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GAMLEG-JR: A PRODUCTION CODE OF
MULTI-GROUP CROSS SECTIONS AND ENERGY
ABSORPTION COEFFICIENTS FOR GAMMA RAYS

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GAMLEG-JR

A Production Code of Multi-group Cross Sections and
Energy Absorption Coefficients for Gamma Rays

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GAMLEG-JR is a modification of GAMLEG to produce multi-group photon cross sections for use in the S_n -type transport codes. In the GAMLEG code, the cross section data for the photoelectric effect, pair production and coherent scattering are read in tabular form by cards. GAMLEG-JR generates these cross section data by simple empirical formulae as a function of atomic number Z. The code also produces the group-averaged gamma-ray energy absorption coefficient (KERMA factor). An integration of obtaining the group averaging transfer cross sections has been modified in the present code, because the original integration method is inadequate for calculations of higher Legendre moments in the low energy region.

The group cross sections produced by the code are compared with the theoretical ones.

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GAMLEG-JR, ガンマ線多群定数および発熱定数作成コード

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GAMLEG-JR は Sn 輸送計算コード用の多群光子断面積作成コードとして開発された GAMLEG を改造したものである。GAMLEG では光電効果、電子対生成およびコヒーレント 散乱断面積を入力データとして用意しなければならないが、GAMLEG-JR では原子番号 Z の 関数として表わす経験式を用いて、これらの断面積を求めるように変更した。また GAMLEG-JR は群定数化されたガンマ線発熱定数 (KERMA) も求められるようプログラムの改造が行なわれている。また原典では、遷移断面積の積分方法が低エネルギー領域で高次のルジヤンドル モーメントに対して適切でなくなるので、本コードではその積分法を変更した。

本コードで計算された群定数を理論値等と比較し、その計算精度が評価された。

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1. Introduction

The GAMLEG code was designed to generate multigroup photon cross sections for use in the Sn-type transport calculations. For performing numerical integration to produce group-averaged cross sections in the code, the cross section data for photoelectric, pair production and coherent scattering reactions have to be prepared in tabular forms by input cards. However, the preparation of those data are somewhat troublesome for users. In order to eliminate such trouble GAMLEG-JR generates those cross section data by using the simple empirical formulae as a function of atomic number Z . The code also produces the energy deposition coefficient (KERMA factor) given by

$$h_\gamma(I) = 1.6 \times 10^{-13} (\mu_{en}/\rho) \cdot (M/N_0) \cdot \bar{E}_I [\text{barn} \cdot \text{watt} \cdot \text{sec/atom}], \quad (1)$$

where M is the atomic mass number, N_0 is the Avogadro's number, and \bar{E}_I is the mean energy of the I -th group. The (μ_{en}/ρ) is the mass energy absorption coefficient given by⁴⁾

$$\mu_{en}/\rho = \left(\frac{c}{\rho}\right)f_c + \left(\frac{\tau}{\rho}\right)f_\tau + \left(\frac{k}{\rho}\right)f_k, \quad (2)$$

where the first, second and third terms represent respectively the mass energy-transfer coefficient for Compton scattering, photoelectric absorption and pair production. The code calculates the mass energy absorption coefficient by neglecting the bremsstrahlung effect of recoil electrons.

The original code, GAMLEG, calculates analytically the energy integral of an equation for the average transfer cross section. However, this integration method was found not to be adequate for obtaining the higher Legendre moments than the 6th order at low energy region below about 0.1 MeV, because of round-off errors caused by the machine computation. The present code, GAMLEG-JR, calculates this integral by the numerical integration based on the Simpson's rule for equally spaced μ ($= 1+1/E'-1/E$).

The present code is written in FORTRAN-IV for use on the FACOM-230/75 machine. The program provides up to 50-energy groups and up to nine Legendre moments for each of unlimited number of elements. Flux weighting data are limited to a maximum of 500 values.

The paper presents also the results of evaluation for the calculated cross sections by comparing with theoretical values.

2. Absorption Cross Sections

2.1 Photoelectric Cross Section¹⁾

An empirical formula of photoelectric cross section for the K-shell photoeffect above 0.2 MeV, τ_k , is given by

$$\tau_k = Z^5 \sum_{n=1}^4 \frac{a_n + b_n Z}{1 + c_n Z} e^{-p_n} \quad (\text{barns/atom}), \quad (3)$$

where a_n , b_n , c_n and p_n are given in the following table.

n	a_n	b_n	c_n	p_n
1	1.6268×10^{-9}	-2.683×10^{-12}	4.173×10^{-2}	1
2	1.5274×10^{-9}	-5.110×10^{-19}	1.027×10^{-2}	2
3	1.1330×10^{-9}	-2.177×10^{-12}	2.013×10^{-2}	3.5
4	-9.12×10^{-11}	0.0	0.0	4

The ratio of the total photoelectric to K-shell photoelectric cross section is written as

$$\tau_{pe}/\tau_k = 1 + 0.01481 \ln^2 Z - 0.000788 \ln^2 Z \quad (4)$$

For an element with the atomic number greater than 8, and for photon energy less than $E_0 = 0.01 \exp[0.031(Z-8)]$ MeV, the cross section for K-shell is calculated by the formula;

$$\begin{aligned} \tau_k = & \frac{3}{2} \phi_0 \frac{Z^5}{(137)^4} n^5 (\gamma^2 - 1)^{3/2} \left[\frac{4}{3} + \frac{\gamma(\gamma-2)}{\gamma+1} \right] \left\{ 1 - \frac{1}{2\gamma(\gamma^2-1)^{1/2}} \right. \\ & \times \left. \ln \frac{\gamma+(\gamma^2-1)^{1/2}}{\gamma-(\gamma^2-1)^{1/2}} \right\} \cdot f \quad [\text{barn/atom}], \end{aligned} \quad (5)$$

where

$$f = 2\pi \left(\frac{I}{hv} \right)^{1/2} \left[\frac{\exp(-4x) \arccot x}{1 - \exp(-2\pi x)} \right],$$

$$\phi_0 = 8\pi r_0^2/3 = 6.6537 \times 10^{-25} \text{ (cm}^2\text{)},$$

$$r_0 = e^2/(mc^2) = 2.8182 \times 10^{-13} \text{ (cm)},$$

$$mc^2 = 0.51084 \text{ (MeV)},$$

$$n = mc^2/(hv),$$

$$\gamma = h\nu/(mc^2) + 1,$$

$I = (Z-0.3)^2 Ry$ (photon energy at K-shell edge in units of MeV)

$Ry = 13.52$ (eV) (Rydberg's constant),

$$x = [I/(h\nu-I)]^{1/2}$$

The cross sections τ_{LI} , τ_{LII} and τ_{LIII} for L-shell are given by

$$\tau_{LI} = \frac{2^{12}\pi\phi_0(137)^3}{(Z-S_2)^2} \left(\frac{\nu_2}{\nu}\right)^4 \left(1+3\frac{\nu_2}{\nu}\right) \frac{\exp(-8\xi_2 \operatorname{arccot} \xi_2)}{1-\exp(-4\pi\xi_2)}, \quad (6)$$

$$\tau_{LII} + \tau_{LIII} = \frac{2^{12}\pi\phi_0(137)^3}{(Z-S_2)^2} \left(\frac{\nu_2}{\nu}\right)^5 \left(3+8\frac{\nu_2}{\nu}\right) \frac{\exp(-8\xi_2 \operatorname{arccot} \xi_2)}{1-\exp(-4\pi\xi_2)}, \quad (7)$$

where

$$S_2 = 4.15 \quad (Z>10),$$

$$\nu_2 = \frac{1}{4} (Z-S_2)^2 Ry,$$

$$\xi_2 = [\nu_2/(\nu-\nu_2)]^{1/2}.$$

2.2 Pair Production Cross Section²⁾

The pair production cross section, κ , is written as follows:

i) $E < 1.022$ MeV

$$\kappa = 0.0, \quad (8)$$

ii) 1.022 MeV $< E < 2.0$ MeV

$$K = \frac{Z^2 r_0^2}{137} \cdot \frac{2\pi}{3} \cdot \left(\frac{K-2}{K}\right)^3 \left[1 + \frac{1}{2} + \frac{23}{40} p^2 + \frac{11}{60} p^3 + \frac{29}{960} p^4 + \dots\right], \quad (9)$$

iii) $E > 2.0$ MeV

$$K = \frac{Z^2 \cdot r_0^2}{137} \left\{ \frac{28}{9} \ln(2K) - \frac{218}{27} + \left(\frac{2}{K}\right)^2 [6 \ln(2K) - \frac{7}{2} \right.$$

$$+ \frac{2}{3} \ln^3(2K) - \ln^2(2K) - \frac{1}{3} \pi^2 \ln(2K) + 2\zeta(3) + \frac{\pi^2}{6} \right)$$

$$- \left(\frac{2}{K}\right)^4 \left[\frac{3}{16} \ln(2K) + \frac{1}{8}\right] - \left(\frac{2}{K}\right)^6 \left[\frac{29}{9.256} \ln(2K) \right.$$

$$\left. - \frac{77}{27.512} + \dots\right\}, \quad (10)$$

where,

$$\rho = (2k-4)/(2+k+2\sqrt{2K}),$$

$$\xi(3) = \sum_{n=1}^{\infty} \frac{1}{n^2} = 1.2020569,$$

$$K = h\nu/mc^2.$$

2.3 Coherent Scattering Cross Section

The coherent scattering cross section is given by

$$\frac{d\sigma_R(\theta)}{d\Omega} = \frac{r_0^2}{2} (1+\cos^2\theta) [F(g, Z)]^2, \quad (11)$$

where $F(g, Z)$ is an atomic form factor and depends on knowledge of the atomic wave function.

Figure 1 shows the coherent scattering cross sections of H, Al, Fe and Pb given in Ref. 3). In the present code, the cross sections are evaluated from a function of atomic number Z and photon energy E obtained by using the least squares method for the data given in Ref. 3).

$$\sigma_R = \exp[-0.09615(\ln E + 11.532)^2 + 2.357 \ln \frac{Z}{26} + 9.436]. \quad (12)$$

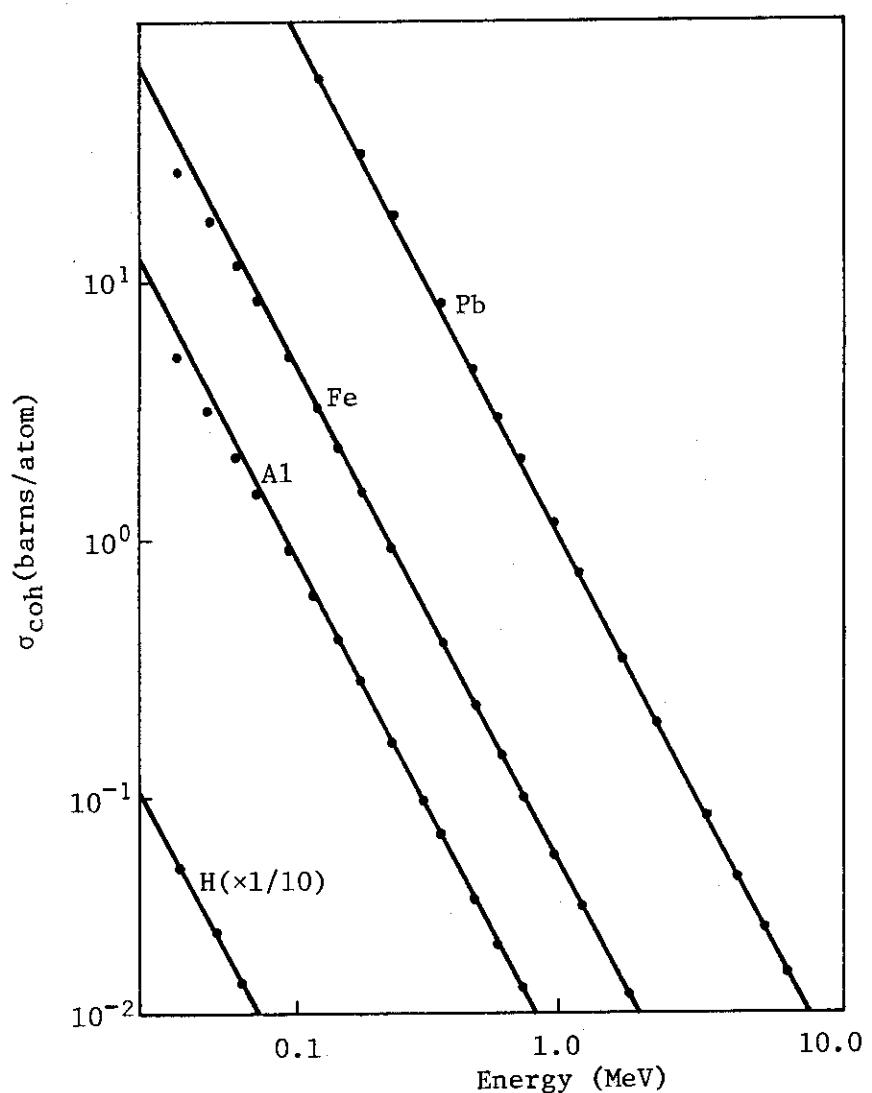


Fig. 1 Coherent gamma-ray scattering cross section³⁾

3. Energy Deposition Coefficient

The mass energy absorption coefficient, μ_{en}/ρ , is the weighted sum of the probabilities per unit path length for Compton scattering (c/ρ), photoelectric absorption (τ/ρ) and pair production (κ/ρ):

$$\frac{\mu_{en}}{\rho} = \left(\frac{c}{\rho}\right)f_c + \left(\frac{\tau}{\rho}\right)f_\tau + \left(\frac{\kappa}{\rho}\right)f_\kappa. \quad (13)$$

The weights f_c , f_τ and f_κ are conversion factors which are the fraction of the photon energy converted eventually into kinetic energy of electrons and dissipated to the medium via collision losses as ionization and excitation.

