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PREDICTION OF LOFT LI-4 EXPERIMENT
—CSNI STANDARD PROBLEM NO.5—

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Prediction of LOFT L1-4 Experiment — ^{CSNI} ~~CNSI~~ Standard
Problem No.5 —

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LOFT L1-4 experimental results were predicted by LOFT Analysis Group and Code Development Group using RELAP-4J and ALARM-P1 respectively. The input data prepared by the former group were used in both the analyses. Thus any differences in the results should stem from the differences in code performance characteristics of the two codes.

- (1) The coolant behaviors predicted by RELAP-4J and ALARM-P1 are in good agreement although some differences do exist between these two calculation models.
- (2) Large difference is seen in coolant flow rate across the pump. The coast down and the flow rate by ALARM-P1 are larger and smaller respectively than by RELAP-4J.
- (3) An explicit method of the ALARM-P1 leads to unstable calculation at a T shaped junction when one of the two volumes connected by the junction is filled with subcooled water.
- (4) Coolant flow in the downcomer, heat transfer to and from the steam generator secondary and suppression tank behavior must be modified to better predict the experimental results.
- (5) Additional instrumentation in reflood assist and ECC injection lines are necessary to better understand the coolant behavior.

Keywords: LOFT, LOCA, Reactor Safety, Blowdown, RELAP-4J Code, ALARM-P1 Code, Coolant Behavior, ECCS

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LOFT L1-4 実験の予備解析

— CSNI 標準問題 No.5 —

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ECCをコールドレグに注入する実験であるL1-4実験をRELAP-4J及びALARM-P1を用いて予測した。この解析では、入力データの作成に、両方ともRELAP-4Jを用いるので、解析結果に表われる差異は計算コードの特性に基づくものと考えられる。

本解析の結果、LOFT L1-4実験と、計算モデルについて、次のような結論を得た。

- (1) RELAP-4JとALARM-P1により予測された冷却材挙動は、両コードの計算モデルに幾つかの差があるにもかかわらず、非常に良く一致した。
- (2) 主な差異は、ポンプ流量に現われ、ALARM-P1では、ポンプコーストダウンが早く、RELAP-4Jより小さい流量を予測した。
- (3) ALARM-P1では、数値解法が陽的解法であるために、T型ジャンクションで接続された2つのボリュームのうち1つが、サブクール水で満たされる時に計算上の不安定がおきた。
- (4) ダウンカマの流れ、蒸気発生器2次側との熱伝達、圧力抑制容器内冷却材挙動については、実験結果をより良く予測するには、改良が必要である。
- (5) 冷却材挙動をより適確に把握するには、再冠水補助系、ECC注入系に計測点を追加することが望ましい。

* 安全解析部

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1. INTRODUCTION

In view of current demand on nuclear reactor safety research, to perform experiment on loss of coolant accident and related ECC (Emergency Core Cooling) water behavior by using small scale PWR (Pressurized Water Reactor) is primary objective of the LOFT (Loss Of Fluid Test) program¹⁾. The LOFT experiments consist of non-nuclear tests (L1 series) and nuclear tests (L2 and L3 series, and additional test series under consideration). So far five nonnuclear tests have been performed^{2),5)} and the results provide us valuable informations on coolant behavior during a postulated LOCA (Loss Of Coolant Accident) of a PWR.

Among the five tests, the fifth experiment, L1-4, is a double ended cold leg break experiment with ECC injection into cold leg of the operating loop⁶⁾ and it is representative break configuration condition for the design basis accident⁷⁾ in an actual reactor. Therefore the analysis of L1-4 experiment is invaluable with regard to verification of LOCA analysis code as well as better understanding of coolant behavior during LOCA.

From this point of view, CSNI has selected the LOFT L1-4 experiment as the international standard problem No.5 in that prediction of experimental results must be made on blind basis, i.e. without knowing test results.

Responding to the CSNI's request, JAERI (Japan Atomic Energy Research Institute) has dicided to participate in the standard problem No.5 and two groups at JAERI were involved in the prediction. One group is the LOFT analysis group of Reactor Safety Laboratory 1 who has been performing LOFT data analysis since JAERI is one of foreign participants in the LOFT program. The other group is the code development group of Safety Code Development Laboratory who has been developing reactor safety analysis codes.

The reason for the participation of the two groups was that the LOFT analysis group intended to analyze L1-4 experiment because behavior in L1-4 provides base line data for future nuclear test with ECC injection and the code development group aimed to better understand performance characteristics of their developed code for code verification purposes. Thus the analysis group used RELAP-4J⁸⁾ for their analysis in consistent with the previous LOFT data analysis of L1-2⁹⁾ and L1-3A while the code development group used ALARM-P1¹⁰⁾ for the prediction. However input data were prepared by the analysis group and provided to the code development group who then converted them to fit the ALARM-P1 input specifications. Therefore both input are consistent and any difference appeared in the results should

be originated from performance characteristics of each code.

Both groups have completed their calcualtions by June 17, 1977 in order to beat the dead line set by CSNI and the results were mailed to the NRC on June 21, 1977 prior to the scheduled data release date of June 24, 1977.

The present report gives description of the two predicted results of LOFT L1-4 experiment by RELAP-4J and ALARM-P1 responding to the standard problem No.5. In addition, the two results are compared and the differences are dicussed. Although published date of the present report is later than the scheduled data release date of L1-4, only the calculated results which were sent to the NRC are contained in the present report without any alterations.

As a future study, comparison of the present analysis with L1-4 experimental results as well as post test analysis will be conducted as soon as the data become available.

2. DESCRIPTION OF L1-4 EXPERIMENT

LOFT experiment has been performed at INEL (Idaho National Engineering Laboratory) of U.S.A. with the use of LOFT reactor. Detail descriptions of LOFT experiment as well as the test facility are described in references 1) and 6). In the present chapter brief summary of L1-4 experiment is given by depicting available informations from those references for our convenience.

2.1 Objectives of L1-4 Experiment

L1-4 experiment is the fifth experiment of nonnuclear test series of the LOFT program⁶⁾. The specific objectives are:

- (1) Provide comparison of delayed HPIS (High Pressure Injection System) and LPIS (Low Pressure Injection System) injection to the cold leg and the lower plenum.
- (2) Provide data reproducibility information by comparing with other related tests.
- (3) Obtain data for evaluating downcomer bypass and mixing of the emergency core coolant with the primary coolant.
- (4) Determine the effects of PCS (Primary Coolant System) operation and rapid depressurization with boric acid coolant.
- (5) Test system performance with PPS (Primary Protection System) backup under operating procedures as similar as possible to those planned for nuclear operation.
- (6) Provide system thermal hydraulic data to compare with predictions and other experimental data for code verification purposes.

Among the above objectives, item (6) is of our interest with respect to prediction of L1-4 experiment.

2.2 Experimental Procedure

L1-4 is to simulate a double ended 200% cold leg break using the LOFT reactor. In the nonnuclear test series however, a core simulator is installed in the core instead of a nuclear fuel assembly in order to simulate only hydraulic resistance of the fuel assembly. Thus the experiment is called isothermal since no heat source exists in the system.

Fig. 2.1 shows the LOFT system configuration for L1-4 experiment. Although the system configuration is the same as other L1 series tests except L1-1 (hot leg break), it should be noted that ECC inlet to cold leg

of the intact loop is provided in Ll-4 for ECC injection by HPIS, LPIS and accumulator.

Major events of Ll-4 experiment are listed in Table 2.1. The primary system is heated up by electric heaters in pressurizer and irreversible thermal work given to coolant by the two pumps in PCS. Initial test conditions to be achieved are:

| | |
|--------------------|---|
| System temperature | 282°C (540°F). |
| System pressure | 15.6 MPa (2,250 psig). |
| PCS flow rate | 1.512×10^4 kg/sec (2×10^6 lb/h). |

40 hours are required to maintain the system at the initial test conditions for stabilizing the whole system at isothermal conditions.

Blowdown is initiated at time T_0 by opening QOBV (Quick Opening Blowdown Valve) and emergency coolant is injected into cold leg of the intact loop by HPIS, LPIS and accumulator system at the specified timings. HPIS is set to start at 22 ± 2 sec after break with injection rate of 1.085 ± 0.126 liter/sec (17.2 ± 2 gpm) and LPIS pump is set to deliver coolant at 35.5 ± 2 sec after break. The injection rate of LPIS depends on injection line pressure. Injection from accumulator is initiated when system pressure falls below the accumulator tank pressure and the check valve opens.

Test is expected to complete 5 min after break and experimental data are recorded by DAVDS (Data Acquisition and Visual Display System) till completion of the test.

Details of Ll-4 experiment are described in reference 6).

Table 2.1 Major Events of Ll-4 Experiment

| Item | Time | Event |
|------|------------------------|--|
| 1. | T_0 -60 hrs or more | Preparations |
| 2. | T_0 -60 hrs | Start heat up of PCS |
| 3. | T_0 -60 to 40 hrs | Data acquisition system check |
| 4. | T_0 -40 hrs | PCS at test temperature and pressure 282°C, 15.6 MPa (540°F, 2250 psig) |
| 5. | T_0 -3 min | Adjust PCS flow |
| 6. | T_0 | Open QOBV |
| 7. | $T_0+22 \pm 2$ sec | Initiate HPIS flow |
| 8. | $T_0+35.5 \pm 2$ sec | Initiate LPIS flow |
| 9. | T_0+5 min(estimated) | Test completed |

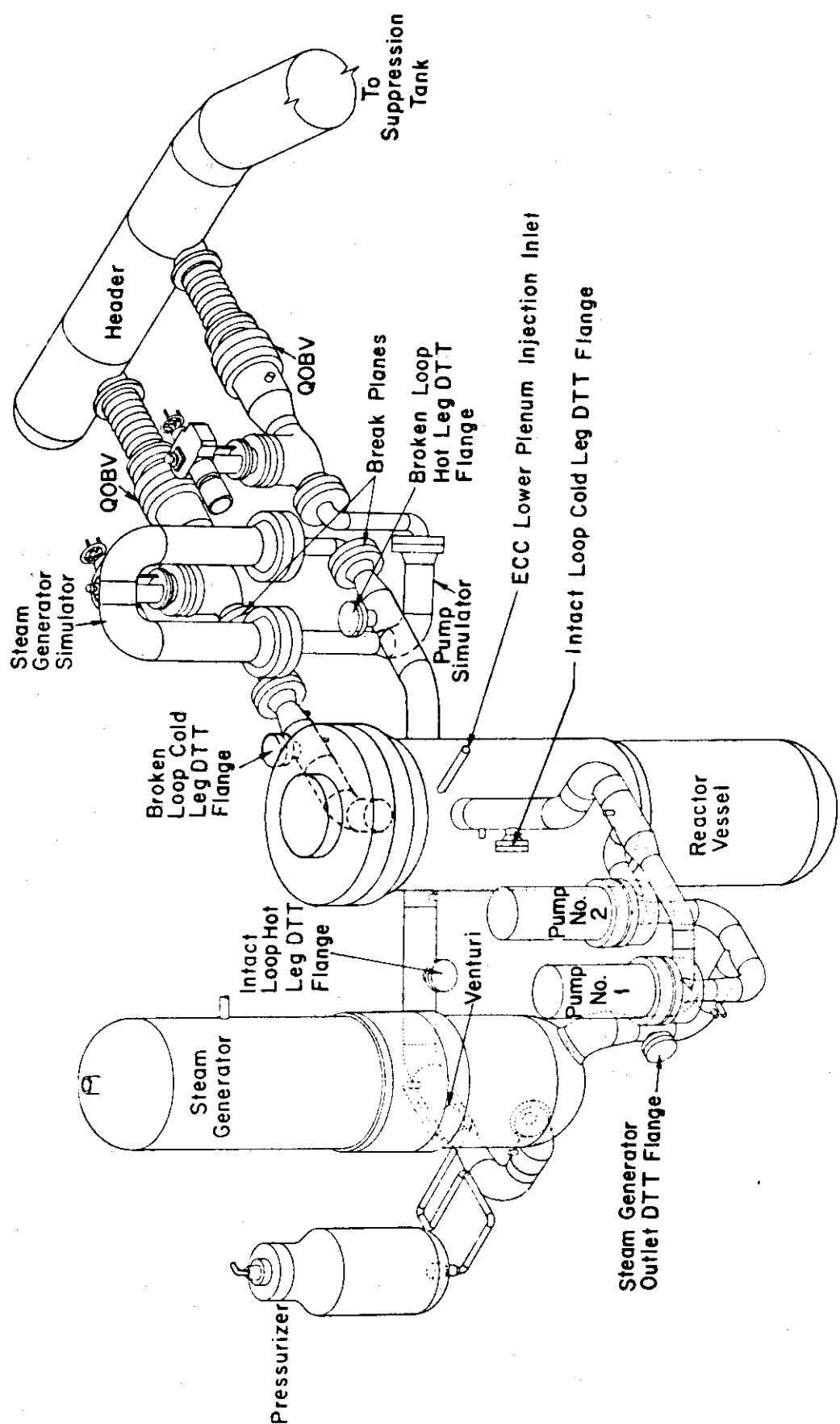


Fig. 2.1 LOFT major components

3. INPUT DATA PREPARATIONS

Input data for the present Ll-4 predictions were prepared by the LOFT analysis group primarily for RELAP-4J analysis and forwarded to the code development group who converted the data to fit the ALARM-P1 input specifications. Thus both input data are essentially the same except a few modifications which were necessarily made due to difference originating from the modeling used in each codes.

In this chapter, method of input data preparations common for RELAP-4J and ALARM-P1 are described. Furthermore input data modified for ALARM-P1 are mentioned.

3.1 Nodalization

3.1.1 Primary Coolant System

Nodalization used for Ll-4 experiment configuration is the same as the previous nodalization for Ll-2 analysis⁹⁾ except ECC injection line. The selection of nodes and junctions are based on the following principles.

- (1) Volume corresponding to horizontal section of PCS piping is selected in order that homogeneous approximation is appropriate in each volume.
- (2) Vertical section of PCS with relatively large height is given single volume where approximation by simple cylindrical vessel seems adequate.
- (3) No significant change in flow area is allowed inside of each volume, but section with such change is assigned to junction.
- (4) Volume is selected such that instrument location becomes nearly at the center of the volume.
- (5) T connection location such as pressurizer surge line outlet and ECC injection location is selected to be approximately at the center of the volume which the T connection belongs to.

Fig. 3.1 shows noding used for RELAP-4J analysis of Ll-4 experiment. It should be noted that ECC injection line is added in accordance with Ll-4 experiment specifications. Otherwise nodalization of the system is unchanged from Ll-2 analysis. For ALARM-P1 analysis, the same noding is used except numbering of each volume as indicated by the volume with symbol * in Fig. 3.1.

3.1.2 ECCS

Input data used for additional volumes and junctions representing ECC injection line are summarized in Table 3.1. Since relative heights of

injection line including accumulator tank were unknown at the time of the present L1-4 analysis, those data were estimated from the available data in reference 6).

Method of determining volumes and junctions for ECCS shall be described in the following.

(a) Accumulator injection system (ACC)

Fig. 3.2 shows schematic drawing of ACC injection system. The injection system was divided into 3 volumes, ACC tank, injection line between stand pipe inlet and check valve, injection line between the check valve and cold leg injection location. Volume of ACC tank excluding the stand pipe is given in reference 6) as 3.682 m^3 (130 ft^3) and liquid volume in the injection line as 0.3625 m^3 (12.8 ft^3). Since stagnant liquid at nearly PCS fluid condition exists between the check valve and cold leg injection, the stagnant region is accounted by volume 29 and the remaining volume of the injection line is given to volume 30. Junctions for accumulator injection system are junctions 31, 32 and 33, corresponding respectively to cold leg injection location, check valve and stand pipe inlet. Friction coefficients for each junctions are determined as follows.

Junction 31

Since ECC injection piping is much smaller (0.1524 m (6 inches)) than cold leg piping (0.3556 m (14 inches)), sudden expansion is assumed and K_F is calculated as 0.45.

Junction 32

In the check valve, no pressure loss is accounted for, i.e. $K_F = 0.0$.

Junction 33

In order to appropriate account for pressure drop in the ACC injection line, $K_F = 38.5$ based on flow area of $5.723 \times 10^{-3} \text{ m}^2$ (0.0616 ft^2) is used in accordance with the information supplied from NRC.

