 : 被覆管をジルカロイ - 2 として、組込みの表を用いる。

= - 4 : 被覆管をジルカロイ - 4 として、組込みの表を用いる。

＝－9：被覆管をステンレス鋼として、組込みの表を用いる。

上記各物性値の組込みの値は、Table-4, 5, 6に示す通りである。なお、ジルカロイ-4のデータはGAPCON-THERMAL-2から採用したもので、未検討なままである。使用にさいしては変更の必要があろう。

4) 燃料ペレット内半径方向熱中性子束分布のコントローラ、IPD(4, J)

このコントローラは第4番目の制御数で、この値によって燃料ペレット内半径方向熱中性子束分布が決定される。

=0 : 前ステップと同じ表を用いる。または、熱中性子束の depression を考慮せずフラットと考える。

=N : 直径対熱中性子束の相対値の表を入力する。入力はN対のデータである。この入力は3.4節に述べる方法によって入力されねばならない。 $N \leq 20$ である。

=-1 : プログラムに組込まれた値が使用される。それは、副プログラム DEPRES によって計算される。

5) 軸方向出力分布のコントローラ、IPD(5, J)

このコントローラは、第5番目の制御数で、この値によって燃料棒の軸方向の出力分布が決定される。

=0 : 前ステップと同じ分布が用いられる。そのため、第1ステップにおいて0を指定することは許されない。

=1 : 新しい出力分布が入力される。この入力は3.4節に述べる入力法によって入力されねばならない。計算の第1ケース第1ステップは必ず1とし、入力カードが用意されねばならない。

3.4 照射履歴に伴って変更しうる物性値、モデル

前節の入力コントローラによって必要とされるとき、各履歴ステップに応じ、読みこまれる。これらのデータとして、1) 燃料ペレット熱伝導率、2) 被覆管の熱的・機械的物性値、

3) 燃料ペレット内半径方向熱中性子分布、4) 軸方向出力分布がある。

これらのデータは、コントロールデータ（3.3節に述べたコントローラ）によって指定された時のみ、付加すればよく、常に入力しなければならないものではない。ただし、計算の第1ステップで4)に述べる軸方向出力分布は計算条件として、必ず入力しなければならない。

1) 燃料熱伝導率

第2番目のコントローラがNのとき（IPD(2, J) = N）だけ必要になる。入力は、NAMELIST法である。NAMELIST名はINPUT2で、入力に必要なFORTRAN名等をTable-7に示す。ここで入力する温度・熱伝導率は表に示す単位で入力されねばならない。第2群中で入力された単位切換 key word KUNITによる変換は行なわれない。コントローラを負にする（プログラム組込みの熱伝導率を使用）場合を除くと、計算の第1ステップでは、このデータを必ず与えなければならない。

2) 被覆管の熱的・機械的物性値

このデータは、被覆管に関する熱的・機械的物性値で照射履歴と共に読み込まれる第3番目

Table-4 20%冷間加工316ステンレス鋼の物性値

温 度 (°C)	熱伝導率 (w/cm/°C)	降伏強さ (kg/cm ²)	ヤング率 (kg/cm ²)	ポアソン比	線熱膨張係数 (cm/cm/°C)	Meyer硬さ (kg/cm ²)
25	0.145	6350	1972000	0.267	16.45E-6	19200
50	0.148	6150	1968000	0.268	16.60E-6	18400
75	0.152	6000	1960000	0.270	16.75E-6	17800
100	0.155	5850	1945000	0.272	16.87E-6	17500
125	0.159	5730	1925000	0.274	17.00E-6	17200
150	0.162	5650	1910000	0.276	17.12E-6	17000
175	0.166	5590	1890000	0.278	17.23E-6	16800
200	0.169	5540	1872000	0.280	17.32E-6	16600
225	0.173	5500	1850000	0.282	17.42E-6	16480
250	0.176	5450	1835000	0.283	17.48E-6	16350
275	0.180	5400	1815000	0.285	17.55E-6	16220
300	0.183	5350	1795000	0.287	17.65E-6	16100
325	0.187	5320	1785000	0.288	17.73E-6	16000
350	0.190	5300	1755000	0.290	17.84E-6	15900
375	0.194	5280	1735000	0.292	17.94E-6	15850
400	0.197	5260	1715000	0.294	18.05E-6	15820
425	0.201	5230	1695000	0.297	18.14E-6	15760
450	0.204	5210	1680000	0.299	18.22E-6	15680
475	0.208	5200	1650000	0.301	18.32E-6	15550
500	0.211	5120	1625000	0.302	18.40E-6	15390
525	0.215	5020	1600000	0.304	18.50E-6	15180
550	0.218	4900	1575000	0.306	18.56E-6	14850
575	0.221	4750	1550000	0.308	18.65E-6	14400
600	0.225	4600	1525000	0.309	18.71E-6	13750
625	0.229	4250	1490000	0.311	18.85E-6	12850
650	0.232	3900	1454000	0.313	18.89E-6	11650

Table-5 ジルカロイ-2の物性値

温 度 (°C)	热伝導率 (w/cm/°C)	降伏強さ (kg/cm ²)	ヤング率 (kg/cm ²)	ポアソン比	線熱膨張係数 (cm/cm/°C)	Meyer硬さ (kg/cm ²)
25	0.126	3150	972000	0.370	5.83E-6	9470
100	0.134	2450	914000	0.400	6.25E-6	7360
200	0.145	1670	850000	0.446	6.66E-6	5030
300	0.156	1110	780000	0.492	6.97E-6	3340
400	0.170	850	710000	0.492	7.18E-6	2560
500	0.184	700	640000	0.492	7.34E-6	2110

Table-6 ジルカロイ-4の物性値

温 度 (°C)	热伝導率 (w/cm/°C)	降伏強さ (kg/cm ²)	ヤング率 (kg/cm ²)	ポアソン比	線熱膨張係数 (cm/cm/°C)	Meyer硬さ (kg/cm ²)
25	0.129	3150	972000	0.370	5.83E-6	9470
100	0.136	2450	914000	0.400	6.25E-6	7360
200	0.143	2450	914000	0.400	6.25E-6	7360
300	0.152	2450	914000	0.400	6.25E-6	7360
400	0.164	2450	914000	0.400	6.25E-6	7360
500	0.180	2450	914000	0.400	6.25E-6	7360

Table-7 燃料ペレット热伝導率入力について
(NAMELIST名, INPUT2)

	F O R T R A N 变数名	单 位
温 度	C F 1	°C
热 伝 導 率	C F 2	w/cm·°C
热 伝 導 率 (再結晶化後)	C F 3	w/cm·°C

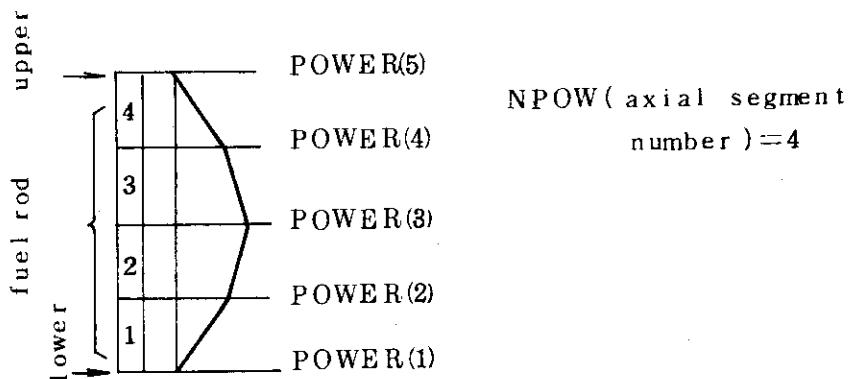
のコントローラがNのとき ($IPD(3,J)=N$) のみ必要となる。入力はNAMELIST法で、NAMELIST名は、INPUT 3である。入力に必要なFORTRAN変数名等をTable-8に示す。これらの入力値は表に示されるように第2群で入力された単位変換のkey word KUNITの値に従った単位系で入力されねばならない。

3) 燃料ペレット内熱中性子束分布

このデータは、燃料ペレット内熱中性子束分布に関するもので、照射履歴と共に読み込まれた第4番目のコントローラがNのとき ($IPD(4,J)=N$) のみ必要とされる。入力は、NAMELIST方式で、NAMELIST名 INPUT4である。入力に必要なFORTRAN変数名等をTable-9に示す。入力値のうち、直径の単位は、単位変換key word KUNITの値に応じた単位で入力されねばならない。

4) 軸方向出力分布

このデータは、燃料棒の軸方向出力分布を定めるもので、照射履歴と共に読み込まれた第5番目のコントローラが0でないとき ($IPD(5,J)\neq 0$) のみ必要になる。入力はNAMELIST方式で、NAMELIST名 INPUT5である。入力データは、第2群入力のNPOWで与えられた数より1多く必要である。燃料棒の最下部の出力分布をPOWER(1)とし順次上方にNPOW+1までの出力分布を入力する。入力値は、線出力密度そのものの値でも相対値でもよい。この出力分布は、第2群の入力で与えられたIPEAK(軸方向出力分布に対して、履歴データ中の線出力密度が平均値であるかピーク値であるかを指定する)との関係を考慮して入力しなければならない。なお、計算対象となるaxial segmentの相対出力は、そのsegmentの上下端の分布の平均値($POWER(I)+POWER(I+1)/2$)で与えられる。この出力分布の入力例をFig-5に示す。なお、このデータは、計算の第1ステップでは必ず与えねばならない。



Example of input card

b \$ INPUT(1)= 0.01, 0.7, 1.0, 0.7, 0.01 \$

Fig.-5 Input example of fuel rod axial power distribution
(under NPOW=4 and IPEAK=0 condition)

Table-8 被覆管熱的・機械的物性値の入力について
(NAMELIST名, INPUT3)

	FORTRAN 変 数 名	単 位	
		K U N I T = 0	K U N I T = 1
温 度	A A 1	°F	°C
熱伝導率	A A 2	BTU / hr - ft - °F	W / cm - °C
耐 力	A A 3	psi	kg / cm ²
ヤング率	A A 4	psi	kg / cm ²
ボアソン比	A A 5	—	—
線熱膨張係数	A A 6	1 / °F	1 / °C
マイヤー硬度	A A 7	kg / cm ²	kg / cm ²

Table-9 燃料ペレット内径方向熱中性子束分布の入力について

	FORTRAN 変 数 名	単 位	
		K U N I T = 0	K U N I T = 1
直 径	R V 1	in	cm
熱中性子束相対値	R V 2	—	—

3.5 補助照射履歴データ

先に3.3節でふれたように、FREG-3は照射履歴のパラメータとして、線出力密度、冷却材入口温度、冷却材圧力の3つを用意している。さらにこれらに加えて例えればプレナム内温度等のパラメータを照射履歴に依存させて変化させたいような場合、ここで述べる入力によって処理することができる。

3.5.1 照射履歴に依存して変化させることができるパラメータ

照射履歴と共に入力し、照射履歴に応じて変えることができるパラメータは、以下の通りである。

1) プレナム内温度

FREG-3は通常プレナム内温度を、冷却材出口温度に10°Fを加えた温度にとっている。この一定値である10°Fをここで述べる方法によって照射履歴に応じた値に変化させることができる。

2) 冷却材出口温度

第2群の入力の中のDTTEMP(冷却材出口と入口の温度差)を照射履歴と共に変化させる。

3) 再組織化するときのペレット密度

第2群入力のうち FRS IN (ペレットが再組織化するときのペレット密度)

4) ペレット外表面粗さ

第2群入力のペレット外表面粗さ, ROUF

5) 被覆管内表面粗さ

第2群入力の被覆管内表面粗さ, ROUC

6) 冷却材-被覆管熱伝達係数

冷却材-被覆管表面熱伝達係数を固定値とするが、照射履歴に従って変化させる。

3.5.2 使用法

このデータを使用して計算したいとき、その使用法は以下の通りである。

- 1) 照射履歴に依存して変化させたいパラメータを決定する。ただし、選べるパラメータの種類の個数は、最大3個までである。これを決定したら、第2群の入力の ISPA にその個数を入力する。
- 2) 決定したパラメータが何であるかを指定する。そのために、第2群入力の NAMSP にパラメータのコード番号を入力する。NAMSP の値によって選定されるパラメータを Table-10 に示す。

Table-10 照射履歴データに追加しうるパラメータ

NAMSP	Explanation	unit
1	冷却材出口温度とプレナム内温度の温度差	°C
2	冷却材出口-入口温度差	°C
3	再組織化するときのペレット密度	fraction
4	ペレット外表面粗さ	cm
5	被覆管内表面粗さ	cm
6	冷却材-被覆管熱伝達係数 (固定値であるが時間依存)	W/cm ² ~°C

- 3) 選定したパラメータの照射履歴による変化値を第3群入力カードの 41~70 コラムに入力する。

3.5.3 使用入力例

プレナム温度と被覆管表面熱伝達係数を履歴性をもつデータに切換えることを考える。

- 1) 第2群入力の ISPA, NAMSP に、次のように数値を入れる。

ISPA = 2 (パラメータがプレナム温度と熱伝達係数の2個である)

NAMSP(1) = 1, NAMSP(2) = 6 (Table-10 を参照すれば、プレナム温度のコード番号は 1, 热伝達係数は 6 である)

- 2) 第2群の照射履歴カードの 41~50 コラムにプレナム温度と冷却材温度の温度差を、51~60 コラムに熱伝達係数を入力する (Fig-6 参照)。この場合、パラメータは 2 個であるから 61~70 コラムはブランクである。

card column	1	10	11
1	0.0		
2	1 0.0		
3	1 0 0.0		
4	2 0 0.		
5	3 0 0.		
6	5 0 0.		

	41	50	51	60	61	70	71
1	0.0	1.134	b				
2	5.0	1.134	r				
3	5.0	1.134	n				
4	100.	0.057	k				
5	100.	0.057					
6	100.	0.057					

history data

coolant / clad heat transfer coefficient
Temperature difference between plenum and coolant

Fig-6 Example using history-depended parameter on irradiation history card (3rd input group)

3.5.4 使用上の注意

- 1) 照射履歴データについて説明したように、100日あるいは100w/cmをこえるような時間、出力変化の入力は、プログラム内で自動的に小分割が行なわれる。そのような場合には、ここで与えられたパラメータも、時間に対して直線内挿の値が用いられる。
- 2) このパラメータの単位は、第2群入力中のKUNITの値のいかんにかかわらず、Table -10に記載された単位で入力されねばならない。
- 3) ここで述べたオプションの各パラメータは、プログラム内で使用されている変数を直接置き換えるようにプログラムされている。すなわち、NAMSP=2, 3, 4, 5によって与えられる値は、第2群入力中のデータ、DTEMP, FRSIN, ROUF, ROUCを置き換える。
このために、連続したケースの計算を行うときには、新しいケースの最初の入力にさいしそれぞれの値を再設定しなければならない。もしこれを行なわないと、前ケースの最終値が、次ケースの初期値として計算される。
- 4) NAMSP(I)=6(冷却材-被覆管表面熱伝達係数を変化させる)のとき、これによって与えられる数値は、第2群入力中のSIGHFに置き換る。そのため、正数値ならば、その値を熱伝達係数とし、0または負の数値の場合は、SIGHFについて説明したオプションと同性値のものとして取扱かわれる。
- 5) NAMSP(I)=1(冷却材出口温度とプレナム内平均温度の温度差)のとき、これによつて与えられる数値は、プログラム内で変数の置き換えをしない。したがつて、計算ケースが変つても、第2群入力で再設定する等の必要はない。
- 6) ISPA=0と与えたときには、たとえ照射履歴カード中に、この節で説明した追加データがパンチされていたとしても(コラム41~70),すべて無視される。
- 7) ISPAに与えた数とNAMSPに与えた数が一致しない場合、追加の履歴データの個数はいずれか小さい方の数と解釈する。

例えば、ISPA=3, NAMSP(1)=1あるいはISPA=1, NAMSP(1)=1, NAMSP(2)=2のとき、いずれもISPA=1, NAMSP(1)=1と解釈し、照射履歴入力カードのコラム41~50に与えられた数値のみしか用いられない。

3.6 被覆管クリープダウンデータの入力

FREG-3の計算に、被覆管クリープダウン量を取り入れたいとき、入力データとして時間対変化量の表を入力して計算を遂行することができる。

まず、第2群入力中のICREPの値として、次に述べるデータカードの枚数（正整数）を入力する。

計算に使用するクリープダウン量データは、入力の第4群として入力される。入力形式はFig-7に示す通りである。

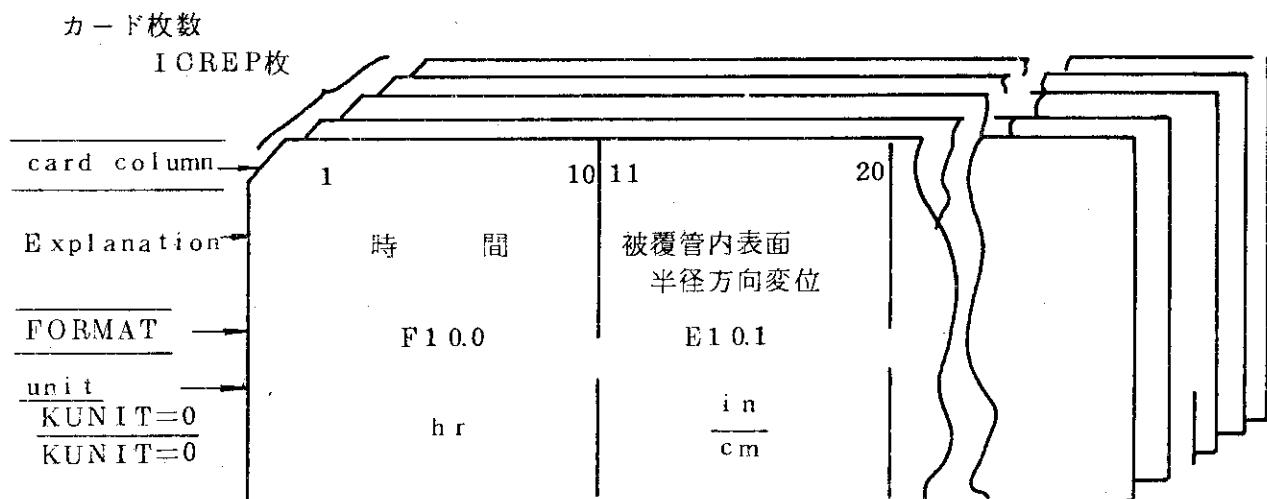


Fig-7 Input card FORMAT of cladding
creep down data

クリープダウン量は、履歴データによって与えられる照射時間について上記入力値から、直線内挿によってえられる。このえられた被覆管変位量は、被覆管の全変位量に加算される。したがって、クリープダウン変位量の符号は、負となるので、マイナス(-)を入れて入力されねばならない。入力の照射時間の単位はhrであり、第2枚目よりの時間は第1枚目の時間を基準とした積算時間である。ここで入力された時間の単位はhr、照射履歴の時間の単位はdayであるが、プログラム内で単位変換が行なわれる。

4. 入出力について

FREG-3 のサンプル入出力を Appendix-B に示す。このサンプル計算に使用した入力データは、111ページにカードイメージのまま示されているので、入力データとして示すことを省略する。

4.1 入力データ

1) 表 紙

Appendix B のとびらの下方の出力は出力の表紙である。

2) 入力データ

111ページ上段は入力カードイメージのままプリントしたものである。

3) 111ページ下段は照射履歴を整理したものである。この履歴は計算に使用する履歴で、入力履歴そのままではない。入力履歴点は、TIME STEP N_a の次に ** で示される。** のない履歴点は 3.3 節に述べた計算に使用する分割内挿履歴点である。

4) 使用オプション

112から113ページ上段は第2群入力で IOUT=1 のとき出力される。FREG-3 に用意されている計算モデルと計算式の総括表である。この計算で使用するモデルおよび計算式については、各タイトルの最後に key word name=I で示される。例えば、最後の Fuel Creep は LCREP=0 であるから、下方の説明でこの計算に燃料クリープは考慮していないことを示している。

なお、各タイトル下方のオプションの説明の左側に * で示したものがある。例えば fuel thermal expansion equation では NEXP=2 に * が付されている。この * は FREG-3 のテスト計算結果から、妥当と考えられる計算結果を与えるモデル、計算式を示す。

5) 主入力データ

113ページ下段に示される値は、主として第2群で入力されたデータを示す。右側に FORTRAN symbol name, 場合によってその値を示す。

ペレット直径等については、メートル系とインチ系の両者が併記されている。FREG-3 のプログラム中では、原則としてメートル系で計算している。そのため、インチ系で入力された場合、入力データはメートル系に換算された後再度インチ系に変換されるので、入力値と若干ずれを生じることがある。これら単位系の変換は、第2群入力の KUNIT でコントロールされている。KUNIT=0 ならばインチ系入力、KUNIT=1 ならばメートル系入力である。ただし、KUNIT=1 の方は、プログラム内の DATA statement により設定されているので、特に指定する必要はないが、インチ系入力では KUNIT=0 を第2群入力で必ず指定しなければならない。

6) 物性値、計算使用値

114ページは、この計算に使用される 1) 燃料ペレットの熱伝導率、2) 被覆管の物性値、3) 燃料ペレット内半径方向熱中性子束分布相対値 (depression factor) を示している。

7) 軸方向出力分布

114ページの最下部は、この計算に使用する軸方向出力分布相対値を示す。右側にラインプリンターによる分布図を描いている。これは入力値の check に便利なはずである。

4.2 計算結果の出力

115ページ以後は、FREG-3 の計算結果の出力である。115から121は、計算の第2ステップの計算結果を示している。これら出力値の説明を Table B-1 に示す。Table B-1 の左方の数字(1)～(84)は、115から122ページ中に書き込まれた数字にそれぞれ対応する。

117ページ下段は、3.3.2節の⑧で説明したコントローラ IPD(I, J)=1としたときの出力である。

122ページは、計算の第3ステップの計算結果を3.3.2節の⑧で説明したコントローラ IPD(I, J)<0 として、計算結果の要約を出力したものである。

118ページと119ページ上段のランプリンタによる温度分布図は、3.3.2節の⑧で説明したコントローラ IPD(I, J)=2としたとき出力される。この Sample problem のステップ2では IPD(I, J)=1 なので本来ならば出力されないが参考のため収録した。それぞれ第1セグメント(最下部)、第5セグメント(中央部)、第10セグメント(最上部)の温度分布を示す。118～119ページのそれぞれの図の右下方にプリントされているギャップコンダクタンスと115ページのギャップコンダクタンスは多少のちがいが生じる。これは、118～119ページでプリントしているギャップコンダクタンスの値は、収斂する1ステップ前の値であるからである。正しく収斂した値は115ページに記載されている。

謝 辞

この入力手引をまとめに当り、森島淳好氏（燃料安全第一研究室室長）から多くの教示をえた。また、図、表の整理については梅原啓子嬢を煩わした。記して謝意を表す。

参 考 文 献

- 1) G. R. Horn and F. E. Panisko, User's Guide for GAPCON : A Computer Program to Predict Fuel-to-Cladding Heat Transfer Coefficients in Oxide Fuel Pins, HEDL-TME 72-128, September 1972.
- 2) C. R. Hann, C. E. Beyer and L. J. Parchen, GAPCON-THERMAL-1 : A Computer Program for Calculating the Gap Conductance in Oxide Fuel Pins, BNWL-1778 September 1973
- 3) C. E. Beyer, C. R. Hann, D. D. Lanning, F. E. Panisko and L. J. Parchen, GAPOON-THERMAL-2, A Computer Program for Calculating the Thermal Behavior of an Oxide Fuel Rod, BNWL-1898, November 1975.
- 4) C. E. Beyer, C. R. Hann, D. D. Lanning, F. E. Panisko and L. J. Parchen, Users Guide for GAPCON-THERMAL-2 : A Computer Program for Calculating the THERMAL BEHAVIOR of an Oxide Fuel Rod, BNWL-1897, November 1975.
- 5) A. M. Ross and R. L. Stoute, Heat Transfer Coefficients Between UO_2 and Zircaloy-2, CRFD-1075 or AECL-1552, June 1962.
- 6) Y. Harayama, et al, to be published.

謝 辞

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- 1) G. R. Horn and F. E. Panisko, User's Guide for GAPCON : A Computer Program to Predict Fuel-to-Cladding Heat Transfer Coefficients in Oxide Fuel Pins, HEDL-TME 72-128, September 1972.
- 2) C. R. Hann, C. E. Beyer and L. J. Parchen, GAPCON-THERMAL-1 : A Computer Program for Calculating the Gap Conductance in Oxide Fuel Pins, BNWL-1778 September 1973
- 3) C. E. Beyer, C. R. Hann, D. D. Lanning, F. E. Panisko and L. J. Parchen, GAPOON-THERMAL-2, A Computer Program for Calculating the Thermal Behavior of an Oxide Fuel Rod, BNWL-1898, November 1975.
- 4) C. E. Beyer, C.R.Hann, D.D.Lanning, F.E.Panisko and L.J.Parchen, Users Guide for GAPCON-THERMAL-2 : A Computer Program for Calculating the THERMAL BEHAVIOR of an Oxide Fuel Rod, BNWL-1897, November 1975.
- 5) A. M. Ross and R. L. Stoute, Heat Transfer Coefficients Between UO₂ and Zircaloy-2, CRFD-1075 or AECL-1552, June 1962.
- 6) Y. Harayama, et al, to be published.

Appendix A

LISTING OF FREQ-3

* SOURCE STATEMENT *

```

      C      FREG-3  MAIN PROGRAMME          MAIN0010
      C
      C      REAL MUF,MOL,MOLEFR,MOLFR          MAIN0020
      C
      C      *****          MAIN0030
      C      COMMON /THIS / BASE(100),HS(7,100),MODE(5,100)  MAIN0040
      C      COMMON /BURN / BURN(20),BUOLD(20)          MAIN0050
      C      COMMON /IXR / IX,IR,IIH,MAXTEP          MAIN0060
      C      *****          MAIN0070
      C      COMMON /PWR/RAY/ PAVRG,FUEL,L,POER(21),AI(21),NPW,PTOT,LPMAX,  MAIN0080
      C                  PKPWR,IPEAK,DELP,PMAX          MAIN0090
      C
      1      COMMON /BRNRAY/ VOLCC,A1Z,ATZ,A8Z,A10Z          MAIN0100
      2      COMMON /MLM9 / TAVGX(20)          MAIN0110
      3      COMMON /COM_02/ IPWR,ISTEP,ITER,KUUNT          MAIN0120
      4      COMMON /COM_05/ BURNUP,TDAVS,VVOID,TOTLDY,TOTBUR  MAIN0130
      5      COMMON /COM_10/ VVOIDZ,FRUO2,TLEMNA,NPWI          MAIN0140
      6      COMMON /COM_20/ RHO,RHOS,FRUO2,FRPUPU          MAIN0150
      7      COMMON /COM_8M/ ISTOP,ICASE          MAIN0160
      8      COMMON /COM123/ IOUT1,IPROF          MAIN0170
      9      COMMON /INPUT / FRDEN,FHSIN,DSINZ,FRPU02,FR40,FR41,DFS,DCT,  MAIN0180
      10     DCG,DVLDZ,VPLEN4,ATHMOS,S,XX,ROUF,ROUC,EXTP,DE,V,  MAIN0190
      11     TINLET,DELTA,THMX,IFRTM,DB0,BN,HBC,SIGHF,IFFLUX,  MAIN0200
      12     NCLAD,NCUN,NFLX,KOOL,NEWK,NEWCL,NEWFLX,VOIDZL,NOH,  MAIN0210
      13     FRACHE,FRACAR,FRACH,FRACN,FRACKR,FRACXL,HGACEL,  MAIN0220
      14     DTEMP,ITOT,HG ,PEKAVG,MINI,ICDF,ISTOR,ICREP,ISWELL  MAIN0230
      15     INEXP,EXPANHIST          MAIN0240
      16     COMMON /FINVT / FNVT(20),TNVT(20)          MAIN0250
      17     COMMON /CONVER/ NONCON          MAIN0260
      18     COMMON /HISTMA/ APOWER          MAIN0270
      19     COMMON /NUCLEI/ NUCLET,A(4D,23)          MAIN0280
      20     COMMON /DIAL / FPDIAL          MAIN0290
      21     DATA ISTPLM,IR / 5,5 /          MAIN0300
      C
      C      DATE AND TIME CALL ..... STEPO          MAIN0310
      22     CALL HYOSHI          MAIN0320
      C
      C      CARD IMAGE DATA PRINT AND REWIND ..... DATAPR          MAIN0330
      23     CALL DATAPR          MAIN0340
      C
      C      INITIALIZE AND THE BEGIN CALCULATIONS.          MAIN0350
      C
      25     100 CONTINUE          MAIN0360
      C
      C      ITCT IS ITERATION TOTAL COUNTER. SEE PRINT1          MAIN0370
      26     KUUNT = ICASE = ITOT = 0          MAIN0380
      27     TDAYS=TOTALDAY=0.0          MAIN0390
      28     TOTBUR = 0.0          MAIN0400
      29     DO 110 IBS1=20          MAIN0410
      C      FAST FLUENCE(FNVT)+THERMAL FLUENCE(TNVT) ZERO SET  MAIN0420
      30     BUOLD(IW) = 0.0          MAIN0430
      31     110 BURN(IW)=FNVT(IW)=TNVT(IW)=0.0          MAIN0440
      C DATA INPUT (HISTORY INDEPENDENT DATA)          MAIN0450
      32     CALL DATINP(1)          MAIN0460
      C HISTORY-INDEPENDENT INPUT DATA CHECK          ...CHECK(1)  MAIN0470
      C IF THERE IS NO CARD FOR INPUT DATA STOP THE CALCULATION  ...CHECK  MAIN0480
      C DATE AND TIME CALL          ...STEP0  MAIN0490
      C

```

* SOURCE STATEMENT (FTMAIN) *

```

      C HISTORY STEP ARRANGEMENT ..... HISTR(1,NEXT)          MAIN0600
      33    IF(IOUT1,EQ,1)          CALL HISTR(1,NEAT)          MAIN0610
      34    CALL DUT1          MAIN0620
      C HISTORY INDEPENDENT-INPUT-DATA PRINT OUT ..... STEP1          MAIN0630
      35    CALL STEP1          MAIN0640
      C OPTIONAL SIGNAL INPUT ARRANGE AND PRINT OUT ..... STEP2(0)          MAIN0650
      36    CALL STEP2(0)          MAIN0660
      C SET UP FLEMUR MOLE CONTENT ..... MOLMOL(1)          MAIN0670
      37    CALL MOLMOL(1)          MAIN0680
      C SET UP DECAY CONSTANT OF SPECIFIED ISOTOPES          MAIN0690
      38    IF(NNUCLEI,GE,1) CALL CURIE(1)          MAIN0700
      C
      C HISTORY DATA SET IIH IS HISTORY-STEP-COUNTER          MAIN0710
      C
      39    470 CONTINUE          MAIN0720
      C
      C HISTORY DATA SETTING AT EACH TIME (BURNUP) STEP .. HISTR(2,NEXT)  MAIN0730
      40    CALL HISTR(2,NEXT)          MAIN0740
      41    IF(NEXT,EG,4*NEXT) GO TO 100          MAIN0750
      C DATA INPUT (HISTORY AND HISTORY DEPENDENT DATA).... DATINP(2)  MAIN0760
      42    CALL DATINP(2)          MAIN0770
      43    CALL DATINP(2)          MAIN0780
      C
      C HISTORY-DEPENDENT INPUT DATA CHECK          ...DEPRESC + +  MAIN0790
      44    IF((IIH,EQ,1,OR,MODE(1,IIH),NE,0)          CALL STEP2(1)  MAIN0800
      C FUEL THERMAL CONDUCTIVITY PRINT ..... STEP2(2)          MAIN0810
      45    IF((IIH,EQ,1,OR,MODE(2,IIH),NE,0)          CALL STEP2(2)  MAIN0820
      C
      C CLADDING MECHANICAL PROPERTY PRINT ..... STEP2(3)          MAIN0830
      46    IF((IIH,EQ,1,OR,MODE(3,IIH),NE,0)          CALL STEP2(3)  MAIN0840
      C CLADDING-YIELD-STRENGTH FOR FILL UP TABLE          ...FYIELD( + )  MAIN0850
      47    IF((IIH,EQ,1,OR,MODE(4,IIH),GT,0)          CALL STEP2(4)  MAIN0860
      C RADIAL FLUX DEPRESSION PRINT ..... STEP2(4)          MAIN0870
      48    IF((IIH,EQ,1,OR,MODE(4,IIH),GT,0)          CALL STEP2(4)  MAIN0880
      C AXIAL POWER DISTRIBUTION PRINT ..... PAPLOT( + )          MAIN0890
      49    IF((IIH,EQ,1,OR,MODE(5,IIH),GT,0)          CALL PAPLOT(NPON,NEWK,  MAIN0900
      C
      C FP GAS RELEASE RATE MODIFIED (FPDIAL)          MAIN0910
      50    IF(FPDIAL,NE,1.0 ,AND, IIH,EG,1)          CALL STEP2(5)  MAIN0920
      C AXIAL POWER DISTRIBUTION CALC..... POWDIS          MAIN0930
      51    CALL POWDIS          MAIN0940
      C
      C TDAYS = CELTA TIME (TIME STEP)          MAIN0950
      52    TDAYS=TOTALDAY*WTM/WTM*VOLCC/1.E6          MAIN0960
      53    FACT = 1.          MAIN0970
      54    IF(NHIST,EG,0) GO TO 200          MAIN0980
      55    IF(PAVRG,GT,0.0) GO TO 201          MAIN0990
      56    TDAYS=0.0          MAIN1000
      57    GO TO 202          MAIN1010
      58    201 CONTINUE          MAIN1020
      59    TDAYS=BURNUP*WTM/(PAVRG/1.E6)          MAIN1030
      60    202 CONTINUE          MAIN1040
      61    TOTLDY=TOTALDAY+TDAYS          MAIN1050
      62    GO TO 204          MAIN1060
      63    200 CONTINUE          MAIN1070
      64    203 PP=PAVRG          MAIN1080
      65    IF(PP,LE,0.0) PP=PKPOWER          MAIN1090
      66    IF(PP,LE,0.0) GO TO 204          MAIN1100
      67    FACT = APOWER/PP          MAIN1110
      68    204 CONTINUE          MAIN1120
      C

```

* SOURCE STATEMENT (FTMAIN) *

```

69      DO 480, IPOW=1,NPOW          MAIN1190
70      P=(POWER(IPOW)+POWER(IPOW+1))*0.5   MAIN1200
71      P=P*FACT                         MAIN1210
72      BURN(IPOW)=BURN(IPOW)+P*1.0E-6*T DAYS/WTM  MAIN1220
73      480 CONTINUE                      MAIN1230
74      IF(NHIST.EQ.0) TOTBUR=TOTBUR+PAVRG*FACT*1.E-6*T DAYS/WTM  MAIN1240
75      CALL MOLMOL(2)                   MAIN1250
C   FISSION GAS GENERATION KRYPTON AND XENON    ...FISGAS( + )  MAIN1260
C   BEGIN AXIAL CALCULATIONS                  MAIN1270
C   ISSTOP=1STPLM                           MAIN1280
C   CALL ST3T08(1)                         MAIN1290
C   MAIN1300
76      ISSTOP=1STPLM
77      CALL ST3T08(1)                         MAIN1310
C   MAIN1320
C   DELTV1=DELTIV2*1.0                      MAIN1330
C   MAIN1340
78      DO 1410 ISSTEP=1,1STPLM             MAIN1350
80      MAXTEP = ISSTEP                   MAIN1360
81      NONCON=1                           MAIN1370
C   MAIN1380
C   AXIAL NODE GAP CONDUCTANCE ITERATION..... ST3T08(2)  MAIN1390
82      CALL ST3T08(2)                   MAIN1400
C   COOLANT-CLADDING HEAT TRANSFER, HEAT FLUX,CLAD TEMP...STEP3  MAIN1410
C   ...HTCW                         MAIN1420
C   ...HTCLM                         MAIN1430
C   FUEL TEMP,DISTRIBUTION,RESTRUCTURING TEMPERATURE ...STEP4  MAIN1440
C   MAIN1450
C   FUEL THERMAL CONDUCTIVITY           ...FLOND  MAIN1460
C   HOT GAP CALCULATION (MHVEL=0)       ...STEP5  MAIN1470
C   (MHVEL=1)                         ...STEP5A  MAIN1480
C   FUEL THERMAL EXPANSION             ...EXPAND  MAIN1490
C   ...FALPHA                         MAIN1500
C   FUEL DENSIFICATION                ...DENSEF  MAIN1510
C   FUEL DENSIFICATION (HALDEN)        ...DENSHA  MAIN1520
C   DENSGA                           MAIN1530
C   CLADDING CREEP                   ...CREEP   MAIN1540
C   FUEL SWELLING (MHVEL=0)           ...SWELL   MAIN1550
C   (MHVEL=1)                         ...SWELLA  MAIN1560
C   FUEL RELOCATION (GAPCON THERMAL-2)  RELOC   MAIN1570
C   FISSION GAS RELEASE AT THIS TIME STEP ...MOLMOL(3)  MAIN1580
C   ...TEPP( + )                     MAIN1590
C   THERMAL CONDUCTIVITY OF GAS MIXTURE ...STEP6  MAIN1600
C   GAP CONDUCTANCE                  ...STEP7  MAIN1610
C   CLADDING YIELD STRENGTH          ...FYIELD( + )  MAIN1620
C   FUEL THERMAL CONDUCTIVITY        ...FCOND   MAIN1630
C   ...STEP8                         MAIN1640
C   DATE AND TIME CALL              ...STEP0   MAIN1650
C   STORED ENERGY (UNIT CONVERSION)  ...STOREN  MAIN1660
C   FUEL HEAT CAPACITY VS TEMPERATURE ...HCAP   MAIN1670
C   ...TEPP                           MAIN1680
C   STORED ENERGY                   ...CARL   MAIN1690
C   GAP CONDUCTANCE CONVERGENCE TRACE AND PRINT ...GAPRO  MAIN1700
C   FUEL TEMPERATURE PROFILE        ...PROF   MAIN1710
C   FISSION GAS RELEASE MAXIMUM VALUE SETTING ...MOLMOL(4)  MAIN1720
C   ...TEPP( + )                     MAIN1730
C   DELTXX=TAVGXX((STEP+1))-TAVGXX(STEP)  MAIN1740
C   DELTV1=AHS(DELTXX)/TAVGXX((STEP+1))  MAIN1750
C   MAIN1760
C   MAIN1770

```

* SOURCE STATEMENT (FTMAIN) *

```

85      IF(DELTIV1.LE.0.005) ISTOP = 1STEP          MAIN1780
86      IF(DELTIV1.LE.0.005.AND.DELTV2.LE.0.005.AND.ISSTEP.GT.2)  MAIN1790
87      *     AND.NONCON.EQ.0) GO TO 1420            MAIN1800
C----- NONCON = 0 SET IN SUB. ST3T08 CST, NO. 102 + 3 LINE  MAIN1810
87      DELTV3 = DELTV2                         MAIN1820
88      DELTV2=DELTIV1                         MAIN1830
89      1410 CONTINUE                         MAIN1840
90      ISSTEP = 1STPLM                         MAIN1850
91      PRINT 701((IH*DELTIV3,NONCON            MAIN1860
C   MAIN1870
92      701 FORMAT(/ 1X,130(1H*),/ 10X+30HNO CONVERGENCE IN AXIAL ITERATION  MAIN1880
1      * 10X+30HNO CONVERGENCE NO., 12+3X+30HRELATIVE ERROR (PREVIOUS STEP) ,  MAIN1890
* 12+3X+30HGAFF CONDUCTANCE, ITERATION, FLAG , 12+12H (=0=NORMAL)  MAIN1900
2      * 12+13H(1H*) )  MAIN1910
C   VOLUMETRIC AVERAGE TEMPERATURE CONVERGENCE END    DO 1410  MAIN1920
C   MAIN1930
93      1420 CONTINUE                         MAIN1940
94      ISTOP=1STEP                          MAIN1950
95      SEC = FLOAT(LTIME-KTIME)/1000.          MAIN1960
C***** NEW OUTPUT ROUTINE CALL *****74/08/29 MAIN2010
C
97      IF(CODE(1,1IM) .LT. 0) 10+15          MAIN2020
98      10 CONTINUE                         MAIN2030
99      CALL PRINT1                         MAIN2040
C   ...HEAD(1)                         MAIN2050
C   ...HEAD(-1)                         MAIN2060
100     GO TO 20                            MAIN2070
101     20 CONTINUE                         MAIN2080
102     CALL PRINT2                         MAIN2090
103     20 CONTINUE                         MAIN2100
C   FISSION GAS MAXIMUM RELEASE CALCULATION..... MOLMOL(5)  MAIN2110
104     CALL MOLMOL(5)                      MAIN2120
C   FISSION GAS RADIACTIVITY AMOUNTS CALCULATION          MAIN2130
105     IF(NUCLEI.GE.1) CALL CURIE(2)        MAIN2140
C   MAIN2150
106     DO 30 1W = 1,NPOW                   MAIN2160
107     RUCLD(1W)=BURN(1W)                  MAIN2170
108     30 CONTINUE                         MAIN2180
C   MAIN2190
109     GO TO 470                          MAIN2200
C   * 1 * 2 * 3 * 4 * 5 * 6 * 7 MAIN2210
C   * 1 * 2 * 3 * 4 * 5 * 6 * 7 MAIN2220
C***** MAIN2230
110     END                                MAIN2240
C***** MAIN2250

```

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* SOURCE STATEMENT *

```
1      SUBROUTINE STEP0                      STP00010
C      THIS SUBROUTINE IS CALLED FROM MAIN    STP00020
C                                              STP00030
2      COMMON /HIZUKE/ K1,K2,K3,K4,K5,K6      STP00040
3      CALL DATE(K1,K2)                      STP00050
4      CALL TIME(KK)                         STP00060
5      K3 = KK/3600000                         STP00070
6      K4 = MOD(KK+3600000)/60000             STP00080
7      K5 = MOD(KK+60000)/1000                STP00090
8      K6 = MOD(KK+1000)                      STP00100
9      RETURN                                  STP00110
10     END                                     STP00120
                                         ****STP00130
                                         STP00140
```

~~SOURCE STATEMENT~~

```

SUBROUTINE STEP1
C THIS SUBROUTINE IS CALLED FROM MAIN
REAL MU,F,MOLR,MOLEFR,MOLFR,LFUEL,KB,LVOIDZ
COMMON /POWRAY/ PAVRG,FUELLE,FL,POWER(21),AI(21),NPOW,PTOT,LPMAX,
1          PKPWR,JPEAK,DELP,PMAX
COMMON /DATA/ P1,CCPIN3,SECDAY,AVGAD,RR,CONEN
COMMON /COM/ 0/TITLE(20),AA(7,30),BB(6,51),CF(3,30),RV(2,20)
COMMON /COM/ 05/BURNUP,TDAYS,VVOIDZ,TOTLDY,TOTBUR
COMMON /COM/ 10/VVOIDZ,FRU02,TPLEMA,NPOW1
COMMON /COM/ 12/DENSIT,FR38,FR39
COMMON /COM/ 13/RFS,FNPOW,RSINZ,RVOIDZ
COMMON /COM/ 15/NCR,GAP
COMMON /COM/ 21/NNNNNN,INF
COMMON /COM/ 90/VOLGAS,W,HGC
COMMON /COM/157/RCI+RCO
COMMON /INPUT/ FRDEN,FRSIN,DSINZ,FRPU02,FR35,FR40,FR41,DFS,DCI,
1          DCL,DV01DZ,VPLNZ,ATMOS,S,XX,ROUR,ROUCH,EXTP,DE,V
2          TINLET,DELT,TMAX,TFR,TM,TD80,BK,HBC,SIGHF,IFLUX,
3          NCLAD,NCON,NFLX,KUUL,NEWK,NEWCL,NEWFLX,VVOIDZL,NOD+
4          FRACHE,FRACAR,FRACH,FRACN,FRACKR,FRACXE,HGACEL,
5          DTEMP,ZCLAD,HG,PEKAVG,MINI,ICDF,ISTOR,ICHEP,ISWELLST
6          ,NEXP,MEXP,NHIST
COMMON /HIZUKE/ K1,K2,K3,K4,K5,K6
COMMON /D15/ MDEN,MREL0C, SINTEM
COMMON /DIMEN/ DV01DX(20),DV01DH(20),DFSX(20),DCIX(20),DCOX(20),
1          VVOIDX(20),VV01DH(20),TSINX(20),RSINX(20)
2          ,ZLENGT(5,20),V01D(20)
COMMON /INPUT/ A/MRFST,LCREP,UDISH,HDISH
COMMON /HIS/ V/BASE(100),HIS(7,100),MODE(5,100)
COMMON /DIAL/ FPDIAL
COMMON /HIST/ NNHIST,NAXTEP
COMMON /PLOT/ IPLOT

C C INITIALIZE AND BEGIN EXECUTION.

23      FNPOW=NPOW
24      FL = FUEL / FNPOW
25      FR38=1.-FR35
26      RSINZ=DSINZ/2.
27      RVOIDZ=DV01DZ/2.
28      VVOIDZ=P1*VVOIDZ**2*VVOIDZ/FNPOW
C..... WE ASSUME THE INITIAL CENTRAL HOLE PENETRATE FROM BOTTOM TO TOP
C..... THEN RECALCULATE CENTRAL HOLE DIAMETER (CORRECT INPUT DIAMETER)
C..... VVOIDZ=P1*VVOIDZ/(PI*FL)
29      VVOIDZD=VVOIDZ/(PI*FL)
30      DV01DZD=RVOIDZD/2.
31      IF(VVOIDZD.GT.0.) VVOIDZL=FLUELL

C FRU02=1.-FRPU02
32      DLSN11=FRU02*11.46+FRU02*10.97
33      FR39=1.-FR40-FR41
34      IF(FRPU02.LE.+1.E-10) FR39=0.
35      GAP=DCI-DFS
36      DFS=DFS/2.
37      DCI=DCI/2.
38      RC1=DCI/2.
39      RC0=DCI/2.
40      VOLGAS=P1/4.*((DCI**2-DFS**2)*FL+VVOIDZ

```

* SOURCE STATEMENT (STEP1

```

----- INITIALIZE COLD DIMENSION SET
41      DU_11 I=1,NPCW
42      DVOIDCX(I)=DVOIDDH(I)=DVOIDDD
43      VV01DX(I)=VV01DH(I)=VV01DZ
44      DF5C(I) = DFS
45      DCIX(I) = DCI
46      DCCAC(I) = DCC
47
48      RSINX(I)=RSINZ
49      VVIDL(I)=FL
50      IF (VV01DZ.LE.0.0) VVIDL(I)=0.0
51      J1 CONTINUE
52
53      *WRITE(6,*51) TITLE,K1,K2,K3,K4
54      *WRITE(6,*502)
55      *WRITE(6,*503) FRPU02,FR49,FR40,FR41,FRU02,FR35+FR38
56      DUM1 = DFS / 2.54
57      DUM2 = DSINZ / 2.54
58      DUM3 = DVG1DZ / 2.54
59      *WHITE(6,*504) FRDEN,FRDEN,FRSIN,FRSIN,DFS,DUM1,DSINZ,DUM2,
60      *          DVOIDDZ,DUM3
61      DUM1 = GAP / 2.54
62      DUM2 = DCI / 2.54
63      DUM3 = DCC / 2.54
64      DUM4 = FUELL / 2.54
65      DUM5 = V01DZL / 2.54
66      DUM6=DDISH/2.54
67      DUM7 = HDISH / 2.54
68      *WHITE(6,*505) DDISH,DUM6+HDISH,DUM7
69      *WHITE(6,*506) GAP,DUM1,DCI,DUM2,DCO,DUM3,FUELL+DUM4,V01DZL,DUM5,
70      *          S*X+XX
71      DUM1 = VPLENZ / ( 2.54**3 )
72      DUM3 = DTEMP + 1.8
73      DUM4 = DE / 2.54
74      DUM5 = V / .3048
75      DUM7 = ROLCF / 2.54
76      DUM8 = ROUC / 2.54
77      *WHITE(6,*510) VPLENZ,DUM1+DTEMP,DUM3,DE,DUM4,V,DUM5,
78      *          ROLF+DUM7,ROUC+DUM8
79      DUM1 = 1.8*TM + 32.0
80      *WHITE(6,*514) TM+DUM1
81      *WHITE(6,*513) ATMOS+ATMOS
82      *WHITE(6,*520) FRACHE,FRACAR,FRACH,FRACN,FRACKR,FRACKE
83      IF(SIGHF) 180,190,200
84      180 IF(SIGHF,EQ,-1.) *WHITE(6,*581) SIGHF
85      IF(SIGHF,EQ,-2.) *WHITE(6,*582) SIGHF
86      IF(SIGHF,EQ,-3.) *WHITE(6,*583) SIGHF
87      IF(SIGHF,EQ,-4.) PRINT 584, SIGHF
88      GO TO 210
89      190 *WHITE(6,*580) SIGHF
90      GO TO 210
91
92      200 DUM1 = SIGHF * 30.48 ** 2 * 3600. / 1.8 / 1055,
93      *WHITE(6,*589) SIGHF,DUM1
94      210 CONTINUE
95      IF(IFLUX) 220,220,230
96      220 *WHITE(6,*590) IFLUX
97
98      230 *WHITE(6,*591) TFLUX
99      240 CONTINUE

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* SOURCE STATEMENT (STEP1) *

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C   FUEL THERMAL EXPANSION COEFFICIENT OPTION PRINT          STP11190
C   IF(NEXP.GT.0) WRITE(6,633) NEXP                         STP11200
C   IF(KOOL.GT.0) WRITE(6,639) KOOL                         STP11210
C   IF(MDEN.GT.0) WRITE(6,641) MDEN                         STP11220
C   IF(MDEN.EQ.1) WRITE(6,645) SINTEM                      STP11230
C   IF(MRELOC.EQ.1) WRITE(6,651) MRELOC                     STP11240
C   IF(FRSIN.GT.FRDEN) MREST = 1                           STP11250
C   IF(MREST.EQ.0) WRITE(6,655) MREST                      STP11260
C   IF(MREST.EQ.1) WRITE(6,656) MREST                      STP11270
C   IF(MREST.EQ.1) MREST = 1                               STP11280
C   IF(CIPLT.LE.0) RETURN                                  STP11290
C   KPOW=NPOW/2.0+0.5001                                  STP11300
C   IF(KPOW.LE.0) KPOW=1                                  STP11310
C   WRITE(8) (TITLE(I),I=1,20),KPOW,NPOW,MAXTEP          STP11320
C   WRITE(8) FRPU02,FR39,FR40,FR41,FRU02,FR35,FR38,FRDEN,FRSIN,    STP11330
A   DFS,DSIN2,DDISH,HDISH,GAP,DC1,DC2,FRACAR,FRACN,FRACKR,FRACXE,    STP11340
B   VOIDLZ,S1XX,VPLENZ,DTEMP,DE,VY,ROUF,ROUC,           STP11350
C   TM,ATMOS,FRACAR,FRACN,FRACKR,FRACXE,                STP11360
D   SIGHT,MODE(2,1),MODE(3,1),MODE(4,1),FLUX,IPAK,        STP11370
E   ICREP,ICDF,ISWELL,NEXP,MEXP,MDEN,                  STP11380
F   MRELOC,MPEST                                         STP11390
103  RETURN                                              STP11400
104  * 1 * 2 * 3 * 4 * 5 * 6 * 7 * 8 * 9 * 10 * 11 * 12 * 13 * 14 * 15 * 16 * 17 * 18 * 19 * 20 * 21 * 22 * 23 * 24 * 25 * 26 * 27 * 28 * 29 * 30 * 31 * 32 * 33 * 34 * 35 * 36 * 37 * 38 * 39 * 40 * 41 * 42 * 43 * 44 * 45 * 46 * 47 * 48 * 49 * 50 * 51 * 52 * 53 * 54 * 55 * 56 * 57 * 58 * 59 * 60 * 61 * 62 * 63 * 64 * 65 * 66 * 67 * 68 * 69 * 70 * 71 * 72 * 73 * 74 * 75 * 76 * 77 * 78 * 79 * 80 * 81 * 82 * 83 * 84 * 85 * 86 * 87 * 88 * 89 * 90 * 91 * 92 * 93 * 94 * 95 * 96 * 97 * 98 * 99 * 100 * 101 * 102 * 103 * 104 * 105 * 106 * 107 * 108 * 109 * 110 * 111 * 112 * 113 * 114 * 115 * 116 * 117 * 118 * 119 * 120 * 121
109  501 FORMAT(1H1,20A4,10X,2A4,15,3H HR,1J3,7H MINUTE      STP11440
110  502 FORMAT(/58X,18I1*) / 58X, 18I* INPUT VALUES * /      STP11450
111  503 FORMAT(7X,1H*,9X,16HFUEL COMPOSITION, 99X,1H*/ 7A,BH* (1) , STP11460
A  F11.4, 24H WEIGHT FRACTION FU02 .62X,                 STP11470
B  21HFRU02 * * / 7X,BH*                                         STP11480
C  F11.4, 24H WEIGHT FRACTION PU239 .62X,                STP11490
D  21HFR391,FR40-+FR41 * * / 7X,BH* (2) , STP11500
E  F11.4, 24H WEIGHT FRACTION PU240 .62X,                STP11510
F  21HFR40 * * / 7X,BH* (3) , STP11520
G  F11.4, 24H WEIGHT FRACTION PU241 .62X,                STP11530
H  21HFR41 * * / 7X,BH*                                         STP11540
I  F11.4, 24H WEIGHT FRACTION U02 .62X,                 STP11550
J  21HFRU02=1,-FRPU02 * * / 7X,BH* (4) , STP11560
K  F11.4, 24H WEIGHT FRACTION U235 .62X,                STP11570
L  21HFR35 * * / 7X,BH*                                         STP11580
M  F11.4, 24H WEIGHT FRACTION U238 .62X,                STP11590
N  21HFR38=1,-FR35 * * / 7X,BH*                                         STP11600
112  304 FORMAT(7X,
A  47H* (5) FUEL DENSITY ,F14.5,4H(FRA, STP11610
B  10H(DCTN TD) ,F13.5,3H(FRACTION TD) FRDEN ,F14.5,4H(FRA, STP11620
C  47H* (6) RESTRUCTURED FUEL DENSITY ,F14.5,4H(FRA, STP11630
D  10H(DCTN TD) ,F13.5,3H(FRACTION TD) FRSIN ,F14.5,4H(FRA, STP11640
E  47H* (7) PELLET DIAMETER ,F14.5,4H(CM, STP11650
F  10H ) ,F13.5,3H(INCHES) DFS ,F14.5,4H(CM, STP11660
G  47H* (8) INITIAL RESTRUCTURED FUEL DIAMETER ,F14.5,4H(CM, STP11670
H  10H ) ,F13.5,3H(INCHES) DSIN2 ,F14.5,4H(CM, STP11680
I  47H* (9) INITIAL CENTER HOLE DIAMETER ,F14.5,4H(CM, STP11690
J  10H ) ,F13.5,3H(INCHES) VOIDLZ ,F14.5,4H(CM, STP11700
113  500 FORMAT(7X,
1  47H* (1) PELLET DISH DIAMETER ,F14.5,4H(CM, STP11710
2  10H ) ,F13.5,3H(INCHES) DDISH ,F14.5,4H(CM, STP11720
3  47H* (2) PELLET DISH DEPTH ,F14.5,4H(CM, STP11730
4  10H ) ,F13.5,3H(INCHES) HDISH ,F14.5,4H(CM, STP11740
114  50n FORMAT(7X,
A  47H* PELLET-TO-CLAD DIAMETRAL GAP ,F14.5,4H(CM, STP11750
B  10H ) ,F13.5,3H(INCHES) GAP=DC1-DFS ,F14.5,4H(CM, STP11760
C  47H* (10) CLAD INSIDE DIAMETER ,F14.5,4H(CM, STP11770
D  10H ) ,F13.5,3H(INCHES) DC1 ,F14.5,4H(CM, STP11780
E  47H* (11) CLAD OUTSIDE DIAMETER ,F14.5,4H(CM, STP11790
F  10H ) ,F13.5,3H(INCHES) DCO ,F14.5,4H(CM, STP11800
G  47H* (12) FUEL LENGTH ,F14.5,4H(CM, STP11810
H  10H ) ,F13.5,3H(INCHES) LFUEL(REAL) ,F14.5,4H(CM, STP11820
I  47H* (13) INITIAL CENTER HOLE LENGTH ,F14.5,4H(CM, STP11830
J  10H ) ,F13.5,3H(INCHES) LVOIDLZ(REAL) ,F14.5,4H(CM, STP11840
K  47H* (14) SORBED GAS CONTENT ,F14.5,4H(CC/C, STP11850
L  10H(GRAM) ,F13.5,3H(CC/GRAM) S ,F14.5,4H(CC/C, STP11860
M  47H* (15) FRACTION OF SORBED GAS WHICH IS H2 ,F14.5,4H(CM, STP11870
N  10H XX * ) STP11880
115  510 FORMAT(7X,
A  47H* (16) PLENUM VOLUME ,F14.5,4H(CC, STP11890
B  10H(CM) ,F13.5,3H(CC, IN.) VPLENZ ,F14.5,4H(CC, STP11900
* 48H* (17) AXIAL TEMPERATURE GRADIENT ACROSS CORE,F13.5,4H(DEG, STP11910
* 10H(C) ,F13.5,3H(DEG F) DTEMP ,F14.5,4H(DEG F, STP11920
E  47H* (18) COOLANT PASSAGE EQUIVALENT DIAMETER ,F14.5,4H(CM, STP11930
F  10H ) ,F13.5,3H(INCHES) DE ,F14.5,4H(CM, STP11940
G  47H* (20) COOLANT VELOCITY ,F14.5,4H(M/S, STP11950
H  10H(EC) ,F13.5,3H(FT/SEC) V ,F14.5,4H(M/S, STP11960
I  47H* (23) FUEL SURFACE ROUGHNESS, ARITH, MEAN ,E14.5,4H(CM, STP11970
N  10H ) ,F13.5,3H(INCHES) ROUF ,F14.5,4H(M/S, STP11980
O  47H* (24) CLAD ID SURFACE ROUGHNESS ARITH, MEAN,E14.5,4H(CM, STP11990
P  10H ) ,F13.5,3H(INCHES) ROUC ,F14.5,4H(M/S, STP12000
116  513 FORMAT(7X,
A  47H* (36) FILL GAS PRESSURE ,F14.5,4H(ATM, STP12110
B  10H(SPHERES) ,F13.5,3H(ATMOSPHERES) ATMOS * ) STP12120
117  514 FORMAT(7X,
A  47H* (35) MELTING TEMPERATURE OF THE FUEL ,F14.5,4H(DEG, STP12130
B  10H(C) ,F13.5,3H(DEG F) TM * ) STP12140
C  * 1 * 2 * 3 * 4 * 5 * 6 * 7 * 8 * 9 * 10 * 11 * 12 * 13 * 14 * 15 * 16 * 17 * 18 * 19 * 20 * 21 * 22 * 23 * 24 * 25 * 26 * 27 * 28 * 29 * 30 * 31 * 32 * 33 * 34 * 35 * 36 * 37 * 38 * 39 * 40 * 41 * 42 * 43 * 44 * 45 * 46 * 47 * 48 * 49 * 50 * 51 * 52 * 53 * 54 * 55 * 56 * 57 * 58 * 59 * 60 * 61 * 62 * 63 * 64 * 65 * 66 * 67 * 68 * 69 * 70 * 71 * 72 * 73 * 74 * 75 * 76 * 77 * 78 * 79 * 80 * 81 * 82 * 83 * 84 * 85 * 86 * 87 * 88 * 89 * 90 * 91 * 92 * 93 * 94 * 95 * 96 * 97 * 98 * 99 * 100 * 101 * 102 * 103 * 104 * 105 * 106 * 107 * 108 * 109 * 110 * 111 * 112 * 113 * 114 * 115 * 116 * 117 * 118 * 119 * 120 * 121
118  520 FORMAT(7X,
A  30H* FILL GAS COMPOSITION, 95X, 1H*/7X,STP12190
B  10H* (37) ,F8.4, 30H MOLE FRACTION HELIUM ,+57X, STP12200
C  21HFRACHE * /7X, STP12210
D  10H* (38) ,F8.4, 30H MOLE FRACTION ARGON ,+57X, STP12220
E  21HFRACAR * /7X, STP12230
F  10H* (39) ,F8.4, 30H MOLE FRACTION HYDROGEN ,+57X, STP12240
G  21HFRACH * /7X, STP12250
H  10H* (40) ,F8.4, 30H MOLE FRACTION NITROGEN ,+57X, STP12260
I  21HFRACN * /7X, STP12270
J  10H* (41) ,F8.4, 30H MOLE FRACTION KRYPTON ,+57X, STP12280
K  21HFRACKR * /7X, STP12290
L  10H* (42) ,F8.4, 30H MOLE FRACTION XENON ,+57X, STP12300
M  21HFRACXE * /7X, STP12310
119  525 FORMAT(7X,1H*,124X,1H*) STP12320
120  580 FORMAT(7X,
A  27H* (43) COOLANT IS SODIUM,78X, 7HSIGHF = F8.2, 3X, 1H*) STP12330
121  581 FORMAT(7X, STP12340

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* SOURCE STATEMENT (STEP1)*

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      A 53H* (43) COOLANT IS WATER (DITTUS-BEELTER EQUATION), 52X, STP12370
      B 7HSIGHF =, F8.2, 5X, 1H*) STP12380
122 582 FORMAT( 7X,
      A 52H* (43) COOLANT IS WATER (JENS LOTTES EQUATION) , 53X, STP12400
      B 7HSIGHF =, F8.2, 5X, 1H*) STP12410
123 583 FORMAT( 7X,
      A 50H* ( ) COOLANT IS WATER (SUBCOOL=DITTUS BEELTER, SATURAT STP12420
      B 14HE(JENS LOTTES), 31X,7HSIGHF =, F8.2, 5X, 1H*) STP12440
124 584 FORMAT( 7X,
      A 52H* (43) COOLANT IS WATER (TOM.S CORRELATION) , 53X, STP12450
      B 7HSIGHF =, F8.2, 5X, 1H*) STP12460
125 589 FORMAT( 7X,
      A 52H* (43) COOLANT NOT SPECIFIED, FILM COEFFICIENT IS ,F12.2, STP12480
      B 5H*(X/CM2-C), F14.2,14H(BTU/HR-FT2-F),4X,5HSIGHF,15X,1H*) ) STP12500
126 590 FORMAT( 7X,
      A 34H* (44) FAST FLUX IRRADIATION ,71X, 7HIFLUX =,13,10X,1H*) STP12520
127 591 FORMAT( 7X,
      A 34H* (44) THERMAL FLUX IRRADIATION,71X, 7HIFLUX =,13,10X,1H*) STP12540
128 593 FORMAT( 7X,
      1 80H* (45) FUEL THERMAL EXPANSION IS TAKEN INTO ACCOUNT. STP12560
      2 ,25X,7HNEXP =,13,10X,1H*) ) STP12570
129 639 FORMAT( 7X,
      A 60H* (46) IF(KOOL.GT.0) THE COOLANT TEMPERATURE IS THE SAME , STP12590
      B 52H-TEMPERATURE OF THE CLADDING IS, KOOL =,13, STP12600
      C ,10X,1H*) STP12610
130 640 FORMAT( 7X,
      A 84H* (55) NUMBER OF AXIAL SEGMENTS (LIMIT OF 20) STP12620
      B ,21X, 7HNPK =,13,10X,1H*) ) STP12640
131 641 FORMAT( 7X,
      1 80H* ( ) FUEL DENSIFICATION IS TAKEN INTO ACCOUNT. STP12660
      2 ,25X, 7HMDEN =, 13, 10X,1H*) ) STP12670
132 645 FORMAT(7X,
      1 60H* ( ) FABRICATE SINTERING TEMPERATURE (DEG C) STP12680
      2 45X,7HSIN:EM=F6.1,7X,1H*)
133 651 FORMAT( 7X,
      1 80H* ( ) FUEL RELOCATION MODEL IS USED. STP12710
      2 ,25X, 7MMRELUC =, 13, 10X,1H*) ) STP12720
134 655 FORMAT( 7X,
      1 80H* ( ) RESTRUCTURING CALCULATION IS NOT PERFORMED STP12740
      2 ,25X, 7MHREST =, 13, 10X,1H*) ) STP12750
135 656 FORMAT( 7X,
      1 80H* ( ) RESTRUCTURING CALCULATION IS PERFORMED STP12770
      2 ,25X, 7MHREST =, 13, 10X,1H*) ) STP12780
      C * 1 * 2 * 3 * 4 * 5 * 6 * 7 STP12790
*****END*****STP12800
*****END*****STP12820
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* SOURCE STATEMENT *

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1      SUBROUTINE STEP2(KS)
C
C THIS SUBROUTINE IS CALLED FROM MAIN
C
2      REAL MUF,MOL,MOLEFR,MOLEFR
C
3      COMMON /YIELD/ IYIELD
C
4      COMMON /MCNV/ MCNV
C
5      COMMON /POWER/ PAVRG,FUELLE,FL,POWER(21),A1(21),NPOW,PTOT,LPMAX,
1          PKPOWER,DELP,PMAX
C
6      COMMON /BRNRAY/ VOLCC,AZ1,AZ2,AZ3,A92,A102
C
7      COMMON /DATA 1/ ZH(7,6),ZR4(7,6),ST(7,26),TABLE(2, 80)
C
8      COMMON /DATA 4/ PI,CCP(13),SECDAV,AVOGAD,RR,CONEN
C
9      COMMON /DATA 6/ NZR2,NZR4,NST
C
10     COMMON /CON 0/ TITLE(20),AC(7, 30),BB(6, 51),CF(3, 30),RV(2, 20)
C
11     COMMON /CON 1/ DENSIT,FR38,FR39
C
12     COMMON /CON 14/ KCOR
C
13     COMMON /CON 20/ RHG,PHOS,FRUU,FRPUPU
C
14     COMMON /CON 21/ N,V,V,V,V,V,V
C
15     COMMON /CON25/ VOLUME
C
16     COMMON /CON 90/ VOLGAS,W,HGC
C
17     COMMON /CON128/ IOUT1,IIPROF
C
18     COMMON /INPUT /
FRDEN=FRSIN*DSINZ,FRPU02,FR35,FR40,FR41,DFS,OCI,
1          DCO,DV9IDZ,VPLENZ,ATMOS,XX,ROUG,ROUC,EXTP,OE,V,
2          TINLET,DELT,TMAX,TFR,TM,DBD,BK,H3C,SIGHF,IFLUX,
3          NCLAD,CON,INFLX,KOOL,NEWK,NEWCL,NEWFLX,VOLDZL,NOH,STP2250
4          FRACHE,FRAGAR,FRACHN,FRACKR,FRACKE,HGACEL,
5          PTEMP,ZCLAD,HG,PEKAVG,MINI,ICDF,ISTOR,ICREP,ISWELL,STP2270
6          ,INEXP,MEXP,NHMIST
C
19     COMMON /INPUT A/ MRESTR,LCREP,LDISH,HDISH
C
20     COMMON /POWER/ PWRREF(21)
C
21     COMMON /DATA 3/ VOLAT(29),F15GH(29)
C
22     COMMON /DTAL/ FFDIAL
C
23     COMMON /NUCLEI/ NUCLEI(1,AC(0,23))
C
24     DIMENSION YCF(3, 30),RVINCH(20)
C
25     IF(KS,GT,0) GO TO 10000
C
26     RHOUDENS=FRDEN
C
27     RHODENS=DENSIT*FRSIN
C
28     VOLUME#T/4.*((DFS**2-DVOIDZ**2)
C
29     VOLCC=VOLUME
C
30     #RHOD*VOLCC
C
31     GRPUCC=RHO*GRPUCC
C
32     UAT=T#235.*FR35+238.*FR38
C
33     FRUU=UAT*T/(UAT*T+32.)
C
34     PUAT=T#239.*FR39+240.*FR40+241.*FR41
C
35     FRPUPU=PUAT*T/(PUAT*T+32.)
C
36     #2*FR38*FRUU*AVOGAD/238.*VOLCC*GRPUCC
C
37     #72*FR9*FRPUPU*AVOGAD/239.*VOLCC*GRPUCC
C
38     #87*FR40*FRPUPU*AVOGAD/240.*VOLCC*GRPUCC
C
39     #92*FR41*FRPUPU*AVOGAD/241.*VOLCC*GRPUCC
C
40     #112*FR35*FRUU*AVOGAD/235.*VOLCC*GRPUCC
C
41     A1=A1/
C
42     A7=A7Z
C
43     A6 =#482
C
44     A9 =#A9Z
C
45     A10=A10Z
C
46     IF(NOH) 3,3,2
C
47     2 WRITE(6,601) NOH
C
48     GO TO 4
C
49

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* SOURCE STATEMENT (STEP2) *

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50     3 WRITE(6,602) NOH
51     * CONTINUE
C
C CLADDING CREEP OPTION PRINT
C
52     IF(ICREP,LT,0) WRITE(6,611) ICREP
53     IF(ICREP,GT,0) WRITE(6,617) ICREP
54     IF(ICREP,LE,1) WRITE(6,621) ICREP
C
C CLADDING ELASTIC DEFORMATION OPTION PRINT
C
55     IF(ICDF,LT,0) WRITE(6,621) ICDF
C
C FUEL SHELLING OPTION PRINT
C
56     IF(ISWELL,LE,1) WRITE(6,632) ISWELL
57     IF(ISWELL,LE,2) WRITE(6,633) ISWELL
C
C STORED ENERGY OPTION PRINT
C
58     IF(ISTOR) 73,71,71
59     71 WRITE(6,641) ISTOR
60     GO TO 74
61     73 WRITE(6,643) ISTOR
62     74 CONTINUE
C
C PEAK ON AVERAGE SELECT OPTION PRINT
C
63     IF(IPEAK) 81,81,82
64     81 WRITE(6,651) IPEAK
65     GO TO 83
66     82 WRITE(6,653) IPEAK
67     83 CONTINUE
68     IF(IOUT1) 84,84,86
69     84 WRITE(6,651) IOUT1
70     GO TO 85
71     86 CONTINUE
72     IF(IIPROF,GT,0) WRITE(6,680) IIPROF
C
73     IF(MEXP,GT,0) WRITE(6,691) MEXP
C
74     IF(MCNV,EQ,0) WRITE(6,701) MCNV
75     IF(MCNV,NE,1) WRITE(6,702) MCNV
C
C CLADDING YIELD STRENGTH OPTION PRINT
C
76     IF(IYIELD,LE,0) WRITE(6,710) IYIELD
C
77     IF(NHMIST,LE,0) WRITE(6,720) NHMIST
78     IF(NHMIST,LE,1) WRITE(6,721) NHMIST
79     IF(NUCLEI,LE,1) WRITE(6,725) NUCLEI
80     WRITE(6,902)
81     RETURN
C
82 10000 CONTINUE
83     GO TO 1111,2222,3333,4444,5555,6666,7777, KS
84     1111 CONTINUE
85     RETURN

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* SOURCE STATEMENT (STEP2) *

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86      2222 CONTINUE                                         STP21190
C
C     THERMAL CONDUCTIVITY OF FUEL PRINT
C
87      IF(NEWK.GT.0) WRITE(6,903)                                         STP21200
88      IF(NCON) 200,205,210                                         STP21210
89      200 KCON = NCON * (-1)                                         STP21220
90      IF(KCON.EQ.2) WRITE(6,732) NCON                                         STP21230
91      IF(KCON.EQ.2,AND,FRDEN.LT.,95) KCON = 1                                         STP21240
92      IF(KCON.EQ.3) WRITE(6,733) NCON                                         STP21250
93      IF(KCON.EQ.4) WRITE(6,734) NCON                                         STP21260
94      IF(KCON.EQ.5) WRITE(6,735) NCON                                         STP21270
95      GO TO 220                                         STP21280
96      205 WRITE(6,1001) NCON                                         STP21290
97      STOP                                         STP21295
98      210 KCON = -1                                         STP21300
99      WRITE(6,736) NCON                                         STP21310
100     GO TO 220                                         STP21320
101     220 WRITE(6,900)                                         STP21330
102     IF(NCON) 230,230,250                                         STP21340
103     230 GO TO (231,231+260,260+260,260) ,NCON                                         STP21350
104     231 DO 250 J=1,11                                         STP21360
105     TE=4300.+FLDAT(J-1)                                         STP21370
106     CF(1,J)=TEMP                                         STP21380
107     CF(2,J)=FCOND(FRSIN+TEMP+273.,KCON)                                         STP21390
108     IF(FRDEN,GE.,95) GO TO 232                                         STP21400
109     CF(2,J)=FCOND(FRDEN+TEMP+273.,KCON)                                         STP21410
110     GO TO 250                                         STP21420
111     232 CF(2,J)=FCOND(FRDEN+TEMP+273.,KCON)                                         STP21430
112     250 CONTINUE                                         STP21440
113     NNI = 11                                         STP21450
114     GO TO 290                                         STP21460
115     260 GO 270 J=1,11                                         STP21470
116     TEMP=300.+FLDAT(J-1)                                         STP21480
117     CF(1,J)=TEMP                                         STP21490
118     CF(2,J)=FCOND(FRSIN+TEMP+273.,KCON)                                         STP21500
119     CF(3,J)=FCOND(FRSIN+TEMP+273.,KC01)                                         STP21510
120     270 CONTINUE                                         STP21520
121     NNI=11                                         STP21530
122     GO TO 290                                         STP21540
123     290 NNI = NCON                                         STP21550
124     298 DO 298 J = 1,NNN                                         STP21560
125     YCF(1,J) = CF(1,J) * 1.8 + 32.                                         STP21570
126     YCF(2,J) = CF(2,J)*57.8                                         STP21580
127     YCF(3,J) = CF(3,J)*57.8                                         STP21590
128     295 CONTINUE                                         STP21600
129     WRITE(6,740) ((CF(1,J)+YCF(1,J),J=1,3),J=1,NNN)                                         STP21610
130     WRITE(6,900)                                         STP21620
131     WRITE(6,902)                                         STP21630
132     RETURN                                         STP21640
133     3333 CONTINUE                                         STP21650
134     IF(NEWK.GT.0) GO TO 300                                         STP21660
135     WRITE(6,903)                                         STP21670
136     300 CONTINUE                                         STP21680

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* SOURCE STATEMENT (STEP2) *

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137     WRITE(6,900)                                         STP21700
138     IF(NCLAD.LE.1) WRITE(6,751) NCLAD                                         STP21710
139     IF(NCLAD.LE.-2) WRITE(6,752) NCLAD                                         STP21720
140     IF(NCLAD.LE.-4) WRITE(6,754) NCLAD                                         STP21730
141     IF(NCLAD.LE.-9) WRITE(6,759) NCLAD                                         STP21740
142     IF(NCLAD.LE.-2) GO TO 320                                         STP21750
143     NN = NZP2                                         STP21760
144     DO 310 I=1,7                                         STP21770
145     DO 310 J=1,NZK2                                         STP21780
146     310 AA(I,J) = ZR*(I,J)                                         STP21790
147     GO TO 370                                         STP21800
148     320 IF(NCLAD.LE.-4) GO TO 340                                         STP21810
149     NN = NZP1                                         STP21820
150     DO 330 I=1,7                                         STP21830
151     DO 330 J=1,NZK1                                         STP21840
152     330 AA(I,J) = ZR*(I,J)                                         STP21850
153     GO TO 370                                         STP21860
154     340 IF(NCLAD.LE.-9) GO TO 360                                         STP21870
155     NN = NZP1                                         STP21880
156     DO 350 I=1,7                                         STP21890
157     DO 350 J=1,NZP1                                         STP21900
158     350 AA(I,J) = ST(I,J)                                         STP21910
159     GO TO 370                                         STP21920
160     360 CONTINUE                                         STP21930
C
C     CLADDING MATERIAL SPECIFICATION ERROR PRINT
C
161     WRITE(6,760) NCLAD                                         STP22000
162     STOP                                         STP22010
163     370 CONTINUE                                         STP22020
164     IF(NCLAD.LE.1) NN=NCLAD                                         STP22030
165     WRITE(6,770) (YIELD                                         STP22040
166     WRITE(6,900)                                         STP22050
167     WRITE(6,781)                                         STP22060
168     WRITE(6,902)                                         STP22070
169     DO 380 J=1,NN                                         STP22080
170     380 WRITE(6,790) (AA(I,J),I=1,7)                                         STP22090
171     WRITE(6,902)                                         STP22100
172     RETURN                                         STP22110
173     4444 CONTINUE                                         STP22120

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C
C     FLUX DEPRESSION PRINT
C
174     IF(NEWK.GT.0,OR.,NEWCL,GT.0) GO TO 400                                         STP22130
175     WRITE(6,903)                                         STP22140
176     400 CONTINUE                                         STP22150
177     WRITE(6,900)                                         STP22160
178     DO 410 J=1,NF                                         STP22170
179     410 RVINCH(J) = RV(1,J) / 2.54                                         STP22180
180     WRITE(6,900)                                         STP22190
181     WRITE(6,810) NFLX*(RV(1,J),RVINCH(J),RV(2,J),J=1,NF)                                         STP22200
182     WRITE(6,902)                                         STP22210
183     RETURN                                         STP22220
184     5555 CONTINUE                                         STP22230
C
C     CORRECTED F.P. GAS RELEASE RATE PRINT OUT
C
185     IF(FPDIAL.LE.0.0) PRINT 907,FPDIAL                                         STP22240

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* SOURCE STATEMENT (STEP2) #*

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186      PRINT 903
187      DO 510 I = 1 , 29
188      FISGR(I)*FISGR(I)*FPDIAL
189      IF(FISGR(I).GE.1.0) FISGR(I) = 1,
190      510 CONTINUE
191      PRINT 901
192      PRINT 904,FPDIAL
193      PRINT 905
194      DU 515 I = 1 , 29
195      PRINT 906,VOLAT(I),FISGR(I)
196      515 CONTINUE
197      PRINT 902
198      RETURN
199      5666 CONTINUE
200      7777 CONTINUE
201      RETURN
C   *    1   *   2   *   3   *   4   *   5   *   6   *   7   STP22530
202      601 FORMAT( 7X,
A 84H* (57) THE HYDROGEN IS ASSUMED TO REACT WITH THE CLADDING STP22530
B   .21X, 7HNOH * ,13+10X,1H* ) STP22540
203      602 FORMAT( 7X,
A 84H* (57) HYDROGEN IS ASSUMED TO REMAIN IN FUEL PIN STP22540
B   .21X, 7HNOH * ,13+10X,1H* ) STP22550
204      621 FORMAT( 7X,
A105H* (60) ELASTIC CLAD DEFLECTION TAKEN INTO ACCOUNT. STP22550
B   .7HICDF * ,13+10X,1H* ) STP22560
205      632 FORMAT( 7X,
A105H* ( ) GEITHOFF, ET AL. MODEL IS USED. STP22560
B   .7HISWELL* ,13+10X,1H* ) STP22570
206      633 FORMAT( 7X,
A105H* ( ) REVISED GAP CLOSURE MODEL IS USED. STP22570
B   .7HISWELL* ,13+10X,1H* ) STP22580
207      641 FORMAT( 7X,
A105H* (62) STORED ENERGY CALCULATION IS NOT PERFORMED. STP22580
B   .7HISTOK * ,13+10X,1H* ) STP22590
208      643 FORMAT( 7X,
A105H* (62) STORED ENERGY CALCULATION IS PERFORMED. STP22590
B   .7HISTOK * ,13+10X,1H* ) STP22740
209      651 FORMAT( 7X,
A105H* (63) A PEAK POWER NEEDS TO BE INPUT. STP22740
B   .7HIPEAK * ,13+10X,1H* ) STP22750
210      653 FORMAT( 7X,
A105H* (63) AN AVERAGE POWER NEEDS TO BE INPUT. STP22750
B   .7HIPEAK * ,13+10X,1H* ) STP22760
211      654 FORMAT( 7X,
A 95H* ( ) CLADDING CREEP VALUES DETERMINED FROM STP22760
B   .2 10X, 7HICREP * ,13+10X,1H* ) STP22830
212      617 FORMAT( 7X,
A105H* (59) A TABLE OF TIME VERSUS CLADDING CREEP DOWN VALUES MUST P22830
B5T BE USED. !CHEP=THE NUMBER OF CARDS. .7HICREP * ,13+10X,1H* ) STP22860
213      661 FORMAT( 7X,
A 80H* (64) OPTIONAL EQUATION LIST DID NOT PRINT STP22860
B   .25X, 7HIOUT1 * ,13+10X,1H* ) STP22880
214      662 FORMAT( 7X,
A 60H* (64) OPTIONAL EQUATION LIST IS PRINTED STP22880
B   .25X, 7HIOUT1 * ,13+10X,1H* ) STP22920
215      663 FORMAT( 7X,
A 60H* (65) RADIUS TEMPERATURE PROFILE IN FUEL PIN IS PRINTED STP22920
B   .25X, 7HIIPROF * ,13+10X,1H* ) STP22950

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* SOURCE STATEMENT (STEP2) #*

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216      641 FORMAT( 7X,
A 60H* ( ) FUEL THERMAL EXPANSION IS TAKEN INTO ACCOUNT. STP22960
B   .45X, 7HMEXP * ,13+10X,1H* ) STP22970
217      701 FORMAT( 7X,
1 80H* (67) GAPCON-THERMAL-1 ORIGINAL CONVERGENCE METHOD IS USED STP23000
2   .25X, 7HMCINV * ,13+10X,1H* ) STP23010
218      702 FORMAT( 7X,
1 80H* (66) NEWTON RAPHSON METHOD IS USED STP23020
2   .25X, 7HMCINV * ,13+10X,1H* ) STP23030
219      710 FORMAT( 7X,
A105H* ( ) YIELD STRENGTH IS USED FROM TABLE DATA WHICH IS ASSISTP23040
B5NED BY NCLAD .7HYIELD* ,13+10X,1H* ) STP23070
220      720 FORMAT( 7X,
1 35H* ( ) TIME DEPENDENT HISTORY .70X, 7HNHIST * ,13+10X,1H* ) STP23090
221      721 FORMAT( 7X,
1 35H* ( ) BURNUP DEPENDENT HISTORY .70X, 7HNHIST * ,13+10X,1H* ) STP23100
222      725 FORMAT( 7X,
1 42H* ( ) FISSION PRODUCTS YIELD PRINT OUT, 63X, 7HNNUCLEI*, STP23120
2   .13+10X,1H* ) STP23140
223      732 FORMAT( 7X,
A 84H* (46) FUEL THERMAL CONDUCTIVITY VALUES DETERMINED FROM WARSTP23160
B5 DESIGN EQUATIONS .21X, 7H(NCON)* ,13+10X,1H* ) STP23170
224      733 FORMAT( 7X,
A 84H* (48) FUEL THERMAL CONDUCTIVITY VALUES DETERMINED FROM DATSTP23190
BA OF GODFREY, ET AL .21X, 7H(NCON)* ,13+10X,1H* ) STP23200
225      734 FORMAT( 7X,
A 84H* (48) FUEL THERMAL CONDUCTIVITY VALUES DETERMINED FROM DATSTP23220
BA OF LYONS, ET AL .21X, 7H(NCON)* ,13+10X,1H* ) STP23230
226      735 FORMAT( 7X,
A 84H* (48) FUEL THERMAL CONDUCTIVITY VALUES DETERMINED FROM RESSTP23250
2AK=41 EQUATION .21X, 7H(NCON)* ,13+10X,1H* ) STP23260
227      736 FORMAT( 7X,
A 84H* (48) FUEL THERMAL CONDUCTIVITY VALUES WERE INPUTTED STP23270
B   .21X, 7H(NCON)* ,13+10X,1H* ) STP23280
228      740 FORMAT( 7X, 1H*, 17X, *TEMPERATURE*, 46X, *THERMAL CONDUCTIVITY*, 30X STP23300
1   , 1H* / 7X, 1H*, 124X, 1H* / 7X, 1H*, 54X, *UNRESTRUCTURED FUEL* STP23310
2   , 21X, *RESTRUCTURED FUEL*, 13X, 1H* / 7X, 1H*, 7X, 29X, 1H* / 14X STP23320
3   , 28X, 1H* / 10X, 28X, 1H* / 8X, 1H* / 7X, 1H*, 10X, *DEG C*, 18X STP23330
4   , *(DEG F), 18X, *(BTU/HR-FT-F*), 10X STP23340
5   , *(BTU/HR-FT-F*), 8X, 1H* / 7X, 1H*, 124X, 1H* / STP23350
6   , 7X, 1H*, 7X, F10.0, 4X, F10.0, 18X, F10.3, 5X, F10.3, 13X, F10.3 STP23360
7   , 5X, F10.3, 12X, 1H* ) STP23370
229      751 FORMAT( 7X,
A 84H* (50) CLADDING NOT SPECIFIED, PROPERTIES WERE INPUTTED STP23380
B   .21X, 8H(NCLAD)* ,13+ 9X,1H* ) STP23400
230      752 FORMAT( 7X,
A 34H* (51) CLADDING IS ZIRCALOY-2 .71X, 8H(NCLAD)* ,13+ 9X,1H* ) STP23420
231      754 FORMAT( 7X,
A 34H* (51) CLADDING IS ZIRCALOY-4 .71X, 8H(NCLAD)* ,13+ 9X,1H* ) STP23440
232      759 FORMAT( 7X,
A 41H* (50) CLADDING IS 316 STAINLESS STEEL, 64X, STP23450
B   .8H(NCLAD)* ,13+ 9X,1H* ) STP23470
233      760 FORMAT( 5X, 36HGLADDING MATERIAL SPEC. ERROR NCLAD* ,13+ STP23480
1 10H STEP2 ) STP23490
234      770 FORMAT( 7X, 1H*, 104X +8H 1YIELD* ,13+ 9X,1H* ) STP23500
235      781 FORMAT( 7X, 1H*, 10X, 40HTEMPERATURE THERMAL YIELD STP23510
A   .7X, 50HYOUINGS POISONS THERMAL MAYE, STP23520
B   1HR *16X, 1H* / 7X, 1H*, 24X, 30HCONDUCTIVITY STRENGTH STP23530
C   , 3X, 50HMODULUS RATIO EXPANSTON HARDN STP23540

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* SOURCE STATEMENT (STEP2)*