3.1 Compton scattering⁴⁾

The f_c for the Compton scattering is given by

$$f_c(h\nu) = \frac{1}{h\nu} \int_0^{T_{max}} P_c(h\nu, T) T [1 - G_{br}(T)] dT, \quad (14)$$

where

$$T_{max} = \frac{2(h\nu)^2}{mc^2 + 2h\nu},$$

$$P_c(h\nu, T) = \frac{d\sigma}{dT} / \sigma_T,$$

$$\frac{d\sigma}{dT} = \frac{\pi r_o^2 mc^2}{(h\nu_o - T)^2} \left\{ \left[\frac{mc^2 T}{(h\nu_o)^2} \right]^2 + 2 \left[\frac{h\nu_o - T}{h\nu_o} \right]^2 \right.$$

$$\left. + \frac{h\nu_o - T}{(h\nu_o)^3} [(T - mc^2)^2 - (mc^2)^2] \right\},$$

$$\sigma_T = 2\pi r_o^2 \left\{ \frac{1+\alpha}{\alpha^3} \left[\frac{2\alpha(1+\alpha)}{1+2\alpha} - \ln(1+2\alpha) \right] \right.$$

$$\left. + \frac{\ln(1+2\alpha)}{2\alpha} - \frac{1+3\alpha}{(1+2\alpha)^2} \right\},$$

$$\alpha = h\nu/(mc^2).$$

The $P_c(h\nu, T)$ is the probability that a free electron is recoiled with kinetic energies between T and $T + dT$ as a result of the Compton scattering

of a photon of energy $h\nu$. The $G_{br}(T)$ is the average fraction that an electron of initial kinetic energy T dissipates its energy in bremsstrahlung. In the code, however, we have assumed that $G_{br}(T) = 0$.

3.2 Photoelectric absorption⁴⁾

The f_τ for the photoelectric absorption is written as follows:

$$f_\tau = \begin{cases} 1 - \left(\frac{\tau_k}{\tau}\right) \left(\frac{F_k \bar{E}_k}{h\nu}\right), & \text{for K-shell,} \\ 1 - \frac{F_L \bar{E}_L}{h\nu}, & \text{for L-shell,} \end{cases} \quad (15)$$

where τ_k is the photoelectric cross section for K-shell, F_k and F_L are the mean fluorescence yields for K-shell and L-shell, respectively, and \bar{E}_k and \bar{E}_L are the mean energies of the fluorescence photons. The fluorescence yields and average energies of fluorescence for the K and L shells are shown in Table 1 for several elements.

Table 1 Fluorescence yields and average energies of fluorescence⁴⁾

Element	Z	F_k	\bar{E}_k (keV)	F_L	\bar{E}_L (keV)
C	6	0.0	0.279		
N	7	0.0	0.393		
O	8	0.0	0.524		
Na	11	0.013	1.041		0.031
Mg	12	0.020	1.255		0.048
Al	13	0.030	1.487		0.069
P	15	0.051	2.020		0.169
S	16	0.069	2.317		0.206
Ar	18	0.105	2.977		0.286
K	19	0.129	3.337		0.334
Ca	20	0.151	3.719		0.385
Fe	26	0.312	6.472		0.714
Cu	29	0.404	8.142		0.937
Mo	42	0.747	17.787	0.072	2.343
I	53	0.868	29.291	0.134	4.145
Pb	82	0.955	77.002	0.400	11.719
U	92	0.961	100.964	0.449	15.509

3.3 Pair production⁴⁾

The f_k for the pair production is given by

$$f_k = 1 - \frac{2mc^2}{hv} - (hv) \int_0^{hv-2mc^2} P_p(hv_1 T^+ T^-) [T^- G_{br}(T^-) + T^+ G_{br}(T^+) + \tau(T^+)] dT^+ . \quad (16)$$

Table 2 and Fig. 2 give the f_k values⁴⁾ for several elements obtained from Eq. (16) by omitting the integral over $\tau(T^+)$ which accounts for the annihilation of positrons in flight. In the present code the f_k value is obtained with the linear interpolation over photon energies and atomic numbers using Table 2.

Table 2 Energy absorption fraction of pair-production reaction f_k with corrections for bremsstrahlung losses but without correction for annihilation of positrons⁴⁾

Element Z	H	C	N	O	Na	Mg	Al	P	S	A	K	Ca	Fe	Cu	Pb
Photon energy(MeV)	1	6	7	8	11	12	13	15	16	18	19	20	26	29	82
1.5	0.318	0.318	0.318	0.317	0.37	0.37	0.317	0.316	0.316	0.316	0.316	0.317	0.314	0.312	
2.0	0.488	0.487	0.489	0.486	0.485	0.485	0.487	0.484	0.484	0.483	0.483	0.482	0.484	0.480	0.471
3.0	0.658	0.655	0.654	0.654	0.652	0.651	0.653	0.649	0.648	0.647	0.646	0.645	0.646	0.640	0.616
4.0	0.743	0.738	0.737	0.736	0.733	0.732	0.734	0.729	0.728	0.726	0.725	0.724	0.722	0.715	0.675
5.0	0.794	0.787	0.788	0.785	0.780	0.779	0.780	0.775	0.774	0.771	0.770	0.770	0.769	0.763	0.757
6.0	0.828	0.820	0.818	0.816	0.811	0.810	0.809	0.804	0.803	0.799	0.798	0.796	0.788	0.781	0.712
8.0	0.870	0.858	0.855	0.853	0.846	0.843	0.842	0.836	0.834	0.829	0.827	0.824	0.811	0.804	0.712
10.0	0.895	0.879	0.876	0.873	0.863	0.861	0.857	0.851	0.848	0.842	0.839	0.836	0.819	0.808	0.700

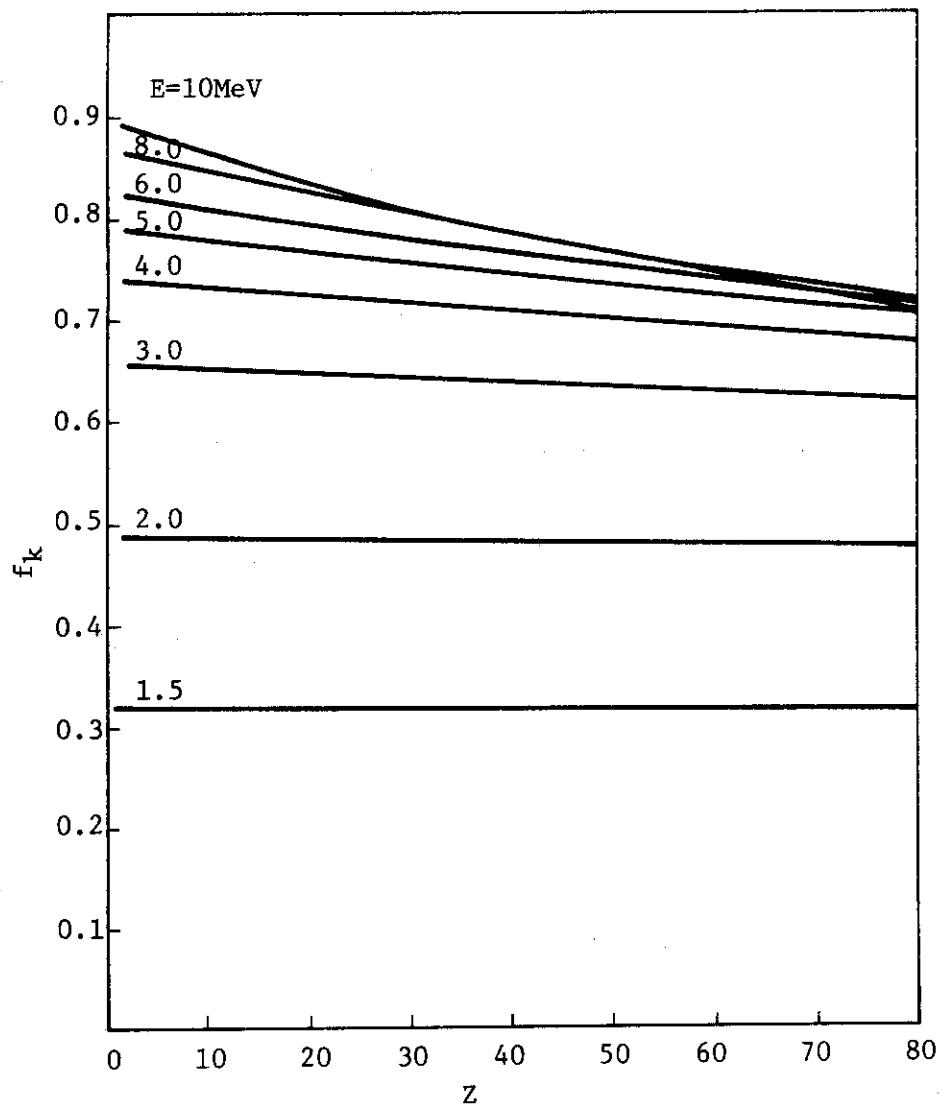


Fig. 2 Energy absorption fraction for pair production reaction f_k with correction for bremsstrahlung losses as a function of incident photon energy and atomic number of medium

4. Modification of Integration Method for Transfer Cross Section

The average transfer cross section from group h to group g is written by

$$\sigma_{\text{sn}}^{g \leftarrow h} = \frac{\int_{E' \text{ in } h} f(E') \int_{E \text{ in } g} \sigma_{\text{sn}}(E' \rightarrow E) dE' dE}{\int_{E' \text{ in } h} f(E') dE'}, \quad (17)$$

where $f(E')$ is a weighting function given by input data and $\sigma_{\text{sn}}(E' \rightarrow E)$ of Eq. (17) are given by

$$\sigma_{\text{sn}}(E' \rightarrow E) = \frac{3}{8E'^2} \left[\frac{E'}{E} + \frac{E}{E'} + 2 \left(\frac{1}{E'} - \frac{1}{E} \right) + \left(\frac{1}{E'} - \frac{1}{E} \right)^2 \right] \cdot P_n \left(1 + \frac{1}{E'} - \frac{1}{E} \right), \quad (18)$$

for $E'/(1+2E') < E < E'$.

The original code, GAMLEG, calculates analytically the E integral of Eq. (18). However, this integration was not adequate for the higher Legendre moments than the 6th order at low energy region below about 0.1 MeV, because of round-off errors caused by the machine computation. Therefore, GAMLEG-JR calculates this integral by using the numerical integration based on the Simpson's rule for equally spaced μ , a Compton scattering angle. The E integral of Eq. (18) is written by

$$\begin{aligned} \int \sigma_{\text{sn}}(E' \rightarrow E) dE &= \int \sigma_{\text{sn}}(E' \rightarrow E) \frac{dE}{d\mu} d\mu \\ &= \int \frac{3}{8E'^2} \left[1+E'(1-\mu) + \frac{1}{1+E'(1-\mu)} + 2(\mu-1) + (\mu-1)^2 \right] \\ &\quad \times \left[\frac{E'}{1+E'(1-\mu)} \right]^2 \cdot P_n(\mu) d\mu, \end{aligned} \quad (19)$$

where $\mu = 1 + 1/E' - 1/E$.

4. Modification of Integration Method for Transfer Cross Section

The average transfer cross section from group h to group g is written by

$$\sigma_{\text{sn}}^{g \leftarrow h} = \frac{\int_{E' \text{ in } h} f(E') \int_{E \text{ in } g} \sigma_{\text{sn}}(E' \rightarrow E) dE dE'}{\int_{E' \text{ in } h} f(E') dE'}, \quad (17)$$

where $f(E')$ is a weighting function given by input data and $\sigma_{\text{sn}}(E' \rightarrow E)$ of Eq. (17) are given by

$$\sigma_{\text{sn}}(E' \rightarrow E) = \frac{3}{8E'^2} \left[\frac{E'}{E} + \frac{E}{E'} + 2 \left(\frac{1}{E'} - \frac{1}{E} \right) + \left(\frac{1}{E'} - \frac{1}{E} \right)^2 \right] \cdot P_n \left(1 + \frac{1}{E'} - \frac{1}{E} \right), \quad (18)$$

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where $\mu = 1 + 1/E' - 1/E$.

5. Evaluations of Calculated Multigroup Cross Sections

In order to evaluate the calculational accuracies of GAMLEG-JR, cross sections generated by the code were compared with experimental and theoretical values given in Ref. 2.

Table 3 shows the ratio of the calculated photoelectric cross sections to those given in Ref. 2 for elements of Z=1, 4, 6, 13, 26, 53, 82 and 92. Deviations from the values given in Ref. 2 are less than 1 to 5 percent for most of energies above 0.2 MeV for all elements except for hydrogen. However, in the energy region below 0.2 MeV, the discrepancies gradually increase because of irregularities in the higher electron shell structure. In the GAMLEG-JR, the photoelectric cross section for hydrogen is corrected empirically by using the ratio given in table 3.

Table 4 shows the ratio of the calculated pair production cross sections to those given in Ref. 2 for elements of Z=1, 6, 13, 26, 53, 82 and 92. Deviations from the values given in Ref. 2 are less than 1 to 2 percent for all energy region and for all elements.

Table 5 presents the ratio of the mass energy absorption coefficients calculated by GAMLEG-JR to those given in Ref. 2 for elements of Z=1, 6, 13, 26, 82 and 92. The calculated values are larger by about 10 to 15 percent than those given in Ref. 2 for energy regions above 0.2 MeV and are smaller by about 10 to 50 percent at lower energies below 0.2 MeV. Major sources of the discrepancies at higher energies may be the neglect of energy dissipation effect due to bremsstrahlung at the Compton scattering and of annihilation effect of positrons due to the pair production reactions in the calculation for the energy absorption coefficient. At lower energies, the insufficient accuracy of the empirical formula for the photoelectric cross section is the source of the discrepancy.