(b) LPIS

LPIS is represented by fill junction 34 with injection flow rate as the function of system pressure. Initiation of injection is made by trip signal set at 36 sec after break.

(c) HPIS

Fill junction 35 is also given to HPIS. Injection flow rate is assumed constant and injection is initiated by trip signal set at 22 sec after break.

3.2 Initial Fluid Conditions

Initial fluid conditions were determined from actual experimental conditions of L1-4 which was performed on May 4, 1977. The actual conditions as shown in Table 3.2 were informed to the standard problem participants from USNRC which is the responsible organization for performing L1-4 experiment under the guidance of CSNI and those data were used as input data. Since not all of pressure and temperature distribution in PCS were given, they were determined as described in the following.

3.2.1 Pressure Distribution

Pressure distribution in the LOFT system was determined with the help of previous LOFT experiment data of L1-2 and L1-3A. In these tests, pressure difference was measured at several locations as shown in Fig. 3.3. Since flow rate, pressure and temperature of coolant in the primary system were almost identical in L1-2 and L1-3A, the measured pressure difference must be also nearly the same. Fig. 3.4 shows differential pressure distribution in the system based on L1-2 and L1-3A data. It should be noted that smaller orifices were installed in inlet and outlet nozzles of steam generator in case of L1-2 experiment and thus differential pressure across steam generator and pump head are larger in L1-2. However pressure difference between pump outlet to steam generator inlet is nearly the same for L1-2 and L1-3A.

According to L1-4 experiment specifications, larger orifices in steam generator as used in L1-3A are installed and therefore pressure distribution in L1-4 should be similar to L1-3A. In Fig. 3.4 pressure distribution used for the present analysis is shown by solid line. Pressure distribution corresponding to each volume is summarized in Table 3.3, where reference pressure is the measured pressure in pressurizer vessel.

3.2.2 Temperature Distribution

According to measured temperature of L1-3A and L1-4, isothermal temperature distribution was not established as can be seen in Fig. 3.5.

Therefore in the present analysis, temperature distribution was assumed as shown in Fig. 3.5 so that temperature distribution in the system becomes physically realistic. Temperature corresponding to each volume is summarized also in Table 3.3.

3.3 Pump Conditions

Primary circulation pump of the LOFT reactor is a canned rotor pump and two identical pumps are used for coolant circulation. Since detailed pump data are not available other than those given in reference 6), input data were retrieved from the RELAP-4 model used in the LOFT analysis by EG&G¹¹⁾. However the retarding torque equation used in the EG&G analysis is not employed in RELAP-4J and therefore the retarding torque was assumed constant by setting pump speed ratio at initial value.

It should be noted that when actual pump speed of No.1 pump, i.e. 1647 rpm, was used, pressure balance could not be established in the calculation across the pump. Thus initial pump speed was assumed 1679 rpm instead in order to achieve the pressure balance.

Pump data actually used in the present analysis are summarized in Table 4.2 and compared with the data used in the EG&G LOFT analysis.

3.4 Steam Generator Conditions

Steam generator secondary was kept hot standby conditions during experiment. In the present analysis however, steam generator is not considered as a heat source since the effect of steam generator is not significant during blowdown process as discussed in L1-2 analysis⁹⁾.

3.5 ECCS Injection Conditions

3.5.1 Accumulator

As shown in Table 3.2, accumulator was pressurized at 4.3 MPa (613.4 psig) by nitrogen gas and coolant temperature was maintained at 33.3°C (92°F) till injection initiates. These conditions were used as the input data.

3.5.2 HPIS

HPIS initiated coolant injection at 22 sec after break. Injection flow rate and coolant temperature were assumed 1.072 liter/sec (17 gpm) and 33.3°C (92°F), respectively, in accordance with L1-4 experiment specifications.

3.5.3 LPIS

Actual starting time of LPIS pump was 36 sec after break. Injection flow rate depends on injection line pressure as shown in Fig. 3.6. Thus the pressure-flow rate relation was used in the analysis in the form of fill table. Coolant temperature was assumed 33.3°C (92°F) same as HPIS.

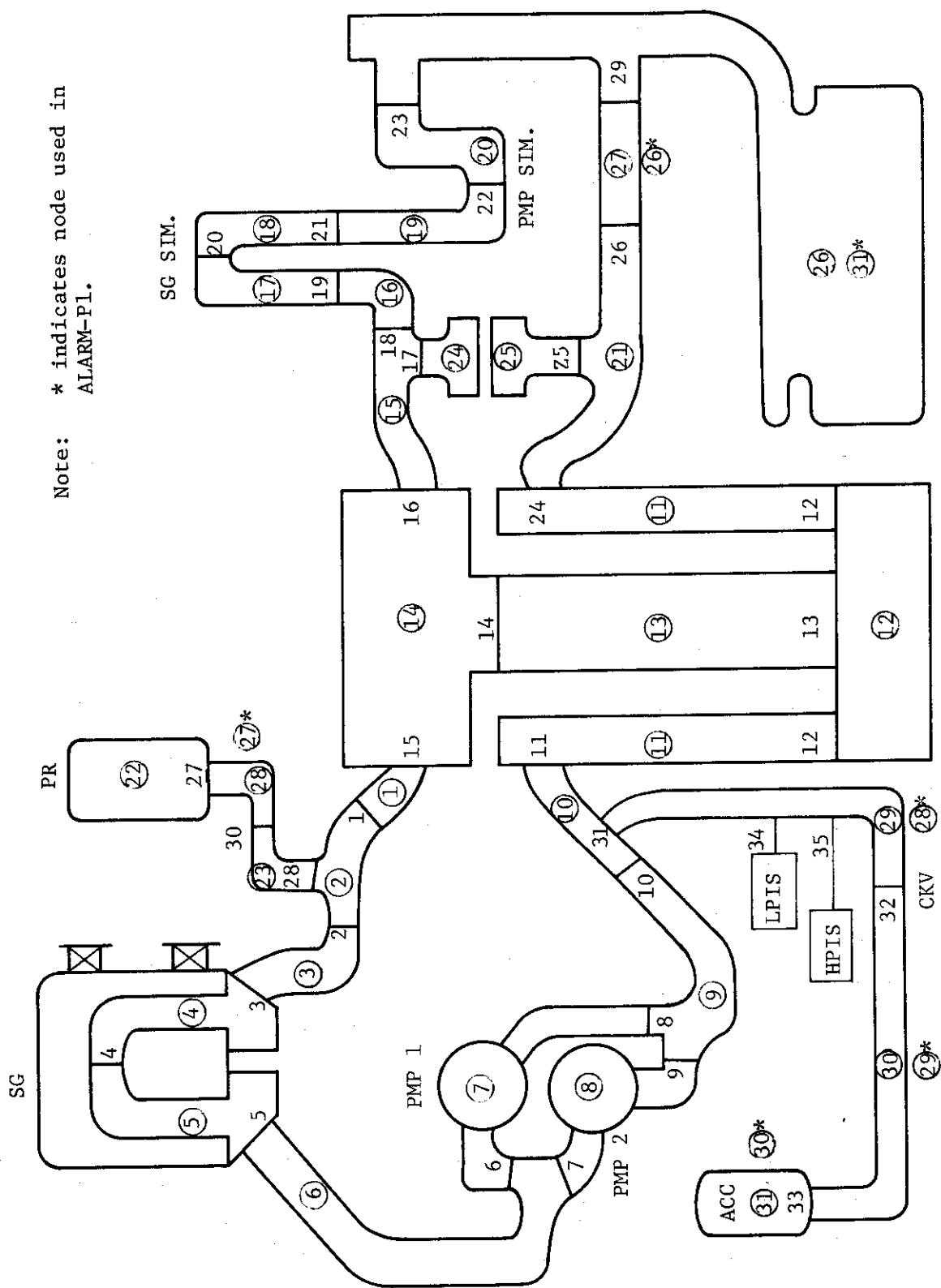


Fig. 3.1 LOFT Noding for L1-4 Analysis

(1) Volume data

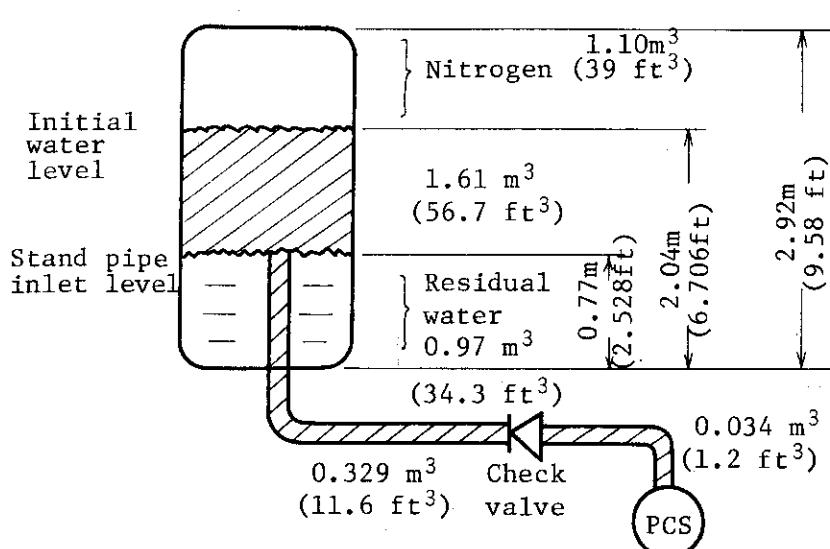
Table 3.1 Volume and Junction Data of ECC Injection Line

| Volume No. | Description | Volume m^3 (ft^3) | Flow Area m^2 (ft^2) | Height m (ft) | Elevation m (ft) | Notes on volume data |
|------------|---|--|---|-------------------|---------------------|-----------------------------|
| 29 | Injection line between check valve to cold leg of the intact loop | 0.034 (1.2) | 0.0062 (0.06681) | 0.044 (0.1458) | 0.142 (0.466) | Estimated from fluid volume |
| 30 | Injection line between the check valve and stand pipe inlet | 0.329 (11.6) | 0.0062 (0.06681) | 0.77 (2.528) | 0.186 (0.6118) | Estimated from fluid volume |
| 31 | Accumulator vessel | 3.68 (130.0) | 1.26 (13.57) | 2.92 (9.58) | 0.186 (0.6118) | |

(2) Junction Data

| Junction No. | Location | Connecting Volumes | | Flow Area m^2 (ft^2) | Elevation m (ft) | Configuration | Form Loss Coefficients | | |
|--------------|-----------------------------|--------------------|----|---|---------------------|-------------------|------------------------|-------|-----------|
| | | From | To | | | | K_F | K_R | K_{RES} |
| 31 | Injection point at cold leg | 29 | 10 | 0.006 (0.0645) | 0.142 (0.466) | Vertical junction | 1.0 | 1.0 | 0.0 |
| 32 | Check valve | 30 | 29 | 0.006 (0.0645) | 0.186 (0.6118) | Vertical junction | 0.0 | 0.0 | 0.0 |
| 33 | Stand pipe inlet | 31 | 30 | 0.0062 (0.06681) | 0.957 (3.1398) | Vertical junction | 38.5 | 38.5 | 0.0 |
| 34 | LPIS injection point | 0 | 29 | 0.006 (0.0645) | 0.164 (0.5389) | Vertical junction | 0.0 | 0.0 | 0.0 |
| 35 | HPIS injection point | 0 | 29 | 0.006 (0.0645) | 0.164 (0.5389) | Vertical junction | 0.0 | 0.0 | 0.0 |

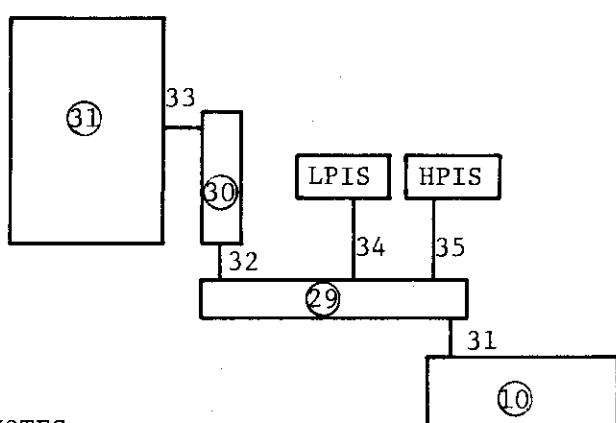
(1) Schematic drawing of ACC injection system



NOTES:

1. Shaded portion of water can be injected.
2. Relative elevation of ACC tank with respect to PCS is unknown.
3. Injection line consists of 4" and 6" pipes.

(2) Node and Junction Representation of ECC Injection System



NOTES:

- ① PCS cold leg
- ② Cold leg to check valve
- ③ Check valve to stand pipe inlet
- ④ Accumulator tank

Fig. 3.2 Accumulator Injection Line

Table 3.2 Initial and Other Conditions from the LOFT L1-4 Test

(1) Initial Conditions

| Item | Instrument Designations | Initial Conditions |
|---|-------------------------|---|
| Intact Loop | | |
| Average Mass Flow Rate | FT-P139-27-1, 2 & 3 | 268.4 kg/s (2.13×10^6 lbm/hr) |
| Pump Speed (each primary coolant pump) | RPE-PC-1 RPE-PC-2 | 1647 RPM 1787 RPM |
| Temperature | | |
| Hot leg near vessel | TE-PC-2 | 279°C (535°F) |
| Steam generator inlet | TE-SG-1 | 281°C (537°F) |
| Steam generator outlet | TE-SG-2 | 279°C (534°F) |
| Cold leg near vessel | TE-PC-1 | 279°C (535°F) |
| Vessel | | |
| Temperature | | |
| Downcomer-Instrument stalk 1 | TE-1ST-2 | 282°C (539°F) |
| Downcomer-Instrument stalk 2 | TE-2ST-2 | 279°C (535°F) |
| Lower Plenum-Instrument stalk 1 | TE-1ST-9 | 282°C (540°F) |
| Lower Plenum-Instrument stalk 2 | TE-2ST-14 | 279°C (535°F) |
| Core Simulator | TE-CS-1 | 279°C (535°F) |
| Broken Loop | | |
| Temperature | | |
| Cold leg near vessel | TE-BL-1 | 279°C (535°F) |
| Cold leg near break plane | TE-P138-170 | 272°C (522°F) |
| Hot leg near vessel | TE-BL-2 | 281°C (537°F) |
| Hot leg near break plane | TE-P138-171 | 272°C (522°F) |
| Pressurizer | | |
| Pressure | Several Measurements | 15.65 MPa gauge (2270 psig) |
| Liquid Volume | LT-P139-6, 7 & 8 | 0.66 m ³ (23.3 ft ³) |
| Gas Volume | LT-P139-6, 7 & 8 | 0.30 m ³ (10.7 ft ³) |
| Steam Generator Secondary | | |
| Pressure | PT-P4-10A | 6.55 MPa gauge (950 psig) |
| Liquid Volume | LT-P4-8B | 3.46 m ³ (122 ft ³) |

Table 3.2 Continued

| Item | Instrument Designations | Initial Conditions | |
|--|-------------------------|---|--|
| Emergency Core Cooling System | | | |
| Accumulator | | | |
| Pressure | PT-P120-43 | 4.14 MPa gauge (601 psig) | |
| Temperature | TE-P120-41 | 33°C (92°F) | |
| Gas Volume | LIT-P120-44 | 1.16 m ³ (41 ft ³) | |
| Injected Liquid Volume | LIT-P120-44 | 2.05 m ³ (72.3 ft ³) | |
| Pumped ECC | | | |
| Temperature of Borated Water Storage Tank (BWST) | TE-P120-1 | 26°C (78°F) | |

(2) Other Conditions

| | |
|-----------------------------------|-------------|
| Time of primary coolant pump trip | T = 0 sec |
| Time of HPIS initiation | To + 22 sec |
| Time of LPIS valved in | To + 36 sec |