```
D 3HESS+14X,1H* /7X, 1H*,87X, 6HCUEFF, + 31X, 1H*/7X,STP23550
E 1H*, 12X,50H(DEC)  (*CF/C)  (KG/CH2)  (KG/CM STP23560
F 2H*)+24X,21H*/C)  (KG/CH2)  , 15X,1H* ) STP23570
236 790 FORMAT( 7X,1H*,F20.1,F14.5,F15.1+17.5+F13.3,E17.5,F13.1,15X,1H*) STP23580
237 810 FORMAT(7X,
1 70H* (54) FLUX DEPRESSION VALUES USED STP23600
2 ,35X,7H(NFLX)=,13,10X,1H* / STP23610
3 2(7X,1H*,124X,1H* /) 7X,1H*+27X, "DIAMETER",36X,"FLUX RATIO" STP23620
4 ,43X,1H* / 7X,1H*,21X,"( CM )",9X,"(INCH)",82X,1H* / STP23630
5 , 7X,1H*,124X,1H* / (7X,1H*,17X,+10.4,5X,F10.4+27X,F10.4 STP23640
6 ,45X, 1H* ) ) STP23650
238 820 FORMAT( 7X,
1 84H* ( ) FUEL NOT CREEP STP23660
2 ,21X, 7HLCREP =,13,10X,1H* ) STP23670
239 821 FORMAT( 7X,
1 84H* ( ) FUEL CREEP STP23680
2 ,21X, 7HLCREP =,13,10X,1H* ) STP23690
240 900 FORMAT( 7X,1H*,124X,1H* ) STP23700
241 901 FORMAT(7X,1H*,124X,1H* / 7X,1H*,124X,1H* ) STP23710
242 902 FORMAT( 7X,1H*,124X,1H* / 7X,126(1H*) ) STP23720
243 903 FORMAT(1H1 / 7X,126(1H*), / 7X,1H*,124X,1H* ) STP23730
244 904 FORMAT( 7X,
1 84H* ( ) F.P. GAS RELEASE RATE CONTROL DIAL STP23740
2 ,21X, 7HPPDIAL=,F5.3,8X,1H* / STP23750
3 ,21X,1H*,124X,1H* ) STP23760
245 905 FORMAT(7X,1H*,10X,40HVOLUME AVG, TEMP,(C) RELEASE RATE STP23770
1 ,74X,1H* / 7X,1H*,124X,1H* ) STP23780
246 906 FORMAT(7X,1H*,20X,F10.2,15X,F12.6+77X,1H* ) STP23790
247 907 FORMAT(// 10(1H*), " CAUTION FPDIAL NEGATIVE FPDIAL=",F3.1, /) STP23800
C
248 1001 FORMAT(5X, 47HFUEL THERMAL CONDUCTIVITY SPEC. NO ERROR NCON= ,13, 1H*,10H STEP2 STP23810
C * 1 * 2 * 3 * 4 * 5 * 6 * 7 STP23820
***** STP23830
***** STP23840
***** STP23850
***** STP23860
***** STP23870
***** STP23880
249 END STP23890
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* SOURCE STATEMENT *

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1      SUBROUTINE STEP3
2      THIS SUBROUTINE IS CALLED FROM ST3T08
3
4      REAL MUF,MOL,MOLEFR,MOLFR
5      COMMON /COM39/ HFLUX(20)
6      COMMON /DATA 4/ PI,CCPIN3,SECDAY,AVOGAD,RH,CONEN
7      COMMON /COM 0/ TITLE(20),AA(7,30),BB(6,51),CF(3,30),RV(2,20)
8      COMMON /COM 02/ IPW,ISTEP,ITER,KOUNT
9      COMMON /COM 03/ T0,P,DELRC0,DELRC1,TCOOL,STP
10     COMMON /COM 08/ II,JCASE,TCOOLF,XHOTOT
11     COMMON /COM 21/ NNN,NNN,NNF
12     COMMON /COM 35/ TBI,TBU,TCC,TCI,TCO,TFS,TH,THR
13     COMMON /COM 38/ QVRAB,QVRAC,QVRAF,MF
14     COMMON /COM37/ TAVGC
15     COMMON /INPUT / FRDEN,FRSIN,DSINZ,FRRU02,FR35,FR40,FR41,DFS,CCI,
16                  DCO,DVD02,VPLNE,ATMOS,S,XX,ROUC,EXTP,DE,V,STP30100
17                  TINLET,DELT,TMAX,TFRT,TH,DBO,BK,HHC,SIGHT,IFLUX,
18                  NCLAD,NCNON,NFLX,KUOL,NEWL,NEWL,NEWL,FWRK,VOIDZL,NDH,STP30120
19                  FRACHE,FRACAR,FRACH,FRACN,FRACKR,FRACXE,HGACEL,
20                  DTEMP,ZCLAD,HG,PKAvg,MINI,ICDF,ISOR,ICHEP,ISWELL,STP30200
21                  ,NEXP,MEXP,NHIST,STP30210
22
23     COMMON /COM3P/ TSAT
24
25     *****
26     QVVRAC=P   /(PI*(DC0+*DELRC0))
27     HFLLUX=(P0W)*QVVRAC
28     QVVRAD=P   /(PI*(DC1+*DELRC1))
29     QVVRAS=P   /(PI*(DFS+*DELK))
30
31     IF(KOOL.GT.0) GO TO 600
32     IF(SIGHT) 590+600+610
33
34     590 CONTINUE
35
36     CLADDING-TO-COOLANT HEAT TRANSFER COEFFICIENT OF WATER
37
38     KDJ=1 ..DITTUS BOELTER,      KDJ=2 ..JENS LOTTES
39     KDJ#3 SUBCOLL2..DITTUS-BOELTER + BUILDING,..,JENS-LOTTES
40     KDJ=1#IFIX(SIGHF)
41
42     *****
43     CALL HTCW(KDJ,TCOOL,QVVRAC,V,DE,MF,TCO,EXTP,TSAT)
44     GO TO 630
45
46     *****
47     600 CALL HTCLM (HF,TCOOL,DE,V)
48     610 HF=SIGHF
49     620 CONTINUE
50
51     *****
52     IF(HF.LE.0.0) TCO = TCOOL
53     IF(HF.LE.0.0) GO TO 630
54
55     *****
56     TCO=TCOOL+QVVRAC/HF
57
58     630 CONTINUE
59     TAVGC=TCO+20,
60     QVVRAA=(QVVRAC+QVVRAD)/2.
61     !IRY=1
62
63     640 CONTINUE
64     INI = 1
65     IM2 = 30
66     TCC = 1ERP(TAVGC,AA,2,NN,INI1,INI2,INI3,31)
67     !IRY=1!IRY+1
68
69     640 CONTINUE
70     DE=(QVVRAA+(DC0+*DELRC0)-DC1-2,*DE,HCY)/(2.0*TCC)
71
72

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* SOURCE STATEMENT (STEP 3) *

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42      TCI=TCU+DELT
43      TAVGC1=(TCU+TCI)/2,
44      DEL=ABS(TAVGC1-TAVGC)
45      IF(DEL<0.55) 670+670,650
46      650  TAVGC=TAVGC1
47      IF(||THY-50| 640,640,660
48      660  WRITE(6,1470)
49      670  CONTINUE
50      GO TO 690
51      680  TCI=TCUOL
52      TAVGC=TCI-20,
53      GOVRRAA=(GOVRAC+GOVRAI)/2,
54      ITTRY=0
55      IN1=7
56      IN2=30
57      682  CONTINUE
58      ITTRY=ITTRY+1
59      TCC=TERP(TAVGC,AA,2,NN,IN1,IN2,[N3,32])
60      DELTC=GOVRRAA*(DCO+2,*DELRC0-UC1-2,*DELRC)/(2.0*TCC)
61      TCO=TCI-DELT
62      TAVGC1=(TCO+TCI)/2,
63      DEL=ABS(TAVGC-TAVGC1)
64      IF(DEL<0.55) 688+689,684
65      684  TAVGC=TAVGC1
66      IF(||THY-50| 682,682,686
67      686  WRITE(6,1470)
68      688  CONTINUE
69      H=0.0
70      690  CONTINUE
71      GOVRAG=(GOVRAS+GOVRAI)/2,
C
C      SET UP SYSTEM OF N NODES OF EQUAL THICKNESS, RADII IN FEET
C
72      TFS=TCI*GOVRAG/HG
73      RETURN
74      1470 FORMAT(10X,"NO CONVERGENCE IN TCC      STEP31")
*****END*****

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* SOURCE STATEMENT *

```

1      SUBROUTINE STEP4                               STP40010
C      THIS SUBROUTINE IS CALLED FROM ST3TO8          STP40020
C
2      REAL MU,F,MOL,MOLEFR,MOLFR                  STP40030
3      COMMON /POWRAY/ PAVRG,FUELL,FL,POWER(21),A1(21),NPOW,PTOT,LPMAX,    STP40040
4      COMMON /DATA 4/ PI,CPI(3),SECDAY,AVGAD,RRCONEN   STP40050
5      COMMON /COM 0/ TITLE(20),AAC(7,50),BB(6,50),CF(3,30),RV(2,20)  STP40060
6      COMMON /COM 1/ TTC(51),TSR(51),QIN(51),Q(51),TS(51),CLCRP(2,20) STP40070
7      COMMON /COM 02/ IPOS,(STEP,ITER,KOUNT)           STP40080
8      COMMON /COM 03/ TO,PDELRCQ,DELRC,DEL,R,TCOOL,STP  STP40090
9      COMMON /COM 04/ RSINF,NQS,QUINTOT              STP40100
10     COMMON /COM 05/ BURNUP,TDAYS,VVOID,TOTLDY,TOTBUR  STP40110
11     COMMON /COM 13/ RFS,FNPWR,R$INZ,RVOID1Z         STP40120
12     COMMON /COM 14/ KCON                           STP40130
13     COMMON /COM 21/ N,NNN,NNN,NF                   STP40140
14     COMMON /COM 35/ TBL,TBO,TCC,TCI,TCO,TFS,TH,THR  STP40150
15     COMMON /COM49P/ DC(20,51),IPROF               STP40160
16     COMMON /COMGAB/ DSIN,RSIN,TSIN,TSINC,DVOID,T    STP40170
17     COMMON /INPUT / FRDEN,FRSIN,DSINZ,FRP02,FR35,FR46,FR41,DFS,DCI,  STP40180
18             DCO,DVOIDZ,VPLNZ,ATMOS,S,XX,ROU,F,ROUC,EXTP,DE,V,  STP40190
19             TINLET,DELT,TMAX,TFR,TM,DB0,BK,HBC,SIGHF,IFLUX,  STP40200
20             INCLAD,NCON,NFLX,ROUL,NEWL,NEWCL,EFLX,VVOIDZ,NOH,  STP40210
21             FRAHC,FRCAR,FRAHC,FRCAR,FRAHC,X,HGACEL,  STP40220
22             DTMP,ZCLAU,HG,PEKAVG,MINI,ICDF,ISTOR,ICREP,ISWELL  STP40230
23             +NEXP,+HEXP,INHIST                         STP40240
24     COMMON /RESTRU/ ISINT,RVOIDX,VVOIDC,VLENGT       STP40250
25     COMMON /INPUT / MREST,LCKEP,DDISH,HDISH        STP40260
26
27     N=50                                         STP40270
28     DR=(HFS+DELH-RVOID)/FLOAT(N)                 STP40280
29     R0=(HFS+DELH)                                STP40290
30     DO 700 I=1,N                                 STP40300
31
32     R=R0-DR*(I-1)                                STP40310
33     DD=(2.*R-DR)                                STP40320
34     IN1 = 2                                     STP40330
35     IN2 = 20                                    STP40340
36     INDC=RFS/R0*DD                                STP40350
37     RATIO = TERP(DDDR,RV,2,NE,IN1,IN2,IN3+41)    STP40360
38     RDR=DR                                         STP40370
39     IF(RDR.GE.RSIN .AND.(R.GT.RSIN )) Q(1)=PI*(R**2-RDR**2)*RAT(0*000  STP40380
40     IF(RDR.LT.RSIN .AND.R.LE.RSIN ) Q(1)=((R**2-RSIN **2)*000+(RSIN **2-RDR**2)*000)*PI*RATIO  STP40390
41     IF(RDR.LT.RSIN .AND.R.LE.RSIN ) W(1)=PI*(R**2-RDR**2)*RATIO*000  STP40400
42     700 CONTINUE                                  STP40410
43
44     C     CONNECT FOR ACCUMULATION OF ERROR IN HEAT GENERATION  STP40420
45     SUMG=0.                                         STP40430
46     DO 710 I=1,N                                 STP40440
47     710 SUMG=SUMG+Q(I)                          STP40450
48
49     IF(SUMG.LE.0.0) CORR = 1.0                  STP40460
50     IF(SUMG.LE.0.0) GO TO 715                  STP40470
51
52     *****  STP40480
53     CORR=TOT/SUMG                            STP40490
54     715 CONTINUE                                  STP40500
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* SOURCE STATEMENT (STEP4) 2*

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42     DO 720 I=1,N                                STP40510
43     720 S(I)=CORR*Q(I)                         STP40520
44     ACC=1.                                         STP40530
45     Q(1)=R*TOT-Q(1)                           STP40540
46     DO 730 I=2,N                                STP40550
47     730 QIN(I)=QIN(I-1)-W(I)                  STP40560
48     IME#0                                         STP40570
49     DC 860 I=1,N                                STP40580
50     R=(RFS+DELH)- DR*FLOAT(I-1)                STP40590
51     RDR=R-DR                                         STP40600
52     IF(I,GT,1) GO TO 740                      STP40610
53     TAV=TFS                                         STP40620
54     TZ=TFS                                         STP40630
55     GO TO 750                      STP40640
56     740 TAV=TT(I-1)                           STP40650
57     TZ=TT(I-1)                           STP40660
58     750 CONTINUE                                  STP40670
59     DEN=FRDEN                                         STP40680
60     IF(R,LE,RSIN ) DEN=RFSIN                  STP40690
61     760 TAVK = TAV + 273.                      STP40700
62     IF(NCON) 770,780,800                      STP40710
63     770 C = FCOND(DEN,TAVK,KCON)            STP40720
64     GO TO 810                                         STP40730
65     780 WRITE(6,1910) NCON                     STP40740
66     STOP                                         STP40750
67     800 KK=2                                         STP40760
68     IF(R,LE,RSIN ) KK=3                         STP40770
69     IN1 = 3                                         STP40780
70     IN2 = 30                                       STP40790
71     C = TERP(TAV,CF,KK,NNN,IN1,IN2,IN3,42)    STP40800
72     810 CONTINUE                                  STP40810
73     IF(RDR.LT.1,E=20) GO TO 820              STP40820
74     *****  STP40830
75     IF(W(I),LE,0.0) GO TO 820              STP40840
76     *****  STP40850
77     TERM=(RDR**2/(R**2-RDR**2)-QIN(I))/Q(I)*ALOG(R/RDR)  STP40860
78     GO TO 830                                         STP40870
79     Q(I) = HEAT RATE IN I RING                STP40880
80     QIN(I) = TOTAL HEAT RATE UNTIL INNER RING (I-1)  STP40890
81     R = OUTER RADIUS OF I RING                 STP40900
82     RDR = INNER RADIUS OF RING I               STP40910
83     820 TERM=0.                                STP40920
84     830 TT(I)=TZ+Q(I)/(2.*PI*C)*(5.-TERM)    STP40930
85     TAV1=(TZ+TT(I))/2.                         STP40940
86     TTAV=TAV                                         STP40950
87     DIFF=ABS(TAV-TAV1)                         STP40960
88     IF(DIFF-ACC) 860,860,840                  STP40970
89     840 TAV=TAV1                                         STP40980
90     IME=IME+1                                     STP40990
91     IF(IME>10) 760,850,850                  STP41000
92     850 WRITE(6,1920) TTAV,TAV1                STP41010
93     860 IME#0                                         STP41020
94     DC(I,IPOW+1) = RFS + DELR                 STP41030
95     DO 870 I=1,N                                STP41040
96     870 TS(I)=RFS+DELH-RVOID*FLOAT(I)/FLOAT(N)  STP41050
97     DC(I,IPOW+1) = TS(I)                         STP41060
98     870 CONTINUE                                  STP41070
99     BB(3,1) = TFS                                STP41080
100    BB(4,1) = RFS                                STP41090

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* SOURCE STATEMENT (STEP4) *

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93      IN1 = 2                                STP41190
94      IN2 = 20                               STP41200
95      DDD = RFS * 2.0                          STP41210
96      BB(5,1) = TERP(DDD,RV, 2,NF,IN1,IN2,IN3,43) STP41220
97      DC(I,POW,I+1) = TFS                  STP41230
C      RV(1,I),RV(2,I) ARE DIAMETER AND DEPRESSION FACTOR RESPECTIVELY STP41240
C      RV IS SETTED IN SUBROUTINE STEP2          STP41250
98      DO 890 I=1,N                           STP41260
99      DC(I,POW,I+1) = TT(I)                 STP41270
100     BB(3,I+1) = BB(1,I) = TT(I)           STP41280
101     BB(4,I+1) = BB(2,I) = TS(I)           STP41290
102     880 CONTINUE                           STP41300
103     IN1 = 2                                STP41310
104     IN2 = 20                               STP41320
105     DDD = TS(I) * 2.0                      STP41330
106     BB(5,I+1) = TERP(DDD,RV, 2,NF,IN1,IN2,IN3,44) STP41340
C      . . . . . MREST RESTRUCTURE OPTION ( NOX IGNORE )
C
C      IF(MREST.LE.0) GO TO 900                STP41350
107     IF(FRDEN.GE.FRSIN) FRSEN=FRDEN        STP41380
108     TSINC=1.E0                            STP41390
C      *****
109     IF(TOTLDY.LE.0.0) GO TO 890            STP41400
C
C      ISINT IS THE SIGN OF RESTRUCTURING BEGIN STP41410
110     ISINT=1                         STP41420
111     VOIDZL=FULL                         STP41430
C
C      RESTRUCTURING TEMPERATURE REFER D-936    STP41440
C
112     RETEM=.00001367*ALOG10(24.*TOTLDY ) +.000480 STP41450
113     TSINC=1./RETEN-273.                   STP41460
114     890 CONTINUE                           STP41470
115     TSIN = TSINC                         STP41480
116     IN1 = 0                                STP41490
117     IN2 = N + 1                           STP41500
118     RSIN = TEMP(TSIN,EB,2,N,IN1,IN2,IN3,45) STP41510
119     (FRSIN,LE,RSIN), RSIN=RSIN2          STP41520
120     DS1=2.*RSIN                         STP41530
C***** ****
121     FACT = 0.0                            STP41540
122     IF(RSIN,LE,0.0) GO TO 5               STP41550
123     FACT = (FRSIN-FRDEN) / FRSIN         STP41560
124     5 CONTINUE                           STP41570
125     SWAV = RVO1D2**2 + FACT*(RSIN**2 - RSINZ**2) STP41580
126     VOID = SWRT(SWAV)                   STP41590
C***** ****
127     RVOID=SWRT((RSIN**2)*(FRSIN-FRDEN)/FRSIN) STP41600
128     IF(VOID,LE,RVOID) RVOID=RVOID         STP41610
129     DVOID=2.*RVOID                        STP41620
130     ELTC=FL-VOIDZL/FNPOW                STP41630
131     VTCPI=ELTC*RVOIDD**2                 STP41640
132     VVCID=(PI*FL*RVOIDD**2-VTC)          STP41650
133     900 CONTINUE                           STP41660
134     RETURN                                STP41670
135     1920 FORMAT(10 NOCONVERGENCE IN TEMP CALC AFTER 10 ITERATIONS. ASSUMED STP41680
136     1TEMP =',F7.2,' ,CALCULATED TEMP =',F7.2//') STP41690
137     1910 FORMAT(3X,26HNCON SPEC NO. ERROR NCNPF,13.8H   STEP4 ) STP41700
C***** ****

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* SOURCE STATEMENT (STEP4) *

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137      END                                STP41780

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* SOURCE STATEMENT *

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1      SUBROUTINE STEPS                                         STP50010
C      THIS SUBROUTINE IS CALLED FROM ST3T08                         STP50020
C      REAL MU,F,MOL,MOLEFR,MOLFR                               STP50030
2      COMMON /POWERAY/ PAVRG,FUELL,FL,POWER(21),AI(21),NPOW,PTOT,LPMAX,   STP50040
3      COMMON /POWERAY/ PKPOWR,IPEAK,DELPL,PMAX                      STP50050
4      COMMON /DATA 4/ PI,CCPINS,SECUDAY,AVOIDAD,RH,CONEN             STP50060
5      COMMON /DATA 5/ SDOT,SDOTT,EF,MUF,EPST,EPSC                STP50070
6      COMMON /COM 07/ TITLE(20),AA(7,30),BB(6,51),CF(3,30),HV(2,20)  STP50080
7      COMMON /COM 17/ TTC(51),TSRC(51),WIN(51),Q(51),TS(51),CLCRP(2,20) STP50090
8      COMMON /COM 02/ IPOW,ISTEP,ITER,KOUNT                         STP50100
9      COMMON /COM 03/ T01P,DELRQ,DELRC,DELRC,TCOL,STP                  STP50110
10     COMMON /COM 05/ BURNUP,TDAYS,VVOID,TOTLDY,TOTBUR               STP50120
11     COMMON /COM 5J/ DELRCC,DELRC,DELRC,TSHOUL                     STP50130
12     COMMON /COM 13/ RFS,FNPOW,RSINZ,RYOID2                         STP50140
13     COMMON /COM 15/ INCK,GAP                                     STP50150
14     COMMON /COM 21/ N,NN,NNN,INF                                STP50160
15     COMMON /COM025/ VOLUME                                     STP50170
16     COMMON /COM 35/ TBL,TBU,TCC,TCI,TCO,TF5,TH,THR               STP50180
17     COMMON /COM048/ DSIN,RSIN,TSIN,TSINC,DVOID,RYCID,IT          STP50190
18     COMMON /COM 56/ VOLGP,VOLGAP                                STP50200
19     COMMON /COM 57/ VRUF,ALPHAC,PRESCH                           STP50210
20     COMMON /COM RG/ GG(20,100)                                 STP50220
21     COMMON /COM157/ PC1,RCU                                     STP50230
22     COMMON /COM357/ TAVGC                                     STP50240
23     COMMON /COM568/ DELRB,DELRP,DELRC,DELRT,TAVGF,VAVGT           STP50250
24     COMMON /D15 / MDEN,MELOC,SINTEM                            STP50260
25     COMMON /MOL579/ PRESTO(20)                                STP50270
26     COMMON /MOL598/ TBAR(20)                                 STP50280
27     COMMON /INPUT / FRDEN,FRSIN,DSINZ,FRPU02,FR35,FR40,FR41,DFS+DCI,   STP50290
1      DCO,DVIDZ,VPLENZ,ATMOS,S,XX,ROU,ROUC,EXTP,DE,V,           STP50300
2      TINLET,DELT,TMAX,TFR,TM,DBUBK,WBC,SIGHT,IFLUX,            STP50310
3      NCLAD,NCON,NFLX,KUOL,NEWK,NEWCL,NEWFLX,VOIDZL,NOH,STP50320
4      FRACHE,FRACAR,FRACH,FRACN,FRACKR,FRACE,HGACEL,           STP50330
5      UTEMP,ZCLAD,HG,PEKAVG,MINI,ICDF,ISTOR,ICREP,ISWELL,STP50340
6      ,NEXP,MEXP,NH1ST                                         STP50350
28     COMMON /BURN / BURN(20),BUOLD(20)                          STP50360
29     COMMON /COM M5/ STREST                                    STP50370
30     COMMON /BNGAS/ AKH(20),AXE(20),PH(20),ENXE(20),ENKR(20)    STP50380
31     COMMON /ELONG/ FILENT(5)                                STP50390
32     COMMON /INPUT A/ MREST,LCHEP,DDISH,HDISH                 STP50400
33     COMMON /ST5DEN / DLPLD,DEDSL                           STP50410
34     COMMON /COMBW/ ISTOP,+1CASE                            STP50420
35     COMMON /REL01/ RGAPC(20),RFSC(20),DELEXP(20)             STP50430
36     C
37     DIMENSION      DELCT(50),DELL(50)                         STP50440
38     DATA SC1,SC2 /1.E-4,1.15E-4/                           STP50450
39     C
40     SC1,SC2 ARE STRESS COEFFICIENT IN CLADDING CREEP CALCULATION STP50460
41     C
42     6U      =BURN(IPOW)                                     STP50470
43     DO 100 I=1,20                                         STP50480
44     100 GG(1,ITER) = 0.0                                     STP50490
45     C
46     C      VOLUME AVERAGE THE TEMPERATURE.                   STP50500
47     C
48     42      TS(N+1)=RYOID                                STP50510
49     C
50     43      DU 910 1=1,N                                     STP50520
51     C
52     50      =BURN(IPOW)                                     STP50530
53     51      DO 100 I=1,20                                 STP50540
54     52      GG(1,ITER) = 0.0                               STP50550
55     C
56     53      C      VOLUME AVERAGE THE TEMPERATURE.       STP50560
57     C
58     54      TS(N+1)=RYOID                                STP50570
59     C
60     55      DU 910 1=1,N                                 STP50580
61     C
62     56      TS(N+1)=RYOID                                STP50590
63     C
64     57      TS(N+1)=SINTEM                            STP50600
65     C
66     58      TS(N+1)=SINTEM                            STP50610
67     C
68     59      TS(N+1)=SINTEM                            STP50620
69     C
70     60      TS(N+1)=SINTEM                            STP50630
71     C
72     61      TS(N+1)=SINTEM                            STP50640
73     C
74     62      TS(N+1)=SINTEM                            STP50650
75     C
76     63      TS(N+1)=SINTEM                            STP50660
77     C
78     64      TS(N+1)=SINTEM                            STP50670
79     C
80     65      TS(N+1)=SINTEM                            STP50680
81     C
82     66      TS(N+1)=SINTEM                            STP50690
83     C
84     67      TS(N+1)=SINTEM                            STP50700
85     C
86     68      TS(N+1)=SINTEM                            STP50710
87     C
88     69      TS(N+1)=SINTEM                            STP50720
89     C
90     70      TS(N+1)=SINTEM                            STP50730
91     C
92     71      TS(N+1)=SINTEM                            STP50740
93     C
94     72      TS(N+1)=SINTEM                            STP50750
95     C
96     73      TS(N+1)=SINTEM                            STP50760
97     C
98     74      TS(N+1)=SINTEM                            STP50770
99     C
100    75      TS(N+1)=SINTEM                            STP50780
101    C
102    76      ***** FUEL THERMAL EXPANSION *****      STP50790
103    CALL EXPAND (RFS+RD,TI,TF5,FRPU02,DELRT,DELL,L,NEXP,MEXP,  STP50800
104    1      RYOTU )                                         STP50810
105    C
106    77      ***** FUEL THERMAL EXPANSION *****      STP50820
107    78      ***** FUEL THERMAL EXPANSION *****      STP50830
108    79      ***** FUEL THERMAL EXPANSION *****      STP50840
109    80      ***** FUEL THERMAL EXPANSION *****      STP50850
110    81      ***** FUEL THERMAL EXPANSION *****      STP50860
111    82      ***** FUEL THERMAL EXPANSION *****      STP50870
112    83      ***** FUEL THERMAL EXPANSION *****      STP50880
113    84      ***** FUEL THERMAL EXPANSION *****      STP50890
114    85      ***** FUEL THERMAL EXPANSION *****      STP50900
115    86      ***** FUEL THERMAL EXPANSION *****      STP50910
116    87      ***** FUEL THERMAL EXPANSION *****      STP50920
117    88      ***** FUEL THERMAL EXPANSION *****      STP50930
118    CALL DENSF(FRDEN,BU,TSIN,RFS,DELRC,MDEN,DFS)           STP50940
119    C
120    89      ***** FUEL THERMAL EXPANSION *****      STP50950
121    90      ***** FUEL THERMAL EXPANSION *****      STP50960
122    91      ***** FUEL THERMAL EXPANSION *****      STP50970
123    92      ***** FUEL THERMAL EXPANSION *****      STP50980
124    93      ***** FUEL THERMAL EXPANSION *****      STP50990
125    94      ***** FUEL THERMAL EXPANSION *****      STP51000
126    95      ***** FUEL THERMAL EXPANSION *****      STP51010
127    96      ***** FUEL THERMAL EXPANSION *****      STP51020
128    97      ***** FUEL THERMAL EXPANSION *****      STP51030
129    98      ***** FUEL THERMAL EXPANSION *****      STP51040
130    99      ***** FUEL THERMAL EXPANSION *****      STP51050
131    100     ***** FUEL THERMAL EXPANSION *****      STP51060
132    101     ***** FUEL THERMAL EXPANSION *****      STP51070
133    102     ***** FUEL THERMAL EXPANSION *****      STP51080
134    103     ***** FUEL THERMAL EXPANSION *****      STP51090
135    104     ***** FUEL THERMAL EXPANSION *****      STP51100
136    105     ***** FUEL THERMAL EXPANSION *****      STP51110
137    106     ***** FUEL THERMAL EXPANSION *****      STP51120
138    107     ***** FUEL THERMAL EXPANSION *****      STP51130
139    108     ***** FUEL THERMAL EXPANSION *****      STP51140
140    109     ***** FUEL THERMAL EXPANSION *****      STP51150
141    110     ***** FUEL THERMAL EXPANSION *****      STP51160
142    111     ***** OLD SWELLING MODEL *****      STP51170
143    112     DELVB=(SDOT*VOLUME*FRDEN+SDOTT*VC)*BU      /1.E4-(1.-FRDEN)*(1.+VH+,*STP51170
144    113     13*VC+.3*VL)                                STP51180

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* SOURCE STATEMENT (STEPS) *

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84      IF(DELVB) 940,940,950                               STP51190
85      940  DELVB=U,                                     STP51200
86      950  CONTINUE                                     STP51210
87      DELRB=DELVB/(3.*PI*RFS)                           STP51220
C      ****
C      88      GG(11,ITER) = DELRB                         STP51230
C      89      TAVGC=(TCI+TCG)/2.                           STP51240
C      C      CLADDING THERMAL EXPANSION AA(b,j)           STP51250
C      C      90      IN1 = 7                                STP51260
C      91      IN2 = 30                                 STP51270
C      92      ALPHAC = TERP(TAVGC,AA,6,NN,IN1,IN2,IN3,56)   STP51280
C      93      DELRC=RCI*ALPHAC*(TAVGC-25.)               STP51290
C      94      DELRC1=DELRC                            STP51290
C      95      DELRC0=RCC*ALPHAC*(TAVGC-25.)               STP51300
C      96      DELRC=U,                                 STP51310
C      97      PRESI=ATMOS*14.696*((TCI+TFS)/2.0)+273.0/298.  STP51320
C      98      IF((ISTEP,LE,1,AND,ITER,LE,1)) PRESTO(1)=PRESI  STP51330
C      99      PRESCN=2.0*(EXTP*(RCO+DELRC0)**2-PRESTO(ISTEP)*(RCI+DELRC)**2)  STP51340
C      C      CLADDING CREEP                                STP51350
C      C      100     IF(ICREP.LE.0) GO TO 960                STP51360
C      101     IN1 = 2                                STP51370
C      102     IN2 = 20                                 STP51380
C      103     DELRC = TERP(TOTLDY,CLCRP,2,NCR,IN1,IN2,IN3,57)  STP51390
C      104     960  CONTINUE                                STP51400
C      105     IF(ICREP.GE.0) GO TO 962                STP51410
C      C      **** CLADDING CREEP ****                      STP51420
C      106     ICRP=1*ICREP                                STP51430
C      107     CALL CAEP(TOTLDY*24.,IHC(IPOW),STRESS,TAVGC,EXIP,PRESTO(ISTEP),  STP51440
C      108     1      UCO,DCI,SC1,SC2,EPST,DEPS,ICK)          STP51450
C      109     DELRC=RCI*EPST                                STP51460
C      C      ****
C      110     DELRC=DELRC-DELRC                           STP51470
C      111     DELRC0=DELRC0-DELRC                           STP51480
C      112     DELRP=U,                                 STP51490
C      113     GO TO 970                                STP51500
C      114     962  CONTINUE                                STP51510
C      115     IF((ICDF.GT.0.0)) GO TO 970                STP51520
C      C      CLADDING ELASTIC DEFORMATION                 STP51530
C      C      116     IN1 = 7                                STP51540
C      117     IN2 = 30                                 STP51550
C      118     EC = TERP(TAVGC,AA,4,NN,IN1,IN2,IN3,58)       STP51560
C      119     CMU = TERP(TAVGC,AA,5,NN,IN1,IN2,IN3,59)       STP51570
C      120     DELRP=(RCI+DELRC)/EC*((RCO+DELRCU)**2-(RCI+DELRC)**2)*((PRESTO(ISTEP)-CMU)*(PRESTO(ISTEP)-CMU))  STP51580
C      121     15*EXTP*((RCO+DELRCU)**2*(1.+CMU))           STP51590
C      122     DELRC=DELRC+DELRP                            STP51600
C      123     DELRC0=DELRC0+DELRP                           STP51610
C      124     PRESCN=0,                                 STP51620
C      970  CONTINUE                                STP51630

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* SOURCE STATEMENT (STEPS) *

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125     DELH=DELRT+DELRE+DELRD                           STP51640
126     TH=GAP/2.*DFLRC-DELH                           STP51650
127     GU(15,ITER) = TH                                STP51660
128     THX = TH - 1.98*(RHOUF + RHOUC)               STP51670
129     GG(12,ITER) = THXX                            STP51680
130     DELRBH=0.0,                                 STP51690
131     DELRHP=0.0,                                 STP51700
132     132  IF((ISHELL=1)) 1000,1000,980              STP51710
133     950  CONTINUE                                STP51720
134     IF((THXX.LE.0.0)) GO TO 1000                STP51730
C      FUEL SWELLING
C      ISHELL = 0  SWELLING IS NOT TAKEN INTO ACCOUNT  STP51740
C      ISHELL = 1  GEITHOF, ET AL, MODEL (OLD SWELLING MODEL)  STP51750
C      ISHELL = 2  REVISED GAP CLOSURE MODEL (NEW SWELLING MODEL)  STP51760
C      **** NEW SWELLING MODEL ****                  STP51770
135     GG(20,ITER) = 4HNEW                           STP51780
136     CALL SWELL(R1300,R1500,R1700,RFS,RVOID,PI,BU,TH,GAP,DELRT,DELRD)  STP51790
137     1HC,DELBH,RHOUF,RHOUC,THRF,DELBRH,DELRD)        STP51800
138     GG(13,ITER) = DELRBH                          STP51810
139     GG(16,ITER) = TH                                STP51820
C      ****
C      139  IF(TH.GT.0) GO TO 990                      STP51830
C      140  IF(TH.GT.(1.98*(RHOUF+RHOUC) + 1.0E-6)) GO TO 990  STP51840
C      140  TH=1.98*(RHOUF+RHOUC)+1.0E-6             STP51850
141     GG(17,ITER) = TH                                STP51860
142     990  CONTINUE                                STP51870
143     IF(DELRH,LT,DELRBH,AND,TH.GT.0) DELRH=DELRBH  STP51880
144     GG(14,ITER) = DELRB                           STP51890
145     1000  CONTINUE                                STP51900
146     DELRRE=0.0,                                 STP51910
147     IF(MRELOC.LE.0) GO TO 1100                  STP51920
C      ----- GAP WAS CLOSED , THXX.LE.0.0            STP51930
148     IF((THXX.LE.0.0)) GO TO 1100                STP51940
C      PPPPP=(POWER(IPOW)+POWER(IPOW+1))/2.0         STP51950
C      **** FUEL RELOCATION MODEL ****              STP51960
150     CALL RELOC(DELRRE,DFS,GAP,PPPPP,IPOW+NPOW,MRELOC)  STP51970
C      ****
C      151     IF(DELRRE) 1120,1120,1120                STP51980
152     1120  DELRRE=0.0,                            STP51990
153     GO TO 1100,                                STP52000
154     1130  CONTINUE                                STP52010
155     IF((THXX-DFLRRE) 1110,1110,1100              STP52020
C      IF GAP WAS STICKED DUE TO RELOCATION , CORRECT GAP WIDTH  STP52030
156     1110  THDM=1.98*(RHOUF+RHOUC)+1.E-6          STP52040
157     DELRRE=GAP/2. + DELRC - DELR - THDM          STP52050
158     1100  CONTINUE                                STP52060
C      DELR=DELRT+DELRB+DELRD+DELRRE                STP52070
159     TH=GAP/2. + DELRC - DELR                      STP52080
C      TH=TH-1.98*(RHOUF+RHOUC)                      STP52090
160     VOLGAP=P1/4.*((DC1)+2.*DELR)**2-(DFS+2.*DELR)**2*FL  STP52100
161     CRUF=1.980*(RHOUF+RHOUC)                      STP52110
162     VRUF=PI*DFS*CRUF*FL                          STP52120
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164

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FACOM 230-75 (M7) FORTRAN-D -760229+ V06-L07 76.09.03 PAGE 142

* SOURCE STATEMENT (STEPS 1*)

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165 IF(VOLGAP.LE.VRUF) VOLGAP=VRUF           STP52370
166 VOLGP=VOLGAP+VVG1D                      STP52380
167 VCGD=R1*(CRFS+ DELR)*#2-R1350**2)      STP52390
168 VCGD=R1*(CRFS+ DELR)*#2-R1350**2)      STP52400
169 VRU1=R1*(R1700**2-RVOID**2)             STP52410
170 RDISH = DDISH/2.                          STP52420
171 TSHOUL=TEPP(RDISH,TT,TS,N)              STP52430
172 PLENGT(1)=L                             STP52440
173 PLENGT(2)=FL*(1.+FALPHA(TSHOUL,NEXP)*(TSHOUL-25.)) STP52450
174 PLENGT(3)=FL*(1.+FALPHA(TT(N),NEXP)*(TT(N)-25.)) STP52460
175 PLENGT(4)=PLENGT(2)+PLENGT(1)          STP52470
176 PLENGT(5)=PLENGT(3)-PLENGT(1)          STP52480
C----- TH IS HOT GAP AT THIS STEP ,CALCULATE COLD GAPC(IPW) STP52490
C----- COLD GAP DEFINE AT ROOM TEMPERATURE (25, DEG C) STP52500
C----- COLD GAP DEFINE AT ROOM TEMPERATURE (25, DEG C) STP52510
C----- COLD GAP DEFINE AT ROOM TEMPERATURE (25, DEG C) STP52520
177 XDLR = 0.0                           STP52530
178 DO 10 I=1,N                         STP52540
179   T1 = BB(3,I)                        STP52550
180   T2 = BB(3,I+1)                      STP52560
181   T3 = (T1+T2)/2.0                   STP52570
182   ALP = FALPHA(T3,NEXP)              STP52580
183   RINGR = BB(4,I) - BB(4,I+1)        STP52590
184   DELRN = RINGR*ALP*(25.-T3)         STP52600
185   XDLR = XDLR + DELRN               STP52610
186 10 CONTINUE                         STP52620
187  DELEXP(IPW) = XDLR                 STP52630
188  RGAPC(IPW) = TH-XDLR               STP52640
189  RFSD(IPW) = (RFS+DELR) + XDLR     STP52650
190  RETURN                               STP52660
191  *****END*****                      STP52670
                                         STP52680
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* SOURCE STATEMENT *

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1      SUBROUTINE STEPSA                                         ST5A0010
C
C THIS SUBROUTINE IS CALLED FROM ST3TOR                         ST5A0020
C
C
2      REAL MUFL,MOLFL,MOLEFR,MOLFR                           ST5A0030
3      COMMON /POWRAY/ PAVRG,FUELLE,FL,POUER(21),AA(21),NPOW,PTOT,LPMAX,   ST5A0040
4      1      PKOWN,IPEAK,DELP,PMAX                                ST5A0050
5      COMMON /DATA 4/ PI,CCPIN3,SECUDAY,AVGAD,RK,CONEN          ST5A0070
6      COMMON /COM 5/ SDOT,SDOT1,EF,MUF,EPSC,EPSCIC             ST5A0080
7      COMMON /COM 6/ TITLE(20),AA(1,30),BB(6,31),CF(3,30),HV(2,20) ST5A0090
8      COMMON /COM 1/ TTK(51),TSRC(51),IN(51),T(51),CLCRP(2,20) ST5A0100
9      COMMON /COM 02/ IPDN+1,STEP,ITER,KOUNT                  ST5A0110
10     COMMON /COM 03/ TOTP+DELRC,DELRC,DELRC,TCOOL,STP        ST5A0120
11     COMMON /COM 05/ BURNUP,TDAYS,VVOID,TOTLDY,TOTBUR         ST5A0130
12     COMMON /COM 3/ DELRCC,DELRC,DELRC,TSHOU                 ST5A0140
13     COMMON /COM 13/ RFS,FNHOW,RSINZ,RVOIDZ                 ST5A0150
14     COMMON /COM 15/ NCR,GAP                                ST5A0160
15     COMMON /COM 21/ N,NN,NNN,NF                             ST5A0170
16     COMMON /COM25/ VOLUME                                 ST5A0180
17     COMMON /COM 35/ TBT,TB0,TCC,TC1,TC0,TFS,TH,THR          ST5A0190
18     COMMON /COM46/ DSIN,RSINT,TSIN,TINC,DV01D,RVOID1,T       ST5A0200
19     COMMON /COM 56/ VOLGP,VOLGAP                            ST5A0210
20     COMMON /COM 57/ VRUF,ALPHAC,PRESCN                   ST5A0220
21     COMMON /COM 86/ GG(20,100)                            ST5A0230
22     COMMON /COM157/ RCI,RC0                                ST5A0240
23     COMMON /COM357/ TAVGC                                 ST5A0250
24     COMMON /COM568/ DELRB,DELHP,DELRCI,DELRT,TAVGF,VAVGT    ST5A0260
25     COMMON /D15/ MLEN,MELUC, SINTEM                      ST5A0270
26     COMMON /ML5938/ TBAR(20)                            ST5A0280
27     COMMON /INPUT / FROEN,FRSIN,DSINZ,FPPU02,FR35,FR40,FR41,DFS,RC1,   ST5A0290
1      DCD,DV01D,VPLNZ,ATMOS,S,XX,R0UF,ROUC,EXTP,DE,V,       ST5A0300
2      TFL,LET,DELTA,MAX,TFR,IM,DRD,BK,HBC,SIGHF,IFLUX,      ST5A0310
3      NCAD,NCON,NFLX,KROL,NEWK,NEWCL,NEFLA,VOLDL,NOH,I      ST5A0320
4      FRACHE,FRACAR,FRACH,FRACNR,FRACRE,FRACCE,MGACEL,    ST5A0330
5      DTMP,LCLAD,HG,PEKAVG,MINI,ICDF,ISTOR,ICREP,IS4ELL,ST5A0340
6      <NEXP>,EXH,NHIST                                     ST5A0350
28     COMMON /BURN / BUHN(20),BUUD(20)                      ST5A0360
29     COMMON /COM 55/ R1700,R1500,R1350                     ST5A0370
30     COMMON /COM 55/ STA,FST                               ST5A0380
31     COMMON /ENGGAS/ AKH(20),AHE(20),PH(20),ENXE(20),ENKR(20) ST5A0390
32     COMMON /ELUNG/ PLNGT(5)                            ST5A0400
33     COMMON /INPUT / PREST1,LCHEP,UDTSH,HDISH            ST5A0410
34     COMMON /CUDATA/ RESGAH,PCOUNT                      ST5A0420
35     COMMON /ST50HN / DLPLD,DENSL                      ST5A0430
36     COMMON /CUMB8/ ISTOP+1CASE                        ST5A0440
37     COMMON /GRADE/ IGRADE,HTOPG,RINT                  ST5A0450
38     C
39     DIMENSION DELCT(50),DELL(50)                      ST5A0460
40     DATA SC1,SC2 /1,E-4,1,1D-4/                      ST5A0470
41     C
42     SC1,SC2 ARE STRESS COEFFICIENT IN CLADDING CREEP CALCULATION ST5A0480
43     C
44     50      =BUR4(IPDN)
45     DO 100 I=1,20
46     100 GGI,ITER) = 0.0
47     C
48     FUEL VOLUME AVERAGED TEMPERATURE                  VAVGT(DEG-C) ST5A0490
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50     TSH(N+1)=RVOID
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* SOURCE STATEMENT (STEPSA) *

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44     910 I=1,N                                         ST5A0600
45     911
46     910 TSH(I)=(RFS+DELRL)-(CC(RFS+DELRL)-RVU1D)/FLOAT(N)*(B1-1.0) ST5A0610
47     VAFLR=(TSP(1)*#2-TS(2)*#2)*PI*(TFS+TT(1))*,.5) ST5A0620
48     920 I=2,N                                         ST5A0630
49     VAFLR=VAFLR+(TSR(1)*#2-TSR(1+1)*#2)*PI*(TT(1)+TT(1-1))*,.5) ST5A0640
50     CONTINUE                                         ST5A0650
51     VAVGT=VAFLR/((CC(RFS+DELRL)-RVU1D)*#2*PI) ST5A0660
52     IF(KOUNT,EW,0) TBAN(RF)=VAVGT
53     C
54     FUEL RADIUS AVERAGED TEMPERATURE                TAVGF(DEG-C) ST5A0670
55     C
56     TEMP=0,                                           ST5A0680
57     DO 930 I=1,N                                     ST5A0690
58     930 TEMP = TEMP + (BB(3,I) + BB(3,I+1)) / 2.0 ST5A0700
59     TAVGF = TEMP / FLOAT(N)                         ST5A0710
60     C
61     CLADDING THERMAL EXPANSION AA(6,J),DELRC,GAP1 ST5A0720
62     IN1 = 7                                         ST5A0730
63     IN2 = 30                                         ST5A0740
64     ALPHAC = TERP(TAVGC,AA,6,NN,IN1,IN2,IN3,56) ST5A0750
65     DELRC=RC0*ALPHAC*(TAVGC=25.)
66     PRESI=ATMOS*14.696*((TC1+TFS)/2.)+273./298. ST5A0760
67     IF(ISTEP,EW,1) AND(ITER,EW,1) PRESTO(1)=PRESI ST5A0770
68     PRESI=2.0*(EXTP*(RC0+DELRC)**2-(RC1+DELRC)**2)*(1,-CMU)+(PRESTO(1)ISTEP)ST5A0780
69     GAP01 = GAP/2.0                                  ST5A0790
70     GAP1 = GAP01 + DELRL                            ST5A0795
71     C
72     CLADDING ELASTIC DEFORMATION AA(4,J),AA(5,J),DELRL,GAP2 ST5A0800
73     DELRL = 0.0                                      ST5A0810
74     IF(ICDF,EW,0) GO TO 970                         ST5A0820
75     IN1 = 7                                         ST5A0830
76     IN2 = 30                                         ST5A0840
77     EC = TERP(TAVGC,AA,4,NN,IN1,IN2,IN3,58) ST5A0850
78     CMU = TERP(TAVGC,AA,5,NN,IN1,IN2,IN3,59) ST5A0860
79     DELRL=(RC1+DELRC)**2-(RC0+DELRC)**2*(1,-CMU)+(PRESTO(1)ISTEP)ST5A0870
80     1-EXTP*(RC0+DELRC)**2*(1,-CMU))               ST5A0880
81     2-EXTP*(RC1+DELRC)**2*(1,-CMU))               ST5A0890
82     DELRCC=DELRL+DELRP                            ST5A0900
83     DELRC=DELRL+DELRLP                           ST5A0910
84     PRESI=0,                                         ST5A0920
85     970 CONTINUE                                     ST5A0930
86     GAP2 = GAP1 + DELRL                           ST5A0940
87     C
88     CLADDING CREEP                                CLCRP,DELRC,DELRL,GAP3 ST5A0950
89     DELRCC = 0.0                                     ST5A0960
90     IF(ICREP,EW,0) GO TO 962                      ST5A0970
91     IF(ICREP,LT,0) GO TO 960                      ST5A0980
92     IN1 = 2                                         ST5A0990
93     IN2 = 20                                         ST5A1000
94     DELRCC = TERP(TOTLDY,CLCRP,2,NCR,IN1,IN2,IN3,57) ST5A1010
95     GO TO 961                                     ST5A1020
96     960 CONTINUE                                     ST5A1030
97     ICR=-1*ICREP                                    ST5A1040
98     ST5A1050
99     ST5A1060
100    ST5A1070
101    ST5A1080
102    ST5A1090
103    ST5A1100
104    ST5A1110
105    ST5A1120
106    ST5A1130
107    ST5A1140
108    ST5A1150
109    ST5A1160
110    ST5A1170
111    ST5A1180

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* SOURCE STATEMENT (STEP5A)*

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89      CALL CREEP(TOTLDY*24.,PH1(IPOW),STREST,TAVGC,EXTP,PRESTO,(STEP), ST5A1190
       1      DCO,DC1,SC1,SC2,EPST,DEPS,ICK )
90      DELRC = (-1)*RCI*EPST ST5A1200
91      961 DELRC = DELRC + DELRCC ST5A1210
92      DELRC = DELRC + DELRCC ST5A1220
93      962 CONTINUE ST5A1230
94      GAP3 = GAP2 + DELRCC ST5A1240
95      C FUEL DENSIFICATION MDEN,DELROE ST5A1250
96      C
97      DELROE=0.0 ST5A1260
98      DENSE,BU,C ST5A1270
99      IF(MDEN,LE,0) GO TO 931 ST5A1280
100     TSIN,SINTEM ST5A1290
101     CALL DENSF(FRDEN,BU,TSIN,RFS,DELROE,MDEN,DFS) ST5A1300
102     DELS=DELPHD ST5A1310
103     931 CONTINUE ST5A1320
104     GAP9 = GAP3 - DELROE ST5A1330
105     RUMIT = RFS + GAP9 + DELROE ST5A1340
106     103 CONTINUE ST5A1350
107     104 REGAP = 2.0*(RHOUF + ROUC) + 1.E-5 ST5A1360
108     105 IGRDOL = IGRADE ST5A1370
109     106 IN1 = 0 ST5A1380
110     107 IN2 = IN1 + 1 ST5A1390
111     108 RL300 = TEMP(1300.,BU,2,IN1,IN2,IN3,52) ST5A1400
112     109 RL350 = TEMP(1350.,BU,2,IN1,IN2,IN3,53) ST5A1410
113     110 RL400 = TEMP(1400.,BU,2,IN1,IN2,IN3,54) ST5A1420
114     111 RL450 = TEMP(1700.,BU,2,IN1,IN2,IN3,55) ST5A1430
115     112 IF(MREST,LT,0) RL700 = RSIN ST5A1440
116     113 GO20,ITER) = 4HNO ST5A1450
117     C MOST CONSERVATIVE FUEL SWELLING ST5A1460
118     118 RSWEL = DELRB = 0.0 ST5A1470
119     119 IF(CISWELL,LE,0) GO TO 510 ST5A1480
120     120 GU(20,ITER) = 4HOLD ST5A1490
121     121 CALL SWELLAT_1 ,RL300,RL350,RL400,RL450,RVOID,P1,BU, SDOT,SDOT,VOLUME,FRDEN,DELVB,DELRA) ST5A1500
122     122 IF(DELRA,LT,0.0) DELRE = 0.0 ST5A1510
123     123 RSWEL = DELRB ST5A1520
124     124 510 CONTINUE ST5A1530
125     C CONSERVATIVE FUEL THERMAL EXPANSION ST5A1540
126     125 RALPHA = DELRT = 0.0 ST5A1550
127     126 RD = CRF - RVOID ) / FLOAT(N) ST5A1560
128     127 IF(CNEXPA,LE,0) GO TO 520 ST5A1570
129     128 CALL EXPAND_ (RFS,RD,TT,TFS,FRPUC2,DELRT,DELCT,CELL,L,NEXP+2 , RVOID ) ST5A1580
130     130 RALPHA = DELRT ST5A1590
131     131 520 CONTINUE ST5A1600
132     132 DELRSM = RSWEL + RALPHA ST5A1610
133     133 ROLD = RFS + DELROE + DELRT + DELRB ST5A1620
134     134 IF(CDELRS,LE,GAP9) GO TO 530 ST5A1630
135     135 IGRAD = 1 ST5A1640
136     136 RINT = DELRSM - GAP9 ST5A1650
137     137 130 CONTINUE ST5A1660
138     138 RINT = 1 ST5A1670
139     139 RINT = DELRSM - GAP9 ST5A1680
140     140 130 CONTINUE ST5A1690
141     141 530 CONTINUE ST5A1700
142     142 DELRSM = RSWEL + RALPHA ST5A1710
143     143 IF(CDELRS,LE,GAP9) GO TO 540 ST5A1720
144     144 IGRAD = 1 ST5A1730
145     145 RINT = DELRSM - GAP9 ST5A1740
146     146 130 CONTINUE ST5A1750
147     147 RINT = 1 ST5A1760
148     148 130 CONTINUE ST5A1770

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* SOURCE STATEMENT (STEP5A)*

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C RINT IS POSITIVE ST5A1780
132     DELRME=0.0 ST5A1790
133     GO TO 900 ST5A1800
134     530 CONTINUE ST5A1810
C FUEL THERMAL EXPANSION AS SPECIFIED NEXP AND MEAP ST5A1820
135     RALPHA = DELRT = 0.0 ST5A1830
136     IF(CNEXP,LE,0) GO TO 540 ST5A1840
137     CALL EXPAND_ (RFS,RD,TT,TFS,FRPUC2,DELRT,DELCT,CELL,L,NEXP,MLXP, RVOID ) ST5A1850
138     138 RALPHA = DELRT ST5A1860
139     540 CONTINUE ST5A1870
140     140 DELRSM = RSWEL + RALPHA ST5A1880
141     141 IF(CDELRS,LE,GAP9) GO TO 570 ST5A1890
142     142 IGRAD = 2 ST5A1900
143     143 RINT = DELRSM - GAP9 ST5A1910
144     144 DELRE=0.0 ST5A1920
145     145 GO TO 900 ST5A1930
146     146 570 CONTINUE ST5A1940
C FUEL SWELLING CALCULATION AS SPECIFIED ISWELL ST5A1950
147     147 RSWEL = DELRB = 0.0 ST5A1960
148     148 IF(CISWELL,LE,0) GO TO 580 ST5A1970
149     149 IF(CISWELL,LE,2) GO(20,ITER) = 4HNEW ST5A1980
150     150 CALL SWELLAT_(ISWELL,RL300,RL350,RL400,RL450,RVOID,P1,BU, SDOT,SGQT,VOLUME,FRDEN,DELVB,DELRA) ST5A1990
151     151 IF(DELRA,LT,0.0) DELRE = 0.0 ST5A2000
152     152 RSWEL = DELRB ST5A2010
153     153 580 CONTINUE ST5A2020
154     154 DELRSM = RSWEL + RALPHA ST5A2030
155     155 IF(CDELRS,LE,GAP9) GO TO 590 ST5A2040
156     156 IGRAD = 3 ST5A2050
157     157 DELRSM = GAP9 ST5A2060
158     158 DELRK = GAP9-RALPHA ST5A2070
159     159 RINT = 0.0 ST5A2080
160     160 PCONT = 0.0 ST5A2090
161     161 DELRE=0.0 ST5A2100
162     162 GO TO 800 ST5A2110
163     163 590 CONTINUE ST5A2120
C FUEL RELOCATION MRELOC,RRELOC ST5A2130
164     164 RRELOC = DELRRE = 0.0 ST5A2140
165     165 IF(CMELOC,EQ,0) GO TO 600 ST5A2150
166     166 PPPP = ((POWER(IPOW)+POWER(IPOW+1))/2, ST5A2160
167     167 CALL RELOC(DELRRE,DFS,GAP,PPPPP,IPOW,NPOW,MRELOC) ST5A2170
168     168 IF(CDELRE,LT,0.0) DELRRE = 0.0 ST5A2180
169     169 RRELOC = DELRRE ST5A2190
170     170 600 CONTINUE ST5A2200
171     171 DELRSM = RSWEL + RALPHA + RRELOC ST5A2210
172     172 IF(CDELRS,LE,GAP9) GO TO 610 ST5A2220
173     173 IGRAD = 4 ST5A2230
174     174 RINT = DELRSM - GAP9 ST5A2240
175     175 PCONT=0.0 ST5A2250
176     176 GO TO 900 ST5A2260
177     177 610 CONTINUE ST5A2270
178     178 IGRAD = 5 ST5A2280

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* SOURCE STATEMENT (STEP5A)*

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179      DELRSM = DELRT + DELRB + DELRRE          ST5A2370
180      HOTGP = GAP9 - DELRSM + RESGAP         ST5A2380
181      RINT = 0.0                               ST5A2390
182      PCONT=0.0                             ST5A2400
183      GO TO 900                            ST5A2410
184      800 CONTINUE                         ST5A2420
C      CONTACT PRESSURE ASSUMPTION ( PCONT ) IN KG/CM2   ST5A2430
C      CONTACT      CONTACT                  ST5A2440
C      GRADE       PRESSURE                 ST5A2450
C      (GRADE)     (ASSUMED)                ST5A2460
C      (KG/CM2)                 ST5A2470
C      A  1 HARD1      PFACE(CALCULATED IN STEP?)  ST5A2480
C      b  2 HARD2      170.(MAX)    76. + 94*COEF   ST5A2490
C      C  3 SOFT       0.                      ONLY SWELLING   ST5A2500
C      D  4 SOFT       0.                      SWELLING + RELOCATION ST5A2510
C      E  5 OPEN       0.                      ST5A2520
C      C      DEFINE RINTMX                   ST5A2530
C      C      RINTMX = (RFS + DELRDE + DELRSM ) * RLIMIT / ROLD  ST5A2540
C      *      = (RFS + DELRDE + GAP9)           ST5A2550
185      COEF = RINT / RINTMX                  ST5A2560
186      IF((COEF.LT..0.OR.COEF.GT.1.) WRITE(6+2020) COEF,IGRADE  ST5A2570
187      IF((COEF.LT..0.OR.COEF.GT.1.) STOP             ST5A2580
188      IF((GRADE,E0.2) PCONT =170. * COEF           ST5A2590
189      IF((GRADE,E0.3) PCONT = 76. * COEF           ST5A2600
190      IF((ITER.GT.1.AND.IGDOLD,E0.4.AND.IGRADE,E0.2) PCONT = 170.*COEF  ST5A2610
191      900 CONTINUE                         ST5A2620
192      GO(18,ITERJ) = RINT                  ST5A2630
193      GO(19,ITERJ) = IGRADE                ST5A2640
194      C      DELR CALCULATION               ST5A2650
C      C      DELR = DELRSM + DELRDE          ST5A2660
195      TH = HOTGP                          ST5A2670
196      VCOLD = PI*(RFS + DELR)**2 - R1350**2  ST5A2680
197      VCOLD = PI*(R1350**2 - R1700**2)        ST5A2690
198      VMOT = PI*(R1700**2 - RV010**2)        ST5A2700
200      RDISH = DVISH/2.                     ST5A2710
201      TSHOUL=TEPP(RDISH,TT,TS,N)          ST5A2720
202      PLENGT(1)=L                         ST5A2730
203      PLENGT(2)=L*(1.+FALPHA(TSHOUL+NEXP)*(TSHOUL-25.))  ST5A2740
204      PLENGT(3)=L*(1.+FALPHA(TT(N)+NEXP)*(TT(N)-25.))  ST5A2750
205      PLENGT(4)=PLENGT(2)-PLENGT(1)        ST5A2760
206      PLENGT(5)=PLENGT(3)-PLENGT(1)        ST5A2770
207      RETURN                                ST5A2780
C      *      1      *      2      *      3      *      4      *      5      *      6      *      7  ST5A2790
208      2000 FORMAT(7X,'MEAP SPEC ERROR  MEXP='',15.5X,7H STEP5A,    ) ST5A2800
209      2010 FORMAT(7X,'INFRINT ERROR, 4X, 8H IGRADE='',13.4X,7H FRINT='',  ) ST5A2810
1. F12.5, 5X, 7H STEP5A                      ) ST5A2820
210      2020 FORMAT(7X,'COEF ERROR   COEF='',F12.5,5X,'IGRADE='',15.5X,'STEP5A' ) ST5A2830
*                                         ) ST5A2840
211      END                                  ST5A2850

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* SOURCE STATEMENT *

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1      SUBROUTINE STEP6
2      C
3      C THIS SUBROUTINE IS CALLED FROM ST3T08
4      C
5      REAL MU,FML,MOL,MOLEFR,MOLEFR
6      COMMON /DATA 1/ 2R(T,6),ZR4(T,6)*ST(7,26)+TABLE(2* 80)
7      COMMON /DATA 2/ EKLJ(6),GMWT(6),SIGLJ(6)
8      COMMON /COM 35/ TBL,TBC,TCC,TCI,TCO,TFS,TH,THR
9      COMMON /COM678/ TOTMOL,ABTGAS,VISMIX,GK,GASKON
10     COMMON /COM600/ TGAS,LOC1,HGOLD
11     DIMENSION PHICAP(6,6),CSUBP(6),VISCOS(6),OMEGA(6),CON(10)
12     TGAS=(C1+TFS)/2,
13     ABTGAS=(TGAS)+273.
14
15     C
16     C CALCULATE THERMAL CONDUCTIVITY AND VISCOSITY OF THE GAS
17
18     DO 1040 I=1,6
19     TKE=ABTGAS/EKLJ(I)
20     IN1 = 2
21     IN2 = BC
22     OMEGA(I) = TERP(TKE, TABLE+2,BU,IN1,IN2+IN3+61)
23
24     1040 CONTINUE
25     DO 1050 J=1,6
26     VISCOS(J)=2.67E-5*SQRT(ABTGAS*GMWT(I))/(OMEGA(I)*SIGLJ(I)**2)
27
28     1050 CONTINUE
29     DO 1060 J=1,6
30     PHICAP(I,J)=1./SQRT(8.)/(SQRT(1.+GMWT(I)/GMWT(J)))*(1.+SWRT(VISCOS(J))
31     1/J/VISCOS(J))*(GMWT(J)/GMWT(I))**2
32
33     1060 CONTINUE
34     DO 1070 I=1,6
35     IF(I.EQ.3) GO TO 1070
36     IF(I.EQ.4) GO TO 1070
37
38     COi(I)=1.9891E+4*(SQRT(ABTGAS/GMWT(I)))/(SIGLJ(I)**2*OMEGA(I))
39
40     1070 CONTINUE
41     CSUBP(3)=6.947-0.2UE-3*ABTGAS+,608E-7*ABTGAS**2
42     CSUBP(4)=6.524+1.25E-3*ABTGAS-1.E-9*ABTGAS**2
43
44     DO 1080 I=3,4
45     COi(I)=(CSUBP(I)+1.25*1.987)*VISCOS(I)/GMWT(I)
46
47     1080 CONTINUE
48     GASKON=0,
49     VISMIX=0,
50     DO 1090 I=1,6
51     DEGOM=,
52     DO 1090 J=1,6
53     DEGOM=DENUM*MOLEFR(J)*PHICAP(I,J)
54
55     1090 CONTINUE
56     GASKON=GASKON+MOLEFR(I)*CON(I)/DENOM
57     VISMIX=VISMIX+MOLEFR(I)*VISCOS(I)/DENOM
58
59     1100 CONTINUE
60     GK = GASKON * 4.1H58
61
62     RETURN
63
64     ****
65
66     END

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* SOURCE STATEMENT *

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1      SUBROUTINE STEP7
2      C THIS SUBROUTINE IS CALLED FROM STOTOR
3      C
4      REAL MUF,MOL,MOLEFR,MLPFR
5      COMMON /FTNVT / FNTV(20),INVT(20)
6      COMMON /IYIELD/ IYIELD
7      COMMON /POXRAY/ PAVG,FUELL,FL,POWER(21),AI(21),NPWR,PTOT,LPMAX,
8      1          PKPWR,IPEAK,DELP,PRMAX
9      COMMON /DATA 4/ PI,CCPIN,SECDAY,AVOGAD,RR,CONEN
10     COMMON /DATA 5/ SCUT,SIOT1,EF,MUF,BPSI,F,EPSTC
11     COMMON /COM 0/ TITLE(20),AA(7,30),BB(6,51),CF(3,30)+RV(2,20)
12     COMMON /COM 1/ TTK(51),TSR(51),W(51),TS(51),CLCRP(2,20)
13     COMMON /COM 02/ IPWR,ITER,KOUNT
14     COMMON /COM 03/ TOP,IP,DELRC,DELRC,TCOL,STP
15     COMMON /COM 05/ BURNUP,TDAYS,VVOID,TOTLTY,TOTBUR
16     COMMON /COM 08/ II,JCEA,E,TCOOL,AMOTOT
17     COMMON /COM 13/ RFS,FPNPOW,RSLNZ,PVOIDZ
18     COMMON /COM 14/ KCON
19     COMMON /COM 21/ N+N,NMN,NF
20     COMMON /COM 35/ TB1,TB2,TC1,TC2,TC3,TFS,TH,THK
21     COMMON /COM 56/ VOLGP+VOLGAP
22     COMMON /COM 57/ VRUF,ALPHAC,PRESCN
23     COMMON /COM 86/ GG(70,100)
24     COMMON /COM 90/ VOLGAS,W,HGC
25     COMMON /COM357/ TAVGC
26     COMMON /COM378/ TOTMOL,ABTGAS,VISMIX,GK,GASKON
27     COMMON /MUL78/ PRESTO(20)
28     COMMON /MUL78/ MOLEFR(6)
29     COMMON /INPUT / FRDEN,FRSIN,DSINZ,FRPU02,FR35,FR40,FR41,DF5,DE1,
30           DCO,DVIDZ,VPLNZ,ATMDS,S,XX,ROUf,ROUC,EXTP,DE,V, S
31           TINLET,DELT,IMAX,TRF+TM,DOB,BK+B,C1+SIGHF,IFLUK, S
32           NLCLAD,ICON,NFLX,KOOL,NEWK,NEWFLX,VOIDZL,NOH, S
33           FRACHE,FRACAR,FRACH,FRACN,FRACKR,FRACKE+HGACEL, S
34           DTEMP,ZCLAD,HG,PEKAVG,MINI,ICDF,ISTOR,ICREP,ISWELL, S
35           +NEXP,MEXP,NHIST, S
36           COMMON /COM M7/ STREST,CFLAG
37           COMMON /MREV1/ MREV1
38           DIMENSION ABCD(7)
39           DATA ABCD / 1HA,1HB,1HC,1HD,1HE,1HF,1HG
40           C CALCULATE GAS PRESX(IPWR)SURE IN THE PIN
41           ABCV=(TT(N))+273.
42           V2=VVOID
43           V1=PI*((RC1+DELRC)**2-(RFS+DELRC)**2)*FL
44           IF(V1,LE,VOLGAP) VL=VOLGAP
45           VOLVOT=VL/ABTGAS+V2/ABTCV
46           PRESX(IPWR)=84.80804*TOTHOL/VOLVOT
47           IF(ISTEP,EG,1) PRESTO(1)=PRESX(IPWR)
48           EMH1(X*MOLEFR(1)*4,0+MOLEFR(2)*39.94+MOLEFR(3)*2.016+MOLEFR(4)*28.0*STP70530
49           12*MOLEFR(5)*83.80+MOLEFR(6)*131.3
50           ELL=VISMIX/PRESTO(1)*STEP70530
51           GIPG2 = 3.468 / 14.22 * ELL
52           C CLAD STRESS PRINT-OUT NO-TAMENI MAIKAI KEISAN-SURU YOONI SYUSEI 8/30 STP70570
53           IN1 = 7
54           IN2 = 30

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* SOURCE STATEMENT (STEP7) *

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45       EC = TERP(TAVGC,AA+4,NN,IN1,IN2,IN3,71)           S
46       CMU = TERP(TAVGC,AA,5,NN,IN1,IN2,IN3,72)           S
47       YDSTR = FYIELD(IYIELD,TAVGC,FNTV(IPWR))           S
48       RC1=DC1/2,                                         S
49       RCO=DCG/2,                                         S
50       RSORMC=(RC0+DELRC0)**2-(RC1+DELRC1)**2           S
51       RSORMPC=(RC0+DELRC0)**2+(RC1+DELRC1)**2           S
52       ALUGC=ALOG((RC0+DELRC0)/(RC1+DELRC1))           S
53       STREST=ALPHAC*EC*(TC1-TC0)/(2.*1./CMU)*ALOGC)*(1.-(2.*((RC0+DELRC0)*STP70680
54           1)*2*/RSORMC*ALUGC))                           S
55       TH=TH-1.98*(ROUf+ROUC)                            S
56       PFACE = 0,                                         S
57       GGL18,ITER) = TR                                  S
58       CFLAG=1H                                           S
59       IF(THR) 1120,1120,1110                           S
60       1110 CONTINUE                                     S
61       IF(MREV1,LT,0) GO TO 1112                         S
62       HGAS = GK/(TH+GIPG2)                            S
63       GO TO 1114                                         S
64       C ..... RESAR-41 GAP CONDUCTANCE                 S
65       1112 CONTINUE                                     S
66       GBTU = GK*57.79,                                 S
67       THFT = TH/2.54/12,                                S
68       HGAS1 = 1500.*GBTU + 4./0.006 + 12.*THFT)        S
69       HGAS2 = GBTU / (THFT/2, + 14.4E-6)                S
70       HGAS = AMAX1(HGAS1,HGAS2)                        S
71       1114 CONTINUE                                     S
72       C ..... HGAS = GK/(CEE*(ROUf+ROUC)+GIPG2)        S
73       HGSLID=0,                                         S
74       CFLAG=1H                                           S
75       GO TO 1180                                         S
76       1120 CONTINUE                                     S
77       TRAABS(THR)                                     S
78       GG(19,ITER) = TR                                S
79       PFACE=(TRFC/(RC1+DELRC)+PRESCN/RSORMC)/(RSORMC/RSORMC+CMU+EC*(1.-STP70950
80       1400./2.E5)                                     S
81       PRMAX=((YDSTR-STREST)*RSORMC+PRESCN)/RSORMC   S
82       IF(PFACE,LT,0.0) PFACE=0.0                      S
83       TFSK = TFS + 273,                                S
84       IF(NCON) 1160,1160,1130                           S
85       1130 CONTINUE                                     S
86       IN1 = 3                                           S
87       IN2 = 30                                         S
88       FK = TERP(TFS,CF,2,NCON,IN1,IN2,IN3,74)           S
89       GO TO 1170                                         S
90       1160 FK=FCOND(FRDEN,TFSK,NCUN)                  S
91       1170 CONTINUE                                     S
92       IN1 = 7                                           S
93       IN2 = 30                                         S
94       CK = TERP(TCI,AA,2,NN,IN1,IN2,IN3,75)           S
95       CKN = 2. * FK + CK / (FK*CK)                   S
96       CFACE=PFACE                                     S
97       CEE=1.980*EXP(-.00125*(PFACE))                 S
98       GG(9,ITER2) = CEE                               S
99       ROUGH=SURF((ROUf**2+ROUC**2)/2.)               S
100      ROUGH=ROUGH                                     S
101      AMEYER = TERP(TCI,AA,7,NN,IN1,IN2,IN3,76)         S

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* SOURCE STATEMENT (STEP7) 3*

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39      IF(CYIELD.GT.0) HMEYER = 2.8*YDSTR          STP71190
100     CZZSWNT(CROGM)                           STP71200
101     AO=140.2*CZ2-.103                         STP71210
102     HSOL=CRM*CPFACE/(AO*CZZ+HMEYER)           STP71220
103     HSOL10=HSOL                                STP71230
104     HGAS=GK/(CEE*(R0UF+R0UC)+G1*G2)           STP71240
105     IF(MREV1.GE.0) GO TO 1180                  STP71250
106     GKBTU=GK * 57.79                            STP71260
107     GPSI=PFACE * 14.22                          STP71270
108     HGAS = 0.6 * PPST + GKBTU/14.4E-6           STP71280
109     C .....                                     STP71290
110     C .....                                     STP71300
111     1180 CONTINUE                               STP71310
112     TFSR=TFS +273.                            STP71320
113     TCISR=TCI+273.                            STP71330
114     AF=NFS+DELR                             STP71340
115     AC=RCI+DELRC                            STP71350
116     HRAD=0.56687E-11/(1./EPSIF+AF/AC*(1./EPSIC-1.))*(TFSR**2+(CISK**2)) STP71360
117     * (TFSR+TCISR)                           STP71370
118     HGC=HSOL10+HGAS+HRAD                      STP71380
119     C .....                                     STP71390
120     1190 CONTINUE                               STP71400
121     C .....                                     STP71410
122     IF(MREV1.GE.0) GO TO 1190                  STP71420
123     HGAS=HGAS/1763.0                          STP71430
124     HGC=HGAS                                  STP71440
125     HSOL10=HRAD=0.0                           STP71450
126     C .....                                     STP71460
127     RETURN                                     STP71470
128     C*****                                         STP71560
129     END                                         STP71570
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* SOURCE STATEMENT *

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1      SUBROUTINE STEP7A                               ST7A0010
C      THIS SUBROUTINE IS CALLED FROM ST3T08          ST7A0020
C
2      REAL MUF,MOL,MOLEFR,MOLEFR                   ST7A0030
3      COMMON /IGRADE/ IGRADE,HOTGP,RINT             ST7A0040
4      COMMON /MREV1/  MREV1                         ST7A0050
5      COMMON /FTNVT/  FNVT(20),TNVT(20)            ST7A0060
6      COMMON /YIELD/  YIELD                         ST7A0070
7      COMMON /PWRAY/  PAVRG,FUELLE,FL,POWER(21),AI(21),NPW,PTOT,LPMAX,   ST7A0080
8      COMMON /DATA 4/  PI,CCPN3,SECDAY,MVGAD,RR,CONEN   ST7A0090
9      COMMON /DATA 5/  SDOT,SDOTT,EF,MUF,EPSEN,EPSC    ST7A0100
10     COMMON /COM 0/  TITLE(20),AA(7,30),BB(6,51),CF(3,30),KV(2,20)  ST7A0110
11     COMMON /COM 1/  TTS(51),TSR(51),WIN(51),W(51),CLCRP(2,20)  ST7A0120
12     COMMON /COM 02/ IPOW,ISTEP,ITER,KOUNT           ST7A0130
13     COMMON /COM 03/ TOP,DELRC,DELRC,TCOOL,STP       ST7A0140
14     COMMON /COM 04/ BURNUP,TDAY,TWCID,TUTLDY,TOTBUR  ST7A0150
15     COMMON /COM 08/ II,JCASE,TCODE,XMOTOT           ST7A0160
16     COMMON /COM 13/ RFS,FNPOW,RHSINZ,RVOTD2         ST7A0170
17     COMMON /COM 14/ KCON                           ST7A0180
18     COMMON /COM 21/ NNN,NNN,NF                      ST7A0190
19     COMMON /COM 35/ TB1,TB2,TC1,TC2,TFS,TH,THR      ST7A0200
20     COMMON /COM 56/ VOLGP,VOLGAP                  ST7A0210
21     COMMON /COM 57/ VRUF,ALPHAC,PRESCH            ST7A0220
22     COMMON /COM 67/ PFACE,VOLGVT,HSOLID,HGAS,HRAD,GIPG2,PHE5X(20)  ST7A0230
23     COMMON /COM 8G/ GG(20,100)                     ST7A0240
24     COMMON /COM 90/ VOLGAS,WHMG               ST7A0250
25     COMMON /COM1357/ RCI,RCI                   ST7A0260
26     COMMON /COM357/ TAVGC                      ST7A0270
27     COMMON /COM678/ TOTMOL,ABTGAS,VISMIX,GR,GASKUN  ST7A0280
28     COMMON /HOL579/ PRESTO(20)                 ST7A0290
29     COMMON /HOL678/ MOLEFR(6)                  ST7A0300
30     COMMON /INPUT/ FRDEN,FRSIN,DSINZ,FRPU02,FR35,FF40,FR41,DFS,DC1,   ST7A0310
1      DCO,DV1,DZ,VLENZ,ATMOS$+XX,ROUFC,RCUC,EXTP,DE,V,  ST7A0320
2      TINLET,CELT,TMAX,TER,TM,DB0,BK,FBC,SIGHF,IFLUX,  ST7A0330
3      NCLAD,NCON,NFLX,KCOL,NEWK,NEWCL,NEWFLX,VOLDL,NOH  ST7A0340
4      FRACHE,FRACAH,FRACH,FRACN,FRACKR,FRACNE,FGACEL,  ST7A0350
5      DTEMP,ZCLAD,HG,PEKAVG,MINI,ICDF,ISTOR,ICREP,ISELL  ST7A0360
6      INEXP,MEXP,NHIST                           ST7A0370
31     COMMON /COM M7/ STRETH,CFLAG                ST7A0380
32     COMMON /CUSAT7A/ RESGAP,PCONT              ST7A0390
33     COMMON /RELUI1/ RGAPC(20),NFS0(20),DELEXP(20)  ST7A0400
34     DIMENSION ABCD(7)                         ST7A0410
35     DATA ABCD / 1MA,1MB,1MC,1HD,1ME,1MF,1HG /  ST7A0420
36     C
37     C CALCULATE GAS PRESA(IPOW, ) PRESSURE IN THE PIN  ST7A0430
38     C
39     IF(ITER,EW,1,AND,(GRADE,NE,5)                ST7A0440
40     1      VOLGAP=(RFS+DELRC+RESGAP/2)*RESGAP*PI*2.*FL  ST7A0450
41     ABTCV=(TTS(1))+273.                         ST7A0460
42     V2=VVOID                         ST7A0470
43     V1=PI*(RCI+DELRC)**2-(RFS+DELRC)**2*FL        ST7A0480
44     IF(ITER,EW,1,AND,(GRADE,NE,5)                ST7A0490
45     1      VOLGAP=(RFS+DELRC+RESGAP/2)*RESGAP*PI*2.*FL  ST7A0500
46     ABTCV=(TTS(1))+273.                         ST7A0510
47     V2=VVOID                         ST7A0520
48     V1=PI*(RCI+DELRC)**2-(RFS+DELRC)**2*FL        ST7A0530
49     IF(ITER,EW,1,AND,(GRADE,NE,5)                ST7A0540
50     1      VOLGAP=(RFS+DELRC+RESGAP/2)*RESGAP*PI*2.*FL  ST7A0550
51     IF(ITER,EW,1,AND,(GRADE,EW,5)                ST7A0560
52     1      VOLGAP=(RFS+DELRC+HOTGP/2). *HOTGP*PI*2.*FL  ST7A0570
53     VOLGVT=V1/ABTGAS+V2/ABTCV                  ST7A0580
54     VOLGAP=V1=VOLGAP                         ST7A0590
55     VOLGVT=V1/ABTGAS+V2/ABTCV                  ST7A0590

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* SOURCE STATEMENT (STEP7A) *

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44     PRES((IPOW)=84,80604*TOTMOL/VOLGVT          ST7A0600
45     IF(ISTEP,EO,1) PRESTO(1)=PRESA(IPOW)          ST7A0610
46     EMMIX=MOLEFR(1)+0*MOLEFR(2)*39.94+MOLEFR(3)*2.016+MOLEFR(4)*28.05    ST7A0620
47     12*MOLEFR(5)*93.80*MOLEFR(6)*131.3          ST7A0630
48     ELL=VISMIX/PRESTO(1)STEP+SQRT(ABTGAS/EMMIX)  ST7A0640
49     GIPG2 = 5.445 / 14.22 * ELL                  ST7A0650
50     C
51     IN1 = 1                                     ST7A0660
52     IN2 = 30                                    ST7A0670
53     EC = TERP(TAVGC,AA,4,NN,IN1,IN2,IN3,71)      ST7A0680
54     CMU = TERP(TAVGC,AA,5,NN,IN1,IN2,IN3,72)      ST7A0690
55     YDSTR = FYIELD(1)YIELD,TAVGC,FNVT(IPOW)      ST7A0700
56     RCI=UCI/2.                                  ST7A0710
57     RCJ=DCI/2.                                  ST7A0720
58     RSURPC=(RCJ+DELRC)*(RCI+DELRC)**2            ST7A0730
59     RSURPC=(RCJ+DELRC)*(RCI+DELRC)**2            ST7A0740
60     ALOC=ALOG(RCJ+DELRC)/(RCI+DELRC)            ST7A0750
61     ALOC=ALOG(RCJ+DELRC)/(RCI+DELRC)            ST7A0760
62     STB5=STALPHAC+C((CI-TCO)/(2.*(1.-CMU)*ALOC)*(1.-(2.*(RCJ+DELRC)*ST7A0770
63     1)**2/RSURMC*ALOC))                         ST7A0780
64     C
65     CONTACT PRESSURE CALCULATION                 PFACE(KG/CM2)  ST7A0790
66     C
67     TH = RINT                                     ST7A0800
68     PFACE=(TH*EC/(RCI+DELRC)+PRESCH)/RSURPC/RSURMC+CMU+EC*(1.-ST7A0810
69     1NUF/EP)                                     ST7A0820
70     PFACE=(TH*EC/(RCI+DELRC)+PRESCH)/RSURPC/RSURMC+CMU+EC*(1.-ST7A0830
71     1NUF/EP)                                     ST7A0840
72     GG(16,ITER) = PFACE                         ST7A0850
73     IF(IGRADE,EO,1) GO TO 1120                  ST7A0860
74     PFACE = PCONT                                ST7A0870
75     C
76     1120  CONTINUE                                ST7A0880
77     PRMAX=((YDSTR-STRESS)*RSURMC+PRESCH)/RSURPC  ST7A0890
78     IF(PFACE,GT,PRMAX) PFACE=PRMAX              ST7A0900
79     IF(PFACE,LT,0.0) PFACE=0.0                  ST7A0910
80     TFS = TFS + 273.                            ST7A0920
81     IF(NCON) 1160,1160+1130                      ST7A0930
82     1130  CONTINUE                                ST7A0940
83     IN1 = 3                                     ST7A0950
84     IN2 = 30                                    ST7A0960
85     FK = TERP(TFS,CF,2,NCON,IN1,IN2,IN3,74)      ST7A0970
86     GO TO 1170                                ST7A0980
87     1160  FK=COND(FRDEN,1FSK,KCON)             ST7A0990
88     1170  CONTINUE                                ST7A1000
89     IN1 = 7                                     ST7A1010
90     IN2 = 30                                    ST7A1020
91     CK = TERP(TCI,AA,2,NN,IN1,IN2,IN3,75)      ST7A1030
92     CKM = 2. * FK * CK / ( FK+CK )             ST7A1040
93     C
94     HOT GAP CORRECTION FACTOR (CEE) CALCULATION  ST7A1050
95     CEE = EXP(-.00125*PFACE)                  ST7A1060
96     C
97     HSOLID CALCULATION                         HSOLID(W/CM2,0EG-C)  ST7A1070
98     C
99     ROUGH=SQRT((ROUF**2+ROUC**2)/2.)           ST7A1080
100    CROUGH=ROUGH                                ST7A1090
101    HMEYER = TERP(TCI,AA,7,NN,IN1,IN2,IN3,76)    ST7A1100
102    IF(YIELD,GT,0) HMEYER = 2.8*YDSTR            ST7A1110
103    CZZ=SQRT(CROUGH)                          ST7A1120
104    AO=140.2*CZZ,103                           ST7A1130
105    HSOLID = CKM * PFACE/(AO*CZZ*HMEYER)        ST7A1140
106

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* SOURCE STATEMENT (STEP/A) 24

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C      HOT GAP CALCULATION          HOTGAP(CM)           ST7A1190
C      IF(IGRADE<=15) HOTGP = CEE*KESGAP    ST7A1200
90     TH = HOTGP                 ST7A1210
91     HOTGAP = HOTGP + GAPG2        ST7A1220
92     VOLGAP=(VHS+DELH+HOTGP)/2.0 * HOTGP + P1 * 2.0 * FL   ST7A1230
93     VOLSP=VOLGAP + VVJTD        ST7A1240
94

C      HGAS CALCULATION          HGAS(CM/CM2/DEG-C)    ST7A1250
C      HGAS = BK/HOTGAP          ST7A1260
95     118U CONTINUE              ST7A1270
96     CFAG = ABCD(IGRADE)       ST7A1280
C      HRAD CALCULATION          HRAD(CM/CM2/DEG-C)    ST7A1290
C      TCISK=TCI+273.            ST7A1300
97     AF=RF5*DELR              ST7A1310
100    AC=RCI*DELC              ST7A1320
101    HRAD=(C156RH7E-11/(1./RFSTF+AF/AC*(1./EPSC-1.0)*(TFSK**2*TCISK**2))ST7A1330
*          *(TFSK+TCISK)          ST7A1340
102    HC=HSOL10+HGAS+HRAD      ST7A1350
103    GG(1,ITER) = ITER         ST7A1360
104    GG(2,ITER) = IT(4)        ST7A1370
105    GG(3,ITER) = HG           ST7A1380
106    GG(4,ITER) = HGC          ST7A1390
107    GG(5,ITER) = HSOL10      ST7A1400
108    GG(6,ITER) = HGAS          ST7A1410
109    GG(7,ITER) = HRAD          ST7A1420
110    GG(8,ITER) = CEF          ST7A1430
111    GG(17,ITER) = PFACE       ST7A1440
112    GG(18,ITER) = RINT          ST7A1450
C      ----- TH IS HOT GAP AT THIS STEP , CALCULATE COLD GAP RGAPC(IPW)ST7A1460
C      COLD GAP DEFINE AT ROOM TEMPERATURE (25. DEG C)          ST7A1470
C      XDELR = 0.0          ST7A1480
113    DO 10 I=1,N          ST7A1490
114    T1= BB(3,I)          ST7A1500
115    T2 = BB(3,I+1)        ST7A1510
116    T3 = (T1+T2)/2.        ST7A1520
117    ALP = FALPHA(T3,NEAP)  ST7A1530
118    RINGR = BB(4,I) - BB(4,I+1)  ST7A1540
119    DELRIN = RINGR*ALP*(25.-T3)  ST7A1550
120    XDELR = XDELR + DELRIN  ST7A1560
121
122    10 CONTINUE          ST7A1570
123    DELEXP(IPW) = XDELR      ST7A1580
124    RGAPC(IPW) = TH-XDELR    ST7A1590
125    RFSD(IPW) = (RF5*DELR) + XDELR  ST7A1600
126    RETURN                ST7A1610
127
*****END*****ST7A1700
128

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* SOURCE STATEMENT *

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1      SUBROUTINE STEPS
2      C THIS SUBROUTINE IS CALLED FROM ST3TOB
3      C
4      REAL *MUF,MOL,MOLEFR,MOLEFR
5      COMMON /MREVI / MREVI
6      COMMON /POWRAY/ PAVRS,FUELLE,FL,POWEK(21),AI(21),NPOW,PTOT,LPMAX,
7      PKPDRW,IPEEK,DELPH,PNAX
8      COMMON /BRNGAS/ AKN(20),AKE(20),PHI(20),ENKE(20),ENKR(20)
9      COMMON /BURN / BURN(20),BULD(20)
10     COMMON /DATA 4/ PI,CCFN(3),SECDAY,AVOGAD,RR,CONER
11     COMMON /COM 0/ TITLE(20),AC(7, 30),BB(6, 51),CF(3, 30),RV(2, 20)
12     COMMON /COM 1/ TTL(51),TSR(51),INC(51),S(51),TS(51),CLCR(2,20)
13     COMMON /COM 02/ Ipow,ISTEP,ITER,KOUNT
14     COMMON /COM 03/ TCI,DELRG,DELRG,DELRG,TCOL,STP
15     COMMON /COM 05/ BURNUP,TDAYS,VVOID,TOTLDY,TOTBUR
16     COMMON /COM 06/ 111JCASE+COOLF,IMOTOT
17     COMMON /COM 13/ RFS,IFNPOW,RSTINZ,VVOIDZ
18     COMMON /COM 21/ RHOIRHOS,FRUU,FRPUU
19     COMMON /COM 21/ NUNNNNNN,NF
20     COMMON /COM 35/ TB1,TB0,TCC,TC1,TC0,TFS,TH,THH
21     COMMON /COM 38/ DUVRAB,QOVRAC,QOVRAS,HF
22     COMMON /COM 48 / HGA(20),RGAPX(20),TCLINE(20)
23     COMMON /COM 128/ IOT1,IIPHOF
24     COMMON /COM 43P/ DC(20,51),IPROF
25     COMMON /COM78 / PFACE,VOLVLT,HSOLN,HGAS,FRAD,G1P62,PRESX(20)
26     COMMON /COM48 / DSIN,RSINT,TSIN,TSINC,VVOID,VVOIDC,T
27     COMMON /COM678 / DELRP,DELRP,DELRP,DELRP,TAVGF,VAVGT
28     COMMON /COM678 / TOTMOL,ABTGAS,VISMI,GR,GASKN
29     COMMON /COM678 / MOLEFR(6)
30     COMMON /COM 838 / VOLTX(20)
31     COMMON /COM 88 / NOCONV,HGND,HGCND,ISTPNO,IPONO,NPONO
32     COMMON /COM 8M / IS10P,JCASE
33     COMMON /H12UE/ K1,K2,K3,K4,K5,K6
34     COMMON /INPUT / FROEV,FRSTN,DSINZ,FRPDU02,FR35,FR40,FR41,DFS,DCI,
35     DCO,VVOIDZ,VPLENZ,ATMOS,SAXX,ROUF,ROUC,EXTP,DE,V,
36     TINLET,DELT,THAX,TR,TH,DEO,BK,BCK,SGHF,IFLUX,
37     NCLAD,ICON,INFLX,KUDL,NEWL,NEWL,NEWFLX,VVOIDZL,NCH+STP80380
38     FRACHE,FRACR,FRACH,FRACN,FRACKR,FRACX,HGACEL,
39     DTEMP,2CLAD,HG,PEKAVG,MIN1,ICDF,ISTOR,ICREP,ISWEIL,STP80400
40     ,NEXP,NEXP,NHIST
41     COMMON /PRIN02/ CP1(20),CP2(20),ST1(20),ST2(20),
42     ST3(20),ST4(20),ST5(20),ST6(20)
43     COMMON /RESTRUS/ ISINT,VVOIDX,VVOIDC,VLENGT
44     COMMON /DIMEN1/ DVVIDX(20),DVVIDC(20),DFSX(20),DCIX(20),DCDX(20),
45     VVVIDX(20),VVVIDC(20),TSINX(20),RSINX(20)
46     ZLENGT(5+20),VUDL(20)
47     DATA CP1,CP2,ST1+ST2+ST3,ST4+ST5+ST6 / 160*0.0 /
48     DATA TSINC/0.0/
49
50     IF (MREVI.EQ.0,AND,THR,ST,0,0) PFACE=0.
51     VOLTX(IPON)=VOLVLT
52     HGAS(IPON)=HG
53     TCLINE(IPON)=TT(N)
54     RGAPX(IPON)=TH
55     -----
56     CALL STORE(VAVGT,TSR,TFS,TT,N,PI,DFS,RHO,
57     1,CHNUM,CPMIN,CPMAX,STORE,STOR,STORB,STOREB,STOREC,CPNUMF)
58

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* SOURCE STATEMENT (STEP8) */

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59     C
60     CP1(IPON) = CPNOM
61     CP2(IPON) = CPNOMF
62     ST1(IPON) = STOR
63     ST2(IPON) = STURR
64     ST3(IPON) = STORE
65     ST4(IPON) = STOREB
66     ST5(IPON) = STOREC
67     ST6(IPON) = STOREF
68
69     IF (ISTEP.LT.1,STOP,OR,IPROF.LE.0) GO TO 20000
70     IP=OF=0
71     HGDM=1G*1763.
72     ****CALL PROF, GAPRO ****
73     CALL PROF(TM,TC1,TC0,TCOL,TH,HGDM,JCASE,IPON,NPOW,MIN1,ISTEP,
74     *          LPHAX)
75     ****
76     20000 CONTINUE
77     IF (NOCONV.EQ.1) CALL GAPRO(JCASE,JCASE)
78     IF (NOCONV,EQ.1) WRITE(5,1680) HGND,HGCND,ISTPNO,(PJNUO,NPONO
79     NOCONV = 0
80
81     RSIN=0.
82     TSINC=0.0
83     RVOID=DARVOID
84     VTC=0.0
85
86     IF (T.LE..001,OR,FRDEN,EQ.FRSIN) GO TO 1350
87     IF (FRDEN.GE.,FRSIN) FRSIN=FRDEN
88     ****
89     RETEN=.00001567*ALOG10(24.*TOTLDY) + .000480
90     TSINC=1./RETEN-273.
91     TSIN=1.8*TSINC+32.
92     TSIN = TSINC
93     1340 CONTINUE
94     IN1 = 6
95     IN2 = 51
96     RSIN = TEHP(TSIN+BB+2*H,IN1,IN2,IN3+82)
97     IF (RSIN,LE.RSIN2) RSIN = RSINZ
98     DSIN=2.*RSIN
99     ****
100    FACT = 0.0
101    IF (FRSIN,LE.0,0) GO TO 5
102    FACT = (FRSIN-FRDEN) / FRGIN
103    5 CONTINUE
104    SQRV = VVOIDZ**2 + FACT*(RSIN**2 - RSINZ**2)
105    RVCID = SQRT(SQRV)
106    ****
107    IF (VVOID,LE,VVOIDZ) RVOID = VVOIDZ
108    DVVIDZ=2.*VVOID
109    ELTC=FL-VVOIDZ/FNPOW
110    VTC=PI*ELTC*VVOIDZ**2
111    VVOID=(PI*FL*RVOID**2-VTC)
112    1350 CONTINUE
113    **** MODIFY HOT DIMENSION TO COLD STATE(VOID AND RESTRUCTURE RADIUS)
114    ****
115    TTT = TT(N)
116    ALP=ALPHA(TTT+NEXP)
117    C. ISINT IS ALWAYS SETTED TO 0 AT EACH AXIAL SECTION LOOP IN SUB. ST3TO8STP81180

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* SOURCE STATEMENT (STEP#) 2*

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C      AND SET TO 1 IN SUB, STEP4 IF RESTRUCTURING OCCURED      STP81190
88     IF (ISINT,LE,0) ALP=0.0                                STP81200
89     IF (KVOID,LE,2) ALP = 0.0                                STP81210
90     RVOIDX=RVOID/(1.+ALP*(TTT+25.))                      STP81220
91     VVOIDC=(PI*FL*RVOIDX**2-VTC)                          STP81230
92     IF (VVOIDC,LE,0.0) VVOIDC=0.0                          STP81240
C      C..... WE ASSUMED THE CENTRAL VOID ALWAYS FORMED UNIFORM DIAMETER FROM      STP81250
C      BOTTOM TO TOP                                         STP81260
C
93     IF (RVOIDX,LE,1.E-10) GO TO 10                         STP81270
94     VLENGT=VVCDC/(PI*RVOIDX**2)                          STP81280
95     GO TO 20                                              STP81290
96     10 CONTINUE                                           STP81300
97     VLENGT=0.0                                         STP81310
98     20 CONTINUE                                           STP81320
C      WHERE RVOIDX IS THE RADIUS OF CENTRAL VOID AT ROOM TEMPERATURE      STP81330
C      VVOIDC IS THE VOLUME OF CENTRAL VOID AT ROOM TEMPERATURE      STP81340
C      VLENGT IS THE LENGTH OF CENTRAL VOID EQUAL TO 1-SECTION      STP81350
C      LENGTH (=FL)                                         STP81360
C
99     RETURN                                              STP81370
C      * 1   * 2   * 3   * 4   * 5   * 6   * 7      STP81380
100    1680 FORMAT(//, 2X, 'NON-CONVERGENCE IN HGC -- HG =', F9.6, ', HGC =', STP81390
      *F9.6, 2X, 'STEP #', I2, ', IPW =', I2, ', OF ', I2, ')      STP81400
101    1770 FORMAT(1H ,24X,'RADIUS',10X,'TEMPERATURE',15X,'RADIUS',12X,'TEMPERSTP81450
      14TURE',10X,'PERCENT OF',/,(24X,'(INCHES)',11X,'(DEG F)',18X,'(CM)',STP81460
      212X,'(DEG C)',12X,'FUEL RADIUS',/,(24X,F6.4,9X,F10.0,17X,F6.4,15X,STP81470
      3 F7.0,10X,F10.2))                                         STP81480
*****                                                       STP81490
102    END                                                 STP81500

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* SOURCE STATEMENT *

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1      SUBROUTINE ST3T06(KS)                               ST380010
2      C
3      C THIS SUBROUTINE IS CALLED FROM MAIN               ST380020
4      C
5      REAL MUF,MOL,MGLEFR,MGLFR                         ST380030
6      COMMON /ANKRAXE/ ANKR,ANXE                         ST380040
7      COMMON /MEMO1/ MEMO1(20,5),HATA(20)                ST380050
8      COMMON /MCN/ MCN(1)                                ST380060
9      COMMON /MAIMOLY/ TAVGX,VOLTYS                      ST380070
10     COMMON /POWRAY/ PAVRG,FUELL,FL,POWER(21),A1(21),NPWR,PTOT,LPMAX,   ST380080
11     1          PKPOWR,IPKAW,DELP,PMAX                     ST380100
12     COMMON /BRNGAS/ AKR(20),AXE(20),PHI(20),ENKE(20),ENKR(20)    ST380120
13     COMMON /BRNRAY/ VOLCC,AZL,AZV,A92,A102             ST380130
14     COMMON /DATA/ PI,CCPIN3,SECDAY,AVGADIRR,CONEN        ST380140
15     COMMON /CUM/ 0/ TITLE(7,30),BB(6,51),CF(3,30)+RV(2,20)  ST380150
16     COMMON /CUM/ 0/ IPOW,ISTEP,ITER,AKUNT              ST380160
17     COMMON /CUM/ 0/ RSINP,QUS,QUU,STOT                 ST380170
18     COMMON /CUM/ 0/ RFS1,FNPW,RHSIN,RVOIDZ             ST380180
19     COMMON /CUM/ 1/ RHO,RHGS,FRUL,FRPUPI              ST380190
20     COMMON /CUM/ 2/ RHO,RHGS,FRUL,FRPUPI              ST380200
21     COMMON /CUM/ 3/ NINNNNNNNN                         ST380210
22     COMMON /CUM/ 4/ USINRSIN,T SIN,T SINC,UVOID,UVOLD,UVOLDU,T  ST380220
23     COMMON /CUM/ 5/ NOCONV,HGNO,HGCNO,ISPNNO,IPONNO,NPWNNO  ST380230
24     COMMON /CUM/ 6/ GG(20,10)                           ST380240
25     COMMON /CUM/ 7/ BM/(STOP,ICASE)                   ST380250
26     COMMON /CUM/ 8/ VOLGAS,W,HGC                         ST380260
27     COMMON /CML838/ VOLTX(20)                          ST380270
28     COMMON /CML938/ TBAR(20)                          ST380280
29     COMMON /INPUT/ FREDEN,FRSIN,DSINZ,FRPLU2,FR35,FR40,FR41,DFS,DCI,   ST380290
30     DCU,DVIDZ,VPLENZ,ATMG5,S,AX,ROU,C,EXP,D,E,V  ST380300
31     1          TINLET+DELTA,TMAX1,FR1,TD60,BK,HBC,SIGHF,IFLUX,  ST380310
32     2          KCLAD,NCON,NFLX,KCOL,NEWK,NEWFLX,VOIDZL,NOD,  ST380320
33     3          FRACHE,FHACAR,FHACH,FRACN,FRACAE,HGACEL,  ST380330
34     4          DTEMPVZ,CLAD,HG,PLKAVG,MINI,ICDF,ISTOP,ICREP,ISWELL  ST380340
35     5          INEXF,EXP,LNMH,IST  ST380350
36     6          COMMON /CUM/ 9/ TH,TBC,TCC,TCI,TCU,TES,TH,THR  ST380360
37     COMMON /CUM/ 10/ QDVRAB,WDVRAC,WDVRASHF            ST380370
38     COMMON /CUM/ 11/ STRECI,CFLAG                         ST380380
39     COMMON /CUM/ 12/ DELRC,DELRCDE,DELRR,DELRRV,TSHOU  ST380390
40     COMMON /CUM/ 13/ K1700,R1200,I1350                  ST380400
41     COMMON /CUM/ 14/ PFACE,VOLGVT,HSCLID,HGAS,HRAD,G1PG2,PRESX(20)  ST380410
42     COMMON /CUM/ 15/ RCI,RCO                            ST380420
43     COMMON /CUM/ 16/ SELRN,DELHP,SHLRCL,DELRT,TAVGF,VAVGT  ST380430
44     COMMON /CUM/ 17/ TOTMOL,ABTGAS,VISMIX,GR,GASKON  ST380440
45     COMMON /PHIN01/ TCOLT(20),HFILM(20),TCOK(20),TCICA(20),  ST380450
46     *          GCG(20),GCT(20),TJUMP(20),URTF(20),URSF(20),  ST380460
47     *          DRF(20),DRKC(20),DRPL(20),DRPLD(20),TFSCA(20),  ST380470
48     *          DHCC(20),RH1(20),BR2(20),BR3(20),BH4(20),  ST380480
49     *          RATE(20),RATC(20),CPRES(20),CSTRES(20),GASC(20),  ST380490
50     *          GASC8(20),ITERZ(20)  ST380500
51     COMMON /PHIN02/ DRDF(20),DRRF(20),FCONT(20),TOISH(20)  ST380510
52     COMMON /PRESTRU/ ISINT,VVOIDDX,VVOIDC,VLENGT           ST380520
53     COMMON /DIMEN1/ DV01DX(20),DV01DH(20),FWSX(20),DC1X(20),DC0X(20),  ST380530
54     1          VVOIDX(20),VVOIDH(20),ISINX(20),HSINX(20)  ST380540
55     2          ,VLENGT(5,20),VCDL(20)  ST380550

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* SOURCE STATEMENT (ST3T05) *

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47     COMMON /ELONG/ PLENIG(5)                           ST380600
48     COMMON /COLVER/ NOCONC                          ST380610
49     COMMON /MREV1/ MREV1                           ST380620
50     COMMON /NEVGAS/ MGAS                           ST380630
51     COMMON /SISDEN/ DLFDL,DENS1                  ST380640
52     COMMON /DIMEN2/ DENSFL(5,20)                  ST380650
53     ****
54     DIMENSION PREHG(20),HGAC(20)                  ST380660
55     DATA PREHG / 20*0.5678 /                      ST380670
56     ****
57     GO TO 1111,2222                                KS
58     1111 CONTINUE
59     DO 444 I=1,20
60     DO 443 J=1,5
61     443 MEM1(I,J)=0
62     444 HATA(I)=4H
63     RETURN
64
65     2222 CONTINUE
66     TAVGX*U,
67     VOLTXS*U,
68     DO 1370 IPOW=1,NPWR
69
70     C
71     C CALCULATE THE POWER, TCOOL, THE NEW NUMBER OF XE AND KR
72     C ATOMS IN EACH SEGMENT.
73
74     DV01DZ=VVOIDX(IPOW)
75     DFS=DC1X(IPOW)
76     DCI=DC1A(IPOW)
77     DCO=DC0A(IPOW)
78     VV01DZ=VV01DX(IPOW)
79     RV01DZ=DV01DZ/2.
80     RFS=DFS/2.
81     RCI=DC1/2.
82     RCO=DC0/2.
83     ISINT=0
84     RSINZ=RSINX(IPOW)
85     P=(POWER(IPOW)+PGEW(IPOW+1))*0.5
86     TCOOL=TINLET+DTEMP*A1(IPOW)
87     TCOOLF=TCOOL*1.8+32
88     IF(RSINZ.GT.0.) GO TO 500
89     WGT=RHO*(RFS**2-RV01DZ**2)*PI
90     WGT=0.
91     GO TO 510
92     500 WGT=RHO*(HFS**2-RSINZ**2)*PI
93     WGT=WHS*(RSINZ**2-RV01DZ**2)*PI
94     510 WGT=0.
95     RSIN=RSINZ
96     DSIN=DSINZ
97     RVCID=RV01DZ
98     DV01D=VV01DZ
99     VV01D=VV01DZ
100    STOT=P
101    C
102    C GRAM IS IN *CM2/GRAM OF FUEL
103    GGRAM=STOT/WGTCM
104    GGRAM=GGRAM*RHO
105    GWS=GGRAM*RHO
106    C
107    INITIALIZE
108    NOCONV=0

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* SOURCE STATEMENT (ST3T06) *

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92      ITEM = ITEE = 0                               ST381190
93      DELR = DELRC = DELRC0 = DELTA0 = DELHGU = 0.0   ST381200
94      HGACEL = 0.8                                ST381210
95      IF(ISTEP.EQ.1) HGACEL=0.6                   ST381220
96      IF(ISTEP.EQ.2) HGACEL=0.5                   ST381230
97      IF(ISTEP.EQ.3) HGACEL=0.4                   ST381240
98      IF(ISTEP.EQ.4) HGACEL=0.3                   ST381250
99      IF(ISTEP.EQ.5) HGACEL=0.2                   ST381260
100     IF(ISTEP.LE.3) GO TO 518                  ST381270
101     IF(MEMO1(IPOW,ISTEP-1).LT. 8) GO TO 518    ST381280
102     HGACEL = HGAC1(IPOW)                      ST381290
103     ITEE = MEMO1(IPOW,ISTEP-1)                 ST381300
104     518  CONTINUE                                ST381310
105     IUSC = 0                                    ST381320
106     HGOLD = 0.5678                            ST381330
107     OLDDOL = HGCOLD = 0.5678                  ST381340
108     HG1+HG2=HGCI*HGCO=0.5678                  ST381350
109     HGMAX = 10E+3                             ST381360
110     HGMIN = 0.0                                ST381370
C-----
111     IF(ISTEP.LE.2) GO TO 550                  ST381380
112     HG = PREHG(IPOW)                         ST381390
113     550  CONTINUE                                ST381400
114     CCCCCC  HG = INITIAL HG IS INPUTTED AT SUB. STEP1  ST381420
115     C GAP CONDUCTANCE ITERATION LOOP          ST381430
116     520  CONTINUE                                ST381440
117     ITEM=ITEM+1                                ST381450
118     ITEE = ITEE + 1                            ST381460
C
C     STEP3 COOLANT-CLADDING HEAT TRANSFER, HEAT FLUX, CLADDING TEMP.  ST381470
C     STEP4 FUEL TEMPERATURE DISTRIBUTION, RESTRUCTURING TEMPERATURE  ST381480
C     STEPS THERMAL EXPANSION, SWELLING, HOT GAP                      ST381490
C     MULMOL(2) FISSION GAS RELEASE RATE                           ST381500
C     STEP6 THERMAL CONDUCTIVITY OF GAS MIXTURE                  ST381510
C     STEP7 GAP CONDUCTANCE                                ST381520
C
C
117     CALL STEP3                                ST381530
118     CALL STEP4                                ST381540
119     IF(MREV1.LE.0)                            ST381550
120     IF(MREV1.EQ.1)                            ST381560
121     CALL MOLMOL(3)                          ST381570
122     CALL STEP5                                ST381580
123     IF(MREV1.LE.0)                            ST381590
124     IF(MREV1.EQ.1)                            ST381600
125     BEGIN CONVERGENCE OF HG NODS.             ST381610
C
126     10  DELTA=HG+HG                               ST381620
127     DELHG=HG+HGOLD                            ST381630
128     HGOLD=HG                                ST381640
129     IF(ABS(DELTA/HG).LT.0.01.AND.ITEM.GT.1) NONCON = 0  ST381650
130     IF(ABS(DELTA/HG).LT.0.01.AND.ITEM.GT.1) GO TO 1230  ST381660
131     FAC1 = FAC2 = 1.0                         ST381670
132     IF(ISTEP.EQ.1.AND.ITEM.GT.1) GO TO 1230    ST381680
133     IF(ISTEP.EQ.2.AND.ITEM.GT.5) GO TO 1230    ST381690
134     IF(ISTEP.EQ.3.AND.ITEM.GT.10) GO TO 1230   ST381700
135     IF(ITEM.GT.45) GO TO 1220                ST381710
136     IF(ITEE.LE.3) GO TO 1200                ST381720
137     IF(.NOT.(DEL2*DELL.GT.0.AND.DEL1*DELTA.LT.,0)) GO TO 1192  ST381730
138     IF(ABS(HG-HG1)/(DELTA).LT.0.001) GO TO 1192  ST381740
139     HGACEL = HGACEL * 0.5                    ST381750
140     HG = (HG+HG1) / 2.0                     ST381760
141     GO TO 520                                ST381770
142     11.2  CONTINUE                                ST381780
143     IF(DELTA*DELTA0.LT.,0.AND.ABS(DELHG/DELHG0).GT.0.8) FAC1=0.8  ST381790
144     IF(DELTA*DELTA0.GT.,0.AND.ABS((HGCOLD-HG)/HG).LT.0.003) FAC1=1.25  ST381800
145     HGACEL = HGACEL * FAC1                  ST381810
146     IF(HGACEL.GT.0.5) HGACEL=0.6            ST381820
147     IF(ITEE.LE. 10.AND. HGACEL.LT.0.1 ) HGACEL=0.1  ST381830
148     IF(ITEE.LE. 15.AND. ITEE.GT. 10.AND. HGACEL.LT.0.07 ) HGACEL=0.07  ST381840
149     IF(ITEE.LE. 20.AND. ITEE.GT. 15.AND. HGACEL.LT.0.05 ) HGACEL=0.05  ST381850
150     IF(ITEE.LE. 25.AND. ITEE.GT. 20.AND. HGACEL.LT.0.04 ) HGACEL=0.04  ST381860
151     IF(ITEE.LE. 30.AND. ITEE.GT. 25.AND. HGACEL.LT.0.03 ) HGACEL=0.03  ST381870
152     IF(ITEE.LE. 35.AND. ITEE.GT. 30.AND. HGACEL.LT.0.02 ) HGACEL=0.02  ST381880
153     IF(ITEE.LE. 40.AND. ITEE.GT. 35.AND. HGACEL.LT.0.01 ) HGACEL=0.01  ST381890
154     IF(HGACEL.LT.0.015) HGACEL=0.015           ST381900
155     IF(DELTA*DELTA0.LT.0.AND.ABS((OLDDOL-HG)/HG).LT.0.012) FAC2=.5  ST381910
156     HGACEL = HGACEL * FAC2                  ST381920
157     1200  CONTINUE                                ST381930
158     HG2 = HG1                                ST381940
159     HG = HG                                ST381950
160     HGHG+HGACEL*DELTA                      ST381960
161     IF((HG-HG).LT.-.567.AND.ITEE.LE.5) HGACEL=0.5  ST381970
162     1210  CONTINUE                                ST381980
163     DELTA0=DELTA                            ST381990
164     DELHG=DELHG                            ST382000
165     OLDDOL = HGCOLD                          ST382010
166     HGCOLD = HGC                            ST382020
167     DEL2=DELL                                ST382030
168     OLDDOL=HG2*HGCI                          ST382040
169     DELTA0=DEL1*DELTA                        ST382050
170     HGCOLD=HGCI*HGC                          ST382060
171     GG(8,ITER) = HGACEL                      ST382070
172     GO TO 520                                ST382080
173     20  HG2 = HG                                ST382090
174     DELTA2 = HGC - HG                        ST382100
175     IF(DELTA2.LT.0.0.AND.HG.LT.HGMAX) HGMAX = HG  ST382110
176     IF(DELTA2.GT.0.0.AND.HG.GT.HGMIN) HGMIN = HG  ST382120
177     IF(HGMAX.LT.HGMIN) GO TO 1213            ST382130
178     1212  IF(ITER.LE.1) GO TO 1211            ST382140
179     HATA(IPOW)=1H                            ST382150
180     IF(ABS(DELTA2/HG2).LT.0.01) HATA(IPOW)=1HA  ST382160
181     IF(ABS(DELTA2/HG2).LT.0.01) GO TO 1230    ST382170
182     IF(ABS((HG2-HG1)/HG1).LT.0.0002) HATA(IPOW)=1HB  ST382180
183     IF(ABS((HG2-HG1)/HG1).LT.0.0002) GO TO 1230    ST382190
184     IF(ISTEP.EQ.1.AND.ITEM.GT.1) GO TO 1230    ST382200
185     IF(ITER.GT.45) GO TO 1220                ST382210
186     HG = HG2 - DELTA2*(HG2-HG1)/(DELTA2-DELL)  ST382220
187     IF(HG.GT.HGMAX) HG = HGMAX                ST382230
188     IF(HG.LE.HGMIN) HG = HGMIN                ST382240
189     DELTA1 = DELTA2                          ST382250
190     HG1 = HG2                                ST382260
191     IF(HG.EQ.HGMAX.AND.HG1.EQ.HGMIN) HG = (HGMAX+HGMIN)/2.0  ST382270
192     IF(HG.EQ.HGMIN.AND.HG1.EQ.HGMAX) HG = (HGMAX+HGMIN)/2.0  ST382280
193     GO TO 520                                ST382290

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* SOURCE STATEMENT (ST3T08)*

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194 1211 CONTINUE          ST382370
195   DELTA1 = HGC+ HG      ST382380
196   HG1 = HG              ST382390
197   HG = HGC              ST382400
198   IF (ABS(DELTA1).GT.0.8.AND.HG1.NE.0.568) HG = 0.568 ST382410
199   GO TO 520             ST382420
200 1213 HMX = HGMAX + HGMIN ST382430
201   HMM = 0.2*(HGMAX + HGMIN) ST382440
202   HGMAX = HMX             ST382450
203   HGMIN = HMM             ST382460
204   GO TO 1212             ST382470
205 1220 CONTINUE           ST382480
C NOV-CONVERGENCE IN GAP CONDUCTANCE ST382490
206   NOCONV = 1             ST382500
207   HGIO = HG              ST382510
208   HGCO = HGC              ST382520
209   ISTPNO = ISTEP         ST382530
210   IPGWNO = IPOW          ST382540
211   NPOWNO = NPOW          ST382550
212   IF (ITER.GT.45) WRITE(6,3000) ST382560
213   NP1 = N + 1             ST382570
214   IF (ITER.GT.45) WRITE(6,3010) (BB(3,I),I=1,NP1) ST382580
215 1230 CONTINUE           ST382590
216   IF (ITER.GT.50.AND.NOCONV.EQ.0) GO TO 1220 ST382600
C----- CALL STEP8 ST382610
217   PREHGI(IPOW) = HG      ST382620
218   HGACI(IPOW) = HGACEL   ST382630
219   MERO1(IPOW,ISTEP) = ITER ST382640
220   C----- ST382650
C***** DONT RETURN TO GAP-CON ITERATION LOOP IN THIS VERSION ST382660
221   TAVGX=TAVGX+TBAC(IPOW) ST382670
222   VOLTXS=VOLTXS+VOLTX(IPOW) ST382680
C----- ST382690
C***** STORE THE NODAL INFORMATION FOR OUTPUT 74.8.26 ***** ST382700
223   IF (ISTEP.LT.ISTOP) GO TO 2001 ST382710
C----- ST382720
224   TCOLT(IPOW) = TCOOL    ST382730
225   HFLTM(IPOW) = HF       ST382740
226   TCOLCA(IPOW) = TCD     ST382750
227   TCICAC(IPOW) = TCI     ST382760
228   CCNMB(IPOW) = TCC     ST382770
229   TGPXPC(IPOW) = (TCI+TFS)/2, ST382780
230   HFLXFB(IPOW) = GOVKAS ST382790
231   GCSL(IPOW) = HSOLID   ST382800
232   GCGL(IPOW) = HNGAS    ST382810
233   GCR(IPOW) = HRAD     ST382820
234   GCTC(IPOW) = HGC      ST382830
235   TJUMP(IPOW) = *1PG2   ST382840
C----- ST382850
236   DRTF(IPOW) = DELRT   ST382860
237   DRSF(IPOW) = DELRB   ST382870
238   DRUF(IPOW) = DELRDE   ST382880
239   DRHF(IPOW) = DELKRE   ST382890
240   DRF(IPOW) = DELR     ST382900
241   DRTC(IPOW) = DELRCI   ST382910
242   DRPC(IPOW) = DELRP   ST382920
243   DRCLD(IPOW) = DELRCI+DELRP+DELRC   ST382930
244   TFSCA(IPOW) = TFS    ST382940
245   DRCC(IPOW) = DELRCC  ST382950

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* SOURCE STATEMENT (ST3T08)*

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246   BR1(IPOW) = RVOID    ST382960
247   BR2(IPOW) = R1700    ST382970
248   BR3(IPOW) = R1390    ST382980
249   RH+(IPOW) = RFS + DELR  ST382990
250   RATF(IPOW) = DELP/RFS *100. ST383000
251   RATC(IPOW) = DELRCO/RCO *100. ST383010
252   CPRES(IPOW) = PFACE   ST383020
253   CSTRES(IPOW) = STREST ST383030
254   GASC(IPOW) = GASKON   ST383040
255   GASCB(IPOW) = GK     ST383050
C----- ST383060
256   ITERZ(IPOW) = ITER   ST383070
257   FCOUNT(IPOW) = CFLAG ST383080
C----- ST383090
258   DVCDX(IPOW) = RVOIDX*2, ST383100
259   DVOLDH(IPOW) = RVOID *2, ST383110
260   DFSX(IPOW) = DFS     ST383120
261   DCIX(IPOW) = DCI     ST383130
262   DCOK(IPOW) = DCO     ST383140
263   VVOLDX(IPOW) = VVOIDC ST383150
264   VVOLDH(IPOW) = VVOID  ST383160
265   TSINX(IPOW) = TSINC   ST383170
266   PSINX(IPOW) = PSIN    ST383180
267   VOIDL(IPOW) = VLENGT  ST383190
268   TDISH(IPOW) = TSHOUL ST383200
C----- ST383210
269   DO 25 J=1,5          ST383220
270   ZLENGT(J,IPOW) = PLENGT(J) ST383230
271   25 CONTINUE           ST383240
C----- ST383250
272   DENSL(1,IPOW) = DENSL ST383260
273   DENSL(2,IPOW) = FL*DENSL ST383270
274   DENSL(3,IPOW) = PLENGT(4) + DENSL(2,IPOW) ST383280
275   DENSL(4,IPOW) = PLENGT(4) ST383290
276   DENSL(5,IPOW)=0.0    ST383300
C----- ST383310
277   2001 CONTINUE          ST383320
C----- ST383330
278   1370 CONTINUE          ST383340
C----- ST383350
279   IF (MGAS.LE.0)          CALL MOLMOL(4) ST383360
280   IF (MGAS.EQ.1)          CALL MOLMO4  ST383370
281   RETURN                 ST383380
C----- ST383390
282   3000 FORMAT(1H1, 7X, 18H FUEL TEMPERATURE ,80X,6HS13T08) ST383400
283   3010 FORMAT(1H1 , 10X, 10F10.2) ST383410
284   END                     ST383420