Table 3 Ratio of the photoelectric cross sections calculated by GAMLEG-JR to those given by Ref. 2 ($\sigma_{\text{cal}}/\sigma_{\text{Ref}}$) for a number of elements

Z E(MeV)	1	4	6	13	26	53	82	92
1.5(-2)*	0.785	0.509	0.476	0.388	0.979	0.712	0.445	0.546
2.0(-2)	0.986	0.606	0.641	0.610	0.335	0.670	0.598	0.481
4.0(-2)	1.354	0.760	0.929	0.871	0.892	0.884	0.620	0.582
6.0(-2)	1.514	0.820	0.865	0.919	0.989	0.808	0.568	0.532
1.0(-1)	1.663	0.878	0.903	0.954	1.032	0.981	0.908	0.477
1.5(-1)	1.764	0.905	0.927	0.961	1.018	1.017	0.982	0.917
2.0(-1)	1.817	0.923	0.939	0.957	1.004	1.019	1.014	0.993
4.0(-1)	1.948	0.971	0.975	0.983	1.010	1.017	1.018	1.029
6.0(-1)	2.000	0.992	0.998	1.000	1.019	1.000	0.995	1.016
8.0(-1)	2.034	1.009	1.009	1.000	1.017	1.000	0.990	1.000
1.0	2.055	1.020	1.021	1.010	1.015	0.998	0.986	1.000
1.5	2.119	1.038	1.037	1.010	1.019	1.010	1.000	1.011
2.0	2.119	1.037	1.023	0.997	0.998	1.000	0.989	1.018
3.0	2.139	1.036	1.025	0.995	0.993	0.985	1.001	1.007
4.0	2.158	1.045	1.033	0.993	0.992	0.992	1.017	1.024
6.0	2.164	1.045	1.035	0.995	0.986	0.989	1.024	1.033
8.0	2.190	1.049	1.035	0.995	0.987	0.992	1.030	1.032
10.0	1.483	1.039	1.036	0.989	0.983	0.986	1.017	1.021

* to be read as 1.5×10^{-2}

Table 4 Ratio of the pair production cross sections calculated by GAMLEG-JR to those given by Ref. 2 ($\sigma_{\text{cal}}/\sigma_{\text{Ref.}}$) for a number of elements

Z E(MeV)	1	6	13	26	53	82	92
1.5	1.002	1.006	1.010	1.009	1.011	1.009	1.009
3.0	0.992	0.995	0.995	1.000	1.000	1.003	1.004
4.0	0.999	1.000	1.000	1.005	1.008	1.010	1.012
6.0	1.007	1.002	1.004	1.010	1.014	1.019	1.019
8.0	1.000	1.003	1.010	1.009	1.017	1.029	1.023
10.0	1.000	1.004	1.008	1.014	1.016	1.016	1.020
15.0	1.007	1.000	1.013	1.017	1.001	0.968	0.957

Table 5 Ratio of the mass energy absorption coefficients calculated by GAMLEG-JR to those given in Ref. 2 ($\mu_{\text{en,cal}}/\mu_{\text{en,Ref.}}$)

Z E(MeV)	1	6	13	26	82	92
0.04	1.048	0.928	1.091	0.713	0.549	0.512
0.06	0.938	0.934	1.083	0.991	0.556	0.517
0.1	1.074	1.060	1.075	0.986	0.776	0.613
0.2	1.109	1.105	1.095	1.056	0.971	0.989
0.4	1.072	1.068	1.112	1.065	1.035	1.056
0.6	1.053	1.061	1.079	1.105	1.055	1.081
0.8	1.094	1.093	1.075	1.099	1.073	1.090
1.0	1.088	1.082	1.029	1.092	1.085	1.102
1.5	1.023	1.027	1.086	1.042	1.074	1.098
2.0	1.069	1.073	1.093	1.091	1.100	1.122
3.0	1.070	1.073	1.105	1.098	1.124	1.142
4.0	1.099	1.086	1.073	1.131	1.151	1.168
5.0	1.009	1.082	1.098	1.113	1.131	1.152
6.0	1.034	1.043	1.010	1.090	1.121	1.142
8.0	1.032	1.075	0.928	1.113	1.126	1.154
10.0	1.071	1.079	0.818	1.115	1.116	1.094

6. Input Preparation

The input data necessary for GAMLEG-JR are defined and listed below, in order of the original input. Integers are read according to a 14I5 format, and floating point numbers are read with a 6E12.5 format. All energies are in MeV and read in the descending order beginning at the highest energy.

Card 1 (8I5)

1. IG Number of groups plus one.
2. N Number of integration intervals/group.
3. NMAX Number of Legendre components to be prepared (≤ 9).
4. KON -1 = input flux weighting.
0 = no weighting.
1 = source weighting.
5. ICAL 0 = give the absorption and coherent scattering cross sections by input card.
1 = calculate above cross sections and gamma-ray heat generation coefficients by the code.
6. IPRT0 0 = no effect.
1 = print detailed information for absorption and coherent scattering cross sections.
7. IPRT1 0 = no effect.
1 = print detailed information for heat generation coefficients.
8. NACT 0 = no effect.
1 = add the gamma-ray heat generation coefficients to the cross section table as an activation cross section.

Cards 2 (input if KON=-1)

Card 2.1 (I5)

IF Number of input fluxes.

Cards 2.2 (6E12.5)

(EFLUX(I), I=1, IF)

Energies at which input fluxes are given.

Cards 2.3 (6E12.5)

(FLUX(I), I=1, IF)

Input flux weighting function.

Cards 3Card 3.1 (15)

IS Number of input sources.

Cards 3.2 (6E12.5)

(ES(I), I=1, IS)

Energies at which input sources are given.

Cards 3.3 (6E12.5)

(S(I), I=1, IS)

Input sources.

Cards 4 (6E12.5)

(EG(I), I=1, IG)

Gamma-ray energy group boundaries in MeV.

Cards 5Card 5.1 (15)

IZ Number of materials to be processed.

Card 5.2 (6E12.5)

(Z(I), I=1, IZ)

Atomic numbers of elements

Cards 6 (input if ICAL = 0)Card 6.1 (2I5)

1. IA Number of input absorption cross sections.

2. IC Number of input coherent scattering cross sections.

Card 6.2 (6E12.5)

(SIGA(I), I=1, IA)

Absorption cross sections (barns) for the first element.

Card 6.3 (6E12.5)

(EA(I), I=1, IA)

Energies of which absorption cross sections are given for the first element.

Cards 7 (input if ICAL=0 and IC≠0)Card 7.1 (6E12.5)

(SIGCOH(I), I=1, IC)

Coherent scattering cross sections (barns) for the first element.

Cards 7.2 (6E12.5)

(ECOH(I), I=1, IC)

Energies at which coherent scattering cross sections are given for the first element.

Input cards 6 and (possibly) 7 are repeated for each element.

7. Sample Input and Output

A sample problem of 20-group structure and nine Legendre moments is present for iron. A no weighting option and ten integration intervals in each group were used. A list of the sample problem is shown in Table C-1 of Appendix C.

The sample output for the average cross sections of iron is presented in Table C-2 of Appendix C. For each group, the column entries are σ_{heat} , σ_a , $v\sigma_f$, σ_t , $\sigma_{g \leftarrow g}$, $\sigma_{g \leftarrow g+1}$, The heading of each table identifies the element by its atomic number and the Legendre component by P_n , $n=0, 1, 2, \dots, NMAX-1$.

The format and the sequence of punched output is the same as those of GAMLEG.

Running time required to generate the cross sections for the sample problem was about 6 seconds in CPU on the FACOM 230/75.

References

- 1) Lathrop K. D.: "GAMLEG", LA-3267 (1965).
- 2) Hubbell J. H.: "Photon Cross Section, Attenuation Coefficients, and Energy Absorption Coefficients from 10 KeV to 100 GeV", NSRDS-NBS 29 (1969).
- 3) Storm E., et al.: "Photon Cross Sections from 0.001 to 100 MeV for Element 1 through 100", LA-3753 (1967).
- 4) Berger, R. T.: "The X- or Gamma-Ray Energy Absorption or Transfer Coefficient: Tabulations and Discussions", Radiation Research, 15, 1 ~ 29 (1961).

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The format and the sequence of punched output is the same as those of GAMLEG.

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References

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Appendix A Description of Subroutines Added to GAMLEG

1. CROSS

called from: Main Routine

subroutine called: POTO, PAIR, COHER, NROW

CROSS controls the subroutines which calculate photoelectric, pair-production and coherent scattering cross sections, and heat generation coefficients.

2. POTO

called from: CROSS

subroutine called: POTO3

POTO calculates the photoelectric cross section for K-shell at high energy.

3. POTO3

called from: POTO

subroutine called: P06MV1

POTO3 calculates the photoelectric cross section for K-shell at low energy.

4. P06MV1

called from: POTO3

subroutine called: FUNC1, FUNC2

5. FUNC1, FUNC2

called from: P06MV1

The function subroutines FUNC1 and FUNC2 calculate the photoelectric cross sections.

6. PAIR

called from: CROSS

PAIR calculates the pair-production cross section.

7. COHER

called from: CROSS

COHER calculates the coherent scattering cross section.

8. NROW

called from: CROSS

subroutine called; INTFK, INTFT, COMPT

NROW calculates the heat generation coefficient for each interaction:
photoelectric, f_T , pair production, f_k , and Compton scattering, f_C .

9. INTFFT

called from: NROW

INTFFT interpolates the fluorescence yield and the averaged energy
from the values given in Table 1.

10. INTFK

called from: NROW

INTFK interpolates the f_k value from the values given in Table 2.

Appendix B Program List of GAMLEG-JR

SOURCE ELEMENT LIST (8BIT MODE)

ELEMENT NAME ((GAMLEG)) ESTABLISHED 77.01.25

```

C
C PROGRAM GAMLEG-JR  ( MODIFIED BY JAERI ON 1976 )           GAM00010
C **** FOLLOWING ROUTINE WAS ADDED                           GAM00020
C   1. CALCULATION OF PHOTO ELECTRIC, PAIR PROPUCTIVE, AND COHERENT   GAM00030
C      SCATTERING CROSS SECTION                                     GAM00040
C   2. CALCULATION OF HEAT PRODUCTION COEFFICIENT.                  GAM00050
C
C
C GIVEN SOURCE AND ABSORPTION ENERGY DEPENDENCE CODE PROVIDES       GAM00060
C GROUP AVERAGED CROSS SECTIONS FOR INPUT TO THE DTF OR DDF          GAM00070
C CODES. UP TO N (N LESS THAN 10) LEGENDRE TRANSFER SCATTERING CROSSSECTIONS GAM00080
C SECTIONS ARE PREPARED.                                              GAM00090
C
C THREE WEIGHTING OPTIONS ARE AVAILABLE: (A)-UNWEIGHTED, (B)-SOURCE GAM00100
C ENERGY WEIGHTING, (C)-WEIGHTING WITH INPUT FLUX                   GAM00110
C
C
C COMMON EG( 51),ASG( 50),SIGS( 50),SIGC( 50),DF( 50),FG( 50),           GAM00120
C 1FLUX( 500),SC( 500),ESC( 500),IS,SIGA( 500),EAC( 500),IA,SGC( 50),    GAM00130
C 2SIGCOH( 500),ECOH( 500),IC+SIGMATIC( 54,50),TRANS( 50, 50, 9),        GAM00140
C 3FLUXSC( 50,101),EFLUXC( 500),Z(50),SIGTOT( 50),GXX( 50),ENNUC( 500)   GAM00150
C COMMON /JDB/IGA+IM,FN,ICAL,IPRT0,IPRT1,J1,GE( 51)                      GAM00160
C
C DEFINITION OF VARIABLES                                         GAM00170
C SIGA(I)=ABSORPTION C/S                                         GAM00180
C EAC(I)=ABSORPTION ENERGIES                                      GAM00190
C SC(I)=SOURCE                                                       GAM00200
C ESC(I)=SOURCE ENERGIES                                         GAM00210
C SIGCOH(I)=COHERENT SCATTERING CROSS SECTION                    GAM00220
C ECOH(I)=ENERGIES FOR ABOVE                                     GAM00230
C EG(I)=GROUP ENERGIES                                           GAM00240
C ASG(I)=GROUP AVG ABSORPTION CROSS SECTION                     GAM00250
C SIGS(I)=GROUP AVG SCATTERING CROSS SECTION                   GAM00260
C SIGC(I)=GROUP AVG COHERENT CROSS SECTION                      GAM00270
C FG(I)=GROUP AVG FLUX                                         GAM00280
C SG(I)=GROUP AVG SOURCE                                       GAM00290
C TRANS(I,J)=GROUP AVG TRANSFER CROSS SECTIONS                 GAM00300
C SIGMAT(I,J)=SCATTERING TRANSFER MATRIX                         GAM00310
C
C GXX(I)=GROUP AVG HEAT GENERATION COEFFICIENT                GAM00320
C ENNU(I)=FINE GROUP HEAT GENERATION COEFFICIENT               GAM00330
C
C FLUXS(I)=WEIGHTING FUNCTION                                    GAM00340
C
C IA=NO. ABSORPTION ENERGIES                                     GAM00350
C IS=NO. SOURCE ENERGIES                                         GAM00360
C IC=NO. COHERENT SCATTER ENERGIES                            GAM00370
C IG=NO. GROUP ENERGIES                                         GAM00380
C N=NO. INTEGRATION PTS. PER GROUP                         GAM00390
C IF=NO. OF INPUT FLUXES                                       GAM00400
C
C

```

SOURCE ELEMENT LIST (8BIT MODE)

```

C      NMAX=NO. OF LEGENDRE COMPONENTS REQUESTED          GAM00530
C      Z(I)=ATOMIC NUMBERS                         GAM00540
C      ICAL 0/1 =INPUT X-SEC / COMPUTE X-SEC AND COHERENT X-SEC GAM00550
C      IPRT0 0/1 =NO EFFECT / PRINT DETAIL ABS AND COHERENT X-SEC GAM00560
C      IPRT1 0/1 =NO EFFECT / PRINT DETAIL HEAT COEFF.        GAM00570
C
C      INPUT                                         GAM00580
C
C      NIN=5                                         GAM00590
READ(NIN,501)IG,N,NMAX,KON,ICAL,IPRT0,IPRT1,NACT           GAM00600
WRITE( 6,503)IG,N,NMAX,KON,ICAL,IPRT0,IPRT1,NACT           GAM00610
IF(KON.GE.0)GOTO2                                     GAM00620
READ(NIN,501)IF                                         GAM00630
READ(NIN,502)(EFLUX(I),I=1,IF)                         GAM00640
READ(NIN,502)(FLUX(I),I=1,IF)                          GAM00650
WRITE( 6,504)(I,EFLUX(I),FLUX(I),I=1,IF)               GAM00660
2 READ(NIN,501)IS                                     GAM00670
READ(NIN,502)(ES(I),I=1,IS)                           GAM00680
READ(NIN,502)( S(I),I=1,IS)                           GAM00690
READ(NIN,502)(GE(I),I=1,IG)                           GAM00700
WRITE( 6,505)(I,ES(I),S(I),I=1,IS)                   GAM00710
WRITE( 6,506)(I,GE(I),I=1,IG)                        GAM00720
501 FORMAT(14I5)                                     GAM00730
502 FORMAT(6E12.5)                                    GAM00740
503 FORMAT('1 INPUT DATA' /)                         GAM00750
1     '0   IG   NO. OF GROUPS             ',15,          GAM00760
2     '  N   NO. OF INTEGRATION POINTS/GROUP   ',15/        GAM00770
3     '  NMAX NO. OF LEGENDRE COMPONENTS    ',15,          GAM00780
4     '  KON  CONTROL -1/0/1 = FLUX/NONE/SOURCE  ',15/        GAM00790
5     '  ICAL 0/1 = X-SEC INPUT/CALCULATE    ',15,          GAM00800
6     '  IPRT0 0/1 = PRINT DETAIL X-SEC NO/YES   ',15/        GAM00810
7     '  IPRT1 0/1 = PRINT DETAIL HEAT COEFF NO/YES ',15,        GAM00820
8     '  NACT 0/1 = OUTPUT HEAT COEFF NO/YES    ',15,        GAM00830
504 FORMAT(10H0      ,14H ENERGY (MEV) ,11H INPUT FLUX,/,(3X,15.2X,GAM00840
12(E12.5,2X)))                                         GAM00850
505 FORMAT(10H0      ,14H ENERGY (MEV) ,7H SOURCE,/,(3X,15.2X,2(E12GAM00860
1.5)))                                                 GAM00870
506 FORMAT(10H0      ,20H GROUP ENERGY BOUNDS,/,(3X,15.2X,E12.5)) GAM00880
C
C      CONTROL INTEGERS                               GAM00890
IGA=IG=1                                         GAM00900
IM=N+1                                         GAM00910
IMA=N*2                                         GAM00920
IGB=IG*2+NACT                                GAM00930
IGD=IG=2                                         GAM00940
FN=N                                           GAM00950
J1=0                                           GAM00960
C
C      EXPRESS ENERGIES IN REST MASS UNITS          GAM00970
ERM=1./.51099                                     GAM00980
ERMIN=0.51099                                     GAM00990
DO5I=1,IG                                         GAM01000
5 EG(I)=ERM*GE(I)                                 GAM01010
DO6I=1,IS                                         GAM01020
                                         GAM01030
                                         GAM01040
                                         GAM01050
                                         GAM01060