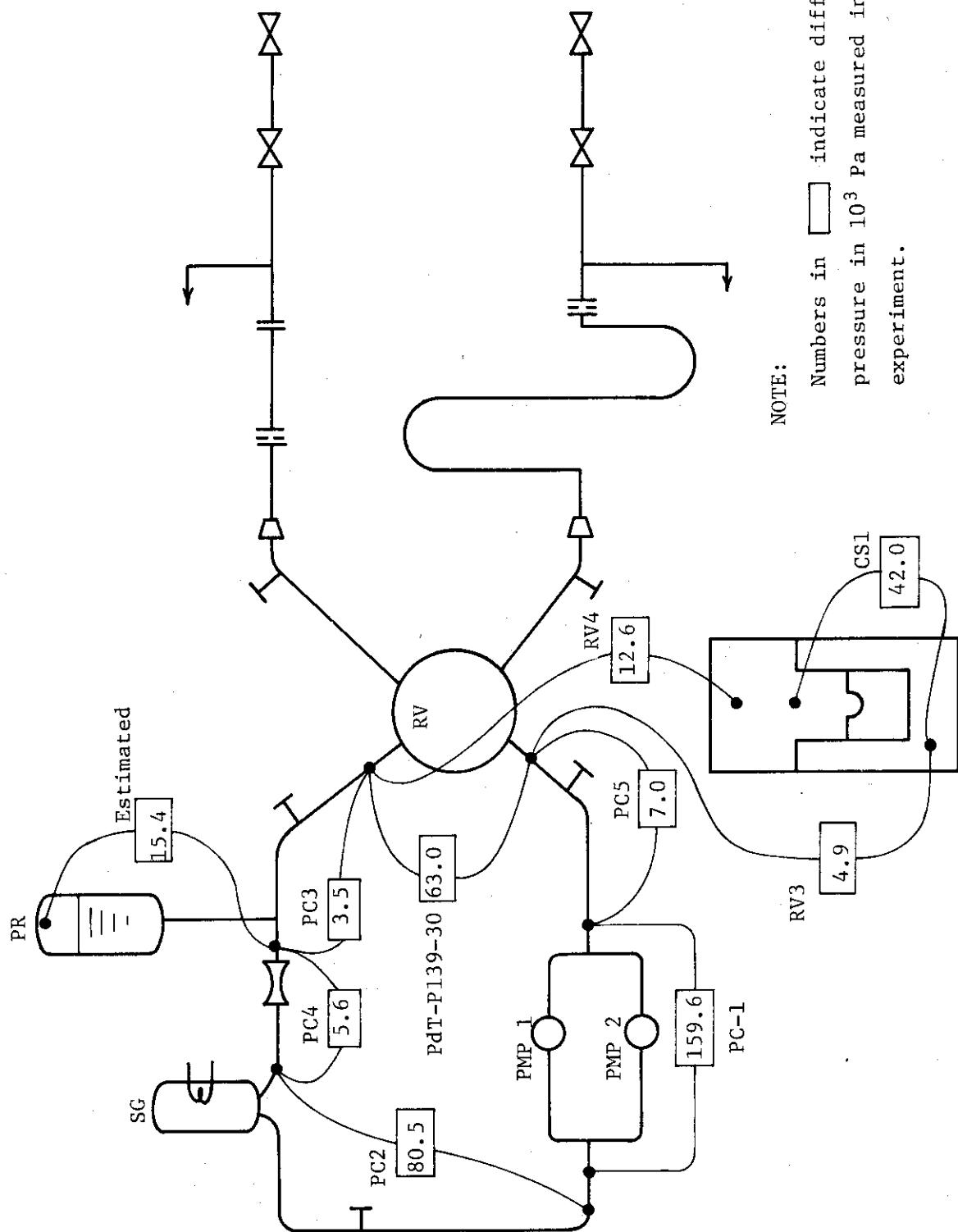


Fig. 3.3 L1-3A Initial Differential Pressure

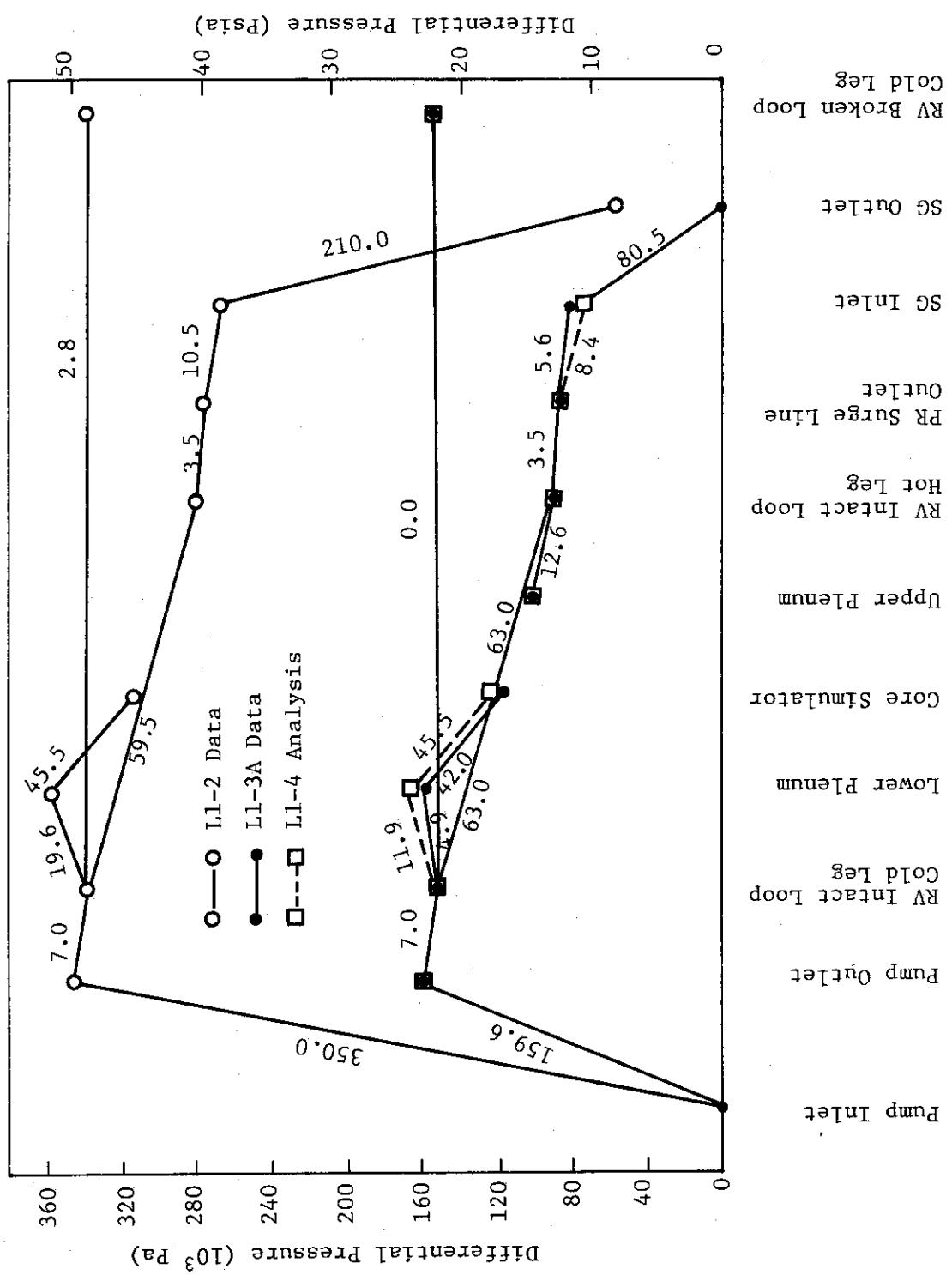


Fig. 3.4 Differential Pressure Distribution in PCS

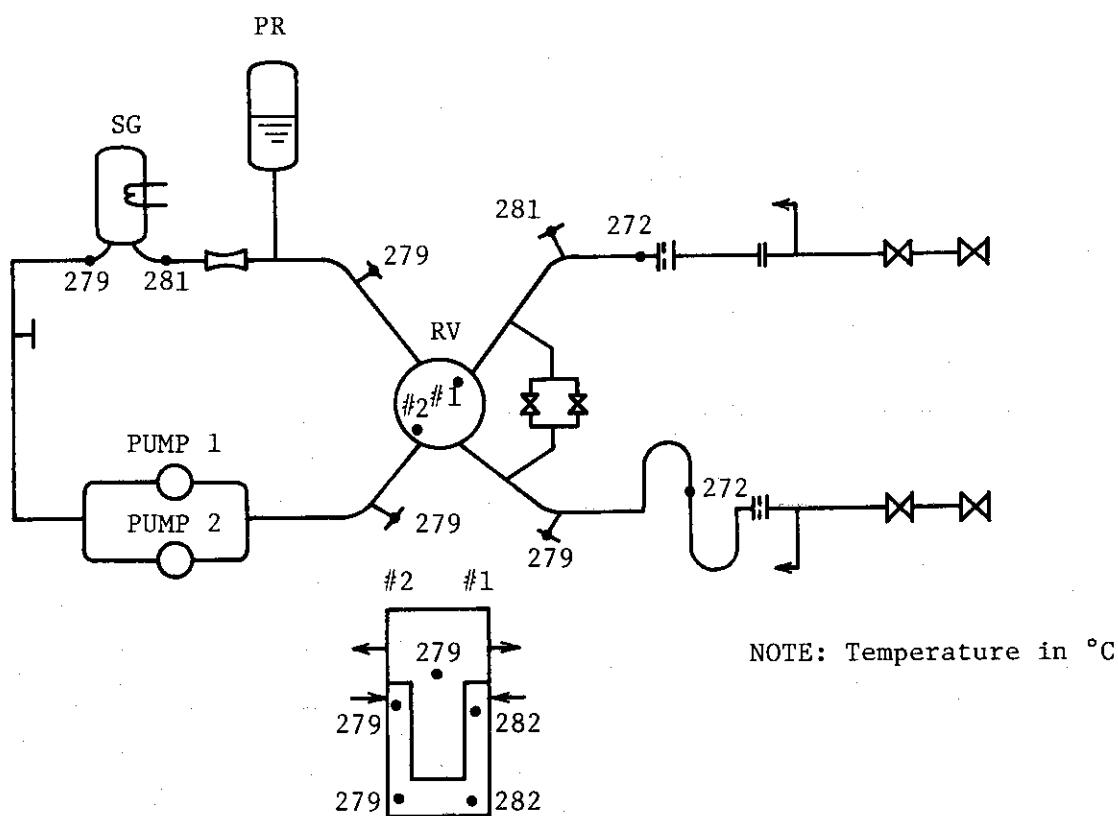


Fig. 3.5 Initial Temperature Distribution in PCS

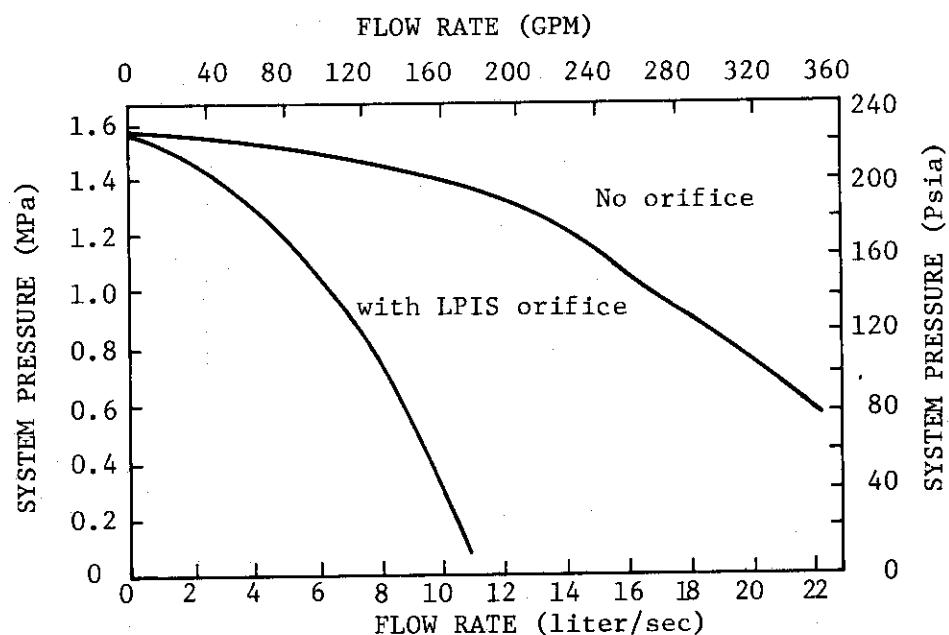


Fig. 3.6 LPIS Injection Flow Rate

Table 3.3 Initial Pressure & Temperature Distribution for L1-4

| Components | ΔP | Psia | $^{\circ}\text{F}$ | Vol.# | Notes |
|--------------------------------|------------|--------|--------------------|----------|--------------------|
| Pressurizer (Vapor) | +1.4 | 2282.4 | | | See note below (1) |
| PR surge line center | +1.1 | 2283.2 | | | See note below (1) |
| PR inlet downstream | -1.2 | 2284.9 | 536 | (2) | |
| SG inlet after reducer | -3.5 | 2283.7 | 537 | (3) | |
| SG riser center | -3.5 | 2280.2 | 536 | (4) | |
| SG Top | -3.5 | 2276.7 | | | |
| SG downcomer center | -3.5 | 2273.2 | 535 | (5) | |
| SG outlet | +1.3 | 2269.7 | | | |
| SG outlet piping | +1.3 | 2271.0 | 534 | (6) | |
| SG outlet at loop seal | | 2272.3 | | | |
| Pump No.1 & No.2 | +23.1 | 2285.1 | 535 | (7), (8) | |
| Pump outlet | -0.5 | 2295.4 | | | |
| Cold leg center | -0.5 | 2294.9 | 535 | (9) | |
| Cold leg near RV | +0.8 | 2294.4 | 535 | (10) | |
| Downcomer center | +0.9 | 2295.2 | 537 | (11) | |
| Lower plenum 24" above | +0.4 | 2296.1 | | | |
| Lower plenum center | -3.4 | 2296.5 | 537 | (12) | |
| Core center | -3.5 | 2293.1 | 536 | (13) | |
| Core simulator center | -2.4 | 2289.6 | | | |
| Upper plenum center | -1.8 | 2287.2 | 535 | (14) | |
| RV outlet (intact) hot leg | 0.0 | 2285.4 | 535 | (1) | |
| Blowdown loop hot leg | -1.5 | 2285.4 | 535 | (15) | |
| SG simulator (riser) | -1.5 | 2283.9 | 535 | (16) | |
| SG simulator (Top) | +3.0 | 2282.4 | 530 | (17) | |
| SG simulator to pump simulator | +3.1 | 2285.4 | 530 | (18) | |
| Pump simulator | -3.1 | 2288.5 | 525 | (19) | |

Table 3.3 Continued

| Components | ΔP | Psia | $^{\circ}F$ | Vol. # | Notes |
|-----------------------------------|-----------------|--------|-------------|--------|-------|
| Discharge pipe | -3.1 | 2285.4 | 522 | (20) | |
| Reflood assist line hot leg side | -0.9 from BL HL | 2284.5 | 530 | (24) | |
| Reflood assist line cold leg side | -0.9 from BL CL | 2293.5 | 530 | (25) | |
| Blowdown loop cold leg | 0.0 | 2294.4 | 537 | (21) | |
| Blowdown nozzle | | 2266.4 | 522 | (27) | |
| Suppression tank | | 13.8 | 183 | (26) | |

Note: (1) PR surge line is divided into two volumes:

| Components | ΔP | Psia | $^{\circ}F$ | Vol. # | Notes |
|-------------------|------------|--------------------|--------------|--------|-------|
| PR : top | +0.4 | 2282.4 | 654 | | |
| Center | +0.5 | 2282.8 | 649 | (22) | |
| Bottom | +0.5 | 2283.3 (2283.6) | 644 (608) | (28) | |
| Surge line center | +1.1 | 2283.8 (2284.4) | (572) | (23) | |
| Surge line outlet | | | | | |

(2) Gauge pressure based on 12.4 psia at atmospheric pressure

(3) ECC injection line

| | Psia | $^{\circ}F$ | Vol. # | Notes |
|--|--------|-------------|--------|-------|
| ECC Injection line (Same as vol. (10) operating loop cold leg) | 2294.4 | 490 | (29) | |

4. COMPARISON OF MODELS USED FOR L1-4 ANALYSIS BY RELAP-4J AND ALARM-P1

For the present L1-4 prediction, two codes are used, namely RELAP-4J and ALARM-P1. RELAP-4J⁸⁾ is a JAERI's modified version of RELAP-4 Mod 2¹²⁾ and ALARM-P1¹⁰⁾ is an EM based PWR-LOCA analysis code developed at JAERI by the code development group. Both codes are basically of similar type, i.e. a one dimensional node junction type loop code. However physical models used in RELAP-4J and ALARM-P1 are slightly different and those difference would lead to different performance characteristics of each codes. Major differences in physical models used for L1-4 analysis are summarized in Table 4.1 and are compared in the following.