```

* SOURCE STATEMENT *

```

1      SUBROUTINE CARL(TSS,TFS,TT,N,P1,DFS,STORE)
C
C      THIS SUBROUTINE IS CALLED FROM STEP 8
C      REFER BNWL-1778, GAPCON THERMAL-1, PAGE 4-19
C      CALCULATING STORED ENERGY OF THE FUEL
C
C      DIMENSION AREA(50),TVOL(50),HCAT(50)
C      DIMENSION TSS(50),TT(50)
C      REAL K1,K2,K3
C
DO 10 I=1,N
 10 AREA(I) = ((TSS(I)**2-TSS(I+1)**2)*PI)
    TVOL(I) = ((TFS*TT(I)) * .5) + 273.
    DO 20 I=2,N
 20  TVOL(I) = ((TT(I)+TT(I-1)) * .5) + 273.
    TKEL = 535.285
    ED = 37.6346
    K1 = 19.1450
    K2 = .000784733
    K3 = 5643730.0
    R = .001986
    CL = 1.0
    STORE = 0.0
    DO 40 I=1,N
 40  TEMPK = TVOL(I)
    HCAT(I)=CL*(K2*(TEMPK**2-298.**2)+K3*EXP(-ED/R/TEMPK)
    * +K1*TKEL*(1./EXP(TKEL/TEMPK)-1.)-1./(EXP(TKEL/298.)-1.))
    STORE = STORE + HCAT(I)*AREA(I)
    40 CONTINUE
    STORE = STORE*4./(PI*DFS**2)
C
C      NOW CONVERT IT TO CAL./GRAM OF UO2
C
    STORE = STORE/27.0
    RETURN
C*****END

```

CARL0010
CARL0020
CARL0030
CARL0040
CARL0050
CARL0060
CARL0070
CARL0080
CARL0090
CARL0100
CARL0110
CARL0120
CARL0130
CARL0140
CARL0150
CARL0160
CARL0170
CARL0180
CARL0190
CARL0200
CARL0210
CARL0220
CARL0230
CARL0240
CARL0250
CARL0260
CARL0270
CARL0280
CARL0290
CARL0300
CARL0310
CARL0320
CARL0330
CARL0340
CARL0350
CARL0360

* SOURCE STATEMENT *

```

1      SUBROUTINE CHECK(KE)                               CHEC0010
C
C      THIS SUBROUTINE INPUT THE DATA CHECK           CHEC0020
C      THIS SUBROUTINE IS CALLED FROM DATINP        CHEC0030
C
2      COMMON /POWRAY/ PAVRG,FUELLE,FL,POWER(21),AI(21),NPOW,P10T,LPMAX,   CHEC0040
1          PKPOW,IPEAK,DELT,PMAX                         CHEC0050
3      COMMON /INPUT/ FRDEN,FRSIN,DSINZ,FRPU02,FR35,FR40,FR41,DFS,DCI,   CHEC0060
1          DCO,VOID1Z,VPLENZ,ATMOS,S,XX,ROUF,ROUC,EXTP,DE,V,   CHEC0070
2          TINLET,DELT,TMAX,TFR,TMD,BK,HBC,SIGHF,IFLUX,   CHEC0080
3          NCLAD,NCON,NFLX,KOOL,NEWK,NEWL,NEWFLX,VOIDL,NOH,CHEC0110
4          FRACHE,FRACAR,FRACH,FRACRN,FRACKR,FRACXE,HGACEL,   CHEC0120
5          DTEMP,ZCLAD,HG,PKAVG,MINI,ICDF,ISTOR,ICREP,ISWELL,CHEC0130
6          ,NEXP,MEXP,NHIST                                CHEC0140
4      COMMON /INPUTA/ MREST,LCREP,DDISH,HDISH          CHEC0150
5      COMMON /COM 0/ TITLE(20),AA(7, 30),BB(6, 51),CF(3, 30),RV(2, 20)  CHEC0160
6      COMMON /COM 21/ N,NN,NNN,NF                      CHEC0170
7      COMMON /D15 / MDEN,MRELOC, SINTEM             CHEC0180
8      DIMENSION II(10),III(10)                      CHEC0190
C
9      GO TO 10000,20000,30000,40000                ),KE
C
10     ======                                         CHEC0220
11    10000 CONTINUE                                CHEC0230
12    DO 1 J=1,10                                     CHEC0240
13    1 II(J)=0                                     CHEC0250
14    IF(NPOW,LE,0,OR,NPO4,GT,20) II(1)=1           CHEC0260
15    IF(KOOL,EW,1) GO TO 10                        CHEC0270
16    IF(.NOT.,(SIGHF,EQ,0,OR,SIGHF,EQ,-1,)) GO TO 10  CHEC0280
17    IF(V,LE,0,OR,DE,LE,0,) II(2)=1                 CHEC0290
18    10 CONTINUE                                    CHEC0300
19    IF(MDEN,EW,0,OR,MDEN,EW,2) GO TO 14            CHEC0310
20    IF(MDEN,EW,1) GO TO 12                        CHEC0320
21    IF(FRDEN,LT,0.895,OR,FRDEN,GT,1.0,OR,   CHEC0330
22    SINTEM,LT,1300.,OR,SINTEM,GT,1700.,) II(3)=1   CHEC0340
23    GU TO 14                                     CHEC0350
24    12 IF(MDEN,NE,2) GO TO 13                      CHEC0360
25    13 IF(FRDEN,LT,0.895,OR,FRDEN,GT,0.945,OR,   CHEC0370
26    SINTEM,LT,1400.,OR,SINTEM,G1,1800.,) II(3)=2   CHEC0380
27    14 CONTINUE                                    CHEC0390
28    15 CONTINUE                                    CHEC0400
29    16 TFLMPST,EW,1,AND,FRSIN,LE,FRDEN) II(4)=1   CHEC0410
30    HATA = 0.0                                     CHEC0420
31    DO 2 J=1,10                                     CHEC0430
32    2 IF((II(J),NE,0) HATA=1.0                  CHEC0440
33    IF(HATA,NE,0) GO TO 20                        CHEC0450
34    RETURN                                         CHEC0460
35    20 CONTINUE                                    CHEC0470
36    PRINT 501                                     CHEC0480
37    IF((II(1),EW,1) *WRITE(6,1000) NPOW          CHEC0490
38    IF((II(2),EW,1) *WRITE(6,1010) SIGHF,DE,V   CHEC0500
39    IF((II(3),EW,1) *WRITE(6,1020) MDEN,FRDEN,SINTEM  CHEC0510
40    IF((II(4),EW,1) *WRITE(6,1030) MDEN,FRDEN,SINTEM  CHEC0520
41    IF((II(5),EW,1) *WRITE(6,1040) MREST,FRSIN,FRDEN  CHEC0530
42    *WHITE(6,502)                                CHEC0540
43    STOP                                           CHEC0550
C
44    ======                                         CHEC0560
45    20000 CONTINUE                                CHEC0570
46    DO 201 J=1,10                                CHEC0580
47    201 III(J)=0                                CHEC0590

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* SOURCE STATEMENT (CHECK) **

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44    IF(RV(1+NF),LT,DFS) III(1) = 2               CHEC0600
45    HATA = 0.0                                     CHEC0610
46    DO 202 J=1,10                                CHEC0620
47    202 IF((II(J),NE,0) HATA = 1.0              CHEC0630
48    IF(HATA,NE,0) GO TO 220                      CHEC0640
49    RETURN                                         CHEC0650
50    220 CONTINUE                                    CHEC0660
51    *WHITE(6,501)                                CHEC0670
52    IF((II(1),EQ,2) *WHITE(6,2010) DFS,RV(1+NF)  CHEC0680
53    *WHITE(6,502)                                CHEC0690
54    STOP                                           CHEC0700
C
55    30000 CONTINUE                                CHEC0710
56    RETURN                                         CHEC0720
57    40000 CONTINUE                                CHEC0730
58    RETURN                                         CHEC0740
59    ======                                         CHEC0750
60    501 FORMAT(//,7X,50(1H*),24H INPUT THE DATA ERROR : 50(1H*) //)  CHEC0770
61    502 FORMAT( 3/ 7X, 12A(1H*)                   / )  CHEC0780
62    1000 FORMAT( 7X,                                CHEC0790
63    1116H* ( ) NUMBER OF AXIAL SEGMENTS *** NPOW SHOULD BE < NPOW  CHEC0800
64    2,GE,1,AND,NPOW,LE,20) ***                      NPOW =, 14 //)  CHEC0810
65    1010 FORMAT( 7X,                                CHEC0820
66    1115H* ( ) CALCULATE THE COOLING-TO-COOLANT HEAT TRANSFER COEF  CHEC0830
67    2FICIENT                                     SIGHF =, F10.4 /7X,CHEC0840
68    3116H* ( ) COOLANT PASSAGE EQUIVALENT DIAMETER           CHEC0850
69    DE =, F10.4 /7X,CHEC0860
70    5116H* ( ) COOLANT VELOCITY                  CHEC0870
71    V =, F10.4 /7X,CHEC0880
72    7126H* ( ) WHEN (SIGHF,EQ,0,) OR (SIGHF,EQ,-1,) V AND DE SHOCHEC0890
73    BULD NOT BE ZERO,                            ) CHEC0900
74    1020 FORMAT( 7X,                                CHEC0910
75    1 60HIF(FRDEN,EQ,1) (0,8, ,LE,FRDEN,LE,1,0 ) AND (1300.,LE,SINT  CHEC0920
76    2 19HEM,LE,1700,) MDEN=-13,     8H, FRDEN=-, E12.5,  9H, SINTEM=-, ) CHEC0930
77    3     E12.5,  6H,CHECK                           ) CHEC0940
78    1030 FORMAT( 7X,                                CHEC0950
79    1 60HIF(FRDEN,EQ,2) (0,895,LE,FRDEN,LE,0,945) AND (1400.,LE,SINT  CHEC0960
80    2 19HEM,LE,1800,) MDEN=-13,     8H, FRDEN=-, E12.5,  9H, SINTEM=-, ) CHEC0970
81    3     E12.5,  6H,CHECK                           ) CHEC0980
82    1040 FORMAT( 7X,                                CHEC0990
83    1 58HIF(MREST,EQ,1) FR SIN SHOULD BE GREATER THAN FR DEN. MREST=,12,CHEC1000
84    2 10H,  FR SIN=-,F10.5+10H,  FR DEN=-,F10.5  ) CHEC1010
85    2010 FORMAT( 7X,                                CHEC1020
86    1116H* ( ) PELLET DIAMETER                  CHEC1030
87    2 DFS =, F10.4 /7X,CHEC1040
88    3116H* ( ) FLUX DEPRESSION VALUES USED      CHEC1050
89    4 MAXIMUM DIAMETER                         RV(1,NF)=, F10.4 /7X,CHEC1060
90    5 40H SHOULD BE ( RV(1,NF),GE,DFS )          ) CHEC1070
91    END                                           CHEC1080

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* SOURCE STATEMENT *

```

1      SUBROUTINE CREEP(1AU,PHI,SIGC,CTEM,PEXT,PINT,DCO,DCI,SC1,SC2,
1                      EPST,DEPS,ICREEP)
C
C      THIS SUBROUTINE IS CALLED FROM STEP5
C
2      COMMON /CREP1/ A1,A2,A3,A4,A5
2          /CREP2/ B1,B2,B3,B4
2          /CREP3/ C1,C2
2          /CREP4/ D1,D2
2          /CREP5/ E1,E2,E3
2          /CREP6/ F1,F2,F3,F4,F5,F6,G1,G2,G3,G4
C----- INPUT PARAMETERS -----
C
C      PHI..... FAST NEUTRON FLUX (N/CM2/SEC)
C      TAU..... TIME IN REACTOR (HOUR)
C      CTEM... MEAN CLADDING TEMPERATURE (DEG C)
C      PEXT... EXTERNAL PRESSURE (KG/MM2)
C      DCO.... CLAD OD (CM)
C      DCI.... CLAD ID(CM)
C      SIGC... CIRCUMFERENTIAL STRESS (KG/NM2)
C      ICREEP.. CREEP DEFORMATION MODELS AND EQUATION OPTION
C              = 1 BUCKLE (BNWL-B-253,1973)
C              = 2 OLD AT&T(PNC) MODEL
C              = 3 ZRY PRESSURE TUBE . . . . . ROSS-ROSS,P.A.+HUNT
C              = 4 FIGO (WAPD-TM-618 ADDENDUM 2 P-5)
C              = 5 AT&T(PNC) NEW
C
3      CLTK=CTEM+273.
4      PEXTPAPEXT*100.*14.22
5      PINTP=PINT*100.*14.22
6      RCOH =DCO/2./2.54
7      RC1H =DC1/2./2.54
8      SIGCP=SIGC*100.*14.22
C
9      IF(ICREEP) 20+20+21
10     20 WRITE(*,110) ICREEP
11     110 FORMAT(//,10X,35HAPPOINTED OPTION ERROR      ICRE=    13   /)
12     ICREEP=1
13     21 CONTINUE
C
14     GO TO (1,2,3,4,5,6,7,8,9,10)           //ICREEP
15     1 CONTINUE
CC ----- BUCKLE -----
C      CONSTANTS
C      R ..... GAS CONSTANT          1.98 CAL/MOLE/DEG K
C      Q ..... ACTIVATION ENERGY      16960 CAL/MOLE
C      ALP .... TRANSIENT CREEP COEFF. 900
C      K ..... ;                      0.006
C      SC ..... STRESS COEFFICIENT    1.E-4 - 1.7E-4
C
16     R=1.98
17     A=00.
18     C=U.006
19
20     A1=SINH(SC1*SIGCP)
21     A2=EXP(-Q/R/CLTK)
22     A3=PHI**0.85

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* SOURCE STATEMENT (CRFP)

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23     A4=(TAU+A  *(1.-EXP(-C*TAU)))
24     A5=(1.-A  *C*EXP(-C*TAU))
C
25     EPST=9.5E-13*A1*A2*A3*A4
26     DEPS=9.5E-13*A1*A2*A3*A5
C
27     RETURN
28     2 CONTINUE
C----- OLD AT&T -----
C      CONSTANTS
C      Q ..... ACTIVATION ENERGY      14000 CAL/MOLE
C      R ..... GAS CONSTANT          1.98 CAL/MOLE/DEG K
C      SC ..... STRESS COEFFICIENT    1.15E-4
C
29     R=1.98
30     G=14000.
C
31     B1=SINH(SC2*SIGCP)
32     B2=EXP(-Q/R/CLTK)
33     B3=P-1**U.65
34     B4=TAU
C
35     EPST=1.02E-13*B1*B2*B3*B4
36     DEPS=1.02E-13*B1*M2*B3
37     RETURN
C
38     3 CONTINUE
C----- ZRY PRESSURE TUBE (ZIRCONIUM 2.5 NB)
C      CONSTANTS
C      BETA .... MATERIAL PROPERTY COEFF. 1422*4.E-27
C      TREF .... REFERENCE TEMP.        160 DEG C
C
39     BETAA=1422.*4./1.E27
40     TREF=160.
41     C1=BETA
42     C2=CTEM-TREF
C
43     EPST=C1*SIGC*PHI*C2*TAU
44     DEPS=C1*SIGC*PHI*C2
45     RETURN
C
46     44 CONTINUE
C----- ZR PRESSURE TUBE (ZIRCONIUM 2.5 NB)
C      CONSTANT
C      BETA .... MATERIAL PROPERTY COEFF. 1422*4/3 E-27
C      TREF .... REFERENCE TEMP.        160 DEG C
C
47     BETAA=1422.*4./3./1.E27
48     TREF=160.
C
49     D1=BETA
50     D2=CTEM-TREF
C
51     EPST=D1*SIGC*PHI*D2*TAU
52     DEPS=D1*SIGC*PHI*D2
53     RETURN
C

```

* SOURCE STATEMENT (CREP) *

```

54      4 CONTINUE
C ----- FIGRO -----
C   CONSTANTS
C     C .....           1.11E-24
C     D .....           1.03E-24
C     TREF ..... REFERENCE TEMP. 149 DEG C
C     SIGA=REFERENCE STRESS 8.44KG/MM2
C     SIGG=GENERALIZED STRESS (KG/MM2)
C     PINT,... INTERNAL PRESSURE (KG/MM2)
C
C
55     C=1.11E-24
56     D=1.03E-24
57     TREF=149,
58     SIGA=.44
59     RC=(DCO+DC1)/4,
60     TC=(DC0+DC1)/2,
61     SIGGSQRT(S.)*(PEXT-PINT)*RC/(2.*TC)
62     E1=SIGG
63     IF(SIGG.GE.SIGA) GO TO 50
64     EPSTC*SIGG*(CTEM-TREF)*PHI*TAU
65     DEPS=EPSTC*SIGG*(CTEM-TREF)*PHI
66     GO TO 51
67 50 CONTINUE
68     E2=D*SIGG**4
69     E3=C*SIGG*(CTEM-TREF)
70     EPST=(E3+E2)*PHI*TAU
71     DEPS=(E2+E3)*PHI
72 51 CONTINUE
73     RETURN
C
74      5 CONTINUE
C
C ----- ATR (NEW) -----
C   CONSTANTS
C     R1 ..... GAS CONSTANT          1.985 CAL/MOLE/DEG K
C     TREF ..... REFERENCE TEMP.      300 DEG C
C     HCAP ..... 14000 CAL/MOLE
C
C
75     R1=1.985
76     TREF=300,
77     HCAP=14000,
78     F1=TAU**0.085
79     F2=SIGCH**2.61
80     F3=EXP(1.19*(CTEM-TREF)/CLTK)
81     F4=SIGCF**1.225
82     F5=PHI**0.85
83     F6=EXP(-HCAP/R1/CLTK)
C
C
84     G1=1.19E-15*F1*F2*F3
85     G2=2.12E-18*TAU*F4*F5*F6
86     EPST=G1+G2
87     F7=TAU**(-0.085-1.)
88     G3=1.156E-15 *0.085*F7*F2*F3
89     G4=2.12 E-18*F4*F5*F6
90     DEPS=G3+G4
91     RETURN
C
92      6 CONTINUE
93      7 CONTINUE

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* SOURCE STATEMENT (CREP) *

```

94      8 CONTINUE
95      9 CONTINUE
96      10 CONTINUE
97      RETURN
98      END