```

SOURCE ELEMENT LIST (8BIT MODE)

```

6 ES(I)=ERM*ES(I)
  IF(KON.GE.0)GOTO9
  DO8I=1,IF
  8 EFLUX(I)=ERM*EFLUX(I)
C   INITIALIZE FLUX AND AVERAGE FLUX, SOURCE, AND SCATTERING CROSS
C SECTION
  9 NNN=1
  DO 18 K=1,IGA
  H=(EG(K)-EG(K+1))/FN
  ASIG=0.
  AFLU=0.
  ASOU=0.
  DO17I=1,IM
  AA=FLOAT(I-1)*H+EG(K+1)
  FFFI1=I-1
  C  AA=EG(K+1)*(FN-FFF11)/FN+EG(K)*FFF11/FN
  AA=EG(K)*(FN-FFF11)/FN+EG(K+1)*FFF11/FN
  AB=AA
  IF(KON)10,11,12
  10 CALLAL(AB,FLUX,EFLUX,IF)
  GOTO13
  11 AB=1.0
  GOTO13
  12 CALLAL(AB,S,ES,IS)
  13 IF(I.EQ.1)GOTO15
  IF(I.NE.IM)GOTO16
  15 AB=AB*.5
  16 FLUXS(K+1)=AB
  AFLU=AFLU+AB
  ASIG=ASIG+AB*SIGMAS(AA)
  CALLAL(AA,S,ES,IS)
  17 ASOU=ASOU+AB*AA
  FG(K)=AFLU
  SIGS(K)=ASIG/FG(K)
  18 SG(K)=ASOU/FG(K)
  WRITE(6,181)(K,FG(K),SIGS(K),SG(K),K=1,IGA)
  181 FORMAT(6H0GROUP,14H AVG FLUX ,14H AVG SIGMA S ,
  112H AVG SOURCE,//,(14.2X,3(E12.5,2X)))
C   CALCULATE LEGENDRE MOMENTS - FOR EACH ELEMENT
  DO 37 M=1,NMAX
  DO37K=1,IGA
  DIF=0.
  C  HA=(EG(K)-EG(K+1))/FN
  DO27L=K,IGA
  AIN=0.
  DO25I=1,IM
  AX=EG(K)-FLOAT(I-1)*HA
  FFFI1=I-1
  C  AX=EG(K)*(FN-FFF11)/FN+EG(K+1)*FFF11/FN
  AX=EG(K+1)*(FN-FFF11)/FN+EG(K)*FFF11/FN
  @=AX/(1.+2.*AX)
  BU=AMIN1(AX,EG(L))

```

SOURCE ELEMENT LIST (8BIT MODE)

```

      BL=AMAX1(Q,EG(L+1))
      IF(L.EQ.1)BL=Q
      QQ=0.0
C      IF(BL.LT.BU) QQ=FLUXS(K,I)*SIGLEG(M,AX,BU,BL)
25 AIN=AIN+QQ
      TRANS(K,L,M)=AIN/FG(K)
      IF(M.EQ.1) DIF=DIF-TRANS(K,L,M)
27 CONTINUE
      IF(M.NE.1) GO TO 37
      DIFF=SIGS(K)+DIF
      WRITE(6,507)K,DIFF
507 FORMAT(4H0D DIFFERENCE=GROUP AVG SCATTER CROSS SECTION,
14H AND SUM OF GROUP AVERAGED TRANSFERS. GROUP.
212.6H , IS=1PE12.5)
      DF(K)=DIF
37 CONTINUE
C      ELEMENT DEPENDENT PORTION
C      READ(NIN,501) IZ
      READ(NIN,502) (Z(I),I=1,IZ)
      DO 2000 MZ=1,IZ
      ZA=Z(MZ)*0.249375
      WRITE(6,515) Z(MZ)
515 FORMAT('1'//20X,'*** GAMMA-RAY CROSS SECTIONS FOR ATOMIC NUMBER
1=F4.0,' ***')
      DO 2000 M=1,NMAX
      DO 20 I=1,IGA
      DO 19 J=1,IGB
19 SIGMAT(J,I)=0.0
      SIGTOT(I)=0.0
      GXX(I)=0.0
20 ASG(I)=0.0
101 IF(M.GT.1)GOTO3000
1000 IF(ICAL.EQ.0) GO TO 2010
      Z3=Z(MZ)
C      CALL CROSS(Z3,IA,IC,EA,SIGA,ECOH,SIGCOH)
      CALL CROSS(Z3,IA,IC,EA,SIGA,ECOH,SIGCOH,ENNU,DF,ZA)
      GO TO 3002
2010 CONTINUE
      READ(NIN,501)IA,IC
      READ(NIN,502)(SIGA(I),I=1,IA)
      READ(NIN,502)(EA(I),I=1,IA)
      IF(IC.EQ.0)GOTO31
      READ(NIN,502)(SIGCOH(I),I=1,IC)
      READ(NIN,502)(ECOH(I),I=1,IC)
      WRITE(6,508)'I',ECOH(I),SIGCOH(I),I=1,IC)
508 FORMAT(10H0           ,14H ENERGY (MEV) ,17H COHERENT SCATTER./,(3X,GAM02090
115.2X,2E14.7))
      DO301=1,IC
30 ECOH(I)=ECOH(I)*ERM
31 WRITE(6,509)'I',EA(I),SIGA(I),I=1,IA)
509 FORMAT(10H0           ,14H ENERGY (MEV) ,11H ABSORPTION./,(3X,15.2X,GAM02140

```

SOURCE ELEMENT LIST (8BIT MODE)

```

12(E12.5,2X)) GAM02150
DO32I=1,IA GAM02160
32 EA(I)=EA(I)*ERM GAM02170
3002 CONTINUE GAM02180
NNN=1 GAM02190
DO35J=1,IGA GAM02200
C H=(EG(J)-EG(J+1))/FN GAM02210
AABS=0. GAM02220
ACOH=0. GAM02230
ANU=0. GAM02240
DO34I=1,IM GAM02250
IF(ICAL.NE.0) GO TO 33 GAM02260
C AX=FLOAT(I-1)*H+EG(J+1) GAM02270
FFFI1=I-1 GAM02280
C AX=EG(J+1)*(FN-FFFI1)/FN+EG(J)*FFFI1/FN GAM02290
AX=EG(J)*(FN-FFFI1)/FN+EG(J+1)*FFFI1/FN GAM02300
AB=AX GAM02310
AC=AX GAM02320
CALLAL(AB,SIGA,EA,IA) GAM02330
AABS=AABS+FLUXS(J,I)*AB GAM02340
IF(IC.EQ.0) GOT034 GAM02350
CALLAL(AX,SIGCOH,ECOH,IC) GAM02360
ACOH=ACOH+FLUXS(J,I)*AX GAM02370
GO TO 34 GAM02380
33 AABS=AABS+FLUXS(J,I)*SIGA(NNN) GAM02390
ACOH=ACOH+FLUXS(J,I)*SIGCOH(NNN) GAM02400
ANU=ANU+FLUXS(J,I)*ENN(NNN) GAM02410
NNN=NNN+1 GAM02420
34 CONTINUE GAM02430
ASG(J)=AABS/FG(J) GAM02440
IF(ICAL.NE.0) GXX(J)=ANU/FG(J) GAM02450
35 SIGC(J)=ACOH/FG(J) GAM02460
IF(ICAL.EQ.0) GO TO 103 GAM02470
WRITE(6,2900) (I,ASG(I),SIGC(I),GXX(I),I=1,IGA) GAM02480
2900 FORMAT('0 GROUP ABSORB COHERENT HEAT',HEAT',,
           *      /' X-SEC. X-SEC. COEFF',,
           *      /(1X,I3,3X,3E13.5)) GAM02490
           *      /' GAM02500
           *      /' GAM02510
103 CONTINUE GAM02520
DO 102 K=1,IGA GAM02530
SIGTOT(K)=ASG(K)-DF(K)*ZA+SIGC(K) GAM02540
102 CONTINUE GAM02550
C FORM CROSS SECTION TABLE GAM02560
3000 DO38J=1,IGA GAM02570
IF(NACT.EQ.1) SIGMAT(1,J)=GXX(J) GAM02580
SIGMAT(NACT+1,J)=ASG(J) GAM02590
SIGMAT(NACT+2,J)=0.0 GAM02600
38 SIGMAT(NACT+3,J)=SIGTOT(J) GAM02610
LLL=M=1 GAM02620
PC =2*LLL+1 GAM02630
DO39I=1,IGA GAM02640
IAB=I+3+NACT GAM02650
DO39J=1,IGA GAM02660
JA=J-I+1 GAM02670
                               GAM02680

```

SOURCE ELEMENT LIST (8BIT MODE)

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39 SIGMAT(IAB,J)=PC*TRANS(JA+J+M)*ZA          GAM02690
IF(M.GT.1) GO TO 43                           GAM02700
DO 42 J=1,IGA                                  GAM02710
42 SIGMAT(NACT+4,J)=SIGMAT(NACT+4,J)+SIGC(J)  GAM02720
43 CONTINUE                                     GAM02730
GAM02740
C PRINT AND PUNCH CROSS SECTION TABLE          GAM02750
NAB=M-1                                         GAM02760
WRITE(6,510)NAB,Z(MZ)                         GAM02770
510 FORMAT(2H0P,I2,20H CROSS SECTION TABLE,     GAM02780
115H ATOMIC NUMBER= E11.3,40X)                 GAM02790
MA=1                                           GAM02800
MB=8                                           GAM02810
40 MC=MINO(MB,IGA)                            GAM02820
WRITE(6,511)(J,J=MA,MC)                      GAM02830
WRITE(6,513)                                     GAM02840
DO41=1,IGB                                     GAM02850
41 WRITE(6,512)I,(SIGMAT(I,J),J=MA,MC)        GAM02860
MA=MA+8                                       GAM02870
MB=MB+8                                       GAM02880
IF(MA.LE.IGA)GOTO40                           GAM02890
511 FORMAT(7HO      ,8(8H GROUP=I2+3X))       GAM02900
512 FORMAT(14,3X, 8E13.6)                      GAM02910
513 FORMAT(1H0)                                 GAM02920
NPUN=7                                         GAM02930
DO 514 J=1,IGA                                GAM02940
514 CALL PUNSH(SIGMAT(1,J),IGB,NPUN)           GAM02950
GAM02960
C 2000 CONTINUE                                 GAM02970
STOP                                           GAM02980
END                                            GAM02990
SUBROUTINE CROSS(Z,NMAX,MMAX,EA,SIGA,ECOH,SIGCOH,ENNU,DF,ZA) GAM03010
DIMENSION EA(1),SIGA(1),ECOH(1),SIGCOH(1),SPOT( 500),SPAR( 500), GAM03020
1      EE( 500),ENNU(1)+DF(1)                  GAM03030
COMMON /JDB/IGA,IM,FN,ICAL,IPRT0,IPRT1,J1,GE( 51)  GAM03040
GAM03050
C REM=1.0/0.51099                             GAM03060
NMAX=IGA*IM                                   GAM03070
MMAX=IGA*IM                                   GAM03080
DO 5 I=1,500                                    GAM03090
SIGA(I)=0.0                                     GAM03100
SPOT(I)=0.0                                     GAM03110
SPAR(I)=0.0                                     GAM03120
SIGCOH(I)=0.0                                   GAM03130
ENNU(I)=0.0                                     GAM03140
5 CONTINUE                                     GAM03150
IF(J1 .NE. 0) GO TO 20                           GAM03160
N=1                                           GAM03170
DO 10 K=1,IGA                                  GAM03180
DO 10 I=1,IM                                   GAM03190
FFF|I=1-1                                     GAM03200
GAM03210
GAM03220

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SOURCE ELEMENT LIST (8BIT MODE)

```

EE(N)=GE(K)*(FN-FFFF1)/FN+GE(K+1)*FFFF1/FN          GAM03230
EA(N)=EE(N)*REM                                     GAM03240
ECOH(N)=EA(N)                                       GAM03250
N=N+1                                              GAM03260
10 CONTINUE                                         GAM03270
20 CONTINUE                                         GAM03280
CALL POTO(Z,NMAX,EE,SPOT)                           GAM03290
CALL PAIR(Z,NMAX,EE,SPAR)                           GAM03300
DO 30 I=1,NMAX                                     GAM03310
SIGA(I)=SPOT(I)+SPAR(I)
30 CONTINUE                                         GAM03320
80 FORMAT('1'//'*0*** ATOMIC NO. ',F8.3,' ***'
     1   '/*0*.25X,'--- ABSORPTION CROSS SECTION ---',15X,'--- COHEREN' GAM03350
     2 T SCATTERING CROSS SECTION ---'/*0*,12X, 'ENERGY      PHOTO C  GAM03360
     3 PAIR C  TOTAL C')
     CALL COHER(Z,MMAX,EE,SIGCOH)                     GAM03380
     IF(IPR0.EQ.0) GO TO 60
     WRITE(6,80) Z
     DO 50 K=1,1GA
     NNN=(K-1)*IM
     WRITE(6,100) K
     WRITE(6,110) (EE(NNN+I),SPOT(NNN+I),SPAR(NNN+I),SIGA(NNN+I),
     1           SIGCOH(NNN+I),I=1,IM-1)
50 CONTINUE                                         GAM03450
100 FORMAT(' GROUP',I3)                            GAM03460
110 FORMAT(' 10X,E12.5,2X,3E12.4,25X,E12.4)        GAM03470
60 CONTINUE                                         GAM03480
J1=1
C
CALL NRWZ(Z,NMAX,EE,SPOT,      SPAR,ENNU,DF,ZA)    GAM03520
RETURN                                             GAM03530
END
SUBROUTINE POTO(Z,NMAX,EA,SPOT)                      GAM03540
PHOTO ELECTRIC TOTAL CROSS SECTION                 GAM03550
CBS-29                                           GAM03560
C
*****                                           GAM03570
DIMENSION SPOT(500),EA(500),A(4,4)                GAM03580
A(1,1)=1.6268E-09                                GAM03590
A(1,2)=-2.683E-12                                GAM03600
A(1,3)=4.173E-02                                GAM03610
A(1,4)=1.
A(2,1)=1.5274E-09                                GAM03620
A(2,2)=-5.110E-13                                GAM03630
A(2,3)=1.027E-02                                GAM03640
A(2,4)=2.
A(3,1)=1.1330E-09                                GAM03650
A(3,2)=-2.177E-12                                GAM03660
A(3,3)=2.013E-02                                GAM03670
A(3,4)=3.5
A(4,1)=-9.12E-11                                GAM03680
A(4,2)=0.
A(4,3)=0.
A(4,4)=4.                                         GAM03690
GAM03700
GAM03710
GAM03720
GAM03730
GAM03740
GAM03750
GAM03760

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SOURCE ELEMENT LIST (8BIT MODE)