4.1 Numerical Method

Fully implicit method was used in the present RELAP-4J analysis although RELAP-4J is capable of performing fully explicit method as well. ALARM-P1 on the other hand employs fully explicit method to solve the set of governing equations because of its unmatured stage of development. Therefore computational time of ALARM-P1 is approximately 3 times longer than that of RELAP-4J in the present case mainly due to smaller time steps associated with explicit method.

4.2 Discharge Model

RELAP-4J allows the use of C_D correlation⁸⁾ in the form of

$$C_D = 0.57 + \frac{0.002}{\text{Junction Quality}}$$

for the discharge coefficient associated with the Moody model when critical flow is detected. Use of the C_D correlation results in larger flow in the range of smaller junction quality in consistence with experimental results.

ALARM-P1 employs the Zaloudek equation¹³⁾ and the Moody model for discharge flow calculation. The Zaloudek equation is used when stagnation quality is less than 2% and smoothly connected to the Moody model which is used in quality range above 2%. The following modification of the Zaloudek equation is made for the smooth transition.

$$G = C_1 \sqrt{2g_c p (P - C_2 P_{sat})}$$

where $C_1 = \frac{C_{Moody}}{\sqrt{2g_c p P_{sat} (1 - C_2)}}$

C_2 : input constant ($0.5 < C_2 < 1.0$)

$C_2 = 0.85$ in the present analysis

G_{Moody} : Critical mass velocity calculated from the Moody model corresponding to $x = 0.0$ and P_{sat}

ρ : Density

P_{sat} : Saturation pressure

P : Pressure

g_c : gravitational constant

In the present analysis, the discharge coefficient for the Moody model was chosen as 0.6.

The above discharge models were applied to those junctions where two phase critical flow is expected to occur, i.e. pressurizer surge line outlet and break planes.

4.3 Phase Separation Model

According to L1-2 analysis, results were sensitive to phase separation in volume having relatively large height such as steam generator, downcomer, upper plenum and pressurizer. Therefore phase separation was assumed in the volumes corresponding to those components.

Phase separation in RELAP-4J can be calculated by using either constant bubble rise velocity with gradient of bubble density or bubble rise velocity determined by the Wilson model. The Wilson model was used in the present analysis in pressurizer and accumulator vessel and constant bubble rise velocity of 0.9 m/sec (3 ft/sec) with gradient of 0.8 was assumed in downcomer, upper plenum, steam generator inlet side and suppression tank.

Since the Wilson model is not used in ALARM-P1, constant bubble rise velocity of 0.9 m/sec with density gradient of 0.8 was employed in those volumes where phase separation was assumed in RELAP-4J.

4.4 Pump Model

Pump model used in RELAP-4J is the standard pump model employed in RELAP-4 and based on pump performance characteristics curve which is given as input data table. Two-phase effects on a pump can be considered by the use of two-phase option.

In ALARM-P1, pump behavior is solved by the homologous law and a set of input characteristic curves. Required curves are Q-H, n-H, n- τ and Q- τ

relations at the rating and the reversal flow and rotation conditions. When cavitation is expected, the pump head and hydraulic torque are modified as follows;

$$\Delta P' = \Delta P - \sigma X_e,$$

$$T_h = T_h - \sigma X_e W / \omega_p$$

where

ΔP = Uncavitated pump pressure rise

T_h = Uncavitated hydraulic torque

$\Delta P'$ = Cavitated pump pressure rise

T_h' = Cavitated hydraulic torque

σ = Cavitation constant (input data)

X_e = Quality at impeller eye

W = Mass flow rate

ω = Angular velocity

The frictional torque is neglected during coast down.

In the present ALARM-P1 calculation, the cavitation constant σ of 10^{-3} kg/m² was used because data of the pump behavior used in the LOFT L1-4 experiment was not clear. Therefore in the ALARM-P1 calculation, the cavitation was actually neglected.

It should be noted that the ALARM-P1 pump model is not provided with two phase option such as that used in RELAP-4J. Thus the result of ALARM-P1 is always based on single phase pump characteristics.

4.5 Heat Slab

Heat slab was considered in RELAP-4J and ALARM-P1 only in downcomer where hot wall effect may become significant during later portion of blow-down. However the L1-2 analysis indicated that effect of heat slab is not significant and addition of heat slab to downcomer volume did not alter the results. Hence heat transfer to steam generator secondary was neglected in the present analysis.

4.6 Momentum Flux Option

Momentum flux was taken into account for all junctions in RELAP-4J analysis although one dimensional momentum flux calculation seems unreasonable for a T shaped connections such as ACC injection location. Thus

ALARM-P1 analysis did not employ one dimensional momentum flux option to ACC injection location, Junction 31, and for all other junctions including pressurizer surge line, one dimensional momentum flux option was used as trial basis.

4.7 Two Phase Friction Multiplier

Two phase friction multiplier is calculated in RELAP-4J by the use of the Baroczy correlation¹⁴⁾ while the Thom¹⁵⁾ and the Martinelli-Nelson¹⁶⁾ correlation are used in ALARM-P1 in the form of a built-in table.

Table 4.1 Comparison of Models Used in RELAP-4J and ALARM-P1

| Items | RELAP-4J | ALARM-P1 |
|-------------------------------|---|---|
| Numerical Method | Fully implicit method (also capable of explicit method) | Fully explicit method |
| Discharge Model | $x > 0.0$ Moody with C_D correlation, i.e. $C_D = 0.57 + \frac{0.002}{\text{Junction Quality}}$ | $x > 0.02$ Moody $x \leq 0.02$ Zaloudek |
| Phase Separation Model | Bubble rise velocity Wilson correlation or $V_B = 3.0 \text{ ft/sec}$ Bubble density gradient $C = 0.8$ | Bubble rise velocity $V_B = 0.9 \text{ m/sec}$ Bubble density gradient $C = 0.8$ |
| Pump Model | RELAP-4 Model in INEL L1-4 Analysis | ALARM-P1 standard pump model, No Two Phase Option |
| Heat Slab | Considered only in downcomer | Same as RELAP-4J Analysis |
| Two Phase Friction Multiplier | Baroczy | Thom and Martinelli-Nelson |

Table 4.2 Comparison of Pump Data

| | | RELAP-4J | L1-2 | L1-3 | L1-4 |
|--|--------|----------|---------|---------|----------|
| Speed ratio | Pump 1 | 0.48 | 0.6324 | 0.5584 | 0.488993 |
| | Pump 2 | 0.506 | 0.6324 | 0.5584 | 0.5 |
| Rated Speed (RPM) | | 3530 | 3530 | 3530 | 3530 |
| Rated Head (ft) | | 408.95 | 350.0 | 306.0 | 408.95 |
| Rated torque(ft·lb _f) | | 465.0 | 465.0 | 465.0 | 465.0 |
| Mom of Inertia (lb _m ·ft ²) | | 340.0 | 521.0 | 294.0 | 340.0 |
| Rated Density (lb _m /ft ³) | | 38.75 | 38.75 | 38.75 | 38.75 |
| Initial Fric. Torque | Pump 1 | 40.0522 | 65.10 | 75.96 | 40.0522 |
| | Pump 2 | 46.529 | 65.10 | 75.96 | 46.529 |
| Pressure (psia) | Pump 1 | 2286.0 | 2254.8 | 2263.98 | 2265.47 |
| | Pump 2 | 2285.1 | 2256.0 | 2265.33 | 2266.98 |
| Rated Flow (GPM) | | 5000 | 5000 | 5000 | 5000 |
| Mass flow (lb _m /hr) | Pump 1 | 295.9 | 307.722 | 307.722 | 300.657 |
| | Pump 2 | 295.8 | 289.5 | 289.5 | 296.565 |

5. RESULTS AND DISCUSSIONS OF RELAP-4J AND ALARM-P1 CALCULATIONS

LOFT L1-4 experimental results were predicted by using RELAP-4J and ALARM-P1 with input data described in the previous chapter. Those input data including initial conditions for L1-4 are listed Appendices 1 and 2 as exactly the same format as those sent to USNRC.

In the present chapter, results of both analyses shall be discussed in terms of coolant behavior and ECC water in each component of the LOFT reactor and comparison of the two results shall be presented with emphasis on the difference in the models used in each computer codes. Results of the calculations are listed in Appendices 3 and 4 at selected time steps in compliance with the standard problem specifications.

5.1 Broken Loop Cold Leg

Fig. 5.1 shows calculated discharge flow rates through the break by RELAP-4J and ALARM-P1 and it is apparent that both results are in good agreement although different models were used in low quality range, i.e. the Moody model with the C_D correlation in RELAP-4J and the Zaloudek equation in ALARM-P1. In the figure, as well as all other figures, A stands for ALARM-P1 results and R for RELAP-4J. In the quality range above 0.02 the Moody model was used in ALARM-P1 with $C_D = 0.60$ while the C_D correlation in RELAP-4J yields 0.58 at quality of 0.02. This difference is not significant and both calculations should give nearly identical flow rate when input value for the Moody model are consistent. It should be noticed in Fig. 5.1 that slight flow rate recovery is calculated at 6.5 sec and 7.5 sec respectively in RELAP-4J and in ALARM-P1. The recovery corresponds to mixture level rise in downcomer. Fig. 5.2 shows junction flow from reflood assist line to broken loop cold leg and it indicates that calculated flow in ALARM-P1 shows oscillatory behavior with decreasing amplitude for initial 8 sec until initiation of the inflow from the reflood assist line. Oscillatory flow is also seen in RELAP-4J calculation. However the oscillation is observed only during the period of coolant inflow from reflood assist line into cold leg. The oscillation observed during initial 8 sec in ALARM-P1 calculation is associated with numerical technique used in ALARM-P1. It is usually true that explicit method often results in unstable calculation. It can be seen in Fig. 5.2 that the oscillation is symmetrical with medium value at zero flow. The fluctuation disappears at 8 sec after break corresponding to initiation of flashing in

reflood assist line.

Flow rate at the reflood assist line outlet calculated by RELAP-4J becomes extremely unstable after 52 sec as can be seen in Fig. 5.2. This unstable fluctuation is also observed in calculated density in Fig. 5.3. This oscillatory flow corresponds to the mixture level in downcomer. The downcomer mixture level increases as injected ECC water accumulates in lower plenum and downcomer. Calculated mixture level shows that the mixture level reaches to the top of cold leg nozzle at 52 sec after break and the nozzle is covered by two phase mixture. Thus coolant flow from downcomer to broken loop cold leg becomes extremely low quality flow resulting in sudden increase of coolant density in the cold leg. Calculated results then becomes unstable.

Pressure transients in cold leg of the broken loop agree reasonably well between the two calculations except in the later period of blowdown as can be seen in Fig. 5.4. Pressure in RELAP-4J decreases slightly faster than ALARM-P1 due to larger discharge flow rate at the break plane defined as the exit of discharge nozzle.

Calculated temperature is also presented in Fig. 5.4. Since temperature shows saturation temperature corresponding to system pressure, lower temperature is predicted in RELAP-4J in accordance with lower predicted pressure.

Density in cold leg is shown in Fig. 5.3. It can be seen that density in ALARM-P1 stays nearly the same until 6.5 sec and then suddenly drops while density calculated by RELAP-4 smoothly decreases and at 6.5 sec it becomes almost same density calculated by ALARM-P1. Higher density calculated by ALARM-P1 during initial 6.5 sec is due to early flow reversal in intact loop hot leg. The reverse flow causes decrease in positive flow at core inlet and it leads to increase in flow rate at downcomer outlet to broken loop cold leg. The difference is originated in smaller flow rate calculated in ALARM-P1. The density recovery calculated around 6~7 sec is due to mixture level rise in downcomer. Following ECC injection, density in RELAP-4J decreases slower than ALARM-P1. The slower decrease corresponds to larger amount of coolant inflow from downcomer into broken loop cold leg.

Slight difference between RELAP and ALARM calculation is observed in differential pressure across break planes in Fig. 5.5. The difference arises from definition of total differential pressure at junction, i.e. total differential pressure in ALARM-P1 is defined as difference between

pressures in adjacent volumes while total differential pressure includes pressure loss due to momentum flux change in RELAP-4J. Thus the difference between two calculations indicates magnitude of momentum flux term.

5.2 Broken Loop Hot Leg

Discharge flow rate from hot leg of the broken loop shows excellent agreement between RELAP-4J and ALARM-P1 as can be seen in Fig. 5.6. Agreement in calculated pressure is also satisfactory as shown in Fig. 5.7. Slight difference in calculated temperature is noticed in Fig. 5.7 corresponding to difference in calculated pressure in later portion of blow-down as discussed in the previous section.

Calculated density is presented in Fig. 5.8 and good agreement is noticed. Density recovery at 15 sec after break corresponds to the end of coolant discharge from pressurizer. As soon as pressurizing effect is stopped reverse flow from steam generator inlet in intact loop hot leg occurs and large amount of coolant trapped in the steam generator flows into the upper plenum. At the same time, core flow becomes positive flow. The positive flow results in increase of mixture level in the upper plenum to reach the hot leg nozzle and thus density in the hot leg increases.

Fig. 5.9 shows coolant flow from reflood assist line. The initiation of coolant inflow to hot leg calculated by RELAP-4J is slightly earlier than ALARM-P1. However difference is not significant. Prior to the initiation of inflow, oscillation is observed in ALARM-P1 result as also seen in broken loop cold leg. The oscillation is due to numerical method used in ALARM-P1. Differential pressure across steam generator simulator and pump simulator are in good agreement as shown in Fig. 5.10.

5.3 Intact Loop Cold Leg

Junction flow at the downcomer inlet from intact loop cold leg is shown in Fig. 5.11. Agreement between RELAP-4J and ALARM-P1 is satisfactory except initial few seconds during which junction flow at the downcomer inlet calculated by RELAP-4J is larger than that of ALARM-P1. The reason is that lower flow rate is predicted during this period in ALARM-P1. The junction flow starts decreasing at 22 sec corresponding to coolant injection into cold leg. It should be noticed that effect of coolant injection is not predicted immediately following ACC injection initiation, but there is delay of a few seconds due to the existence of small volume

(volume 29). The volume represents small region between cold leg injection location and check valve where coolant initial condition is approximately same as primary system coolant. Thus injected coolant from ECCS first fills the small volume and then flows into cold leg. It takes a few seconds to fill the volume by injected coolant.

Sudden flow recovery at 25 sec corresponds to sharp temperature drop in cold leg as shown in Fig. 5.12, indicating that coolant in cold leg is all condensed and it becomes subcooled single phase liquid.

Junction flow at junction 10 represents flow rate between ECC injection location and pump discharge outlet, and the result is shown in Fig. 5.13. It should be noticed in Fig. 5.13 that noticeable oscillation appears in ALARM-P1 calculation between 25 sec and 36 sec. The oscillation corresponds to the period in which coolant temperature sharply drops to subcooled temperature indicating that cold leg is being filled by injected water. Presence of subcooled water in the system seems to result in unstable calculation in case of ALARM-P1.

The oscillation is also observed in pressure transient in Fig. 5.12. Except the oscillatory behavior between 26 sec and 38 sec, calculated results agree extremely well.

Fig. 5.14 shows average density and quality in intact loop cold leg. It can be seen that average density of ALARM-P1 is higher than that of RELAP-4J indicating effect of difference in calculated pump flow. During initial 3 sec, ALARM-P1 predicts constant density corresponding to single phase flow while RELAP-4J predicts two phase mixture after 2 sec. Faster cooldown predicted by ALARM-P1 results in smaller flow rate than RELAP-4J. Therefore coolant in volume 10 stays larger in ALARM-P1 to result in higher density.