```

* SOURCE STATEMENT *

```

1      SUBROUTINE CURIE(KS)                                CURI0010
C **** **** **** **** **** **** **** **** **** **** **** **** CURI0020
C THIS ROUTINE CALCULATE NUMBERS OF CURIOS OF EACH ISOTOPES CURI0030
C DC( ) ... DECAY CONSTANT (1/SEC)                      CURI0040
C A( ) ... NUMBERS OF ATOM PER UNIT LENGTH             CURI0050
C DISIN = 3.7 E10 DISINTEGRATION / SEC                CURI0060
C
C **** **** **** **** **** **** **** **** **** **** **** CURI0080
2      COMMON /NUCLEI/ NUCLEI,A(*,23)                   CURI0090
3      COMMON /DECAY/ DC2,DC3,DC4,DC5,DC6,DC12,DC14,DC15,DC21,DC22,DC23,CURI0100
4          DC25,DC26,DC28,DC31,DC33,DC34,DC35,DC85,DCB5,CURI0110
5      COMMON /FFMOL/ FF(4,23),RKR(6,23),RXE(6,23),RXX(10,20,2) CURI0120
6      COMMON /POWRAY/ PAVRG,FEUILL,FL,POWER(21),AT(21),INPOW,PTOT,LPMAX, CURI0130
7          PKPOWR,IPEAK,DELPHMAX,CURI0140
8          DATA DISIN /3.7E10/
C
9      DIMENSION CURRI(19,21),ATOMS(19,21)               CURI0150
10     DIMENSION DC(19),B(20),C(20)                     CURI0160
11     DATA DISIN /3.7E10/
C
12     GO TO (1,2,3) + KS                               CURI0170
C-----SET UP DECAY CONSTANT ARRAY                    CURI0180
C-----CONTINUE                                     CURI0190
13     DC(1)=0.0                                         CURI0200
14     DC(2)=0.0                                         CURI0210
15     DC(3)=DC85H                                       CURI0220
16     DC(4)=DC89                                         CURI0230
17     DC(5)=0.0                                         CURI0240
18     DC(6)=DC21                                         CURI0250
19     DC(7)=DC22                                         CURI0260
20     DC(8)=DC23                                         CURI0270
21     DC(9)=0.0                                         CURI0280
22     DC(10)=DC25                                         CURI0290
23     DC(11)=DC31                                         CURI0300
24     DC(12)=0.0                                         CURI0310
25     DC(13)=DC26                                         CURI0320
26     DC(14)=DC33                                         CURI0330
27     DC(15)=0.0                                         CURI0340
28     DC(16)=DC28                                         CURI0350
29     DC(17)=DC34                                         CURI0360
30     DC(18)=DC35                                         CURI0370
31     DC(19)=0.0                                         CURI0380
32     RETURN                                           CURI0390
C-----CONTINUE                                     CURI0400
33     DO 10 I=1,19                                     CURI0410
34     B(I)=C(I)=0.0                                    CURI0420
35     DO 10 J=1,21                                     CURI0430
36     ATOMS(I,J)=CURRI(I,J)=0.0                         CURI0440
37     BB=CC=0.0                                         CURI0450
38     DO 15 I=1,INPOW*                                CURI0460
39     DO 20 K=1,19                                     CURI0470
40     J=K+20                                           CURI0480
C-----CALCULATE ATOMS AND CURIOS                   CURI0490
41     ATOMS(K,I)=A(I,J)*FL                           CURI0500
42     CURRI(K,I)=DC(I)*ATOMS(K,I)/DISIN              CURI0510
43     B(I)=B(I)+ATOMS(K,I)                           CURI0520
44     C(I)=C(I)+CURRI(K,I)                           CURI0530
45     ATOMS(K,21)=ATOMS(K,21)+ATOMS(K,I)             CURI0540
46     CURRI(K,21)=CURRI(K,21)+CURRI(K,I)             CURI0550
47     20 CONTINUE                                     CURI0560
48     BB=BB+C(I)                                     CURI0570
49     CC=CC+C(I)                                     CURI0580
50     15 CONTINUE                                     CURI0590
C-----PRINT OUT PIN INVENTORY                      CURI0600
51     FLAG=0.0                                         CURI0610
52     CALL HEAD(-1)                                   CURI0620
53     WRITE(6,100)                                     CURI0630
54 1000    CONTINUE                                     CURI0640
55     WRITE(6,103)                                     CURI0650
56     WRITE(6,104) <(DC(I),I=1,10)                  CURI0660
C
57     WRITE(6,107)                                     CURI0670
58     WRITE(6,113)                                     CURI0680
59     DO 25 I=1,INPOW*                                CURI0690
60     WRITE(6,105) I,(ATOMS(J,I),J=1,10)             CURI0700
61     25 CONTINUE                                     CURI0710
62     WRITE(6,108) <(ATOMS(J,21),J=1,10)             CURI0720
63     WRITE(6,114)                                     CURI0730
64     DO 26 I=1,INPOW*                                CURI0740
65     WRITE(6,105) I,(CURRI(J,I),J=1,10)             CURI0750
66     26 CONTINUE                                     CURI0760
67     WRITE(6,108) <(CURRI(J,21),J=1,10)             CURI0770
C
68     IF(INPOW.LE.6) CALL HEAD(-1)                   CURI0780
69     IF(INPOW.LE.8) WRITE(6,110)                     CURI0790
C
70     WRITE(6,112)                                     CURI0800
71     WRITE(6,104) <(DC(I),I=11,19)                 CURI0810
72     WRITE(6,107)                                     CURI0820
73     WRITE(6,113)                                     CURI0830
74     DO 30 I=1,INPOW*                                CURI0840
75     WRITE(6,105) I,(ATOMS(J,I),J=11,19)+B(I)       CURI0850
76     30 CONTINUE                                     CURI0860
77     WRITE(6,108) <(ATOMS(J,21),J=11,19),BB        CURI0870
78     WRITE(6,114)                                     CURI0880
79     DO 32 I=1,INPOW*                                CURI0890
80     WRITE(6,105) I,(CURRI(J,I),J=11,19)+C(I)       CURI0900
81     32 CONTINUE                                     CURI0910
82     WRITE(6,108) <(CURRI(J,21),J=11,19)+CC        CURI0920
C
83     IF(FLAG.LE.0.0) WRITE(6,115)                   CURI0930
84     IF(FLAG.GE.1.0) WRITE(6,116)                   CURI0940
85     IF(FLAG.GE.1.) RETURN                          CURI0950
86     FLAG=1.0                                         CURI0960
C-----RELEASED TO PLENUM AND GAP                   CURI0970
87     DO 45 I=1,19                                     CURI0980
88     B(I)=C(I)=0.0                                    CURI0990
89     ATOMS(I,21)=CURRI(I,21)=0.0

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* SOURCE STATEMENT (CURIE) *

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41     ATOMS(K,I)=A(I,J)*FL                           CURI1000
42     CURRI(K,I)=DC(I)*ATOMS(K,I)/DISIN              CURI1010
43     B(I)=B(I)+ATOMS(K,I)                           CURI1020
44     C(I)=C(I)+CURRI(K,I)                           CURI1030
45     ATOMS(K,21)=ATOMS(K,21)+ATOMS(K,I)             CURI1040
46     CURRI(K,21)=CURRI(K,21)+CURRI(K,I)             CURI1050
47     20 CONTINUE                                     CURI1060
48     BB=BB+C(I)                                     CURI1070
49     CC=CC+C(I)                                     CURI1080
50     15 CONTINUE                                     CURI1090
C-----PRINT OUT PIN INVENTORY                      CURI1100
51     FLAG=0.0                                         CURI1110
52     CALL HEAD(-1)                                   CURI1120
53     WRITE(6,100)                                     CURI1130
54 1000    CONTINUE                                     CURI1140
55     WRITE(6,103)                                     CURI1150
56     WRITE(6,104) <(DC(I),I=1,10)                  CURI1160
57     WRITE(6,107)                                     CURI1170
58     WRITE(6,113)                                     CURI1180
C-----CALCULATE ATOMS AND CURIOS                   CURI1190
59     ATOMS(K,I)=A(I,J)*FL                           CURI1200
60     CURRI(K,I)=DC(I)*ATOMS(K,I)/DISIN              CURI1210
61     B(I)=B(I)+ATOMS(K,I)                           CURI1220
62     C(I)=C(I)+CURRI(K,I)                           CURI1230
63     ATOMS(K,21)=ATOMS(K,21)+ATOMS(K,I)             CURI1240
64     CURRI(K,21)=CURRI(K,21)+CURRI(K,I)             CURI1250
65     20 CONTINUE                                     CURI1260
66     BB=BB+C(I)                                     CURI1270
67     CC=CC+C(I)                                     CURI1280
68     15 CONTINUE                                     CURI1290
C-----PRINT OUT PIN INVENTORY                      CURI1300
69     FLAG=0.0                                         CURI1310
70     CALL HEAD(-1)                                   CURI1320
71     WRITE(6,100)                                     CURI1330
72     WRITE(6,103)                                     CURI1340
73     WRITE(6,104) <(DC(I),I=1,10)                  CURI1350
74     WRITE(6,107)                                     CURI1360
75     WRITE(6,113)                                     CURI1370
76     DO 25 I=1,INPOW*                                CURI1380
77     WRITE(6,105) I,(ATOMS(J,I),J=1,10)             CURI1390
78     25 CONTINUE                                     CURI1400
79     WRITE(6,108) <(ATOMS(J,21),J=1,10),BB        CURI1410
80     WRITE(6,114)                                     CURI1420
81     DO 26 I=1,INPOW*                                CURI1430
82     WRITE(6,105) I,(CURRI(J,I),J=1,10)+B(I)       CURI1440
83     26 CONTINUE                                     CURI1450
84     WRITE(6,108) <(CURRI(J,21),J=1,10)+CC        CURI1460
85     IF(FLAG.LE.0.0) WRITE(6,115)                   CURI1470
86     IF(FLAG.GE.1.0) WRITE(6,116)                   CURI1480
87     IF(FLAG.GE.1.) RETURN                          CURI1490
88     FLAG=1.0                                         CURI1500
C-----RELEASED TO PLENUM AND GAP                   CURI1510
89     DO 45 I=1,19                                     CURI1520
90     B(I)=C(I)=0.0                                    CURI1530
91     ATOMS(I,21)=CURRI(I,21)=0.0

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SOURCE STATEMENT (CURIE) *

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90      45 CONTINUE                                CURI1190
91      BB=CC*0.0                                    CURI1200
92      DO 35 I=1,NPOW                            CURI1210
93      DO 40 K=1,19                               CURI1220
94      ATOMS(K+1)=ATOMS(K+1)*FF(1,I)           CURI1230
95      CURR(K+1)=CURR(K+1)*FF(1,I)           CURI1240
96      B(I)=B(I)+ATOMS(K+1)                   CURI1250
97      C(I)=C(I)+CURR(K+1)                   CURI1260
98      ATOMS(K+21)=ATOMS(K+21)+ATOMS(K,I)    CURI1270
99      CURR(K+21)=CURR(K+21)+CURR(K+1)       CURI1280
100     40 CONTINUE                                CURI1290
101     BB=BB*B(I)                                CURI1300
102     CC=CC+C(I)                                CURI1310
103     35 CONTINUE                                CURI1320
C
104     CALL HEAD(-1)                             CURI1330
105     WRITE(6,100)                             CURI1340
106     WRITE(6,201)                             CURI1350
107     GO TO 1000                               CURI1360
C
108     3 CONTINUE                                CURI1370
109     RETURN                                   CURI1380
C
110     100 FORMAT(40X,25HRADIO-ACTIVITY OF ISOTOPE / 40X,25(1H*) / ) CURI1390
111     101 F01FORMAT(10X,5(1H*),15H INVENTORY,5(1H*),/) CURI1400
112     103 FORMAT(4X,5HAXIAL /                  CURI1410
113     1 5X, 122HNODE   83 KR     84 KR     85M KR   85 KR   CURI1420
114     2 86 KR     131M TE   131 TE   131 I   131 XE   132 TECURI1430
115     3 4/2X+8(1H*),10(2X+10(1H*)) ) CURI1440
116     105 FORMAT(1X,12*DECAY CONST / 3X,7H(1/SEC),10(1X,1PE11.4) ) CURI1450
117     106 FORMAT(1X,12+2X,10(1X,1PE11.4) ) CURI1460
118     107 FORMAT(1H )                           CURI1470
119     108 FORMAT(/1X,9HSUB-TOTAL,10(1X,1PE11.4) ) CURI1480
120     112 FORMAT(4X,5HAXIAL,111X,4HNODE /      CURI1490
121     1 5X, 124HNODE   132 I   132 XE   133 I   133 XE   CURI1500
122     2134 XE   133 I   135M XE   135 XE   136 XE   SUB-TOTCURI1510
123     3AL /                                     CURI1520
124     4 2X,4(1H*),10(2X+10(1H*)) ) CURI1530
125     110 FORMAT(/)                            CURI1540
126     113 FORMAT(2X,12HNU. OF ATOMS )          CURI1550
127     114 FORMAT(/2X,6HCURIE )                 CURI1560
128     115 FORMAT(/ 1X,110(1H*), 25H INVENTORY FP GAS SUMMARY ) CURI1570
129     116 FORMAT(/ / 1X,110(1H*),25H RELEASED FP GAS SUMMARY ) CURI1580
130     201 FORMAT(10X,5(1H*),17H RELEASED FP GAS *5(1H*),/) CURI1590
C
131     END                                     CURI1600
C
132     END                                     CURI1610
133     END                                     CURI1620
134     END                                     CURI1630
135     END                                     CURI1640
136     END                                     CURI1650
137     END                                     CURI1660
138     END                                     CURI1670

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* SOURCE STATEMENT *

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1      SUBROUTINE DATAPR                         DAPR0010
C
C      THIS SUBROUTINE IS CALLED FROM MAIN        DAPR0020
C
C
2      DIMENSION IA(20)                          DAPR0030
3      IC=0                                      DAPR0040
4      1 IC=IC+1                                DAPR0050
5      READ(5,100,END=500) IA                   DAPR0060
6      IF(IC.EQ.1) GO TO 1000                  DAPR0070
7      IF(.NOT.(MOD(IC,50).EQ.1)) GO TO 400    DAPR0080
8      700 WRITE(6, 900)  (K,K=1,8)            DAPR0090
9      7000 WRITE(6, 200)  (K,K=1,8)           DAPR0100
10     800 CONTINUE                                DAPR0110
11     WRITE(6, 300) IC,IA                      DAPR0120
12     GO TO 1                                     DAPR0130
13     500 CONTINUE                                DAPR0140
14     WRITE(6, 400)  (K,K=1,8)            DAPR0150
15     5000 RETURN                                 DAPR0160
16     RETURN                                   DAPR0170
17     100 FORMAT(20A4)                           DAPR0180
18     200 FORMAT(1H1 4(/) 40X,35H N P U T      DATA   L I S T / DAPR0190
19     2   40X, 35(1H*) /                      DAPR0200
20     3   10X,10HCARD NO.,2X,B(9H,...,...,11) / DAPR0210
21     300 FORMAT(10X,19*1H,*2X,20A4)           DAPR0220
22     400 FORMAT(12X,8(9H,...,...,...,1) 10X,11HEND OF CARD ) DAPR0230
23     900 FORMAT(/22X,8(9H,...,...,...,1) )      DAPR0240
24     *****                                         DAPR0250
25     END                                         DAPR0260
26     *****                                         DAPR0270
27     END                                         DAPR0280

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* SOURCE STATEMENT *

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1      BLOCK DATA  DATA1                               DAT10010
2      C
3      C
4      REAL MUF,MOL,MOLEFR,MOLFR                   DAT10020
5      COMMON /DATA 1/ ZR(7,6),ZR4(7,6),ST(7,26),TABLE(2, 80)  DAT10030
6      COMMON /DATA 2/ EKLJ(6),GMWT(6),SIGLJ(6)          DAT10040
7      COMMON /DATA 3/ VOLAT(29),FISGR(29)            DAT10050
8      COMMON /DATA 4/ PI,CCPIN3,SECDAY,AVOGAD,RR,CONEN  DAT10060
9      COMMON /DATA 5/ SDOT,SDOTT,EF,MUF,EPSTIF,EPSTIC   DAT10070
10     COMMON /DATA 6/ NZR2,NZR4,NST                  DAT10080
11     COMMON /DATA 7/ NZR2,NZR4,NST / 6,6,26 /          DAT10090
12     C
13     C     FP GAS RELEASE RATE FROM UO2 PELLET       REF. D-936
14     DATA VOLAT/0.0,.755,.755,.760,.785,.800,.810,.820,.825,  DAT10100
15     1.830,.840,.850,.855,.890,.920,.940,.955,.975,.965,.1000,.1015,.103 / DAT10110
16     20,.1100,.1160,.1300,.1470,.1690,.2000,.10000 / DAT10120
17     DATA FISGR/0.,.0006,.0008,.001,.002,.003,.004,.005,.006,.007,.008,.009,.01,.011,.012,.013,.014,.015,.016,.017,.018,.019,.02,.021 / DAT10130
18     1,.099,.01,.02,.03,.04,.05,.06,.07,.08,.09,.1,.16,.2,.3,.4,.5,.52,  DAT10140
19     2,.1 / DAT10150
20     C
21     C     INFLUXING TEMPERATURE FOR TABULATION (C)    DAT10160
22     C     THERMAL CONDUCTIVITY (W/CM/C)             DAT10170
23     C     YIELD STRENGTH (KG/CM2)                   DAT10180
24     C     YOUNG'S MODULUS (KG/CM2)                  DAT10190
25     C     POISSON'S RATIO (IND)                      DAT10200
26     C     LINEAR COEF. THERMAL EXPANSION (1/C)       DAT10210
27     C     MEYER HARDNESS NUMBER (KG/CM2)             DAT10220
28     C
29     C     ZRH(I,J)= PROPERTIES OF ZIRCALOY-2        DAT10230
30     C
31     DATA ((ZRH(I,J),I=1,7),J=1,6) / DAT10240
32     1 25. , 0.128 , 3150. , 972000. , 0.370 , 5.83E-6 , 9470. ,  DAT10250
33     2 100. , 0.134 , 2450. , 914000. , 0.400 , 6.25E-6 , 7360. ,  DAT10260
34     3 200. , 0.142 , 1670. , 850000. , 0.446 , 6.66E-6 , 5030. ,  DAT10270
35     4 300. , 0.156 , 1110. , 780000. , 0.492 , 6.97E-6 , 3340. ,  DAT10280
36     5 400. , 0.170 , 850. , 710000. , 0.492 , 7.18E-6 , 2360. ,  DAT10290
37     6 500. , 0.184 , 700. , 640000. , 0.492 , 7.34E-6 , 2110. / DAT10300
38     C
39     C     ZRH-4 DATA BY B.B.SCOTT (WCAP-3629-41) PAGE 6  DAT10310
40     C
41     DATA ((ZRH4(I,J),I=1,7),J=1,6) / DAT10320
42     1 25. , 0.129 , 3150. , 972000. , 0.370 , 5.83E-6 , 9470. ,  DAT10330
43     2 100. , 0.136 , 2450. , 914000. , 0.400 , 6.25E-6 , 7360. ,  DAT10340
44     3 200. , 0.143 , 1670. , 850000. , 0.446 , 6.66E-6 , 5030. ,  DAT10350
45     4 300. , 0.156 , 1110. , 780000. , 0.492 , 6.97E-6 , 3340. ,  DAT10360
46     5 400. , 0.170 , 850. , 710000. , 0.492 , 7.18E-6 , 2360. ,  DAT10370
47     6 500. , 0.184 , 700. , 640000. , 0.492 , 7.34E-6 , 2110. / DAT10380
48     C
49     C     ST(I,J)= PROPERTIES OF 20-PERCENT GOLD WORKED TYPE 316 SS  DAT10390
50     C
51     DATA ((ST(I,J),I=1,7),J=1,10) / DAT10400
52     1 25. , 0.143 , 6350. , 1972000. , 0.267 , 16.45E-6 , 19200. ,  DAT10410
53     2 50. , 0.146 , 6150. , 1966000. , 0.268 , 16.62E-6 , 18400. ,  DAT10420
54     3 75. , 0.152 , 6000. , 1960000. , 0.270 , 16.75E-6 , 17800. ,  DAT10430
55     4 100. , 0.153 , 5850. , 1945000. , 0.272 , 16.87E-6 , 17500. ,  DAT10440
56     5 125. , 0.159 , 5730. , 1925000. , 0.274 , 17.00E-6 , 17200. ,  DAT10450
57     6 150. , 0.162 , 5650. , 1910000. , 0.276 , 17.12E-6 , 17000. ,  DAT10460
58     7 175. , 0.166 , 5590. , 1890000. , 0.278 , 17.23E-6 , 16800. ,  DAT10470
59     C
60     C     ST(I,J)= PROPERTIES OF 20-PERCENT GOLD WORKED TYPE 316 SS  DAT10480
61     C
62     DATA ((ST(I,J),I=1,7),J=1,10) / DAT10490
63     1 25. , 0.143 , 6350. , 1972000. , 0.267 , 16.45E-6 , 19200. ,  DAT10500
64     2 50. , 0.146 , 6150. , 1966000. , 0.268 , 16.62E-6 , 18400. ,  DAT10510
65     3 75. , 0.152 , 6000. , 1960000. , 0.270 , 16.75E-6 , 17800. ,  DAT10520
66     4 100. , 0.153 , 5850. , 1945000. , 0.272 , 16.87E-6 , 17500. ,  DAT10530
67     5 125. , 0.159 , 5730. , 1925000. , 0.274 , 17.00E-6 , 17200. ,  DAT10540
68     6 150. , 0.162 , 5650. , 1910000. , 0.276 , 17.12E-6 , 17000. ,  DAT10550
69     7 175. , 0.166 , 5590. , 1890000. , 0.278 , 17.23E-6 , 16800. ,  DAT10560
70     C
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* SOURCE STATEMENT *

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1      SUBROUTINE DATINP(KS)                               DATP0010
C
C      THIS SUBROUTINE IS CALLED FROM STEP1             DATP0020
C      THIS SUBROUTINE INPUT THE DATA (IF UNIT IS C.G.S., KUNIT=1) DATP0030
C
2      REAL KB,LVOIDZ+LFUEL                           DATP0040
3      COMMON /IYIELD/ IYIELD                         DATP0050
4      COMMON /MCINV/ MCINV                          DATP0060
5      COMMON /CM 1/                                DATP0070
6      1 TT( $1),TSRC(51),GIN(51),N(51),TS(51),CLCRPD(2,20) DATP0080
7      COMMON /COM 03/ TO,P,DELRC0,DELRC,DELR,TCOOL,STP DATP0090
8      COMMON /CD 05/ BURNJP,TDAYS,VVOIDZ,TOTLDY,TOTBUR DATP0100
9      COMMON /COM 10/ VVOIDZ,FRU02,TPLENA,NPOW1 DATP0110
10     COMMON /COM 12/ DESEN1,FR38,FR39               DATP0120
11     COMMON /COM 15/ NCK+GAP                         DATP0130
12     COMMON /COM 21/ NANN+NNNN+NF                   DATP0140
13     COMMON /COM128/ IOUT1,IIPROF                  DATP0150
14     COMMON /D15/  MDEN,MRELOC,SINTED             DATP0160
15     COMMON /IXIR/ IX,IR,IH,MAXIEP                 DATP0170
16     COMMON /POWRAY/                               DATP0180
17     1 PAVRGD,FUEL ,FL   ,POWER(21),AI(21),NPOW,PTOT,LPMAX, DATP0190
18     2 PKPOW1,IPEAK (DELPO ,PMAKD)                DATP0200
19     COMMON /PONREF/ PONREF(21)                   DATP0210
20     COMMON /COM 07/                               DATP0220
21     1 TITLE(20),AADUM(7, 30),BBDDUM(6, 51),CFDDUM(3, 30),RVDDUM(2, 20) DATP0230
22     COMMON /INPUT/                               DATP0240
23     1 HDEG ,FRSIN ,DSINZ,FRHJ02,FR35 ,FR40 ,FR41 ,DFSDDUM,DCDDUM, DATP0250
24     2 DCDDUM,DSDDUM,VPLEN,ATMOS ,S   ,XX ,ROUDF +ROUCU +EXTPU + DATP0260
25     2 DEDIM ,VDDM + DATP0270
26     3 TINLET,DELT ,TMAX ,TFR ,TM   ,DBDDUM,BDDUM +BCCDDUM+SIGHFD, DATP0280
27     3 IFLUK , DATP0290
28     4 INCLAD ,NCON ,INFLA ,KOOL ,NEWK ,NEWFL ,INFLA ,VVOIDZL+NOH , DATP0300
29     5 FRACR,FRACR,FRACH ,FRACN ,FRACKR,FRACXE ,HGACEL, DATP0310
30     6 DTEMP0,ZCLAD ,HG   ,PEKAVG,MINI ,ICOF ,ISTOR ,ICREP ,ISWELL, DATP0320
31     7 NEXP ,MLXP ,NHIST ,COMMON /PRINT / PRINT           DATP0330
32     COMMON /MREVI / MREVI                         DATP0340
33     COMMON /NHIST / NHIST ,IPD(5,50)             DATP0350
34     COMMON /HIS / BASE(100),HIS(7,100),MODE(5,100) DATP0360
35     COMMON /HIST1/ NHIST ,ISTEP                  DATP0370
36     COMMON /INPUT A/ MREST,LCREP,DDISH,HDISH          DATP0380
37     COMMON /NUCLEI/ NUCLEI ,A(40,23)              DATP0390
38     COMMON /SPARE/ ISPA,NAMSP(3)                 DATP0400
39     COMMON /NEWGAS/ MGAS                         DATP0410
40     COMMON /TOTAL/ FPDIAL                      DATP0420
41     COMMON /PLGT / IPLOT                         DATP0430
42     DIMENSION AA1(30),AA2(30),AA3(30),AA4(30),AA5(30),AA6(30),AA7(30) DATP0440
43     DIMENSION CF1(30),CF2(30),CF3(30)             DATP0450
44     DIMENSION CLCHP(2,20)                        DATP0460
45     DIMENSION HISTIN(7,50)                        DATP0470
46     DIMENSION RV1(20),RV2(20)                     DATP0480
47     DATA PMAX,DELPO,FRDEN,FRSIN,DSINZ,FRPU02,FR35,FR40,FR41,DFS, DATP0490

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* SOURCE STATEMENT (DATINP)*

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*      DVOIDZ,DCI,DCO+VPLEN+ATMOS+S,XX,ROUC,ROUF,EXTP,TINLET, DATP0500
*      DE+V,PAVRG,TDAYS,DELT,TMAX,TFR,TM, SIGHF,FRACR, DATP0510
*      FRACR,FRACH,FRACN,FRACKR,FRACXE,HGACEL,ZCLAD,PKPOW+, DATP0520
*      PEKAVG,DTEMP,LFUEL,LVOIDZ,SINTED,SINTED / 45*0.0 / DATP0530
*      DATA HG /0,5678 / DATP0540
*      DATA NOH,KUNIT / 1+1 / DATP0550
*      DATA MCINV +MM+ ,MREVI +NUCLEI+ DATP0560
1      1 ISTOR ,IFLUK ,INCLAD ,NCON ,KOOL ,NEXP ,NHIST ,ICREP ,MINI DATP0570
2      2 ICOF ,ISWELL,NEXP ,IOUT1 ,IOUT2 ,IIPROF,MDEN ,MRELOC /21*0 DATP0580
*      DATA PRINT / 0 / DATP0590
*      DATA NPOW /10 / DATP0600
*      DATA POWER/23.+63.+96.1,21,1.35+1.4+1.35+1.21+.96+.63+.23 DATP0610
1      1 .10*0.0/ DATP0620
*      DATA MREST,LCREP,DDISH,HDISH / 2*0 + 2*0, / DATP0630
*      DATA WORD1/4HSTON / DATP0640
*      DATA HIST /350*0.0/, HISTIN/ 350*0.0 / , IPD/250*0/ DATP0650
*      DATA RVDDUM(1,1),RVDDUM(1,2),RVDDUM(2,1),RVDDUM(2,2) /0,0+1.0,1.0+1.0/ DATP0660
1      1 , NF,INFLX / 2+2 / DATP0670
1      1 IF(MODE(41),EW,0) RVDDUM(1,2)=DFSDDUM(GM) SEE STATEMENT NO.150 DATP0680
*      DATA CF1,CF2,CF3 / 90*0.0 / DATP0690
*      DATA AA1,AA2,AA3,AA4,AA5,AA6,AA7 / 210*0.0 / DATP0700
*      DATA PONREF / 21*0.0 / DATP0710
*      DATA IYIELD / 0 / DATP0720
*      DATA ISPA/0/,NAMSP/3*0/ DATP0730
*      DATA MGAS/0/ DATP0740
*      DATA FPDIAL/1.0/ DATP0750
*      DATA IPOLT / 0 / DATP0760
*      DATA MREVI /NUCLEI+ ,MREVI +NUCLEI+ DATP0770
1      1 FRPU02,FR40 ,FR41 ,FR35 ,FRDEN ,FRSIN ,SINTED, DATP0780
2      2 DFS ,DSINZ ,DVOIDZ ,DCI ,DCO ,LFUEL ,LVOIDZ+S ,XX , DATP0790
3      3 VPLEN+DTEMP ,DE +V ,ROUF ,ROUC ,TM ,ATMOS , DATP0800
4      4 FRACR,FRACR,FRACH ,FRACN ,FRACKR,FRACXE , DATP0810
5      5 SIGHF ,IFLUK ,NEXP ,KOOL ,NPOW + DATP0820
6      6 NGH ,MINI ,ICREP ,ICOF ,ISWELL,IPEAK ,IOUT1 ,IOUT2 ,IIPROF, DATP0830
7      7 NEXP ,MCINV ,KUNIT ,ISTOR ,NHIST ,MDEN ,MRELOC,IYIELD DATP0840
8      8 ,MREST,LCREP,DDISH,HDISH DATP0850
9      9 ,ISPA,NAMSP,MGAS DATP0860
*      *NUCLEI+FPDIAL,IPOLT DATP0870
*      NAMELIST /INPUT / ,MREVI +NUCLEI+ DATP0880
1      1 FRPU02,FR40 ,FR41 ,FR35 ,FRDEN ,FRSIN ,SINTED, DATP0890
2      2 DFS ,DSINZ ,DVOIDZ ,DCI ,DCO ,LFUEL ,LVOIDZ+S ,XX , DATP0900
3      3 VPLEN+DTEMP ,DE +V ,ROUF ,ROUC ,TM ,ATMOS , DATP0910
4      4 FRACR,FRACR,FRACH ,FRACN ,FRACKR,FRACXE , DATP0920
5      5 SIGHF ,IFLUK ,NEXP ,KOOL ,NPOW + DATP0930
6      6 NGH ,MINI ,ICREP ,ICOF ,ISWELL,IPEAK ,IOUT1 ,IOUT2 ,IIPROF, DATP0940
7      7 NEXP ,MCINV ,KUNIT ,ISTOR ,NHIST ,MDEN ,MRELOC,IYIELD DATP0950
8      8 ,MREST,LCREP,DDISH,HDISH DATP0960
9      9 ,ISPA,NAMSP,MGAS DATP0970
*      *NUCLEI+FPDIAL,IPOLT DATP0980
*      NAMELIST /INPUT2/ CF1,CF2,CF3 DATP0990
*      NAMELIST /INPUT3/ AA1,AA2,AA3+AA4,AA5,AA6,AA7 DATP1000
*      NAMELIST /INPUT4/ RV1, RV2 DATP1010
*      NAMELIST /INPUT5/ POWER DATP1020
*      GO TO (1000,2000+3000,4000) , KS DATP1030
60    1000 CONTINUE DATP1040
*      TITLE CARD INPUT DATP1050
*      CONTROL SIGNAL.....INPUT GROUP NO. 1 DATP1060
62    READ(5,1520,END=5000) TITLE DATP1070
63    DO 5001 I=1,20 DATP1080

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* SOURCE STATEMENT (DATINP) *

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64      IF(TITLE(1),ME,1H ) GO TO 5002                               DATP1190
65 5001 CONTINUE                                              DATP1200
66 5000 STOP                                                 DATP1210
67 5002 CONTINUE                                              DATP1220
68  IF(TITLE(1),EN,WORD1) STOP                                     DATP1230
C
C   NAMELIST INPUT                                              DATP1240
C
C   CONTROL SIGNAL.....INPUT GROUP NO. 2                         DATP1250
C   READ(S,INPUT)                                                 DATP1260
C
C   NPW1 = NPW + 1                                               DATP1270
C   HISTORY CARDS INPUT                                         DATP1280
C
C       HIST(1,J)  TIME(DAY)                                     DATP1290
C       HIST(2,J)  POWER(W/CM)                                    DATP1300
C       HIST(3,J)  TEMP. AT INLET COOLANT                         DATP1310
C       HIST(4,J)  EXTERNAL PRESS. ON CLADDING SURFACE          DATP1320
C
C       IPD(1,J) =                                                 DATP1330
C       IPD(2,J) = (NOT CHANGE)++(NEW FUEL THERMAL CONDUCTIVITY INPUT) DATP1340
C       IPD(3,J) = (NOT CHANGE) --(BUILTIN DATA)++(EXTERNAL)        DATP1350
C       IPD(4,J) = (NOT CHANGE) ++(NEW RAD.FLUX DEPRESS.) --1(BUILT IN) DATP1360
C       IPD(5,J) = (NOT CHANGE) ++(NEW AXIAL POWER DISTRIBUTION)    DATP1370
C
C   J = 0                                                       DATP1380
72   10 J =J+1                                              DATP1390
C
C   CONTROL SIGNAL.....INPUT GROUP NO. 3                         DATP1400
73   READ(S,551)  (HISTIN(I,J),I=1,7) *(IPD(I,J)+J=1,5)           DATP1410
74   IF(HISTIN(1,J),LT,0.0) GO TO 11                               DATP1420
15   GO TO 10                                              DATP1430
76   551 FORMAT (7F10.0, 512)                                     DATP1440
77   11 CONTINUE                                              DATP1450
78   NNMIST = J-1                                             DATP1460
79   MM = MM + 1                                              DATP1470
80   TO TODAYS                                              DATP1480
81   IF(CRMG,GT,-1) GO TO 521                                 DATP1490
82   521 CONTINUE                                              DATP1500
83   IF(ICREF,LE,0) GO TO 140                                 DATP1510
C
C   CONTROL SIGNAL.....INPUT GROUP NO. 4                         DATP1520
84   READ(S,2110)  (CLCRP(I,J),I=1,2),J=1,ICREP                DATP1530
85   NCRICKEP
86   140 CONTINUE                                              DATP1540
C
C   IF(KUNIT,LE,1) GO TO 150                                 DATP1550
88   DFSUM = DFS * 2.54                                         DATP1560
89   DSINZD = DSINZ * 2.54                                     DATP1570
90   DVOIDZD = DVOIDZ * 2.54                                     DATP1580
91   DCIDUM = DCI * 2.54                                       DATP1590
92   ECODUM = ECO * 2.54                                       DATP1600
93   FUELL = LFUEL * 2.54                                     DATP1610
94   VCDIZL = VCDIZ * 2.54                                     DATP1620
95   VPLEND = VPLENZ * 2.54*3                                DATP1630
96   SINTEM = (SINTEM - 32.0) / 1.8                           DATP1640
97   DTEMPD = DTEMP / 1.8                                     DATP1650
98   DECUM = DE * 2.54                                         DATP1660
99   VDUM = V * 0.3048                                         DATP1670
100  EXPFD = EXPX / 14.22                                     DATP1680
101  ROUDF = ROUF * 2.54                                     DATP1690
102  ROUCD = ROUC * 2.54                                     DATP1700
103  RDTSHD = RDTSH * 2.54                                     DATP1710

```

* SOURCE STATEMENT (DATINP) *

```

104   HDISHD = HDISH * 2.54                                     DATP1720
105   GO TO 160                                              DATP1730
106   160 CONTINUE                                              DATP1740
107   DFSUM = DFS                                           DATP1750
108   DSINZD = DSINZ                                         DATP1760
109   DVOIDZD = DVOIDZ                                         DATP1770
110   DCIDUM = DCI                                           DATP1780
111   ECODUM = ECO                                           DATP1790
112   FUELL = LFUEL                                         DATP1800
113   VCDIZL = VCDIZ                                         DATP1810
114   VPLEND = VPLENZ                                         DATP1820
115   SINTEM = SINTEM                                         DATP1830
116   DECUM = DE                                           DATP1840
117   VDUM = V                                           DATP1850
118   EXPFD = EXPX                                         DATP1860
119   ROUDF = ROUF                                         DATP1870
120   ROUCD = ROUC                                         DATP1880
121   DTEMPD = DTEMP                                         DATP1890
122   160 CONTINUE                                              DATP1900
123   PVGUM(1,2) = DFSUM                                     DATP1910
124   SIGMF0 = SIGMF                                         DATP1920
125   DDTSHD = DDTSH                                         DATP1930
126   HDISHD = HDISH                                         DATP1940
127   IF(SIGMF,LE,0) GO TO 170                               DATP1950
128   IF(KUNIT,LE,1) SIGNED = SIGMF                         DATP1960
129   IF(KUNIT,NE,1) SIGMF0 = SIGMF / 1763.                  DATP1970
130   170 CONTINUE                                              DATP1980
C
C   CLADDING CREEF DOWN (DAY VS. CLADDING DIAMETRAL CHANGE) DATP1990
C
C   IF(ICREF,LE,0) GO TO 350                               DATP2000
132   IF(KUNIT,LE,1) GO TO 350                               DATP2010
133   DO 320 J=1,ICREP                                     DATP2020
134   CLCRPD(1,J) = CLCRP(1,J)                            DATP2030
135   CLCRPD(2,J) = CLCRP(2,J) * 2.54                      DATP2040
136   320 CONTINUE                                              DATP2050
137   GO TO 350                                              DATP2060
138   330 DO 340 J=1,ICREP                                     DATP2070
139   CLCRPD(1,J) = CLCRP(1,J)                            DATP2080
140   CLCRPD(2,J) = CLCRP(2,J)                            DATP2090
141   340 CONTINUE                                              DATP2100
142   350 CONTINUE                                              DATP2110
C
C   HISTORY CONVENTION                                         DATP2120
C
C   IF(KUNIT,LE,1) GO TO 370                               DATP2130
144   DO 360 J=1,NNMIST                                     DATP2140
145   HIST(1,J) = HISTIN(1,J)                             DATP2150
146   HIST(2,J) = HISTIN(2,J) * 1000, / 30.48             DATP2160
147   HIST(3,J) = (HISTIN(3,J) - 32.0) / 1.8              DATP2170
148   HIST(4,J) = HISTIN(4,J) / 14.22                     DATP2180
149   HIST(5,J) = HISTIN(5,J)                             DATP2190
150   HIST(6,J) = HISTIN(6,J)                             DATP2200
151   HIST(7,J) = HISTIN(7,J)                             DATP2210
152   360 CONTINUE                                              DATP2220
153   GO TO 390                                              DATP2230
154   370 DO 380 J=1,NNMIST                               DATP2240
155   HIST(1,J) = HISTIN(1,J)                            DATP2250
156
```

* SOURCE STATEMENT (CONTINP) *

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157   380 CONTINUE DATP2370
158   390 CONTINUE DATP2380
159   CALL CHECK(1) DATP2390
160   RETURN DATP2400
161 C ----- DATP2410
162   2000 CONTINUE DATP2420
163   C MODE(1+I1H)=3 SWITCHING SIGN OF PRINT CONTROL DATP2430
164   IF(I1H.LE.1) GO TO 222 DATP2440
165   IF(MODE(1+I1H),EQ.0) MODE(1+I1H)=MODE(1,I1H-1) DATP2450
166   IF(MODE(1+I1H),EQ.3) MODE(1+I1H) = 0 DATP2460
167   C 222 CONTINUE DATP2470
168   C 1IPROF = MODE(1+I1H) DATP2480
169   NEWK = 0 DATP2490
170   IF(MODE(2+I1H),EQ.0) GO TO 230 DATP2500
171   NEWK = 1 DATP2510
172   NCON = MODE(2+I1H) DATP2520
173   IF(NCON,LE.0) GO TO 230 DATP2530
174   C CONTROL SIGNAL.....INPUT GROUP NO. 5 DATP2540
175   DO 220 J=1,NCON DATP2550
176   CFDM(1,J) = CF1(J) DATP2560
177   CFDM(2,J) = CF2(J) DATP2570
178   CFDM(3,J) = CF3(J) DATP2580
179   220 CONTINUE DATP2590
180   230 CONTINUE DATP2600
181   C READ(5,INPUT2) DATP2610
182   CLADDING PROPERTIES READ AND CONVERSION DATP2620
183   NEWCL = 0 DATP2630
184   IF(MODE(3+I1H),EQ.0) GO TO 270 DATP2640
185   NEWCL = 1 DATP2650
186   NCLAD = MODE(3+I1H) DATP2660
187   IF(NCLAD,LE.0) GO TO 270 DATP2670
188   C CONTROL SIGNAL.....INPUT GROUP NO. 6 DATP2680
189   DO 240 J=1,NCLAD DATP2690
190   AAJUM(1,J) = (AA1(J) - 32.0) / 1.0 DATP2700
191   AAJUM(2,J) = AA2(J) * 0.0173 DATP2710
192   AAJUM(3,J) = AA3(J) / 14.22 DATP2720
193   AAJUM(4,J) = AA4(J) / 14.22 DATP2730
194   AAJUM(5,J) = AA5(J) DATP2740
195   AAJUM(6,J) = AA6(J) * 1.8 DATP2750
196   AAJUM(7,J) = AA7(J) DATP2760
197   240 CONTINUE DATP2770
198   GO TO 270 DATP2780
199   250 CONTINUE DATP2790
200   AAJUM(1,J) = AA1(J) DATP2800
201   AAJUM(2,J) = AA2(J) DATP2810
202   AAJUM(3,J) = AA3(J) DATP2820
203   AAJUM(4,J) = AA4(J) DATP2830
204   270 CONTINUE DATP2840
205   C FLUX DEPRESSION CONVERSION DATP2850
206   NEWFLX = 0 DATP2860
207   IF(MODE(4+I1H)) 2010,2030,2020 DATP2870
208   2010 CALL DEPRES(DENSIT,FR35,FR38,DFSDUM,RVDDUM) DATP2880
209   NF = 11 DATP2890
210   GO TO 2030 DATP2900
211   2020 CONTINUE DATP2910
212   NEWFLX = 1 DATP2920
213   NFLX = NF * MODE(4+I1H) DATP2930
214   C CONTROL SIGNAL.....INPUT GROUP NO. 7 DATP2940
215   IF(KUNIT,EQ.1) GO TO 290 DATP2950
216   DO 280 J=1,NF DATP2960
217   RVDDUM(1,J) = RV1(J) * 2.54 DATP2970
218   RVDDUM(2,J) = RV2(J) DATP2980
219   280 CONTINUE DATP2990
220   GO TO 310 DATP3000
221   290 DO 300 J=1,NF DATP3010
222   RVDDUM(1,J) = RV1(J) DATP3020
223   RVDDUM(2,J) = RV2(J) DATP3030
224   300 CONTINUE DATP3040
225   310 CONTINUE DATP3050
226   2030 CONTINUE DATP3060
227   C AXIAL POWER DISTRIBUTION READ DATP3070
228   IF(MODE(5+I1H),EQ.0) GO TO 2050 DATP3080
229   DO 100 I=1,NPOW1 DATP3090
230   100 POWREF(I) = POWER(I) DATP3100
231   2050 CONTINUE DATP3110
232   CALL CHECK(2) DATP3120
233   RETURN DATP3130
234   3000 CONTINUE DATP3140
235   4000 CONTINUE DATP3150
236   RETURN DATP3160
237   C * 1 * 2 * 3 * 4 * 5 * 6 * 7 DATP3170
238   1520 FORMAT(20A*) DATP3180
239   2110 FORMAT(F10.0,E10.0) DATP3190
240   END DATP3200

```

* SOURCE STATEMENT (CONTINP) *

```

200   AAJUM(4,J) = AA4(J) DATP3210
201   AAJUM(5,J) = AA5(J) DATP3220
202   AAJUM(6,J) = AA6(J) DATP3230
203   AAJUM(7,J) = AA7(J) DATP3240
204   270 CONTINUE DATP3250
205   C FLUX DEPRESSION CONVERSION DATP3260
206   NEWFLX = 0 DATP3270
207   IF(MODE(4+I1H)) 2010,2030,2020 DATP3280
208   2010 CALL DEPRES(DENSIT,FR35,FR38,DFSDUM,RVDDUM) DATP3290
209   NF = 11 DATP3300
210   GO TO 2030 DATP3310
211   2020 CONTINUE DATP3320
212   NEWFLX = 1 DATP3330
213   NFLX = NF * MODE(4+I1H) DATP3340
214   C CONTROL SIGNAL.....INPUT GROUP NO. 7 DATP3350
215   IF(KUNIT,EQ.1) GO TO 290 DATP3360
216   DO 280 J=1,NF DATP3370
217   RVDDUM(1,J) = RV1(J) * 2.54 DATP3380
218   RVDDUM(2,J) = RV2(J) DATP3390
219   280 CONTINUE DATP3400
220   GO TO 310 DATP3410
221   290 DO 300 J=1,NF DATP3420
222   RVDDUM(1,J) = RV1(J) DATP3430
223   RVDDUM(2,J) = RV2(J) DATP3440
224   300 CONTINUE DATP3450
225   310 CONTINUE DATP3460
226   2030 CONTINUE DATP3470
227   C AXIAL POWER DISTRIBUTION READ DATP3480
228   IF(MODE(5+I1H),EQ.0) GO TO 2050 DATP3490
229   DO 100 I=1,NPOW1 DATP3500
230   100 POWREF(I) = POWER(I) DATP3510
231   2050 CONTINUE DATP3520
232   CALL CHECK(2) DATP3530
233   RETURN DATP3540
234   3000 CONTINUE DATP3550
235   4000 CONTINUE DATP3560
236   RETURN DATP3570
237   C * 1 * 2 * 3 * 4 * 5 * 6 * 7 DATP3580
238   1520 FORMAT(20A*) DATP3590
239   2110 FORMAT(F10.0,E10.0) DATP3600
240   END DATP3610

```

* SOURCE STATEMENT *

```

1      SUBROUTINE DENSF(DEN,BURN,TSIN,RFS,DELDEN,MDEN,DFS)          DENSO010
C      THIS SUBROUTINE IS CALLED FROM MAIN                               DENSO020
C      ****SUBROUTINE DENSF****                                         DENSO030
C      FUEL DENSIFICATION MODEL                                         DENSO040
2      COMMON /COM 20/ RHO,RHOS,FRUU,FRPUPU                         DENSO050
3      COMMON /STDEN/ ANS,DENS                                         DENSO060
C      DEN ..... INITIAL FUEL FRACTIONAL DENSITY                   DENSO070
C      BURN ..... BURNUP (MM/MTU)                                     DENSO080
C      TSIN ..... INITIAL SINTERED TEMPERATURE (DEG C)             DENSO090
C      RFS ..... INITIAL FUEL RADIUS (CM)                            DENSO100
C      DELDEN .. RADIUS CHANGE DUE TO DENSIFICATION (CM)           DENSO110
C      MDEN
C          = 0  DENSIFICATION IS NOT TAKEN INTO ACCOUNT.            DENSO120
C          = 1  HALDEN MODEL                                         DENSO130
C          = 2  GAPCON THERMAL=2 MODEL                                DENSO140
C      ****END OF SUBROUTINE DENSF****                                 DENSO150
C
4      GO TO (1,2,3,4) + MDEN                                         DENSO160
5      1  CONTINUE
C----- HALDEN
6      PU=BURN/1000.                                                 DENSO170
7      TU=DEN*100.                                                   DENSO180
8      TS=TSIN
9      CALL DENSHT(TD,BU,TS,ANS)                                     DENSO190
10     ANS=ANS/100.
11     DELDEN=-1.*RFS*ANS
12     RETURN
13     2  CONTINUE
C----- GAPCON THERMAL=2
14     BU=BURN
15     CALL DENSGT(DELPI,DFS,RHO,RHOS,BU,ANS)                      DENSO200
16     DELDEN=DELPI
17     3  CONTINUE
18     4  CONTINUE
19     RETURN
20     END

```

* SOURCE STATEMENT *

```

1      SUBROUTINE DENSGT(DELPI,DFS,ROW,ROWS,BN,ANS)                  DENGU010
C      DELRH0=HALOG(BU)*R                                         DENGU020
C      ALUG5=1.6094                                                 DENGU030
C      ALUG6=2.996                                                 DENGU040
C      ALUG5000=7.601                                               DENGU050
2      ANS=0.0
3      DELPI=0.
4      BU=BN
5      IF(BU.LE.20) GO TO 30
6      IF(ROWS.LE.ROW) GO TO 30
7      DATA ROWS/ROW
8      IF(BU.GT.2000)  B=J=2000
9      IF(ROW.GT.10,00) GO TO 10
10     DELRH0=1.0+ALUG(BU/5.)*#0R
11     GO TO 20
12     10  DELRH0=0.2171*DR*ALUG(BU/20.)
13     20  DELPI=-DELH*DFS/4./ROW
14     ANS=DELRH/2./ROW
15     30  RETURN
16     END

```

* SOURCE STATEMENT *

```

1      SUBROUTINE DENSHT(TD,BU,TS,FT)                                DNSHU010
C      THIS SUBROUTINE IS CALLED FROM DENSF                           DNSHU020
C
2      DATA A,C1,C2,C3,C4/22.22+0.9337+0.96085+2.06627+35.63738 /
C      DATA A,C1,C2,C3,C4/22.2+0.93 -1.0   +2.07  -35.           /
C
3      DM=A*(100.-TD)/(TS-1140.)
4      BU=BU*U
5      DR=0.1
6      IT=0
7      DM=C1*EXP(C2*BU1)+C3*EXP(C4*BU1)
8      IF (ABS(DM-DM1)/DM > 1.E-4) 50,50,20
9      20  IF (DM-DM1) 40,50,30
10     30  HU1=BU1-DRU
11     DRU=DRU/10.
12     40  BU1=BU1+DRU
13     IT=IT+1
14     IF (IT.GE.50) GO TO 55
15     GO TO 15
16     55  WRITE(6, 400) DM,DM1,BU1+DRU
17     50  DRU=BU1
18     BU1=BU
19     60  FT =C1*EXP(C2*(BU1+DRU))+C3*EXP(C4*(BU1+DRU))
20     FT=DM1+FT
21     400 FORMAT(5X,47ITERATION TIME OVER  DM,DM1,BU1,DRU,TD,TS =
22     1      ,6F10.5 / )
22     RETURN
23     END

```

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* SOURCE STATEMENT *

```
1      SUBROUTINE DEPRES(DENSIT,FRI0,FRI1,DFS,RV)          DEPR0010
C      THIS SUBROUTINE IS CALLED FROM STEP 1                 DEPR0020
C      REFER BNWL-1778, GAPCON THERMAL-1,A-2, AND GRAPH D-916, D-917   DEPR0030
C
2      DIMENSION RV(2,20)                                     DEPR0040
3      DATA SIGA5,SIGA6,SIGA7,SIGT5,SIGT6,SIGT0/578.,2.33+0.,586.5+0.8,    DEPR0050
14.2 /
4      EN5=DENSIT*FR10*.00225927                           DEPR0060
5      EN8=DENSIT*FR11*.00223079                           DEPR0070
6      EN0=(EN5*EN8)*2.                                      DEPR0080
7      SGA=(EN5*SIGA5+EN8*SIGA8+EN0*SIGA0)                  DEPR0090
8      SGT=(EN5*SIGT5+EN8*SIGT8+EN0*SIGT0)                  DEPR0100
9      CAPS=3.*SGA*SGT/(1.-R*SGA/SGT)                      DEPR0110
10     CAPPA=SQRT(CAPS0)                                    DEPR0120
11     RV(1,1)=0.                                         DEPR0130
12     RV(2,1)=1.                                         DEPR0140
13     DO 10 I=2,11                                       DEPR0150
14     10 RV(1,I)=RV(1,I-1)+DFS/I0,                         DEPR0160
15     DO 20 I=2,11                                       DEPR0170
16     20 R=RV(1,I)/4.*CAPPA                            DEPR0180
17     20 RV(2,I)=1.+R**2.+R**4./4.+R**6./36.+R**8./576.   DEPR0190
18     RETURN                                              DEPR0200
19     ****DEPR0210
20     END                                                 DEPR0220
21     ****DEPR0230
22     ****DEPR0240
23     ****DEPR0250
```

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* SOURCE STATEMENT *

```
1      SUBROUTINE ERROR(IN3,IN4,VALUE)                      ERRO0010
C      THIS SUBROUTINE IS CALLED FROM TERP                  ERRO0020
C
2      DIMENSION ERR(3,150)                                 ERRO0030
C
3      DATA IE/0/                                         ERRO0040
4      IF(IN4,EQ,45,OR,IN4,EQ,52,OR,IN4,EQ,53,OR,IN4,EQ,54,OR,IN4,EQ,55   ERRO0050
* ,OR,IN4,EQ,81,OR,IN4,EQ,82,OR,IN4,EQ,43) RETURN        ERRO0060
5      IE=IE+1                                           ERRO0070
6      ERR(1,IE)=FLOAT(IN3)                                ERRO0080
7      ERR(2,IE)=FLOAT(IN4)                                ERRO0090
8      ERR(3,IE)=VALUE                                    ERRO0100
C
9      IF(IE,LT,150) RETURN                               ERRO0110
10     WRITE(6,100)                                     ERRO0120
11     DO 10 I=1,150+10                                ERRO0130
12     I1=I
13     I2=I1+9
14     WRITE(6,201) (ERR(1,II),II=I1,I2)                ERRO0140
15     WRITE(6,202) (ERR(2,II),II=I1,I2)                ERRO0150
16     WRITE(6,203) (ERR(3,II),II=I1,I2)                ERRO0160
17     WRITE(6,300)
18     10 CONTINUE                                         ERRO0170
19     IE=0                                               ERRO0180
20     100 FORMAT(1H1,20X,43HINTERPOLATION FUNCTION (TERP) ERROR SUMMARY //) ERRO0190
21     201 FORMAT(3X,5H IN3,3X,10F12.0)                  ERRO0200
22     202 FORMAT(3X,5H IN4,3X,10F12.0)                  ERRO0210
23     203 FORMAT(3X,5H VALUE,3X,10G12.5)                ERRO0220
24     300 FORMAT(1H )
25     RETURN                                              ERRO0230
26     END                                                 ERRO0240
27     ****ERRO0250
28     ****ERRO0260
29     ****ERRO0270
30     ****ERRO0280
31     ****ERRO0290
32     ****ERRO0300
33     ****ERRO0310
34     ****ERRO0320
35     ****ERRO0330
```

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* SOURCE STATEMENT *

```

1      SUBROUTINE EXPAND (RFS,RD,TT,TFS,FRF002,DELRT,DELCT,DELL,L,NEXP, EXPAU010
1          MEXP + RVOID ) EXPAU020
C THIS SUBROUTINE IS CALLED FROM STEP 5 EXPAU030
C REFER BNWL-1778,GAPCON THERMAL-1,A-5, AND GRAPH D-612. EXPAU040
C EXPAU050
C EXPAU060
C EXPAU070
C EXPAU080
C EXPAU090
C EXPAU100
C EXPAU110
C EXPAU120
C EXPAU130
C EXPAU140
C EXPAU150
C EXPAU160
C EXPAU170
C EXPAU180
C EXPAU190
C EXPAU200
C EXPAU210
C EXPAU220
C EXPAU230
C EXPAU240
C EXPAU250
C EXPAU260
C EXPAU270
C EXPAU280
C EXPAU290
C EXPAU300
C EXPAU310
C EXPAU320
C EXPAU330
C EXPAU340
C EXPAU350
C EXPAU360
C EXPAU370
C EXPAU380
C EXPAU390
C EXPAU400
C EXPAU410
C EXPAU420
C EXPAU430
C EXPAU440
C EXPAU450
C EXPAU460
C EXPAU470
C EXPAU480
C EXPAU490
C EXPAU500
C EXPAU510
C EXPAU520
C EXPAU530
C EXPAU540
C EXPAU550
C EXPAU560
C EXPAU570
C EXPAU580
C EXPAU590

```

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* SOURCE STATEMENT (EXPAND) **

```

47      DO 13 I=1,L EXPAU600
48      13 DELRT = DELRT + DELL(I)
49      DELRT = DELRT-DELL(L)/2.+DELCT(L) EXPAU610
50      RETURN EXPAU620
51      20 CONTINUE EXPAU630
C----- AREA BALANCE TYPE EXPAU640
52      DO 21 I=1,MESH EXPAU650
53      DELRT=DELRT+DAREA(I) EXPAU660
54      21 CONTINUE EXPAU670
55      DELRT=DELRT +DAREAV EXPAU680
56      RETURN EXPAU690
57      30 CONTINUE EXPAU700
C----- HALF CRACK (TWO REGION TYPE) EXPAU710
58      DO 31 I=1,INDX EXPAU720
59      DELRT=DELRT+DELL(I) EXPAU730
60      31 CONTINUE EXPAU740
C
61      INDX1=INDX+1 EXPAU750
62      IF (INDX1.GE.MESH) GO TO 33 EXPAU760
63      DO 32 I=INDX1,MESH EXPAU770
64      DELRT=DELRT+DAREA(I) EXPAU780
65      32 CONTINUE EXPAU790
66      33 CONTINUE EXPAU800
67      DELRT=DELRT +DAREAV EXPAU810
C
68      RETURN EXPAU820
69      40 CONTINUE EXPAU830
C **** COMPLETE CRACK MODEL EXPAU840
70      DO 35 I=1,MESH EXPAU850
71      DELRT=DELRT+DELL(I) EXPAU860
72      35 CONTINUE EXPAU870
73      DELRT=DELRT + DELV01 EXPAU880
74      RETURN EXPAU890
75      50 CONTINUE EXPAU900
76      RETURN EXPAU910
C***** EXPAU920
77      END EXPAU930
                                         EXPAU940
                                         EXPAU950
                                         EXPAU960

```

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* SOURCE STATEMENT *

```

1      FUNCTION FALPHA(T,KEXP)                               FALP0010
C
C      THIS FUNCTION IS CALLED FROM EXPAND.                  FALP0020
C
C----- FUEL LINEAR THERMAL EXPANSION COEFFICIENT ----- FALP0030
C      IN THIS FUNCTION , THE FALPHA IS AVERAGE ALPHA ( (DL/L)/DT) FALP0040
C      AND IS NOT INSTANTENOUS ALPHA ( D(DL/L)/DT ) .          FALP0050
C      NOW REFERENCE(ROOM) TEMPERATURE IS TR SETTED TO 25. DEG C FALP0060
C      THE AVERAGE ALPHA IS DEFINED BY THE NEXT EQUATION       FALP0070
C          AVG.ALPHA = ( F(T)-F(TREF) ) / ( T-TREF )           FALP0080
C          F(T) = DL/L0 AT T (DEG C)                          FALP0090
C
C      THE DEFORMATION DUE TO THERMAL EXPANSION IS CALCULATED BY FALP0100
C      NEXT EQUATION IN SUBROUTINE (EXPAND)                   FALP0110
C
C          DELR(I) = ALPHA * (T(I)-TR) * R(I)                 FALP0120
C          T(I)=LOCAL TEMPERATURE   R(I)=RING AVERAGE RADIUS FALP0130
C          I=RING POINT NUMBER                                FALP0140
C
C      .... PARAMETERS ....                                FALP0150
C          T=LOCAL TEMPERATURE IN DEG C                      FALP0160
C          OPTION                                         FALP0170
C              KEXP = 1  ROTH AND HALTEMAN (GAPCON HEDL-TM72-128) FALP0180
C                         (PURE UO2)                           FALP0190
C              = 2  CONWAY,FANCEL AND HEIN (BNWL-1778 GAPCON-THERMAFALP0200
C
C          AVERAGE LINEAR THERMAL EXPANSION COEFFICIENT TABLE ( X 1.E-6) FALP0210
C
C----- EMP(C)  GAPCON    GAPCON-THERM                         FALP0220
C----- (25,/)  (ROTH - ) (CONWAY- )                         FALP0230
C----- ..... ..... ..... ..... ..... ..... ..... ..... ..... FALP0240
C----- 100,    9.52500   7.15900                         FALP0250
C----- 300,    9.44500   7.73820                         FALP0260
C----- 500,    9.76500   8.31740                         FALP0270
C----- 800,    9.94500   9.18620                         FALP0280
C----- 1000,   10.06500   9.76540                         FALP0290
C----- 1500,   10.36500  11.21340                         FALP0300
C----- 2000,   10.66500  12.56140                         FALP0310
C----- 2500,   10.96500  14.10940                         FALP0320
C----- ..... ..... ..... ..... ..... ..... ..... ..... ..... FALP0330
C----- (500,/)  ..... ..... ..... ..... ..... ..... ..... ..... FALP0340
C----- 800,    10.23000  10.56180                         FALP0350
C----- 1000,   10.35000  11.14100                         FALP0360
C----- 1500,   10.65000  12.58900                         FALP0370
C----- 2000,   10.95000  14.03100                         FALP0380
C----- 2500,   11.25000  15.48500                         FALP0390
C----- 2800,   11.43900  16.35380                         FALP0400
C----- ..... ..... ..... ..... ..... ..... ..... ..... ..... FALP0410
C----- ..... ..... ..... ..... ..... ..... ..... ..... ..... ..... FALP0420
C----- ..... ..... ..... ..... ..... ..... ..... ..... ..... ..... FALP0430
C----- ..... ..... ..... ..... ..... ..... ..... ..... ..... ..... FALP0440
C----- ..... ..... ..... ..... ..... ..... ..... ..... ..... ..... FALP0450
C----- ..... ..... ..... ..... ..... ..... ..... ..... ..... ..... FALP0460
C----- ..... ..... ..... ..... ..... ..... ..... ..... ..... ..... FALP0470
C----- ..... ..... ..... ..... ..... ..... ..... ..... ..... ..... FALP0480
C----- ..... ..... ..... ..... ..... ..... ..... ..... ..... ..... FALP0490
C----- ..... ..... ..... ..... ..... ..... ..... ..... ..... ..... FALP0500
C----- ..... ..... ..... ..... ..... ..... ..... ..... ..... ..... FALP0510
C----- ..... ..... ..... ..... ..... ..... ..... ..... ..... ..... FALP0520
C----- ..... ..... ..... ..... ..... ..... ..... ..... ..... ..... FALP0530
C----- ..... ..... ..... ..... ..... ..... ..... ..... ..... ..... FALP0540
C----- ..... ..... ..... ..... ..... ..... ..... ..... ..... ..... FALP0550
C----- ..... ..... ..... ..... ..... ..... ..... ..... ..... ..... FALP0560
C----- ..... ..... ..... ..... ..... ..... ..... ..... ..... ..... FALP0570
C----- ..... ..... ..... ..... ..... ..... ..... ..... ..... ..... FALP0580
C----- ..... ..... ..... ..... ..... ..... ..... ..... ..... ..... FALP0590
2      DATA TR/24.999999/                                FALP0600
3      IC=T                                              FALP0610
4      IF=TC*1.5+32.                                     FALP0620
5      TRF=TR*1.8-32.                                     FALP0630
6      IF(KEXP.GT.0) GO TO 100                            FALP0640
7      PRINT 500+KEXP                                     FALP0650
8      STOP                                             FALP0660

```

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* SOURCE STATEMENT (FALPHA) *

```

9      500 FORMAT(1H0,47***** FUEL THERMAL EXPANSION OPTION ERROR KEXP=,12) FALP0600
10     100 CONTINUE                                         FALP0610
11     GO TO (1,2,3,4,5,6) , KEXP                         FALP0620
C----- ROTH AND HALTEMAN                                FALP0630
12     1 CONTINUE                                         FALP0640
13     FALPHA=( (TC**2-TR**2)*0.0006 + (TC-TR)*9.45 )*1.E-6 / (TC-TR) FALP0650
14     GO TO 10                                           FALP0660
C----- GAPCON-THERMAL-1                                 FALP0670
15     2 CONTINUE                                         FALP0680
16     FALPHA=( (TC**2-TR**2)*2.89E-9 + (TC-TR)*6.747E-6 ) / (TC-TR) FALP0690
17     GO TO 10                                           FALP0700
18     3 CONTINUE                                         FALP0710
19     GO TO 10                                           FALP0720
20     4 CONTINUE                                         FALP0730
21     GO TO 10                                           FALP0740
C----- ..... ..... ..... ..... ..... ..... ..... ..... ..... FALP0750
22     5 CONTINUE                                         FALP0760
23     6 CONTINUE                                         FALP0770
24     10 CONTINUE                                         FALP0780
25     RETURN                                            FALP0790
26     END                                               FALP0800

```

* SOURCE STATEMENT *

```

1      FUNCTION FCOND(DENS,TEMP,KCON)          FCON0010
C
C      THIS SUBROUTINE IS CALLED FROM STEP 2 STEP 4 AND STEP 7          FCON0020
C
C-----          FCON0030
C-----          FCON0040
C-----          FCON0050
C-----          FCON0060
C-----          FCON0070
C-----          FCON0080
C-----          FCON0090
C-----          FCON0100
C-----          FCON0110
C-----          FCON0120
C-----          FCON0130
C-----          FCON0140
C-----          FCON0150
C-----          FCON0160
C-----          FCON0170
C-----          FCON0180
C-----          FCON0190
C-----          FCON0200
C-----          FCON0210
C-----          FCON0220
C-----          FCON0230
C-----          FCON0240
C-----          FCON0250
C-----          FCON0260
C-----          FCON0270
C-----          FCON0280
C-----          FCON0290
C-----          FCON0300
C-----          FCON0310
C-----          FCON0320
C-----          FCON0330
C-----          FCON0340
C-----          FCON0350
C-----          FCON0360
C-----          FCON0370
C-----          FCON0380
C-----          FCON0390
C-----          FCON0400
C-----          FCON0410
C-----          FCON0420
C-----          FCON0430
C-----          FCON0440
C-----          FCON0450
C-----          FCON0460
C-----          FCON0470
C-----          FCON0480
C-----          FCON0490
C-----          FCON0500
C-----          FCON0510
C-----          FCON0520
C-----          FCON0530
C
2      D = DENS
3      T = TEMP
4      IF(KCON.GT.0) GO TO 100
5      WRITE(6,1000)
6      FCOND = 0.0
7      RETURN
8      100  CONTINUE
9      GO TO (1,2,3,4,5)          ) * KCON
C      ***** WARD DESIGN EQUATION (DENS.LT.0.95) *****
10     1  FCOND=(1.-2.1*D*D**2)*(-1./(.288*.00252*T)-5.83E-12*T**3)          FCON0280
11     GO TO 50
12     2  FCOND=(3.*D-1.)*(1./(.575+.0503*T)+2.91E-13*T**3)          FCON0310
13     GO TO 50
14     3  FCOND=(1.-2.5*(1.-D))*(45.1/(135.+T) + 4.79E-13*T**3)          FCON0340
15     GO TO 50
C      ***** LYONS EQUATION *****
C      NOW CONVERT TEMPERATURE DEG=C TO DEG-K IN ORIGINAL EQUATION          FCON0370
C
16     4  FCOND=((1.025/.95)*(D/(1.+(1.-D)*.5)))*((38.24/(129.4+T))+(6.1256E          FCON0400
A-13*((T)**3)))          FCON0410
17     GO TO 50
C      ***** RESAR-41 MODEL *****
C
18     5  FCOND=((1.025/.95)*(D/(1.+(1.-D)*.5)))*((1./(11.8+0.0238*(T-273.))          FCON0450
A)+(8.775E-13*((T-273.)*3)))          FCON0460
19     GO TO 50
20     50  CONTINUE
21     RETURN
C
22 1000  FORMAT(1HD, 40H***** THERMAL CONDUCTIVITY OPTION ERROR )          FCON0510
C*****          FCON0520
23  END          FCON0530

```

* SOURCE STATEMENT *

```

1      SUBROUTINE FISGAS(TIN,PHH,P,CONEN,[FLUX,MTIME,AKR,AXE,[P])      FISG0010
C
C      THIS SUBROUTINE IS CALLED FROM MOLMOL(2)                      FISG0020
C
C
C      SUBROUTINE FISGAS IS USED TO CALCULATE THE AMOUNT                FISG0030
C      OF FISSION GAS PRODUCED FOR A GIVEN TIME AND POWER.               FISG0040
C      CALCULATIONS ARE BASED ON TWO MODELS. THE FIRST ASSUMES          FISG0050
C      A PRIMARILY FAST SPECTRUM, AND THE SECOND ASSUMES A              FISG0060
C      THERMAL SPECTRUM.                                              FISG0070
C
C      COMMON /NUCLEI/ NUCLEI,A(40,23)                                     FISG0080
C      COMMON /BRNRAY/ VOLCC,A12,A12,A12,A9Z,A10Z                         FISG0090
C      COMMON /DECAY/ DC2,DC3,DC4,DC5,DC6,DC12,DC14,DC15,DC21,DC22,DC23, FISG0100
C      * DC29,DC26+DC28,DC31,DC33+DC34,DC35,DC45,DC65M                   FISG0110
C      DIMENSION TCX(30),FCX(30),TFX(30),FFX(30),CX(30),FX(30),AX(30), FISG0120
C      *FY(4,20),TY(4,20)                                                 FISG0130
C      DIMENSION Y(20,20),F(20)                                           FISG0140
C      DOUBLE PRECISION X1,X2,X3,X4,X5,X6,X7,X8,X9,X10,X11,X12,X13,X14, FISG0150
C      *X15,X101,X102,X103,X104,X105,X107,X108,X109,X110,X111,X112,X113, FISG0160
C      *X114,X116,X117,X118                                             FISG0170
C      DOUBLE PRECISION AXT                                           FISG0180
C
C      DATA A/ 920*0.0/                                              FISG0190
C      DATA FX/30 + 0.0/                                              FISG0200
C      DATA KKK / 0 /                                              FISG0210
C      DATA DC2,DC3,DC4,DC5,DC6,DC12,DC14,DC15/4.915E-04,3.413E-06,1.365E-06,1.365E-06/ FISG0220
C      *-5.1562E-03,1.925E-04,1.198E-06,3.420E-06,2.469E-10/ FISG0230
C
C      DATA DC55M,DC8,DC21,DC22,DC23,DC26,DC28,DC31,DC33,DC34,DC35,DC25/ FISG0240
C      *4.3735E-05,2.042E-09,6.684E-06,4.620E-04,9.964E-07,9.167E-06,2.873E-06,2.873E-06/ FISG0250
C      *-5.8.370E-05,1.522E-06,7.219E-04,2.092E-05,2.468E-06/ FISG0260
C
C      DATA TCX,TFX,FCX,FFX                                         FISG0270
C
C      1     2.7   0.0   14.0   0.1   FISG0280
C      2     36.0   14.0   0.0   0.0   FISG0290
C      3     60.0   0.0   0.0   0.0   FISG0300
C      4     0.0   0.0   0.0   0.0   FISG0310
C      5     0.0   0.0   0.0   0.0   FISG0320
C      6     0.0   0.0   0.0   0.0   FISG0330
C      7     1110.0   740.0   1.6   1.6   FISG0340
C      8     290.0   90.0   1.6   1.6   FISG0350
C      9     1350.0   950.0   1.6   1.6   FISG0360
C      10    693.0   553.0   6.6   1.4   FISG0370
C      11    0.0   0.0   0.3   0.0   FISG0380
C      12    0.0   0.0   0.0   0.0   FISG0390
C      13    170.0   0.0   13.0   1.5   FISG0400
C      14    1600.0   0.0   0.0   0.0   FISG0410
C      15    597.0   17.0   2.0   2.0   FISG0420
C      16    0.0   0.0   0.0   0.0   FISG0430
C      17    0.0   0.0   0.0   0.0   FISG0440
C      18    0.0   0.0   0.0   0.0   FISG0450
C      19    0.0   0.0   0.0   0.0   FISG0460
C      20    150.0   0.0   0.0   0.0   FISG0470

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* SOURCE STATEMENT (FISGAG) *

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C 21    15.0   0.0   0.0   0.0   FISG0480
C 22    65.0   0.0   0.0   0.0   FISG0490
C 23    5.0   0.0   0.0   0.0   FISG0500
C 24    190.0   0.0   0.0   0.0   FISG0510
C 25    27.0E-01 0.0   0.0   0.0   FISG0520
C
C TABLE FOR DECAY CONSTANT OF THE HEAVY METAL ATOMS                 FISG0530
C N   UC   HALF LIFE   DECAY CONSTANT                                FISG0540
C
C 1     2     23.5 D   4.915E-4   FISG0550
C 2     2     2.35 D   3.413E-5   FISG0560
C 3     3     2.35 D   3.413E-5   FISG0570
C 4     4     14.1 D   1.365E-5   FISG0580
C 5     5     7.3 D   1.582E-3   FISG0590
C 6     6     1.0 D   1.925E-4   FISG0600
C
C 7
C 8
C 9
C 10
C 11
C 12    12     6.75 D   1.188E-6   FISG0610
C 13
C 14    14     2.1 D   3.820E-6   FISG0620
C 15    15     89. Y   2.469E-10   FISG0630
C 16
C 17
C 18
C 19
C 20
C 21
C 22
C 23
C 24
C 25
C
C 14    DATA(TCX(I),I=1,15)/
C        * 2.70E-24, 36.E-24, 60.E-24, 0., 0., 0., 1110.E-24, 290.E-24,
C        * 1350.E-24, 693.E-24, 6.E-24, 0., 170.E-24, 1600.E-24, 597.E-24/ FISG0640
C
C 15    DATA(TFX(I),I=1,25)/
C        * 0., 14.E-24, 0., 0., 0., 0., 740.E-24, 0., 950.E-24, 553.E-24,
C        * 0., 0., 0., 0., 17.E-24, 10*0.0 / FISG0650
C
C 16    DATA(TCX(I),I=16,25)/
C        * 180.E-24, 15.E-24, 45.E-24, 5.E-24, 190.E-24, 2.7E-18/ FISG0660
C
C 17    DATA(FCX(I),I=1,15)/
C        * 14.E-24*0., 0., 0., 0., 0., 1.6E-24, 1.6E-24, 1.6E-24, 6.6E-24,
C        * 3.E-24*0., 13.E-24, 0., 2.6E-24/ FISG0670
C
C 18    DATA(FFX(I),I=1,15)/
C        * 0.1E-24, 0., 0., 0., 0., 0., 1.6E-24, 1.6E-24, 1.6E-24, 1.4E-24, FISG0680
C        * 0., 0., 1.5E-24, 0., 2.6E-24/ FISG0690
C
C 19    DATA(FCX(I),I=16,25)/
C        * 10*0.0 / FISG0700
C 20    DATA(FFX(I),I=16,25)/
C        * 10*0.0 / FISG0710
C
C FISSION YIELDS FOR THOSE ISOTOPES THAT CONTRIBUTE TO THE GAS INVENTORY FISG1160
C *** FAST FISSION YIELDS *** ** THERMAL FISSION YIELDS ** FISG1170
C YIELDS (PS) FROM FISSION YIELDS (PS) FROM FISSION FISG1180

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* SOURCE STATEMENT (F15GAS)*

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C ***** C ***** C ***** C ***** C ***** C ****
C N U-235 U-238 Pu-239 Pu-241 U-238 Pu-239 Pu-241
C101 0.77 , 0.40 , 0.36 , 0.0 , 0.52 , 0.0 , 0.29 , 0.208,
C102 0.92 , 0.65 , 0.52 , 0.0 , 0.97 , 0.0 , 0.47 , 0.341,
C103 1.22 , 0.73 , 0.69 , 0.0 , 1.30 , 0.0 , 0.595 , 0.30 ,
C104 0.0 , 0.0 , 0.0 , 0.0 , 0.0 , 0.0 , 0.0 , 0.0 ,
C105 1.70 , 1.38 , 0.9 , 0.0 , 1.93 , 0.0 , 0.75 , 0.40 ,
C106 0.52 , 0.0 , 0.0 , 0.0 , 0.44 , 0.0 , 0.0 , 0.0 ,
C107 3.11 , 3.2 , 3.3 , 0.0 , 2.52 , 0.0 , 3.7 , 3.01 ,
C108 0.0 , 0.0 , 0.1 , 0.0 , 0.0 , 0.0 , 0.09 , 0.0 ,
C109 0.0 , 0.0 , 0.0 , 0.0 , 0.0 , 0.0 , 0.0 , 0.0 ,
C110 5.5 , 4.4 , 3.5 , 0.0 , 4.33 , 0.0 , 5.2 , 4.44 ,
C111 0.2 , 0.3 , 0.26 , 0.0 , 0.0 , 0.0 , 0.15 , 0.03 ,
C112 0.0 , 0.0 , 0.0 , 0.0 , 0.0 , 0.0 , 0.0 , 0.0 ,
C113 5.5 , 5.5 , 5.7 , 0.0 , 6.69 , 0.0 , 5.3 , 6.54 ,
C114 0.0 , 0.0 , 0.0 , 0.0 , 0.0 , 0.0 , 1.2 , 0.0 ,
C115 5.9 , 6.6 , 6.4 , 0.0 , 7.92 , 0.0 , 7.47 , 7.81 ,
C116 5.6 , 5.9 , 6.3 , 0.0 , 6.17 , 0.0 , 5.7 , 7.23 ,
C117 0.0 , 0.0 , 0.0 , 0.0 , 0.0 , 0.0 , 0.0 , 0.0 ,
C118 0.5 , 0.1 , 0.5 , 0.0 , 0.13 , 0.0 , 1.51 , 0.07 ,
C119 6.0 , 5.9 , 6.9 , 0.0 , 6.46 , 0.0 , 6.66 , 7.04 /
C
C TABLE FOR DECAY CONSTANT OF THE FISSION GAS ( 1 / SEC )
C N LC HALF LIFE DECAY CONSTANT
C101
C102
C103 85M 4.4 H 4.37594E-5
C104 85 10.76 Y 2.04271E-9
C105
C106 21 30. H 6.41805E-6
C107 22 25. H 4.6216E-4
C108 23 8.05 D 9.965E-7
C109
C110 25 78. H 2.46839E-6
C111 31 2.3 H 8.3713E-5
C112
C113 26 21. H 9.16865E-6
C114 33 5.27 D 1.5223E-6
C115
C116 28 6.7 H 2.87375E-5
C117 34 15.6 M 7.40544E-4
C118 35 9.2 H 2.09284E-5
C119
C
C #1 YIELDS FROM FISSION OF U235
C #2 YIELDS FROM FISSION OF U238
C #3 YIELDS FROM FISSION OF PU239
C #4 YIELDS FROM FISSION OF PU241
C.....REFEN HEDL TIME 7/2 128 PAGE B-3 OR JAERI-MEMO 5335 PAGE 20+21+22
21 DATA(I,IY1),I=1,4,J=1,102/
* .00502, .0 , .00290, .00206,
* .00970, .0 , .00470, .00341,
* .01300, .0 , .00535, .00300,
* .0 , .0 , .0 , .0 ,
* .01930, .0 , .00750, .00400,
* .00440, .0 , .0 , .0 ,
* .02520, .0 , .03700, .003010,
* .0 , .0 , .00090, .0 ,
* .0 , .0 , .0 , .0 ,
FISG1190
FISG1200
FISG1210
FISG1220
FISG1230
FISG1240
FISG1250
FISG1260
FISG1270
FISG1280
FISG1290
FISG1300
FISG1310
FISG1320
FISG1330
FISG1340
FISG1350
FISG1360
FISG1370
FISG1380
FISG1390
FISG1400
FISG1410
FISG1420
FISG1430
FISG1440
FISG1450
FISG1460
FISG1470
FISG1480
FISG1490
FISG1500
FISG1510
FISG1520
FISG1530
FISG1540
FISG1550
FISG1560
FISG1570
FISG1580
FISG1590
FISG1600
FISG1610
FISG1620
FISG1630
FISG1640
FISG1650
FISG1660
FISG1670
FISG1680
FISG1690
FISG1700
FISG1710
FISG1720
FISG1730
FISG1740
FISG1750
FISG1760
FISG1770