```

AN=6.023E-23          GAM03770
EO=(Z-0.3)**2*1.352E-5 GAM03780
DO 50 K=1,NMAX         GAM03790
NNMAX=K                GAM03800
E=EA(K)                GAM03810
ZE=0.01*EXP(0.0312*(Z-8.0)) GAM03820
IF(Z.LE.8.) ZE=0.0      GAM03830
IF(E .LE. EO) GO TO 150 GAM03840
IF(E .LE. ZE) GO TO 150 GAM03850
TAUK1=0.0              GAM03860
DO 20 I=1,4             GAM03870
20 TAUK1=TAUK1+((A(I,1)+A(I,2)*Z)/(1.+A(I,3)*Z))*E**(-A(I,4)) GAM03880
TAUK=Z**5*TAUK1        GAM03890
TAUP=TAUK*(1.+0.01481*( ALOG(Z))**2-0.000788*( ALOG(Z))**3) GAM03900
IF(Z.GT.1.1) GO TO 30  GAM03910
C  CORRECTION FOR HYDROGEN GAM03920
EX=ALOG10(E)           GAM03930
FACT=-0.2325*EX*EX + 0.2478*EX + 2.096 GAM03940
TAUP=TAUP/FACT         GAM03950
30 CONTINUE              GAM03960
SPOT(K)=TAUP            GAM03970
50 CONTINUE              GAM03980
GO TO 200               GAM03990
150 CALL POTO3(Z,NNMAX,NMAX,EA,SPOT,EO) GAM04000
200 CONTINUE              GAM04010
RETURN                  GAM04020
END                     GAM04030
SUBROUTINE POTO3(Z,NNMAX,NMAX,EA,SPOT,EO) GAM04040
DIMENSION EA(500),SPOT(500) GAM04050
DATA PHI/3.1415927/,RY/1.352E-5/,FAI/6.6537E-25/ GAM04060
DATA C2M/0.51084/          GAM04070
C
A=1.5*FAI*Z**5*1.0E+24/(137.0**4) GAM04080
DO 10 K=NNMAX,NMAX          GAM04090
NN=K                      GAM04100
E=EA(K)                   GAM04110
HNU=E                      GAM04120
IF(E .LE. EO) GO TO 100    GAM04130
IF(Z.GE.92.0 .AND. E.LE.0.08) GO TO 100 GAM04140
B=(C2M/HNU)**5             GAM04150
G=HNU/ C2M+1.0              GAM04160
X=SQRT(EO/(HNU-EO))       GAM04170
Y=1.0/X                   GAM04180
F=2.0*PHI*SQRT(EO/HNU)*(EXP(-4.0*X*ATAN(Y))) GAM04190
1  /(1.0-EXP(-2.0*PHI*X)) GAM04200
C=(G**2-1.0)**1.5          GAM04210
D=G*(G-2.0)/(G+1.0)        GAM04220
R=1.0/(2.0*G*SQRT(G*G-1)) GAM04230
S=(G+SQRT(G*G-1.0))/(G-SQRT(G*G-1.0)) GAM04240
S=ALOG(S)                  GAM04250
SPOT(K)=A*B*C*(4.0/3.0+D*(1.0-R*S))*F GAM04260
10 CONTINUE                 GAM04270
GO TO 200                  GAM04280
C                           GAM04290
                                GAM04300

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SOURCE ELEMENT LIST (8BIT MODE)

```

100 CALLPO6MV1(Z,NN,NMAX,EA,SPOT) GAM04310
200 CONTINUE GAM04320
      RETURN GAM04330
      END GAM04340
      SUBROUTINE PO6MV1(Z,NNMAX,NMAX,EA,SPOT) GAM04350
      DIMENSION EA(500),SPOT(500) GAM04360
      CALL FUNC1(Z,A) GAM04370
      A=A*1.0E+24 GAM04380
C      GAM04390
      DO 10 K=NNMAX,NMAX GAM04400
      E=EA(K) GAM04410
      HNU=E GAM04420
      CALL FUNC2(Z,HNU,4,1.0,3.0,W1) GAM04430
      CALL FUNC2(Z,HNU,5,3.0,8.0,W2) GAM04440
      SPOT(K)=A*(W1+W2) GAM04450
10  CONTINUE GAM04460
      RETURN GAM04470
      END GAM04480
      SUBROUTINE FUNC1(Z,A) GAM04490
      PAI=3.1415927 GAM04500
      C=(2.0**12)*PAI*6.6537E-25*(137.0**3) GAM04510
      V=(Z-4.15)**2 GAM04520
      A=C/V GAM04530
      RETURN GAM04540
      END GAM04550
      SUBROUTINE FUNC2(Z,HNU,KK,C1,C2,W) GAM04560
      DATA PAI/3.1415927/.C/0.338E-5/ GAM04570
      HNU2=C*(Z-4.15)**2 GAM04580
      B0=HNU2/HNU GAM04590
      TEMP=1-B0 GAM04600
      IF(TEMP.LE.0.0) GO TO 100 GAM04610
      B1=B0**KK GAM04620
      B2=C1*C2*B0 GAM04630
      X2=(B0/(1-B0))**0.5 GAM04640
      F1=-8.0*X2*ATAN2(1.0,X2) GAM04650
      F2=-4.0*PAI*X2 GAM04660
      F=EXP(F1)/(1-EXP(F2)) GAM04670
      W=B1*B2*F GAM04680
100 CONTINUE GAM04690
      RETURN GAM04700
      END GAM04710
      SUBROUTINE NEPAIR(Z,NMAX,EA,SPAR) GAM04720
      *** TOTAL PAIR CREATION CROSS SECTION *** GAM04730
C      PAIR CREATION CROSS SECTION GAM04740
C      NBS-29 GAM04750
C      GAM04760
C      GAM04770
C      GAM04780
C      * NEGLECT SCREING CORRECTION --- SHFS GAM04790
C      DBM ----- COULOMB CORRECTION GAM04800
C      DRA ----- RADIATIVE CORRECTION GAM04810
C      DEP ----- EMPIRICAL MULTIPLIER FOR COULOMB CORRECTION GAM04820
      DIMENSION EA(500),SPAR(500) GAM04830
      RE=7.9398E-26 GAM04840

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SOURCE ELEMENT LIST (8BIT MODE)

```

TETA=1.2020569          GAM04850
C=2.997925E+10          GAM04860
ERME=0.511006             GAM04870
EC2=0.511006*2.0          GAM04880
DO 100 I=1,NMAX          GAM04890
E=EA(I)                  GAM04900
IF(E-EC2) 90,90,55        GAM04910
55 CONTINUE                GAM04920
EK=E/0.511006             GAM04930
IF(E-2.0) 20,30,30        GAM04940
20 ROW=(2.*EK-4.)/(2.+EK+2.*SQRT(2.*EK))      GAM04950
SIG=Z**2*RE*2.*3.14159*(EK-2.0)**3*(1.+ROW/2.+23.*ROW**2/40.  GAM04960
1+11.*ROW**3/60.+29.*ROW**4/960.)/(137.*3.*EK**3)      GAM04970
GO TO 35                  GAM04980
30 SIG=(Z**2*RE/137.)*(28.* ALOG(2.*EK)/9.-218./27.+2./EK)**2*(6.* GAM04990
1 ALOG(2.*EK)-7./2.+2.* ALOG(2.*EK)**3/3.-ALOG(2.*EK)**2-3.14159**2 GAM05000
2.* ALOG(2.*EK)/3.+2.*TETA*3.14159**2/6.)-(2./EK)**4*(3.* ALOG(2.*EK) GAM05010
3/16.+1./8.)-(2./EK)**6*(29./9.256* ALOG(2.*EK)-77./27.512))      GAM05020
35 SA=Z/137.                GAM05030
FZ=SA**2*(1./(1.+SA**2)+0.20206-0.0369*SA**2+0.0083*SA**4-0.002*SAGAM05040
1***)
DBM=28.*Z**2*RE*FZ/(9.*137.)          GAM05050
DRA=1.012                  GAM05060
IF(E-1.5) 1,1,2              GAM05070
1 DEP=-0.0677*(E-1.02)/0.48      GAM05080
GO TO 444                  GAM05090
2 IF(E-2.) 3,3,4              GAM05100
3 DEP=-0.0677-0.0609*(E-1.5)/0.5      GAM05110
GO TO 444                  GAM05120
4 IF(E-3.) 5,5,6              GAM05130
5 DEP=-0.1286-0.007*(E-2.)/1.0      GAM05140
GO TO 444                  GAM05150
6 DEP=0.0922*E-0.4326      GAM05160
444 SIG=SIG*DRA-DEP*DBM      GAM05170
GO TO 10                  GAM05180
90 SIG=0.0                  GAM05190
10 CONTINUE                 GAM05200
SPAR(I)=SIG*1.0E+24          GAM05210
100 CONTINUE                 GAM05220
RETURN                      GAM05230
END                         GAM05240
SUBROUTINE COHER(Z,MMAX,ECOH,SIGCOH)      GAM05250
C COHERENT SCATTERING TOTAL CROSS SECTION      GAM05260
C *** USE A APPROXIMATE CURVE. THIS CURVE WAS CALCULATED BY LEAST      GAM05270
C SQUARES METHOD USING LOS ALAMOS DATA.          GAM05280
C *** UNIT = BARN/ATOM                      GAM05290
C Z = ATOMIC NUMBER                      GAM05300
C E = PHOTON ENERGY (MEV)                  GAM05310
C *** DIMENSION ECOH(500)*SIGCOH(500)      GAM05320
C ALP= 2.357*(ALOG(Z/26.0))+9.436          GAM05330
C DO 100 I=1,MMAX                      GAM05340
C XXXX=ALOG(ECOH(I))                  GAM05350
C                                     GAM05360
C                                     GAM05370
C                                     GAM05380

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SOURCE ELEMENT LIST (8BIT MODE)

```

YYYY=-0.09615*(XXXX+11.532)**2+ALP          GAM05390
SIGCOH(I)=EXP(YYYY)                          GAM05400
100 CONTINUE                                GAM05410
      RETURN                                  GAM05420
      END                                     GAM05430
      SUBROUTINE AL(X,Y,XA,J)                  GAM05440
C       LINEARLY INTERPOLATES FUNCTION Y TO GIVE VALUE AT X
      DIMENSION Y(J),XA(J)                    GAM05450
      !=1                                     GAM05460
      100 A=X-XA(I)+.000001                 GAM05470
          IF(A>1.6.5                         GAM05480
          1 I=I+1                           GAM05490
          IF(I.LE.J)GOTO100                   GAM05500
          WRITE(6,4) I,J,X,XA(I),A           GAM05510
          4 FORMAT(36H0ERROR-ENERGY LESS THAN ALL ENERGIES/10X,2I5,3E12.4)
          CALLEXIT                            GAM05520
          5 N=I
          IF(N.LE.1)GOTO6                     GAM05530
          M=N-1                               GAM05540
          X=Y(N)+(X-XA(N))*(Y(M)-Y(N))/(XA(M)-XA(N))   GAM05550
          RETURN                                GAM05560
          6 X=Y(I)
          RETURN                                GAM05600
          END                                     GAM05610
          FUNCTION SIGMAS(E)                  GAM05620
C       KLEIN-NISHINA SCATTERING CROSS SECTION
          A=1.+2.*E                          GAM05640
          B=E*E                             GAM05650
          C=E-2.-2./E                      GAM05660
          SIGMAS=(ALOG(A)*C+4.+2.*B*(1.+E)/(A*A))/B   GAM05670
          RETURN                                GAM05680
          END                                     GAM05690
          FUNCTION SIGLEG(N,Y,XU,XL)          GAM05700
C-----
C   N : LEGENDRE ORDER                      GAM05710
C   Y : SOURCE ENERGY                        GAM05720
C   XU: UPPER SINK ENERGY                   GAM05730
C   XL: LOWER SINK ENERGY                  GAM05740
C-----                                     GAM05750
C-----                                     GAM05760
C-----                                     GAM05770
C-----                                     GAM05780
C   CONVERT SINK ENERGY TO SCATTERING ANGLE
          AU=1.0+1.0/Y-1.0/XU                GAM05790
          AL=1.0+1.0/Y-1.0/XL                GAM05800
C   DETERMINE NUMBER OF INTEGRAL POINTS K
          DELTMU=0.02                         GAM05810
          IF(N.LE.5) DELTMU=0.04              GAM05820
          K=(AU-AL)/DELMU                     GAM05830
          IF(K.LT.5) K=5                     GAM05840
C   CALL SIMPSON'S INTEGRAL ROUTINE
          CALL SIGINT(SIG,N,Y,AU,AL,K)        GAM05850
C   SIGLEG=SIG
          RETURN                                GAM05860
C-----                                     GAM05870
C-----                                     GAM05880
C-----                                     GAM05890
C-----                                     GAM05900
C-----                                     GAM05910
C-----                                     GAM05920

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SOURCE ELEMENT LIST (8BIT MODE)

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      END                                     GAM05930
      SUBROUTINE SIGINT(SIG,N,Z,AU,AL,K)    GAM05940
      REAL*8 X,Y,SIGMA ,PN                  GAM05950
      DIMENSION PN(1000)                   GAM05960
C
      SIGMA(X,Y)=(1.+Y*(1.-X)+1./(1.+Y*(1.-X))+2.*((X-1.)*(X-1.)*(X-1.))/GAM05980
      * (1.+Y*(1.-X))**2                  GAM05990
C
      Y=Z                                     GAM06000
C
      DETERMINE DELTH                         GAM06010
      DELTH=(AU-AL)/(2*K)
C
      CALCULATE PN(X) FOR EACH INTEGRAL POINTS
      IE=2*K+1
      GO TO (100,110,120,130,140,150,160,170,180),N
C
      100 DO 200 I=1,IE
      PN(I)=1.                                GAM06090
      200 CONTINUE
      GO TO 250                                GAM06100
C
      110 DO 210 I=1,IE
      X=AL+DELTH*(I-1)
      PN(I)=X
      210 CONTINUE
      GO TO 250                                GAM06110
C
      120 DO 220 I=1,IE
      X=AL+DELTH*(I-1)
      PN(I)=(3.*X*X-1.)/2.
      220 CONTINUE
      GO TO 250                                GAM06120
C
      130 DO 230 I=1,IE
      X=AL+DELTH*(I-1)
      PN(I)=(5.*X*X-3.)*X/2.
      230 CONTINUE
      GO TO 250                                GAM06130
C
      140 DO 240 I=1,IE
      X=AL+DELTH*(I-1)
      PN(I)=((35.*X*X-30.)*X*X+3.)/8.
      240 CONTINUE
      GO TO 250                                GAM06140
C
      150 DO 255 I=1,IE
      X=AL+DELTH*(I-1)
      PN(I)=((63.*X*X-70.)*X*X+15)*X/8.
      255 CONTINUE
      GO TO 250                                GAM06150
C
      160 DO 260 I=1,IE
      X=AL+DELTH*(I-1)
      PN(I)=((231.*X*X-315.)*X*X+105.)*X*X-5.)/16.
      260 CONTINUE

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SOURCE ELEMENT LIST (8BIT MODE)