5.4 Intact Loop Hot Leg

Junction flow at junction 1 shows different behavior between RELAP-4J and ALARM-P1 as can be seen in Fig. 5.15. During initial 3 seconds, RELAP-4J result indicates relatively large positive flow while ALARM-P1 result shows flow reversal at 1.5 sec. From 3 to 12 seconds, both flow rates are almost identical. Larger negative flow with the peak at 16 sec is noticed in ALARM-P1 while no such flow is observed in RELAP-4J.

Fig. 5.16 shows junction flow at junction 2 representing coolant flow between pressurizer surge line outlet and steam generator inlet. It is noticed that flow direction calculated by both codes is positive until 12

sec corresponding to the end of coolant discharge from pressurizer. Coolant flow is reversed after 12 sec and the flow again becomes positive after 30 sec due to condensation effect propagating through steam generator where no heat slab is considered. In experimental situation, steam generator would act as heat source and condensation effect may not be present in hot leg in later portion of blowdown. By comparing junction flows at junctions 1 and 2, it is apparent that coolant from pressurizer flows into two directions, i.e. toward steam generator and upper plenum after 1.5 sec in ALARM-P1 and after 3 sec in RELAP-4J. Positive flow toward steam generator inlet disappears when coolant discharge from pressurizer is discontinued at 12 sec after break. Then reverse flow takes place as indicated by junction flow at junction 2. It is noticed that the reverse flow calculated by ALARM-P1 has peak at 15 sec while RELAP-4J result shows smooth curve. The reason is that negative flow calculated by ALARM-P1 is much larger than RELAP-4J due to earlier occurrence of flow reversal which leads to larger accumulated coolant in steam generator inlet.

Junction flow at junction 3 (SG inlet) in Fig. 5.17 is similar to junction flow at junction 2. Both results indicate that positive flow is maintained until the end of coolant discharge from pressurizer. Junction flow at junction 5 (SG outlet) is presented in Fig. 5.18 and reasonably good agreement is observed. It can be seen that steam generator outlet flow is positive throughout transient. Therefore flow direction is separated inside the steam generator as indicated by junction flow rate at steam generator top in Fig. 5.19.

Junction flow at upper plenum inlet from intact loop hot leg is shown in Fig. 5.20. Positive flow lasts for 3.5 sec after break in RELAP-4J calculation while flow reversal occurs at 1.5 sec after break in ALARM-P1. The negative peak at 16 sec observed in ALARM-P1 result is moderated at junction 15.

Discharge flow from pressurizer surge line to hot leg is shown in Fig. 5.21. Both flow rates are nearly the same throughout transient. It should be noticed that sudden drop in flow rate observed at 10.6 second in ALARM-P1 result indicates rapid transition corresponding to the end of two phase discharge. On the other hand RELAP-4J calculation shows relatively smooth transition. The sudden change is also observed in ALARM-P1 result at 20 sec corresponding to transition to steam flow and the result is questionable as compared to RELAP-4J result.

Density in hot leg is shown in Fig. 5.22. During initial 3~4 sec, RELAP-4J predicts higher density than ALARM-P1 in accordance with large positive flow. Further decrease at 12 sec is direct result of the end of coolant discharge from pressurizer and the recovery is due to reverse flow from steam generator. The timing of the recovery is earlier in ALARM-P1 as also noticed by flow rates at junction 2.

Pressure and temperature in hot leg are in good agreement as shown in Fig. 5.23.

5.5 Reactor Vessel

5.5.1 Upper Plenum

Junction flow at junction 15 represents coolant flow out of upper plenum to intact loop hot leg as shown in Fig. 5.24. It can be seen that in RELAP-4J calculation, coolant flow is positive during first 3.5 sec indicating coolant outflow from upper plenum to hot leg. In ALARM-P1 calculation on the other hand, positive flow lasts only 1.5 sec and the flow is reversed. The difference in the timing of flow reversal is due to the difference in the pump flow rate as discussed in 5.4. Positive flow after 36 sec in both calculations corresponds to mixture level rise in upper plenum indicating positive core flow.

Fig. 5.25 represents junction flow at junction 16 corresponding to coolant discharge out of upper plenum to broken loop hot leg. Both flow rates agree quite well with exception that noticeable oscillatory behavior is observed in RELAP-4J calculation. Extremely low flow rate between 6.5 sec and 15 sec corresponds to the period during which the mixture level in upper plenum drops below the hot leg nozzle level due to reverse core flow as can be seen in Fig. 5.26. The mixture level recovers when coolant discharge from pressurizer surge line terminates at 12 sec after break and trapped coolant in steam generator inlet-side flows into upper plenum. At the same time, core flow becomes positive again. It should be noticed that the mixture level calculated by ALARM-P1 drops much lower than the hot leg nozzle while RELAP-4J prediction shows the mixture level stays within the nozzle inlet region. The difference is due to large negative flow at junction 15 calculated by ALARM-P1 so that flow at the core outlet to upper plenum becomes negative flow in order to balance coolant flow in upper plenum.

Junction flow at junction 14 is shown in Fig. 5.27 representing coolant

flow from core simulator into upper plenum. Negative flow between 5~12 sec corresponds to period during which the mixture level drops below the hot leg nozzle in ALARM-P1 or near the bottom of the hot leg nozzle in RELAP-4J. The junction flow shows almost stagnant flow from 8 to 10 sec in RELAP-4J calculation while ALARM-P1 result indicates that negative flow is maintained. Junction flow recovers at 12 sec corresponding to the end of coolant discharge from pressurizer. Flow rates are in good agreement after 12 sec.

Good agreement is observed in pressure and temperature claculation as shown in Fig. 5.28.

5.5.2 Core Simulator

Fig. 5.29 shows junction flow at junction 13 representing coolant flow into the core simulator from lower plenum. Both calculations are in good agreement except during early 3 sec in which RELAP-4J results in larger flow rate in consistent with the fact that positive flow is maintained in this duration. After 3 sec, junction flow at core simulator inlet becomes negative and negative flow lasts a little after the end of coolant discharge from pressurizer. As soon as pressurizer becomes empty, coolant flow from upper plenum to lower plenum through core simulator is weakened and at the core simulator inlet flow becomes stagnant.

Coolant flow out of core simulator into upper plenum is presented in Fig. 5.30. As discussed in the previous section, large negative coolant flow is seen in ALARM-P1 calculation during 5~12 sec while RELAP-4J indicates stagnant flow.

By comparing junction flows at junctions 13 and 14, coolant flow is initially positive in the core simulator during first 2~3 seconds and then flow is reversed. The reverse flow is maintained until the end of coolant discharge from pressurizer at 12 sec. Then coolant flows out of core simulator through junction 13 as well as junction 14 indicating existence of stagnant region in the core simulator.

Pressure and temperature in the core simulator is shown Fig. 5.31 and calculated pressure is slightly lower in RELAP-4J and so is calculated temperature.

5.5.3 Lower Plenum

Lower plenum has two junctions, connecting to either downcomer or core simulator. Junction 12 represents flow from downcomer to lower plenum and

the result is shown in Fig. 5.32. It should be noticed that oscillatory behavior is significant in both calculations especially in RELAP-4J calculation. During initial 3 seconds, junction flow is positive and then both flow becomes negative in both cases. The junction starts oscillating at 25 sec lasting up to 38 sec in ALARM-P1 calculation while RELAP-4J calculation shows no such oscillation. After 43 sec, however, RELAP-4J calculation shows large oscillation indicating flow oscillation in the downcomer indirectly receiving injection effect. The effect of the oscillatory behavior is not seen in the junction flow from lower plenum to core because, due to the assumption of phase separation in downcomer, junction flow at the bottom of downcomer to lower plenum is based on properties of two phase mixture below the mixture level and the properties of the two phase mixture is relatively unaffected by the large oscillation of mixture level.

Pressure and temperature are in good agreement, as shown in Fig. 5.33.

5.5.4 Downcomer

Downcomer outlet flow into lower plenum is shown in Fig. 5.32 in the previous section. It can be seen that the outlet flow into lower plenum is in fairly good agreement except oscillatory behavior observed in ALARM-P1 calculation around 30 sec and also appeared in RELAP-4J calculation at 42 sec as discussed in the previous section.

The inlet flow from cold leg of the intact loop into downcomer is shown in Fig. 5.34. It should be noticed that during initial 2-3 sec, flow rate is larger in RELAP-4J calculation while ALARM-P1 result shows slightly smaller flow rate. At 23 sec after break, both flow rates rapidly decrease and suddenly recover at 25 sec. The recovery corresponds to the end of condensation in volume 10 as discussed in 5.3.

Flow rate from the downcomer to the broken loop cold leg is represented by junction flow at junction 24 and the result is shown in Fig. 5.35. The flow is always positive throughout the transient and it should be noticed that RELAP-4J calculation shows oscillatory behavior with considerably large magnitude during 5 to 15 seconds after break. It may be the direct effect of level rise in the downcomer.

The downcomer mixture level is shown in Fig. 5.36 and the mixture level calculated by the RELAP-4J model rises between 5 and 10 sec and becomes stable at 10 second and after. The level rise is also calculated by RELAP-4J after 50 sec. The second level rise is however a questionable

prediction since unreasonable flow oscillation is calculated in this period in broken loop cold leg.

Pressure and temperature in the downcomer are in good agreement as similar to other calculated results as shown in Fig. 5.37.

5.6 Pressurizer

Pressurizer pressure is shown in Fig. 5.38 and it can be seen that pressure transient during early period agrees well between the two calculations. However after 20 sec, pressure calculated by ALARM-P1 is higher than that of RELAP-4J. Bent appeared at 12 sec corresponds to the end of coolant discharge from pressurizer due to the fact that mixture level in pressurizer reaches to the bottom of the pressurizer vessel and the discharge flow becomes simply single phase flow of steam. A sharp change in flow rate is observed at 20 sec after break for the ALARM calculation and it is associated with calculation model at junction as discussed in 5.3.

The mixture level in the pressurizer vessel is shown in Fig. 5.39. As can be seen in the figure, mixture level decreases with almost the same rate in both RELAP and ALARM calculations. It seems that effect of difference in modeling is not significant with respect to the mixture level calculation in this case. The discharge flow from the pressurizer surge line outlet to hot leg is shown in Fig. 5.40 and flow at pressurizer surge line inlet is shown in Fig. 5.41. Both flow rates are nearly identical except that sharp change in the flow rate is observed in ALARM-P1 calculation at 10.6 sec as discussed in 5.3. Junction flow at surge line inlet shows unstable flow at 10.6 sec corresponding to the end of coolant discharge. It is due to the ALARM-P1 model to calculate junction flow at junction connected to volume where phase separation model is assumed as also discussed in 5.3.

5.7 Pump

Pump coastdown curve is presented in Fig. 5.42. It can be clearly seen that pump coastdown predicted by ALARM-P1 is much faster than that of RELAP-4J corresponding to smaller flow rate calculated in ALARM-P1. Corresponding pump head is shown in Fig. 5.43 and Fig. 5.44 and ALARM-P1 predicts lower pump head during initial transient.

As mentioned in 3.3, input data for RELAP-4J is by no means satisfactory and reliable pump data for the LOFT calculation is still lacked. However

comparison of RELAP-4J result with other LOFT experimental data reveals that pump coastdown predicted by RELAP-4J is still faster than actual pump coastdown. It suggests that ALARM-P1 prediction would be much faster than actual.

5.8 Suppression Tank

Suppression tank is represented by one volume in RELAP-4J and ALARM-P1 analysis. Calculated pressure and temperature are shown in Fig. 5.45. It is noticed that initial pressure employed in RELAP-4J is slightly less than 14.7 psia, ordinary atmospheric pressure, considering elevation of the LOFT site from sea level while ALARM-P1 does not allow to use lower pressure than 14.7 psia in calculation of two phase multiplier. However the results are not sensitive to the initial pressure as can be seen in the figure.

Increase rate of the suppression tank pressure is almost identical. The mixture level is calculated in RELAP-4J and the result is shown in Fig. 5.46. It is found that assumption of mixture level in suppression tank does not result in significant effect on the result. It is because the model used in RELAP-4J is not adequate to account for initially presented air volume in suppression header which plays an important role in pressure rise during early phase of blowdown. Thus present analysis would lead to lower predicted suppression tank pressure if compared to experimental data.

5.9 ECC System

5.9.1 HPIS

HPIS is initiated at 22 sec with injection flow rate of 1.072 liter/sec (17 gpm) at 33.3°C (92°F) and these data are used as an input to both calculations as shown in Fig. 5.47.

5.9.2 LPIS

LPIS injection flow rate is shown in Fig. 5.48. Injection initiates at 36 sec and coolant temperature is 33.3°C (92°F). Calculated flow rate is however different between the two calculations since injection flow rate depends on system pressure. Flow rate calculated by RELAP-4J is slightly higher corresponding to lower system pressure as compared with ALARM-P1.

5.9.3 ACC

Accumulator injection flow rate is shown in Fig. 5.49. Initiation of

injection is at 20 sec after break in RELAP-4J and 21 sec after break in ALARM-P1. Later injection initiation in ALARM-P1 corresponds to higher calculated system pressure since initiation is set by trip signal based on system pressure. Accumulator injection flow rate calculated by ALARM-P1 is smaller than that of RELAP-4J. As can be seen in pressure in accumulator shown in Fig. 5.50, accumulator pressure is virtually identical while cold leg pressure is lower in RELAP-4J. Thus driving force for injection flow is larger in RELAP-4J.

5.9.4 ECC Water in Reactor Vessel

ECC water injected into cold leg from HPIS, LPIS and ACC flows into reactor vessel via downcomer and lower plenum. Thus effect of injected water can be best represented by calculating total amount of coolant accumulated in reactor vessel. Fig. 5.51 shows the calculated total mass in reactor vessel. It is found that effect of ECC injection is not significant except in downcomer. The reason is that occurrence of counter current two phase flow in downcomer is not modeled in RELAP-4J and ALARM-P1 as well. Thus injected water first fills downcomer and then flows into lower plenum. This type of flow pattern is unlikely to occur since cold water flowing into downcomer falls through downcomer gap overcoming upward steam flow and directly reaches lower plenum without accumulating in downcomer. In order to accurately predict coolant flow in downcomer, especially injected coolant behavior, modification of flow model is necessary to accomodate counter current two phase flow.