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* SOURCE STATEMENT (FISGAS)*

```

* .04330, .0 , .05200, .04440 / FISG1780
22 C DATA((TY(I,J),I=1,4),J=11,19)/ FISG1790
* .0 , .0 , .00150, .00030, .00030 / FISG1800
* .0 , .0 , .0 , .0 , .0 / FISG1810
* .06890, .0 , .05300, .06540, .0 / FISG1820
* .0 , .0 , .01200, .0 , .0 / FISG1830
* .07920, .0 , .07470, .07810, .0 / FISG1840
* .06170, .0 , .05700, .07230, .0 / FISG1850
* .0 , .0 , .0 , .0 , .0 / FISG1860
* .00130, .0 , .01510, .00070, .0 / FISG1870
* .06460, .0 , .06660, .07040 / FISG1880
* .0 , .0 , .0 , .0 , .0 / FISG1890
23 C DATA((FY(I,J),I=1,4),J=1,10)/ FISG1900
* .0077 , .0040 , .0038 , .0 , .0 / FISG1910
* .0092 , .0085 , .0052 , .0 , .0 / FISG1920
* .0122 , .0073 , .0069 , .0 , .0 / FISG1930
* .0 , .0 , .0 , .0 , .0 / FISG1940
* .0170 , .0138 , .0090 , .0 , .0 / FISG1950
* .0092 , .0 , .0 , .0 , .0 / FISG1960
* .0311 , .0320 , .0330 , .0 , .0 / FISG1970
* .0 , .0 , .0010 , .0 , .0 / FISG1980
* .0 , .0 , .0 , .0 , .0 / FISG1990
* .0 , .0 , .0440 , .0350 , .0 / FISG2000
* .0550 , .0 , .0 , .0 , .0 / FISG2010
24 C DATA((FY(I,J),I=1,4),J=11,19)/ FISG2020
* .0020 , .0030 , .0026 , .0 , .0 / FISG2030
* .0 , .0 , .0 , .0 , .0 / FISG2040
* .0550 , .0550 , .0570 , .0 , .0 / FISG2050
* .0 , .0 , .0 , .0 , .0 / FISG2060
* .0590 , .0660 , .0640 , .0 , .0 / FISG2070
* .0560 , .0590 , .0630 , .0 , .0 / FISG2080
* .0 , .0 , .0 , .0 , .0 / FISG2090
* .0050 , .0010 , .0050 , .0 , .0 / FISG2100
* .0600 , .0590 , .0690 , .0 / FISG2110
* .0 , .0 , .0 , .0 , .0 / FISG2120
25 C C EN1(A+X,T) = A*DEXP(-X*T) FISG2130
26 EN2(F*AB+B*x,T) = F*AB+B*(1.-DEXP(-X*T))/X FISG2140
27 EN3(DC+C*x,T) = DC*C*(1.-DEXP(-X*T))/X FISG2150
28 FAC(x,T) = (1.-DEXP(-X*T))/X FISG2160
29 C T = TIN FISG2170
30 IF(MTIME.GT.0) GO TO 4 FISG2180
31 A1=A2=A3=A4=A5=A6=A7=A8=A9=A10=A11=A12=A13=A14=A15=0.0 FISG2190
32 A101=A102=A103=A104=A105=A106=A107=A108=A109=A110=0.0 FISG2200
33 A111=A112=A113=A114=A115=A116=A117=A118=A119=0.0 FISG2210
34 A1 = A12 FISG2220
35 A7 = A72 FISG2230
36 A8 = A8Z FISG2240
37 A9 = A9Z FISG2250
38 A10 = A10Z FISG2260
39 GO TO 6 FISG2270
40 C 4 CONTINUE FISG2280
C *** FILE MATERIALS **** FISG2290
C A1 238U----ABS.N FISG2300
C A2 238U----ABS.N FISG2310
C A3 238U----ABS.N AND DECAY(DC2) FISG2320

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* SOURCE STATEMENT (FISGAS)*

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C   A3    239U DECAY----239NP----ABS.N AND DECAY(DC3)      F1SG2370
C   A4    239U ABS.N----240U-----DECAY(DC4)              F1SG2380
C   A5    240U DECAY----240NP(M)---DECAY(DC5)            F1SG2390
C   A6    239NP ABS.N----*                                F1SG2400
C   A6    (M)240NP DECAY----240NP----DECAY(DC6)          F1SG2410
C   A7    238NP ABS.N----239PU----ABS.N                  F1SG2420
C   A7    239NP DECAY----*                                F1SG2430
C   A8    239PU ABS.N----240PU----ABS.N                  F1SG2440
C   A8    240NP DECAY----*                                F1SG2450
C   A9    240PU ABS.N----241PU----ABS.N                  F1SG2460
C   A10   235U ABS.N----236U----ABS.N                  F1SG2470
C   A11   236U ABS.N----237U----DECAY(C12)            F1SG2480
C   A12   237U DECAY----237NF----ABS.N                  F1SG2490
C   A13   237N ABS.N----238NP----ABS.N AND DECAY(DC14)  F1SG2500
C   A14   237N DECAY----238PU----ABS.N AND DECAY(DC15)  F1SG2510
C   A15   238N DECAY----238PU----ABS.N AND DECAY(DC15)  F1SG2520
C   *** GASES OF FISSION PRODUCTS ***
C   A101  YIELD-----83KR----ABS.N                  F1SG2530
C   A102  YIELD-----84KR----*                          F1SG2540
C   A102  83KR ABS.N----*                            F1SG2550
C   A103  YIELD-----85KR(M)---DECAY(DC85M)          F1SG2560
C   A104  YIELD-----85KR----ABS.N AND DECAY(DC85)  F1SG2570
C   A104  (M)85KR DECAY----*                          F1SG2580
C   A104  (0.21)                                     F1SG2590
C   A105  YIELD-----86KR----*                          F1SG2600
C   A105  85KR ABS.N----*                            F1SG2610
C   A106  YIELD-----131TE(M)---DECAY(DC21)          F1SG2620
C   A107  YIELD-----131TE----DECAY(DC22)            F1SG2630
C   A107  (M)131TE DECAY----*                          F1SG2640
C   A107  (0.18)                                     F1SG2650
C   A108  131TE DECAY----131I-----DECAY(DC23)        F1SG2660
C   A108  (M)131TE DECAY----*                          F1SG2670
C   A108  (0.82)                                     F1SG2680
C   A109  131I DECAY----131XE----ABS.N                F1SG2690
C   A110  YIELD-----132TE----DECAY(DC25)            F1SG2700
C   A111  132TE DECAY----132I-----DECAY(DC31)        F1SG2710
C   A112  132I DECAY----132XE----ABS.N                F1SG2720
C   A112  131XE ABS.N----*                            F1SG2730
C   A113  YIELD-----133I-----DECAY(DC26)            F1SG2740
C   A114  133I DECAY----133XE----ABS.N AND DECAY(DC33)  F1SG2750
C   A115  YIELD-----134XE----*                          F1SG2760
C   A115  134XE ABS.N----*                            F1SG2770
C   A115  134XE ABS.N----*                            F1SG2780
C   A116  YIELD-----135I-----DECAY(DC28)            F1SG2790
C   A117  135I DECAY----135XE(M)---DECAY(DC34)        F1SG2800
C   A117  (0.5)                                       F1SG2810
C   A118  YIELD-----135XE----ABS.N AND DECAY(DC35)  F1SG2820
C   A118  135I DECAY----*                            F1SG2830
C   A118  (0.7)                                       F1SG2840
C   A118  (M)135XE----*                            F1SG2850
C   A119  YIELD-----136XE----*                          F1SG2860
C   A119  135XE ABS.N----*                            F1SG2870
C   A119  135XE ABS.N----*                            F1SG2880
C   A1 = A(1,IP)                                     F1SG2890
C   A2 = A(2,IP)                                     F1SG2900
C   A3 = A(3,IP)                                     F1SG2910
C   A4 = A(4,IP)                                     F1SG2920
C   A5 = A(5,IP)                                     F1SG2930
C   A6 = A(6,IP)                                     F1SG2940
C   A7 = A(7,IP)                                     F1SG2950

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* SOURCE STATEMENT (FISGAS)*

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48   A8 = A(8,IP)                                     F1SG2960
49   A9 = A(9,IP)                                     F1SG2970
50   A10 = A(10,IP)                                    F1SG2980
51   A11 = A(11,IP)                                    F1SG2990
52   A12 = A(12,IP)                                    F1SG3000
53   A13 = A(13,IP)                                    F1SG3010
54   A14 = A(14,IP)                                    F1SG3020
55   A15 = A(15,IP)                                    F1SG3030
56   A101 = A(11,IP)                                   F1SG3040
57   A102 = A(22,IP)                                   F1SG3050
58   A103 = A(23,IP)                                   F1SG3060
59   A104 = A(24,IP)                                   F1SG3070
60   A105 = A(25,IP)                                   F1SG3080
61   A106 = A(26,IP)                                   F1SG3090
62   A107 = A(27,IP)                                   F1SG3100
63   A108 = A(28,IP)                                   F1SG3110
64   A109 = A(29,IP)                                   F1SG3120
65   A110 = A(30,IP)                                   F1SG3130
66   A111 = A(31,IP)                                   F1SG3140
67   A112 = A(32,IP)                                   F1SG3150
68   A113 = A(33,IP)                                   F1SG3160
69   A114 = A(34,IP)                                   F1SG3170
70   A115 = A(35,IP)                                   F1SG3180
71   A116 = A(36,IP)                                   F1SG3190
72   A117 = A(37,IP)                                   F1SG3200
73   A118 = A(38,IP)                                   F1SG3210
74   A119 = A(39,IP)                                   F1SG3220
75   C
76   6 CONTINUE
77   IF(IFLUX,NL,0) GO TO 10
78   DO 5 I=1,25
79   CX(I)=CX(I)
80   FX(I)=FX(I)
81   GO TO 20
82   10 DO 15 I=1,25
83   CX(I)=ICX(I)
84   15 FX(I)=TFX(I)
85   20 CONTINUE
86   DO 25 I=1,15
87   25 AX(I) = CX(I)-FX(I)
88   IF(IFLUX,NL,0) GO TO 35
89   DO 30 I=1,4
90   30 Y(I,J) = FY(I,J)
91   GO TO 45
92   35 DO 40 J=1,19
93   40 DO 40 J=1,19
94   40 Y(I,J) = TY(I,J)
95   45 CONTINUE
C
C   PH1= NUETHON FLUX . A12 = U-235 CONCENTRATION
C   A1 = U-238 . A7 = PU-239 . A8 = PU-240 . A9 = PU-241 + A10 = UF1SG3460
C   PHM=P/(CONEN*(A1 *FX(1)+A7 *FX(7)+A8 *FX(B)+A9 *FX(9)+A10 *FX(10)) F1SG3470
C   *          ) / 1000.0
C   PH1 = PHM
C   IF(PH1>LE,0,0) PH1 = 1.0E-24
C   CALL SETIO(26,-2)
C   F(I) = FISSION GAS ATOMS YIELDED BY FISSION
C   DO 50 I=1,19
C   50 F(I)=PHM*(FX(10)*A10*Y(1,I)+FX(1)*A1*Y(2,I)+FX(7)*A7*Y(3,I)+FX(9)*F1SG3540

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* SOURCE STATEMENT (FISGAS)*

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      *A9*Y(4,1)   )
101  9996 FORMAT(1H , ' N INPUT TERMS / (1X,1P6E12,6)          FISG3550
C ****NO NEEDSITY CARDS FROM HERE TO FISG 1910 ****          FISG3560
102  X1=PHI*CX(1)          FISG3570
103  X2=PHI*CX(2)+DC2          FISG3580
104  X3=PHI*CX(3)+DC3          FISG3590
105  X4=DC4          FISG3600
106  X5=DC5          FISG3610
107  X6=DC6          FISG3620
108  X7=PHI*CX(7)          FISG3630
109  X8=PHI*CX(8)          FISG3640
110  X9=PHI*CX(9)          FISG3650
111  X10=PHI*CX(10)         FISG3660
112  X11=PHI*CX(11)         FISG3670
113  X12=DC12          FISG3680
114  X13=PHI*CA(13)         FISG3690
115  X14=PHI*CX(14)+DC14          FISG3700
116  X15=PHI*CX(15)+DC15          FISG3710
117  A1=EN1(A1,X1,T)         FISG3720
118  A2=EN1(A2,X2,T)*EN2(PHI,AX(1),A1,X2,T)          FISG3730
119  A3=EN1(A3,X3,T)*EN3(DC2,A2,X3,T)          FISG3740
120  A4=EN1(A4,X4,T)*EN2(PHI,AX(2),A2,X4,T)          FISG3750
121  A5=EN1(A5,X5,T)*EN2(PHI,AX(3),A3,X5,T)+EN3(DC4,A4,X5,T)          FISG3760
122  A6=EN1(A6,X6,T)*EN3(DC5,A5,X6,T)          FISG3770
123  A10=EN1(A10,X10,T)         FISG3780
124  A11=EN1(A11,X11,T)*EN2(PHI,AX(10),A10,X11,T)          FISG3790
125  A12=EN1(A12,X12,T)*EN2(PHI,AX(11),A11,X12,T)          FISG3800
126  A13=EN1(A13,X13,T)*EN3(CC12,A12,X13,T)          FISG3810
127  A14=EN1(A14,X14,T)*EN2(PHI,AX(13),A13,X14,T)          FISG3820
128  A15=EN1(A15,X15,T)*EN3(CC14,A14,X15,T)          FISG3830
129  A7=EN1(A7,X7,T)*EN2(PHI,AX(15),A15,X7,T)+EN3(DC3,A3,X7,T)          FISG3840
130  A8=EN1(A8,X8,T)*EN2(PHI,AX(7),A7,X8,T)+EN3(DC6,A6,X8,T)          FISG3850
131  A9=EN1(A9,X9,T)+EN2(PHI,AX(8),A8,X9,T)          FISG3860
132  C*****                                         FISG3870
133  X101=PHI*CX(20)          FISG3880
134  X103=DC85M          FISG3890
135  X104=PHI*CX(21)+DC85          FISG3900
136  X106=DC21          FISG3910
137  X107=DC22          FISG3920
138  X108=DC23          FISG3930
139  X109=PHI*CX(22)          FISG3940
140  X110=DC25          FISG3950
141  X111=DC31          FISG3960
142  X112=PHI*CX(23)          FISG3970
143  X113=DC26          FISG3980
144  X114=PHI*CX(24)+DC33          FISG3990
145  X116=DC28          FISG4000
146  X117=DC36          FISG4010
147  IF(CX(20),LE,1,E-30) GO TO 100          FISG4020
148  A101=EN1(A101,X101,T)+F(1)*FAC(X101,T)          FISG4030
149  GO TO 101          FISG4040
150  100 A101=A101+F(1)*T          FISG4050
151  101 A102=A102+(F(2)*PHI*CX(20)*A101)*1          FISG4060
152  A103=EN1(A103,X103,T)+F(3)*FAC(X103,T)          FISG4070
153  A104=EN1(A104,X104,T)*(F(4)+.21*X103*A103)*FAC(X104,T)          FISG4080
154  A105=A105+(F(5)*PHI*CX(21)*A104)*T          FISG4090
155  A106=EN1(A106,X106,T)+F(6)*FAC(X106,T)          FISG4100
156  A107=EN1(A107,X107,T)+(F(7)+.18*X106*A106)*FAC(X107,T)          FISG4110

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* SOURCE STATEMENT (FISGAS)*

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157  A108=EN1(A108,A108,T)+(.82*X106*A106*X107*A107)*FAC(X108,T)          FISG4120
158  J1(CX(22),LE,1,E-30) GO TO 102          FISG4130
159  A109=EN1(A109,A109,T)+X108*A108*FAC(X109,T)          FISG4140
160  GO TO 103          FISG4150
161  102 A109=A109+X108*A108*T          FISG4160
162  103 A110=EN1(A110,X110,T)+F(10)*FAC(X110,T)          FISG4170
163  A111=EN1(A111,A111,T)*X110*A119*FAC(X111,T)          FISG4180
164  IF(CX(23),LE,1,E-30) GO TO 104          FISG4190
165  A112=EN1(A112,X112,T)*(X111*A111+A109)*FAC(X112,T)          FISG4200
166  GO TO 105          FISG4210
167  104 A112=A112+(X111*A111+X109*A109)*T          FISG4220
168  105 A113=EN1(A113,X113,T)+(F(13)*FAC(X113,T))          FISG4230
169  A114=EN1(A114,X114,T)*X113*A115*FAC(X114,T)          FISG4240
170  A115=A115+(F(15)*PHI*CX(24)*A114)*T          FISG4250
171  A116=EN1(A116,X116,T)*F(16)*FAC(X116,T)          FISG4260
172  A117=EN1(A117,X117,T)+.3*X116*A116*FAC(X117,T)          FISG4270
173  A118=EN1(A118,X118,T)+(F(18)+.7*X116*A116*X117*A117)*FAC(X118,T)          FISG4280
174  A119=A119+(F(19)+PHI*CX(25)*A118)*T          FISG4290
C      ANSWER          FISG4300
175  ARK=A101+A102+A103+A104+A105          FISG4310
176  A1=A109+A112+A114+A115+A117+A118+A119          FISG4320
C
177  A(1,IP) = A1          FISG4330
178  A(2,IP) = A2          FISG4340
179  A(3,IP) = A3          FISG4350
180  A(4,IP) = A4          FISG4360
181  A(5,IP) = A5          FISG4370
182  A(6,IP) = A6          FISG4380
183  A(7,IP) = A7          FISG4390
184  A(8,IP) = A8          FISG4400
185  A(9,IP) = A9          FISG4410
186  A(10,IP) = A10          FISG4420
187  A(11,IP) = A11          FISG4430
188  A(12,IP) = A12          FISG4440
189  A(13,IP) = A13          FISG4450
190  A(14,IP) = A14          FISG4460
191  A(15,IP) = A15          FISG4470
192  A(21,IP) = A101          FISG4480
193  A(22,IP) = A102          FISG4490
194  A(23,IP) = A103          FISG4500
195  A(24,IP) = A104          FISG4510
196  A(25,IP) = A105          FISG4520
197  A(26,IP) = A106          FISG4530
198  A(27,IP) = A107          FISG4540
199  A(28,IP) = A108          FISG4550
200  A(29,IP) = A109          FISG4560
201  A(30,IP) = A110          FISG4570
202  A(31,IP) = A111          FISG4580
203  A(32,IP) = A112          FISG4590
204  A(33,IP) = A113          FISG4600
205  A(34,IP) = A114          FISG4610
206  A(35,IP) = A115          FISG4620
207  A(36,IP) = A116          FISG4630
208  A(37,IP) = A117          FISG4640
209  A(38,IP) = A118          FISG4650
210  A(39,IP) = A119          FISG4660
C
211  RETURN          FISG4670
C*****                                         FISG4680

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* SOURCE STATEMENT (FISGAS)*

212 ENQ

FISG6473D

FACOM 230-75 (M7) FORTRAN-D -760229- V06-L07 76.09.03 PAGE 62

* SOURCE STATEMENT *

```
1      FUNCTION FYIELD (TYIELD,TEMP,FNVT)          FYIE0010
C      THIS FUNCTION IS CALLED FROM STEP2 AND STEP7.    FYIE0020
C      CALCULATION OF YIELD STRENGTH OF ZRY REFER D-1001,1002   FYIE0030
2      COMMON /COM_ 0/ TITLE(20),AA(7, 30),BB(6, 51),CF(3, 30),RV(2, 20) FYIE0040
3      COMMON /COM_ 21/ N,NN,NNN,NF                      FYIE0050
4      IN1 = 7                                         FYIE0060
5      IN2 = 30                                        FYIE0070
6      IN3 = 6                                         FYIE0080
7      FYIELD = TERP(TEMP,AA,3,NN,IN1,IN2,IN3,100)     FYIE0090
8      RETURN                                         FYIE0100
9      END                                            FYIE0110
                                                 FYIE0120
                                                 FYIE0130
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* SOURCE STATEMENT *

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1      SUBROUTINE GPRO(CASE,JCASE)                               GPR00010
2      C THIS SUBROUTINE IS CALLED FROM STEP8.                  GPR00020
3      C
4      COMMON /PWRAY/ PAVRG,FUEL,L,POWER(21),A1(21),NPOW,PTOT,LPMAX, GPR00030
5      C          PKPOW,(PEAK+DEL)*PMAX                           GPR00040
6      COMMON /COM 0/ TITLE(20),AA7, 30),BB6, 51),CF(3, 30),HY(2, 20) GPR00050
7      COMMON /COM 02/ IPU,NSTEP,ITER,KOUNT                      GPR00060
8      COMMON /COM 8/ GG(20*100)                                 GPR00070
9      COMMON /HIZUKE/ K1,K2,K3,K4,K5,K6                         GPR00080
10     DIMENSION Z(9),P(121)                                    GPR00090
11     DATA Z / 1H1,1H2,1H3,1H4,1H5,1H6,1H7,1H8,1H9 /
12     JINI = 1                                              GPR00100
13     0 = 0.0001                                         GPR00110
14     IMAX = 120                                           GPR00120
15     JMAX = ITFR                                         GPR00130
16     WRITE(6,1710) JCASE,IPOW,NPOW,K1,K2,K3,K4,K5,K6       GPR00140
17     WRITE(6,600) TITLE                                     GPR00150
18     DO 4 I=1,121                                         GPR00160
19     4 P(I) = 1H                                         GPR00170
20     DO 20 JJ=1,3                                         GPR00180
21     FACT = 0.01 * 10.0**JJ                                GPR00190
22     DO 10 J=1,9                                         GPR00200
23     X = FACT * FLOAT(J)                                  GPR00210
24     10 I = 1.0 + (1.0 + ALOG10(X)) * 60.0               GPR00220
25     IF(I,LE,1) I=1                                     GPR00230
26     IF(I,GT,121) GO TO 20                               GPR00240
27     20 P(I) = Z(JJ)                                    GPR00250
28     CONTINUE                                         GPR00260
29     WRITE(6,604) P                                     GPR00270
30     DO 1 J=JINI,JMAX                                   GPR00280
31     1 P(I) = 1H                                         GPR00290
32     29 IM = 1.0 + (1.0 + ALOG10 (D + GG(3,J))) * 60.0   GPR00300
33     IC = 1.0 + (1.0 + ALOG10 (D + GG(4,J))) * 60.0   GPR00310
34     IS = 1.0 + (1.0 + ALOG10 (D + GG(5,J))) * 60.0   GPR00320
35     IG = 1.0 + (1.0 + ALOG10 (D + GG(6,J))) * 60.0   GPR00330
36     IR = 1.0 + (1.0 + ALOG10 (D + GG(7,J))) * 60.0   GPR00340
37     IF(IC,LE,0) IM = 1                                 GPR00350
38     IF(IS,LE,0) IS = 1                                 GPR00360
39     IF(IG,LE,0) IG = 1                                 GPR00370
40     IF(IR,LE,0) IR = 1                                 GPR00380
41     IF(IC,GT,121) IM = 121                            GPR00390
42     IF(IC,GT,121) IC = 121                            GPR00400
43     IF(IS,GT,121) IS = 121                            GPR00410
44     IF(IG,GT,121) IG = 121                            GPR00420
45     IF(IR,GT,121) IR = 121                            GPR00430
46     IF(IM,LT,1) IM = 1H                                GPR00440
47     P(IC) = IMC                                       GPR00450
48     P(IS) = IM5                                       GPR00460
49     P(IG) = IM6                                       GPR00470
50     P(IR) = IM8                                       GPR00480
51     P(I) = IM9                                       GPR00490
52     P(I) = IM9                                       GPR00500
53     P(I) = IM9                                       GPR00510
54     P(I) = IM9                                       GPR00520
55     P(I) = IM9                                       GPR00530
56     WRITE(6,601) GG(3,J),GG(4,J)+P                 GPR00540
57     DO 3 J=JINI,JMAX                               GPR00550
58     3 WRITE(6,603) (GG(I,J)+I=1,9)                GPR00560
59     WRITE(6,606) (LL,LL=1,10)                      GPR00570
60     DO 5 J=JINI,JMAX                               GPR00580
61     5 J=JINI,JMAX                               GPR00590

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* SOURCE STATEMENT (GPRO) *

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56     3 WRITE(6,605) GG(1,J),(GG(1,J),I=10,20)             GPR00600
57     WRITE(6,607)                                         GPR00610
58     RETURN                                         GPR00620
59     C * 1 * 2 * 3 * 4 * 5 * 6 * 7                         GPR00630
60     1710 FORMAT(1H1,2X,*1,5X,'AXIAL SEGMENT ',12,2X,10F 1+12*2X, / ) GPR00640
61     * 22X, 2AA(15,3H HR,13,7H MINUTE,13,4H SEC,14 / ) GPR00650
62     600 FORMAT(1H + 5A,5(1H),5X,20A4,3X,5(1H*) / )        GPR00660
63     601 FORMAT(1H ,F6.4,F7.4,1X,121A1-)                  GPR00670
64     602 FORMAT( 4A14HITEM, 5X, 4HTMAX, 11X,4HHG=H, 11X,5HHGC=C, 11X, / )
65     * 8HHSOLID=5, 7X,6HHGAS=G, 9X,6HHRAD=R, 9X,6HHGACEL, / ) GPR00680
66     * 8X,3HCEE                                         GPR00690
67     603 FORMAT(2XF4.0,16.2,6X,2G15.5, 2X, 4G15.5, F12.6, / ) GPR00700
68     604 FORMAT( 1X, 121A1 )                                GPR00710
69     605 FORMAT( 2X,F3.0, 10F12.6, 4X,A4 )                  GPR00720
70     606 FORMAT(/5H (ITER,10)(X),1H(+,I2+1H)+3X),6H (11) / ) GPR00730
71     607 FORMAT(5X,50H(1)) INCREASE DUE TO THERMAL EXPANSION /GPR00740
72     1 5X,5SH(2) INCREASE DUE TO SWELLING (OLD MODEL) /GPR00750
73     2 5X,5SH(3) (6) - MEAN ROUGHNESS(R) (R=1.98*(ROUF+ROUC)) /GPR00760
74     3 5X,5SH(4) INCREASE DUE TO SWELLING (NEW MODEL) /GPR00770
75     4 5X,5SH(5) ; (IF (4),GT,(2), (5)=(4) ) /GPR00780
76     5 5X,5SH(6) RADIAL HOT GAP (=GAP/4, -(DELR1+DELR2+DELR3)+DEL) ,GPR00790
77     6 5X,5SH(7) DELRT=(1),DELRB=(5),DELRD=DENS1F(, ,DELRG=CLAD DEFORM /GPR00810
78     7 5X,5SH(7) RADIAL HOT GAP WHICH IS TAKEN INTO ACCOUNT NEW SWELL /GPR00820
79     8 5X,5SH(8) IF HOT GAP .LT. (R) + GAP IS TOUCH AND HOT GAP =(R) /GPR00830
80     9 5X,5SH(8) RADIAL HOT GAP =(R) + 1.E-6 (SOFT TOUCH CONDITION) +GPR00840
81     A 5X,5SH(9) IF GAP IS NOT TOUCH +(B) = 0.0 /GPR00850
82     B 5X,5SH(9) =(C6)-RELOCATION = (H) , IF (9),LT,0 +GAP IS CONTACT/GPR00860
83     C 5X,5SH(10) RADIAL HOT GAP (CONTACT CONDITION) /GPR00870
84     D 5X,5SH(11) OLD OR NEW SWELLING MODEL SIGN /GPR00880
85
86     ****END**** *****GPR00890*****GPR00900

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* SOURCE STATEMENT *

```

1      SUBROUTINE HCAP(TEMP,CPNOM,CPMIN,CPMAX)
C
C      THIS SUBROUTINE IS CALLED FROM STEP 8
C      REFER LNAL-177B: GAPCON THERMAL-1
C      HEAT CAPACITY OF U02 ( KERRISK AND CLIFTON )
C
2      DIMENSION TTK(10),CLMIN(10),CLMAX(10)
3      REAL X1,X2,X3
4      DATA (TTK(I),I=1,10)/0.0,298.,300.,1000.,1500.,2000.,2500.,3000.,
*3100.,3090./
5      DATA (CLMIN(I)),I=1,10)/0.0,.02,.02,.02,.03,.06,.10,.10/
6      DATA (CLMAX(I)),I=1,10)/1.0,1.0,1.02,1.02,1.02,1.02,1.03,1.08,1.1,
*1.1/
7      150 TKEL = 535.245
8      ED = .376946
9      X1 = 19.1450
10     X2 = 0.000784733
11     X3 = 5643730.0
12     R = .001986
C      TEMP = AVERAGE VOLUMETRIC FUEL TEMPERATURE
13     TEMPX = TEMP + 273.0
14     CL = 1.0
15     CPNOM=CL*((1+TKEL**2*EXP(TKEL/TEMPX))/(TEMPX**2*(EXP(TKEL/TEMPX))-
*11)**2)+(2*TK2*TEMPX)+((K3*ED)/(R*TEMPX**2))*EXP(-ED/(R*TEMPX)))
16     CL = TEPP(CPMIN,CLMIN,TTK,10)
17     C1 = 1.0-CLN
18     CMIN=C1*((1+TKEL**2*EXP(TKEL/TEMPX))/(TEMPX**2*(EXP(TKEL/TEMPX))-
*11)**2)+(2*TK2*TEMPX)+((K3*ED)/(R*TEMPX**2))*EXP(-ED/(R*TEMPX)))
19     C2 = TEPP(TEMPX,CLMAX,TTK,10)
20     CMAX=C2*((1+TKEL**2*EXP(TKEL/TEMPX))/(TEMPX**2*(EXP(TKEL/TEMPX))-
*11)**2)+(2*TK2*TEMPX)+((K3*EU)/(R*TEMPX**2))*EXP(-ED/(R*TEMPX)))
21     RETURN
C*****END*****
22 END

```

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* SOURCE STATEMENT *

```

1      SUBROUTINE HEAD (IF )                                HEAD0010
C
C
2      COMMON /COM 0/ TITLE(20),AA(7, 30),BB(6, 51),CF(3, 30),HV(2, 20) HEAD0020
3      COMMON /INPUT  / FRDEN,FRSIN,DSINZ,FRPU02,FR35,FR40,FR41,DFS,DC1, HEAD0030
3      COMMON /INPUT  / DCO,DVIDZ,VPLENZ,ATMOS,S,XX,ROUF,ROUC,EXTP,DE,V, HEAD0040
3      1          DCO,DVIDZ,VPLENZ,ATMOS,S,XX,ROUF,ROUC,EXTP,DE,V, HEAD0050
2          TINLET,DELT,TMAX,TFR,TM,DBS,BK,HBC,SIGHF,IFLUX, HEAD0060
3          NCLAD,NCON,NFLX,KOOL,NEWK,NEWCL,NEWFLX,VCIDLZL,NOH,HEAD0070
4          FRACHE,FRACAR,FRACH,FRACN,FRACKR,FRACXE,IGACEL, HEAD0080
5          OTEMP,ZCLAD,HG,PEKAVG,MINI,ICDF,ISTOR,ICREP,ISWELL,HEAD0090
6          ,NEXP,MEXP,NHIST, HEAD0100
7          COMMON /COM 0/ IP0W,ISTEP,ITER,KOUNT, HEAD0120
8          COMMON /COM 0/ BURNUP,TDAYS,VVOID,TOTLDY,TOTBUR, HEAD0130
9          COMMON /COM 0/ LI,JCASE,TCOOLF,AMUTOT, HEAD0140
10         COMMON /PCRAY/ PAVRG,FUEL,FL,POWER(21),A1(21),NP0W,PTOT,LPMAX, HEAD0150
1          PKP0W,IPEAK,DELP,PMAX, HEAD0160
1          COMMON /COM91/ SEC, HEAD0170
9          DATA IP,JP /20/
10         DATA TSEC/0.0/ HEAD0180
10         C
10         IF (IF) . GT. 0 ONLY TITLE PRINT HEAD0190
10         IF (IF) . LE. 0 HISTORICAL DATA PRINT PAGE HEADING HEAD0200
11         IP=IP+1 HEAD0210
12         IF(IF,GT,0) JP=0 HEAD0220
13         JP=JP+1 HEAD0230
13         C
14         WRITE(6,100) JCASE,TITLE,JP,IP HEAD0240
15         IF(IF,LE,0) RETURN HEAD0250
16         WRITE(6,100)
17         A1=PAVG*1000,*30.48 HEAD0260
18         A2=TINLET*1.8 + 32. HEAD0270
19         A3=TINLET*DELT HEAD0280
20         A4=A3*1.8 + 32. HEAD0290
21         A5=EXTP*14.22 HEAD0300
22         A6=TOTBUR/1000, * 3.37 E19 HEAD0310
23         TSEC=TSEC*SEC HEAD0320
24         T=UR*TOTLDY*24. HEAD0330
25         WRITE(6,110) A1,PAVRG HEAD0340
26         WRITE(6,111) TOTBUR,A6 HEAD0350
27         WRITE(6,115) TOTLDY,THOR HEAD0360
28         WRITE(6,120) A2,TINLET HEAD0370
29         WRITE(6,130) A4,A3 HEAD0380
30         WRITE(6,140) A5,EXTP HEAD0390
31         WRITE(6,150) TSEC,SEC HEAD0400
32         WRITE(6,105) HEAD0410
33         RETURN HEAD0420
33         C
34         100 FORMAT(1H1 / 4X,6HSTEP ,13*5X,20A4,10X,5HPAGE +(2+1H/,13 / ) HEAD0430
35         105 FORMAT(15x,95(1H=)) HEAD0440
36         110 FORMAT(22X,27HLINEAR HEAT RATING(AVERAGE) ,F10.3,10H (KW/FT) , HEAD0450
1          F10.3,10H (WATT/CM) ) HEAD0460
37         111 FORMAT(22X,27HBUH,UP (IN AVERAGE) ,F10.3,10H (MWD/MTU) , HEAD0470
1          E15.4,14H (FISSEONS/CC) ) HEAD0480
38         115 FORMAT(22X,27HTIME IN REACTOR ,F10.3,10H (DAYS) , HEAD0490
1          F10.3,10H (HOURS) ) HEAD0500
39         120 FORMAT(22X,27HCOOLANT INLET TEMPERATURE ,F10.3,10H (DEG F) , HEAD0510
1          F10.3,10H (DEG C) ) HEAD0520
40         130 FORMAT(22X,27HCOOLANT OUTLET TEMPERATURE ,F10.3,10H (DEG F) , HEAD0530
1          F10.3,10H (DEG C) ) HEAD0540
40         135 FORMAT(22X,27HCOOLANT PRESSURE ,F10.3,10H (PSI) , HEAD0550
1          F10.3,10H (KG/CM2) ) HEAD0560
42         150 FORMAT(22X,20HCUMULATED CP TIME ,F10.4,5H(SEC)+5X, HEAD0570
1          26HCOMPUTED TIME AT THIS STEP,F10.4,5H(SEC) ) HEAD0580
43         END HEAD0590

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* SOURCE STATEMENT (HEAD) **

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1          F10.3,10H (DEG C) ) HEAD0600
41         140 FORMAT(22X,27HCOOLANT PRESSURE ,F10.3,10H (PSI) , HEAD0610
1          F10.3,10H (KG/CM2) ) HEAD0620
42         150 FORMAT(22X,20HCUMULATED CP TIME ,F10.4,5H(SEC)+5X, HEAD0630
1          26HCOMPUTED TIME AT THIS STEP,F10.4,5H(SEC) ) HEAD0640
43         END HEAD0650
43         HEAD0660

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* SOURCE STATEMENT *

```

1      SUBROUTINE HISTR(KS,NEXT)
C
C      THIS SUBROUTINE IS CALLED FROM STEP1(KS=1), AND MAIN(KS=2)
C
2      COMMON /HIST / HIST(7,50),IPD(5,50)
3      COMMON /HIS / BASE(100),HIS(?,100),MODE(5,100)
4      COMMON /HIST1/ NHIST,NNHIST
5      COMMON /POKRAY/ PAYRG,FUELL,FL,POWER(21),AI(21),NPOW,PTOT,LPMAX,
6          PPKWH,TPERK,PMMA
7      COMMON /CON 0 / TITLE(20),AA(7,30),BE(6,51),CF(3,30),RV(2,20)
8      COMMON /COM 0 / BURNUP,TDAYS,VVOI,DY,TOTLDY,TOTBUR
9      COMMON /COM 0/ IT,JCASE,TCOLDF,XPTOT
10     COMMON /COM 10/ VVOI02,FR02,TPLEA,NFOU1
11     COMMON /INPUT / FRDN01,FRNSIN,DSIN2,FR03,FR4L,FR41,DFS,DCJ,
12         DCO,DVID2,VPLENZ,ATMOS$,$,XX,ROUF,ROUC,EXTP,DE,V, HIST010
13         TINLET,DELI,TMAX,FRNTM,DB0,BK,HBC,SIGHF,IFLUX, HIST0110
14         NCLAD,NCON,NFLX,KCOL,NEAK,NEAL,NEWFLX,VIDDL,NOSH, HIST0120
15         FRACAR,FRACH,FRACK,FRACAE,FRACEL, HIST0130
16         DTENP,ITOT,AGP,PERAVG,MINI,ICDF,ISTOR,ICREP,ISWELL, HIST0140
17         NLXP,MEXP,NHIST, HIST0150
18         COMMON /XAIR / XA(14,1)H,MAXTEP, HIST0160
19         COMMON /SUTEM/ LCOUNT, HIST0170
20         COMMON /HISTMAX/ APOWER, HIST0180
21         COMMON /SPARE/ ISPA,NAMSP(3), HIST0190
22         DIMENSION DEL(7), HIST0200
23         DIMENSION TS(100), HIST0210
24         DIMENSION BPOW(100), HIST0220
25         DIMENSION UTJ(10,?),XFORM(10,5), FORM(5), HIST0230
26         DATA SINC,BINC / 150., 150. /, HIST0240
27         DATA BINC/1500./, HIST0250
28         DATA DP1,DP2,DP3,DB1,DB2,DB3 / 0.5+2.0,5.0,50.+200.+500. /, HIST0260
29         DATA PLENT/5.5555555/, HIST0270
30         DATA NSYB,10/, HIST0280
31         DATA ((UTJ(I,J), J=1,7), I=1,10) /, HIST0290
32         1 4HLEN,4HUM,-4H COG,4HLANT,4H(TOP,4H) TE,4HMF, ., HIST0300
33         2 4HCOL,4HANT,4H(OUT,4H=IN),4H TEM,4HP,(CC,4H) ., HIST0310
34         3 4HINT,4HEHR,4H DEN,4HSITY,4H (FR,4HACTI,4HON), HIST0320
35         4 4H ELL,4HET S,4HFA,4HCE P,4HDUG,4HNESS,4H(C*) ., HIST0330
36         5 4HCLAD,4HMDING,4P ID ,4HRCG,4HNHES,4HS (CC,4H) ., HIST0340
37         6 4HMEAT,4H TRA,4HNSFE,4HK CO,4HEFF (,4HW,CM,4H2-C), HIST0350
38         7 2E8G /, HIST0360
39         DATA ((XFORMC(I,J), J=1,5), I=1,10) /, HIST0370
40         1 4H(1A,,4H7A4,,4H2X,,4H10F1,4H0,2), HIST0380
41         2 4H(1A,,4H7A4,,4H2X,,4H10F1,4H0,2), HIST0390
42         3 4H(1A,,4H7A4,,4H2X,,4H10F1,4H0,4), HIST0400
43         4 4H(1A,,4H7A4,,4H2X,,4H10E1,4H0,2), HIST0410
44         5 4H(1A,,4H7A4,,4H2X,,4H10E1,4H0,2), HIST0420
45         6 4H(1A,,4H7A4,,4H2X,,4H10E1,4H0,3), HIST0430
46         7 2U4D,0 /, HIST0440
47         C
48         DATA ((UTJ(I,J), J=1,5), I=1,10) /, HIST0450
49         1 4H(1A,,4H7A4,,4H2X,,4H10F1,4H0,2), HIST0460
50         2 4H(1A,,4H7A4,,4H2X,,4H10F1,4H0,2), HIST0470
51         3 4H(1A,,4H7A4,,4H2X,,4H10F1,4H0,4), HIST0480
52         4 4H(1A,,4H7A4,,4H2X,,4H10E1,4H0,2), HIST0490
53         5 4H(1A,,4H7A4,,4H2X,,4H10E1,4H0,2), HIST0500
54         6 4H(1A,,4H7A4,,4H2X,,4H10E1,4H0,3), HIST0510
55         7 2U4D,0 /, HIST0520
56         C
57         GO TO 100,1000+KS, HIST0530
58         100 CONTINUE, HIST0540
59         DO 1 J=1,100, HIST0550
60         DO 2 I=1,7, HIST0560
61         DO 3 I=1,7, HIST0570
62         DO 4 I=1,7, HIST0580
63         DO 5 I=1,7, HIST0590
64         DO 6 I=1,7, HIST0600
65         DO 7 I=1,7, HIST0610
66         DO 8 I=1,7, HIST0620
67         DO 9 I=1,7, HIST0630
68         DO 10 I=1,7, HIST0640
69         DO 11 I=1,7, HIST0650
70         DO 12 I=1,7, HIST0660
71         DO 13 I=1,7, HIST0670
72         DO 14 I=1,7, HIST0680
73         DO 15 I=1,7, HIST0690
74         DO 16 I=1,7, HIST0700
75         DO 17 I=1,7, HIST0710
76         DO 18 I=1,7, HIST0720
77         DO 19 I=1,7, HIST0730
78         DO 20 I=1,7, HIST0740
79         DO 21 I=1,7, HIST0750
80         DO 22 I=1,7, HIST0760
81         DO 23 I=1,7, HIST0770
82         DO 24 I=1,7, HIST0780
83         DO 25 I=1,7, HIST0790
84         DO 26 I=1,7, HIST0800
85         DO 27 I=1,7, HIST0810
86         DO 28 I=1,7, HIST0820
87         DO 29 I=1,7, HIST0830
88         DO 30 I=1,7, HIST0840
89         DO 31 I=1,7, HIST0850
90         DO 32 I=1,7, HIST0860
91         DO 33 I=1,7, HIST0870
92         DO 34 I=1,7, HIST0880
93         DO 35 I=1,7, HIST0890
94         DO 36 I=1,7, HIST0900
95         DO 37 I=1,7, HIST0910
96         DO 38 I=1,7, HIST0920
97         DO 39 I=1,7, HIST0930
98         DO 40 I=1,7, HIST0940
99         DO 41 I=1,7, HIST0950
100        DO 42 I=1,7, HIST0960
101        DO 43 I=1,7, HIST0970
102        DO 44 I=1,7, HIST0980
103        DO 45 I=1,7, HIST0990
104        DO 46 I=1,7, HIST1000
105        DO 47 I=1,7, HIST1010
106        DO 48 I=1,7, HIST1020
107        DO 49 I=1,7, HIST1030
108        DO 50 I=1,7, HIST1040
109        DO 51 I=1,7, HIST1050
110        DO 52 I=1,7, HIST1060
111        DO 53 I=1,7, HIST1070
112        DO 54 I=1,7, HIST1080
113        DO 55 I=1,7, HIST1090
114        DO 56 I=1,7, HIST1100
115        DO 57 I=1,7, HIST1110
116        DO 58 I=1,7, HIST1120
117        DO 59 I=1,7, HIST1130
118        DO 60 I=1,7, HIST1140
119        DO 61 I=1,7, HIST1150
120        DO 62 I=1,7, HIST1160
121        DO 63 I=1,7, HIST1170

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* SOURCE STATEMENT (HISTR) *

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30         2 HIS(I,J) = 0.0, HIST0590
31         DO 3 I=1,5, HIST0600
32         3 MODE(I,J) = 0, HIST0610
33         4 TS(J) = 4H, HIST0620
34         4 BASE(J) = 0.0, HIST0630
35         5 IH = JCASE = 0, HIST0640
36         5 IMAX=NNHIST, HIST0650
37         C----- HISTORY STEP GENERATION BY USING INPUTED HISTORY DATAS-----, HIST0660
38         C
39         IF(NHIST.EQ.0) GO TO 40, HIST0670
40         C..... BURNUP DEPEND HISTORY STEP, HIST0680
41         MAXS=MASTER+IMAX, HIST0690
42         DO 91 I=1,IMAX, HIST0700
43         IF(I.LT.1) GO TO 92, HIST0710
44         HIS(I,I)=HIST(I,I), HIST0720
45         91 HIS(I,I)=0.0, HIST0730
46         GO TO 93, HIST0740
47         92 HIS(I,I)=HIST(I,I) - HIST(I-1,I-1), HIST0750
48         93 CONTINUE, HIST0760
49         BASE(I,I)=HIST(I,I), HIST0770
50         DO 94 K=2,I, HIST0780
51         HIS(K,I)=HIST(K,I), HIST0790
52         94 HIS(K,I)=0.0, HIST0800
53         DO 95 K=1,5, HIST0810
54         MODE(K,I)=IPD(K,I), HIST0820
55         95 MODE(K,I)=IPD(K,I), HIST0830
56         IS(I,I)=2H**, HIST0840
57         91 CONTINUE, HIST0850
58         GO TO 99, HIST0860
59         C
60         C..... TIME DEPEND HISTORY STEP, HIST0870
61         90 CONTINUE, HIST0880
62         C..... INITIALISATION, HIST0890
63         BASE(1)=HIST(1,1), HIST0900
64         HIS(1,1)=0.0, HIST0910
65         BPOW(1)=HIST(2,1), HIST0920
66         DO 61 K=2,I, HIST0930
67         HIS(K,1)=HIST(K,1), HIST0940
68         DO 63 K=1,5, HIST0950
69         MODE(K,1)=IPD(K,1), HIST0960
70         IS(1)=2H*, HIST0970
71         C
72         T1=HIST(1,1), HIST0980
73         P1=HIST(2,1), HIST0990
74         JJ=1, HIST1000
75         C
76         GENERATE TIME DEPEND HISTORY STEP, HIST1010
77         DO 80 I=2,IMAX, HIST1020
78         T2=HIST(I,1), HIST1030
79         P2=HIST(2,1), HIST1040
80         DELT=T2-T1, HIST1050
81         DELP=P2-P1, HIST1060
82         INC=JNC=MNC=1, HIST1070
83         IF(ABS(DELT).LE.PINC) GO TO 85, HIST1080
84         INC=ABS(DELP)/PINC+1, HIST1090
85         MNC=INC, HIST1100
86         85 CONTINUE, HIST1110
87         IF(DELT.LE.DINC) GO TO 86, HIST1120
88         JNC=(DELT/DINC)+1, HIST1130
89         IF(JNC.GE.IINC) MNC=JNC, HIST1140
90

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* SOURCE STATEMENT (HISTR) *

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78      *6 CONTINUE
C..... LINEAR INTERPOLATE EACH OPERATION PARAMETER
79      DO 71 M=1,MNC
80      JJ=JJ+1
81      HIS(1,JJ)=DELT/FLOAT(MNC)
82      DO 73 K=2,7
83      HIS(K,JJ)=HIST(K,1)+C HIST(K,1)+HIST(K,II-1) /MNC + FLOAT(M)
84      73 CONTINUE
C..... BROW( ) IS THE AVERAGE LINEAR POWER FOR BURNUP CALCULATION
85      BROW(JJ)=(HIS(2,JJ)+HIS(2,JJ-1)) / 2.
C..... BASEY( ) IS THE TOTAL IRRADIATION TIME IN DAYS
86      BASE(JJ)=BASE(JJ-1)+HIS(1,JJ)
87      71 CONTINUE
C
88      DO 75 K=1,5
89      75 KUOE(K,JJ)=IPD(K,II)
90      IS(JJ)=2**4
C..... CORRECT INTERPOLATING ERROR FOR EACH VALUE AT NODAL POINT
91      IF(BASE(JJ).GE.T2) BASE(JJ)=T2
92      DO 79 K=2,7
93      IF(HIS(K,JJ).NE.HIST(K,II)) HIS(K,JJ)=HIST(K,II)
94      79 CONTINUE
95      TI=T2
96      P1=P2
C
97      70 CONTINUE
C
98      MASTER=JJ
99      MAXS=MASTER
100     49 CONTINUE
C----- HISTORY STEP GENERATION END -----
C
101     IF(LSPALE.0) GO TO 101
102     DO 102 J=1,ISPA
103     IF(NAMSP(1),LE.0,OK,NAMSP(1),GT,NSYB) *RITE(6,105) NAMSP(1)
104     IF(NAMSP(1),LE.0,OK,NAMSP(1),GT,NSYB) NAMSP(1) = 0
105     102 CONTINUE
106     105 FORMAT(5X,5(1H*)+28H SPARE OPTION ERROR NO.**.12)
107     101 CONTINUE
C
108     WRITE(6,*100)
109     WRITE(6,*100) TITLE
C
C     HISTORY STEP PRINT OUT
C
110     IF(NHIST.EQ.1) GO TO 51
111     WRITE(6,*60003)
112     DO 600 J=1,MAXS
113     DUM5=BASE(J)*24.
114     DUM6=1511,J*24.
115     DUM2 = HIS(2,J) * 30.48 / 1000.
116     DUM3 = HIS(3,J) * 1.8 + 32.0
117     DUM4 = HIS(4,J) * 14.22
118     WRITE(6,*100) J,IS(J),BASE(J),DUM5,HIS(1,J),DUM6,HIS(2,J),DUM2,
1           1          HIS(3,J),DUM3,HIS(4,J),DUM4,(MODE(IM,J),IM=1,5)
119     IF(MOD(J,40).NE.0) GO TO 600
120     WRITE(6,*100)
121     WRITE(6,*6000)
122     690 CONTINUE

```

* SOURCE STATEMENT (HISTR) *

```

123     GO TO 52
124     51 CONTINUE
125     WRITE(6,*7000)
126     DO 700 J=1,MAXS
127     DUM5=3*SEL(J)/1000. * 3.37E19
128     DUM6=HIS(1,J)/1000.*3.37E19
129     DUM2=HIS(2,J) * 30.48 / 1000.
130     DUM3=HIS(3,J) * 1.8 + 32.
131     DUM4=HIS(4,J) * 14.22
132     WRITE(6,*100) J,IS(J),BASE(J),DUM5,HIS(1,J),DUM6,HIS(2,J),DUM2,
1           1          HIS(3,J),DUM3,HIS(4,J),DUM4,(MODE(IM,J),IM=1,5)
133     700 CONTINUE
C
134     52 CONTINUE
C
135     WRITE(6,*6002)
C
136     IF(IPEAK) 31,31,32
137     31 WRITE(6,*6003)
138     GO TO 33
139     32 WRITE(6,*6004)
140     33 CONTINUE
141     WRITE(6,*6005)
C
142     IF(LSPAL.EQ.0) GO TO 109
143     WRITE(6,*8000)
144     DO 113 K=1,MAXS+10
145     K1=K+9
146     IF(K1.GE.MAXS) K1=MAXS
147     WRITE(6,*8001) (KK,KK=K,K1)
148     IF(NHIST.EQ.0) 114,115
149     114 WRITE(6,*6002), (BASE(KK),KK=K,K1)
150     GO TO 116
151     115 WRITE(6,*8003) (BASE(KK),KK=K,K1)
152     116 CONTINUE
C
153     DO 117 I=1,ISPA
154     I1=NAMSP(1)
155     IF(I1.LE.0) GO TO 117
156     DO 118 J=1,5
157     118 FORM(J)=XFORM(I1,J)
158     PRINT FORM,(JT(J),J=1,7),(HIS(1+4,KK),KK=K,K1)
159     117 CONTINUE
160     113 CONTINUE
C
161     109 CONTINUE
C
162     RETURN
C
163     1000 CONTINUE
C
164     I1H = JCASE = JCASE + 1
165     LCOUNT = 0
166     NEXT = 4H
167     IF(I1H.GT.MXSTEP) NEXT = 4HNEXT
168     IF(I1H.GT.MXSTEP) RETURN
C
169     IF(NHIST.EQ.1) GO TO 53
170     TDAYS = HIS(1,I1H)

```

* SOURCE STATEMENT (HISTR) 2*

```

      C *****
171      TOTLDY=BASE(1)H)
172      APOVER=BP04(1)H)
173      GO TO 477
174      53 CONTINUE
175      BURNUP=BHS(1,1)H)
176      TCTBURB=BASE(1)H)
177      477 CONTINUE
178      IF((PEAK.LE.0) GO TO 472
179      PAVRG = HIS(2,1)H)
180      GO TO 474
181      472 PKPOWER = HIS(2,1)H)
182      474 CONTINUE
183      IF((HIS3,1)H).LE.0.) GO TO 475
184      TINLET = HIS(3,1)H)
185      475 IF(HIS4,1)H).LE.0.) GO TO 476
186      EXTP = HIS(4,1)H)
187      LCOUNT = 1
188      476 CONTINUE
      C
      **** DATA SET BY USING SPARE OPTION
189      IF((SPA,LE.0) GO TO 490
190      DO 491 I=1,ISHA
191      I11=NAMSP(I)
192      IF((I11,LE.0) GO TO 491
193      LL=+1
194      IF((I11,EG,1) GO TO 19
      C PLENUM TEMPERATURE MODEL IF PLENT=-1 ,GAS CONDUCTION
      C PLENUM TEMPERATURE MODEL IF PLENT=-2 ,GAS NATURAL CONVECTION
195      IF((I11,EU,2) GO TO 19
      C... ITL,EV,2 COOLANT OUTLET-INLET TEMPERATURE (DTEMP=0.0 IS PROBABLE)
196      IF((HISLL,1)H).LE.0.0) GO TO 491
197      19 CONTINUE
      C
198      GO TO (20+I11+22,23+24+25+26+27+28+29) + 11
199      26 PLENT=HIS(LL,1)H)
200      GO TO 491
201      21 DTEMP=HIS(LL,1)H)
202      GO TO 491
203      22 FRSIN=HIS(LL,1)H)
204      GO TO 491
205      23 ROUN=HIS(LL,1)H)
206      GO TO 491
207      24 ROUNC=HIS(LL,1)H)
208      GO TO 491
209      25 CONTINUE
210      IF((HISLL,1)H).LE.0.0) GO TO 491
211      SIGNR = HIS(LL,1)H)
212      GO TO 491
213      26 CONTINUE
214      27 CONTINUE
215      28 CONTINUE
216      29 CONTINUE
217      491 CONTINUE
218      490 CONTINUE
      C
219      IF(PLENT,LE.0.) CALL TEMPP1(TPLENA,PLENT,1)H)
220      IF(PLENT,LE.0) RETURN
      C

```

* SOURCE STATEMENT (HISTR) 2*

```

221      TPLENA=TINLET+DTEMP+PLENT+273.
222      IF((PEAK,GT,0) GO TO 501
223      IF((PKFCARL,E,0.0) TPLENA=TINLET+DTEMP+273.0
224      GO TO 502
225      501 IF((PAVGGLS,0.0) TPLENA=TINLET+DTEMP+273.0
226      502 CONTINUE
      C
227      RETURN
      C * 1 * 2 * 3 * 4 * 5 * 6 * 7
228      6000 FORMAT(//,
1 43X,39(1H*)/45X,35HH I S T O R Y D A T A /
2 43X,39(1H*) //
3 8X,54H TIME IRRADIATION TIME TIME INTERVALS LINEAR
4 54H HEAT RATE COOLANT INLET COOLANT PRESSURE
A .20H OPERATION MODE /
5 8X,4H STEP,63X,11H TEMPERATURE,29X,20H INPUT CONTROL SIGN /HIST3050
E 6X,5D NO. (WAYS) (HOURS) (DAYS) (HOURS) (*/CM) /HIST3060
7 4B(KW/FT) (DEG C) (DEG F) (KG/CM2) (PSI) /HIST3070
B .4X,20H (1) (2) (3) (4) (5) /
8 8X,4(1H*),3X,5(1H*),4X,20(1H*) / /HIST3090
229 6100 FORMAT(8X,(4+1X,A2,2(F8.3,14X),2(F8.3,4X),2F6+2+4X,514) / /HIST3100
230 6004 FORMAT(/5X,31H,,NOTE..,(**) IS INPUT DATA ) /HIST3110
231 6003 FORMAT(1H*,55X,12H(CHEAP POWER) ) /HIST3120
232 6004 FORMAT(1H*,55X,15H(AVERAGE POWER) ) /HIST3130
233 6005 FORMAT(5X,14H(TEMPERATURE MODE / 5X,14(1H*) / /HIST3140
1 5X,124H(10) TEMPERATURE PROFILE PRINT-OUT OPTION *0 NOT PRINTED HIST3150
2*1 DETAIL PROFILE PRINT = 2 PLOT PROFILE BY LINE PRINTER HIST3160
3/5X,124H(12) FUEL THERMAL CONDUCTIVITY CONTROLLER =0 NOT CHANGE HIST3170
4=N-N TH DATA READ-IN --N USE PREPARATED EQUATION HIST3180
5/5X,124H(3) CLADDING PROPERTY CONTROLLER =0 NOT CHANGE HIST3190
6=N-N TH DATA READ-IN --N USE PREPARATED TABLE(ZRY2,ZRY4,1ST) HIST3200
7/5X,124H(4) RADIAL FLUX DEPRESSION CONTROLLER =0 NOT CHANGE HIST3210
8=N-N TH DATA READ-IN --I USE SUBROUTINE DLPRES HIST3220
9/5X,120H(5) AXIAL POWER PROFILE CONTROLLER =0 NOT CHANGE HIST3230
A=1 NEW POWER DISTRIBUTION DATA READ-IN > HIST3240
234 7000 FORMAT(1H1 //,
1 43X,39(1H*)/45X,35HH I S T O R Y D A T A /
2 43X,39(1H*) //
3 8X,54H TIME BURNUP BURNUP INCREMENT LINEAR
4 54H HEAT RATE COOLANT COOLANT PRESSURE
A .20H OPERATION MODE / .8X,4H STEP,3X,38H(MWD) /FISSIONS /HIST3300
5MWD / (FISSIONS,23X,11H TEMPERATURE,31X,18H INPUT CONTROL SIGN / HIST3310
6 8X,55HNO. (MTU) (/CC) (MTU) (/CC) (W/CM) /HIST3320
7 4B(KW/FT) (DEG C) (DEG F) (KG/CM2) (PSI) /HIST3330
B .4X,20H (1) (2) (3) (4) (5) /
8 8X,4(1H*),3X,2(18(1H*),2X), 3(16(1H*),4X),20(1H*) / /HIST3350
235 7100 FORMAT(8X,(4+1X,A2,(F7.1,E11.3,2X),2(2F8.3,4X),2F8,2, 4X,514) / /HIST3370
236 8000 FORMAT(/5X,40H SPECIAL HISTORICAL DATA (USER,S OPTION) /) /HIST3380
237 8001 FORMAT(/ 1X,20H HISTORY STEP NO. ,10X,10(5X,13,X) ) /HIST3390
238 8002 FORMAT( 1X,30H IRRADIATION TIME (DAYS) ,10F10.2 ) /HIST3400
239 8003 FORMAT( 1X,30H BURNUP (MWD/MT) ,10F10.1 / ) /HIST3410
      C
240 6010 FORMAT(1H1)
241 9000 FORMAT(///20X,100(1H*),/ 20X,1H*,98X,1H* / 20X,1H*,9X,20A4+9X,1H*) /HIST3431
242      1 / 20X,1H*,98X,1H* / 20X,100(1H*) / /HIST3432
      C

```

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* SOURCE STATEMENT *

```
1      SUBROUTINE HTCLM(HF,TCOOLF,DE+V)          HTCM0010
C                                              HTCM0020
C THIS SUBROUTINE IS CALLED FROM STEP 3          HTCM0030
C REFER BNWL-1778, GAPCON THERMAL-1, APPENDIX(A-1) HTCM0040
C CLADDING-TO-COOLANT HEAT TRANSFER COEFFICIENT OF SODIUM HTCM0050
C                                              HTCM0060
C HF = HEAT TRANSFER COEFFICIENT IN W/CM2/C          HTCM0070
C HFF= HEAT TRANSFER COEFFICIENT IN BTU/FT2/HR/F        HTCM0080
C TCOOLC = COOLANT TEMPERATURE IN C                  HTCM0090
C DE = EQUIVALENT HYDRAULIC DIAMETER IN CM          HTCM0100
C V = COOLANT VELOCITY IN CM/SEC                   HTCM0110
C DEF = DE/30.48                                     HTCM0120
2      TCOOL = TCOOLF                                 HTCM0130
3      VF = V /30.48 *3600.0                          HTCM0140
4      CNA=54.306-1.67E-2*TCOOL+2.6914E-6*TCOOL**2    HTCM0150
5      RHOA=59.566-7.9504E-3*TCOOL-.2872E-6*TCOOL**2 +.06035E-9*TCOOL**3HTCM0160
6      CPNA=.34574-.79226E-4*TCOOL+.34056E-7*TCOOL**2   HTCM0170
7      HFF = CNA/DEF*(7.+.025*(DEF*VF*RHOA*CPNA/CNA)**(.8)) HTCM0180
8      HF = HFF * 5.67E-4                            HTCM0190
9      RETURN                                         HTCM0200
10     *****                                         HTCM0210
11     END                                           HTCM0220
```

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* SOURCE STATEMENT *

```

1 SUBROUTINE HTCWCKS,T,FLUX,V,D,H,TW,EXTH,TSAT)
2
3 C THIS SUBROUTINE IS CALLED FROM STEP 3
4 C CLADDING-TO-COOLANT HEAT TRANSFER COEFFICIENT OF WATER
5 C
6 C KS=1...DITTS BOELTER (D=929). KS=2...JENS LOTTES (D=526)
7 C KS=3... SUSCOLD=DITTS BOELTER + BOILING--JENS LOTTES
8 C
9 C COMMON /SVTUM/ LCOUNT
10 C DIMENSION TTTCB(2,37)
11 C DIMENSION OF TTTCB(I,J) IS      (SEC**0.8)*(CM**0.2)*(WATT) /
12 C                                     (M **0.8)*(CM**2)   *(DEGC)
13 C
14 C DATA ((TTTB(I,J),I=1,2),J=1,37) /
15 C * 0.,0.,375, 10.,0.,428, 20.,0.,471, 30.,0.,533, 40.,0.,582,
16 C * 50.,0.,631, 60.,0.,678, 70.,0.,720, 80.,0.,760, 90.,0.,797,
17 C *100.,0.,831, 110.,0.,864, 120.,0.,896, 130.,0.,925, 140.,0.,950,
18 C *150.,0.,972, 160.,0.,989, 170.,0.,1004, 180.,0.,1016, 190.,0.,1028,
19 C *200.,1.,038, 210.,1.,044, 220.,1.,049, 230.,1.,052, 240.,1.,055,
20 C *250.,1.,056, 260.,1.,054, 270.,1.,051, 280.,1.,047, 290.,1.,040,
21 C *300.,1.,032, 310.,1.,024, 320.,1.,021, 330.,1.,026, 340.,1.,046,
22 C *350.,1.,107, 360.,1.,255
23 C
24 C DATA W1#W2#W3#W4#W5#W6#W7#W8#W9
25 C 1 / 147.40, 411932, -0.0591875.7595E-4, -1.5756E-6, -1.2442E-8,
2 1.2722E-10, -4.803E-13, 4.3416E-16 /
26 C DATA LCOUNT/0/
27 C
28 C   T = COOLANT TEMPERATURE, C
29 C   FLUX = HEAT FLUX, W/CM2
30 C   V = COOLANT VELOCITY, M/SEC
31 C   D = EQUIVALENT HYDRAULIC DIAMETER CM
32 C   H = HEAT TRANSFER COEFFICIENT, W/CM2/C
33 C   TW = TEMPERATURE AT CLADDING OO,
34 C   TSAT = SATURATION TEMPERATURE OF COOLANT PRESSURE (EXTH)
35 C
36 C   IF(LCOUNT.LE.0) GO TO 111
37 C   P=EXP(1)
38 C   . . . . . TSAT = WATER SATURATION TEMPERATURE IN DEG C
39 C   TSAT=1+P*(W2#P*(K3#P*(K4#P*(K5#P*(K6#P*(K7#P*(W8#P#W9)))))))
40 C
41 C   111 CONTINUE
42 C   GO TO (1111,2222,3333,4444,5555 ) ,KS
43 C   3333 CONTINUE
44 C   IF(T,GE,TSAT) GO TO 2222
45 C   1111 CONTINUE
46 C   ITRY = 0
47 C   TPI = 7
48 C   G=V**0.8/D**0.2
49 C
50 C   6 CONTINUE
51 C   IN1 = 2
52 C   IN2 = 37
53 C   S = TERP(TF1,TTTB,2,37,IN1,IN2,IN3,99)
54 C   IN3=0
55 C
56 C   TH = T + FLUX/VH
57 C   TF = (TA + TH) / 2.
58 C   DIFF = ABS(TF - TF1)
59 C   IF( DIFF > 2.0) 1,1,2
60 C   2 ITRY = ITRY + 1
61 C   IFC ITRY=500 3,3,4
62 C
63 C   SUBROUTINE HTCWCKS,T,FLUX,V,D,H,TW,EXTH,TSAT)
64 C THIS SUBROUTINE IS CALLED FROM STEP 3
65 C CLADDING-TO-COOLANT HEAT TRANSFER COEFFICIENT OF WATER
66 C
67 C KS=1...DITTS BOELTER (D=929). KS=2...JENS LOTTES (D=526)
68 C KS=3... SUSCOLD=DITTS BOELTER + BOILING--JENS LOTTES
69 C
70 C COMMON /SVTUM/ LCOUNT
71 C DIMENSION TTTCB(2,37)
72 C DIMENSION OF TTTCB(I,J) IS      (SEC**0.8)*(CM**0.2)*(WATT) /
73 C                                     (M **0.8)*(CM**2)   *(DEGC)
74 C
75 C DATA ((TTTB(I,J),I=1,2),J=1,37) /
76 C * 0.,0.,375, 10.,0.,428, 20.,0.,471, 30.,0.,533, 40.,0.,582,
77 C * 50.,0.,631, 60.,0.,678, 70.,0.,720, 80.,0.,760, 90.,0.,797,
78 C *100.,0.,831, 110.,0.,864, 120.,0.,896, 130.,0.,925, 140.,0.,950,
79 C *150.,0.,972, 160.,0.,989, 170.,0.,1004, 180.,0.,1016, 190.,0.,1028,
80 C *200.,1.,038, 210.,1.,044, 220.,1.,049, 230.,1.,052, 240.,1.,055,
81 C *250.,1.,056, 260.,1.,054, 270.,1.,051, 280.,1.,047, 290.,1.,040,
82 C *300.,1.,032, 310.,1.,024, 320.,1.,021, 330.,1.,026, 340.,1.,046,
83 C *350.,1.,107, 360.,1.,255
84 C
85 C DATA W1#W2#W3#W4#W5#W6#W7#W8#W9
86 C 1 / 147.40, 411932, -0.0591875.7595E-4, -1.5756E-6, -1.2442E-8,
87 C 1.2722E-10, -4.803E-13, 4.3416E-16 /
88 C DATA LCOUNT/0/
89 C
90 C   T = COOLANT TEMPERATURE, C
91 C   FLUX = HEAT FLUX, W/CM2
92 C   V = COOLANT VELOCITY, M/SEC
93 C   D = EQUIVALENT HYDRAULIC DIAMETER CM
94 C   H = HEAT TRANSFER COEFFICIENT, W/CM2/C
95 C   TW = TEMPERATURE AT CLADDING OO,
96 C   TSAT = SATURATION TEMPERATURE OF COOLANT PRESSURE (EXTH)
97 C
98 C   IF(LCOUNT.LE.0) GO TO 111
99 C   P=EXP(1)
100 C   . . . . . TSAT = WATER SATURATION TEMPERATURE IN DEG C
101 C   TSAT=1+P*(W2#P*(K3#P*(K4#P*(K5#P*(K6#P*(K7#P*(W8#P#W9)))))))
102 C
103 C   111 CONTINUE
104 C   GO TO (1111,2222,3333,4444,5555 ) ,KS
105 C   3333 CONTINUE
106 C   IF(T,GE,TSAT) GO TO 2222
107 C   1111 CONTINUE
108 C   ITRY = 0
109 C   TPI = 7
110 C   G=V**0.8/D**0.2
111 C
112 C   6 CONTINUE
113 C   IN1 = 2
114 C   IN2 = 37
115 C   S = TERP(TF1,TTTB,2,37,IN1,IN2,IN3,99)
116 C   IN3=0
117 C
118 C   TH = T + FLUX/VH
119 C   TF = (TA + TH) / 2.
120 C   DIFF = ABS(TF - TF1)
121 C   IF( DIFF > 2.0) 1,1,2
122 C   2 ITRY = ITRY + 1
123 C   IFC ITRY=500 3,3,4

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* SOURCE STATEMENT CTCX *

```

29   3 T=1 = (CTF+1F1D)/2.
30   GO TO 6
31   4 WRITE(6,600)
32   1 CONTINUE
33   IF (TW.LE.T) TW=T
34   GO TO 9999
35 2222 CONTINUE
C      QDVRAC IS HEAT FLUX (KATT/CM2) + NOA CHANGE TO HFLEX (KCAL/M2-HR)
C
C      HFLEX = FLUX + B600.
36   HF = 1.22*(HFLEX**0.75)*EXP(EXP1/63.3)
37   H = HF/8600.
38   IF (H.LE.0.02) TW = 7
39   IF (H.LE.0.01) RETURN
40   TSAT = FLUX / H
41   TW = TSAT + FLUX / H
42   IF (TW.LE.T) TW=T
43   GO TO 9999
44 4444 CONTINUE
C----- TOM'S CORRELATION
C      FLUX (n/cm2) CONVERT TO (BTU/HR-FT2)          3170.
C      PRESSURE (KG/CM2)    TU (PSIA)                14.22
C
C      FLX = FLUX*3170.
45   P = EXP1*14.22
46   HF = (1/10.072)*EXP(P/1260.)*FLX**0.5
47   H = HF*.677E-4
48   IF (H.LE.0.0) TW=T
49   GO TO 9999
50 5555 CONTINUE
51 9999 CONTINUE
52      ITEMP = 0
53      IF (TW.GT.500.) ITEMP = 500
54      IF (TW.GT.1200.) ITEMP = 1200
55      IF (ITEMP.GT.0) WRITE(6,610) ITEMP,TW+T,V,FLUX,D,H
56      IF (ITEMP.EQ.1200) STOP
57      RETURN
58
59      *      1      *      2      *      3      *      4      *      5      *      6      *      7
60 600 FORMAT(10A, 'NO CONVERGENCE, ITERATION TIME IS 50TIMES OVER
      1      FROM HTCW')
610 FORMAT(//7X,
      1      50H**** CAUTION ***      CLADDING SURFACE TEMPERATURE IS: 15.,
      2      33H DEGC OVER           SURFACE TEMP.:= E12.5, 6H DEGC//7X,
      3      30H COOLANT TEMPERATURE ((TCOOL)=,E12.5,20HDEG-C, COOLANT VEL: E12.5,
      4      30H(OCITY) (V),E12.5+26HN/SEC, HEAT FLUX(QDVRAC)=,E12.5,
      5      30HWC/CM2,                                //7X,
      6      30H(EQUIVALENT HYDRAULIC DIA,(DE)=,E12.5,20HCM, HEAT TRANSFER C: E12.5,
      7      10HGEFF,(HF)=,E12.5+30HW/CM2=C, . . . ,SUBROUTINE HTCW
      ****
      END

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* SOURCE STATEMENT *

```
1      SUBROUTINE HYOSHI          HYOS0010
2      COMMON /HTLUKE/ K1,K2,K3,K4,K5,K6          HYOS0020
3      WRITE(6,10)          HYOS0030
4      WRITE(6,20)          HYOS0040
5      WRITE(6,30)          HYOS0050
6      WRITE(6,20)          HYOS0060
7      WRITE(6,40) K1,K2,K3,K4          HYOS0070
8      WRITE(6,60)          HYOS0080
9      10 FORMAT(1H1/)          HYOS0090
10     20 FORMAT(40X,55(1H*))          HYOS0100
11     30 FORMAT(40X,1H*,53X,1H* / 40X,1H*,53X,1H* /          HYOS0110
12        1 40X,55H*          HYOS0120
13        2 40X,55H*          HYOS0130
14        3 40X,55H*          HYOS0140
15        4 40X,55H*          TIME DEPENDENT PELLET-CLADDING GAP CONDUCTANCE
16        5 40X,55H*          ANALYSIS COMPUTER PROGRAM          * / HYOS0150
17        6 40X,55H*          * / HYOS0160
18        7 40X,55H*          * / HYOS0170
19        8 40X,55H*          * / HYOS0180
20        9 40X,55H*          * / HYOS0190
21        A 40X,55H*          * / HYOS0200
22        B 40X,55H*          * / HYOS0210
23        C 40X,55H*          * / HYOS0220
24        D 40X,55H*          * / HYOS0230
25        E 40X,55H*          * / HYOS0240
26      JAERI          DIVISION OF REACTOR SAFETY
27      FUEL RELIABILITY LABORATORY-1          * / HYOS0250
28      40 FORMAT(//40X,1D-HRUN DATE...,2X,2A4,15,3H HR,13,7H MINUTE
29      50 FORMAT(/ 40X,1DHTITLE.....,2X,20A4)          * / HYOS0260
30      60 FORMAT(// 7X,10H***NOTE*** )          * / HYOS0270
31      RETURN          * / HYOS0280
32      END          > HYOS0290
33      * / HYOS0300
34      * / HYOS0310
35      * / HYOS0320
36      * / HYOS0330
```

* SOURCE STATEMENT *

```

1      SUBROUTINE MOLMOL(KS)
C
C      THIS SUBROUTINE IS CALLED FROM MAIN (KS=1,2,5)
C          AND ST3TOB (KS=3,4)
C
C
2      REAL MUFI,MOL,MOLEFR,MOLFR
3      COMMON /FFMOL/ FF(6,23),RKR(6,23),RXE(6,23),AKX(10,20,2)
4      COMMON /IXIR/ IX,IR,IH,MAXIEP
5      COMMON /MLPRI/ GMOL(1),GHOLR(6),FRACTN(6),MOL(6),XMOLS(21)
6      COMMON /MATMOL/ TAVG,VOLTXS
7      COMMON /POWRAY/ PAVRG,FUEL,L,POWER(21),A1(21),NPWR,PTOT,EPMAX,
8          PKPOWER,IPEAK,DELPH,PMAX
9      COMMON /BRNGAS/ AKR(20),AXE(20),PH(20),ENKE(20),ENKR(20)
10     COMMON /MUL676/ MULEFR(6)
11     COMMON /MUL593B/ TEAR(20)
12     COMMON /MUL579/ PRESTO(20)
13     COMMON /MOLM9/ TAVGXX(20)
14     COMMON /ML338/ VCLTX(20)
15     COMMON /DATA 3/ VOLAT(29)*FISGR(29)
16     COMMON /DATA 4/ PI+CCPIN3,SECDAY,AVUGAD,RR+CONEN
17     COMMON /COM 02/ IPW,ISTEP,ITER,COUNT
18     COMMON /COM 03/ TD,P,DELRCC,DELRG,DELRH,TCOOL,STP
19     COMMON /COM 05/ BURNUP,TDAYS,VVOID,TOTLDY,TOTBUR
20     COMMON /COM 07/ !,JCASE,TCOOLF,XHOTOT
21     COMMON /COM 11/ VVODIZ,FPU02,IPLEN,IPW1
22     COMMON /COM 13/ RF5,FNPW,RSTINZ,RVOIDZ
23     COMMON /COM 046/ USIN,RSTIN,TSIN,TSINC,DV010,RVOID,T
24     COMMON /COM 36/ VOLGH,VOLGP
25     COMMON /COM 90/ VOLGAS,WNGC
26     COMMON /COM 566/ DELPR,DELRP,DELCI,DELR,TAvgF,VAVGT
27     COMMON /COM 678/ TOTMOL,ABTAS,VISMIA,GK,GASKON
28     COMMON /NEAGAS/ NGAS
29     COMMON /INPUT/ FROEN,FRHSIN,DSINZ,FRPI02,FH35,FH40,FR41,DFS,DCI,
30         DCU,DVCI02,VPLENZ,ATMUS,S,XX,ROUF,ROUC,EXTP,DE,V,
31         TINLET,DELT,TMAX,TR,TM,DBU,B,HBC,SIGHF,!FLUX,
32         INCLAD,INCH4NFLX,ROOL,NEWK,NEWL,NEWFLX,VOIDZ,NOH,
33         FRACHE,FRACAH,FRACH,FRACN,FRACKP,FRACAE,HGACEL,
34         DIEMP,ZCLAD,HG,PEKAVG,MINI,ICDF,ISTDR,ICREP,ISWELL,
35         MOLM0410
36         MOLM0420
37         MOLM0430
38         MOLM0440
39         MOLM0450
40         MOLM0460
41         MOLM0470
42         MOLM0480
43         MOLM0490
44         MOLM0500
45         MOLM0510
46         MOLM0520
47         MOLM0530
48         MOLM0540
49         MOLM0550
50         MOLM0560
51         MOLM0570
52         MOLM0580
53         MOLM0590
54
55 DATA FACTFT / 1.0 /
56 ****
57 GO TO 100,200,300,400,500 +KS
58 100 CONTINUE
59 SIP#273/2SB.
60
61 C      SETUP PLenum MOle Content.
62
63 XMOLS(NPWR) = SIP#VPLENZ*ATMUS/PR

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* SOURCE STATEMENT (MOLMOL) *

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C
42      DO 710 J=1,23
43      FF(1,J) = RKR(1,J) + AXE(1,J) * S,0
44      DO 711 I=1,NPWR
45      FF(I,J)=ATC(I)=0,0
46      711 CONTINUE
47      RETURN
48
49 2.00 CONTINUE
50      ANKR = AXE = AVKR = AXE = GTMKR = GTMXE = RRKR = RRXE = 0,0
51      IAMODU(1,1)=0
52      IF((IX,ES,1) .EQ. 1) IX=IP
53      DO 20 IPW=1,NPWR
54      P=(PWRK(IPW)+PWER(IPW+1))*0.5
55
56      MTIME = 1
57      IF((IH,ES,1) .EQ. 1) MTIME = 0
58      FISSION GAS GENERATION CALC, AKR( ),AXE( ) CALL FISGAS
59      T = TDAYS * SECDAY
60      CALL FISGAS (T,PH(IPW),F,CONEN,IFLUX,MTIME,AKR(IPW),AXE(IPW),
61                  *           IPW )
62      ANKR=ANKR+AKR(IPW)
63      ANAE=ANAE+AXE(IPW)
64      ANER=ANER+AVUGAD/FLOAT(IPW)+FUEL
65      AVXE=AVXE+AVUGAD/FLOAT(IPW)*FUEL
66      AKA(1,1,IPW+1) = AKR(IPW)
67      AKA(1,1,IPW+2) = AXE(IPW)
68      FNV(TIPW) = FNV(TIPW) + PH(IPW)*T*FACTFT
69      TNVT(TIPW) = TNVT(TIPW) + PH(IPW)*T
70
71 20 CONTINUE
72      DO 720 I=2,6
73      DO 720 J=1,23
74      FF(I,J) = RKR(1,J) + AXE(1,J) * S,0
75      RETURN
76
77 300 CONTINUE
78
79 C      INTERPOLATE FISSION GAS RELEASE TABLE ON VOL, AVG. TEMP,
80
81 C      TVOLAV=VAVGT
82 C      IF(ISTEP.GT.1) GO TO 1030
83 C      F=TEPF(VOLAV,FISGR,VOLAT,29)
84 C      RDCT(IPW)=F
85 C      RU=RDCT(IPW)
86 C      IF(MDEN.GE.1.AND.MGAS.EQ.-1) RD=DENSFL(1,IPW)/0.03
87
88 C      CALCULATE GAS COMPOSITION
89
90      FILMOL=STP*VOLGAS*           ATMOS/PR
91      MOL(1)=FILMOL*FRACHE
92      MOL(2)=FILMOL*FRACAR
93      MOL(3)=FILMOL*FRACH+*S*XX*FL/RR*RD
94      IF(NOH.GT.0) MOL(3)=0
95      MOL(4)=FILMOL*FRACKR+AKR(IPW)/AVUGAD*FL*RDCT(IPW)
96      MOL(5)=FILMOL*FRACAE*AXE(IPW)/AVUGAD*FL*RDCT(IPW)
97      MOL(6)=FILMOL*FRACAE*AXE(IPW)
98
99 C      CALCULATE MOLE FRACTIONS OF GAS IN THE FUEL PIN.