```

260 CONTINUE                                GAM06470
GO TO 250                                  GAM06480
C                                         GAM06490
170 DO 270 I=1,IE                           GAM06500
X=AL+DELTH*(I-1)                          GAM06510
PN(I)=(((429.*X*X-693.)*X*X+315.)*X*X-35.)*X/16.  GAM06520
270 CONTINUE                                GAM06530
GO TO 250                                  GAM06540
C                                         GAM06550
180 DO 280 I=1,IE                           GAM06560
X=AL+DELTH*(I-1)                          GAM06570
PN(I)=(((6435.*X*X-12012.)*X*X+6930.)*X*X-1260.)*X*X+35.)/128.  GAM06580
280 CONTINUE                                GAM06590
C                                         GAM06600
250 CONTINUE                                GAM06610
C                                         GAM06620
SUMEND=0.                                    GAM06630
SUMEID=0.                                    GAM06640
DO 300 I=1,K                               GAM06650
X=AL+2.*DELTH*(I-1)                      GAM06660
SUMEND=SUMEND+SIGMA(X,Y)*PN(2*I-1)        GAM06670
SUMEID=SUMEID+SIGMA((X+DELTH),Y)*PN(2*I)  GAM06680
300 CONTINUE                                GAM06690
C                                         GAM06700
SIG=DELTH/3.*((2.*SUMEND+4.*SUMEID-SIGMA(AL,Y)*PN(1)+SIGMA(AU,Y)*
1 PN(2*K+1))                                GAM06710
RETURN                                     GAM06720
END                                         GAM06730
SUBROUTINE NROW(Z,NMAX,EE,TAUP,      PAIR,ENNU,DF,ZA)  GAM06740
GAM06750
GAM06760
C                                         THIS IS USED TO CALCULATE GAMMA-RAY ENERGY
C                                         TRANSFER (ABSORPTION) COEFFICIENT  GAM06770
C                                         GAM06780
C                                         GAM06790
C                                         DIMENSION ZTBL(15),ENNU(500)          GAM06800
DIMENSION TZK(10),TFK(10),TZL(10),TFL(10),TZE(5),TEK(5),TEL(5)  GAM06810
COMMON /JDB/IGA,IM,FN,ICAL,IPRTO,IPRT1,J1,GE( 51)  GAM06820
C                                         TZK -- ATOMIC NO. FOR K-SHELL FLUORESCENCE YIELD  GAM06830
DATA TZK/ 7.0, 10.0, 15.0, 20.0, 30.0, 40.0, 50.0, 60.0, 80.0,  GAM06840
*          100.0 /                                GAM06850
C                                         TFK -- FLUORESCENCE YIELD OF K-SHELL  GAM06860
DATA TFK/ 0.001, 0.010, 0.051, 0.151, 0.435, 0.711, 0.843,  GAM06870
*          0.909, 0.953, 0.965 /                  GAM06880
C                                         TZL -- ATOMIC NO. FOR L-SHELL FLUORESCENCE YIELD  GAM06890
DATA TZL/ 31.0, 35.0, 40.0, 50.0, 60.0, 73.0, 74.0, 80.0, 90.0,  GAM06900
*          100.0 /                                GAM06910
C                                         TFL -- FLUORESCENCE YIELD OF L-SHELL  GAM06920
DATA TFL/ 0.010, 0.032, 0.060, 0.118, 0.173, 0.248, 0.293,  GAM06930
*          0.382, 0.444, 0.467 /                  GAM06940
C                                         TZE -- ATOMIC NO. FOR FLUORESCENCE ENERGY  GAM06950
DATA TZE/ 3.0, 10.0, 20.0, 50.0, 100.0 /             GAM06960
C                                         TEK -- FLUORESCENCE ENERGY OF K-SHELL  GAM06970
DATA TEK/ 0.054, 0.849, 3.719, 25.843, 124.054 /    GAM06980
C                                         TEL -- FLUORESCENCE ENERGY OF L-SHELL  GAM06990
TEL -- FLUORESCENCE ENERGY OF L-SHELL  GAM07000

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SOURCE ELEMENT LIST (8BIT MODE)

```

      DATA TEL/ 0.0, 0.018, 0.385, 3.609, 19.141 /          GAM07010
      DATA ZTBL/1.0,6.0,7.0,8.0,11.0,12.0,13.0,15.0,16.0,18.0,   GAM07020
           1         19.0,20.0,26.0,29.0,82.0/          GAM07030
C
C
      IF(IPRT1.EQ.1) WRITE(6,1400) Z          GAM07040
1400 FORMAT('1',//0*** ATOMIC NO. ',F8.3,'***')
      1           '/0'25X,'--- MASS ENERGY TRANSFER COEFFICIENT ---'
      1           '/0'          ENERGY     F*FT    K*FK    S*FC  GAM07050
      2           TRANS COEFF'
CCCC  INTERPOLATE EACH TABLES FOR PHOTOELECTRIC ABSORPTION FACTOR  GAM07060
C           K-SHELL
      CALL INTFT(Z,AEK,TZE,TEK, 5)          GAM07070
      AEK=AEK*1.0E-3
      CALL INTFT(Z,AFK,TZK,TFK,10)          GAM07080
C           L-SHELL
      CALL INTFT(Z,AEL,TZE,TEL, 5)          GAM07090
      AEL=AEL*1.0E-3
      CALL INTFT(Z,AFL,TZL,TFL,10)          GAM07100
C           THRESHOLD ENERGY OF K-SHELL
      ECUT=(Z-0.3)**2*1.352E-5          GAM07110
      TEMP=1.0/(1.+0.01481*( ALOG(Z))**2-0.000788*( ALOG(Z))**3)
      K=0          GAM07120
      DO 1000 KK=1,1GA          GAM07130
      IF(IPRT1.EQ.1) WRITE(6,1800) KK          GAM07140
      DO 1000 JJ=1,IM          GAM07150
      K=K+1          GAM07160
      E=EE(K)          GAM07170
C***  CALCULATE FTAU (PHOTOELECTRIC ABSORPTION FACTOR)          GAM07180
C
      IF(E.LE.ECUT) GO TO 20          GAM07190
      FTAU = 1.0-TEMP*AEK*AFK/E          GAM07200
      GO TO 30
20  FTAU = 1.0-AEL*AFL/E          GAM07210
30  CONTINUE          GAM07220
C***  CALCULATE FK (PAIR PRODUCTION FACTOR)          GAM07230
C
      IF(E.LE.1.0) GO TO 180          GAM07240
      SET UP EACH SIDE OF GIVEN ATOMIC NO.
      IF(Z.LT.ZTBL(1)) GO TO 2000          GAM07250
      IF(Z.GT.ZTBL(15)) GO TO 110          GAM07260
      DO 120 I=1,15          GAM07270
      IF(Z.EQ.ZTBL(I)) GO TO 130          GAM07280
      IF(Z.LT.ZTBL(I)) GO TO 140          GAM07290
120  CONTINUE          GAM07300
140  ICO=0          GAM07310
      N1=I-1          GAM07320
      N2=I          GAM07330
      GO TO 150
130  ICO=1          GAM07340
      N1=I          GAM07350
      GO TO 150
110  ICO=2          GAM07360
      N1=14          GAM07370

```

SOURCE ELEMENT LIST (8BIT MODE)

```

N2=15                                GAM07550
150 CONTINUE                           GAM07560
C   INTERPOLATE ENERGY RANGE          GAM07570
  CALL INTFK(N1,Y1,E)                 GAM07580
  IF(ICO.EQ.1) GO TO 160              GAM07590
  CALL INTFK(N2,Y2,E)                 GAM07600
C   INTERPOLATE ATOMIC NO. RANGE     GAM07610
  FK=Y1+(Z-ZTBL(N1))*(Y2-Y1)/(ZTBL(N2)-ZTBL(N1)) GAM07620
  GO TO 170                            GAM07630
160 FK=Y1                                GAM07640
170 CONTINUE                           GAM07650
  IF(FK.GE.0.0) GO TO 190              GAM07660
180 FK=0.0                                GAM07670
C***                                     GAM07680
190 FPH=TAUP(K)*FTAU                  GAM07690
  FPA=PAIR(K)*FK                      GAM07700
  CALL COMPT(E,FC)                    GAM07710
  SFC=DF(KK)*ZA*FC                   GAM07720
C   HEAT PRODUCTION COEFF. --- KERMA FACTOR (WATT*SEC*BARN) GAM07730
  ENNU(K)=FPH+FPA+SFC                GAM07740
  IF(IPRT1.EQ.0) GO TO 1000           GAM07750
  IF(JJ.EQ.1M) GOTO 1000              GAM07760
  WRITE(6,1500) E,FPH,FPA+SFC,ENNU(K) GAM07770
1000 ENNU(K)=ENN(K)*E*1.6E-13        GAM07780
C                                         GAM07790
C                                         GAM07800
C                                         GAM07810
C                                         GAM07820
C                                         GAM07830
C                                         GAM07840
1500 FORMAT(10X,E12.4,2X,4E12.4)      GAM07850
1800 FORMAT(' GROUP',I3)               GAM07860
1700 FORMAT(10X,'***ERROR ATOMIC NO., ',F8.4) GAM07870
  END                                     GAM07880
  SUBROUTINE INTFK(N,Y,E)             GAM07890
C                                         GAM07900
C                                         GAM07910
C                                         GAM07920
C                                         GAM07930
C                                         GAM07940
C                                         GAM07950
C                                         GAM07960
C                                         GAM07970
C                                         GAM07980
C                                         GAM07990
C                                         GAM08000
C                                         GAM08010
C                                         GAM08020
C                                         GAM08030
C                                         GAM08040
C                                         GAM08050
C                                         GAM08060
C                                         GAM08070
C                                         GAM08080
C
C   THIS IS USED TO INTERPOLATE FK TABLE
C
DIMENSION FK(8,15),EG(8)                GAM08080
DATA FK/ 0.318,0.488,0.658,0.743,0.794,0.828,0.870,0.895,
1      0.318,0.487,0.655,0.738,0.787,0.820,0.858,0.879, GAM08080
2      0.318,0.489,0.654,0.737,0.786,0.818,0.855,0.876, GAM08080
3      0.317,0.486,0.654,0.736,0.785,0.816,0.853,0.873, GAM08080
4      0.317,0.485,0.652,0.733,0.780,0.811,0.846,0.863, GAM08080
5      0.317,0.485,0.651,0.732,0.779,0.810,0.843,0.861, GAM08080
6      0.317,0.487,0.653,0.734,0.780,0.809,0.842,0.857, GAM08080
7      0.316,0.484,0.649,0.729,0.775,0.804,0.836,0.851, GAM08080
8      0.316,0.484,0.648,0.728,0.774,0.803,0.834,0.848, GAM08080
9      0.316,0.483,0.647,0.726,0.771,0.799,0.829,0.842, GAM08080
A      0.316,0.483,0.646,0.725,0.770,0.798,0.827,0.839, GAM08080
B      0.316,0.482,0.645,0.724,0.769,0.796,0.824,0.836, GAM08080
C      0.317,0.484,0.646,0.722,0.763,0.788,0.811,0.819, GAM08080
D      0.314,0.480,0.640,0.715,0.757,0.781,0.804,0.808, GAM08080
E      0.312,0.471,0.616,0.675,0.701,0.712,0.712,0.700/ GAM08080

```

SOURCE ELEMENT LIST (8BIT MODE)

```

      DATA EG/1.5+2.0,3.0+4.0,5.0+6.0,8.0+10.0/
C           N --- SUBSCRIPT OF ATOMIC NO. TABLE          GAM08090
C           E --- ENERGY                                GAM08100
C           Y --- DEMANDED VALUE                         GAM08110
C
C           IF(E.LT.EG(1))    GO TO 100                  GAM08120
C           IF(E.GT.EG(8))   GO TO 110                  GAM08130
C           DO 120 I=1,8
C           IF(E.EQ.EG(I))  GO TO 130                  GAM08140
C           IF(E.LT.EG(I))  GO TO 140                  GAM08150
C
C           120 CONTINUE
C           K1=I
C           GO TO 160
C
C           140 K1=I-1
C           K2=I
C           GO TO 150
C
C           100 K1=1
C           K2=2
C           GO TO 150
C
C           110 K1=7
C           K2=8
C
C
C           150 CONTINUE
C           Y=FK(K1,N)+(E-EG(K1))*(FK(K2+N)-FK(K1,N))/(EG(K2)-EG(K1))
C           RETURN
C
C           160 Y=FK(K1,N)
C           RETURN
C           END
C           SUBROUTINE INTFT(Z,E,X,Y,N)
C
C           THIS IS USED TO INTERPOLATE FK OR EK OF FTAU TABLE          GAM08310
C
C           DIMENSION X(1),Y(1)                                     GAM08320
C
C           IF(Z.LT.X(1))  GO TO 250          GAM08330
C           IF(Z.GT.X(N))  GO TO 130          GAM08340
C           DO 100 I=1,N
C           IF(Z.EQ.X(I))  GO TO 110          GAM08350
C           IF(Z.LT.X(I))  GO TO 120          GAM08360
C
C           100 CONTINUE
C           K1=I
C           GO TO 200
C
C           120 K1=I-1
C           K2=I
C           GO TO 150
C
C           130 K1=N-1
C           K2=N
C
C           INTERPOLATE LOG(Y) LINER IN LOG(X)          GAM08370
C
C           150 IF(Y(K1).EQ.0.0) GO TO 250          GAM08380
C           E=Y(K1)*EXP(ALOG(Z/X(K1))*ALOG(Y(K2)/Y(K1))/ALOG(X(K2)/X(K1)))
C           RETURN
C
C           200 E=Y(K1)
C           RETURN