CSNI STANDARD PROBLEM L1-4

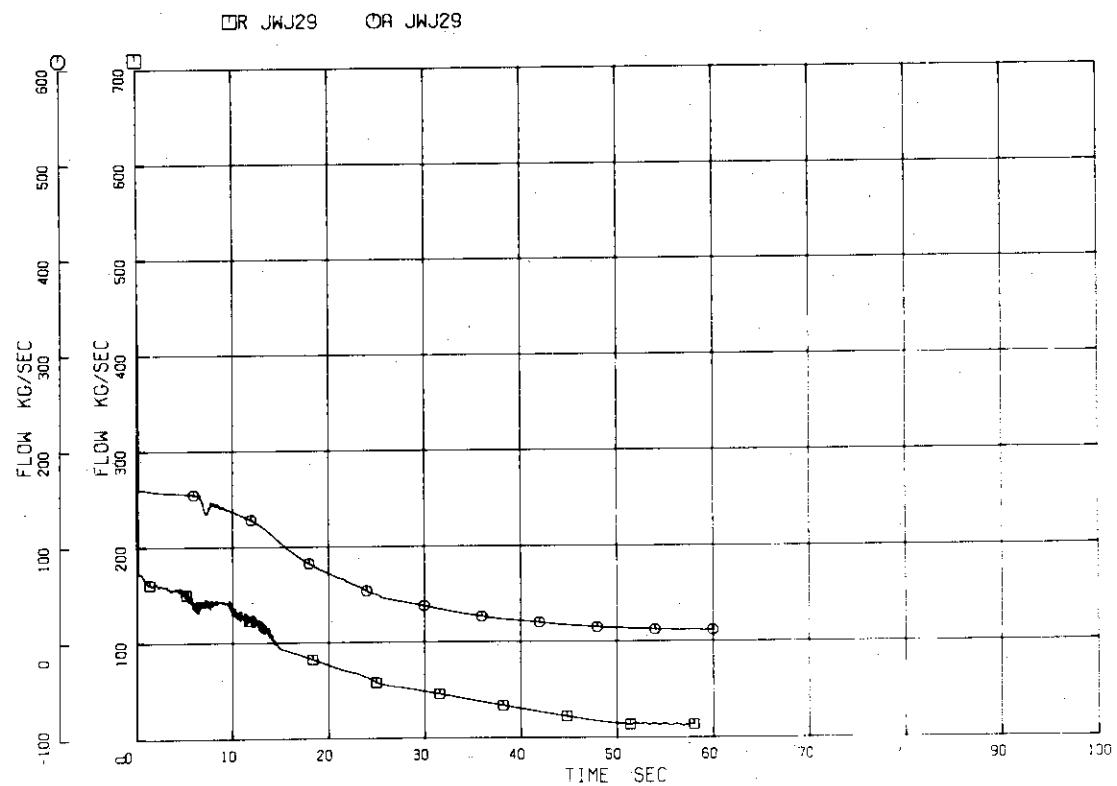


Fig. 5.1 Discharge Flow Rate at Broken Loop Cold Leg Break Plane

CSNI STANDARD PROBLEM L1-4

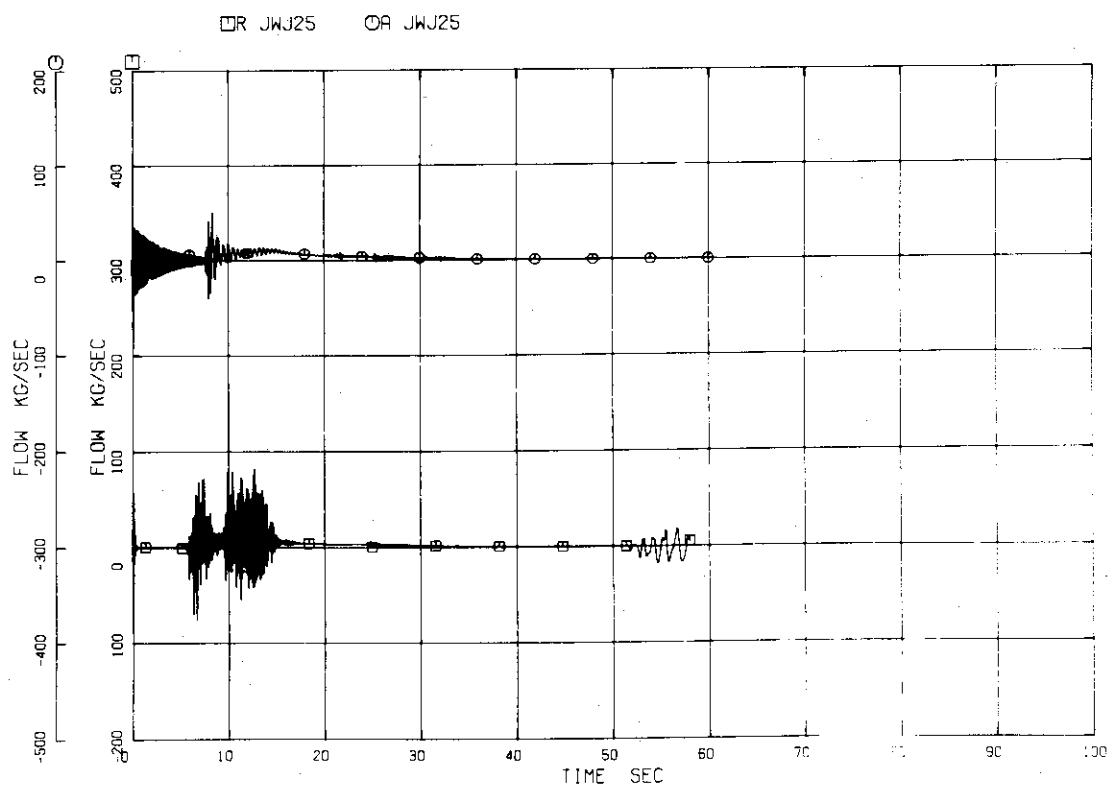


Fig. 5.2 Junction Flow at Reflood Assist Line Outlet in Broken Loop Cold Leg

CSNI STANDARD PROBLEM L1-4

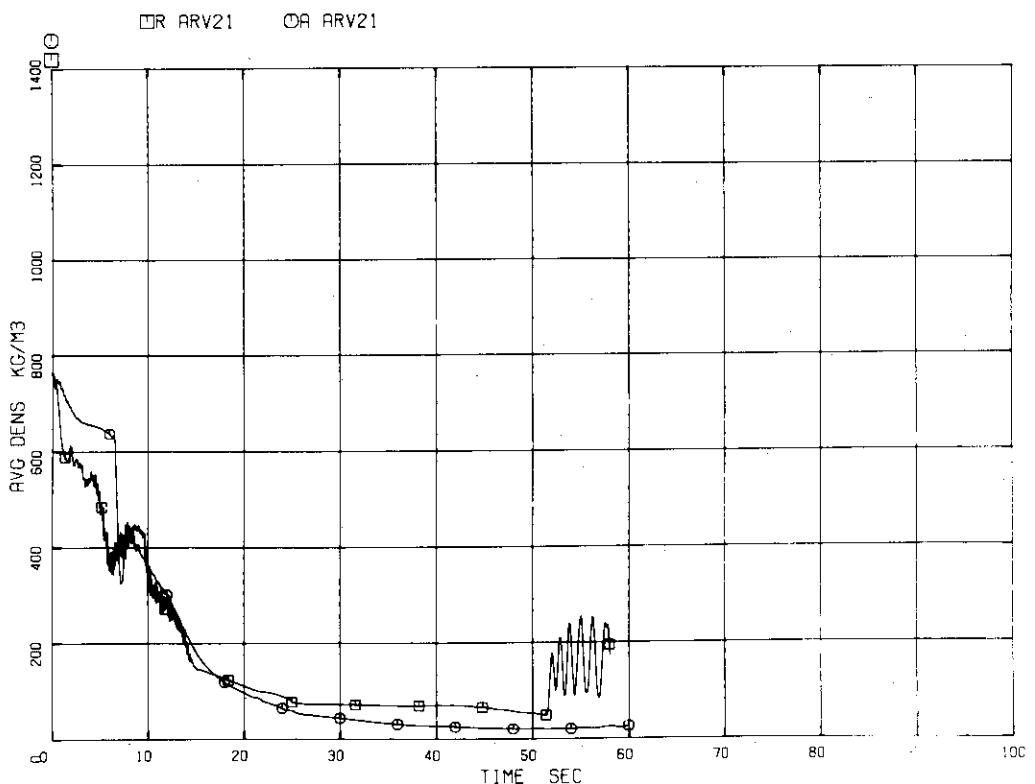


Fig. 5.3 Density in Broken Loop Cold Leg (DE-BL-1)

CSNI STANDARD PROBLEM L1-4

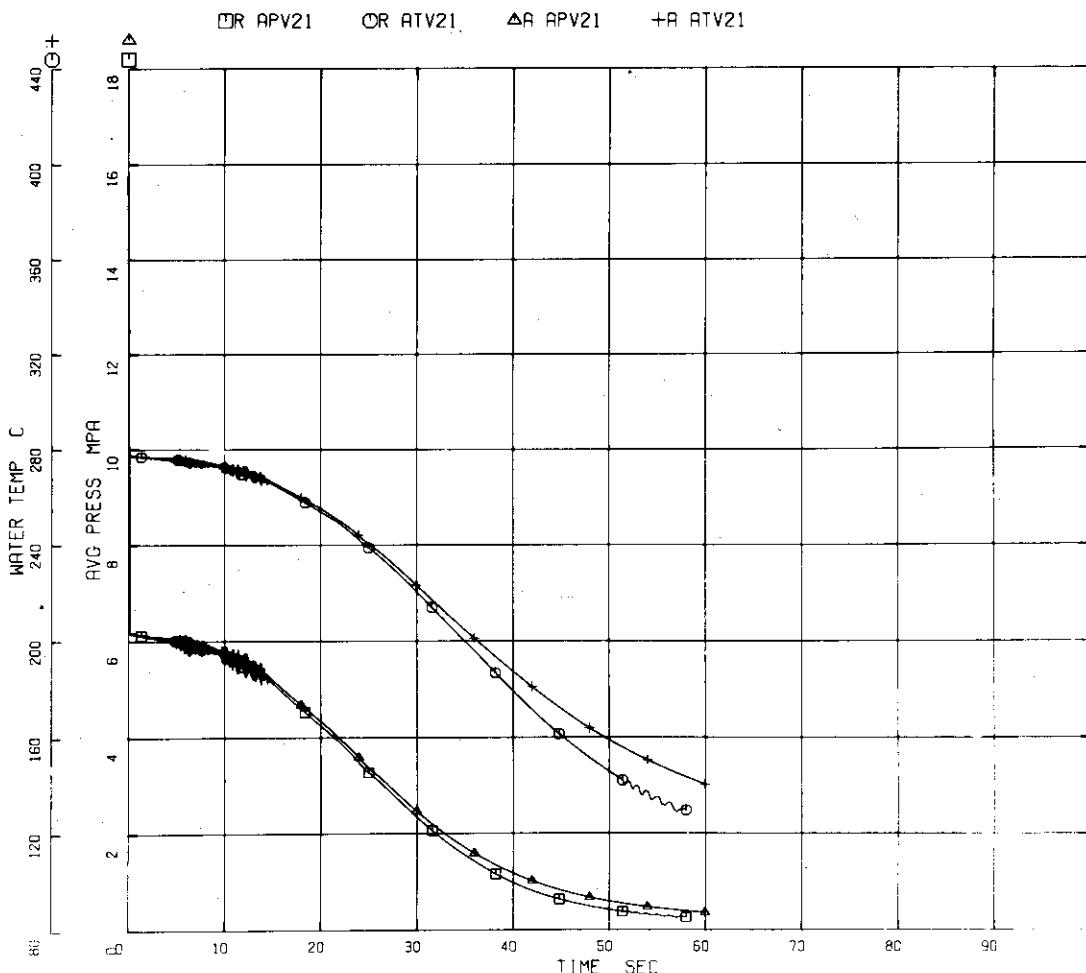


Fig. 5.4 Pressure and Temperature in Broken Loop Cold Leg (PE-BL-1, TE-BL-1)

CSNI STANDARD PROBLEM L1-4

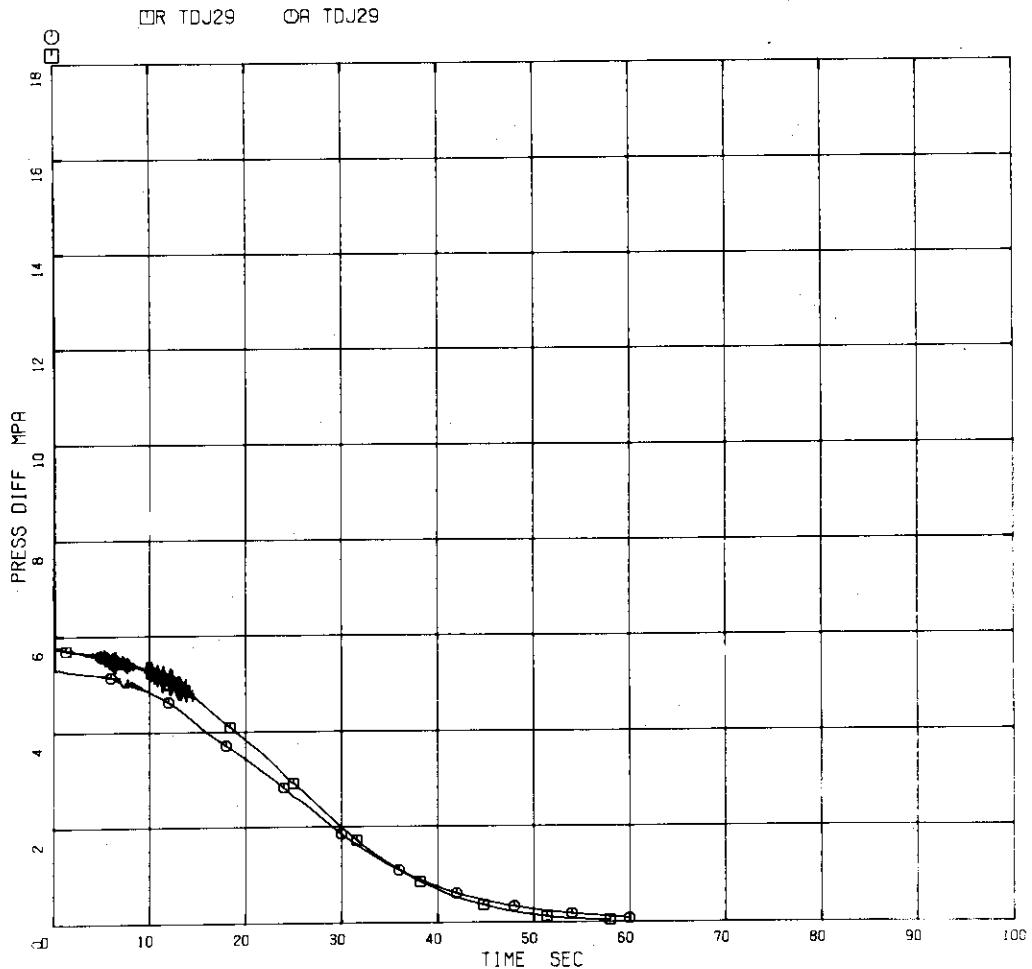


Fig. 5.5 Differential Pressure at Break Plane in Broken Loop Hot Leg (PdE-BL-3)