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* SOURCE STATEMENT (MOLMOL) *

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86      XMOLS(IPOW)=0.0                                MOLM1190
87      DO 1010 I=1,6                                MOLM1200
88      XMOLS(IPOW)=XMOLS(IPOW)+MOL(I)             MOLM1210
89  1010  CONTINUE                                     MOLM1220
90      DO 1020 I=1,6                                MOLM1230
C      XMOL(I,IPOW)=MOL(I)/XMOLS(IPOW)           MOLM1240
C      MOLEFR(I)=XMOL(I,IPOW)                      MOLM1250
91      MOLEFR(I)=MOL(I)/XMOLS(IPOW)              MOLM1260
92  1020  CONTINUE                                     MOLM1270
93  1030  CONTINUE                                     MOLM1280
94      TOTMOL=XMOLS(IPOW)                         MOLM1290
C      RETURN TO BETWEEN STEPS AND STEP6            MOLM1300
95      RETURN                                         MOLM1310
C      =====
C      400 CONTINUE                                     MOLM1320
96      IST1 = ISTEP + 1                            MOLM1330
97      FFS = RKRS = RXES = 0.0                      MOLM1340
98      FFD=0.0                                       MOLM1350
100     DO 1372 IPOW = 1,NH0W                      MOLM1360
101     FF(ISTEP+1,IPOW) = TEPP(TBAR(IPOW),FISGR,VOLAT+29) MOLM1370
102     FF(ISTEP+1,21) = FF(ISTEP+1,21) + FF(ISTEP+1,IPOW) MOLM1380
103     RKRC(ISTEP+1,IPOW) = AKR(IPOW) + FF(ISTEP+1,IPOW) MOLM1390
104     RXE(ISTEP+1,IPOW) = AXE(IPOW) + FF(ISTEP+1,IPOW) MOLM1400
105     RKH(IST1,21)=RKH(IST1,21) + RKRC(IST1,IPOW)        MOLM1410
106     RXE(IST1,21)=RXE(IST1,21) + RXE(IST1,IPOW)        MOLM1420
107     RKH(IST1,IPOW)=RKH(IST1,IPOW) + RXE(IST1,IPOW)    MOLM1430
108     RXE(IST1,IPOW)=RXE(IST1,IPOW) + RXE(IST1,IPOW)    MOLM1440
109     RXEMAX(IPOW) = RXE(1,IPOW)                   MOLM1450
110     RKMAX(IPOW) = RKRC(1,IPOW)                  MOLM1460
111     IF(FF(IST1,IPOW).GT.FF(1,IPOW)) FFMAX(IPOW)=FF(IST1,IPOW) MOLM1470
112     IF(RKH(IST1,IPOW).GT.RKH(1,IPOW)) RKMAX(IPOW)=RKH(IST1,IPOW) MOLM1480
113     IF(RXE(IST1,IPOW).GT.RXE(1,IPOW)) RXEMAX(IPOW)=RXE(IST1,IPOW) MOLM1490
114     FFS = FFS + FFMAX(IPOW)                      MOLM1500
115     RKRS = RKRS + RKMAX(IPOW)                  MOLM1510
116     RXES = RXES + RXEMAX(IPOW)                MOLM1520
117     FFD=FFD+ENSFL(1,IPOW)/0.03                 MOLM1530
118  1372  CONTINUE                                     MOLM1540
119     FFMAX(21) = FFS                           MOLM1550
120     RKMAX(21) = RKRS                         MOLM1560
121     RXEMAX(21) = RXES                         MOLM1570
122     FFMAX(22) = FFS /FNPOW                     MOLM1580
123     FFD=FFD/FNPOW                           MOLM1590
124     IF(MDN,GE,1,AND,MDAS,EQ,1) FD=FFD          MOLM1600
125     RKMAX(22) = RKRS /FNPOW                   MOLM1610
126     RXEMAX(22) = RXES /FNPOW                  MOLM1620
127     FF(IST1,22)=FF(IST1,21)/FNPOW            MOLM1630
128     RKH(IST1,22)=RKH(IST1,21)/FNPOW          MOLM1640
129     RXE(IST1,22)=RXE(IST1,21)/FNPOW          MOLM1650
130     ENTRY MOLM4D                               MOLM1660
131     TAVGXX(ISTEP+1)=TAVGX/FNPOW               MOLM1670
132     VOLTXS=VOLTXS+VPLEN/TPLENA               MOLM1680
133     TVOLAV = TAVGXX(ISTEP+1)                  MOLM1690
134     ----- CONTINUE OF SUB. MOLM04 (NEW GAS RELEASE CALCULATION) MOLM1700
135     -----
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* SOURCE STATEMENT (MOLMOL) *

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134     F=TEPP(TVOLAV,FISGR,VOLAT+29)             MOLM1780
135     FF(ISTEP+1,23) = F                         MOLM1790
C     CALCULATE GAS COMPOSITION
C
136     FILMOL=STH*(FNPOW*VOLGAS+VPLEN)          ATMOS/RR
137     MOL(1)=FILMOL*FRACHE                       MOLM1800
138     MOL(2)=FILMOL*FRACAR                       MOLM1810
139     MOL(3)=FILMOL*FRACH + W*S*XX*FUELL/RR*FD   MOLM1820
140     IF(NOH,GT,0) MOL(3)=0.0                     MOLM1830
141     MOL(4)=FILMOL*FRACN+W*S*(1.-XX)*FUELL/RR*FD MOLM1840
142     MOL(5)=FILMOL*FRACKR + RKMAX(22)/AVOGAD * FUELL MOLM1850
143     MOL(6)=FILMOL*FRACKE + RXEMAX(22)/AVOGAD * FUELL MOLM1860
C
144     GMOL(1)=FILMOL*FRACHE                      MOLM1870
145     GMOL(2)=FILMOL*FRACAR                      MOLM1880
146     GMOL(3)=FILMOL*FRACH                       MOLM1890
147     IF(NOH,GT,0) GMOL(3)=0.0                    MOLM1900
148     GMOL(4)=FILMOL*FRACN                        MOLM1910
149     GMOL(5)=FILMOL*FRACKR                      MOLM1920
150     GMOL(6)=FILMOL*FRACKE                      MOLM1930
C
151     GMOLR(1)=GMOL(2)=0.0                         MOLM1940
152     GMOLR(3)=W*S*XX*FUELL/RR*FD                 MOLM1950
153     IF(NOH,GT,0) GMOLR(3)=0.0                   MOLM1960
154     GMOLR(4)=W*S*(1.-XX)*FUELL/RR*FD           MOLM1970
155     GMOLR(5)=RKMAX(22)/AVOGAD*FUELL            MOLM1980
156     GMOLR(6)=RXEMAX(22)/AVOGAD*FUELL          MOLM1990
C
C     CALCULATE MOLE FRACTIONS OF GAS IN THE FUEL PIN.
C
157     XMOTOT=0                                      MOLM2000
158     DO 1380 I=1,6                                MOLM2010
159     XMOTOT=XMOTOT+MOL(I)                         MOLM2020
160  1380  CONTINUE                                     MOLM2030
161     DO 1390 I=1,6                                MOLM2040
162     MOLEFR(I)=MOL(I)/XMOTOT                      MOLM2050
163  1390  CONTINUE                                     MOLM2060
C
164     PRESTO(ISTEP+1)=84.80804*XMOTOT/VOLTXS       MOLM2070
165     XMOLS(IPOW)=PRESTO(ISTEP+1)*VPLEN/(84.80804*TPLENA) MOLM2080
166     DO 1400 I=1,IPOW                            MOLM2090
167     RROOT(I)=FFMAX(22)                          MOLM2100
168     XMOLS(I)=PRESTO(ISTEP+1)*VOLTX(I)/84.80804 MOLM2110
169  1400  CONTINUE                                     MOLM2120
170     RETURN                                         MOLM2130
C
171     500 CONTINUE                                     MOLM2140
C
172     IF(MODE(1,IH),LT,0) GO TO 1840               MOLM2150
C
173     IF(ANHR,EQ,0.0,AND,ANXE,EQ,0.0) GO TO 10000  MOLM2160
174     AVKR=ANHR/FNPOW                            MOLM2170
175     AVXE=ANXE/FNPOW                            MOLM2180
176     GTMKR=AVKR/AVOGAD*FUELL                   MOLM2190
177     RRKR=GMOL(5)/GTMKR                         MOLM2200
178     RXE=GMOLR(6)/GTMKE                         MOLM2210
179

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* SOURCE STATEMENT (COLMOL) */

180 10000 CONTINUE . . . . . MOLM2370
      C . . . . . MOLM2380
181     CALL HEAD(-1) . . . . . MOLM2390
      C . . . . . MOLM2400
182     WRITE(6,405) . . . . . MOLM2410
183     WRITE(6,410) . . . . . MOLM2420
184     DO 43 I=1,NPOW . . . . . MOLM2430
185     WRITE(6,420) I,AKR(I),AXE(I),FF(1,I),FFMAX(I),RKR(1,I),RKRMAX(I),
1     RXE(1,I),RXEMAX(I) . . . . . MOLM2440
186     45 CONTINUE . . . . . MOLM2450
187     I=21 . . . . . MOLM2460
188     WRITE(6,430) ANKR,ANXE,FF(1,I),FFMAX(I),RKR(1,I),RKRMAX(I),
1     RXE(1,I),RXEMAX(I) . . . . . MOLM2470
189     I=22 . . . . . MOLM2480
190     WRITE(6,440) AVKR,AVXE,FF(1,I),FFMAX(I),RKR(1,I),RKRMAX(I),
1     RXE(1,I),RXEMAX(I) . . . . . MOLM2490
191     I=23 . . . . . MOLM2500
192     WRITE(6,450) GMKR,GMXE,GMOLR(5),GMOLR(6) . . . . . MOLM2510
193     **** PLENUM VOLUME AND PRESSURE CHANGE DUE TO ELONGATION MOLM2520
194     A1=A2*A3*U,0 MOLM2530
195     DO 1830 I=1,NPOW MOLM2540
196     A1=A1+DENSFL(2,I) MOLM2550
197     A2=A2+DENSFL(5,I) MOLM2560
198     A3=A3+DENSFL(4,I) MOLM2570
199     1830 CONTINUE MOLM2580
200     XL1=A1 MOLM2590
201     XL2=A2 MOLM2600
202     XL3=A3 MOLM2610
203     VP1=P1*A1*DCL**2/4. MOLM2620
204     VP2=P1*A2*DCL**2/4. MOLM2630
205     VP3=P1*A3*DCL**2/4. MOLM2640
206     C . . . . . MOLM2650
207     VPLE1=VPLEN-Z-VP1 MOLM2660
208     VPLE2=VPLEN-Z-VP2 MOLM2670
209     VPLE3=VPLEN-Z-VP3 MOLM2680
210     VOLPT=VOLT*S-VPLENZ/TPLENA MOLM2690
211     VOLPT1=VOLPT+VPLE1/TPLENA MOLM2700
212     VOLPT2=VOLPT+VPLE2/TPLENA MOLM2710
213     VOLPT3=VOLPT+VPLE3/TPLENA MOLM2720
214     PREST1=84.40804*XMOTOT/VOLPT1 MOLM2730
215     PREST2=84.40804*XMOTOT/VOLPT2 MOLM2740
216     PREST3=84.40804*XMOTOT/VOLPT3 MOLM2750
217     *P1=1.703 MOLM2760
218     WRIT6(5,472) XL3,VP3,VPLE3,PREST3 MOLM2770
219     WRIT6(6,474) XL1,VP1,VPLE1,PREST1 MOLM2780
220     WRIT6(6,476) XL2,VP2,VPLE2,PREST2 MOLM2790
221     1840 CONTINUE MOLM2800
222     C . . . . . MOLM2810
223     C . . . . . MOLM2820
224     GO 1810 J=1,23 MOLM2830
225     FF(1,J)=FFMAX(J) MOLM2840
226     RKR(1,J)=RKRMAX(J) MOLM2850
227     RXE(1,J)=RXEMAX(J) MOLM2860
228     1810 DO 1411 I=1,NPOW MOLM2870
229     1411 CONTINUE MOLM2880
230     RETURN MOLM2890
      C . . . . . MOLM2900
231     C . . . . . MOLM2910
232     C . . . . . MOLM2920
233     C . . . . . MOLM2930
234     C . . . . . MOLM2940
235     C . . . . . MOLM2950

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* SOURCE STATEMENT (COLMOL) */

225     AKR(1)=AKR(1) MOLM2960
226     AXE(1)=AXE(1) MOLM2970
227     1811 CONTINUE MOLM2980
228     RETURN MOLM2990
      C . . . . . MOLM3000
229     C . . . . . MOLM3010
230     400 FORMAT(10X,3DHAS RELEASE MECHANISM INFORMATION / 10X,33(1H-) ) MOLM3020
231     410 FORMAT(5X,11H AXIAL GENERATED F,P GAS GAS ) MOLM3030
      1:LEASE RATE RELEASED GAS (ATOMS PER UNIT LENGTH) /MOLM3040
      3 5X,12TH SECTION (ATOMS PER UNIT LENGTH) UNTIL NMOLM3050
      4:0 THIS TIME ===== KRYPTON ===== XENON =MOLM3060
      5=====/ THIS STEP / MOLM3070
      6 5X,12TH NUMBER KRYPTON XENON MAX, YAMOLM3080
      7LUE STEP MAX, VALUE IN THIS STEP MAX, VALUE IN MOLM3090
      8THIS STEP / MOLM3100
      9 10X,(1H-),1X,2(2X,12(1H-)),2X,2(2X,12(1H-)), MOLM3110
      * 2X,2(2X,12(1H-)) MOLM3120
232     420 FORMAT(10X,17X,1X,2E14.5,2E12.6,2E14.5,2E14.5) MOLM3130
233     430 FORMAT(7X,10HAXIAL SUM,,1X,2E14.5,2E12.6,2E14.5) MOLM3140
234     440 FORMAT(7X,10HAXIAL AVG,,1X,2E14.5,2E12.6,2E14.5) MOLM3150
235     450 FORMAT(7E11TOTAL MOLES / 6X,12HIN FUEL MOLM3160
      1 2E14.5,2E14.5,15X,E14.5 ) MOLM3170
      460 FORMAT(//10X,5DHRELEASE RATE (BY VOLUME AVERAGE TEMP.),.....,MOLM3180
      1+F10.5 / 10X,5DHRECALCULATED RELEASE RATE KR , XE ,.....,MOLM3190
      2,2F10.5 ) MOLM3200
236     470 FORMAT( 3() ) MOLM3210
      1 10X,110HAXIAL PELLET PELLET STUCK PELL MOLM3220
      2E1 VOLUME CHANGED PLENUM PLENUM PRESSURE MOLM3230
      3 /10X,110HLENGTH CHANGE LENGTH CHANGE CHANGE MOLM3240
      4 BY ELONG VOLUME INDUCED PELLET MOLM3250
      5 /10X,110H (CM) (CM) -ATION MOLM3260
      6 (CM) LENGTH CHANGE MOLM3270
      7 / 35X,4(5X,15(1H-)) MOLM3280
237     472 FORMAT(10X,30HDUE TO THERMAL EXPANSION +3(F15.7,5X),F15.5 ) MOLM3290
238     474 FORMAT(10X,30HDUE TO AXIAL DENSIFICATION +3(F15.7,5X),F15.5 ) MOLM3300
239     476 FORMAT(10X,30HDUE TO EXPANSION + DENSITY +3(F15.7,5X),F15.5 ) MOLM3310
      C . . . . . MOLM3320
240     END MOLM3330

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* SOURCE STATEMENT *

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1      SUBROUTINE MOLM04
2      ***** THIS ROUTINE CALCULATE FP GAS RELEASE
3      BY NEW RELEASED MODEL (HARAYAMA)
4
5      COMMON /FFMOL / FF(6-23),RKR(6-23),RXE(6-23),AKX(10-20+2)
6      COMMON /IXIR / IX,IH,I1H,MAXTEP
7      COMMON /POWRAY/ PAVRG,FUEL,FL,POWER(21),AI(21),NPOW,PTOT,LPMAX,
8      COMMON /PKPOWER,IPKPOWER,DELP,PMAX
9      COMMON /BRNGAS/ AKR(20),AXE(20),PHI(20),ENXE(20),ENKR(20)
10     COMMON /ML5938/ TBAR(20)
11     COMMON /DATA 3/ VOLAT(29),FISGR(29)
12     COMMON /COM 02/ Ipow,ISTEP,ITER,KOUNT
13     COMMON /GASRE/ FFMAX(23),RKRMX(23),RAEMAX(23),AKHO(20),AXEO(20)
14
15     IS11=ISTEP+1
16     FNPOW = FLOAT(NPOW)
17     FFS=RKKS*RXES=0.0
18     TBS=0.0
19     DO 1372 IPOW= 1,NPOW
20       TOTGO=AKR(IPOW)+AXEO(IPOW)
21       TOTGN=AKR(IPOW)+AXE(IPOW)
22       IF(TOTGN.LE.0.0) GO TO 1377
23       IF(TOTGO.GE.1.0001) GO TO 1375
24       1377 CONTINUE
25       FFS(IST1+IPOW)=TEPP(TBAR(IPOW),FISGR+VOLAT,29)
26
27     **** FP GAS INVENTORY INCREASE TO PRVIOUS STEP
28
29     IF(FF(IST1,IPOW).LT.FF(1,IPOW)) GO TO 1373
30     GAS RELEASE RATE INCREASE TO PRVIOUS RELEASE RATE(FF(1,IPOW))
31     FFMAX(IPOW)=FF(1,IPOW)
32     GO TO 1374
33     1373 CONTINUE
34     GAS RELEASE RATE DECREASE TO PRVIOUS RELEASE RATE
35     IF(TOTGN.LE.0.0) FFMAX(IPOW) = FFS(IST1+IPOW)
36     IF(TOTGN.LE.0.0) GO TO 1374
37     RATG = TOTGO / TOTGN
38     FFMAX(IPOW)=(1.-RATG)*FF(1,IPOW) + RATG*FF(1,IPOW)
39     1374 CONTINUE
40     GO TO 1376
41     1375 CONTINUE
42
43     **** FP GAS INVENTORY DECREASE TO PRVIOUS STEP
44
45     FFMAX(IPOW)=FF(1,IPOW)
46     1376 CONTINUE
47
48     RKPMAX(1)IPOW)=RKR(1,IPOW)*AKR(1,IPOW)*FFMAX(1,IPOW)
49     RXEMAX(1)IPOW)=RXE(1,IPOW)*AXE(1,IPOW)*FFMAX(1,IPOW)
50
51     FF(1,21)=FF(1,21) + FF(1,IPOW)
52     RKR(1,21)=RKR(1,21) + RKR(1,IPOW)
53     RXE(1,21)=RXE(1,21) + RXE(1,IPOW)
54
55     FFS=FFS + FFMAX(1,IPOW)
56     RKRS=RKRS + RKRMX(1,IPOW)
57     RAES=RXES + RXEMAX(1,IPOW)
58     TB=TB+TBAR(1,IPOW)

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* SOURCE STATEMENT (MOLM04) *

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1      C
2      1372 CONTINUE
3
4      TB=TB/FNPOW
5      FF(IST1+23) = TEPP(TB+FISGR+VOLAT,29)
6      FFMAX(23)=FFS
7      RKRMX(23)=RKRS
8      RXEMAX(23)=RXES
9
10     FFMAX(22)=FFS/FNPOW
11     RKRMX(22)=RKRS/FNPOW
12     RXEMAX(22)=RXES/FNPOW
13
14     FF(IST1+22)=FF(IST1+21)/FNPOW
15     RKR(IST1+22)=RKR(IST1+21)/FNPOW
16     RXE(IST1+22)=RXE(IST1+21)/FNPOW
17
18     CALL MOLM04
19
20     RETURN
21     END

```

* SOURCE STATEMENT *

```

1      SUBROUTINE OUT1                               OUT10010
C
C      OPTIONAL EQUATION OUTPUT                  OUT10020
C      THIS SUBROUTINE IS CALLED FROM MAIN WHEN IOUT1=1   OUT10030
C
C
2      COMMON /COM_0/ TITLE(20),AACT(7, 30),BB(6, 51),CF(3, 30),RV(2, 20) OUT10070
3      COMMON /HIZURE/ K1,K2,K3,K4,K5,K6          OUT10080
4      COMMON /IOUT2/ IOUT2                      OUT10090
5      COMMON /COM128/ IOUT1,IIPROF               OUT10100
6      COMMON /HIS / HASEC(100)+HIS(7,100),MODE(5,10U) OUT10110
7      COMMON /IYIELD/ IYIELD                   OUT10120
8      COMMON /POWRAY/ PAVRG,FUELLE,FL,POWER(21),AI(21),NPUW,PTOT,LPMAX, OUT10130
9      COMMON /MCNV / MCNV                      OUT10140
10     COMMON /D15 / MDEN,MRELOC,SINTED           OUT10150
11     COMMON /INPUT / FRDEN,FRFSIN,DSINZ,FRP02,FR35,FR40,FR41,DFS,DC1, OUT10160
12     COMMON /INPUT / DCU,DV01DZ,VPLNZ,ATMUS,SXK,R0UF,R0UC,EXTP,DE,V, OUT10170
13     COMMON /INPUT / TINLET,DELT,TMAX,TRK+TM,DOB,BK+HBC+SIGHF,IFLUX, OUT10180
14     COMMON /INPUT / NCLAD,NCON,NFLX,KOOL,NEWK,NEWCL,NEWFLX,V01DZL,NOH+OUT10200
15     COMMON /INPUT / FNACHE,FRACAR,FRACH,FRACN,FRACKR,FRACKE,NGACEL, OUT10210
16     COMMON /INPUT / DTEMP,ITOT,MG,IPKAVG,MINI,ICLF,ISTOR,ICREP,ISWELL,OUT10220
17     COMMON /INPUT / NEXP,MEXP,NHIST                OUT10230
18     COMMON /INPUT / MREST,LCHEP,DDISH,HDISH            OUT10240
19     COMMON /MREVI / MREVI                      OUT10250
20
21     CALL STEP0                               OUT10270
22     WRITE(6, 503)  TITLE,K1,K2,K3,K4          OUT10280
23     WRITE(6,1010)                            OUT10290
24     WRITE(6,1020)                            OUT10300
25     WRITE(6,1011)                            OUT10310
26     WRITE(6,1030)                            OUT10320
27     WRITE(6,1060)                            OUT10330
28     WRITE(6,1040)                            OUT10340
29     WRITE(6,1103)                            OUT10350
30     WRITE(6,1101)                            OUT10360
31     WRITE(6,1102)                            OUT10370
32     WRITE(6,1104)                            OUT10380
33     WRITE(6,1105)                            OUT10390
34     WRITE(6,1106)                            OUT10400
35     WRITE(6,1107)                            OUT10410
36     WRITE(6,1108)                            OUT10420
37     WRITE(6,1109)                            OUT10430
38     WRITE(6,11010)                           OUT10440
39     WRITE(6,11011)                           OUT10450
40     WRITE(6,11012)                           OUT10460
41     WRITE(6,11013)                           OUT10470
42     WRITE(6,11014)                           OUT10480
43     WRITE(6,11015)                           OUT10490
44     WRITE(6,11016)                           OUT10500
45     WRITE(6,11017)                           OUT10510
46     WRITE(6,11018)                           OUT10520
47     WRITE(6,11019)                           OUT10530
48     WRITE(6,11020)                           OUT10540
49     WRITE(6,11021)                           OUT10550
50     WRITE(6,11022)                           OUT10560
51     WRITE(6,11023)                           OUT10570
52     WRITE(6,11024)                           OUT10580
53     WRITE(6,11025)                           OUT10590

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* SOURCE STATEMENT (OUT1) **

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47     WRITE(6,1143)                            OUT10600
48     WRITE(6,1050)                            OUT10610
49     WRITE(6,1145)  IPEAK                  OUT10620
50     WRITE(6,10402)                           OUT10630
51     WRITE(6,10503)                           OUT10640
52     WRITE(6,1150)  ICHEP                  OUT10650
53     WRITE(6,1040)                           OUT10660
54     WRITE(6,1151)                            OUT10670
55     WRITE(6,1152)                            OUT10680
56     WRITE(6,1153)                            OUT10690
57     WRITE(6,1105)                            OUT10700
58     WRITE(6,1106)  ISTOR                  OUT10710
59     WRITE(6,1107)                            OUT10720
60     WRITE(6,1108)                            OUT10730
61     WRITE(6,1109)                            OUT10740
62     WRITE(6,11050)                           OUT10750
63     WRITE(6,11040)                           OUT10760
64     WRITE(6,1111)                            OUT10770
65     WRITE(6,1050)                           OUT10780
66     WRITE(6,1110)                            OUT10790
67     WRITE(6,1040)                           OUT10800
68     WRITE(6,1181)                            OUT10810
69     WRITE(6,1050)                           OUT10820
70     WRITE(6,1190)  ISWELL                  OUT10830
71     WRITE(6,11040)                           OUT10840
72     WRITE(6,11191)                           OUT10850
73     WRITE(6,1050)                           OUT10860
74     WRITE(6,1200)  NEXP                   OUT10870
75     WRITE(6,1040)                           OUT10880
76     WRITE(6,1202)                            OUT10890
77     WRITE(6,1201)                            OUT10900
78     WRITE(6,1050)                            OUT10910
79     WRITE(6,1210)  SIGHF                  OUT10920
80     WRITE(6,1040)                           OUT10930
81     WRITE(6,1211)                            OUT10940
82     WRITE(6,1212)                            OUT10950
83     WRITE(6,1050)                            OUT10960
84     WRITE(6,1220)  MEXP                   OUT10970
85     WRITE(6,1040)                           OUT10980
86     WRITE(6,1221)                            OUT10990
87     WRITE(6,1050)                           OUT11000
88     WRITE(6,1230)  MCONV                  OUT11010
89     WRITE(6,1040)                           OUT11020
90     WRITE(6,1231)                            OUT11030
91     WRITE(6,1050)                           OUT11040
92     WRITE(6,1235)  MREVI                  OUT11050
93     WRITE(6,1040)                           OUT11060
94     WRITE(6,1236)                            OUT11070
95     WRITE(6,1050)                           OUT11080
96     WRITE(6,1240)  MDEN                   OUT11090
97     WRITE(6,1040)                           OUT11100
98     WRITE(6,1241)                            OUT11110
99     WRITE(6,1242)                            OUT11120
100    WRITE(6,1050)                           OUT11130
101    WRITE(6,1250)  MRELOC                  OUT11140
102    WRITE(6,1040)                           OUT11150
103    WRITE(6,1251)                            OUT11160
104    WRITE(6,1050)                           OUT11170
105    WRITE(6,1252)                            OUT11180

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* SOURCE STATEMENT (OUT1) 1*

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106      WRITE(6,1260) IIPROF          OUT11190
107      WRITE(6,1040)               OUT11200
108      WRITE(6,1261)               OUT11210
109      WRITE(6,1050)               OUT11220
110      WRITE(6,1270) MREST          OUT11230
111      WRITE(6,1040)               OUT11240
112      WRITE(6,1271)               OUT11250
113      WRITE(6,1050)               OUT11260
114      WRITE(6,1275) LCREP          OUT11270
115      WRITE(6,1040)               OUT11280
116      WRITE(6,1276)               OUT11290
117      WRITE(6,1060)               OUT11300
118      WRITE(6,1030)               OUT11310
119      RETURN                      OUT11320
120      C * 1 * 2 * 3 * 4 * 5 * 6 * 7 OUT11330
121      503 FORMAT(1H1/ 20A4,10X,2A4,I5,3H MR,13,7H MINUTE ) OUT11340
122      1000 FORMAT(1H1 )             OUT11350
123      1010 FORMAT( // 50X, 39(1H-) ) OUT11360
124      1011 FORMAT( 50X, 39(1H-) ) OUT11370
125      1020 FORMAT( 50X, 39H) FREG3 OPTIONAL MODEL AND EQUATION 1 OUT11380
126      1030 FORMAT( 7X, 126(1H-) ) OUT11390
127      1040 FORMAT( 7X,1H1,124X,1H1, / 7X,1H1,124X,1H1 ) OUT11400
128      1060 FORMAT( 7X,1H1,124X,1H1, / 7X,1H1,124X,1H1 / 7X,1H1,124X,1H1 ) OUT11420
129      1100 FORMAT( 7X, 1H1, 4X, *117H**** FUEL THERMAL CONDUCTIVITY EQUATION **** CONTROL SIGOUT11440
*NAL...INPUT GROUP NO. 3 FORMATTED 12 COLUMN 73-74 K3=, 12,2H 1) OUT11450
130      1101 FORMAT( 7X, 1H1, *124H   K2 = (NCON),GT,0 : READ IN TABLE FROM CARDS (INOUT11470
*PUT GROUP NO. 53. NAMELIST INPUT2 , OUT11480
* 1H1 / 7A+ 1H1,               OUT11490
*124H   K2 *           0 : SAME AS PREVIOUS STEP, OUT11500
*               OUT11510
* 1H1 / 7X, 1H1,               OUT11520
*124H   K2 = (NCON) = -2 : WARD DESIGN EQUATION ( DENSOUT11530
*ITY,LT,0.95 FRACTIONAL ), OUT11540
* 1H1               OUT11550
131      1102 FORMAT( 7X, 1H1, *124H   K2 = (NCON) = -2 : WARD DESIGN EQUATION ( DENSOUT11570
*ITY,GE,0.95 FRACTIONAL ) ,89.5 59.0 , OUT11580
* 1H1 / 7X, 1H1,               OUT11590
*124H   K2 = (NCON) = -3 : GODFREY EQUATION, OUT11600
*               90.7 59.0 , OUT11610
* 1H1 / 7X, 1H1,               OUT11620
*124H   * K2 = (NCON) = -4 : LYONS EQUATION, (DOCKET STOUT11630
*N=50447-1 P,4,2-3) ,93.0 62.0 , OUT11640
* 1H1               OUT11650
132      1104 FORMAT( 7X, 1H1, *124H   K2 = (NCON) = -5 : RESAR-41 EQUATION (DOCKET STOUT11670
*N=50480-1 P,4,4-9) ,86.2 64.5 , OUT11680
* 1H1               OUT11690
133      1103 FORMAT( 7A, 1H1, *124H               ----INTEGRAL KDT (WOUT11710
*/CM)---- FROM TD(DEG=C), AT RHO=0.95 0/2800 500/2600 , OUT11720
* 1H1 / 7X, 1H1,               OUT11730
*124H               OUT11740
*               ----(W/CM)---- , OUT11750
* 1H1               OUT11760
134      1120 FORMAT( 7A, 1H1, 4X, OUT11770

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* SOURCE STATEMENT (OUT1) 1*

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*117H**** CLADDING PROPERTIES **** CONTROL SIGOUT11780
*NAL...INPUT GROUP NO. 3 FORMATTED 12 COLUMN 75-76 K3=, 12,2H 1) OUT11790
135      1121 FORMAT( 7X, 1H1, *124H   K3 (NCLAD),GT,0 : READ IN TABLE FROM CARDS (INOUT11810
*PUT GROUP NO. 6). NAMELIST INPUT3 , OUT11820
* 1H1 / 7A+ 1H1,               OUT11830
*124H   K3 =           0 : SAME AS PREVIOUS STEP, OUT11840
*               OUT11850
* 1H1 / 7X, 1H1,               OUT11860
*124H   K3 =(NCLAD) = -2 : ZIRCALOY-2 ( BUILT IN DATA OUT11870
*), REFER D- 964 , OUT11880
* 1H1               OUT11890
136      1122 FORMAT( 7A, 1H1, *124H   K3 =(NCLAD) = -4 : ZIRCALOY-4 ( BUILT IN DATA OUT11910
*), REFER D- 964 , OUT11920
* 1H1 / 7A+ 1H1,               OUT11930
*124H   K3 =(NCLAD) = -9 : 20-PERCENT COLD WORKED TYPE OUT11940
*316 STAINLESS STEEL,               OUT11950
* 1H1               OUT11960
137      1125 FORMAT( 7X, 1H1, 4X, *113H**** CLADDING YIELD STRENGTH EQUATION **** CONTROL SIGOUT11980
*NAL...INPUT GROUP NO. 2 NAMELIST /INPUT/ IYIELD=,I2,5X + 1H1 ) OUT11990
138      1126 FORMAT( 7X, 1H1, *124H   IYIELD= 0 : YIELD STRENGTH IS USED FROM OUT12000
*TABLE DATA WHICH IS ASSIGNED BY NCLAD, , OUT12020
* 1H1               OUT12030
139      1130 FORMAT( 7X, 1H1, 4X, *117H**** RADIAL FLUX DEPRESSION **** CONTROL SIGOUT12050
*NAL...INPUT GROUP NO. 3 FORMATTED 12 COLUMN 77-78 K4=, 12,2H 1) OUT12060
140      1131 FORMAT( 7X, 1H1, *124H   K4 (NFLX),GT,0 : READ IN TABLE FROM CARDS (INOUT12080
*PUT GROUP NO. 7). NAMELIST INPUT4 , OUT12090
* 1H1 / 7X, 1H1,               OUT12100
*124H   K4 =           0 : FLAT (FIRST STEP). SAME AS POUT12110
*PREVIOUS STEP (FROM SECOND STEP) , OUT12120
* 1H1 / 7X, 1H1,               OUT12130
*124H   K4 = (NFLX) = -1 : BUILT IN EQUATION ( BESSSEL IOUT12140
*ZERO DISTRIBUTION ) REFER D- 916.917 , OUT12150
* 1H1               OUT12160
141      1140 FORMAT( 7A, 1H1, 4X, *117H**** AXIAL POWER DISTRIBUTION **** CONTROL SIGOUT12180
*NAL...INPUT GROUP NO. 3 FORMATTED 12 COLUMN 79-80 K5=, 12,2H 1) OUT12190
142      1141 FORMAT( 7X, 1H1, *124H   K5 ,GT,0 : READ IN TABLE FROM CARDS (INOUT12210
*PUT GROUP NO. 8). NAMELIST INPUT5 , OUT12220
* 1H1 / 7A+ 1H1,               OUT12230
*124H   K5 =           0 : SAME AS PREVIOUS STEP, OUT12240
*               OUT12250
* 1H1               OUT12260
143      1142 FORMAT( 7X, 1H1, 4X, *113H**** IRRADIATION MODEL **** CONTROL SIGOUT12280
*NAL...INPUT GROUP NO. 2 NAMELIST /INPUT/ IFLUX =,I2,5X + 1H1 ) OUT12290
144      1143 FORMAT( 7X, 1H1, *124H   IFLUX = 0 : FAST FLUX IRRADIATION, OUT12300
*               , OUT12320
* 1H1 / 7X, 1H1,               OUT12330
*124H   IFLUX = 1 : THERMAL FLUX IRRADIATION, OUT12340
*               , OUT12350
* 1H1               OUT12360

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* SOURCE STATEMENT (OUT1) */

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145 1145 FORMAT( 7X, 1HI, 4X,                                     OUT12370
      *113H***** LINEAR HEAT RATE ASSIGNMENT SIGNAL ***** CONTROL SIGOUT12380
      *NAL...INPUT GROUP NO. 2 NAMELIST /INPUT/ IPEAK =,12.5X + 1HI ) OUT12390
146 1146 FORMAT( 7X, 1HI,                                     OUT12400
      *124H           IPEAK,GT,0 : LINEAR HEAT RATE WHICH IS ASOUT12410
      *SIGNED BY GROUP=3-INPUT IS CONSIDERED TO ROD-AVG-VALUE.   , OUT12420
      * 1HI / 7X, 1HI,                                     OUT12430
      *124H           IPEAK,LE,0 : LINEAR HEAT RATE WHICH IS ASOUT12440
      *SIGNED BY GROUP=3-INPUT IS CONSIDERED TO ROD-PEAK-VALUE.   , OUT12450
      * 1HI                                     ) OUT12460
147 1150 FORMAT( 7X, 1HI, 4X,                                     OUT12470
      *113H***** CLADDING CREEP ***** CONTROL SIGOUT12480
      *NAL...INPUT GROUP NO. 2 NAMELIST /INPUT/ ICREP =,12.5X + 1HI ) OUT12490
148 1151 FORMAT( 7X, 1HI,                                     OUT12500
      *124H           ICREP,GT,0 : READ IN TABLE FROM CARDS (INOUT12510
      *PUT GROUP NO. 4). FORMATTED FLU,0, E10,0   , OUT12520
      * 1HI / 7X, 1HI,                                     OUT12530
      *124H           ICREP = 0 : NOT CREEP.               OUT12540
      *
      * 1HI                                     ) OUT12550
149 1153 FORMAT( 7X, 1HI,                                     OUT12570
      *124H           ICREP = -2 : SAME AS AIR ZIRCALOY TUBE. OUT12580
      *J,NUCL,MAT, 41,(1971), P327, REFER D- 950
      * 1HI / 7X, 1HI,                                     OUT12590
      *124H           ICREP = -3 : SAME AS PRESSURE TUBE.    OUT12610
      * REFER D- 751
      * 1HI / 7X, 1HI,                                     OUT12630
      *124H           ICREP = -4 : SAME AS FIGRO WAPD-TM 612. OUT12640
      * REFER D- 952
      * 1HI / 7X, 1HI,                                     OUT12660
      *124H           ICREP = -5 : ATRC(NEW) MODEL.        OUT12670
      * REFER D- 953
      * 1HI                                     ) OUT12690
150 1160 FORMAT( 7X, 1HI, 4X,                                     OUT12700
      *113H***** STORED ENERGY CALCULATION ***** CONTROL SIGOUT12710
      *NAL...INPUT GROUP NO. 2 NAMELIST /INPUT/ ISTOR =,12.5X + 1HI ) OUT12720
151 1161 FORMAT( 7X, 1HI,                                     OUT12730
      *124H           ISTOR = 0 : STORED ENERGY CALCULATION ISOUT12740
      * NOT PERFORMED.   , OUT12750
      * 1HI / 7X, 1HI,                                     OUT12760
      *124H           ISTOR,LT,0 : STORED ENERGY CALCULATION ISOUT12770
      * REFER D- 700
      * 1HI                                     ) OUT12790
152 1170 FORMAT( 7X, 1HI, 4X,                                     OUT12800
      *113H***** HISTORY INPUT ***** CONTROL SIGOUT12810
      *NAL...INPUT GROUP NO. 2 NAMELIST /INPUT/ NHIST =,12.5X + 1HI ) OUT12820
153 1171 FORMAT( 7X, 1HI,                                     OUT12830
      *124H           NHIST = 0 : TIME DEPENDENT HISTORY. OUT12840
      *
      * 1HI / 7X, 1HI,                                     OUT12860
      *124H           NHIST = 1 : BURNUP DEPENDENT HISTORY. OUT12870
      *
      * 1HI                                     ) OUT12890
154 1180 FORMAT( 7X, 1HI, 4X,                                     OUT12900
      *113H***** CLADDING ELASTIC DEFORAMTION ***** CONTROL SIGOUT12910
      *NAL...INPUT GROUP NO. 2 NAMELIST /INPUT/ ICDF =,12.5X + 1HI ) OUT12920
155 1181 FORMAT( 7X, 1HI,                                     OUT12930
      *124H           ICDF = 0 : ELASTIC CLAD DEFLECTION NOT OUT12940
      *TAKEN INTO ACCOUNT.   , OUT12950

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* SOURCE STATEMENT (OUT1) */

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      * 1HI / 7X, 1HI,                                     OUT12960
      *124H           ICDF,LT,0 : ELASTIC CLAD DEFLECTION TAKEOUT12970
      *N INTO ACCOUNT.   , OUT12980
      * 1HI                                     ) OUT12990
156 1190 FORMAT( 7X, 1HI, 4X,                                     OUT13000
      *113H***** FUEL SWELLING MODEL ***** CONTROL SIGOUT13010
      *NAL...INPUT GROUP NO. 2 NAMELIST /INPUT/ ISWELL =,12.5X + 1HI ) OUT13020
157 1191 FORMAT( 7X, 1HI,                                     OUT13030
      *124H           ISWELL = 0 : FUEL SWELLING IS NOT TAKEN OUT13040
      *NTO ACCOUNT.   , OUT13050
      * 1HI / 7X, 1HI,                                     OUT13060
      *124H           ISWELL = 1 : GEITHOFF, ET AL. MODEL IS USOUT13070
      *ED,           USED IN GAPCON ( CONSERVATIVE MODEL )   , OUT13080
      * 1HI / 7X, 1HI,                                     OUT13090
      *124M           ISWELL = 2 : REVISED GAP CLOSURE MODEL ISOUT13100
      * USED,          USED IN GAPCON THERMAL-1 ( OPTIONAL )   , OUT13110
      * 1HI                                     ) OUT13120
158 1200 FORMAT( 7X, 1HI, 4X,                                     OUT13130
      *113H***** FUEL THERMAL EXPANSION EQUATION ***** CONTROL SIGOUT13140
      *NAL...INPUT GROUP NO. 2 NAMELIST /INPUT/ NEXP =,12.5X + 1HI ) OUT13150
159 1202 FORMAT( 7X, 1HI,                                     OUT13160
      *124H           NEXP = 0 : -----THERMAL EXPANSIONOUT13170
      *CN COEFF, AVERAGE DELTA,L/L/(T2-T1) 25/2800 500/2800   , OUT13180
      * 1HI / 7X, 1HI,                                     OUT13190
      *124H           NEXP = 1 : -----(<DEG-C>)----   , OUT13200
      *
      * 1HI                                     ) OUT13210
160 1204 FORMAT( 7X, 1HI,                                     OUT13230
      *124M           NEXP = 0 : FUEL THERMAL EXPANSION IS NOOUT13240
      *T TAKEN INTO ACCOUNT.   , OUT13250
      * 1HI / 7X, 1HI,                                     OUT13260
      *124M           NEXP = 1 : ROTH AND HALTEMAN, ( GAOUT13270
      *PCON )          REFER D-812 1.1145E-5 1.1430E-5   , OUT13260
      * 1HI / 7X, 1HI,                                     OUT13290
      *124M           NEXP = 2 : CONWAY,FINCEL AND MAIN ( GAOUT13300
      *PCON THERMAL-1 ) REFER D-812 1.4978E-5 1.6354E-5   , OUT13310
      * 1HI                                     ) OUT13320
161 1210 FORMAT( 7X, 1HI, 4X,                                     OUT13330
      *120H***** CALCULATE THE CALDDING-TO-COOLANT HEAT TRANSFER COEFFICOUT13340
      *IENT *****   , 1HI / OUT13350
      * 7X, 1HI, 4X,                                     OUT13360
      *113H           SIGHF = 0 : CONTROL SIGOUT13370
      *NAL...INPUT GROUP NO. 2 NAMELIST /INPUT/ SIGHF =, F7.3, 1HI ) OUT13380
162 1211 FORMAT( 7X, 1HI,                                     OUT13390
      *124H           SIGHF,GT,0 : COOLANT IS UNSPECIFIED AND TOUT13400
      *HE FILM COEFFICIENT WILL BE SET TO SIGHF,   , OUT13410
      * 1HI / 7X, 1HI,                                     OUT13420
      *124H           SIGHF = 0 : COOLANT IS LIQUID SODIUM. ( OUT13430
      *PRESENTED HEDL-TME 71-32, JUNE 1971 ).   , OUT13440
      * 1HI / 7X, 1HI,                                     OUT13450
      *124H           SIGHF = -1 : COOLANT IS WATER. ( OUT13460
      *DITTUS-BEELTER EQUATION ). REFER D- 929   , OUT13470
      * 1HI                                     ) OUT13480
163 1212 FORMAT( 7X, 1HI,                                     OUT13490
      *124H           SIGHF = -2 : COOLANT IS WATER. ( OUT13500
      *JENS LOTTES EQUATION ) REFER D- 526   , OUT13510
      * 1HI / 7X, 1HI,                                     OUT13520
      *124H           SIGHF = -3 : SUBCOOL=DITTUS BEELTER, SATOUT13530
      *URATE=JENS LOTTES   , OUT13540

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* SOURCE STATEMENT (OUT1) *

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      * 1H)
164 1220 FORMAT( 7X, 1H), 4X, ) OUT13550
      *113H***** FUEL THERMAL EXPANSION MODEL ***** CONTROL SIGOUT13570
      *NAL...INPUT GROUP NO. 2 NAMELIST /INPUT/ MEXP = 12.5X + 1H ) OUT13580
165 1221 FORMAT( 7X, 1H), ) OUT13590
      *124H               MEXP = 1 : GAPCON MODEL. ( MOST CONGOUT13600
      *SERVATIVE )          ) OUT13610
      * 1H) / 7X, 1H).      ) OUT13620
      *124H               MEXP = 2 : PLASTIC MODEL. ( AREA BALOUT13630
      *ANCE TYPE )          ) OUT13640
      * 1H) / 7X, 1H).      ) OUT13650
      *124H               MEXP = 3 : TWO REGION MODEL. ( HALF CRAOUT13660
      *CK TYPE )           ) OUT13670
      * 1H) / 7X, 1H).      ) OUT13680
      *124H               MEXP = 4 : BRITTLE MODEL. ( COMPLETEOUT13690
      * CRACK TYPE )        ) OUT13700
      * 1H)                 ) OUT13710
166 1230 FORMAT( 7X, 1H), 4X, ) OUT13720
      *113H***** GAP CONDUCTANCE CONVERGENCE METHOD ***** CONTROL SIGOUT13730
      *NAL...INPUT GROUP NO. 2 NAMELIST /INPUT/ MCNV = 12.5X + 1H ) OUT13740
167 1231 FORMAT( 7X, 1H), ) OUT13750
      *124H               MCNV = 0 : SIMILAR METHOD WHICH IS USEDOUT13760
      * FOR GAPCON-THERMAL=. ) OUT13770
      * 1H) / 7X, 1H).      ) OUT13780
      *124H               MCNV = 1 : NEWTON-RAPHSON METHOD. OUT13790
      *
      * 1.4)                ) OUT13800
168 1235 FORMAT( 7X, 1H), 4X, ) OUT13810
      *113H***** GAP CONDUCTANCE EQUATION ***** CONTROL SIGOUT13830
      *NAL...INPUT GROUP NO. 2 NAMELIST /INPUT/ MREV1 = 12.5X + 1H ) OUT13840
169 1236 FORMAT( 7X, 1H), ) OUT13850
      *124H               MREV1 = -1 : RESAR=41 EQUATION OUT13860
      *
      * 1.4) / 7X, 1H).      ) OUT13870
      * 60H               MREV1 = 1 : RUSS AND STOUTE EQUATION OUT13880
      * .64X, 1H)            ) OUT13890
170 1240 FORMAT( 7X, 1H), 4X, ) OUT13900
      *113H***** FUEL DENSIFICATION MODEL ***** CONTROL SIGOUT13920
      *NAL...INPUT GROUP NO. 2 NAMELIST /INPUT/ MDEN = 12.5X + 1H ) OUT13930
171 1241 FORMAT( 7X, 1H), ) OUT13940
      *124H               MDEN = 0 : DENSIFICATION IS NOT TAKEN OUT13950
      * ACCOUNT.           ) OUT13960
      * 1H)                 ) OUT13970
172 1242 FORMAT( 7X, 1H), ) OUT13980
      *124H               MDEN = 1 : HALDEN DENSIFICATION MODEL. OUT13990
      * REFER D- 946         ) OUT14000
      * 1H) / 7X, 1H).      ) OUT14010
      *124H               MDEN = 2 : GAPCON THERMAL-2 DENSIFICATIONOUT14020
      *MD MODEL             ) OUT14030
      * 1H)                 ) OUT14040
173 1250 FORMAT( 7X, 1H), 4X, ) OUT14050
      *113H***** FUEL RELOCATION MODEL ***** CONTROL SIGOUT14060
      *NAL...INPUT GROUP NO. 2 NAMELIST /INPUT/ MRELOC = 12.5X + 1H ) OUT14070
174 1251 FORMAT( 7X, 1H), ) OUT14080
      *124H               MRELOC = 0 : RELOCATION IS NOT TAKEN INTOOUT14090
      * ACCOUNT.           ) OUT14100
      * 1H)                 ) OUT14110
175 1252 FORMAT( 7X, 1H), ) OUT14120
      *124H               MRELOC = 1 : GAPCON THERMAL 2 RELOCATION OUT14130

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* SOURCE STATEMENT (OUT1) *

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      *MD MODEL              REFER D-1143           ) OUT14140
      * 1H)                  ) OUT14150
176 1260 FORMAT( 7X, 1H), 4X, ) OUT14160
      *113H***** TEMPERATURE DISTRIBUTION PRINTED ***** CONTROL SIGOUT14170
      *NAL...INPUT GROUP NO. 2 NAMELIST /INPUT/ TIPROF = 12.5X + 1H ) OUT14180
177 1261 FORMAT( 7X, 1H), ) OUT14190
      *124H               TIPROF = 0 : RADIAL TEMPERATURE PROFILE OUT14200
      *S NOT PRINTED.       ) OUT14210
      * 1H) / 7X, 1H).      ) OUT14220
      *124H               TIPROF = 1 : RADIAL TEMPERATURE PROFILE OUT14230
      *S PRINTED.           ) OUT14240
      * 1H)                 ) OUT14250
178 1270 FORMAT( 7X, 1H), 4X, ) OUT14260
      *113H***** RESTRUCTURING MODEL ***** CONTROL SIGOUT14270
      *NAL...INPUT GROUP NO. 2 NAMELIST /INPUT/ MREST = 12.5X + 1H ) OUT14280
179 1271 FORMAT( 7X, 1H), ) OUT14290
      *124H               MREST = 0 : RESTRUCTURING CALCULATION ISOUT14300
      *NOT PERFORMED.       ) OUT14310
      * 1H) / 7X, 1H).      ) OUT14320
      *124H               MREST = 1 : RESTRUCTURING CALCULATION ISOUT14330
      * PERFORMED.          ) OUT14340
      * 1H)                 ) OUT14350
180 1275 FORMAT( 7X, 1H), 4X, ) OUT14360
      *113H***** FUEL CREEP ***** CONTROL SIGOUT14370
      *NAL...INPUT GROUP NO. 2 NAMELIST /INPUT/ LCREP = 12.5X + 1H ) OUT14380
181 1276 FORMAT( 7X, 1H), ) OUT14390
      *124H               LCREP = 0 : FUEL NOT CREEP. OUT14400
      *
      * 1H) / 7X, 1H).      ) OUT14410
      *124H               LCREP = 1 : FUEL CREEP. OUT14420
      *
      * 1H)                 ) OUT14430
      * 1H) * 1 * 2 * 3 * 4 * 5 * 6 * 7 OUT14440
182   END                 ) OUT14450
                                ) OUT14460
                                ) OUT14470

```

* SOURCE STATEMENT *

```

1      SUBROUTINE PAPLOT(NPOW,NEWK+NEWCL+NEWFLX)
C
C   THIS SUBROUTINE IS CALLED FROM MAIN
C   AXIAL POWER DISTRIBUTION PRINT
C
2   COMMON /POWREF/ POWREF(21)
3   DIMENSION PWE1(21),PNORM(21),PLOT(51)
4   DIMENSION IF(7)
5   DATA ISPAN1,ISPAN1 / 50,51 /
6   IFLAT = 0
7   DO 10 I=1,NPOW
8   PWE1(I) = (POWREF(I) + POWREF(I+1)) / 2.0
9   10 CONTINUE
10  PAMAX = PAMIN = PTOT = PWE1(1)
C
11  IF(NPOW,LT,1) GO TO 30
12  DO 20 I=2,NPOW
13  IF(PAMAX,LT,PWE1(I)) PAMAX = PWE1(I)
14  IF(PAMIN,GT,PWE1(I)) PAMIN = PWE1(I)
15  PTOT = PTOT + PWE1(I)
16  20 CONTINUE
17  30 CONTINUE
18  PAAVG = PTOT / FLOAT(NPOW)
19  FSPAN = PAMAX - PAMIN
20  IF(FSPAN,LT,0.0001) IFLAT = 1
21  DO 40 I=1,NPOW
22  PNORM(I) = PWE1(I) / PAAVG
23  40 CONTINUE
24  40 AVG = FLOAT(ISPAN) * (PAMAX - PAMIN) / (PAMAX + PAMIN) + 1.0
25  IPOS=100
26  IPOS = 64 + IAVG
27  ENCODE(4+100,IF(3)) IPOS
28  IF(1)=4H+
29  IF(2)=4H-
30  IF(3)=4H*4H
31  IF(4)=4HVS,
32  IF(5)=4H
33  IF(6)=4H
34  IF(7)=4H
35  IF(NEWK,GT,0,OK .NEWCL,GT,0,OK .NEWFLX,GT,0) GO TO 45
36  WRITE(*,600)
37  NPOW1 = NPOW + 1
38  WRITE(*,600) NPOW,NPOW+1,NPOW1
39  WRITE(*,610)
40  WRITE(*,612)
41  IF((IAVG,LT,1.6,OR,(IAVG,GT,4.6)) GO TO 47
42  WRITE(*,614)
43  WRITE(*,616)
44  WRITE(*,620) NPOW1+POWREF(NPOW1)
C
45  DO 70 III=1,NPOW
46  I = NPOW + 1 - III
47  DO 50 ISP=1,ISPAN1
48  PLOT(ISP) = 1H
49  PLOT(1) = PLOT(IAVG) = PLOT(ISPAN1) = 1H
50  II = 1
51  IF(IF(1,LT,0,1) GO TO 60

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* SOURCE STATEMENT (PAPLOT) *

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52  II = (FLOAT(ISPAN) * (PWE1(I) - PAMIN)) / FSPAN + 1.0          PAPLU600
53  60 PLOT(I) = 1H*                                              PAPLU610
54  IF(I,LT,1) WRITE(6+630) (,POWREF(I),PNORM(I),PLOT)                PAPLU620
55  IF(I,EQ,1) WRITE(6+640) (,POWREF(I),PNORM(I),PLOT)                PAPLU630
56  70 CONTINUE
57  WRITE(*,600)
58  RETURN
C   * 1   * 2   * 3   * 4   * 5   * 6   * 7 PAPLU650
59  100 FORMAT(I4)                                              PAPLU660
60  600 FORMAT(1H / 7X,126(1H*), / 7X,1H*,124X,1H*)                  PAPLU670
61  610 FORMAT(7X,
4 56H( C ) AXIAL POWER DISTRIBUTION SEGMENT NO.,13, PAPLU680
B 21H, 1ODAL POINT NO.,13,122A,BPOWER,12 ,1H),11X,1H*) PAPLU690
62  612 FORMAT(7X, 1H*, 34X, 1 BUPNPOT SEGMENT ,.....,AXIAL POWER DISTRIBUTION (SEG, PAPLU700
2 1HMENT MEAN),....., 14X,1H* / 2 1H* PAPLU710
3 7X, 1H*, 34X, 1 B1H, 1H*, 34X,1H*) PAPLU720
4 30HVALUE  MEAN  MIN. , 44A* 4HMAX, +12X, 1H* ) PAPLU730
63  620 FORMAT(7X,1H*,5X 1 2CH, TOW,.....,POWER(,12, 2H)*, F12.6 ,83A ,1H* ) PAPLU740
64  630 FORMAT(7X,1H*,5X 1 2CH, 1H*,5X 1 BUPNPOT,.....,POWER(,12, 2H)*, 2F12.6 , 6A, 51A1, 14X,1H* ) PAPLU750
65  640 FORMAT(7X,1H*,5X 1 2CH, 3C10M,....,POWEH(,12, 2H)*, 2F12.6 , 6A, 51A1, 14X,1H* ) PAPLU760
66  650 FORMAT(7X,1H*,124X,1H* / 7X,126(1H*) 1 PAPLU770
67  660 FORMAT(7X,1H*,124X,1H* ) PAPLU780
68  670 FORMAT(7X, 1H*, 324X, 1H* ) PAPLU790
C   * 1   * 2   * 3   * 4   * 5   * 6   * 7 PAPLU800
69  END PAPLU810

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* SOURCE STATEMENT *

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1      SUBROUTINE PDAUTS          PDIS0010
C      THIS SUBROUTINE IS CALLED FROM STEP-1 AND MAIN          PDIS0020
C      REFER ENAL-1778, GAFCON THERMAL-1          PDIS0030
C      COMMON /PDAUTS/ PAVRG,FUELL,FL,POW(21),AI(21),NPOW,PTCT,LPMAX,          PDIS0040
C      *          PPKPOW,IPEAK,DELP,PNMAX          PDIS0050
3      COMMON /PDAREF/ POWER(21)          PDIS0060
C      C          PDIS0070
C      C          PDIS0080
C      C          PDIS0090
C      C          PDIS0100
C      C          PDIS0110
C      C          PDIS0120
C      NPOW = NPC* + 1          PDIS0130
C      AI(1) = (POWER(1)+POWER(2))*AINCR          PDIS0140
C      LPMAX = 3          PDIS0150
C      POLD = (POWER(1)+POWER(2))*5          PDIS0160
C      IF(NPOW.LE.1) GO TO 101          PDIS0170
C      DO 100 I=2,NPOW          PDIS0180
C      P = (POWER(I)+POWER(I+1))*5          PDIS0190
C      AI(I) = AI(I-1) + (POWER(I+1)+POWER(I))*AINCR          PDIS0200
C      IF(PLT,POLD) GO TO 100          PDIS0210
C      LPMAX = 1          PDIS0220
C      POLD = P          PDIS0230
C      100 CONTINUE          PDIS0240
C      101 CONTINUE          PDIS0250
C      AI(1) = AI(NPOW)          PDIS0260
C      C      NORMALIZE THE POWER AND SUCH THAT AI(1)=1.0          PDIS0270
C      C      PDIS0280
C      C      PDIS0290
C      IF(IPEAK.LE.0) GO TO 300          PDIS0300
C      DO 200 I=1,NPOW          PDIS0310
C      POW(I) = POWER(I) * PAVRG / AI(1)          PDIS0320
C      AI(I) = AI(I)/AITOT          PDIS0330
C      200 CONTINUE          PDIS0340
C      POW(NPOW+1) = POWER(NPOW+1) * PAVRG / AI(1)          PDIS0350
C      C      PDIS0360
C      250 GO TO 900          PDIS0370
C      C      CALCULATE POWER DISTRIBUTION BASED ON PEAK POWER (KW/FT)          PDIS0380
C      C      PDIS0390
C      C      PDIS0400
C      300 CONTINUE          PDIS0410
C      PEAK = POWER(1)          PDIS0420
C      DO 310 I=2,NPOW          PDIS0430
C      PEAK = AMAX(PEAK,POWER(I))          PDIS0440
C      310 CONTINUE          PDIS0450
C      C      NORMALIZE THE POWER DISTRIBUTION TO PPKPOW          PDIS0460
C      C      PDIS0470
C      C      PDIS0480
C      DO 320 I=1,NPOW          PDIS0490
C      POW(I) = POWER(I) * PPKPOW / PEAK          PDIS0500
C      AI(I) = AI(I)/AITOT          PDIS0510
C      320 CONTINUE          PDIS0520
C      PAVRG = AI(1)*PPKPOW/(PEAK)          PDIS0530
C      900 CONTINUE          PDIS0540
C      PTCT = FUELL*PAVRG          PDIS0550
C      RETURN          PDIS0560
C      C*****          PDIS0570
39     END          PDIS0580

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* SOURCE STATEMENT *

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1      SUBROUTINE PRINT1          PRIN0010
C                                         PRIN0020
C                                         PRIN0030
2      REAL LFUEL,LF,MOL,MOLEFR      PRIN0040
C                                         PRIN0050
3      COMMON /MOL678/ MOLEFR(6)     PRIN0060
4      COMMON /ML5938/ TBAR(20)      PRIN0070
5      COMMON /MOL9/   FMOL(6,21),RDOT(20) PRIN0080
6      COMMON /MOL579/ PRESTO(20)    PRIN0090
7      COMMON /MUL9/   TAVGXX(20)    PRIN0100
8      COMMON /COM39/  HFUX(20)      PRIN0110
9      COMMON /COM8/   HGA(20),RGAPX(20),TCLINE(20) PRIN0120
C                                         PRIN0130
10     COMMON /BURN/  BURN(20),BUOLD(20) PRIN0140
11     COMMON /MOLPRI/ GMOL(1,6),GMOLR(6),FRACTN(6),MOL(6),XMOLS(21) PRIN0150
12     COMMON /PRIN01/ TCULT(20),MFILM(20),TCOCA(20),TCICA(20) , PRIN0160
*      CCONB(20),TGAPC(20),HFLXFB(20),GCS(20),GCC(20) , PRIN0170
*      GCR(20),GCT(20),TJUMP(20),DRTF(20),DRSF(20) , PRIN0180
*      DPF(20),DRTC(20),DRPC(20),DRCLD(20),TFSCA(20) , PRIN0190
*      DRCC(20),BR1(20),BR2(20),BR4(20),PR1(20) , PRIN0200
*      RATF(20),RATC(20),CPRES(20),CSTRES(20),GASCC(20) , PRIN0210
*      GASCB(20),ITERZ(20)           PRIN0220
13     COMMON /PRIN02/ CP1(20),CP2(20),ST1(20),ST2(20) , PRIN0230
*      ST3(20),ST4(20),ST5(20),ST6(20)           PRIN0240
14     COMMON /PRIN03/ DRDF(20),DRRF(20),FCONT(20),TDISH(20) PRIN0250
C                                         PRIN0260
15     COMMON /INPUT/ FRDEN,FRSIN,DSINZ,FRPU02,FR4U,FR4L,DFS,DCI, PRIN0270
1       DCO,DVID2,VPLNZ,ATMOS,SIXX,ROUF,ROUC,EXTP,DE,V, PRIN0280
2       TINLET,DELT,TMAX,IFR,TH,DBU,BK+B,C,SIGNF,I,FLUX, PRIN0290
3       NCLAD,NCON,NFLX,KOOL,NEWK,NEWCL,NEFLX,VOLIDZL,NOH,PRIN0300
4       FRA�E,FRACAR,FRAFH,FRACN,FRACKR,FRACKE,HGACEL, PRIN0310
5       DTEMP(TOT,HO),PEKAVG,MINI,ICDF,ISTOR+ICHEP+ISWELL,PRIN0320
6       ,NEXP,+NEXP,NHIST           PRIN0330
16     COMMON /COM 08/ IIN,CASE,TCOOLF,XMOTOT           PRIN0340
17     COMMON /COM 10/ VVOIDZ,FRUG2,TPLENA,NPOW1           PRIN0350
18     COMMON /POWRAY/ PAVRG ,LFUEL ,LF ,POWER(21)           PRIN0360
1       ,AI(21) ,NPOW ,PTOT ,LPMAX ,PKPOW           PRIN0370
2       ,IMEAK ,DELP ,PMAX           PRIN0380
19     COMMON /BRNGAS/ NKR(20) ,NXE(20) ,PHI(20) ,ENXE(20) PRIN0390
1       ,ENKR(20)           PRIN0400
20     COMMON /COM 02/ IPW,ISTEP,ITER,KOUNT           PRIN0410
21     COMMON /COM 05/ BURNUP,TODAYS,VOID,TOTLDY,TOTBUR           PRIN0420
22     COMMON /MEMOI/ MEMOI(20,5),HATA(20)           PRIN0430
23     COMMON /FFMOL/ FFL6(23),RKH6(23),XRE(6,23),AKX(10,20,2) PRIN0440
24     COMMON /PRIMOL/ AANKR,AANAE           PRIN0450
25     COMMON /DIMEN1/ DV01DX(20),DV01DH(20),DFSX(20),DCIA(20),DCUX(20), PRIN0460
1       VV01DX(20),VV01DH(20),TSINX(20),RSINX(20)           PRIN0470
2       ,ZLENGT(5,20),VVIDL(20)           PRIN0480
26     COMMON /COM3/ TSAT           PRIN0490
27     COMMON /NUCLEI/ NUCLEI,A(40,23)           PRIN0500
28     COMMON /COM128/ IOUT1,IIPRF           PRIN0510
29     COMMON /CUN49P/ DC(20,1),IPRF           PRIN0520
30     COMMON /DIMEN2/ DENSFL(5,20)           PRIN0530
31     COMMON /PLOT / IPLOT           PRIN0540
32     DIMENSION XDUM1(20),XDUM2(20),XDUM3(20)           PRIN0550
33     DIMENSION NAME(6,2)           PRIN0560
34     DIMENSION GMOLG(6)           PRIN0570
35     DIMENSION GMOLG(6)           PRIN0580
C                                         PRIN0590

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* SOURCE STATEMENT (PRINT1) *

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5      DATA (NAME(1,J):J=1,2) /4H HE,4H LITHIUM/          PRIN0600
1       ,(NAME(2,J):J=1,2) /4H A,4H RUBIDIUM/           PRIN0610
2       ,(NAME(3,J):J=1,2) /4H HYDROGEN/                PRIN0620
3       ,(NAME(4,J):J=1,2) /4H NITR,4H OXYGEN/           PRIN0630
4       ,(NAME(5,J):J=1,2) /4H KRY,4H POTASSIUM/         PRIN0640
5       ,(NAME(6,J):J=1,2) /4H X,4H NEON/               PRIN0650
36     DATA GMOLG / 6*0.0 /           PRIN0660
37     DATA KAIG /0/           PRIN0670
38     DATA IDME/1H /           PRIN0680
39     DATA INODE/4H NODE/           PRIN0690
C                                         PRIN0700
C----- PARAMETERS DESCRIPTION ----- PRIN0710
C
C NFWN      NUMBER OF AXIAL NODES           PRIN0720
C LFIEL     FUEL ELEMENT LENGTH (CM)        PRIN0730
C PGFER     AXIAL POWER DISTRIBUTION (WATT/CM) PRIN0740
C
C BURN      BURNUP AT EACH NODE AND TIME (MW/TON) PRIN0750
C TCGLT     COOLANT TEMPERATURE (DEG C)        PRIN0760
C MFILM     FILM COEFFICIENT (W/CM^2/C)        PRIN0770
C TCCCA     CLAD OD TEMPERATURE (DEG C)        PRIN0780
C TCCFA     CLAD ID TEMPERATURE (DEG F)        PRIN0790
C TCICA     CLAD ID TEMPERATURE (DEG C)        PRIN0800
C TCIFA     CLAD THICKNESS (CM)                 PRIN0810
C CCONB    CLAD THERMAL CONDUCTIVITY (W/CM/C)    PRIN0820
C TGIPC     MEAN GAP TEMPERATURE (DEG C)        PRIN0830
C HFLXFB    FUEL SURFACE HEAT FLUX (W/CM^2)      PRIN0840
C GCS       SOLID-SOLID CONTACT CONDUCTANCE (W/CM^2/C) PRIN0850
C CGC       CONDUCTION THROUGH THE GASES ( )       PRIN0860
C GCR       RADIATION CONDUCTANCE ( )             PRIN0870
C GCT       TOTAL GAP CONDUCTANCE ( )             PRIN0880
C FOUT      FP GAS RELEASE RATE AT EACH AXIAL NODE PRIN0890
C TJUMP     TEMPERATURE JUMP DISTANCE (CM)        PRIN0900
C DRTF      INCREASE OF FUEL OD DUE TO THERMAL EXPANSION (CM) PRIN0910
C DRSF      DECREASE OF FUEL OD DUE TO DENSIFICATION PRIN0920
C DRF       TOTAL FUEL OD INCREASE (CM) = DRTF + DRFSF PRIN0930
C DHTC     INCREASE OF CLAD OD DUE TO THERMAL EXPANSION (CM) PRIN0940
C DRPC     ELASTIC DEFORMATION ( )                PRIN0950
C DRCC     CREEP ( )                           PRIN0960
C DRCLD    TOTAL CLAD OD INCREASE = DRTC + DRPC + DRCC ( ) PRIN0970
C TFSCA    FUEL SURFACE TEMPERATURE (DEG C)        PRIN0980
C TCLINE   FUEL CENTER-LINE TEMPERATURE (DEG C)      PRIN0990
C TBAR     VOLUME AVERAGED FUEL TEMPERATURE (DEG C)    PRIN1000
C BR1      CENTRAL VOID RADIUS (CM)              PRIN1010
C BR2      AT 1700DEG C RADIUS ( )                PRIN1020
C BR3      AT 1350 ( )                          PRIN1030
C BR4      FUEL SURFACE RADIUS ( HOT OD ) (CM)      PRIN1040
C RATF     PERCENT CHANGE IN ORIGINAL FUEL OD (PERCENT) PRIN1050
C CPRES    FUEL-CLAD CONTACT PRESSURE (KG/CM^2)      PRIN1060
C CSTRES   CLADDING HOOP STRESS (KG/CM^2)          PRIN1070
C
C CP1      NOMINAL HEAT CAPACITY (CAL/K-MOLE)      PRIN1080
C CP2      (BTU/LB-F)                            PRIN1090
C ST1      STORED ENERGY AT TBAR (CAL/GRAM)          PRIN1100
C ST2      (BTU/LB)                             PRIN1110
C ST3      VOLUME AVERAGED STORED ENERGY (CAL/GRAM) PRIN1120
C                                         PRIN1130
C                                         PRIN1140
C                                         PRIN1150
C                                         PRIN1160
C                                         PRIN1170
C                                         PRIN1180

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* SOURCE STATEMENT (PRINT1) *

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C      ST4           :          (BTU/LB)          PRIN1190
C      ST5           : STORED ENERGY PER UNIT LENGTH (CAL/CM) PRIN1200
C      ST6           :          (BTU/FT)          PRIN1210
C
C      NKR           : GENERATED KR PER UNIT LENGTH IN FUEL (MOLES/INCH) PRIN1220
C      NAE           : XE
C      PHI           : NEUTRON FLUX (INV)          PRIN1230
C      HFLUX          : CLAD OR HEAT FLUX          PRIN1240
C      PRESTO         : INTERNAL GAS PRESSURE AT EACH AXIAL ITERATION (KG/CM2) PRIN1250
C      TAVGKX        : VOLUME AVERAGED TEMPERATURE OF TOTAL FUEL (DEG C) PRIN1260
C      GASCC          : THERMAL CONDUCTIVITY OF FILL GAS (W/CM/C)          PRIN1270
C      GASC8          :          (BTU/HR-FT-F)          PRIN1280
C      * 1 * 2 * 3 * 4 * 5 * 6 * 7 PRIN1290
C      * 1 * 2 * 3 * 4 * 5 * 6 * 7 PRIN1300
C      * 1 * 2 * 3 * 4 * 5 * 6 * 7 PRIN1310
C      * 1 * 2 * 3 * 4 * 5 * 6 * 7 PRIN1320
C      * 1 * 2 * 3 * 4 * 5 * 6 * 7 PRIN1330
C      * 1 * 2 * 3 * 4 * 5 * 6 * 7 PRIN1340
C      * 1 * 2 * 3 * 4 * 5 * 6 * 7 PRIN1350
C      * 1 * 2 * 3 * 4 * 5 * 6 * 7 PRIN1360
C      * 1 * 2 * 3 * 4 * 5 * 6 * 7 PRIN1370
C      * 1 * 2 * 3 * 4 * 5 * 6 * 7 PRIN1380
C      * 1 * 2 * 3 * 4 * 5 * 6 * 7 PRIN1390
C      * 1 * 2 * 3 * 4 * 5 * 6 * 7 PRIN1400
C      * 1 * 2 * 3 * 4 * 5 * 6 * 7 PRIN1410
C      * 1 * 2 * 3 * 4 * 5 * 6 * 7 PRIN1420
C      * 1 * 2 * 3 * 4 * 5 * 6 * 7 PRIN1430
C      * 1 * 2 * 3 * 4 * 5 * 6 * 7 PRIN1440
C      * 1 * 2 * 3 * 4 * 5 * 6 * 7 PRIN1450
C      * 1 * 2 * 3 * 4 * 5 * 6 * 7 PRIN1460
C      * 1 * 2 * 3 * 4 * 5 * 6 * 7 PRIN1470
C      * 1 * 2 * 3 * 4 * 5 * 6 * 7 PRIN1480
C      * 1 * 2 * 3 * 4 * 5 * 6 * 7 PRIN1490
C      * 1 * 2 * 3 * 4 * 5 * 6 * 7 PRIN1500
C      * 1 * 2 * 3 * 4 * 5 * 6 * 7 PRIN1510
C      * 1 * 2 * 3 * 4 * 5 * 6 * 7 PRIN1520
C      * 1 * 2 * 3 * 4 * 5 * 6 * 7 PRIN1530
C      * 1 * 2 * 3 * 4 * 5 * 6 * 7 PRIN1540
C      * 1 * 2 * 3 * 4 * 5 * 6 * 7 PRIN1550
C      * 1 * 2 * 3 * 4 * 5 * 6 * 7 PRIN1560
C      * 1 * 2 * 3 * 4 * 5 * 6 * 7 PRIN1570
C      * 1 * 2 * 3 * 4 * 5 * 6 * 7 PRIN1580
C      * 1 * 2 * 3 * 4 * 5 * 6 * 7 PRIN1590
C      * 1 * 2 * 3 * 4 * 5 * 6 * 7 PRIN1600
C      * 1 * 2 * 3 * 4 * 5 * 6 * 7 PRIN1610
C      * 1 * 2 * 3 * 4 * 5 * 6 * 7 PRIN1620
C      * 1 * 2 * 3 * 4 * 5 * 6 * 7 PRIN1630
C      * 1 * 2 * 3 * 4 * 5 * 6 * 7 PRIN1640
C      * 1 * 2 * 3 * 4 * 5 * 6 * 7 PRIN1650
C      * 1 * 2 * 3 * 4 * 5 * 6 * 7 PRIN1660
C      * 1 * 2 * 3 * 4 * 5 * 6 * 7 PRIN1670
C      * 1 * 2 * 3 * 4 * 5 * 6 * 7 PRIN1680
C      * 1 * 2 * 3 * 4 * 5 * 6 * 7 PRIN1690
C      * 1 * 2 * 3 * 4 * 5 * 6 * 7 PRIN1700
C      * 1 * 2 * 3 * 4 * 5 * 6 * 7 PRIN1710
C      * 1 * 2 * 3 * 4 * 5 * 6 * 7 PRIN1720
C      * 1 * 2 * 3 * 4 * 5 * 6 * 7 PRIN1730
C      * 1 * 2 * 3 * 4 * 5 * 6 * 7 PRIN1740
C      * 1 * 2 * 3 * 4 * 5 * 6 * 7 PRIN1750
C      * 1 * 2 * 3 * 4 * 5 * 6 * 7 PRIN1760
C      * 1 * 2 * 3 * 4 * 5 * 6 * 7 PRIN1770

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* SOURCE STATEMENT (PRINT1) *

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75      IF(LEW,KAIG) WRITE(6,99)
76      *WRITE(6,202) 1,TCOCA(1),TCOF,TCIHC(1),TCIF,CCUNB(1),A1,TGAPC(1), PRIN1780
77      1,A3,HFLXFB(1),A2,(MEMU1(1,J),J=1,5),H1AC(1) PRIN1790
78      DO 20 J=1,5 PRIN1800
79      20 ITSUB=ITSUB+MEMO1(1,J) PRIN1810
80      21 CONTINUE PRIN1820
81      ITOT=ITOT+ITSUB PRIN1830
82      *WRITE(6,204) ITSUB+ITOT PRIN1840
83      22 CONTINUE PRIN1850
84      IF(NPOW,GT,15) CALL HEAD(-1) PRIN1860
85      IF(NPOW,LT,5) WRITE(6,1000) PRIN1870
86      23 CONTINUE PRIN1880
87      IF(NPOW,GT,15) WRITE(6,1000) PRIN1890
88      24 CONTINUE PRIN1900
89      IF(NPOW,LT,5) WRITE(6,1000) PRIN1910
90      25 CONTINUE PRIN1920
91      IF(NPOW,GT,15) CALL HEAD(-1) PRIN1930
92      IF(NPOW,LT,5) WRITE(6,1000) PRIN1940
93      26 CONTINUE PRIN1950
94      IF(NPOW,GT,15) CALL HEAD(-1) PRIN1960
95      IF(NPOW,LT,5) WRITE(6,1000) PRIN1970
96      27 CONTINUE PRIN1980
97      IF(NPOW,GT,15) CALL HEAD(-1) PRIN1990
98      IF(NPOW,LT,5) WRITE(6,1000) PRIN2000
99      28 CONTINUE PRIN2010
100     IF(NPOW,GT,15) CALL HEAD(-1) PRIN2020
101     IF(NPOW,LT,5) WRITE(6,1000) PRIN2030
102     29 CONTINUE PRIN2040
103     IF(NPOW,GT,15) CALL HEAD(-1) PRIN2050
104     IF(NPOW,LT,5) WRITE(6,1000) PRIN2060
105     30 CONTINUE PRIN2070
106     IF(NPOW,GT,15) CALL HEAD(-1) PRIN2080
107     IF(NPOW,LT,5) WRITE(6,1000) PRIN2090
108     31 CONTINUE PRIN2100
109     IF(NPOW,GT,15) CALL HEAD(-1) PRIN2110
110     IF(NPOW,LT,5) WRITE(6,1000) PRIN2120
111     32 CONTINUE PRIN2130
112     IF(NPOW,GT,15) CALL HEAD(-1) PRIN2140
113     IF(NPOW,LT,5) WRITE(6,1000) PRIN2150
114     33 CONTINUE PRIN2160
115     IF(NPOW,GT,15) CALL HEAD(-1) PRIN2170
116     IF(NPOW,LT,5) WRITE(6,1000) PRIN2180
117     34 CONTINUE PRIN2190
118     IF(NPOW,GT,15) CALL HEAD(-1) PRIN2200
119     IF(NPOW,LT,5) WRITE(6,1000) PRIN2210
120     35 CONTINUE PRIN2220
121     IF(NPOW,GT,15) CALL HEAD(-1) PRIN2230
122     IF(NPOW,LT,5) WRITE(6,1000) PRIN2240
123     36 CONTINUE PRIN2250

```

C INFORMATION FOR GAS

C.....

A1=VPLENZ/16.3871 PRIN2300

A1=VPLENZ,VPLENZ,A1 PRIN2310

A1 = TPLENA = 273. PRIN2320

A2 = A1*1.8 + 32. PRIN2330

WRITE(6,502) A1,A2 PRIN2340

IF(SIGMF,LT,0) WRITE(6,516) TSAT PRIN2350

A1=ATMOS*14.22 PRIN2360

* SOURCE STATEMENT (PRINTER) 2*