```

SOURCE ELEMENT LIST (8BIT MODE)

```

250 E=0.0          GAM08630
      RETURN        GAM08640
      END          GAM08650
      SUBROUTINE COMPT(E,FC) GAM08660
C
C      THIS IS USED TO CALCULATE COMPTON SCATTERING COEFF. GAM08670
C
COMMON /JDB/IGA,IM,FN,ICAL,IPRT0,IPRT1,J1,GE( 51) GAM08700
      REAL MC2        GAM08710
C
MC2=0.510976        GAM08720
NM=E*FN            GAM08730
IF(NM.LT.10) NM=10  GAM08740
IF(NM.GT.50) NM=50  GAM08750
TMAX=2.*E*E/(MC2+2.*E) GAM08770
DEL=TMAX/FLOAT(NM) GAM08780
T1=0.0              GAM08790
T2=0.0              GAM08800
TOT=0.0              GAM08810
DO 1000 I=1,NM      GAM08820
T1=T2              GAM08830
T2=T1+DEL          GAM08840
TOT=TOT+(PC(E,T1)*T1 + PC(E,T2)*T2)*DEL/2.  GAM08850
1000 CONTINUE        GAM08860
FC=TOT/E          GAM08870
RETURN            GAM08880
END              GAM08890
FUNCTION PC(E,T)    GAM08900
C
REAL MC2          GAM08910
C
PAI=3.1415927     GAM08920
MC2=0.510976     GAM08930
R2 =7.9396E-26    GAM08940
AL=E/0.510976    GAM08950
TEM=1.0/E**2      GAM08960
C
DSIG=PAI*R2*MC2*((MC2*T*TEM)**2 + 2.*TEM*(E-T)**2
1   +(E-T)*TEM*((T-MC2)**2-MC2**2)/E) / (E-T)**2  GAM09020
SIGT =2.*PAI*R2*((2.*(1.+AL)/(1.+2.*AL)- ALOG(1.+2.*AL)/AL)
1   *(1.+AL)/AL**2*ALOG(1.+2.*AL)/(2.*AL)           GAM09030
2   -(1.+3.*AL)/(1.+2.*AL)**2)                      GAM09040
GAM09050
C
PC=DSIG/SIGT      GAM09060
RETURN            GAM09070
END              GAM09080
GAM09090

```

SOURCE ELEMENT LIST (8BIT MODE)

ELEMENT NAME ((POPOP4)) ESTABLISHED 77.01.25

```

SUBROUTINE DTFPUNCE(NN,R,IUM,NCARD,NPUN) GAM09100
C *** STOLEN FROM ANISN GAM09110
C *** DTFPUN USES VARIABLE FORMAT TO PUNCH AND NUMBER CARDS GAM09120
DIMENSION E(6),NN(6),R(6),IE(6),IEXP(6),S1(6),S2(6) GAM09130
DIMENSION FMT(26),FBT(4),FET(2) GAM09140
DATA POS,XNEG/'+' ','-' '/' GAM09150
DATA FMT(1)*FMT(26)*FET(1)*FET(2)/*(' ',''18)'',''18)'/' GAM09160
DATA FBT(1)*FBT(2)*FBT(3)*FBT(4)/*'12.2',''A1.I''5,A1',''12,'/' GAM09170
DO 2 J=1,6 GAM09180
K=(J-1)*4 + 1 GAM09190
DO 3 I=1,4 GAM09200
L=K+I GAM09210
3 FMT(L)=FBT(I) GAM09220
2 CONTINUE GAM09230
IF(IUM.EQ.6)GO TO 4 GAM09240
K=IUM*4 + 2 GAM09250
FMT(K)=FET(1) GAM09260
FMT(K+1)=FET(2) GAM09270
4 DO 1 I=1,IUM GAM09280
S1(I)=POS GAM09290
IF(E(I).LT.0.0)S1(I)=XNEG GAM09300
CALL FLTDX(E(I),IE(I),IEXP(I)) GAM09310
S2(I)=XNEG GAM09320
IF(IEXP(I).GE.0)S2(I)=POS GAM09330
IEXP(I)=ABS(IEXP(I)) GAM09340
1 CONTINUE GAM09350
C*** WRITE (7,FMT) (NN(I),R(I),S1(I),IE(I),S2(I),IEXP(I),I=1,IUM) GAM09360
      WRITE(NPUN,FMT) (NN(I),R(I),S1(I),IE(I),S2(I),IEXP(I),I=1,IUM) GAM09370
1,NCARD GAM09380
RETURN GAM09390
END GAM09400
SUBROUTINE FLTDX(E1,NE1,N1) GAM09410
C *** STOLEN FROM ANISN GAM09420
C *** FLTDX CONVERTS FLOATING NUMBER TO INTEGER GAM09430
N=-4 GAM09440
E=ABS(E1) GAM09450
IF(E.NE.0.0)GO TO 1 GAM09460
N=0 GAM09470
NE=0 GAM09480
GO TO 6 GAM09490
3 E=E*10.0 GAM09500
N=N-1 GAM09510
1 IF(E.GE.1.0)GO TO 4 GAM09520
GO TO 3 GAM09530
5 E=E/10.0 GAM09540
N=N+1 GAM09550
4 IF(E.GE.10.0)GO TO 5 GAM09560
E=E*10000.0 GAM09570
2 NE=E GAM09580
E=E-FLOAT(NE) GAM09590
IF(E.LT.0.5)GO TO 6 GAM09600
IF(NE,NE,99999)GO TO 7 GAM09610

```

SOURCE ELEMENT LIST (8BIT MODE)

```

N=N+1                                GAM09620
NE=10000                             GAM09630
GO TO 6                               GAM09640
7 NE=NE+1                            GAM09650
6 NE1=NE                            GAM09660
N1=N                                GAM09670
RETURN                               GAM09680
END                                  GAM09690
SUBROUTINE PUNSH(X,N,NPUN)          GAM09700
C *** STOLEN FROM ANISN           GAM09710
C *** CLEVER SET OF SUBROUTINES WHICH PUNCH CARDS IN ANISN FORMAT
C *** PUNSH SETS UP EACH CARD PUNCHED BY DTFPUN UTILIZING REPEATS
DIMENSION ETR(6),NN(6),R(6),X(1)    GAM09720
DATA BB,RR/'  ',' ' /                GAM09730
NCARD=1                             GAM09740
I6=0                                 GAM09750
K=0                                 GAM09760
ITRIP=0                            GAM09770
II=N+1                            GAM09780
DO 1 I=2,II                         GAM09790
IF(ITRIP.LE.0)GO TO 2              GAM09800
ITRIP=0                            GAM09810
GO TO 3                            GAM09820
2 IF(I.GE.II)GO TO 4              GAM09830
IF(X(I).NE.X(I-1))GO TO 4          GAM09840
K=K+1                            GAM09850
IF(K.LT.98)GO TO 1              GAM09860
ITRIP=1                            GAM09870
4 I6=I6+1                           GAM09880
NN(16)=0                           GAM09890
R(16)=BB                           GAM09900
IF(K.LE.0)GO TO 5              GAM09910
NN(16)=K+1                           GAM09920
R(16)=RR                           GAM09930
K=0                                 GAM09940
5 ETR(I6)=X(I-1)                  GAM09950
IF(I6.GE.6)GO TO 6              GAM09960
3 IF(I.LT.II)GO TO 1              GAM09970
6 CALL DTFPUNK(ETR,NN,R,I6,NCARD,NPUN)
NCARD=NCARD +1                      GAM09980
I6=0                                 GAM09990
1 CONTINUE                           GAM10000
RETURN                               GAM10010
END                                  GAM10020
GAM10030
GAM10040
GAM10050

```

Appendix C List of Sample Input and Output

Table C-1 Sample input data

.....*,...,1,...*,...,2...,*,...,3...,*,...,4,...*,...,5,...*,...,6,...

*HIEDRUN RFNAME=J9103.GAMLEGJR

*DISK PUNCH

*DATA

21	10	9	0	1	0	0	1	
21								
14,0		12,0		10,0		8,0		6,5
4,0		3,0		2,5		2,0		1,66
1,0		0,8		0,6		0,4		0,3
0,1		0,05		0,02				
1,0		1,0		1,0		1,0		1,0
1,0		1,0		1,0		1,0		1,0
1,0		1,0		1,0		1,0		1,0
1,0		1,0		1,0		1,0		1,0
14,0		12,0		10,0		8,0		6,5
4,0		3,0		2,5		2,0		1,66
1,0		0,8		0,6		0,4		0,3
0,1		0,05		0,02				
3								
8,0		26,0		82,0				

Table C-2 Sample output

INPUT DATA

IG NO. OF GROUPS	21	N NO. OF INTEGRATION POINTS/GROUP	10
NMAX NO. OF LEGENDRE COMPONENTS	9	KON CONTROL -1/0/1 = FLUX/NONE/SOURCE	0
ICAL 0/1 = X-SEC INPUT/CALCULATE	1	IPRTO 0/1 = PRINT DETAIL X-SEC NO/YES	0
IPRT1 0/1 = PRINT DETAIL HEAT COEFF NO/YES	0	NACT 0/1 = OUTPUT HEAT COEFF NO/YES	1

	ENERGY (MEV)	SOURCE
1	0.14000E+02	0.10000E+01
2	0.12000E+02	0.10000E+01
3	0.10000E+02	0.10000E+01
4	0.80000E+01	0.10000E+01
5	0.65000E+01	0.10000E+01
6	0.50000E+01	0.10000E+01
7	0.40000E+01	0.10000E+01
8	0.30000E+01	0.10000E+01
9	0.25000E+01	0.10000E+01
10	0.20000E+01	0.10000E+01
11	0.16000E+01	0.10000E+01
12	0.13300E+01	0.10000E+01
13	0.10000E+01	0.10000E+01
14	0.80000E+00	0.10000E+01
15	0.60000E+00	0.10000E+01
16	0.40000E+00	0.10000E+01
17	0.30000E+00	0.10000E+01
18	0.20000E+00	0.10000E+01
19	0.10000E+00	0.10000E+01
20	0.50000E-01	0.10000E+01
21	0.20000E-01	0.10000E+01

GROUP ENERGY BOUNDS

1	0.14000E+02
2	0.12000E+02
3	0.10000E+02
4	0.80000E+01
5	0.65000E+01
6	0.50000E+01
7	0.40000E+01
8	0.30000E+01
9	0.25000E+01
10	0.20000E+01
11	0.16000E+01
12	0.13300E+01
13	0.10000E+01
14	0.80000E+00
15	0.60000E+00
16	0.40000E+00
17	0.30000E+00
18	0.20000E+00
19	0.10000E+00
20	0.50000E-01
21	0.20000E-01

GROUP	AVG FLUX	AVG SIGMA S	AVG SOURCE
1	0.10000E+02	0.16858E+00	0.10000E+01
2	0.10000E+02	0.19092E+00	0.10000E+01
3	0.10000E+02	0.22116E+00	0.10000E+01
4	0.10000E+02	0.25788E+00	0.10000E+01
5	0.10000E+02	0.30315E+00	0.10000E+01
6	0.10000E+02	0.35698E+00	0.10000E+01
7	0.10000E+02	0.42038E+00	0.10000E+01
8	0.10000E+02	0.48712E+00	0.10000E+01
9	0.10000E+02	0.54912E+00	0.10000E+01
10	0.10000E+02	0.61752E+00	0.10000E+01
11	0.10000E+02	0.69001E+00	0.10000E+01

12	0.10000E+02	0.78636E+00	0.10000E+01
13	0.10000E+02	0.89204E+00	0.10000E+01
14	0.10000E+02	0.10033E+01	0.10000E+01
15	0.10000E+02	0.11631E+01	0.10000E+01
16	0.10000E+02	0.13392E+01	0.10000E+01
17	0.10000E+02	0.15159E+01	0.10000E+01
18	0.10000E+02	0.17863E+01	0.10000E+01
19	0.10000E+02	0.21047E+01	0.10000E+01
20	0.10000E+02	0.23592E+01	0.10000E+01

DIFFERENCE-GROUP AVG SCATTER CROSS SECTION AND SUM OF GROUP AVERAGED TRANSFERS, GROUP 1 , IS=-1.86265E-08
 DIFFERENCE-GROUP AVG SCATTER CROSS SECTION AND SUM OF GROUP AVERAGED TRANSFERS, GROUP 2 , IS=-2.23517E-08
 DIFFERENCE-GROUP AVG SCATTER CROSS SECTION AND SUM OF GROUP AVERAGED TRANSFERS, GROUP 3 , IS=-2.23517E-08
 DIFFERENCE-GROUP AVG SCATTER CROSS SECTION AND SUM OF GROUP AVERAGED TRANSFERS, GROUP 4 , IS=-2.98023E-08
 DIFFERENCE-GROUP AVG SCATTER CROSS SECTION AND SUM OF GROUP AVERAGED TRANSFERS, GROUP 5 , IS=-4.47035E-08
 DIFFERENCE-GROUP AVG SCATTER CROSS SECTION AND SUM OF GROUP AVERAGED TRANSFERS, GROUP 6 , IS=-5.21541E-08
 DIFFERENCE-GROUP AVG SCATTER CROSS SECTION AND SUM OF GROUP AVERAGED TRANSFERS, GROUP 7 , IS=-5.21541E-08
 DIFFERENCE-GROUP AVG SCATTER CROSS SECTION AND SUM OF GROUP AVERAGED TRANSFERS, GROUP 8 , IS=-5.96046E-08
 DIFFERENCE-GROUP AVG SCATTER CROSS SECTION AND SUM OF GROUP AVERAGED TRANSFERS, GROUP 9 , IS=-1.04308E-07
 DIFFERENCE-GROUP AVG SCATTER CROSS SECTION AND SUM OF GROUP AVERAGED TRANSFERS, GROUP 10 , IS=-1.34110E-07
 DIFFERENCE-GROUP AVG SCATTER CROSS SECTION AND SUM OF GROUP AVERAGED TRANSFERS, GROUP 11 , IS=-1.93715E-07
 DIFFERENCE-GROUP AVG SCATTER CROSS SECTION AND SUM OF GROUP AVERAGED TRANSFERS, GROUP 12 , IS=-2.23517E-07
 DIFFERENCE-GROUP AVG SCATTER CROSS SECTION AND SUM OF GROUP AVERAGED TRANSFERS, GROUP 13 , IS=-2.83122E-07
 DIFFERENCE-GROUP AVG SCATTER CROSS SECTION AND SUM OF GROUP AVERAGED TRANSFERS, GROUP 14 , IS=-1.78814E-07
 DIFFERENCE-GROUP AVG SCATTER CROSS SECTION AND SUM OF GROUP AVERAGED TRANSFERS, GROUP 15 , IS=-1.19209E-07
 DIFFERENCE-GROUP AVG SCATTER CROSS SECTION AND SUM OF GROUP AVERAGED TRANSFERS, GROUP 16 , IS=-2.98023E-08
 DIFFERENCE-GROUP AVG SCATTER CROSS SECTION AND SUM OF GROUP AVERAGED TRANSFERS, GROUP 17 , IS= -2.98023E-08
 DIFFERENCE-GROUP AVG SCATTER CROSS SECTION AND SUM OF GROUP AVERAGED TRANSFERS, GROUP 18 , IS= 2.98023E-08
 DIFFERENCE-GROUP AVG SCATTER CROSS SECTION AND SUM OF GROUP AVERAGED TRANSFERS, GROUP 19 , IS= 2.98023E-07
 DIFFERENCE-GROUP AVG SCATTER CROSS SECTION AND SUM OF GROUP AVERAGED TRANSFERS, GROUP 20 , IS= 2.68221E-06