CSNI STANDARD PROBLEM L1-4

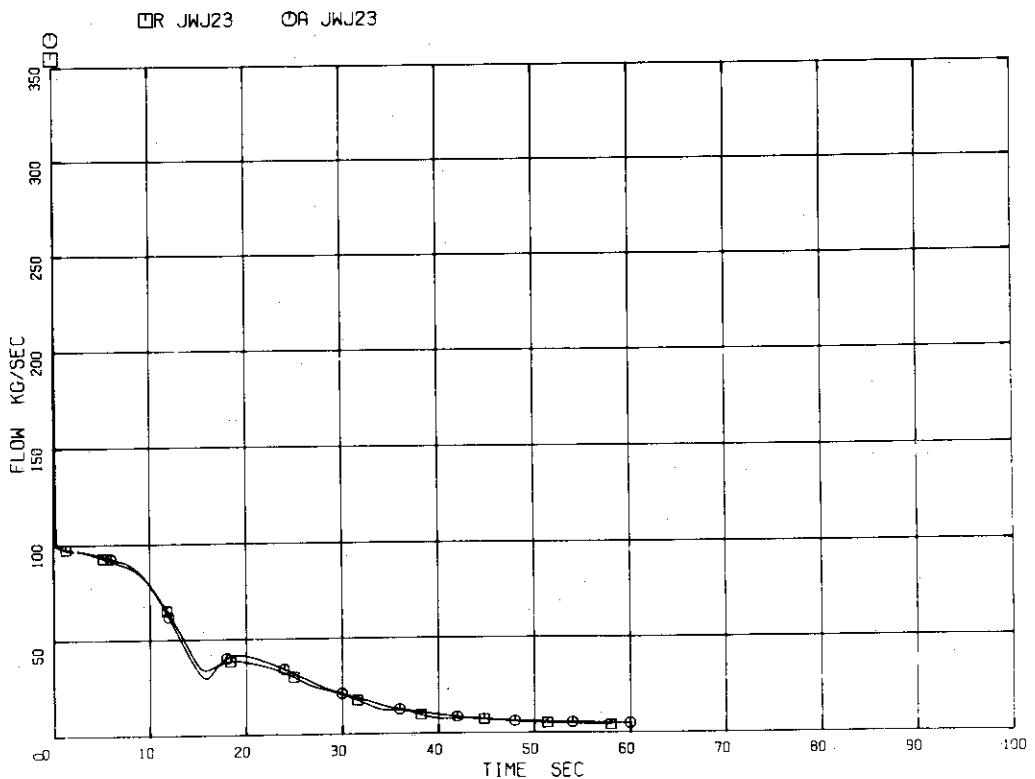


Fig. 5.6 Discharge Flow Rate at Break Plane in Broken Loop Hot Leg

CSNI STANDARD PROBLEM L1-4

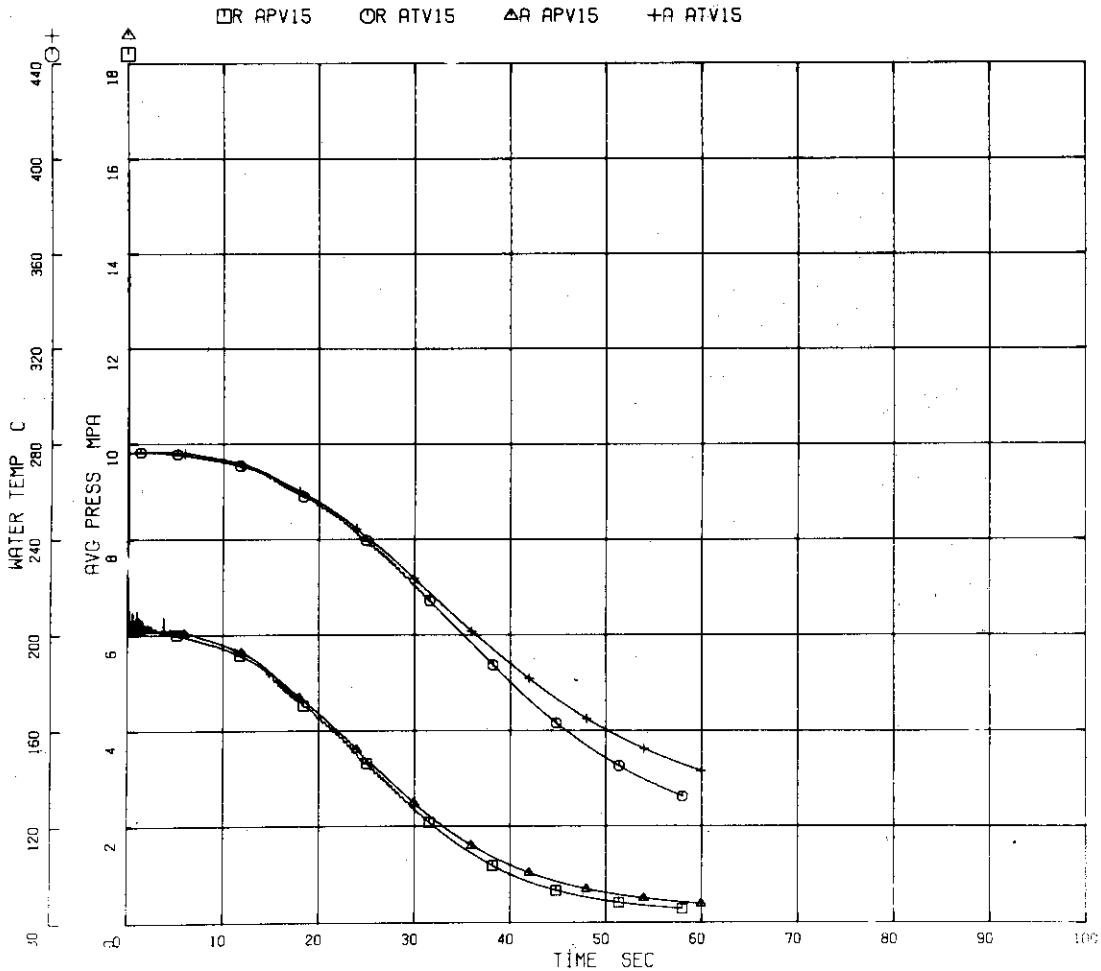


Fig. 5.7 Pressure and Temperature in Broken Loop Hot Leg (PE-BL-2, TE-BL-2)

CSNI STANDARD PROBLEM L1-4

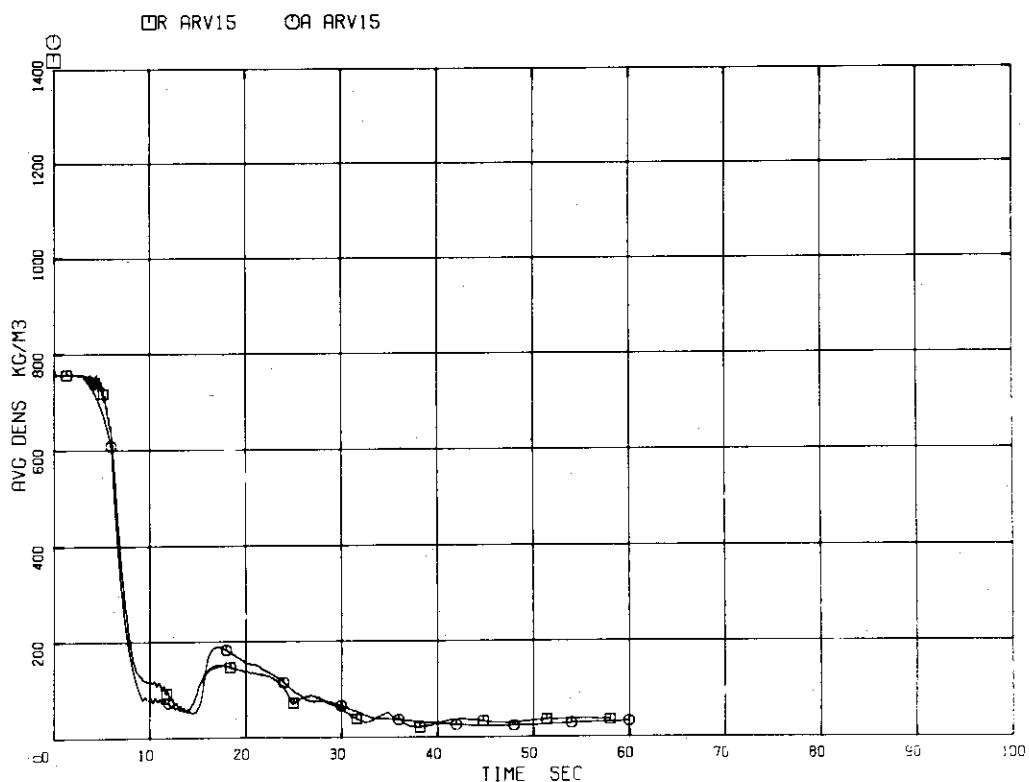


Fig. 5.8 Average Density in Broken Loop Hot Leg (DE-BL-2)

CSNI STANDARD PROBLEM L1-4

□R JWW17 □A JWW17

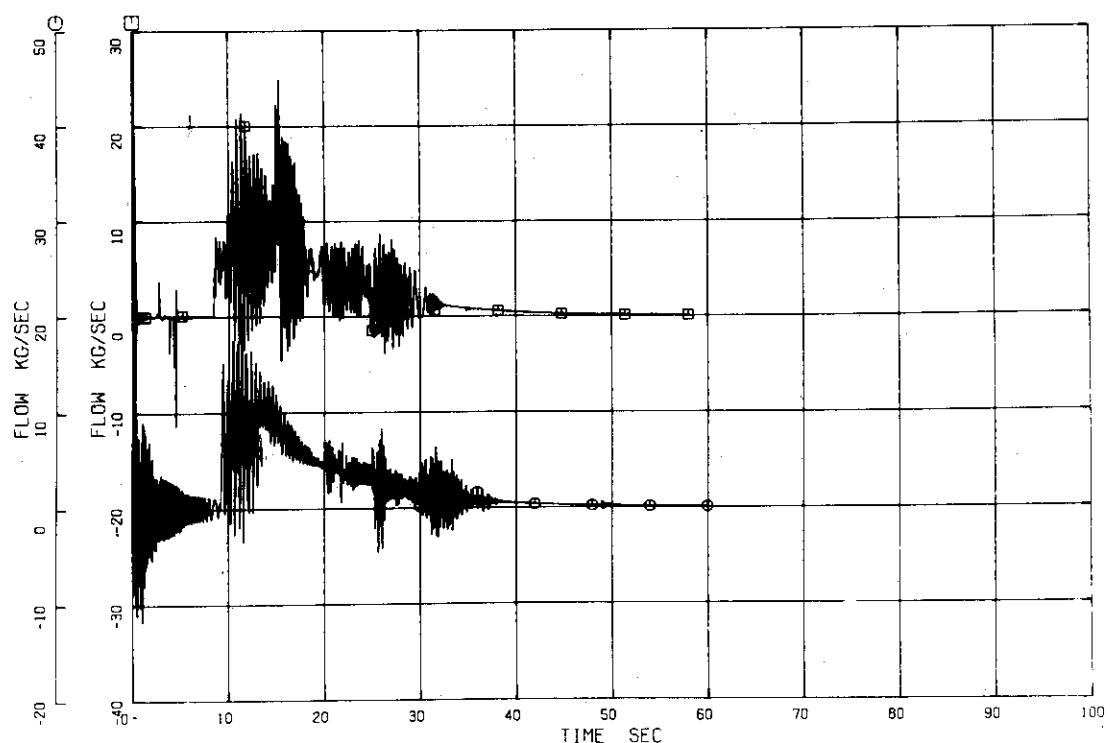


Fig. 5.9 Junction Flow at Reflood Assist Line Outlet

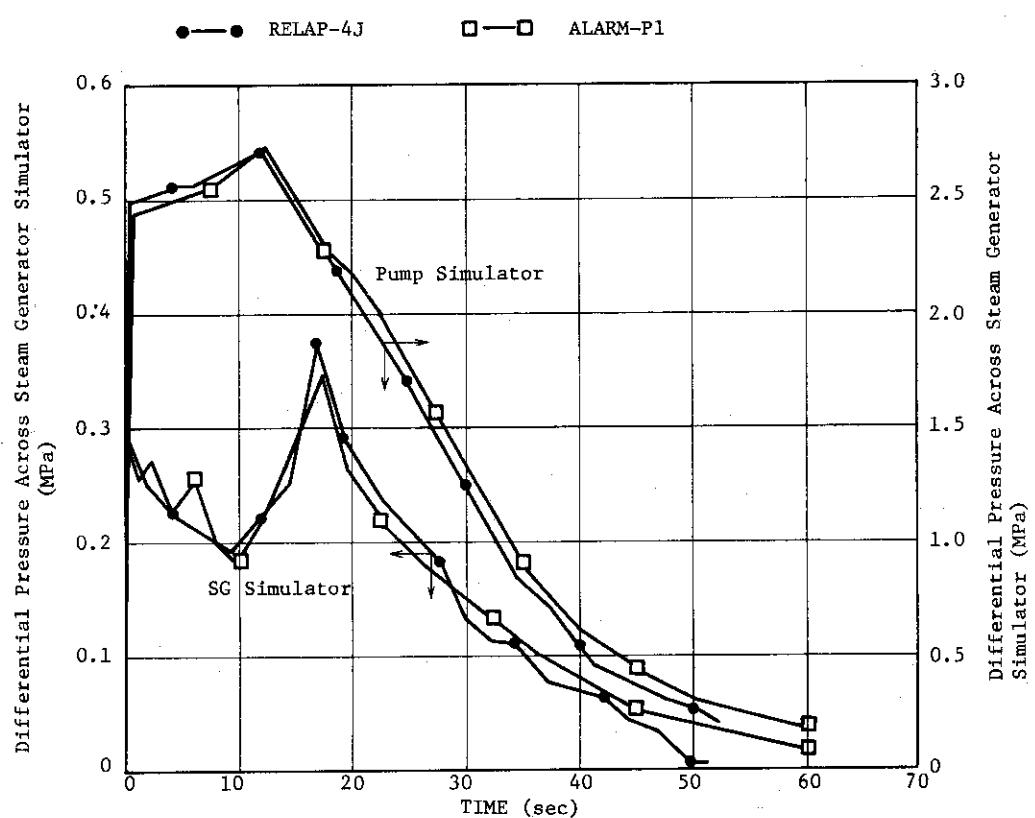


Fig. 5.10 Differential Pressure Across Steam Generator Simulator and Pump Simulator (PdE-BL-5, 6, 7, 8)

CSNI STANDARD PROBLEM L1-4

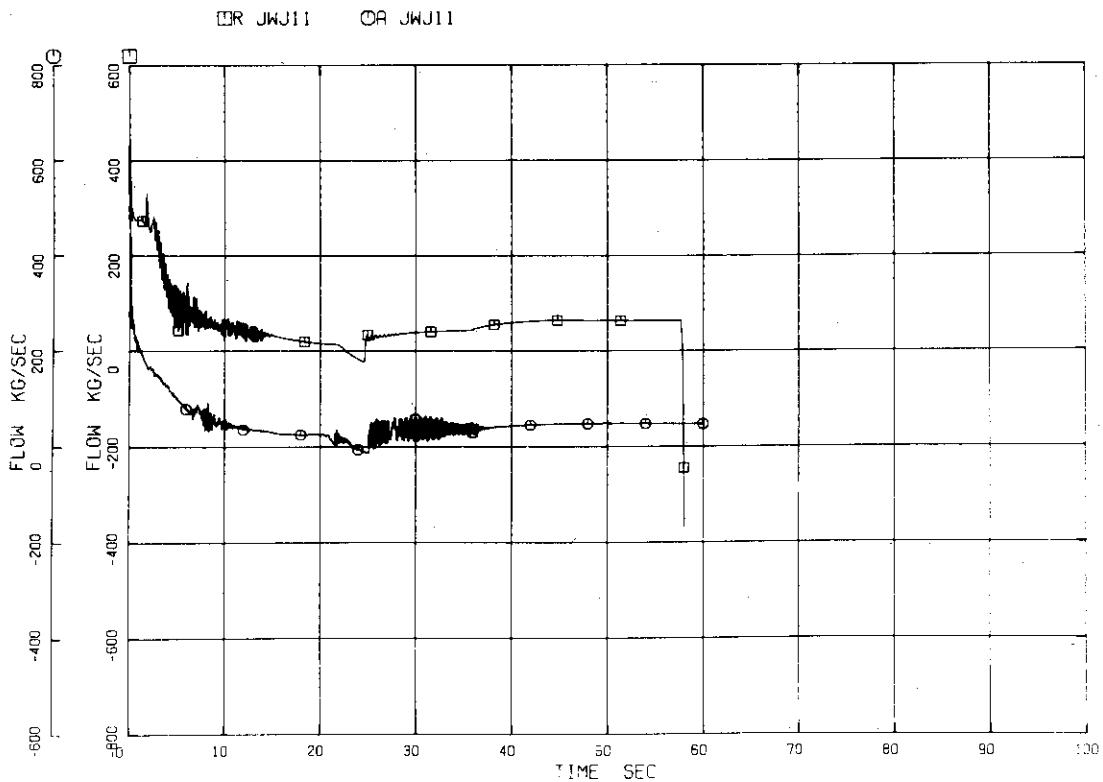


Fig. 5.11 Junction Flow at Downcomer Inlet from Intact Loop Cold Leg
CSNI STANDARD PROBLEM L1-4