```

124      WRITE(6,503) ATMOS,A1
125      A1=PRESTO(I,STEP+1)*4.22
126      WRITE(6,504) PRESTO(I,STEP+1),A1
C
127      WRITE(6,505) XMOTOT
128      WRITE(6,506) XMOLSL(NPON+1)
129      A1=XMOTOT*XMOLSL(NPON+1)
130      WRITE(6,507) A1
131      WRITE(6,510) RDOT(I)
C
132      WRITE(6,508)
133      A1=0.
134      A2=0.
135      GMOLG(5)=ANHNP
136      GMOLG(1)=ANHNL
137      A3=GMOLG(5)+GMOLG(6)
138      DO 51 I=1,6
139      WRITE(6,509) (NAME(I,J),J=1,2)+GMOLG(I)+GMOLP(I),
     1           MOL(I),MOLEFR(I)
140      A1=A1+GMOLG(I)
141      A2=A2+GMOLP(I)
142 51 CONTINUE
143      WRITE(6,510) A1,A3,A2,XMOTOT
C
C ===== STORED ENERGY =====
C
144      WRITE(6,511)
145      DO 52 I=1,NPOX
146      IF(I,EW,KAIG) WRITE(6,999)
147      WRITE(6,512) I,CP1(I),CP2(I),ST1(I),ST2(I),ST3(I),ST4(I),
     1               ST5(I),ST6(I)
148 52 CONTINUE
C
C ===== CONVERGENCE STATUS
C
149      WRITE(6,1000)
150      WRITE(6,513)
151      DO 53 J=1,1STEP
152      I=J+1
153      A1=TAVGXA(I)+A1*.32.
154      A2=PRESTO(I)*14.22
155      WRITE(6,514) J,TAVGXX(I),A1+PRESTO(I),A2
156 53 CONTINUE
157      ERROR=ABS((TAVGXX(I,STEP)-TAVGXX(I,STEP+1))/TAVGXX(I,STEP+1))
158      WRITE(6,610) ERROR
C
159      CALL HEAD(4)
160      WRITE(6,620)
161      DO 54 I=1,NPOX
162      A1=DRDF(I)*10.
163      A2=DRRF(I)*10.
C
164      A3=RSTUX(I)*10.
165      A4=TSIAC(I)
166      A5=UVCDIX(I)*10./2.
167      A6=UFSAX(I)*10./2.
168      A7=DCIX(I)*10./2.
169      A8=DCGX(I)*10./2.
170      A9=VVVOUD(I)*1000.

```

* SOURCE STATEMENT (PRINTER) 2*

```

171      A10=VUCLID(I)*10./2.
172      A11=VUCLD(I)*10.
C
173      IF(I,EW,KAIG) WRITE(6,99)
174      WRITE(6,500) (A1,A2,A3,A4,A10,A11,A9,A5,A6,A7,A8
175 54 CONTINUE
176      WRITE(6,1000)
177      WRITE(6,640)
178      A1=2*D3B4+R5=0.0
179      R5=7*R6*B5B10=B11*B0.0
180      DO 55 I=1,NPOX
181      A1=LLENGL(I)
182      A2=LLENGL(I)
183      A3=LLENGL(I)
184      A4=LLENGL(I)
185      A5=LLENGL(I)
186      A6=LLENGL(I)
187      A7=LLENGL(I)
188      A8=DEFLC(I)
189      A9=DEFLC(I)
190      A10=DEFLC(I)
191      A11=DENSFLC(I)
192      B1=B1,A1
193      A2=52*12
194      B3=53*13
195      B4=54*14
196      B5=55*15
197      B6=B6*16
198      R9=3*9*9
199      IF(I,EW,KAIG) WRITE(6,99)
200      WRITE(6,500) (A1,A2,A3,A4,A5,A6,A7,A8,A9
201 55 CONTINUE
202      WRITE(6,655) B1,B2,B3,B4,B5,B6,B7
C
203      IF(IPROF,NE,1) RETURN
C***** DETAIL TEMPERATURE DISTRIBUTION PRINT OUT (IF IPROF,EW,1 ONLY)
C
204      CALL HEAD(4)
205      NMING = 50
206      WRITE(6,661)
C
207      DO 71 I=1,NPOX,I
C
208      II = I
209      IO = I + 6
210      IF(16,JE,NPOX) IO = NPOX
211      WRITE(6,662) (INODE,II,II=I,16)
212      WRITE(6,663) (IDUMB,II=I,16)
213      WRITE(6,673) (IDUMB,II=I,16)
214      WRITE(6,664) (TCOLT(II),II=I,16)
C
215      DO 72 J=1,16
216      XDDM1(J)=COX(J)/2. + DRCLD(J)
217      XDDM2(J)=COX(J)/2. + DRCLD(J)
218 72 CONTINUE
C
219      WRITE(6,665) (XDDM1(II),TCOC(II),II=I,16)
220      WRITE(6,666) (XDDM2(II),TCIC(II),II=I,16)

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* SOURCE STATEMENT (PRINT11) *

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221      WRITE(6,667) (16AFC(I),I=1,16)          PRIN3550
222      WRITE(6,668) (BR4(I),TFSCL(I),I=1,16)      PRIN3560
223      K=5                                         PRIN3570
224      DO 73 I=1,16                                PRIN3580
225      XDU3(I)=BR4(I)-(SF4(I)-BR1(I))/FLOAT(NRING)*FLOAT(*)  PRIN3600
226      WRITE(6,669) K,(ALUM3(I)+DC(I),I=1,16)      PRIN3610
227      DO 74 K=10,NRING+5                         PRIN3620
228      IF(K.GE.NRING) GO TO 74                  PRIN3630
229      DO 75 I=1,16                                PRIN3640
230      XDU3(I)=BR4(I)-(SF4(I)-BR1(I))/FLOAT(NRING)*FLOAT(*)  PRIN3650
231      XDU3(I)=BR4(I)-(SF4(I)-BR1(I))/FLOAT(NRING)*FLOAT(*)  PRIN3660
232      CONTINUE                                     PRIN3670
233      WRITE(6,671) (BR1(I),TCLINE(I),I=1,16)      PRIN3680
234      WRITE(6,672)                               PRIN3690
235      /* CONTINUE                                     PRIN3700
236      RETURN                                     PRIN3710
237      * 1 * 2 * 3 * 4 * 5 * 6 * 7 PRIN3720
238      * 1 * 2 * 3 * 4 * 5 * 6 * 7 PRIN3730
239      99 FORMAT(1H )                                PRIN3740
240      100 FORMAT(1H )                                PRIN3750
241      101 FORMAT(3X,12TH AXIAL AXIAL LAGRANGE HEAT    PRIN3760
242      102 FORMAT( AVERAGE COOLANT FILM COEFFICIENT CLAD UPK1,V1,I0  PRIN3770
243      103 FORMAT(2D SURFACE / 3X,12TH SECTION DISTANCE RATING      PRIN3780
244      104 FORMAT( NEUTRON TEMP. BTU      PRIN3790
245      105 FORMAT( 4 HEAT FLUX / 3X,12TH NUMBER (CM) CINCH) (W/CM) (K/W/FT) PRIN3820
246      106 FORMAT( 5 (AUX1) FLUX (W) (WT/CM2-C) /HR=F12-F WATPRIN3830
247      107 FORMAT( 6 T CM2-C10/F12-F2 /      PRIN3840
248      108 FORMAT( 7 3X7(1H-),2X14(1H-),4X18(1H-),4X8(1H-),2X10(1H-),2X8,8(1H-),4X12(1H-),4X22(1H-),2X17+F8,2+2X2F10,4+2A,F4,2+2X1PE10,2+2A+2F12,3PRIN3850
249      109 FORMAT( 12X4,17+F8,2+2X2F10,4+2A,F4,2+2X1PE10,2+2A+2F12,3PRIN3860
250      110 FORMAT( 12X4,2F12,3 )      PRIN3870
251      201 FORMAT(5X)                               PRIN3880
252      202 FORMAT(5X,CLAD OD CLAD ID CLAD THERPRIN3930
253      * 203 * 204     GAP FUEL SURFACE NO, OF GAP = PRIN3910
254      * 205 * 206     AXIAL TEMPERATURE TEMPERATURE CONDUCTIVITPRIN3930
255      * 207     AVERAGE TEMPERATURE HEAT FLUX CONDUCTANC PRIN3940
256      * 208     +12TH SECTION TEMPERATURE (ATT / (HTPRIN3950
257      * 209     ) / ITERATIONS PRIN3970
258      203 FORMAT(5X,4
259      * 209 NUMBER (DEG C) (DEG C) (DEG F) CM2-C) HR=PRIN3990
260      * 210 (CUG C) (DEG F) (WT/CM2-C10/F12-F2) 1 2 3 4 PRIN4000
261      * 211 3X7(1H-),2X14(1H-),3X11,16(1H-),3X8,20(1H-),3X1,16(1H-),4 PRIN4010
262      * 212 3X12(1H-),3X17(1H-),4 PRIN4020
263      204 FORMAT(7X,13TH AXIAL GAP CONDUCTANCE (BTU/HR=F12-F) GAS TPRIN4070
264      205 FORMAT(13X,13TH AXIAL INCREASE IN FUEL RADIUS(MM) INCREASE IN CLAD RADIUS(MM)PRIN4080
265      206 1000 INTEGRAL RELEASE JUMP PRIN4090
266      207 RADIAL 3X132TH SECTION SOLID GAS* RELEASE JUMP PRIN4100
267      208 THERMAL THERMAL * PRIN4110
268      209 HOT GAP 6 / 2X132TH NUMBER -BOTH CONDUCT RADIANT TOTAL RATE DIST. PRIN4130

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* SOURCE STATEMENT (PRINT11) *

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271      741 EXPANSION SWELLING TOTAL EXPAND CREEP PRESSURE SOTALPRIN4140
272      8 (MM)                               PRIN4150
273      9 / 2X7(1H-),4(1X7(1H-)),2X7(1H-),2X8,3(1H-),2X1 PRIN4150
274      * 5X(1H-),2X1(1H-))      PRIN4170
275      742 FORMAT(2X,17+F8,2+2X17,5,2A,F4,5,SF10,6+2X4+5,5+2X,F4,5,1X,A1) PRIN4180
276      743 FORMAT(1 1 2 * 3 * 4 * 5 * 6 * 7 PRIN4190
277      4,1 FORMAT(2X,13TH AXIAL FUEL FUEL FUEL VOL, AVG FUEL BOUPRIN4200
278      1000 RADIUS (MM) PERCENT CHANGE FILL GAS CONFRIN4210
279      2A1 CLAD ID PRIN4220
280      3 / 2X130TH SECTION SURFACE CENTER FUEL CENTRAL 1700 PRIN4230
281      4 1350 ORIGINAL RADIUS CONDUCTIVITY PRESSURE PRIN4230
282      5 THERMAL PRIN4230
283      6 / 2X130TH NUMBER TEMP. TEMP. TEMP. VOID DEG C PRIN4230
284      7 100 C SURFACE FUEL OD CLAD ID CAL/SEC BTU / PRIN4270
285      8 STRESS PRIN4280
286      803 FORMAT(3X,132H CUG C) (CUG C) (DEG F) (CM2) (HR=F12-F) (KG/CM2) PRIN4290
287      140 (CM2) (HR=F12-F) (KG/CM2) (HR=F12-F) (KG/CM2) PRIN4310
288      220 (KG/CM2) * 12X7(1H-),1X3(2X8(1H-)),2X34(1H-),2(2X8(1H-)),2(2X8(1H-)) PRIN4320
289      * 3 PRIN4330
290      402 FORMAT(2X,17,1X,3+10,3,4F9.5,2F9.4,2F10,3) PRIN4340
291      501 FORMAT(10A,35HPLenum VOLUME ,F12.5+14H (CM3) PRIN4360
292      1 * 5X,F12.5+14H (CINCH3) ) PRIN4370
293      502 FORMAT(10A,35HPLenum TEMPERATURE ,F12.5+14H (DEG CF) PRIN4380
294      1) * 2A,F12.5+14H (DEG F) ) PRIN4390
295      503 FORMAT(10A,35HINITIAL PLenum PRESSURE ,F12.5+14H (KG/CM2) PRIN4400
296      12) * 5X,F12.5+14H (PSI) ) PRIN4410
297      504 FORMAT(10A,35HGASAT Saturate TEMPERATURE ,F12.5+14H (DEG CM) PRIN4420
298      1) ) PRIN4430
299      505 FORMAT(10A,35HGASAT INTERNAL GAS PRESSURE ,F12.5+14H (KG/CM2) PRIN4440
300      12X * 5X,F12.5+14H (PSI) ) PRIN4450
301      505 FORMAT(10A,35HTOTAL GAS MOLES IN A PIN ,E12.5+14H (MOLES) PRIN4460
302      1) ) PRIN4460
303      506 FORMAT(10A,35HGASES IN PLenum ,E12.5+14H (MOLES) PRIN4490
304      1) ) PRIN4500
305      507 FORMAT(10A,35HGASES IN A GAP ON CENTRAL VOID ,E12.5+14H (MOLES) PRIN4510
306      1) ) PRIN4520
307      512 FORMAT(2X,17,2X+2F10,3, 3CX2F10,3) ) PRIN4530
308      513 FORMAT(10X,65HAXIAL VOLUME-TEMPERATURE AVERAGED (CONVERGENCE PRIN4540
309      1 IN ITERATION) /1X5,5HITER,0X,11HTEMPERATURE,11X,14HINNER PRESSPRIN4550
310      2UMS / 2X13H(DEG C) (DEG F),7X,18H(KG/CM2) (PSI) ) PRIN4560
311      514 FORMAT(2X,14+1X+2F10,3,5X,F2F10,3) PRIN4570
312      515 FORMAT(10A,35HFp GAS RELEASED RATE (PIN AVERAGE) ,F12.5+14H (MFAC) PRIN4580
313      1(ON) ) PRIN4590
314      508 FORMAT(10X,BUFCOMPOSITION OF PIN GAS (MOLES) / 10X,30(1H-)// PRIN4600
315      1 2A1 964 INITIAL FUEL GAS GENERATED IN FUEL RELEASED PRIN4610
316      2 GAS CUMULATED GAS FRACTION / PRIN4620
317      3 2GX,3(5X,15(1H-)),10X,15(1H-),5X8(1H-)) PRIN4630
318      509 FORMAT(12A,244+3(5X,15(1H-)),10X,F12.10+5X,F8.6) PRIN4640
319      510 FORMAT(12A,8(1H-),3(5X,15(1H-)),10X,15(1H-),5X8(1H-)) PRIN4650
320      1 13X,5HTOTAL,3(5X,F15.10),10X,F15.10) PRIN4660
321      511 FORMAT( / 10X,13(1H-)/ PRIN4670
322      1 23X,9H AXIAL * 89HNOMINAL HEAT CAPACITY PRIN4680
323      2 STORED ENERGY VOLUME AVERAGE STORED ENERGY /PRIN4690
324      3 23X,7HSECTION,50X,41H STORED ENERGY PER UNIT LENGTH /PRIN4700
325      4 23X 9H NUMBER CAL/K-MOLE BTU/LB-F CAL/GRAM BTU/LB CPRIN4710
326      5 5AL/GRAM BTU/LB CAL/CM BTU/FOOT /23X,7(1H-),2X+20(1H-), PRIN4720

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* SOURCE STATEMENT (PRINT1) *

```
6 5X,18(1H-),5X,18(1H-),5X,18(1H-)) PRIN4730
266 610 FORMAT(19X,40HCONVERGENCE RELATIVE ERROR (FRACTION) ,F8.5, PRIN4740
1 5X, 35H(CONVERGENCE CRITERION 0.005) ) PRIN4750
267 620 FORMAT( 135H AXIAL DENSIFICATION RELOCATION RESTRUCTURINGPRIN4760
1 CENTRAL VOID (HOT) RADIUS FOR NEXT STEP PRIN4770
2MM) / PRIN4780
3 135H SECTION FICATION RADIUS TEMP. PRIN4790
4 RADIUS LENGTH VOLUME CENTRAL PELLET CLAD INNEPRIN4800
5R CLAD GUTER / PRIN4810
6 135H NO. (MM) (MM) (MM) (MM) (DEG)PRIN4820
7 C) (MM) (MM) (CUB MM) VOID SURFACE SURFACEPRIN4830
8 SURFACE / PRIN4840
9 1X,7(1H-),3X,2(2X,10(1H-)),2X,30(1H-),2X,40(1H-),1H- )PRIN4850
268 630 FORMAT(6X,12,3X,2F12.6,2X,F10.2,2X,3F10.5,2X,4F10.5) PRIN4860
269 640 FORMAT( 135H AXIAL PELLET ELONGATION LENGTH (CM) PRIN4870
1 DISH PELLET AXIAL DENSIFICATION PRIN4880
2 / PRIN4890
3 135H SECTION DISH (COLD - (CPRIN4900
4 OLD - SHOULDER DENSIFIED DENSIFIED DENSIFY + PRIN4910
5 / PRIN4920
6 135H NO. COLD SHOULDER CENTER DISH) PRIN4930
7 CENTER TEMP. (C) CATION LENGTH(CM) EXPANSION PRIN4940
8 / PRIN4950
9 1X,7(1H-),3X,50(1H-),2X,10(1H-),1X,3(2X,1U(1H-)) ) PRIN4960
270 650 FORMAT(6X,12,3X,5F+0.4,2X,F10.2,1X,3F12.5) PRIN4980
271 655 FORMAT(7 1X,7H(TOTAL),3X,5F10.4,25X,2F12.5) PRIN4990
272 661 FORMAT( 40X,35HDETAIL TEMPERATURE DISTRIBUTION PRIN5000
1 40X,33(1H-)/ PRIN5010
273 662 FORMAT(1X,14HAXIAL SECTION ,7(1X+A4,13+3X) ) PRIN5020
274 663 FORMAT(1X,14X,7CA1,16HRADI(CMD) TEMP(C) ) ) PRIN5030
275 664 FORMAT(1X,14HCLAD(LANT ,7(17.1) PRIN5040
276 665 FORMAT(1X,14HCLAD OD ,7(1X+F8.4, F8.1) ) PRIN5050
277 666 FORMAT(1X,14HCLAD ID ,7(1X+F8.4, F8.1) ) PRIN5060
278 667 FORMAT(1X,14HGAvg. TEMP ,7F17.1 ) PRIN5070
279 668 FORMAT(1X,14HPELLET SURFACE,7(1X+F8.4, F8.1) ) PRIN5080
280 669 FORMAT(1X,11HRADIAL NODE,15,7(1X+F8.4, F8.1) ) PRIN5090
281 670 FORMAT(1X,11X, 15,7(1X+F8.4, F8.1) ) PRIN5100
282 671 FORMAT(1X,14HPELLET CENTER ,7(1X+F8.4, F8.1) ) PRIN5120
283 672 FORMAT(/) PRIN5130
284 673 FORMAT(1X,14(1H-),7(41,16(1H-)) ) PRIN5140
285 C + 1 * 2 * 3 * 4 * 5 * 6 * 7 PRIN5150
C END PRIN5160
PRIN5170
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* SOURCE STATEMENT *

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1      SUBROUTINE PRINT2          PRI20010
C                                         PRI20020
C***** NEW SHORT OUTPUT ROUTINE          PRI20030
C                                         PRI20040
2      REAL LFUEL,LF,MOL , MOLEFR          PRI20050
C-----                                     PRI20060
3      COMMON /MOL678/ MOLEFR(6)          PRI20070
4      COMMON /ML5938/ TBAR(20)          PRI20080
5      COMMON /MOL9 / FXMOL(6,21)+RDOT(20)          PRI20090
6      COMMON /MOL579/ PHESTO(20)          PRI20100
7      COMMON /MOLM9 / TAVERG(20)          PRI20110
8      COMMON /COM39 / HFLUX(20)          PRI20120
9      COMMON /COM89 / HGK(20),RGAPX(20),TCLINE(20)          PRI20130
10     COMMON /BURN / BURN(20),BUOLD(20)          PRI20140
11     COMMON /MOLPR1/ GMOL(6),GMOL(6),FRACTN(6),MOL(6),XMOLS(21)          PRI20150
12     COMMON /PKINOL/ TCOLT(20),TCOLA(20),TCICA(20),          PRI20160
*      CCONE(20),TGAPC(20),HFLXFB(20),GCS(20),GGC(20),          PRI20170
*      GCR(20),GCT(20),TJUMP(20),DRTF(20),DRSF(20),          PRI20180
*      DRFC(20),DRTC(20),DRPC(20),DRCLD(20),TFSCA(20),          PRI20190
*      DRCC(20),BR1(20),BR2(20),BR3(20),BR4(20),          PRI20200
*      RATE(20),RATC(20),CPRES(20),CSTRES(20),GASC(20),          PRI20210
*      GASCB(20),ITERZ(20)          PRI20220
13     COMMON /PRIN02/ CP1(20),CF2(20),ST1(20),ST2(20),          PRI20230
*      ST3(20),ST4(20),ST5(20),ST6(20)          PRI20240
14     COMMON /PRIN03/ DRDF(20),DRKF(20),FCONT(20),TDISH(20)          PRI20250
C-----                                     PRI20260
15     COMMON /INPUT / FRDEN ,FRSIN ,DSINZ ,FRPU02,FH35 ,FR40 ,FR41 ,PRI20270
1      DFS ,DCI ,DCO ,DVUDZ ,VPLNZ ,ATMOS ,S ,XX ,PRI20280
2      ROUN ,ROUC ,LEXP ,LDE ,V ,TINLET ,DELT ,TMAX ,TFR ,TM ,PRI20290
3      OBO ,OBK ,BBC ,SIGMF ,IFLUX ,INCLAD ,NCON ,NFLX ,KOOL ,PRI20300
4      NEWK ,NEWCL ,NEWFLX ,VOIDL ,NOH ,FRACKE ,FRACAR ,FRACH ,PRI20310
5      FACHN ,FRACKR ,FRACKE ,HGACEL ,ITEMP ,ITOT ,HG ,PEKAVG ,PRI20320
6      MINI ,ICDF ,ISTOM ,ICREP ,ISHELL ,NEXP ,NEXP ,INHIST ,PRI20330
COMMON /COM 08/ I1,JCASE,TCOL0+MOTOT          PRI20340
COMMON /COM 10/ VV0ID2,FRU02+TLENAA,INPOW1          PRI20350
COMMON /POWRAY/ PAVRG ,LFUEL ,POWER(21)          PRI20360
1      A1(21),NPOW ,PTOT ,LPMAX ,PKPWR          PRI20370
2      LPEAK ,DEL ,PMAX ,PRI20380
COMMON /BHNNGAS/ NKR(20),NXE(20),PH1(20),ENXE(20),ENKR(20)          PRI20390
COMMON /COM 02/ IPCN ,ISTEP ,ITER ,KOUNT          PRI20400
COMMON /COM 05/ BURNUP ,TDAYA ,VV0ID ,TOTLDY ,TOTBUR          PRI20410
COMMON /MEM01 / MEM01(20,5) ,HATA(20)          PRI20420
COMMON /FFMOL / FF(6,23),KKR(6,23)          PRI20430
COMMON /PRIMOL / AAHK ,AAHXE          PRI20440
COMMON /DIMEN1/ DVGIDX(20),DVGIDH(20),DFSX(20),DCIX(20),DCOX(20)          PRI20450
1      VV0IDX(20),VV0IDH(20),TSINK(20),RSINK(20)          PRI20460
2      +ZLENGT(5,20),VCDL(20)          PRI20470
COMMON /COM3P / TSAT          PRI20480
COMMON /NUCLE1/ NUCLE1,A(40,23)          PRI20490
COMMON /COM128/ IOUT1 ,TIPRF          PRI20500
COMMON /COM49P/ DC(20,51) ,IPRF          PRI20510
COMMON /DIMEN2/ DENSFL(5,20)          PRI20520
COMMON /RELO1/ RSAPC(20),RFS0(20),DEEXP(20)          PRI20530
COMMON /PLOT / IPLOT ,IPLOT          PRI20540
33     DIMENSION GMOLG(6)          PRI20550
C                                         PRI20560
34     DATA GMOLG / 6#0.0/          PRI20570
35     DATA KAIG / 0 /          PRI20580
36     DATA IDUMB /1H /          PRI20590

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* SOURCE STATEMENT (PRINT2) *

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37     DATA INODE /4HNODE/          PRI20600
C                                         PRI20610
38     IF(IPLOT.LE.0) GO TO 61          PRI20620
C                                         PRI20630
39     DUM=0.0          PRI20640
40     WRITE(6,TOTLDY)          PRI20650
41     NN = NPOW + 1          PRI20660
42     WRITE(6,(POWER(1)+I = 1, NN)          PRI20670
43     DO 10 I = 1 , NPOW          PRI20680
44     WRITE(6,BURN(1),TCOLT(1),TCICA(1),TFSCA(1),TCLINE(1),DRTF(1),          PRI20690
1      DRDF(1),DRSF(1),DRRC(1),RGAPX(1),DRTC(1),DRPC(1),          PRI20700
2      DRCC(1),GCT(1),CPRES(1),CSTRES(1),          PRI20710
3      PRESTO(1),MOLEFR(6),MOLEFR(6),ST1(1),          PRI20720
4      RATC(1),RATC(1),DUM + DUM + DUM          PRI20730
45     10 CONTINUE          PRI20740
46     C                                         PRI20750
47     61 CONTINUE          PRI20760
48     C                                         PRI20770
49     IF(NPOW.GT.15) KAIG = 10          PRI20790
50     IF(NPOW.GT.10,AND,NPOW.LE.15) KAIG = NPOW / 2 + 1          PRI20800
51     CALL HEAD(1)          PRI20810
52     DISI = -1.*LF/2.          PRI20820
53     PRINT 101          PRI20830
54     DO 11 I = 1 , NPOW          PRI20840
55     DISI = DISI + LF          PRI20850
56     A1 = DISI / 2.54          PRI20860
57     POWF = (POWER(1) + POWER(1+1))*.5          PRI20870
58     A2 = POWF/1000.*#30.48          PRI20880
59     A3 = #HFILM(1)*30.48**2 * 3600./1.8/1055.          PRI20890
60     IF(I.EQ.KAIG) PRINT 99          PRI20900
61     PRINT 102,I,DISI,A1,POWF,A2,BURN(1),PH(1),TCOLT(1),HFILM(1),A3,          PRI20910
1      TCICA(1)          PRI20920
62     11 CONTINUE          PRI20930
63     IF(NPOW.GE.20) PRINT 99          PRI20940
64     IF(NPOW.LT.20) PRINT 1000          PRI20950
C                                         PRI20960
65     PRINT 301          PRI20970
66     DO 31 I = 1 , NPOW          PRI20980
67     A2 = DRFT(1) *10,          PRI20990
68     A3 = DRSF(1) *10,          PRI21000
69     A4 = DRF (1) *10,          PRI21010
70     A5 = DRTC(1) *10,          PRI21020
71     A6 = DRCC(1) *10,          PRI21030
72     A7 = DRPC(1) *10,          PRI21040
73     A8 = DRCLD(1)*10,          PRI21050
74     A9 = RGAPX(1)*10,          PRI21060
75     A10 = GCS(1) * 1763,          PRI21070
76     A11 = GCG(1) * 1763,          PRI21080
77     A12 = GCR(1) * 1763,          PRI21090
78     A13 = GCT(1) * 1763,          PRI21100
79     A14 = DRDF(1) * 10,          PRI21110
80     A15 = DRRC(1) * 10,          PRI21120
81     A16 = DRPF(1) * 10,          PRI21130
C                                         PRI21140
82     IF(I.EQ.KAIG) PRINT 99          PRI21150
83     PRINT 302,I,A10 , A11 , A12 , A13 , A2 , A3 , A15 , A16 ,          PRI21160
1      A4 , A5 , A6 , A7 , A8 , A9 : FCNT(1)          PRI21170
84     31 CONTINUE          PRI21180

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* SOURCE STATEMENT (PRINT2)*

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82      CALL HEAD(-1)
83      PRINT 401
84      PRINT 403
85      DO 41 I = 1 , NPOW
86      A5 = CPRES(I)
87      IF(I.EQ.1) PRINT 93
88      PRINT 402,I,TFSCA(I),TCLINE(I),TBAR(I),CP1(I),CP2(I),ST1(I),ST2(I)
89      1           +ST3(I),ST4(I),ST5(I),ST6(I),A5
90      41 CONTINUE
91      PRINT 1000
92      C..... INFORMATION FOR GAS .....
93      A1 = VPLENZ/1.6,2871
94      PRINT 501,VPLENZ,A1
95      A1 = TPLENA - 273.
96      A2 = A1 * 1.8 + 32.
97      PRINT 502,A1 , A2
98      IF(SIGMF.LT.0.0) PRINT 516+TSAT
99      A1 = ATMOS * 14.22
100     PRINT 503+ATMOS , A1
101     A1 = PRESTO(ISTEP+1)*14.22
102     PRINT 504, PRESTO(ISTEP+1) , A1
103     C
104     PRINT 505, XMOTOT
105     PRINT 506, XMOLSI(NPOW+1)
106     A1 = XMOTU1 - XMOLSI(NPOW+1)
107     PRINT 507,A1
108     PRINT 515,RDUT(1)
109     C
110     PRINT 509, (MOLEFR(I),I = 1 + 6)
111     C
112     PRINT 1000
113     PRINT 513
114     DO 53 J = 1 , 1STEP
115     I = J + 1
116     AJ= TAVGXA(I)*1.8 + 32.
117     A2= PRESTO(I)*14.22
118     PRINT 514+ J + TAVGXX(I) + A1 + PRESTO(I) + A2
119     53 CONTINUE
120     ERROR = ABS((TAVGAX(ISTEP)-TAVGXX(ISTEP+1)) / TAVGAX(ISTEP+1))
121     PRINT 610 , ERROR
122     C
123     PRINT 640,(DELEXP(I),I=1,NPOW)
124     PRINT 620,(PGAPC(I),I=1,NPOW)
125     PRINT 630,(KFSO(I) , I=1,NPOW)
126     C
127     620 FORMAT(// 3X,'COLD RADIAL GAP AT THE END OF THIS STEP (MM)',*
128     1   /(5X,1F10F12.7) )
129     630 FORMAT(// 3X,'COLD PELLET SURFACE RADIUS (MM)' *
130     1   /(5X,1F10F12.7) )
131     640 FORMAT(// 3X,'!THERMAL EXPANSION OF HOT FUEL RADII FOR REDECE'*
132     1   ', TO COLD STATE (MM)' *
133     2   /(5X,1:10F12.7) )
134     C
135     RETURN
136     99 FORMAT(1H )
137     1000 FORMAT(1H )
138     101 FORMAT(2X,12TH AXIAL AXIAL LINEAR HEAT
139     1URUP AVERAGE COOLANT FILM COEFFICIENT CLAD TPR121760
140     2TEMPERATURE / 3X+129HSECTION DISTANCE RATING PR121770

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* SOURCE STATEMENT (PRINT2)*

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3          NEUTRON TEMP. BTU PR121780
4      UD ID/3X,131H NUMBER (CM) (INCH) (W/CM) (KWPR121790
5/FT) (MW/MT) FLUX (NV) (DEG C) WATT/C12-C /HRFT2-F PR121800
6      (DEG C) (DEG C) /
7      JX,7(1H-),2X,1*(1H-),4X,18(1H-),4X,8(1H-),2X,10(1H-),2X,8(1H-),
8      4X,22(1H-),6X,20(1H-)
124    102 FORMAT(3X,7.2F8.2+2X,2F10.4,2X,F10.2,2X,1PE10.3,0PF10.2+2X,2F12.3PR121840
1      ,2X,2F12.3)
125    301 FORMAT(2X,132H AXIAL GAP CONDUCTANCE(BTU/HR=F12-F) PR121860
1      INCREASE IN FUEL RADIUS(MMM) INCREASE IN CLAD RADIUS(PR121870
2MM) RADIAL / 2X+20+5SECTION SOLID GAS- ,
3      21X,7!THERMAL , 13X, 13HDENSI- RE- , 17X, PR121880
4      7!THERMAL ,2X , 7!HOT GAP /
5      3X ,13DHNUMBER -SOLID CONDUCT RADIANT TOTAL EXPANSION SPN121910
6!WELLING F.CATION LOCATION TOTAL EXPAN. CHEEP PRESSURE PR121920
7TOTAL (MM) /
8      1X,5(4H -----),2X,38(1H-),2X,8(1H-),2X,32(1H-),1X,7(1H-))PR121940
126    302 FORMAT(2X,17+FB8.2 ,5F10.6,1X,3F8.5,1X,2F8.5+1X,A1) PR121950
127    401 FORMAT(2X,130H AXIAL FUEL FUEL VOL. AVG NOMINAL HEPAR121960
1T CAPACITY S T O R E D E N E R G Y PR121970
2 CONTACT /
3      2X, 34HSECTION SURFACE CENTER FUEL ,30X ,15HAT VOLUPR121990
4METRIC 8X, 45HVOLUME AVERAGE PER UNIT LENGTH PRESSURE /PR122000
5      2X, 35H NUMBER TEMP. TEMP. , 31X , PR122010
6      13H AVERAGE TEMP. > PR122020
128    403 FORMAT(2X,122H(DEG C) (DEG C) CAL/K-MOLE BTU/LB=PR122030
1      CAL/GRAM BTU/LB CAL/GRAM BTU/LB CAL/CH BTU/FOOT (KG/CPN122040
2H2) /
3      2X,7(1H-),3X,7(1H-),3X,8(1H-),2X,8(1H-),2X,21(1H-),2X,
4      16(1H-), 3X ,17(1H-)+3X+17(1H-),3X,8(1H-)
129    402 FORMAT(2X,[7.1X,3F10.3,1X,2F11.3]2F9.3,2F10.3,1X,F10.3) PR122080
130    501 FORMAT(10X,35HPLENUM VOLUME
1      ,5X,F12.5,14H (INCH3) > ,F12.5,14H (DEG CPR122110
131    502 FORMAT(10X,35HPLENUM TEMPERATURE > ,F12.5,14H (DEG CPR122110
1      ,5X,F12.5,14H (DEG F) > ,F12.5,14H (KG/CM)PR122130
132    503 FORMAT(10X,35HINITIAL PLENUM PRESSURE > ,F12.5,14H (PSI) PR122140
133    516 FORMAT(10X,35HCoolant SATURATE TEMPERATURE > ,F12.5,14H (DEG CPR122150
1      ,5X,F12.5,14H (PSI) > ,F12.5,14H (KG/CM)PR122160
134    504 FORMAT(10X,35HINTERNAL GAS PRESSURE > ,F12.5,14H (KG/CM)PR122170
1      ,5X,F12.5,14H (PSI) > ,F12.5,14H (KG/CM)PR122180
135    505 FORMAT(10X,35HTOTAL GAS MOLES IN A PIN > ,E12.5,14H (MOLES)PR122190
1      ,5X,F12.5,14H (PSI) > ,E12.5,14H (MOLES)PR122200
136    506 FORMAT(10X,35HGASES IN PLENUM > ,E12.5,14H (MOLES)PR122210
1      ,5X,F12.5,14H (PSI) > ,E12.5,14H (MOLES)PR122220
137    507 FORMAT(10X,35HGASES IN A GAP OR CENTRAL VOID > ,E12.5,14H (MOLES)PR122230
1      ,5X,F12.5,14H (PSI) > ,E12.5,14H (MOLES)PR122240
138    515 FORMAT(10X,35HFPP GAS RELEASED RATE (PIN AVERAGE) > ,F12.5,14H (FRACT)PR122250
1      ,110D) > ,F12.5,14H (PSI) > ,F12.5,14H (FRACT)PR122260
139    509 FORMAT(10X,90HCOMPOSITION OF PIN GAS (MOLES) HELIUM ARGON PR122270
1      HYDROGEN NITROGEN KRYPTON XENON / 32X, 8HFRACTION,6F10.6)PR122280
140    513 FORMAT(10X,65HAXIAL VOLUME-TEMPERATURE AVERAGED (CONVERGENCE PR122290
2URE / 22X,18H(DEG. C) (DEG. F)-7X,18H(XG/CM2) (PSI) ) PR122310
141    514 FORMAT(15X,14,1X,2F10.3,5X,2F10.3) PR122320
142    610 FORMAT(10X,40HCONVERGENCE RELATIVE ERROR (FRACTION) + FB.5 , PR122330
15X , 30H(CONVERGENCE CRITERION 0.005) > ,PR122340
143    END > ,PR122350

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* SOURCE STATEMENT *

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1      SUBROUTINE PROF(TM,TCI,TCO,TCOOL,THH,MGDUM,JCASE,IPOW,NPOW,MINI,    PROF0010
*          ISTEP,LMAX)           PROF0020
C      THIS SUBROUTINE IS CALLED FROM STEP8           PROF0030
C      PROF0040
C      PROF0050
C      PROF0060
C      PROF0070
2      COMMON /COM_0/ TITLE(20),AA(7, 30),BB(6, 51),CF(3, 30),HV(2, 20) PROF0080
3      COMMON /COM_1/ 21,NN,MRN,NF           PROF0090
4      COMMON /COM_8/ 8M,ISTOP,JCASE           PROF0100
5      COMMON /COM49P/ DC(20,51),IPRF          PROF0110
6      COMMON /HIZKEE/ K1,K2,K3,K4,K5,K6           PROF0120
7      DIMENSION P(121),S16(25)           PROF0130
8      DIMENSION B(2,51),SY(20)           PROF0140
9      DATA SIGA/ 100/PELLET CENTER PELLET OUTER SURFACECLAD INNER SPROF0150
*      SURFACE CLAD OUTER SURFACE COOLANT           PROF0160
10     DATA SY / 1HA1HS,1HC,1HD,1HE,1HG,1HM,1HO,1HP,1HQ,1HR,1HS,1HT,PROF0170
*          1HM,1HV,1HW,1HX1HY1HZ /           PROF0180
11     *ARHJHI           PROF0190
12     CALL STEP8           PROF0200
13     WRITE(6,1710) JCASE,IPOW,NPOA,K1,K2,K3,K4,K5,K6           PROF0210
14     WRITE(6,6000) TITLE           PROF0220
15     IMAX = 120           PROF0230
16     JMAX = IMAX + 1           PROF0240
17     JMAX = N + 1           PROF0250
18     IF(IPRF) 20,20,22           PROF0260
19     DO 1 JJ=1,JMAX           PROF0270
20     J = JMAX - JJ + 1           PROF0280
21     DO 2 I=1,121           PROF0290
22     2 P(I)=1H           PROF0300
23     IP=1.0+FLOAT(IMAX)*BB(3,J)/3000.           PROF0310
24     IF(I>J,(IMAX+1)) IP = IMAX + 1           PROF0320
25     IF(I>LT,1) IP=1           PROF0330
26     I0 = 1           PROF0340
27     I1 = 1 + IMAX / 3           PROF0350
28     I2 = 1 + IMAX*2/3           PROF0360
29     I3 = 1 + IMAX           PROF0370
30     IF(JJ,EE,1,OR,JJ,EE,JMAX) GO TO 4           PROF0380
31     P(10)=P(11)=P(12)=P(13)=BAR           PROF0390
32     4 P(IP)=1H           PROF0400
33     IF(BB(3,J).GE.TM) P(IP) = 1HM           PROF0410
34     B(1<J) = BB(3,J)           PROF0420
35     B(2<J) = BB(4,J)           PROF0430
36     WRITE(6,602) BB(3,J),BB(4,J)+F           PROF0440
37     IF(JJ,EE,0,EE,JMAX) IFFEND = IP           PROF0450
38     IF(JJ,EE,1,EE) GO TO 1           PROF0460
39     IF(EH<4,JJ).LT.0.001) WRITE(6,602)           PROF0470
40     IF(EH<4,JJ).GE.0.001) WRITE(6,603)           PROF0480
41     1 CONTINUE           PROF0490
42     TIC=TCI           PROF0500
43     TCO=TCO           PROF0510
44     COOLT=TCOOL           PROF0520
45     DUMHG=MGDUM           PROF0530
46     GO TO 26           PROF0540
47     22 CONTINUE           PROF0550
48     DO 25 J=1,JMAX           PROF0560
49     J = JMAX-JJ+1           PROF0570
50     P(1,J) = BB(4,J)           PROF0580
51     R(2,J) = DC( LMAX,J)           PROF0590

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* SOURCE STATEMENT (PROF) *

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52     WRITE(6,701) B(1,J),R(2,J)           PROF0600
53     DO 23 I=1,121           PROF0610
54     23 P(I)=1H           PROF0620
55     DO 24 I=1,IPOW           PROF0630
56     IP=1.0+FLOAT(IMAX)*DC( 1,I)/3000.           PROF0640
57     IF(IP,GT,(IMAX+1)) IP=IMAX+1           PROF0650
58     IF(IP,LT,1) IP=1           PROF0660
59     I0=1           PROF0670
60     I1=1+IMAX/3           PROF0680
61     I2=1+IMAX*2/3           PROF0690
62     I3=1+IMAX           PROF0700
63     IF(JJ,EE,1,OR,JJ,EE,JMAX) GO TO 24           PROF0710
64     P(10)=P(11)=P(12)=P(13)=BAR           PROF0720
65     24 P(IP) = SY(1,I)           PROF0730
66     IF(DC( 1,I).GE.TM) P(IP) = 1HM           PROF0740
67     IF(JJ,EE,JMAX) IFFEND=IP           PROF0750
68     21 CONTINUE           PROF0760
69     WRITE(6,702) P           PROF0770
70     IF(JJ,EE,1,EE) GO TO 25           PROF0780
71     IF(BB(4,JJ,LT,0.001) WRITE(6,602)           PROF0790
72     IF(BB(4,JJ,GT,0.001) WRITE(6,603)           PROF0800
73     25 CONTINUE           PROF0810
74     26 CONTINUE           PROF0820
75     DO 6 I=1,121           PROF0830
76     6 P(I)=1H           PROF0840
77     P(10)=P(11)*BAR           PROF0850
78     IP = 1.0 + FLOAT(IMAX) * TIC / 3000.0           PROF0860
79     P(IP) = 1H           PROF0870
80     IF(T44,GT,0.0) GO TO 7           PROF0880
81     WRITE(6,604) P(I),I=1,IMAX           PROF0890
82     WRITE(6,605) DUMHG,TIC           PROF0900
83     GO TO 8           PROF0910
84     7 CONTINUE           PROF0920
85     DO 13 I=2,55           PROF0930
86     13 P(I) = RH           PROF0940
87     P(10)=P(11)*BAR           PROF0950
88     P(IPEND)=1H           PROF0960
89     WRITE(6,607) P(I)+I=1,55,DUMHG           PROF0970
90     DO 11 I=2,50           PROF0980
91     11 P(I)=1H           PROF0990
92     P(10)=P(11)*BAR           PROF1000
93     P(IP)=1H           PROF1010
94     WRITE(6,608) TIC,(P(I),I=1,41),(SIG(I),I=11,15)           PROF1020
95     9 CONTINUE           PROF1030
96     DO 9 I=1,121           PROF1040
97     9 P(I)=1H           PROF1050
98     DO 12 I=2,50           PROF1060
99     12 P(I)=1H           PROF1070
100    P(10)=P(11)*BAR           PROF1080
101    IP = 1.0 + FLOAT(IMAX) * TIC / 3000.0           PROF1090
102    P(IP)=1H           PROF1100
103    WRITE(6,606) TIC,(P(I),I=1,41),(SIG(I),I=16,20)           PROF1110
104    DO 10 I=1,121           PROF1120
105    10 P(I)=1H           PROF1130
106    P(10)=BAR           PROF1140
107    IP = 1.0 + FLOAT(IMAX) * COOLT / 3000.0           PROF1150
108    P(IP)=1HC           PROF1160
109    WRITE(6,609) COOLT,(P(I),I=1,41),(SIG(I),I=21,25)           PROF1170
110    WRITE(6,609) (P(I),I=1,41)           PROF1180

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* SOURCE STATEMENT (PROF) *

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111      30 IPRDF = 0                               PROF1190
112      RETURN                                     PROF1200
113      C   * 1   * 2   * 3   * 4   * 5   * 6   * 7   PROF1210
114      1710 FORMAT(IH1,2X,'CASE 1,13.5X,AXIAL SEGMENT ',I2,2X,'OF ',I2,2X,
115      * 22X, 244,15,3H,13,7H,MINUTE,I3,4H,SEC,I4)    / ) PROF1220
116      600  FORMAT(IH+, 5X,15(IH#),3X,20A4.3A,P(1H#)) / ) PROF1230
117      601  FORMAT(IH+, F6.0,1PF5.2,X,12I4)           PROF1240
118      602  FORMAT(IH+,13X,1HU,6(1H#),13HPELLET CENTER,18(IH#),4H1000,36(1H#)
119      1,4H2000*36(1H#),4H3000)                   ) PROF1250
120      603  FORMAT(IH+,13X,1H0,6(1H#),22HPELLET HAS CENTER HOLE,9(1H#),4H1000 PROF1260
121      1,36(1H#),4H2000,36(1H#),4H3000)             ) PROF1270
122      604  FORMAT(IH+, 13X,12I4)                   PROF1280
123      605  FORMAT(IH+, 13X,46(IH#),36H THERE IS NO GAP, GAP CONDUCTANCE IS PROF1290
124      1,F7.1,17H BTU/HRF/T2/DEG F /1H ,F6.0          / ) PROF1310
125      606  FORMAT(IH+,F6.0,7X,4I4,1,10X,9A4)         / ) PROF1320
126      607  FORMAT(IH+, 13X,55A1,36H THERE IS A GAP, GAP CONDUCTANCE IS PROF1330
127      1,F7.1,17H BTU/HRF/T2/DEG F                  / ) PROF1340
128      608  FORMAT( 14X,4I4)                         PROF1350
129      703  FORMAT(IH ,F5.3,F6.0 )                   PROF1360
130      702  FORMAT(IH+,13X,12I4)                   PROF1370
C   * 1   * 2   * 3   * 4   * 5   * 6   * 7   PROF1380
C*****                                         ***** PROF1400
129      END                                         PROF1410

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* SOURCE STATEMENT *

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1      SUBROUTINE RELOC(DELRRE,DESF,MAP,POW,IPWRK,IPON)      REL0010
1      & MRELLOC )                                         REL0020
C
C   REVISED MODEL (INCREMENTAL) 1976,JANU.                   REL0030
C
2      COMMON /PRIN03/ URDF(20),DRFF(20),FCNT(20),T0ISH(20)    REL0040
3      COMMON /COM89/ HGK(20),HGAP(20),TCLIRE(20)            REL0050
4      COMMON /EURN/ BURN(20),BULD(20)                      REL0060
5      COMMON /ATRY/ IATR1,IATR2,IATR3,IATR4,IATR5,IATR6,IATR7, REL0070
6      COMMON /POWERAY/ PAVG,FUEL,LF,POWER(21),AI(21),KPCN,PTOT,LPMAX,  REL0080
1      PKPDNK,IPACK,DELPH,PMAX                           REL0090
7      COMMON /CN02/ LP0W1,STEP1,TEN,KOUNT                REL0100
8      COMMON /REL01/ HGAPC(20),HFSQ(20),DELEAP(20)        REL0110
C
9      DIMENSION IMD(20),LREL0(20)                         REL0120
C
C   BURN   BURNUP AT EACH NODE AND TIME(MID/MTM)          REL0130
C   POW   LINEAR HEAT RATE DURING TIME INCREMENT(<W/FT)    REL0140
C   GAP   INITIAL MANUFACTURED DIAMETRAL GAP(INCHES)       REL0150
C
C
10     IF(IH.GT.1) GO TO 31                                 REL0160
11     RGAFC(IPON) = GAP / 2,                                REL0170
12     DRFF(IPON) = 0.0                                     REL0180
13     DREL0(IPON) = 0.0                                    REL0190
14     11 CONTINUE                                         REL0200
15     GO TO (1,2,2,4,5) + MRELLOC                         REL0210
16     4 CONTINUE                                         REL0220
17     DELGD=DREL0(IPON)                                   REL0230
18     KUN=BURN(IPON)                                     REL0240
19     P = POW*30,48/1000,                                REL0250
20     GAPR=GA4/2.54                                     REL0260
21     B=EXP(-4.*BUN**0.25)                               REL0270
22     DELGD=(42.*KA/(1.+B))+0.9*B+3.3*GAPR/100,        REL0280
23     IF(MRELLOC,EQ.3) DELGD=DELGD-0.28*GAPR           REL0290
24     IF(DELGD.LT.0.) DELGD=0.0                          REL0300
25     DCRE=DELGD/2.*2.54                                REL0310
26     DREL0(IPON)=ANAX1(DELRE,DREL0(IPON))           REL0320
27     DELRE=DREL0(IPON)                                REL0330
28     RETURN                                             REL0340
29     2 CONTINUE                                         REL0350
30     4 CONTINUE                                         REL0360
31     5 CONTINUE                                         REL0370
32     RETURN                                             REL0380
33     C
33     END                                             REL0390

```

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* SOURCE STATEMENT *

```

1      SUBROUTINE STOREN(CVAVGT,TSR,TFS,TT,N,PI,DFS,RHO)      STOR0010
1      C*NON,CPMIN,CPMAX,STORE,STOR,STORE,STOREC,STOREF,CPNOMF)  STOR0020
1      THIS SUBROUTINE CALCULATE THE HEAT CAPACITY OF UO2 AND   STOR0030
1      THE STORED ENERGY OF FUEL                                STOR0040
1      THIS SUBROUTINE IS CALLED FROM STEPS                      STOR0050
2      DIMENSION TT(100), TSR(100)                                STOR0060
2      ****CALL HCAP + CARL ****CALL HCAP + CARL ****CALL HCAP + CARL  STOR0070
3      CALL HCAP (CVAVGT,CPNOM,CPMIN,CPMAX)                      STOR0080
4      CALL CARL (TSR,TFS,TT,N,PI,DFS,STORE)                     STOR0090
4      *****TEMPK=AVGT+273.                                     STOR0100
5      TEMPK=AVGT+273.                                         STOR0110
6      C1=7.84/32E-4*(1EMPK**2-298**2)+5643730.*EXP(-37.6946/EMPK/0.0019)  STOR0120
6      1360,                                                 STOR0130
7      C2=535.285*(1.0/(EXP(535.285/EMPK)-1.)*1./((EXP(535.285/298.)-1.))  STOR0140
8      STOR=(C1+15.145*C2)/270.                                 STOR0150
9      STORE=STORE*1.5                                         STOR0160
10     STOREP=STORE*1.8                                       STOR0170
10     STOREL=STORE*RHG*(UFS**2/4)*PI*2.54**2                STOR0180
11     STOREC=STORE*RHG*(UFS**2/4)*PI*2.54**2                STOR0190
12     STORE=STOREP*12.*2.54/252.                               STOR0200
12     STORE=STOREC*12.*2.54/252.                               STOR0210
13     C        CONVERT CHROM TO UNITS OF RTU/(LB-DEG F)          STOR0220
14     CPNOMF=CPNOM*270.                                      STOR0230
14     RETURN                                                 STOR0240
15     END                                                 STOR0250
15

```

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* SOURCE STATEMENT *

```

1      SUBROUTINE SWELL(R1300,R1500,K1700,RFS,ROUD,PI,BURNUP,TH,GAP,DELRS)  SWEL0010
1      *T,DELRT,DELRRH,ROUC,THRE,DELRR,DELMD,*)                           SWEL0020
1      THIS SUBROUTINE IS CALLED FROM STEPS                      SWEL0030
1      REFP BNAL=1776. GAPCON THERMAL=1,PAGE 4-23               SWEL0040
1      SWEL0050
2      BFCC = BURNUP / 3500.                                    SWEL0060
3      S1700 = 14. * BFCC**.611/100.                            SWEL0070
4      S1500 = 5.0 * BFCC**.611/100.                            SWEL0080
5      S1400 = 2.0 * BFCC**.611/100.                            SWEL0090
6      STEMPS = 0.4 * BFCC/100.                                 SWEL0100
7      S17MAX = .213.                                         SWEL0110
8      S15MAX = .0754.                                         SWEL0120
9      IF(S1500.GE.S15MAX) S1500 = S15MAX                   SWEL0130
10     IF(S1700.GE.S17MAX) S1700 = S17MAX                   SWEL0140
11     DELVSTP1=(STEMPS*(S15**2-R1300**2)+S1300*(R1300**2-R1500**2)+S1500*SWEL0150
11     **(R1500**2-R1700**2)+S1700*(R1700**2-ROUD**2))  SWEL0160
12     DELRAH = DELVB/T ((3.*PI*RFS)                         SWEL0170
13     TH = GAP/2*(DELRT+DELRRH+DELMD) + DELRC              SWEL0180
13     ****DELRT+DELRRH+DELMD=TH+DELRC=TH                  SWEL0190
14     P01/G=1.93*(ROUF*ROUC) + 1.E-6.                      SWEL0200
15     IF(TH>ROUGH) 10.10*20.                                SWEL0210
16     10 CONTINUE                                           SWEL0220
16     C        GAP WAS CLOSED + THEN MODIFIED GAP WIDTH TO EQUAL MEAN ROUGHNESS SWEL0230
16     AND CONSTRAIN FUEL SHELLING AMOUNT                   SWEL0240
17     THREF=TH                                         SWEL0250
17     TH=1.93*(ROUF*ROUC)+1.E-6.                          SWEL0260
18     DELRRH=DELRRH                                         SWEL0270
19     DELRSH=GAP/2. .. (DELRT+DELMD)+DELRC=TH            SWEL0280
20     RETURN                                               SWEL0290
21     C        GAP IS OPEN                                SWEL0300
22     20 CONTINUE                                           SWEL0310
22     *****RETURN                                         SWEL0320
23     RETURN                                               SWEL0330
24     END                                                 SWEL0340

```

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* SOURCE STATEMENT *

```
1      SUBROUTINE SWELL(SWELL,M1300,R1350,R1500,R1700,RFS,RVOID,PI,BU, SWLA0010
1          SDOT,SDOTT,VOLUME,FRDEN,DELVB,DELRB) SWLA0020
C
C THIS SUBROUTINE IS CALLED FROM STEPSA SWLA0030
C REFER BNWL-1778, GAPCON THERMAL-1,PAGE 4-25 SWLA0040
2      DATA S15MAX,S17MAX / .0764 + .2138 / SWLA0050
C SWLA0060
C ISWELL = 0 SWELLING IS NOT TAKEN INTO ACCOUNT SWLA0070
C ISWELL = 1 GEITHOF, ET AL, MODEL (OLD SWELLING MODEL) SWLA0080
C ISWELL = 2 REVISED GAP CLOSURE MODEL (NEW SWELLING MODEL) SWLA0090
3      DELVB = DELRB = 0.0 SWLA0100
4      IF (ISWELL.EQ.0) RETURN SWLA0110
5      BFCC = BU * 3560, SWLA0120
6      GO TO 1111,2222,3333 1111 ISWELL SWLA0130
7      1111 CONTINUE SWLA0140
8      M=PI*(RFS**2-R1350**2) SWLA0150
9      V=C=PI*(R1350**2-R1700**2) SWLA0160
10     DELVB=(SDOT*VOLUME*FRDEN+SDOTT*VC)*BU /1,E4-(1,-FRDEN)+(.8*VH*. SWLA0170
11     13*VC+.3*VL) SWLA0180
12     RETURN SWLA0190
13     2222 CONTINUE SWLA0200
14     S1700 = 14. * BFCC**4.611/100. SWLA0210
15     S1500 = 5.0 * BFCC**4.611/100. SWLA0220
16     S1300 = 2.0 * BFCC**4.611/100. SWLA0230
17     S17MP = 0.4 * BFCC/100. SWLA0240
18     IF (S1500.GE.S15MAX) S1500 = S15MAX SWLA0250
19     IF (S1700.GE.S17MAX) S1700 = S17MAX SWLA0260
20     DELVA = PI*(STEMP*(RFS**2-R1300**2)+S1300*(R1300**2-R1500**2)+S1500* SWLA0270
     **(R1500**2-R1700**2)+S1700*(R1700**2-RVO*D**2)) SWLA0280
21     DELRA = DELVB / (3.4PI*RFS) SWLA0290
22     RETURN SWLA0300
23     3333 CONTINUE SWLA0310
24     RETURN SWLA0320
25     END SWLA0330
     SWLA0340
     SWLA0350
```

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* SOURCE STATEMENT *

```
1      FUNCTION TEPPU(TC,CRF,CRFT,N)
C THIS FUNCTION IS CALLED FROM MOLMOL(3)+(4)
C TEPPU IS A LINEAR INTERPOLATION FUNCTION WHOSE VALUE IS EQUAL TO TEPPU010
C THE INTERPOLATED VALUE. TEPPU020
C TC IS THE VALUE OF THE INDEPENDENT VARIABLE TEPPU030
C CRF IS DEPENDENT VARIABLE ARRAY TEPPU040
C CRFT IS INDEPENDENT VARIABLE ARRAY TEPPU050
C N IS NUMBER OF POINTS IN VARIABLE ARRAY TEPPU060
C DIMENSION CRF(N),CRFT(N). TEPPU070
2      T = 1 TEPPU080
3      IF(CRFT(1).GT.CRFT(N)) GO TO 200 TEPPU090
4
C     IF(TC.LT.CRFT(1)) GO TO 104 TEPPU100
5     DO 200 I=1,N TEPPU110
6     J = I TEPPU120
7     IF(TC-CRFT(I)).LT.0.102,100 TEPPU130
8     100 CONTINUE TEPPU140
9     104 TEMP = CRF(I) TEPPU150
10    106 RETURN TEPPU160
11    102 TEMP = CRFT(I) TEPPU170
12    RETURN TEPPU180
13    101 TEPPU=CRF(I)-((CRF(I)-CRF(I-1))*(TC-CRFT(I-1))/(CRFT(I)-CRFT(I-1))) TEPPU190
14    RETURN TEPPU200
15
C     200 CONTINUE TEPPU210
16     IF(TC.GE.CRFT(1)) GO TO 104 TEPPU220
17     DO 201 I=1,N TEPPU230
18     J = I TEPPU240
19     IF(TC-CRFT(I)).LT.0.102,101 TEPPU250
20     201 CONTINUE TEPPU260
21     104 TEPPU270
22     GO TO 104 TEPPU280
23     END ***** TEPPU290
     TEPPU300
     TEPPU310
     TEPPU320
     TEPPU330
```

* SOURCE STATEMENT *

```

1   FUNCTION TERP(TT, TABLE, LL, NN, IN1, IN2, IN3, IN4)          TERP0010
2   C THIS FUNCTION IS CALLED FROM STEP3,4,5,6,7,8,HTCH+FYIELD      TERP0020
3   C L = THE INDEX TO THE TABLE                                     TERP0030
4   C DIMENSION TABLE(IN1,IN2)                                       TERP0040
5   C
6   C N=NN                                                       TERP0050
7   C L=LL                                                       TERP0060
8   C IN2=0                                                       TERP0070
9   C
10  C IF(N) 30,30,31                                              TERP0080
11  30  WRITE(6,40) NN,IN2,IN4                                     TERP0090
12  STOP
13  31 CONTINUE
14  IF(N.GT.IN2) WRITE(6,41) NN,IN2,IN4
15  C IF(L.LE.1) WRITE(6,42) L,IN1,IN4                           TERP0100
16  IF(L.GT.1) STOP
17  IF(L.GT.IN1) WRITE(6,43) L,IN1,IN4
18  C
19  C I#1
20  IF(TABLE(I,1).GT.TABLE(I,N)) GO TO 110
21  IF(TT.LT.TABLE(I,1)) GO TO 104
22  IF(TT.GT.TABLE(I,N)) GO TO 106
23  DO 100 J=1,N
24  IF(TT>TABLE(I,J)) 101,102,100
25  100 CONTINUE
26  104 TEMP = TABLE(L,1)
27  IN3=1
28  CALL ERROR(IN3,IN4,TT)
29  RETURN
30  106 TEMP = TABLE(L,N)
31  IN3=1
32  CALL ERROR(IN3,IN4,TT)
33  RETURN
34  102 TEMP = TABLE(L+J)
35  RETURN
36  101 CONTINUE
37  IF(.NOT.(ABS(TABLE(I,J)-TABLE(I,J-1)).LT.1.E-10)) GO TO 109
38  STOP
39  109 CONTINUE
40  TEMP=TABLE(L,J-1)+(TABLE(L,J)-TABLE(L,J-1))*(TT-TABLE(I,J-1))/
41  (TABLE(I,J)-TABLE(I,J-1))
42  RETURN
43  110 IF(TT.GE.TABLE(I,1)) GO TO 104
44  IF(TT.LE.TABLE(I,N)) GO TO 106
45  DO 120 J=1,N
46  IF(TT>TABLE(I,J)) 120,102,101
47  120 CONTINUE
48  * 1 * 2 * 3 * 4 * 5 * 6 * 7
49  40 FORMAT(1H0,5X, 107H*INDEX ERROR IN (TERP)  SIYO SITEIRU MATH)TERP0560
50  1x NO GYOSUU GA ZEPU MATAKA MAINASU NANODE JOB O YAMEMASU N*IN2*, TERP0570
51  2 213, 12H CALLED FROM ,14)                                     TERP0580
52  42 FORMAT(1H0,5X, 106H*INDEX ERROR IN (TERP)  NAISO SAHERU RETU TERP0620
53  1NG BANGCO GA 1 IKA NANODE JOB O YAMEMASU, L,IN1*, TERP0630
54  2 213, 12H CALLED FROM ,14)                                     TERP0640
55  43 FORMAT(1H0,5X, 106H*INDEX ERROR IN (TERP)  NAISO SAHERU RETU TERP0650
56  1NG BANGCO GA MOTO NO DIMENSION YORI OKKII, L,IN1*, TERP0660
57  2 213, 12H CALLED FROM ,14)                                     TERP0670
58  600 FORMAT(5X,5HFUNCTION TERP(TT, TABLE, LL, NN, IN1, IN2, IN3, IN4) ERROR )TERP0680
59  610 FORMAT(5X,3HTT=12.5,5H, L1=.16,5H, L2=.16,5H, N=.16, TERP0690
60  1 .7H, IN1=.16,7H, IN2=.16,7H, IN3=.16,7H, IN4=.16, TERP0700
61  2 //10X,5HTABLE, )                                           TERP0710
62  620 FORMAT( 5X, 10CE12.5,1X )                                     TERP0720
63  ****
64  ENU

```

* SOURCE STATEMENT (TERP) *

```

1x NO GYOSUU GA NOTO NO DIMENSION YORT OKKII . N,IN2*, TERP0600
2 213, 12H CALLED FROM ,14)                                     TERP0610
42 FORMAT(1H0,5X, 106H*INDEX ERROR IN (TERP)  NAISO SAHERU RETU TERP0620
1NG BANGCO GA 1 IKA NANODE JOB O YAMEMASU, L,IN1*, TERP0630
2 213, 12H CALLED FROM ,14)                                     TERP0640
43 FORMAT(1H0,5X, 106H*INDEX ERROR IN (TERP)  NAISO SAHERU RETU TERP0650
1NG BANGCO GA MOTO NO DIMENSION YORI OKKII, L,IN1*, TERP0660
2 213, 12H CALLED FROM ,14)                                     TERP0670
600 FORMAT(5X,5HFUNCTION TERP(TT, TABLE, LL, NN, IN1, IN2, IN3, IN4) ERROR )TERP0680
610 FORMAT(5X,3HTT=12.5,5H, L1=.16,5H, L2=.16,5H, N=.16, TERP0690
1 .7H, IN1=.16,7H, IN2=.16,7H, IN3=.16,7H, IN4=.16, TERP0700
2 //10X,5HTABLE, )                                           TERP0710
620 FORMAT( 5X, 10CE12.5,1X )                                     TERP0720
*****
64  ENU

```

INPUT DATA LIST

CARD NO.*...1....*...2....*...3....*...4....*...5....*...6....*...7....*...8

1, *INPUT SAMPLE PROBLEM (TYPICAL PWR PIN)

2, FR35 = 0.03 , FRDEN = 0.927 , FRSIN = 0.960 , DFS = 0.3669 ,

3, DCI = 0.3734, DCO = 0.422 , LFUEL = 144, VPLENZ = 0.438 ,

4, ATMOS = 20, FRACHE = 1.0 , S = 0.017 , ROUF = 4.E-5 ,

5, ROUC = 2.E-5 , DTEMP = 64.8 , DDISH = 0.183 , SIGHT = -1, ,

6, DE = 0.5512, V = 13.973 , IFLUX = 1 , ISWELL = 1 ,

7, ICDF = -1 , INPOW = 10 , IPEAK = 0 , NEXP = 2 ,

8, MEXP = 4 , MDEN = 2 , MRLOC = 1 , IOUT1 = 1 ,

9, KUNIT = 0 , NUCLEI = 1 , IIPIRF = 1 , TM = 2850,

10, *

11, *
12, 0.0 0.0 545, 2250, -4-4 0 1
13, 1.0 4.0 545, 2250, 1
14, 2.0 8.0 545, 2250, -1
15, 10.0 15.0 545, 2250, -1
16, 50.0 15.0 545, 2250, -1
17, 200.0 15.0 545, 2250, -1
18, 202.0 0.0 77, 2250, 3
19, -1.0 *
20, *INPUT5
21, POWER(1) = .23 + .63 + .96 + 1.21 + 1.35 + 1.4 + 1.35 + 1.21 +
22, .96 + .63 + .23 *
23, STOP
24,

....*...1....*...2....*...3....*...4....*...5....*...6....*...7....*...8

END OF CARD

*
* SAMPLE PROBLEM (TYPICAL PWR PIN)
*

HISTORY DATA

TIME STEP NO.	IRRADIATION TIME (DAYS)	TIME INTERVALS (DAYS)	LINEAR HEAT RATE (W/CM) (KW/FT)	COOLANT TEMPERATURE (DEG C) (DEG F)	INLET (KG/CM2) (PSI)	COOLANT PRESSURE (KG/CM2) (PSI)	OPERATION MODE INPUT CONTROL SIGN					
							(1)	(2)	(3)	(4)	(5)	
1 **	0.0	0.0	0.0	0.0	285.000	545.000	158.23	2250.00	0	-4	-4	0 1
2 **	1.000	24.0	1.000	24.0	131.234	4.000	285.000	545.000	1	0	0	0 0
3 **	2.000	48.0	1.000	24.0	262.467	8.000	285.000	545.000	158.23	2250.00	-1	0 0 0 0 0
4	6.000	144.0	4.000	96.0	377.297	11.500	285.000	545.000	158.23	2250.00	0	0 0 0 0 0
5 **	10.000	240.0	4.000	96.0	492.126	15.000	285.000	545.000	158.23	2250.00	-1	0 0 0 0 0
6 **	50.000	1200.0	40.000	960.0	492.126	15.000	285.000	545.000	158.23	2250.00	0	0 0 0 0 0
7 **	200.000	4800.0	150.000	3600.0	492.126	15.000	285.000	545.000	158.23	2250.00	0	0 0 0 0 0
8	200.500	4812.0	0.500	12.0	369.094	11.250	220.000	428.000	158.23	2250.00	0	0 0 0 0 0
9	201.000	4824.0	0.500	12.0	246.063	7.500	155.000	311.000	158.23	2250.00	0	0 0 0 0 0
10	201.500	4836.0	0.500	12.0	123.031	3.750	90.000	194.000	158.23	2250.00	0	0 0 0 0 0
11 **	202.000	4848.0	0.500	12.0	0.0	0.0	25.000	77.000	158.23	2250.00	3	0 0 0 0 0

..NOTE.. (***) IS INPUT DATA (PEAK POWER)

OPERATION MODE

- (1) TEMPERATURE PROFILE PRINT-OUT OPTION =0 NOT PRINTED =1 DETAIL PROFILE PRINT =2 PLOT PROFILE BY LINE PRINTER
 (2) FUEL THERMAL CONDUCTIVITY CONTROLLER =0 NOT CHANGE =N N-TH DATA READ-IN =--N USE PREPARED EQUATION
 (3) CLADDING PROPERTY CONTROLLER =0 NOT CHANGE =N N-TH DATA READ-IN =--N USE PREPARED TABLE(ZRY2+ZRY4+ST)
 (4) RADIAL FLUX DEPRESSION CONTROLLER =0 NOT CHANGE =N N-TH DATA READ-IN =--1 USE SUBROUTINE DEPRES
 (5) AXIAL POWER PROFILE CONTROLLER =0 NOT CHANGE =1 NEW POWER DISTRIBUTION DATA READ-IN

I FREG3 OPTIONAL MODEL AND EQUATION I

***** FUEL THERMAL CONDUCTIVITY EQUATION ***** CONTROL SIGNAL,,,INPUT GROUP NO. 3 FORMATTED 12 COLUMN 73-74 K2=4
 ----INTEGRAL KDT (W/CM)---- FROM TO(DEG-C) AT RHO=0.95 0/2800 500/2800 ----(W/CM)---

K2 = (NCON),GT,0	:	READ IN TABLE FROM CARDS (INPUT GROUP NO. 5). NAMELIST INPUT2
K2 = 0	:	SAME AS PREVIOUS STEP.
K2 = (NCON) = -2	:	WARD DESIGN EQUATION (DENSITY,LT,0,95 FRACTIONAL).
K2 = (NCON) = -2	:	WARD DESIGN EQUATION (DENSITY,GE,0,95 FRACTIONAL)
K2 = (NCON) = -3	:	GODFREY EQUATION,
* K2 = (NCON) = -4	:	LYONS EQUATION. (DOCKET STN-50447-1 P,4,2-3)
K2 = (NCON) = -5	:	RESAR-41 EQUATION (DOCKET STN-50480-1 P,4,4-9)

***** CLADDING PROPERTIES ***** CONTROL SIGNAL,,,INPUT GROUP NO. 3 FORMATTED 12 COLUMN 75-76 K3=4
 K3 = (NCLAD),GT,0 : READ IN TABLE FROM CARDS (INPUT GROUP NO. 6). NAMELIST INPUT3
 K3 = 0 : SAME AS PREVIOUS STEP.
 K3 = (NCLAD) = -2 : ZIRCALOY-2 (BUILT IN DATA). REFER D= 964
 K3 = (NCLAD) = -4 : ZIRCALOY-4 (BUILT IN DATA). REFER D= 964
 K3 = (NCLAD) = -9 : 20-PERCENT COLD WORKED TYPE 316 STAINLESS STEEL.

***** CLADDING YIELD STRENGTH EQUATION ***** CONTROL SIGNAL,,,INPUT GROUP NO. 2 NAMELIST /INPUT/ IYIELD= 0
 IYIELD= 0 : YIELD STRENGTH IS USED FROM TABLE DATA WHICH IS ASSIGNED BY NCLAD.

***** RADIAL FLUX DEPRESSION ***** CONTROL SIGNAL,,,INPUT GROUP NO. 3 FORMATTED 12 COLUMN 77-78 K4= 0
 K4 = (NFLX),GT,0 : READ IN TABLE FROM CARDS (INPUT GROUP NO. 7). NAMELIST INPUT4
 K4 = 0 : FLAT (FIRST STEP), SAME AS PREVIOUS STEP (FROM SECOND STEP).
 K4 = (NFLX) = -1 : BUILT IN EQUATION (BESSSEL I-ZERO DISTRIBUTION) REFER D= 916,917

***** AXIAL POWER DISTRIBUTION ***** CONTROL SIGNAL,,,INPUT GROUP NO. 3 FORMATTED 12 COLUMN 79-80 K5= 1
 K5 ,GT,0 : READ IN TABLE FROM CARDS (INPUT GROUP NO. 8). NAMELIST INPUT5
 K5 = 0 : SAME AS PREVIOUS STEP.

***** IRRADIATION MODEL ***** CONTROL SIGNAL,,,INPUT GROUP NO. 2 NAMELIST /INPUT/ IFLUX = 1
 IFLUX = 0 : FAST FLUX IRRADIATION.
 IFLUX = 1 : THERMAL FLUX IRRADIATION.

***** LINEAR HEAT RATE ASSIGNMENT SIGNAL ***** CONTROL SIGNAL,,,INPUT GROUP NO. 2 NAMELIST /INPUT/ IPEAK = 0
 IPEAK,GT,0 : LINEAR HEAT RATE WHICH IS ASSIGNED BY GROUP-3-INPUT IS CONSIDERED TO ROD-AVG-VALUE.
 IPEAK,LE,0 : LINEAR HEAT RATE WHICH IS ASSIGNED BY GROUP-3-INPUT IS CONSIDERED TO ROD-PEAK-VALUE.

***** CLADDING CREEP ***** CONTROL SIGNAL,,,INPUT GROUP NO. 2 NAMELIST /INPUT/ ICREP = 0
 ICREP,GT,0 : READ IN TABLE FROM CARDS (INPUT GROUP NO. 4). FORMATTED F10.0, E10.0
 ICREP = 0 : NOT CREEP.
 ICREP = -2 : SAME AS ATR ZIRCALOY TUBE. J.NUCL.MAT. 41,(1971), P327. REFER D= 950
 ICREP = -3 : SAME AS PRESSURE TUBE. REFER D= 951
 ICREP = -4 : SAME AS FIGRO WAPD-TM 61B. REFER D= 952
 ICREP = -5 : ATR(NEW) MODEL. REFER D= 953

***** STORED ENERGY CALCULATION ***** CONTROL SIGNAL,,,INPUT GROUP NO. 2 NAMELIST /INPUT/ ISTOR = 0
 ISTOR = 0 : STORED ENERGY CALCULATION IS NOT PERFORMED.
 ISTOR,LT,0 : STORED ENERGY CALCULATION IS PERFORMED. REFER D= 700

***** HISTORY INPUT ***** CONTROL SIGNAL,,,INPUT GROUP NO. 2 NAMELIST /INPUT/ NHIST = 0
 NHIST = 0 : TIME DEPENDENT HISTORY.
 NHIST = 1 : BURNUP DEPENDENT HISTORY.

***** CLADDING ELASTIC DEFORMATION ***** CONTROL SIGNAL,,,INPUT GROUP NO. 2 NAMELIST /INPUT/ ICDF ==1
 ICDF = 0 : ELASTIC CLAD DEFLECTION NOT TAKEN INTO ACCOUNT.
 ICDF ,LT,0 : ELASTIC CLAD DEFLECTION TAKEN INTO ACCOUNT.