*** GAMMA-RAY CROSS SECTIONS FOR ATOMIC NUMBER = 8, ***

GROUP	ABSORB	COHERENT	HEAT
	X-SEC,	X-SEC,	COEFF,
1	0.16376E+00	0.39593E-05	0.61256E-12
2	0.14631E+00	0.62334E-05	0.70097E-12
3	0.12589E+00	0.10696E-04	0.59384E-12
4	0.10481E+00	0.18785E-04	0.50097E-12
5	0.83326E-01	0.34447E-04	0.42197E-12
6	0.62398E-01	0.63555E-04	0.35401E-12
7	0.43031E-01	0.11992E-03	0.29851E-12
8	0.26930E-01	0.21195E-03	0.23293E-12
9	0.15253E-01	0.34435E-03	0.22083E-12
10	0.81289E-02	0.55705E-03	0.19180E-12
11	0.29804E-02	0.89316E-03	0.16642E-12
12	0.38440E-03	0.15880E-02	0.13863E-12
13	0.15219E-03	0.27898E-02	0.11198E-12
14	0.27002E-03	0.48585E-02	0.89388E-13
15	0.64983E-03	0.10106E-01	0.64698E-13
16	0.16871E-02	0.20526E-01	0.44286E-13
17	0.48056E-02	0.40731E-01	0.30302E-13
18	0.28365E-01	0.11460E+00	0.16517E-13
19	0.25669E+00	0.39042E+00	0.84969E-14
20	0.30229E+01	0.14277E+01	0.15513E-13

P-O CROSS SECTION TABLE ATOMIC NUMBER= 0,800E+01

GROUP= 1	GROUP= 2	GROUP= 3	GROUP= 4	GROUP= 5	GROUP= 6	GROUP= 7	GROUP= 8	
1	0.812564E-12	0.700975E-12	0.593837E-12	0.500969E-12	0.421973E-12	0.354013E-12	0.298514E-12	0.252932E-12
2	0.163757E+00	0.146305E+00	0.125887E+00	0.104812E+00	0.833257E-01	0.623984E-01	0.430312E-01	0.269297E-01
3	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
4	0.500071E+00	0.527198E+00	0.567111E+00	0.619309E+00	0.688142E+00	0.774646E+00	0.881800E+00	0.998944E+00
5	0.115049E-01	0.159455E-01	0.235674E-01	0.273215E-01	0.428199E-01	0.469849E-01	0.762777E-01	0.634457E-01
6	0.0	0.244885E-01	0.344168E-01	0.387147E-01	0.595572E-01	0.633240E-01	0.102407E+00	0.844818E-01
7	0.0	0.0	0.255675E-01	0.271676E-01	0.410161E-01	0.421567E-01	0.672959E-01	0.537520E-01
8	0.0	0.0	0.0	0.208642E-01	0.300418E-01	0.304373E-01	0.473154E-01	0.372868E-01
9	0.0	0.0	0.0	0.0	0.237821E-01	0.231410E-01	0.355661E-01	0.273647E-01
10	0.0	0.0	0.0	0.0	0.0	0.187772E-01	0.278473E-01	0.211754E-01
11	0.0	0.0	0.0	0.0	0.0	0.0	0.230154E-01	0.169135E-01
12	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.141467E-01
13	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
14	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
15	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
16	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
17	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
18	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
19	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
20	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
21	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
22	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
23	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
24	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
GROUP= 9	GROUP= 10	GROUP= 11	GROUP= 12	GROUP= 13	GROUP= 14	GROUP= 15	GROUP= 16	
1	0.220826E-32	0.191800E-12	0.166418E-12	0.138629E-12	0.111980E-12	0.893880E-13	0.646985E-13	0.442863E-13
2	0.152535E-01	0.812892E-02	0.298035E-02	0.384399E-03	0.152193E-03	0.270018E-03	0.649832E-03	0.168710E-02
3	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
4	0.111109E+01	0.124063E+01	0.138044E+01	0.157075E+01	0.178256E+01	0.200665E+01	0.233110E+01	0.269395E+01
5	0.934249E-01	0.969983E-01	0.138978E+00	0.222649E+00	0.229930E+00	0.366138E+00	0.665318E+00	0.699163E+00

6	0.133647E+00	0.135160E+00	0.195353E+00	0.288098E+00	0.282754E+00	0.454295E+00	0.701571E+00	0.643602E+00
7	0.869210E-01	0.921352E-01	0.131806E+00	0.194765E+00	0.172523E+00	0.272886E+00	0.427922E+00	0.338051E+00
8	0.582424E-01	0.630222E-01	0.941255E-01	0.139684E+00	0.124925E+00	0.183296E+00	0.299576E+00	0.253461E+00
9	0.420237E-01	0.442843E-01	0.674312E-01	0.105337E+00	0.950898E-01	0.141613E+00	0.226845E+00	0.201600E+00
10	0.317365E-01	0.330241E-01	0.492896E-01	0.792151E-01	0.751370E-01	0.113113E+00	0.186677E+00	0.163172E+00
11	0.250089E-01	0.255057E-01	0.376967E-01	0.601171E-01	0.586404E-01	0.924040E-01	0.155025E+00	0.137500E+00
12	0.202155E-01	0.203740E-01	0.295903E-01	0.470093E-01	0.456748E-01	0.738355E-01	0.129555E+00	0.115197E+00
13	0.170265E-01	0.166120E-01	0.238607E-01	0.374007E-01	0.362245E-01	0.583675E-01	0.104881E+00	0.963858E-01
14	0.0	0.140606E-01	0.195685E-01	0.303852E-01	0.290520E-01	0.466202E-01	0.834078E-01	0.777533E-01
15	0.0	0.0	0.166165E-01	0.250301E-01	0.237003E-01	0.375185E-01	0.666972E-01	0.614692E-01
16	0.0	0.0	0.0	0.213047E-01	0.195676E-01	0.306497E-01	0.536361E-01	0.488575E-01
17	0.0	0.0	0.0	0.0	0.166735E-01	0.253176E-01	0.437542E-01	0.390753E-01
18	0.0	0.0	0.0	0.0	0.0	0.215739E-01	0.360865E-01	0.317320E-01
19	0.0	0.0	0.0	0.0	0.0	0.0	0.307109E-01	0.260787E-01
20	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.221329E-01
21	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
22	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
23	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
24	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0

GROUP=17 GROUP=18 GROUP=19 GROUP=20 GROUP=

1	0.303022E-13	0.165175E-13	0.849689E-14	0.155133E-13
2	0.480561E-02	0.283647E-01	0.256687E+00	0.302293E+01
3	0.0	0.0	0.0	0.0
4	0.306970E+01	0.370668E+01	0.484591E+01	0.915718E+01
5	0.121617E+01	0.278778E+01	0.408360E+01	0.613425E+01
6	0.117210E+01	0.184873E+01	0.890537E+00	0.505629E+00
7	0.666475E+00	0.820999E+00	0.0	0.0
8	0.495682E+00	0.355055E+00	0.0	0.0
9	0.404922E+00	0.104938E+00	0.0	0.0
10	0.290905E+00	0.118816E-01	0.0	0.0
11	0.204546E+00	0.0	0.0	0.0
12	0.154674E+00	0.0	0.0	0.0
13	0.117333E+00	0.0	0.0	0.0
14	0.898421E-01	0.0	0.0	0.0
15	0.663096E-01	0.0	0.0	0.0
16	0.482511E-01	0.0	0.0	0.0
17	0.359361E-01	0.0	0.0	0.0
18	0.272667E-01	0.0	0.0	0.0
19	0.212790E-01	0.0	0.0	0.0
20	0.169428E-01	0.0	0.0	0.0
21	0.140648E-01	0.0	0.0	0.0
22	0.0	0.0	0.0	0.0
23	0.0	0.0	0.0	0.0
24	0.0	0.0	0.0	0.0

— Deleted the output list for P_1, P_2, \dots, P_7 cross section tables —

P 8 CROSS SECTION TABLE ATOMIC NUMBER= 0,800E+01

	GROUP= 1	GROUP= 2	GROUP= 3	GROUP= 4	GROUP= 5	GROUP= 6	GROUP= 7	GROUP= 8
1	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
2	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
3	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
4	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
5	0.181907E+00	0.244958E+00	0.344227E+00	0.389429E+00	0.548589E+00	0.585992E+00	0.767985E+00	0.706656E+00
6	0.0	0.317955E+00	0.391668E+00	0.383971E+00	0.463898E+00	0.358496E+00	0.305572E+00	0.129666E+00
7	0.0	0.0	0.201300E+00	0.142048E+00	0.101214E+00	-0.265922E-01	-0.218831E+00	0.287883E+00
8	0.0	0.0	0.0	0.539307E-01	-0.196505E-01	-0.108366E+00	-0.272836E+00	0.251353E+00
9	0.0	0.0	0.0	0.0	-0.558443E-01	-0.118248E+00	-0.233658E+00	-0.179825E+00
10	0.0	0.0	0.0	0.0	0.0	-0.110009E+00	-0.188277E+00	-0.126156E+00
11	0.0	0.0	0.0	0.0	0.0	0.0	-0.154426E+00	-0.896439E-01
12	0.0	0.0	0.0	0.0	0.0	0.0	0.0	-0.673694E-01
13	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
14	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
15	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
16	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
17	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
18	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
19	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
20	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
21	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
22	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
23	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
24	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
	GROUP= 9	GROUP=10	GROUP=11	GROUP=12	GROUP=13	GROUP=14	GROUP=15	GROUP=16
1	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
2	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
3	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
4	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
5	0.892100E+00	0.843932E+00	0.857260E+00	0.583861E+00	0.568934E+00	-0.280440E-01	-0.142082E+00	-0.160588E+00
6	0.106123E+00	-0.150448E+00	0.511407E+00	-0.120635E+01	-0.109139E+01	-0.949805E+00	0.427132E+00	0.161883E+00
7	-0.487379E+00	-0.589232E+00	0.793901E+00	-0.658495E+00	0.206228E+00	0.855573E+00	0.259156E+00	-0.486300E+00
8	-0.376765E+00	-0.355549E+00	0.368797E+00	0.640894E-01	0.547321E+00	0.582525E+00	-0.549529E+00	0.397444E+00
9	-0.223144E+00	-0.143434E+00	0.498962E-01	0.333339E+00	0.454873E+00	0.121009E+00	-0.464670E+00	0.450000E+00
10	-0.124327E+00	-0.369229E-01	0.930635E-01	0.360907E+00	0.292868E+00	-0.146469E+00	-0.209037E+00	0.150766E+00
11	-0.691156E-01	0.121258E-01	0.128260E+00	0.295751E+00	0.140016E+00	-0.255444E+00	-0.586212E-02	-0.530698E-01
12	-0.373519E-01	0.313854E-01	0.126578E+00	0.219848E+00	0.383923E-01	-0.270168E+00	0.111640E+00	-0.157626E+00
13	-0.207191E-01	0.380080E-01	0.112926E+00	0.159303E+00	-0.118923E-01	-0.236228E+00	0.166001E+00	-0.188453E+00
14	0.0	0.388085E-01	0.975131E-01	0.116799E+00	0.346777E-01	-0.189754E+00	0.172502E+00	-0.173134E+00
15	0.0	0.0	0.848217E-01	0.869694E-01	-0.423209E-01	-0.148254E+00	0.154151E+00	-0.138086E+00
16	0.0	0.0	0.0	0.681286E-01	-0.432998E-01	-0.116167E+00	0.130306E+00	-0.103463E+00
17	0.0	0.0	0.0	0.0	-0.415252E-01	-0.918611E-01	0.108242E+00	-0.760460E-01
18	0.0	0.0	0.0	0.0	0.0	-0.754713E-01	0.896777E-01	-0.565802E-01
19	0.0	0.0	0.0	0.0	0.0	0.0	0.761890E-01	-0.427404E-01
20	0.0	0.0	0.0	0.0	0.0	0.0	0.0	-0.3388898E-01

21	0,0	0,0	0,0	0,0	0,0	0,0	0,0	0,0
22	0,0	0,0	0,0	0,0	0,0	0,0	0,0	0,0
23	0,0	0,0	0,0	0,0	0,0	0,0	0,0	0,0
24	0,0	0,0	0,0	0,0	0,0	0,0	0,0	0,0
	GROUP=17	GROUP=18	GROUP=19	GROUP=20	GROUP=			
1	0,0	0,0	0,0	0,0				
2	0,0	0,0	0,0	0,0				
3	0,0	0,0	0,0	0,0				
4	0,0	0,0	0,0	0,0				
5	-0,837052E-01	0,470903E-01	-0,170503E-01	0,611579E-04				
6	0,305637E+00	0,844195E-01	-0,469525E-01	0,171103E-01				
7	-0,155056E+00	-0,142633E+00	0,0	0,0				
8	0,2573148E+00	0,143510E+00	0,0	0,0				
9	-0,296205E+00	-0,148211E+00	0,0	0,0				
10	-0,177388E+00	0,612444E-01	0,0	0,0				
11	-0,134940E-01	0,0	0,0	0,0				
12	0,730120E-01	0,0	0,0	0,0				
13	0,103711E+00	0,0	0,0	0,0				
14	0,100657E+00	0,0	0,0	0,0				
15	0,785379E-01	0,0	0,0	0,0				
16	0,530240E-01	0,0	0,0	0,0				
17	0,334172E-01	0,0	0,0	0,0				
18	0,201524E-01	0,0	0,0	0,0				
19	0,120394E-01	0,0	0,0	0,0				
20	0,702016E-02	0,0	0,0	0,0				
21	0,423505E-02	0,0	0,0	0,0				
22	0,0	0,0	0,0	0,0				
23	0,0	0,0	0,0	0,0				
24	0,0	0,0	0,0	0,0				