***** FUEL SWELLING MODEL ***** CONTROL SIGNAL,,,INPUT GROUP NO. 2 NAMELIST /INPUT/ ISWELL= 1
 ISWELL= 0 : FUEL SWELLING IS NOT TAKEN INTO ACCOUNT.
 ISWELL= 1 : GEITHOFF, ET AL, MODEL IS USED. USED IN GAPCON (CONSERVATIVE MODEL)
 ISWELL= 2 : REVISED GAP CLOSURE MODEL IS USED. USED IN GAPCON THERMAL-1 (OPTIONAL)

***** FUEL THERMAL EXPANSION EQUATION ***** CONTROL SIGNAL,,,INPUT GROUP NO. 2 NAMELIST /INPUT/ NEXP = 2
 ----THERMAL EXPANSION COEFF. AVERAGE DELTA,L/L/(T2-T1) 25/2800 500/2800 ----(/DEG-C)---

NEXP = 0	:	FUEL THERMAL EXPANSION IS NOT TAKEN INTO ACCOUNT.
NEXP = 1	:	ROTH AND HALTEMAN, (GAPCON) REFER D=812 1.1145E-5 1.1430E-5
*	NEXP = 2	: CONWAY,FINCEL AND HAIN (GAPCON THERMAL-1) REFER D=812 1.4978E-5 1.6354E-5

***** CALCULATE THE CALDDING-TO-COOLANT HEAT TRANSFER COEFFICIENT ***** CONTROL SIGNAL,,,INPUT GROUP NO. 2 NAMELIST /INPUT/ SIGHF = -1.000
 SIGHF,GT,0. : COOLANT IS UNSPECIFIED AND THE FILM COEFFICIENT WILL BE SET TO SIGHF.
 SIGHF = 0. : COOLANT IS LIQUID SODIUM. (PRESENTED HELO-TME 71-32, JUNE 1971).
 SIGHF = -1. : COOLANT IS WATER. (DITTUS-BEELTER EQUATION), REFER D= 929
 SIGHF = -2. : COOLANT IS WATER. (JENS LOTTE EQUATION) REFER D= 526
 SIGHF = -3. : SUBCOOL=DITTUS BEELTER, SATURATE=JENS LOTTE

***** FUEL THERMAL EXPANSION MODEL ***** CONTROL SIGNAL,,,INPUT GROUP NO. 2 NAMELIST /INPUT/ MEXP = 4
 MEXP = 1 : GAPCON MODEL, (MOST CONSERVATIVE)
 MEXP = 2 : PLASTIC MODEL, (AREA BALANCE TYPE)
 MEXP = 3 : TWO REGION MODEL, (HALF CRACK TYPE)
 MEXP = 4 : BRITTLE MODEL, (COMPLETE CRACK TYPE)

***** GAP CONDUCTANCE CONVERGENCE METHOD ***** CONTROL SIGNAL,,,INPUT GROUP NO. 2 NAMELIST /INPUT/ MCONV = 0
 MCONV = 0 : SIMILAR METHOD WHICH IS USED FOR GAPCON-THERMAL-1,
 MCONV = 1 : NEWTON-RAPHSON METHOD.

***** GAP CONDUCTANCE EQUATION ***** CONTROL SIGNAL,,,INPUT GROUP NO. 2 NAMELIST /INPUT/ MREV1 = 0

MREV1 = -1 : RESAR-41 EQUATION
 MREV1 = 1 : ROSS AND STOUTE EQUATION

***** FUEL DENSIFICATION MODEL ***** CONTROL SIGNAL...INPUT GROUP NO. 2 NAMELIST /INPUT/ MDEN = 2
 MDEN = 0 : DENSIFICATION IS NOT TAKEN INTO ACCOUNT.
 MDEN = 1 : HALDEN DENSIFICATION MODEL.
 MDEN = 2 : GAPCON-THERMAL=2 DENSIFICATION MODEL REFER D= 946

***** FUEL RELOCATION MODEL ***** CONTROL SIGNAL...INPUT GROUP NO. 2 NAMELIST /INPUT/ MRELOC= 1
 MRELOC= 0 : RELOCATION IS NOT TAKEN INTO ACCOUNT.
 MRELOC= 1 : GAPCON-THERMAL 2 RELOCATION MODEL REFER D=1123

***** TEMPERATURE DISTRIBUTION PRINTED ***** CONTROL SIGNAL...INPUT GROUP NO. 2 NAMELIST /INPUT/ TIPROF= 1
 TIPROF= 0 : RADIAL TEMPERATURE PROFILE IS NOT PRINTED.
 TIPROF= 1 : RADIAL TEMPERATURE PROFILE IS PRINTED.

***** RESTRUCTURING MODEL ***** CONTROL SIGNAL...INPUT GROUP NO. 2 NAMELIST /INPUT/ MREST = 0
 MREST = 0 : RESTRUCTURING CALCULATION ISNOT PERFORMED.
 MREST = 1 : RESTRUCTURNIG CALCULATION IS PERFORMED. REFER D= 936

***** FUEL CREEP ***** CONTROL SIGNAL...INPUT GROUP NO. 2 NAMELIST /INPUT/ LCREP = 0
 LCREP = 0 : FUEL NOT CREEP.
 LCREP = 1 : FUEL CREEP.

SAMPLE PROBLEM (TYPICAL PWR PIN)

76-09-09 9 HR 56 MINUTE

 * INPUT VALUES *

 * FUEL COMPOSITION
 * (1) 0.0 WEIGHT FRACTION PU02 FRPU02
 * 0.0, WEIGHT FRACTION PU239 FR39=1.-FR40+FR41
 * (2) 0.0 WEIGHT FRACTION PU240 FR40
 * (3) 0.0 WEIGHT FRACTION PU241 FR41
 * 1.0000 WEIGHT FRACTION U02 FRU02=1.-FRPU02
 * (4) 0.0300 WEIGHT FRACTION U235 FR35
 * 0.9700 WEIGHT FRACTION U238 FR38=1.-FR35
 * (5) FUEL DENSITY 0.92700(FRACTION TD)
 * RESTRUCTURED FUEL DENSITY 0.96000(FRACTION TD) 0.96000(FRACTION TD)
 * (6) 0.93193(CM) 0.36690(INCHES)
 * PELLET DIAMETER 0.0 (CM) 0.0 (INCHES)
 * (7) INITIAL RESTRUCTURED FUEL DIAMETER 0.0 (CM) 0.0 (INCHES)
 * (8) INITIAL CENTER HOLE DIAMETER 0.0 (CM) 0.0 (INCHES)
 * (9) PELLET-DISH DIAMETER 0.18300(CM) 0.07205(INCHES)
 * (10) PELLET-DISH DEPTH 0.01651(CM) 0.00650(INCHES)
 * (11) CLAD INSIDE DIAMETER 0.94844(CM) 0.37340(INCHES)
 * (12) CLAD OUTSIDE DIAMETER 365.76000(CM) 144.00000(INCHES)
 * (13) FUEL LENGTH 0.0 (CM) 0.0 (INCHES)
 * (14) SORBED GAS CONTENT 0.01700(CC/GRAM) 0.01700(CC/GRAM)
 * (15) FRACTION OF SORBED GAS WHICH IS H2 0.0 S XX
 * (16) PLenum VOLUME 7.17753(CU, CM) 0.43800(CU, IN.)
 * (17) AXIAL TEMPERATURE GRADIENT ACROSS CORE 36.00000(DEG C) 64.80000(DEG F)
 * (18) COOLANT PASSAGE EQUIVALENT DIAMETER 1.40005(CM) 0.55120(INCHES)
 * (19) COOLANT VELOCITY 4.25897(M/SEC) 13.97300(FT/SEC)
 * (20) FUEL SURFACE ROUGHNESS, ARITH, MEAN 0.10160E-03(CM) 0.40000E-04(INCHES)
 * (21) CLAD ID SURFACE ROUGHNESS ARITH, MEAN 0.50800E-04(CM) 0.20000E-04(INCHES)
 * (22) MELTING TEMPERATURE OF THE FUEL 2850.00000(DEG C) 5162.00000(DEG F)
 * (23) FILL GAS PRESSURE 20.00000(ATMOSPHERES) 20.00000(ATMOSPHERES) ATOMS
 * FILL GAS COMPOSITION
 * (37) 1.0000 MOLE FRACTION HELIUM FRACHE
 * (38) 0.0 MOLE FRACTION ARGON FRACAR
 * (39) 0.0 MOLE FRACTION HYDROGEN FRACH
 * (40) 0.0 MOLE FRACTION NITROGEN FRACN
 * (41) 0.0 MOLE FRACTION KRYPTON FRACKR
 * (42) 0.0 MOLE FRACTION XENON FRACXE
 * (43) COOLANT IS WATER (DITTUS-BOELTER EQUATION) SIGMF = -1.00
 * (44) THERMAL FLUX IRRADIATION IFFLUX = 1
 * (45) FUEL THERMAL EXPANSION IS TAKEN INTO ACCOUNT. NEXP = 2
 * (46) NUMBER OF AXIAL SEGMENTS (LIMIT OF 20) NPOW = 10
 * (47) FUEL DENSIFICATION IS TAKEN INTO ACCOUNT. MDEN = 2
 * (48) FUEL RELOCATION MODEL IS USED. MRELOC= 1
 * (49) RESTRUCTURING CALCULATION IS PERFORMED. MREST = 1
 * (50) THE HYDROGEN IS ASSUMED TO REACT WITH THE CLADDING NOH = 1
 * (51) ELASTIC CLAD DEFLECTION TAKEN INTO ACCOUNT. ICDF = -1
 * (52) GEITHOFF, ET AL., MODEL IS USED. ISWELL= 1
 * (53) STORED ENERGY CALCULATION IS NOT PERFORMED. ISTOR = 0
 * (54) A PEAK POWER NEEDS TO BE INPUT. IPKAF = 0
 * (55) RADIUS TEMPERATURE PROFILE IN FUEL PIN IS PRINTED IIPROF= 1
 * (56) FUEL THERMAL EXPANSION IS TAKEN INTO ACCOUNT. MEXP = 4
 * (57) GAPCON-THERMAL=1 ORIGINAL CONVERGENCE METHOD IS USED MCQNV = 0
 * (58) YIELD STRENGTH IS USED FROM TABLE DATA WHICH IS ASSIGNED BY NCLAD IYIELD= 0
 * (59) TIME DEPENDENT HISTORY NHIST = 0
 * (60) FISSION PRODUCTS YIELD PRINT OUT NUCLEI= 1
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* (48) FUEL THERMAL CONDUCTIVITY VALUES DETERMINED FROM DATA OF LYONS + ET AL      *
* (NCON)= -4
* TEMPERATURE          THERMAL CONDUCTIVITY
* (DEG C)             UNRESTRICTED FUEL           RESTRICTED FUEL
*                   (WATT/CM-C) (BTU/HR-FT-F)   (WATT/CM-C) (BTU/HR-FT-F)
* 0,      32,        0.092      5.301      0.097      5.578
* 300,    572,       0.053      3.043      0.055      3.202
* 600,    1112,      0.037      2.150      0.039      2.263
* 900,    1652,      0.029      1.693      0.031      1.781
* 1200,   2192,      0.025      1.440      0.026      1.516
* 1500,   2732,      0.023      1.312      0.024      1.380
* 1800,   3272,      0.022      1.273      0.023      1.339
* 2100,   3812,      0.023      1.309      0.024      1.377
* 2400,   4352,      0.024      1.414      0.026      1.488
* 2700,   4892,      0.027      1.585      0.029      1.668
* 3000,   5432,      0.032      1.825      0.033      1.920
*
*****
* (51) CLADDING IS ZIRCALOY-4
* (NCLAD)= -4
* (LYIELD)= 0
* TEMPERATURE          THERMAL CONDUCTIVITY      YIELD STRENGTH      YOUNGS MODULUS      POISONS RATIO      THERMAL EXPANSION COEFF,      MAYER HARDNESS
* (DEG C)             (W/CM/C)            (KG/CM2)           (KG/CM2)           (KG/CM2)           (C /C)           (KG/CM2)
* 25.0     0.12900     3150.0     0.97200E+06     0.370     0.58300E-05     9470.0
* 100.0    0.13600     2450.0     0.91400E+06     0.400     0.62500E-05     7360.0
* 200.0    0.14300     2450.0     0.91400E+06     0.400     0.62500E-05     7360.0
* 300.0    0.15200     2450.0     0.91400E+06     0.400     0.62500E-05     7360.0
* 400.0    0.16400     2450.0     0.91400E+06     0.400     0.62500E-05     7360.0
* 500.0    0.18000     2450.0     0.91400E+06     0.400     0.62500E-05     7360.0
*
*****
* (54) FLUX DEPRESSION VALUES USED
* (NFLX)= 2
* DIAMETER          FLUX RATIO
* ( CM )            (INCH)
* 0.0     0.0          1.0000
* 0.9319  0.3669      1.0000
*
*****
* ( ) AXIAL POWER DISTRIBUTION      SEGMENT NO.= 10,      NODAL POINT NO.= 11      POWER(11)
* INPUT      SEGMENT      .....AXIAL POWER DISTRIBUTION (SEGMENT MEAN).....      *
* VALUE       MEAN        MIN,          AVG,          MAX,      *
* TOP.....POWER(11)= 0.230000      POWER(10)= 0.630000      0.433031      *      |      |
*                  POWER( 9)= 0.960000      0.800604      |      *      |      |
*                  POWER( 8)= 1.210000      1.092649      |      |      *      |
*                  POWER( 7)= 1.350000      1.289023      |      |      |      *
*                  POWER( 6)= 1.400000      1.384693      |      |      |      *
*                  POWER( 5)= 1.350000      1.384693      |      |      |      *
*                  POWER( 4)= 1.210000      1.289023      |      |      *      |
*                  POWER( 3)= 0.960000      1.092649      |      |      |      *
*                  POWER( 2)= 0.630000      0.800604      |      *      |      |
* BOTTOM...POWER( 1)= 0.230000      POWER(10)= 0.433031      *      |      |

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STEP 2

SAMPLE PROBLEM (TYPICAL PWR PIN)

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(3)	LINEAR HEAT RATING(AVERAGE)	2,837 (KW/FT)	93,082 (WATT/CM)					
(4)	BURNUP (PIN AVERAGE)	7,612 (MW/MTU)	0.2565E+18 (FISSIONS/CC)					
(5)	TIME IN REACTOR	1,000 (DAYS)	24,000 (HOURS)					
(6)	COOLANT INLET TEMPERATURE	545,000 (DEG F)	285,000 (DEG C)					
(7)	COOLANT OUTLET TEMPERATURE	609,800 (DEG F)	321,000 (DEG C)					
(8)	COOLANT PRESSURE	2250,000 (PSI)	158,228 (KG/CM2)					
(9)	CUMULATED CP TIME	10,8440 (SEC)	COMPUTED TIME AT THIS STEP 7,6630 (SEC)					
(10)	AXIAL SECTION NUMBER	AXIAL DISTANCE (CM) (INCH)	LINEAR HEAT RATING (W/CM) (KW/FT)	BURNUP (MW/MT)	AVERAGE NEUTRON FLUX (NV)	COOLANT TEMP. (DEG C)	FILM COEFFICIENT BTU / H-FT2-F	CLAD OD SURFACE HEAT FLUX WATT / CM2 BTU / HR-FT2
1	18.29	7.20	40,3075	1,2286	3.30	6,845E+12	286,56	3,106 5470,923 11,962 37918,610
2	54.86	21.60	74,5219	2,2714	6.09	8,958E+12	289,44	3,096 5453,141 22,114 70101,682
3	91.44	36.00	101,7060	3,1000	8.32	1,223E+13	293,37	3,082 5428,721 30,179 95668,420
4	128.02	50.40	119,9850	3,6571	9.81	1,442E+13	298,02	3,070 5406,402 35,602 112856,953
5	164.59	64.80	128,8901	3,9286	10.54	1,549E+13	303,00	3,057 5384,042 38,242 121228,199
6	201.17	79.20	128,8901	3,9286	10.54	1,549E+13	307,98	3,049 5370,083 38,241 121224,430
7	237.74	93.60	119,9850	3,6571	9.81	1,442E+13	312,63	3,045 5363,277 35,598 112846,662
8	274.32	108.00	101,7060	3,1000	8.32	1,223E+13	316,56	3,043 5359,287 30,175 95654,576
9	310.90	122.40	74,5219	2,2714	6.09	8,958E+12	319,44	3,044 5361,862 22,110 70088,559
10	347.47	136.80	40,3075	1,2286	3.30	4,845E+12	321,00	3,044 5361,187 11,959 37910,461
(11)	AXIAL SECTION NUMBER	CLAD OD TEMPERATURE (DEG C) (DEG F)	CLAD ID TEMPERATURE (DEG C) (DEG F)	CLAD THERMAL CONDUCTIVITY (WATT / CM2-C) (BTU / HR-FT-F)	GAP AVERAGE TEMPERATURE (DEG C) (DEG F)	FUEL SURFACE HEAT FLUX WATT / CM2 BTU / HR-FT2	NO. OF GAP CONDUCTANCE ITERATIONS 1 2 3 4 5	
1	290,41	554,74	295,61	564,10	0,151368	8,749080	314,55 598,19 13,712 43467,90 2 5 2 2 0	
2	296,58	565,85	306,15	583,08	0,152157	8,794700	337,89 640,21 25,326 80283,43 2 5 2 2 0	
3	303,17	577,70	316,14	601,06	0,153150	8,852090	356,18 673,12 34,535 109477,11 2 4 2 2 0	
4	309,61	589,30	324,83	616,70	0,154058	8,904551	369,35 696,83 40,718 129075,84 2 4 2 2 0	
5	315,51	599,92	331,78	629,20	0,154828	8,949077	378,08 712,55 43,726 138610,68 2 3 2 2 0	
6	320,53	608,95	336,73	638,12	0,155427	8,983661	382,71 720,88 43,723 138603,41 2 2 2 2 0	
7	324,32	619,77	339,36	642,86	0,155812	9,005941	382,85 721,14 40,712 129056,88 2 2 2 2 0	
8	326,48	619,66	339,22	642,60	0,155934	9,012976	377,91 712,24 34,577 109451,93 2 4 2 2 0	
9	326,70	620,07	336,05	636,90	0,155759	9,002862	366,48 691,67 75,319 80260,43 2 4 2 2 0	
10	324,93	616,87	330,00	626,00	0,155292	8,975862	348,03 658,46 13,708 43454,36 2 5 2 2 0	
(24) ITERATION SUBTOTAL (THIS STEP)= 98								
(24) ITERATION TOTAL(UP TO THIS STEP)= 162								

(10)	SECTION NUMBER	GAP CONDUCTANCE(BTU/HR-FT2-F)	SOLID GAS-SOLID CONDUCT RADIANT	TOTAL	(25)	(26)	(27)	(28)	(29)	(30)	(31)
(11)	AXIAL SECTION NUMBER	GAS TEMP.	RELEASE JUMP DIST. MM	INCREASE IN FUEL RADIUS(MM)	INCREASE IN CLAD RADIUS(MM)	INCREASE IN CLAD RADIUS(MM)	RADIAL HOT GAP				
(12)	(13)	(14)	(15)	(16)	(17)	(18)	(19)	(20)	(21)	(22)	(23)
1	0.0	630,10	5.97	636,07	0,00030	0,000281	0,013084	0.0	0,018755	0,00794 0.0	-0,00532 0,00263 0,06642
2	0.0	693,10	6.72	699,82	0,00035	0,000294	0,016535	0.0	0,023508	0,00819 0.0	-0,00532 0,00288 0,06192
3	0.0	750,59	7.35	757,94	0,00039	0,000304	0,019505	0.0	0,027439	0,00844 0.0	-0,00532 0,00312 0,05823
4	0.0	795,34	7.83	803,17	0,00043	0,000312	0,021668	0.0	0,030227	0,00866 0.0	-0,00532 0,00334 0,05567
5	0.0	821,70	8.15	829,85	0,00044	0,000316	0,022886	0.0	0,031746	0,00885 0.0	-0,00532 0,00353 0,05434
6	0.0	826,92	8.33	835,25	0,00045	0,000319	0,023133	0.0	0,031993	0,00900 0.0	-0,00532 0,00368 0,05424
7	0.0	809,63	8.33	818,13	0,00044	0,000319	0,022367	0.0	0,030926	0,00909 0.0	-0,00532 0,00378 0,05540
8	0.0	772,22	8.14	780,35	0,00041	0,000316	0,020592	0.0	0,028526	0,00912 0.0	-0,00532 0,00381 0,05783
9	0.0	718,74	7.71	726,45	0,00037	0,000310	0,017883	0.0	0,024836	0,00968 0.0	-0,00532 0,00376 0,06146
10	0.0	657,40	7.05	664,45	0,00032	0,000300	0,014544	0.0	0,020216	0,00896 0.0	-0,00532 0,00365 0,06598
(32)	(33)	(34)	(35)	(36)	(37)	(38)	(39)				
AXIAL SECTION NUMBER	FUEL SURFACE TEMP. (DEG C)	FUEL CENTER TEMP. (DEG C)	VOL. AVG FUEL TEMP. (DEG C)	BOUNDARY VOID DEG C	RADIUS (MM)	PERCENT CHANGE IN ORIGINAL RADIUS	FILL GAS CONDUCTIVITY CAL/SEC BTU / SEC -CM-C HR-FT-F	CONTACT PRESSURE (KG/CM2)	CLAD ID THERMAL STRESS (KG/CM2)		
1	333,488	400,058	366,305	0.0	0.0	4,67839	0,4025 0,0683 0,00057 0,13777 0.0	-25,784			
2	369,634	503,520	434,839	0.0	0.0	4,68314	0,5045 0,0735 0,00058 0,14134 0.0	-47,422			
3	396,208	530,641	490,005	0.0	0.0	4,68707	0,5889 0,0767 0,00060 0,14402 0.0	-64,302			
4	413,867	612,751	528,388	0.0	0.0	4,68986	0,6487 0,0834 0,00060 0,14594 0.0	-75,411			
5	424,385	686,636	549,735	0.0	0.0	4,69138	0,6813 0,0874 0,00061 0,14721 0.0	-80,605			
6	428,689	672,245	554,669	0.0	0.0	4,69162	0,6866 0,0906 0,00061 0,14789 0.0	-80,295			
7	426,343	668,727	542,557	0.0	0.0	4,69056	0,6637 0,0926 0,00061 0,14791 0.0	-74,562			
8	416,597	615,823	512,720	0.0	0.0	4,68816	0,6122 0,0932 0,00061 0,14719 0.0	-63,154			
9	396,911	535,408	464,369	0.0	0.0	4,68449	0,5334 0,0923 0,00060 0,14552 0.0	-44,326			
10	366,064	435,536	400,314	0.0	0.0	4,67985	0,4339 0,0898 0,00059 0,14283 0.0	-25,132			

STEP 2 SAMPLE PROBLEM (TYPICAL PWR PIN)

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(60)	PLENUM VOLUME	7.17753 (CM3)	0.43800 (INCH3)
(61)	PLENUM TEMPERATURE	326.35556 (DEG C)	619.80000 (DEG F)
(62)	COOLANT SATURATE TEMPERATURE	344.85963 (DEG C)	
(63)	INITIAL PLENUM PRESSURE	20.00000 (KG/CM2)	284.40000 (PSI)
(64)	INTERNAL GAS PRESSURE	50.50336 (KG/CM2)	718.15785 (PSI)
(65)	TOTAL GAS MOLES IN A PIN	0.13166E-01 (MOLES)	
(66)	GASES IN PLENUM	0.71290E-02 (MOLES)	
(67)	GASES IN A GAP OR CENTRAL VOID	0.60373E-02 (MOLES)	
(68)	FP GAS RELEASED RATE (PIN AVERAGE)	0.00039 (FRACTION)	

COMPOSITION OF PIN GAS (MOLES)

	(49) INITIAL FILL GAS	(50) GENERATED IN FUEL	(51) RELEASED GAS	(52) CUMULATED GAS	(53) FRACTION
HELIUM	0.0131655168	0.0	0.0	0.0131655168	0.999942
ARGON	0.0	0.0	0.0	0.0	0.0
HYDROGEN	0.0	0.0	0.0	0.0	0.0
NITROGEN	0.0	0.0	0.0000061397	0.0000007511	0.000057
KRYPTON	0.0	0.0000061397	0.000000025	0.0000000025	0.000000
XENON	0.0	0.0000360169	0.000000147	0.000000147	0.000001
TOTAL	0.0131655168	0.0000421566	0.000007683	0.01316562851	

STORED ENERGY

	(10) AXIAL SECTION NUMBER	(54) NOMINAL HEAT CAPACITY CAL/K-MOLE BTU/LB-F	(55) STORED ENERGY CAL/GRAM BTU/LB	(56) VOLUME AVERAGE STORED ENERGY CAL/GRAM BTU/LB	(57) STORED ENERGY PER UNIT LENGTH CAL/CM BTU/FOOT
1	1	19.068	5148.368	22.351	40.563
2	2	19.369	5229.645	27.230	49.015
3	3	19.576	5285.587	31.210	56.177
4	4	19.707	5320.771	34.002	61.203
5	5	19.775	5339.246	35.563	64.013
6	6	19.790	5343.416	35.924	64.664
7	7	19.752	5333.114	35.037	63.067
8	8	19.655	5306.733	32.860	59.148
9	9	19.483	5260.466	29.355	52.839
10	10	19.224	5190.610	24.763	44.573

AXIAL VOLUME-TEMPERATURE AVERAGED (CONVERGENCE IN ITERATION)

	(58) ITER.	(59) TEMPERATURE (DEG. C)	(59) INNER PRESSURE (KG/CM2) (PSI)
1	515.618	960.112	51.685 734.958
2	454.518	904.133	50.487 717.926
3	484.427	903.969	50.505 718.181
4	4-4.390	903.902	50.503 718.158

(60) CONVERGENCE RELATIVE ERROR (FRACTION) 0.00008 (CONVERGENCE CRITERION 0.005)

STEP	2	SAMPLE PROBLEM (TYPICAL PWR PIN)	(55)	(56)	(57)	PAGE 4/ 13
(10)	AXIAL SECTION NO.	DENSIFICATION (MM)	RELOCATE (MM)	STRUCTURING (MM)	CENTRAL VOID (MM)	RADIUS FOR NEXT STEP (MM)
				RADIUS (MM)	TEMP. (DEG C)	CENTRAL VOID SURFACE
1	0.0	0.005672	0.0	1731.54	0.0	0.0
2	0.0	0.006973	0.0	1731.54	0.0	0.0
3	0.0	0.007934	0.0	1731.54	0.0	0.0
4	0.0	0.008559	0.0	1731.54	0.0	0.0
5	0.0	0.008589	0.0	1731.54	0.0	0.0
6	0.0	0.008589	0.0	1731.54	0.0	0.0
7	0.0	0.008589	0.0	1731.54	0.0	0.0
8	0.0	0.007934	0.0	1731.54	0.0	0.0
9	0.0	0.006973	0.0	1731.54	0.0	0.0
10	0.0	0.005672	0.0	1731.54	0.0	0.0
(60)	PELLET ELONGATION LENGTH (CM)	DISH COLD - SHOULDER CENTER	DISH COLD - DISH CENTER	SHOULDER TEMP. (C)	PELLET DENSIFICATION DENSIFICATION LENGTH(CM)	AXIAL DENSIFICATION DENSIFY + EXPANSION
(61)	COLD SHOULDER	CENTER	DISH	CENTER		
1	36.5760	36.6852	36.6861	0.1092	0.1101	397.40 0.0
2	36.5760	36.7198	36.7218	0.1438	0.1458	498.01 0.0
3	36.5760	36.7505	36.7535	0.1745	0.1775	502.45 0.0
4	36.5760	36.7732	36.7771	0.1972	0.2011	642.53 0.0
5	36.5760	36.7859	36.7904	0.2099	0.2144	675.33 0.0
6	36.5760	36.7881	36.7926	0.2121	0.2166	680.89 0.0
7	36.5760	36.7793	36.7833	0.2033	0.2073	658.36 0.0
8	36.5760	36.7598	36.7630	0.1838	0.1870	607.43 0.0
9	36.5760	36.7311	36.7332	0.1551	0.1572	529.71 0.0
10	36.5760	36.6971	36.6981	0.1211	0.1221	432.76 0.0
(TOTAL)	365.7600	367.4701	367.4991	1.7101	1.7391	0.0 1.71009

STEP 2 SAMPLE PROBLEM (TYPICAL PWR PIN)

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GAS RELEASE MECHANISM INFORMATION

(ID) AXIAL SECTION NUMBER	(63) GENERATED F.P. GAS (ATOMS PER UNIT LENGTH)		(70) GAS RELEASE RATE UNTIL NOW THIS TIME		(71) RELEASED GAS (ATOMS PER UNIT LENGTH)		(72) KRYPTON XENON	
	KRYPTON	XENON	MAX. VALUE	STEP	MAX. VALUE	IN THIS STEP	MAX. VALUE	IN THIS STEP
1	0.43781E+16	0.24883E+17	0.000231	0.000295	0.0	0.12916E+13	0.0	0.73407E+13
2	0.80943E+16	0.47052E+17	0.000233	0.000350	0.0	0.28347E+13	0.0	0.16478E+14
3	0.11047E+17	0.64885E+17	0.000236	0.000395	0.0	0.43595E+13	0.0	0.25606E+14
4	0.13032E+17	0.76926E+17	0.000240	0.000426	0.0	0.55459E+13	0.0	0.32736E+14
5	0.14000E+17	0.82801E+17	0.000244	0.000443	0.0	0.61982E+13	0.0	0.36659E+14
6	0.14000E+17	0.82801E+17	0.000248	0.000447	0.0	0.62539E+13	0.0	0.36988E+14
7	0.14032E+17	0.76926E+17	0.000252	0.000437	0.0	0.56947E+13	0.0	0.33613E+14
8	0.11047E+17	0.64885E+17	0.000255	0.000413	0.0	0.45616E+13	0.0	0.26793E+14
9	0.80943E+16	0.47052E+17	0.000257	0.000374	0.0	0.30272E+13	0.0	0.17597E+14
10	0.43781E+16	0.24883E+17	0.000259	0.000322	0.0	0.14115E+13	0.0	0.80222E+13
(73) AXIAL SUM,	0.10110E+18	0.59309E+18	0.002455	0.003901	0.0	0.41179E+14	0.0	0.24183E+15
AXIAL AVG.	0.10110E+17	0.59309E+17	0.000245	0.000390	0.0	0.41179E+13	0.0	0.24183E+14
(74) TOTAL MOLES IN FUEL	0.61397E-05	0.36017E-04				0.25007E-08		0.14686E-07
(75) RELEASE RATE (HY VOLUME AVERAGE TEMP.)	0.00039							
(76) RECALCULATED RELEASE RATE KR + XE	0.00041	0.00041						

(77) AXIAL PELLET LENGTH CHANGE	(78) PELLET STUCK LENGTH CHANGE (CM)	(79) PELLET VOLUME CHANGE BY ELONG -ATION (CM ³)	(79) CHANGED PLENUM VOLUME (CM ³)	(80) PLENUM PRESSURE INDUCED PELLET LENGTH CHANGE
DUE TO THERMAL EXPANSION	1.7100925	1.2081621	5.9693722	55.56790
DUE TO AXIAL DENSIFICATION	0.0	0.0	7.1775342	50.50336
DUE TO EXPANSION + DENSIFY	1.7100925	1.2081621	5.9693722	55.56790

STEP 2 SAMPLE PROBLEM (TYPICAL PWR PIN)

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(81) DETAIL TEMPERATURE DISTRIBUTION

AXIAL SECTION	NODE 1		NODE 2		NODE 3		NODE 4		NODE 5		NODE 6		NODE 7	
	RADI(CM)	TEMP(C)	RADI(CM)	TEMP(C)	RADI(CM)	TEMP(C)								
COOLANT	266.6	289.4	293.4	298.0	303.0	308.0	320.5	0.5363	324.3	CLAD OD	0.5362	290.4	0.5362	0.5363
CLAD OD	0.5362	290.4	0.5362	296.6	0.5363	303.2	0.5363	309.6	0.5363	CLAD ID	0.4745	295.6	0.4745	0.4745
CLAD ID	0.4745	295.6	0.4745	306.2	0.4745	316.1	0.4746	324.8	0.4746	GAP AVG. TEMP.	314.6	337.9	356.2	374.1
GAP AVG. TEMP.	314.6	337.9	356.2	369.3	369.3	378.1	382.7	389.3	389.3	PELLET SURFACE	0.4678	333.5	0.4683	369.6
PELLET SURFACE	0.4678	333.5	0.4683	369.6	0.4687	396.2	0.4690	413.9	0.4691	RADIAL NODE 5	0.4211	345.7	0.4215	393.5
RADIAL NODE 5	0.4211	345.7	0.4215	393.5	0.4218	430.0	0.4221	454.8	0.4222	10	0.3743	356.8	0.3747	415.4
10	0.3743	356.8	0.3747	415.4	0.3750	463.5	0.3752	493.1	0.3753	15	0.3275	366.7	0.3278	435.3
15	0.3275	366.7	0.3278	435.3	0.3281	490.2	0.3283	528.3	0.3284	20	0.2807	375.4	0.2810	452.9
20	0.2807	375.4	0.2810	452.9	0.2812	515.9	0.2814	559.9	0.2815	25	0.2339	382.9	0.2342	468.1
25	0.2339	382.9	0.2342	468.1	0.2344	538.1	0.2345	587.4	0.2346	30	0.1871	389.0	0.1873	480.7
30	0.1871	389.0	0.1873	480.7	0.1875	556.7	0.1876	610.5	0.1877	35	0.1404	393.8	0.1405	490.6
35	0.1404	393.8	0.1405	490.6	0.1406	571.4	0.1407	628.8	0.1407	40	0.0936	397.3	0.0937	497.8
40	0.0936	397.3	0.0937	497.8	0.0937	582.1	0.0938	642.0	0.0938	45	0.0468	399.4	0.0468	502.1
45	0.0468	399.4	0.0468	502.1	0.0469	585.5	0.0469	650.1	0.0469	PELLET CENTER	0.0	400.1	0.0	503.5
PELLET CENTER	0.0	400.1	0.0	503.5	0.0	590.6	0.0	652.8	0.0	686.6	613.6	615.8	0.0	635.5
AXIAL SECTION	NODE 8		NODE 9		NODE 10									
	RADI(CM)	TEMP(C)	RADI(CM)	TEMP(C)	RADI(CM)	TEMP(C)								
COOLANT	316.6	319.4	321.0											
CLAD OD	0.5363	326.5	0.5363	326.7	0.5363	324.9								
CLAD ID	0.4745	339.2	0.4746	336.1	0.4746	330.0								
GAP AVG. TEMP.	317.9	366.5	348.0											
PELLET SURFACE	0.4688	416.6	0.4688	396.9	0.4680	366.1								
RADIAL NODE 5	0.4219	451.3	0.4216	421.6	0.4212	378.8								
10	0.3751	483.5	0.3748	444.3	0.3744	390.4								
15	0.3282	513.0	0.3279	464.9	0.3276	400.8								
20	0.2813	539.2	0.2811	483.1	0.2808	409.9								
25	0.2344	562.0	0.2342	498.7	0.2340	417.6								
30	0.1875	581.1	0.1874	511.8	0.1872	424.0								
35	0.1406	596.1	0.1405	522.1	0.1404	429.0								
40	0.0938	607.0	0.0937	529.4	0.0936	432.6								
45	0.0468	613.6	0.0468	533.9	0.0468	434.8								
PELLET CENTER	0.0	615.8	0.0	535.4	0.0	435.5								

CASE 2 AXIAL SEGMENT 1 OF 10

76-09-09 9 HR 56 MINUTE 29 SEC 71

***** (B2) SAMPLE PROBLEM (TYPICAL PWR PIN) *****

400, 0, 0 0-----PELLET CENTER-----1000-----2000-----3000
 400, 0, 09 *
 400, 0, 19 *
 400, 0, 28 *
 400, 0, 37 *
 399, 0, 47 *
 399, 0, 56 *
 399, 0, 65 *
 398, 0, 75 *
 398, 0, 84 *
 397, 0, 94 *
 397, 1, 03 *
 396, 1, 12 *
 395, 1, 22 *
 395, 1, 31 *
 394, 1, 40 *
 393, 1, 50 *
 392, 1, 59 *
 391, 1, 68 *
 390, 1, 78 *
 389, 1, 87 *
 388, 1, 96 *
 387, 2, 06 *
 385, 2, 15 *
 384, 2, 25 *
 383, 2, 34 *
 381, 2, 43 *
 380, 2, 53 *
 379, 2, 62 *
 377, 2, 71 *
 375, 2, 81 *
 374, 2, 90 *
 372, 2, 99 *
 370, 3, 09 *
 369, 3, 18 *
 367, 3, 27 *
 365, 3, 37 *
 363, 3, 46 *
 361, 3, 56 *
 359, 3, 65 *
 357, 3, 74 *
 355, 3, 84 *
 353, 3, 93 *
 350, 4, 02 *
 348, 4, 12 *
 346, 4, 21 *
 343, 4, 30 *
 341, 4, 40 *
 339, 4, 49 *
 336, 4, 58 *
 333, 4, 68 ----- THERE IS A GAP, GAP CONDUCTANCE IS 633.8 BTU/HR/FT2/DEG F

296, |----- CLAD INNER SURFACE
 290, |----- CLAD OUTER SURFACE
 287, | C COOLANT
 | C

CASE 2 AXIAL SEGMENT 5 OF 10

76-09-09 9 HR 56 MINUTE 30 SEC 690

***** (B2) SAMPLE PROBLEM (TYPICAL PWR PIN) *****

687, 0, 0 0-----PELLET CENTER-----1000-----2000-----3000
 687, 0, 09 *
 686, 0, 19 *
 686, 0, 28 *
 685, 0, 38 *
 684, 0, 47 *
 682, 0, 56 *
 681, 0, 66 *
 679, 0, 75 *
 677, 0, 84 *
 675, 0, 94 *
 672, 1, 03 *
 670, 1, 13 *
 667, 1, 22 *
 664, 1, 31 *
 660, 1, 41 *
 657, 1, 50 *
 653, 1, 60 *
 649, 1, 69 *
 644, 1, 78 *
 640, 1, 88 *
 639, 1, 97 *
 630, 2, 06 *
 625, 2, 16 *
 620, 2, 25 *
 614, 2, 35 *
 609, 2, 44 *
 603, 2, 53 *
 597, 2, 63 *
 591, 2, 72 *
 584, 2, 81 *
 578, 2, 91 *
 571, 3, 00 *
 564, 3, 10 *
 557, 3, 19 *
 549, 3, 28 *
 542, 3, 38 *
 534, 3, 47 *
 527, 3, 57 *
 519, 3, 66 *
 511, 3, 75 *
 503, 3, 85 *
 494, 3, 94 *
 486, 4, 03 *
 478, 4, 13 *
 469, 4, 22 *
 460, 4, 32 *
 451, 4, 41 *
 443, 4, 50 *
 433, 4, 60 *
 424, 4, 69 ----- THERE IS A GAP, GAP CONDUCTANCE IS 827.7 BTU/HR/FT2/DEG F

332, |----- CLAD INNER SURFACE
 316, |----- CLAD OUTER SURFACE
 303, | C COOLANT
 | C

CASE 2 AXIAL SEGMENT 10 OF 10

76-09-09 9 HR 56 MINUTE 33 SEC 41

***** (62) SAMPLE PROBLEM (TYPICAL PWR PIN)

	0-----PELLET CENTER-----	1000-----	2000-----	3000-----
436, 0, 0	*	*	*	*
436, 0, 09	*	*	*	*
435, 0, 19	*	*	*	*
435, 0, 28	*	*	*	*
435, 0, 37	*	*	*	*
435, 0, 47	*	*	*	*
434, 0, 56	*	*	*	*
434, 0, 65	*	*	*	*
434, 0, 75	*	*	*	*
433, 0, 84	*	*	*	*
433, 0, 94	*	*	*	*
432, 1, 03	*	*	*	*
431, 1, 12	*	*	*	*
431, 1, 22	*	*	*	*
430, 1, 31	*	*	*	*
429, 1, 40	*	*	*	*
428, 1, 50	*	*	*	*
427, 1, 59	*	*	*	*
426, 1, 68	*	*	*	*
425, 1, 78	*	*	*	*
424, 1, 87	*	*	*	*
423, 1, 97	*	*	*	*
422, 2, 06	*	*	*	*
420, 2, 15	*	*	*	*
419, 2, 25	*	*	*	*
418, 2, 34	*	*	*	*
416, 2, 43	*	*	*	*
415, 2, 53	*	*	*	*
413, 2, 62	*	*	*	*
412, 2, 71	*	*	*	*
410, 2, 81	*	*	*	*
408, 2, 90	*	*	*	*
406, 3, 00	*	*	*	*
405, 3, 09	*	*	*	*
403, 3, 18	*	*	*	*
401, 3, 28	*	*	*	*
399, 3, 37	*	*	*	*
397, 3, 46	*	*	*	*
395, 3, 56	*	*	*	*
393, 3, 65	*	*	*	*
390, 3, 74	*	*	*	*
388, 3, 84	*	*	*	*
386, 3, 93	*	*	*	*
384, 4, 02	*	*	*	*
381, 4, 12	*	*	*	*
379, 4, 21	*	*	*	*
376, 4, 31	*	*	*	*
374, 4, 40	*	*	*	*
371, 4, 49	*	*	*	*
369, 4, 59	*	*	*	*
366, 4, 68	*	*	*	*

THERE IS A GAP, GAP CONDUCTANCE IS 665.5 BTU/HR/FT²/DEG F

330,	I-----+-----	CLAD INNER SURFACE
325,	I-----+-----	CLAD OUTER SURFACE
321,	C	COOLANT
	C	

STEP 2 SAMPLE PROBLEM (TYPICAL PWR PIN)

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(63) RADIOP-ACTIVITY OF ISOTOPE

AXIAL NODE	83 KR	84 KR	85M KR	85 KR	86 KR	131M TE	131 TE	131 I	131 XE	132 TE
DECAY CONST (1/SEC)	0.0	0.0	4.3750E-05	2.0420E-09	0.0	6.6840E-06	4.6200E-04	9.9640E-07	0.0	2.4680E-06
NO. OF ATOMS										
1	2.0698E+16	3.8613E+16	1.3377E+16	1.0618E+16	7.6825E+16	1.3305E+16	2.5476E+15	1.0348E+17	8.9080E+15	1.5522E+17
2	3.8266E+16	7.1392E+16	2.4733E+16	1.9631E+16	1.4204E+17	2.4599E+16	4.7102E+15	1.9131E+17	1.6469E+16	2.8698E+17
3	5.2224E+16	9.7437E+16	3.3754E+16	2.6792E+16	1.9385E+17	3.3572E+16	6.4263E+15	2.6110E+17	2.2477E+16	3.9166E+17
4	6.1609E+16	1.1495E+17	3.9821E+16	3.1607E+16	2.2869E+17	3.9606E+16	7.5837E+15	3.0802E+17	2.6516E+16	4.6206E+17
5	6.6181E+16	1.2348E+17	4.2776E+16	3.3953E+16	2.4566E+17	4.2545E+16	8.1465E+15	3.3088E+17	2.8484E+16	4.9635E+17
6	6.6181E+16	1.2348E+17	4.2776E+16	3.3953E+16	2.4566E+17	4.2545E+16	8.1465E+15	3.3088E+17	2.8484E+16	4.9635E+17
7	6.1609E+16	1.1495E+17	3.9821E+16	3.1607E+16	2.2869E+17	3.9606E+16	7.5837E+15	3.0802E+17	2.6516E+16	4.6206E+17
8	5.2224E+16	9.7437E+16	3.3754E+16	2.6792E+16	1.9385E+17	3.3572E+16	6.4263E+15	2.6110E+17	2.2477E+16	3.9166E+17
9	3.8266E+16	7.1392E+16	2.4733E+16	1.9631E+16	1.4204E+17	2.4599E+16	4.7102E+15	1.9131E+17	1.6469E+16	2.8698E+17
10	2.0698E+16	3.8613E+16	1.3377E+16	1.0618E+16	7.6825E+16	1.3305E+16	2.5476E+15	1.0348E+17	8.9080E+15	1.5522E+17
SUB-TOTAL	4.7796E+17	8.9175E+17	3.0892E+17	2.4520E+17	1.7741E+18	3.0725E+17	5.8833E+16	2.3896E+18	2.0571E+17	3.5845E+18
CURIE										
1	0.0	0.0	1.5816E+01	5.8600E-04	0.0	2.4035E+00	3.1811E+01	2.7866E+00	0.0	1.0354E+01
2	0.0	0.0	2.9245E+01	1.0834E+03	0.0	4.4437E+00	5.8813E+01	5.1519E+00	0.0	1.9142E+01
3	0.0	0.0	3.9912E+01	1.4786E+03	0.0	6.0647E+00	8.0267E+01	7.0313E+00	0.0	2.6125E+01
4	0.0	0.0	4.7086E+02	1.7444E+03	0.0	7.1547E+00	9.4693E+02	8.2949E+00	0.0	3.0820E+01
5	0.0	0.0	5.0580E+01	1.8738E+03	0.0	7.6857E+00	1.0172E+02	4.9106E+00	0.0	3.3108E+01
6	0.0	0.0	5.0580E+01	1.8738E+03	0.0	7.6857E+00	1.0172E+02	8.9106E+00	0.0	3.3108E+01
7	0.0	0.0	4.7086E+01	1.7444E+03	0.0	7.1547E+00	9.4693E+01	8.2949E+00	0.0	3.0820E+01
8	0.0	0.0	3.9912E+01	1.4786E+03	0.0	6.0647E+00	8.0267E+01	7.0313E+00	0.0	2.6125E+01
9	0.0	0.0	2.9245E+01	1.0834E+03	0.0	4.4437E+00	5.8813E+01	5.1519E+00	0.0	1.9142E+01
10	0.0	0.0	1.5816E+01	5.8600E-04	0.0	2.4035E+00	3.1811E+01	2.7866E+00	0.0	1.0354E+01
SUB-TOTAL	0.0	0.0	3.6528E+02	1.3532E-02	0.0	5.5505E+01	7.3461E+02	6.4351E+01	0.0	2.3910E+02

STEP 2		SAMPLE	PROBLEM	(TYPICAL PWR PIN)				PAGE 8 / 17		
(84)	AXIAL NODE	132 I	132 XE	133 I	133 XE	134 XE	135 I	135 XE	136 XE	NODE SUB-TOTAL
DECAY CONST (1/SEC)	8.3700E-05	0.0	9.1670E-06	1.5220E-06	0.0	2.8730E-05	7.2190E-04	2.0920E-05	0.0	
NO. OF ATOMS										
1	4.5736E+15	3.3075E+16	1.8394E+17	1.3651E+17	3.1527E+17	9.0675E+16	1.0826E+15	7.4225E+16	3.4104E+17	1.6240E+18
2	8.4558E+15	6.1151E+16	3.4008E+17	2.5237E+17	5.8290E+17	1.6764E+17	2.0016E+15	1.0702E+17	6.9905E+17	3.0408E+18
3	1.1540E+16	8.3458E+16	4.6413E+17	3.4443E+17	7.9559E+17	2.2880E+17	2.7317E+15	1.2351E+17	1.0011E+18	4.1745E+18
4	1.3614E+16	9.8458E+16	2.4754E+17	4.0632E+17	9.3855E+17	2.6592E+17	3.2226E+15	1.3177E+17	1.2088E+18	4.9387E+18
5	1.4625E+16	1.0577E+17	5.8818E+17	4.3647E+17	1.0082E+18	2.8995E+17	3.4618E+15	1.3520E+17	1.3109E+18	5.3113E+18
6	1.4625E+16	1.0577E+17	5.8818E+17	4.3647E+17	1.0082E+18	2.8995E+17	3.4618E+15	1.3520E+17	1.3109E+18	5.3113E+18
7	1.3614E+16	9.8458E+16	2.4754E+17	4.0632E+17	9.3855E+17	2.6592E+17	3.2226E+15	1.3177E+17	1.2088E+18	4.9387E+18
8	1.1540E+16	8.3458E+16	4.6413E+17	3.4443E+17	7.9559E+17	2.2880E+17	2.7317E+15	1.2351E+17	1.0011E+18	4.1745E+18
9	8.4558E+15	6.1151E+16	3.4008E+17	2.5237E+17	5.8290E+17	1.6764E+17	2.0016E+15	1.0702E+17	6.9905E+17	3.0408E+18
10	4.5736E+15	3.3075E+16	1.8394E+17	1.3651E+17	3.1527E+17	9.0675E+16	1.0826E+15	7.4225E+16	3.4104E+17	1.6240E+18
SUB-TOTAL	1.0562E+17	7.6381E+17	4.2477E+18	3.1522E+18	7.2810E+18	2.0940E+18	2.5001E+16	1.1434E+18	9.1218E+18	3.8178E+19
CURIE										
1	1.0346E+01	0.0	4.5573E+01	5.6153E+00	0.0	7.0408E+01	2.1122E+01	4.1967E+01	0.0	2.5820E+02
2	1.9128E+01	0.0	8.4256E+01	1.0381E+01	0.0	1.3017E+02	3.9029E+01	6.0507E+01	0.0	4.6030E+02
3	2.6108E+01	0.0	1.1499E+02	1.4168E+01	0.0	1.7766E+02	5.3297E+01	6.9833E+01	0.0	6.1546E+02
4	3.0798E+01	0.0	1.3566E+02	1.6714E+01	0.0	2.0959E+02	6.2876E+01	7.4503E+01	0.0	7.1819E+02
5	3.3084E+01	0.0	1.4573E+02	1.7954E+01	0.0	2.2514E+02	6.7554E+01	7.6443E+01	0.0	7.6790E+02
6	3.3084E+01	0.0	1.4573E+02	1.7954E+01	0.0	2.2514E+02	6.7554E+01	7.6443E+01	0.0	7.6790E+02
7	3.0798E+01	0.0	1.3566E+02	1.6714E+01	0.0	2.0959E+02	6.2876E+01	7.4503E+01	0.0	7.1819E+02
8	2.6108E+01	0.0	1.1499E+02	1.4168E+01	0.0	1.7766E+02	5.3297E+01	6.9833E+01	0.0	6.1546E+02
9	1.9128E+01	0.0	8.4256E+01	1.0381E+01	0.0	1.3017E+02	3.9052E+01	6.0507E+01	0.0	4.6030E+02
10	1.0346E+01	0.0	4.5573E+01	5.6153E+00	0.0	7.0408E+01	2.1122E+01	4.1967E+01	0.0	2.5820E+02
SUB-TOTAL	2.3893E+02	0.0	1.0524E+03	1.2967E+02	0.0	1.6259E+03	4.8778E+02	6.4651E+02	0.0	5.6401E+03

***** INVENTORY FP GAS SUMMARY

STEP 2		SAMPLE	PROBLEM	(TYPICAL PWR PIN)				PAGE 10 / 19		
(84)	AXIAL NODE	132 I	132 XE	133 I	133 XE	134 XE	135 I	135 XE	136 XE	NODE SUB-TOTAL
DECAY CONST (1/SEC)	8.3700E-05	0.0	9.1670E-06	1.5220E-06	0.0	2.8730E-05	7.2190E-04	2.0920E-05	0.0	
NO. OF ATOMS										
1	1.3493E+12	9.7575E+12	5.4264E+13	4.0271E+13	9.3009E+13	2.6750E+13	3.1938E+11	2.1897E+13	1.0061E+14	4.7909E+14
2	2.9613E+12	2.1915E+13	1.1910E+14	2.0414E+14	5.8710E+13	7.0096E+11	3.7478E+13	2.4981E+14	1.0649E+15	
3	4.5542E+12	3.2935E+13	1.8316E+14	1.3592E+14	9.0291E+13	1.0780E+12	4.8741E+13	3.9507E+14	1.6474E+15	
4	5.7936E+12	4.1898E+13	2.3301E+14	1.7291E+14	3.9940E+14	1.1486E+14	1.3714E+12	5.6074E+13	5.1440E+14	2.1016E+15
5	6.4750E+12	4.6827E+13	2.6041E+14	1.9324E+14	4.4638E+14	1.2837E+14	1.5327E+12	5.9859E+13	5.8040E+14	2.3515E+15
6	6.5331E+12	4.7247E+13	2.6275E+14	1.9498E+14	4.5038E+14	1.2952E+14	1.5464E+12	6.0396E+13	5.8561E+14	2.3726E+15
7	5.9489E+12	4.3022E+13	2.3925E+14	1.7759E+14	4.1011E+14	1.1794E+14	1.4040E+12	5.7578E+13	5.2820E+14	2.1580E+15
8	4.7653E+12	3.4462E+13	1.9165E+14	1.4222E+14	3.2851E+14	9.4477E+13	1.1280E+12	5.1001E+13	4.1338E+14	1.7238E+15
9	3.1624E+12	2.2870E+13	1.2718E+14	9.4385E+13	2.1800E+14	6.2697E+13	7.4856E+11	4.0023E+13	2.6144E+14	1.1372E+15
10	1.4745E+12	1.0663E+13	5.9303E+13	4.4010E+13	1.0164E+14	2.9234E+13	3.4903E+11	2.3930E+13	1.0995E+14	5.2357E+14
SUB-TOTAL	4.3010E+13	3.1110E+14	1.7301E+15	1.2839E+15	2.9655E+15	8.5286E+14	1.0183E+13	4.5698E+14	3.7339E+15	1.5560E+16
CURIE										
1	3.0522E-03	0.0	1.3444E+02	1.6566E+03	0.0	2.0771E+02	6.2313E+03	1.2381E+02	0.0	7.6173E+02
2	6.6989E-03	0.0	2.9507E+02	3.6335E+03	0.0	4.5587E+02	1.3676E+02	2.1190E+02	0.0	1.6120E-01
3	1.0302E-02	0.0	4.5379E+02	5.5912E+03	0.0	7.0110E+02	2.1033E+02	2.7558E+02	0.0	2.4288E-01
4	1.3106E-02	0.0	5.7729E+02	7.1126E+03	0.0	8.9189E+02	2.6757E+02	3.1705E+02	0.0	3.0562E+01
5	1.4648E-02	0.0	6.4519E+02	7.9491E+03	0.0	9.9679E+02	2.9904E+02	3.3844E+02	0.0	3.3998E+01
6	1.4779E-02	0.0	6.5098E+02	8.0204E+03	0.0	1.0057E+01	3.0172E+02	3.4144E+02	0.0	3.4303E+01
7	1.3457E-02	0.0	5.9277E+02	7.3038E+03	0.0	9.1581E+02	2.7474E+02	3.2555E+02	0.0	3.1382E+01
8	1.0780E-02	0.0	4.7483E+02	5.8504E+03	0.0	7.3360E+02	2.2008E+02	2.8836E+02	0.0	2.5414E+01
9	7.1538E-03	0.0	3.1511E+02	3.8825E+03	0.0	4.8683E+02	1.4605E+02	2.2629E+02	0.0	1.7215E+01
10	3.3356E-03	0.0	1.4693E+02	1.8104E+03	0.0	2.2700E+02	6.8099E+03	1.3530E+02	0.0	8.3245E+02
SUB-TOTAL	9.7313E-02	0.0	4.2864E+01	5.2812E+02	0.0	6.6223E+01	1.9867E+01	2.5838E+01	0.0	2.2922E+00

***** RELEASED FP GAS SUMMARY

STEP 2

SAMPLE PROBLEM (TYPICAL PWR PIN)

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(84) RADIO-ACTIVITY OF ISOTOPE

..... RELEASED FP GAS

AXIAL NODE	B3 KR	B4 KR	B5 KR	B6 KR	131M TE	131 TE	131 I	131 XE	132 TE
DECAY CONST (1/SEC)	0.0	0.0	4.3750E-05	2.0420E-09	0.0	6.6840E-06	4.6200E-04	9.9640E-07	0.0
NO. OF ATOMS									
1	6.1062E+12	1.1391E+13	3.9465E+12	3.1324E+12	2.2664E+13	3.9251E+12	7.5158E+11	3.0527E+13	2.6280E+12
2	1.3401E+13	2.5002E+13	8.6615E+12	6.8748E+12	4.9742E+13	8.6146E+12	1.6495E+12	6.6798E+13	5.7676E+12
3	2.0609E+13	3.8452E+13	1.3321E+13	1.0573E+13	7.6500E+13	1.3249E+13	2.5368E+12	1.0304E+14	8.8700E+12
4	2.6217E+13	4.8917E+13	1.6946E+13	1.3450E+13	9.7318E+13	1.6804E+13	3.2272E+12	1.3108E+14	1.1284E+13
5	2.9301E+13	5.4671E+13	1.8939E+13	1.5032E+13	1.0876E+14	1.8836E+13	3.6068E+12	1.4849E+14	1.2611E+13
6	2.9564E+13	5.5162E+13	1.9109E+13	1.5167E+13	1.0974E+14	1.9005E+13	3.6392E+12	1.4781E+14	1.2724E+13
7	2.6920E+13	5.0229E+13	1.7400E+13	1.3811E+13	9.9928E+13	1.7306E+13	3.3137E+12	1.3459E+14	1.1586E+13
8	2.1565E+13	4.0234E+13	1.3938E+13	1.1063E+13	8.0046E+13	1.3863E+13	2.6544E+12	1.0781E+14	9.2812E+12
9	1.4311E+13	2.6700E+13	9.2497E+12	7.3417E+12	5.3120E+13	9.1996E+12	1.7615E+12	7.1548E+13	6.1593E+12
10	6.6731E+12	1.2449E+13	4.3129E+12	3.4232E+12	2.4768E+13	4.2895E+12	8.2136E+11	3.3361E+13	2.8719E+12
SUR-TOTAL	1.9467E+14	3.6321E+14	1.2582E+14	9.9869E+13	7.2259E+14	1.2514E+14	2.3962E+13	9.7326E+14	8.3783E+13
CURIE									
1	0.0	0.0	4.6664E-03	1.7288E-07	0.0	7.0907E-04	9.3846E-03	8.2207E-04	0.0
2	0.0	0.0	1.0242E-02	3.7942E-07	0.0	1.5562E-03	2.0597E-02	1.8042E-03	0.0
3	0.0	0.0	1.5751E-02	5.8351E-07	0.0	2.3933E-03	3.1676E-02	2.7748E-03	0.0
4	0.0	0.0	2.0037E-02	7.4231E-07	0.0	3.0447E-03	4.0296E-02	3.5299E-03	0.0
5	0.0	0.0	2.2394E-02	8.2961E-07	0.0	3.4028E-03	4.5036E-02	3.9451E-03	0.0
6	0.0	0.0	2.2595E-02	8.3706E-07	0.0	3.4333E-03	4.5440E-02	3.9805E-03	0.0
7	0.0	0.0	2.0574E-02	7.6221E-07	0.0	3.1263E-03	4.1377E-02	3.6245E-03	0.0
8	0.0	0.0	1.6481E-02	6.1056E-07	0.0	2.5043E-03	3.3145E-02	2.9034E-03	0.0
9	0.0	0.0	1.0937E-02	4.0518E-07	0.0	1.6619E-03	2.1996E-02	1.9268E-03	0.0
10	0.0	0.0	5.0997E-03	1.8893E-07	0.0	7.7490E-04	1.0256E-02	8.9840E-04	0.0
SUB-TOTAL	0.0	0.0	1.4878E-01	5.5117E-06	0.0	2.2607E-02	2.9920E-01	2.6210E-02	0.0

(3)	LINEAR HEAT RATING(AVERAGE)	5,674 (KW/FT)	186,164 (WATT/CM)
(4)	BURNUP (PIN AVERAGE)	30,448 (MWD/MTU)	0.1026E+19 (FISSIONS/CC)
(5)	TIME IN REACTOR	2,000 (DAYS)	48,000 (HOURS)
(6)	COOLANT INLET TEMPERATURE	545,000 (DEG F)	285,000 (DEG C)
(7)	COOLANT OUTLET TEMPERATURE	609,800 (DEG F)	321,000 (DEG C)
(8)	COOLANT PRESSURE	2250,000 (PSI)	158,228 (KG/CM2)

(9) CUMULATED CP TIME 14,6920(SEC) COMPUTED TIME AT THIS STEP 3.8480(SEC)

(10)	(11)	(12)	(13)	(14)	(15)	(16)	(17)	(18)
AXIAL SECTION NUMBER	AXIAL DISTANCE (CM) (INCH)	LINEAR HEAT RATING (W/CM) (KW/FT)	BURNUP (MWD/MTU)	AVERAGE NEUTRON FLUX (NV)	COOLANT TEMP. (DEG C)	FILM COEFFICIENT BTU WATT/CM2-C /HR-FT2-F	CLAD TEMPERATURE OD (DEG C)	ID (DEG C)
1	18.79	7.20	80,6149	2,4571	13.19	9.693E+12	286.56	3,102
2	54.86	21.60	149,0439	4,5429	24.38	1.793E+13	289.44	3,088
3	91.44	36.00	203,4121	6,2000	33.27	2.447E+13	293.37	3,071
4	128.02	50.40	239,9700	7,3143	39.25	2.887E+13	298.02	3,056
5	164.59	64.80	257,7803	7,8571	42.16	3.101E+13	303.00	3,048
6	201.17	79.20	257,7803	7,8571	42.16	3.101E+13	307.98	3,043
7	237.74	93.60	239,9700	7,3143	39.25	2.887E+13	312.63	3,047
8	274.32	108.00	203,4121	6,2000	33.27	2.447E+13	316.56	3,050
9	310.90	122.40	149,0439	4,5429	24.38	1.793E+13	319.44	3,050
10	347.47	136.80	80,6149	2,4571	13.19	9.693E+12	321.00	3,047

(25)	AXIAL SECTION NUMBER	GAP CONDUCTANCE(BTU/HR-FT2-F)	SOLID -SOLID CONDUCT	GAS- RADIENT	TOTAL	THERMAL EXPANSION	INCREASE IN FUEL SWELLING	RADIAL FUSION DENSI- TY	RADIAL RE- FICATION	LOCATION	TOTAL	THERMAL EXPAN.	INCREASE IN CLAD RADIUS(MM)	RADIAL HOT GAP (MM)	(29)	(30)	(31)
1	0.0	709.75	6.73	716.49	0.016989	0.0	0.0	0.008103	0.025092	0.00813	0.0	-0.00511	0.00303	0.06049			
2	0.0	824.96	8.09	833.05	0.024663	0.0	-0.003564	0.010863	0.031963	0.00854	0.0	-0.00511	0.00344	0.05402			
3	0.0	905.19	9.25	914.43	0.032000	0.0	-0.009163	0.012915	0.035751	0.00892	0.0	-0.00511	0.00381	0.05061			
4	0.0	987.34	10.01	997.35	0.037392	0.0	-0.012139	0.014251	0.039503	0.00923	0.0	-0.00511	0.00412	0.04717			
5	0.0	1040.70	10.46	1051.16	0.040278	0.0	-0.013428	0.014692	0.041741	0.00946	0.0	-0.00511	0.00435	0.04516			
6	0.0	1048.30	10.65	1058.95	0.040576	0.0	-0.013428	0.014692	0.042039	0.00960	0.0	-0.00511	0.00450	0.04501			
7	0.0	1007.72	10.56	1018.28	0.038235	0.0	-0.012139	0.014251	0.040347	0.00966	0.0	-0.00511	0.00455	0.04675			
8	0.0	933.76	10.10	943.86	0.033281	0.0	-0.009163	0.012915	0.037032	0.00960	0.0	-0.00511	0.00449	0.05001			
9	0.0	837.24	9.15	866.43	0.026193	0.0	-0.003564	0.010863	0.033493	0.00943	0.0	-0.00511	0.00432	0.05338			
10	0.0	740.19	7.87	748.06	0.018553	0.0	0.0	0.008103	0.026656	0.00916	0.0	-0.00511	0.00405	0.05994			

(10)	(11)	(12)	(13)	(14)	(15)	(16)	(17)	(18)	(19)	(20)	(21)	(22)	(23)	(24)	(25)	(26)	(27)	(28)
AXIAL SECTION NUMBER	FUEL SURFACE TEMP. (DEG C)	FUEL CENTER TEMP. (DEG C)	VOL. FUEL TEMP. (DEG C)	Avg FUEL TEMP. (DEG C)	NOMINAL HEAT CAPACITY CAL/K-MOLE	CAL/K-MOLE	BTU/LB-F	BTU/LB	BTU/LB	BTU/LB	BTU/LB	BTU/LB	BTU/LB	BTU/LB	BTU/LB	BTU/LB	BTU/FOOT	CONTACT PRESSURE (KG/CM2)
1	371,852	518,047	442,897	19,401	5238,273	27,809	50,056	28,123	50,621	195,072	23,594	0.0						
2	429,333	740,896	577,237	19,859	5362,045	37,581	67,646	38,145	68,661	264,590	32,003	0.0						
3	471,178	942,072	690,982	20,174	5446,932	46,016	82,828	46,815	84,287	324,732	39,277	0.0						
4	494,467	1044,141	766,994	20,361	5497,550	51,722	93,099	52,736	94,924	365,199	44,244	0.0						
5	506,083	1157,510	805,884	20,452	5522,158	54,661	98,390	55,804	100,447	387,082	46,819	0.0						
6	509,793	1143,487	810,701	20,464	5525,157	55,026	99,047	56,183	101,130	389,713	47,137	0.0						
7	505,418	1101,358	780,990	20,394	5506,491	52,778	95,000	53,830	96,895	373,393	45,163	0.0						
8	489,408	969,196	713,499	20,231	5462,333	47,700	85,861	48,553	87,396	336,789	40,735	0.0						
9	454,528	774,996	606,722	19,946	5385,379	39,755	71,559	40,375	72,675	280,059	33,874	0.0						
10	402,984	554,897	476,816	19,529	5272,842	30,255	54,458	30,619	55,107	212,360	25,685	0.0						

COMPOSITION OF PIN GAS (MOLES) HELIUM ARGON HYDROGEN NITROGEN KRYPTON XENON
FRACTION 0.999784 0.0 0.0 0.000199 0.000002 0.000014

AXIAL VOLUME-TEMPERATURE AVERAGED (CONVERGENCE IN ITERATION)

(58)	(59)
ITER.	INNER PRESSURE
(DEG C) (DEG F)	(KG/CM2) (PSI)
1	57,706
2	55,157
3	55,204
4	55,199

(60) CONVERGENCE RELATIVE ERROR (FRACTION) 0.00019 (CONVERGENCE CRITERION 0.005)

Table B-1 計算結果出力の説明

- (1) 入力された運転履歴の時間ステップ数
- (2) タイトル(入力)
- (3) 線出力密度(燃料棒平均) 参照(12)(各軸方向セグメントの値)
- (4) 燃焼度(燃料棒平均) 参照(13)(各軸方向セグメントの値)
- (5) 積算照射時間
- (6) 冷却材入口温度
- (7) 冷却材出口温度
- (8) 冷却材圧力(均一)
- (9) 計算時間(CPUタイム)
- (10) 軸方向セグメント番号(制限20) 番号1は燃料棒最下部セグメントに対応
- (11) 等分割された燃料棒セグメント中心の底からの高さ
- (12) 軸方向線出力密度分布
- (13) 線出力密度及び照射時間より計算された燃焼度
- (14) 線出力密度より計算された熱中性子束
- (15) 冷却材温度分布。もし $KOOL > 0$ (すなわち被覆内面温度を冷却温度と等しくする) の場合は被覆内面温度と等しい温度がプリントされる。
- (16) 冷却材-被覆管熱伝達係数。もし $KOOL > 0$ の場合は0.0とプリントされる。
- (17) 被覆管外表面熱流束 $q''_{co} = p / (\pi \times (D_{co} + 2 \cdot \Delta r_{co}))$ p =線出力密度
- (18) 被覆管外表面温度
- (19) 被覆管内表面温度
- (20) 被覆管平均熱伝導率 被覆管内外表面の平均温度によって決められた熱伝導率
- (21) ギャップ平均温度 $T_{gap} = (T_{ci} + T_{fs}) / 2$
- (22) 燃料ペレット表面熱流束 $q''_{fs} = p / \pi \times (D_{fs} + 2 \cdot \Delta r_{fs})$
- (23) ギャップ・コンダクタンス収斂計算中の繰返し計算回数
燃料体積平均温度を繰返し計算で求めているため(58 参照、打切5回)
1セグメント当たり数回のギャップ・コンダクタンス収斂計算が行なわれる。
- (24) 収斂計算の繰返し回数の総計 今回のステップの合計(23を合計)及び最初からの積算
- (25) ギャップ・コンダクタンス 接触熱伝達、ガス熱伝導、輻射及び合計
もし、 $MREV1 > 0$ (すなわち RESAR-41 ギャップ・コンダクタンス評価式で計算)の場合、全ギャップ・コンダクタンスが与えられるため、接触熱伝導、輻射の項は0.0とプリントされる。
- (26) 体積平均温度(34)を用いて決められたガス放出率
- (27) Temperature Jump Distance
- (28) ペレット変位量 熱膨張、スウェーリング及びそれらと Relocation(61), Densification(62)を加算した全変位量($= \Delta r_{fuel}$)
- (29) 被覆管変位量 熱膨張、クリープひずみ内外圧力差による弾性変位およびそれらの合計($= \Delta r_{clad}$)
- (30) ホット・ギャップ $r_{gap}^h = r_{gap}^0 + \Delta r_{clad} - \Delta r_{fuel}$ r_{gap}^0 =初期ギャップ

(31) 被覆管ペレットの接触状態を示すサイン

もし $MREV1 \geq 0$ の場合、接触の条件 ($r_{gap}^h <$ 平均表面粗さ) が満されていればスター (*) がプリントされ、満されていなければブランク (空白) となる。

もし $MREV1 < 0$ の場合、接触状態により A, B, C, D, E の文字がプリントされる。それぞれの定義は別表 (Table B-2) に示す。

(32) 燃料ペレット外表面温度

(33) 燃料ペレット中心温度

(34) 燃料ペレット体積平均温度

(35) 燃料ペレット内領域境界半径 (中心孔半径、柱軸晶領域半径、等軸晶領域半径、外表面半径)、中心孔半径は中心孔がなければ 0.0、柱軸晶及び等軸晶領域は温度によって判定するため (1700°C 及び 1350°C)、温度が低ければ各領域は重なり同じ半径がプリントされる。

(36) 燃料ペレット外表面、被覆管外表面での円周方向歪 ($\Delta r/r_0$)

(37) ギャップ・ガスの熱伝導率

(38) 燃料ペレット一被覆管接触圧力 (被覆管 Yield Stress は越えない)

(39) 被覆管内面円周方向熱応力

(40) プレナム体積 (入力値)

(41) プレナム平均温度 (入力値)

(42) 冷却材飽和温度 ($SIGHF < 0$ 以外のときはプリントされない)

(43) 初期プレナム圧力 (入力値)

(44) 照射時プレナム圧力

(45) 燃料棒内 (プレナム、ギャップ、中心孔) に存在するガスの全モル数

(46) (45) のガス中プレナム内に存在するモル数

(47) (45) のガス中ギャップ及び中心孔内に存在するモル数

(48) 燃料棒 体積平均温度を用いて決められた F.P. ガス放出率 ((5)と同じ)

(49) 初期封入ガス中に含まれていた各ガス成分のモル数

(50) 燃料ペレット内で生成された各ガス成分のモル数

(51) 燃料ペレットより放出 (放出率は (70)) された各ガス成分のモル数

(52) プレナム、ギャップ内に初期から蓄積された各ガス成分のモル数 ((49)+(51))

(53) プレナム、ギャップ内に存在している各ガス成分のモル分率

(54) 定圧比熱

$$(55) \text{蓄積エネルギー } E(\text{cal/g - UO}_2) = \left\{ \sum_{i=1}^N m_i \int_{298}^{T_1} c_p(T) dT/m \right\} / 270 \text{ g/mol e UO}_2$$

$$(56) \text{体積平均温度での蓄積エネルギー } \bar{E}(\text{cal/g - UO}_2) = \int_{298}^{\bar{T}} c_p(T) dT / 270 \text{ g/mol e UO}_2$$

(57) 単位長当たりの蓄積エネルギー

(58) 燃料棒の体積平均温度収斂計算中の温度収斂状況

(59) 収斂計算中の内圧収斂状況

(60) 収斂時の相対誤差 (収斂判定条件は体積平均温度の各繰返し計算中の相対誤差が 0.005 以下)

- (61) Densificationによる変位量
- (62) Relocationによる変位量(もしこの変位を考慮することによって接触条件となるような場合、接觸しないという条件を満すまでこの変位量は減じられる)
- (63) 再組織化する温度及び半径(初期燃料密度と再組織化密度(各々入力値)が等しい場合は再組織化は起さないので各々0.0とプリントされる)
- (64) 再組織化によって生ずる中心孔の半径、高さ、及びその体積
但し、高さは常に1セグメント長と同じである。
- (65) 次のタイム・ステップを計算するための形状寸法
但し、中心孔半径は(64)の半径を室温(25°C)での半径に計算したものであり、ペレット表面半径、被覆管内外半径は現Versionでは初期入力値と同じである。中心孔がある場合、この内半径を用いて次のステップの計算が行なわれ、この内半径が小さくなることはない。
- (66) 燃料スタック長の変化 初期セグメント長、ディッシュ肩に相当する半径での温度を用いた軸方向熱膨張量、ペレット中心での温度を用いた軸方向熱膨張量、及び初期セグメント長との各々の差、ディッシュ半径が入力されていない場合は0.0、すなわち中心(中心孔のある場合は内半径)で計算される。
- (67) ディッシュ肩に相当する半径での温度、半径が入力されていない場合はペレット中心温度となる。
- (68) 軸方向Densification考慮による軸方向長さ変化量
Densificationによる“ちぢみ”量及びDensificationと熱膨張の双方を考慮したときのスタック長変化。Densification率は半径方向と同じ値を用いた。
- (69) 各軸方向セグメント内で生成された各分裂生成ガス(Kr, Xe)の単位長さ当たりの原子数
- (70) 各軸方向セグメント体積平均温度によって決定されたガス放出率
このステップ以前までの最大放出率、及びこのステップで計算された放出率がプリントされており、もしこのステップでの放出率が最大放出率より大きくなった場合は置換が行なわれ、次ステップで使われる。もしこのステップでの放出率が最大放出率より小さい場合は、最大放出率を用いて放出量が計算される。
- (71) 生成量及び放出率によって計算された放出されたクリプトン量
(70)と同様に常に最大量が計算に用いられるようになっている。
- (72) (71)と同様なキセノン量
- (73) 軸方向の総計と平均
- (74) (69)、(71)及び(72)の各々の量に軸方向セグメント長を掛けて合計された燃料ピン中の総量
- (75) GAPCON-THERMAL-1 Original Versionで計算されるガス放出率
(燃料ピン全体の体積平均温度によって与えられた放出率)
- (76) (74)の各項を用いて計算された(全放出量)/(全生成量)
- (77) 熱膨張、Densification及びそれらの重ね合せによる、ペレット・スタック長変化量、熱膨張量はディッシュ肩相当半径での温度(67)を用いて計算される。もしディッシュ半径の入力がなければ中心で行なう。
- (78) (77)で計算された長さ変化× πr_{ci}^2 , r_{ci} =被覆管内面半径
- (79) 初期プレナム体積より(78)を差し引いたプレナム体積

- (80) (79)で計算されたプレナム体積を用いて、計算した燃料棒内圧。
ここで計算された内圧は、他の計算に一際影響しない。
- (81) 軸方向セグメント毎の半径方向温度分布。半径は変形後の値である。このプリントアウトは照射履歴に
対応したHistory dataを与える際の各タイム・ステップに依存したコントロール・シグナル（入
力説明参照）によって行なわれる。
- (82) (81)と同様詳細な温度分布をライン・プリンターによって図示してある。この場合(81)と同様なコン
トロール・シグナルとIIPROF = 1 の入力が必要である。左端よりメッシュ温度、半径及びプロット
された温度であり通常(*)によって示されているが、融点(入力)を超えた場合は(M)によって示
される。
- (83) FPガスの各軸方向セグメント毎の原子数及び放射能。
(69)でプリントした値は単位長当たりの数値である。
- (84) プレナム及びギャップへ放出されたFPガスの原子数及び放射能(83)及び(84)はNUCLEI = 1 の入
力によって計算、プリントアウトされる。

Table B-2 接触圧力のgrade区分

被覆管内面変位=熱膨張+内外圧による弾性変形+クリープ

最大ギャップ巾=初期ギャップ+被覆管内面変位-ペレット・デンシフィケーション (= GAP9)

GRADE	1	2	3	4	5
Print Out Symbol	A	B	C	D	E
名称	HARD CONTACT-1	HARD CONTACT-2	MEDIUM	SOFT	OPEN
ペレット変位 (= DELRSM)	(保守的な熱膨張) + (保守的なスウェーリング) (= DELRSM)	(保守的なスウェーリング) + (使用者指定の熱膨張 モデル及び線熱膨張係数 計算式)	(使用者指定のスウェーリング) + (使用者指定の熱膨張 モデル) + (IGRADE = 2 のときと同じ熱膨張 計算式)	(IGRADE = 3 と同じ 変位) + (リロケーション ノン)	IGRADE = 4 と同じ 変位 > DELRSM
HOT GAP	CEE × RESGAP ^(*)	CEE × RESGAP	CEE × RESGAP 但し CEE = 1	CEE × RESGAP 但し CEE = 1	GAP9 - DELRSM
接觸圧力 (= PFACE)	被覆管ペレット 相互干渉量 (RINT) より薄内円筒弾性変形理 論によって計算。	1.70 (max) (kg/cm ²) 7.6 + 9.4 × COEF ^(**)	7.6 (max) (kg/cm ²) 7.6 × COEF	0.0	0.0

(*) CEE = 接触圧力に依存する Gap Correlation factor (= exp (- 0.00125 × PFACE))

(**) RESGAP = $2 \times (\text{ペレット表面粗さ} + \text{被覆管表面粗さ}) + 1 \times 10^{-5}$ (cm)

(***) COEF = 相互干渉量 (RINT = DELRSM - GAP9) / 最大相互干渉可能量

各 GRADE (GRADE) の選択法

最大ギャップ巾 (GAP9) に対して、 GRADE = 1 より遅時ペレット変位 (DELRSM) を計算、比較し DELRSM > GAP9 となつたときは、接触の GRADE とする。