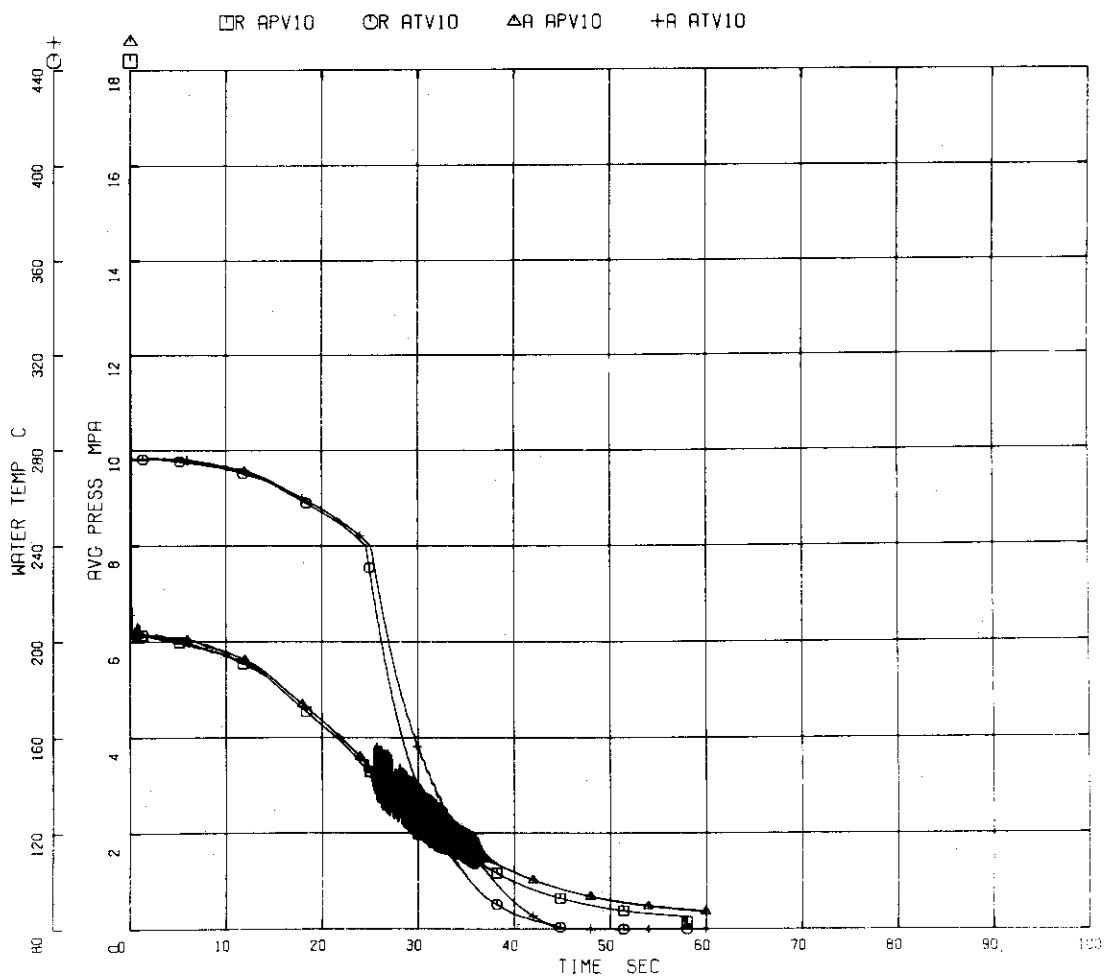


Fig. 5.12 Pressure and Temperature in Inlet Loop Cold Leg (PE-PC-1, TE-PC-1)

CSNI STANDARD PROBLEM L1-4

□R JWJ10 OA JWJ10

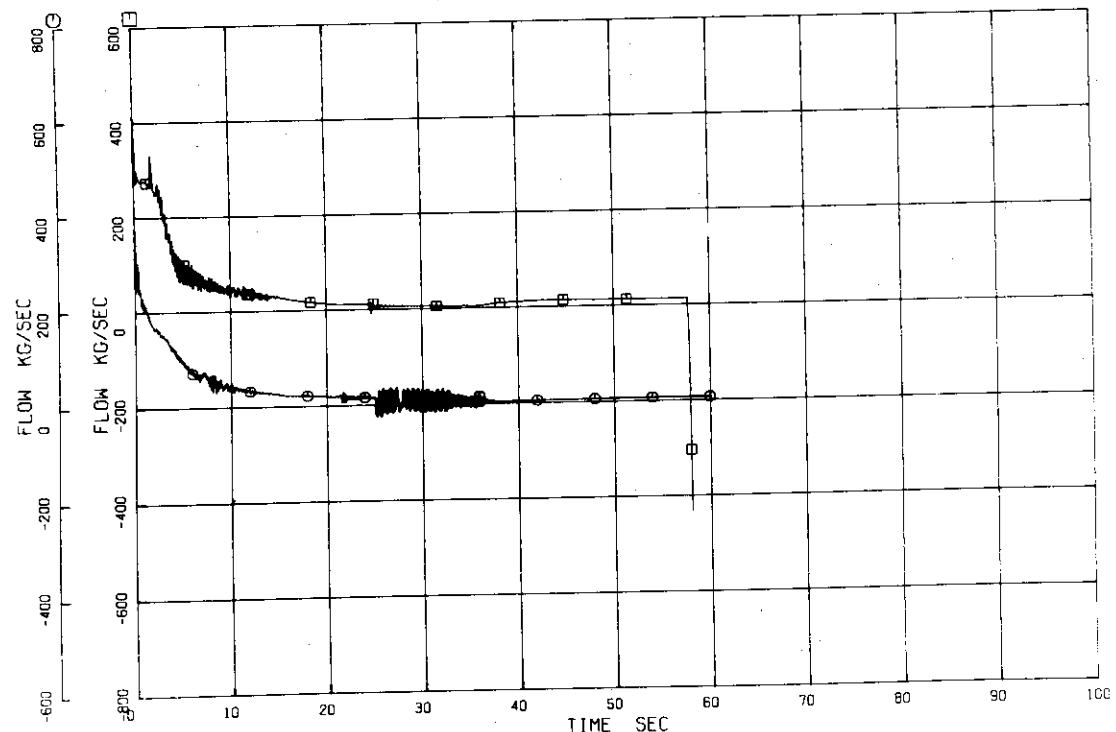


Fig. 5.13 Junction Flow Between Cold Leg Injection Location and Pump Outlet

CSNI STANDARD PROBLEM L1-4

□R ARV10 OA ARV10

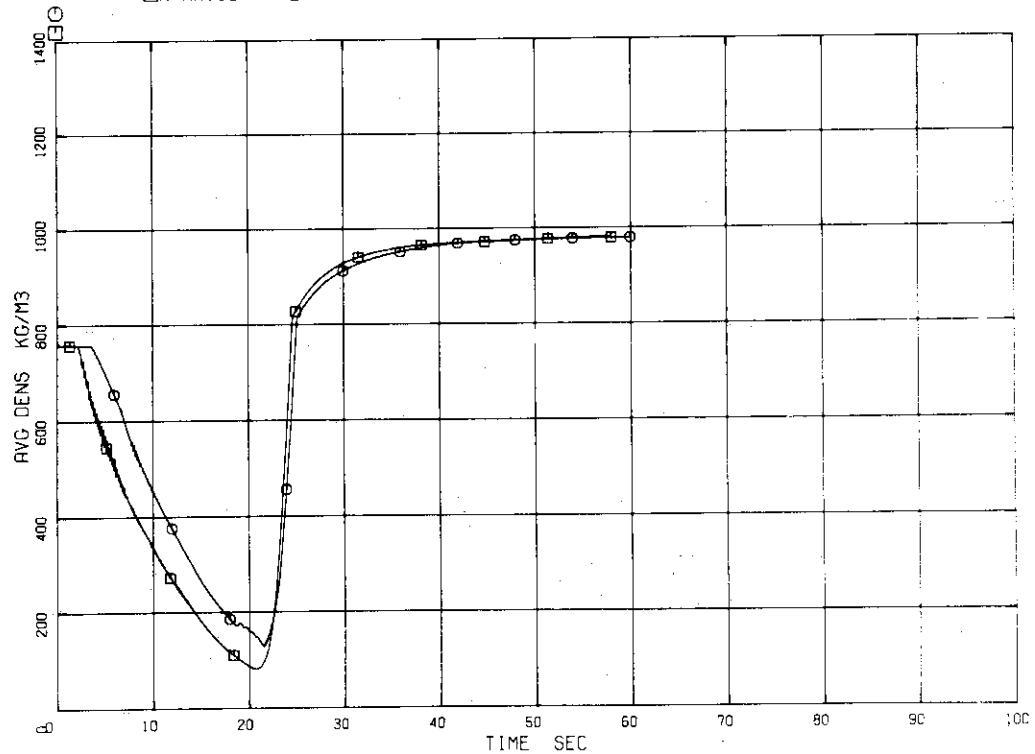


Fig. 5.14 Average Density and Quality in Intact Loop Cold Leg (DE-PC-1)

CSNI STANDARD PROBLEM L1-4

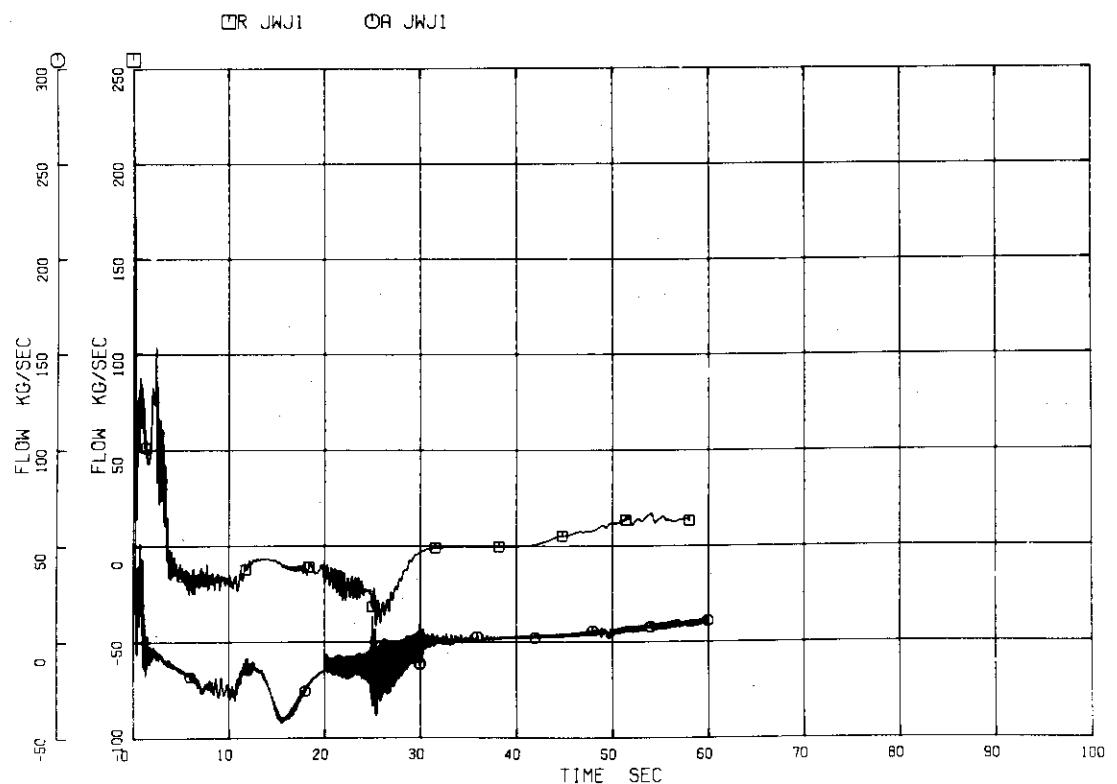


Fig. 5.15 Junction Flow at Upper Plenum Outlet to Intact Loop Hot Leg

CSNI STANDARD PROBLEM L1-4

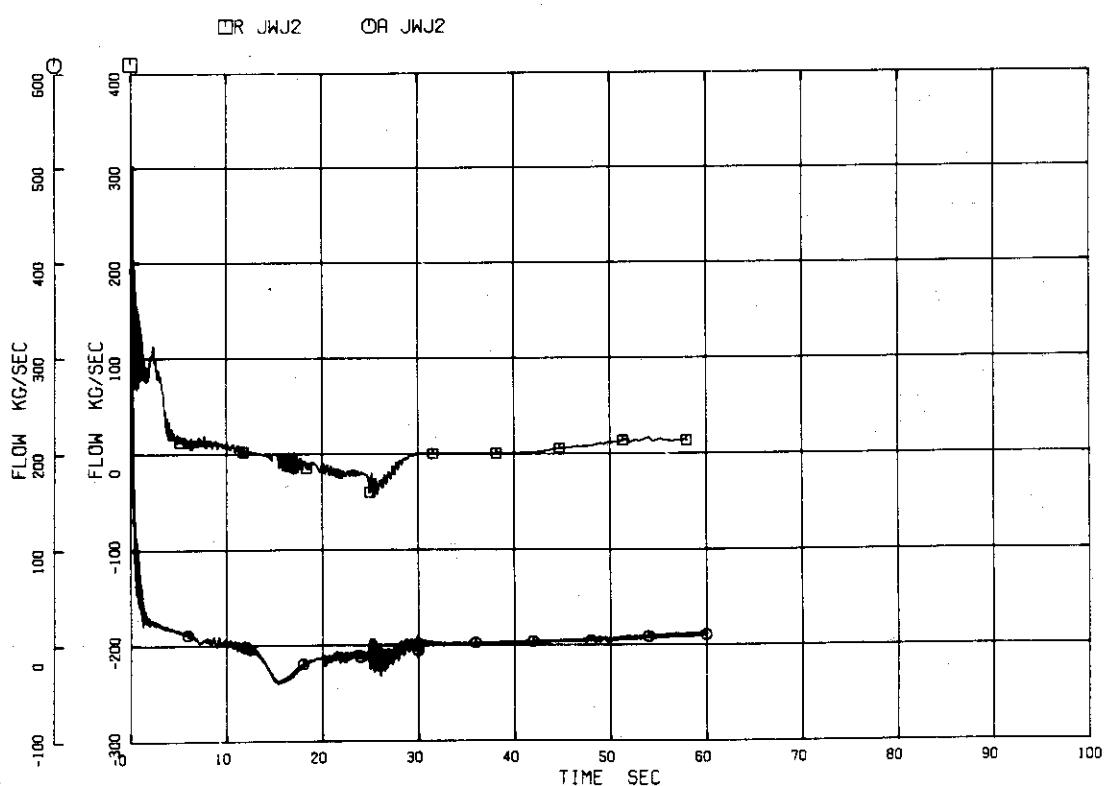


Fig. 5.16 Junction Flow Between Pressurizer Surge Line Outlet and Steam Generator Inlet

CSNI STANDARD PROBLEM L1-4

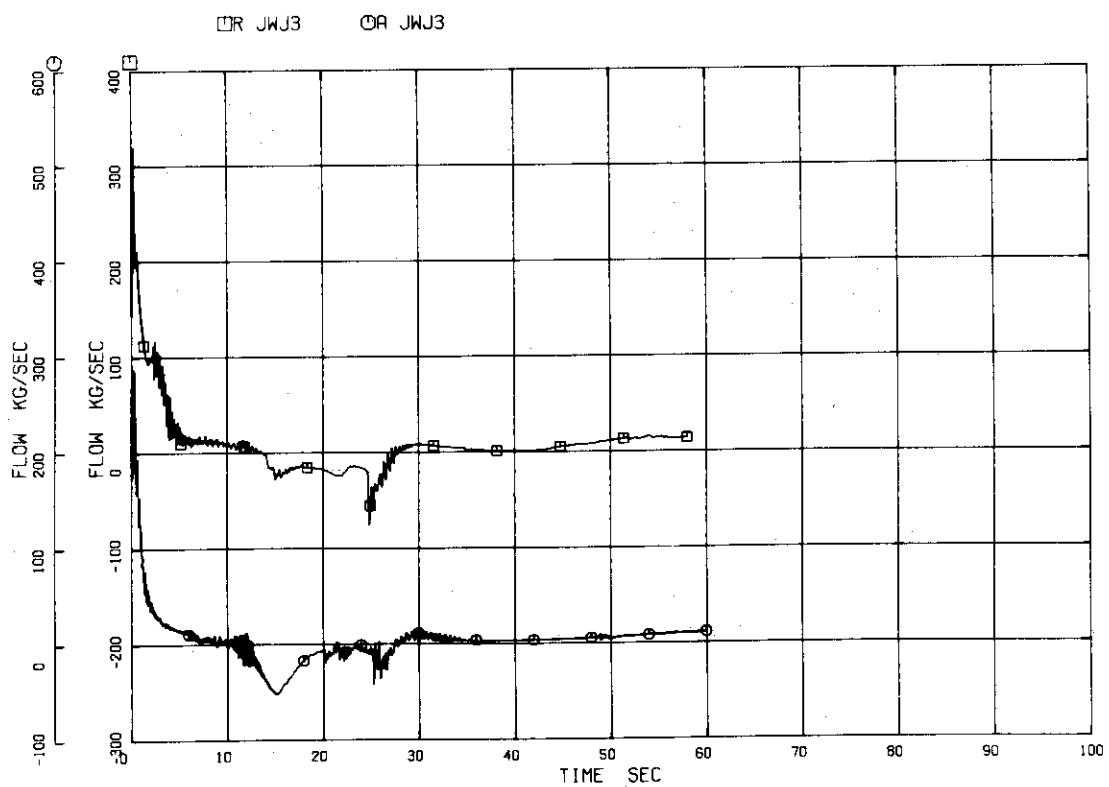


Fig. 5.17 Junction Flow at Steam Generator Inlet

CSNI STANDARD PROBLEM L1-4

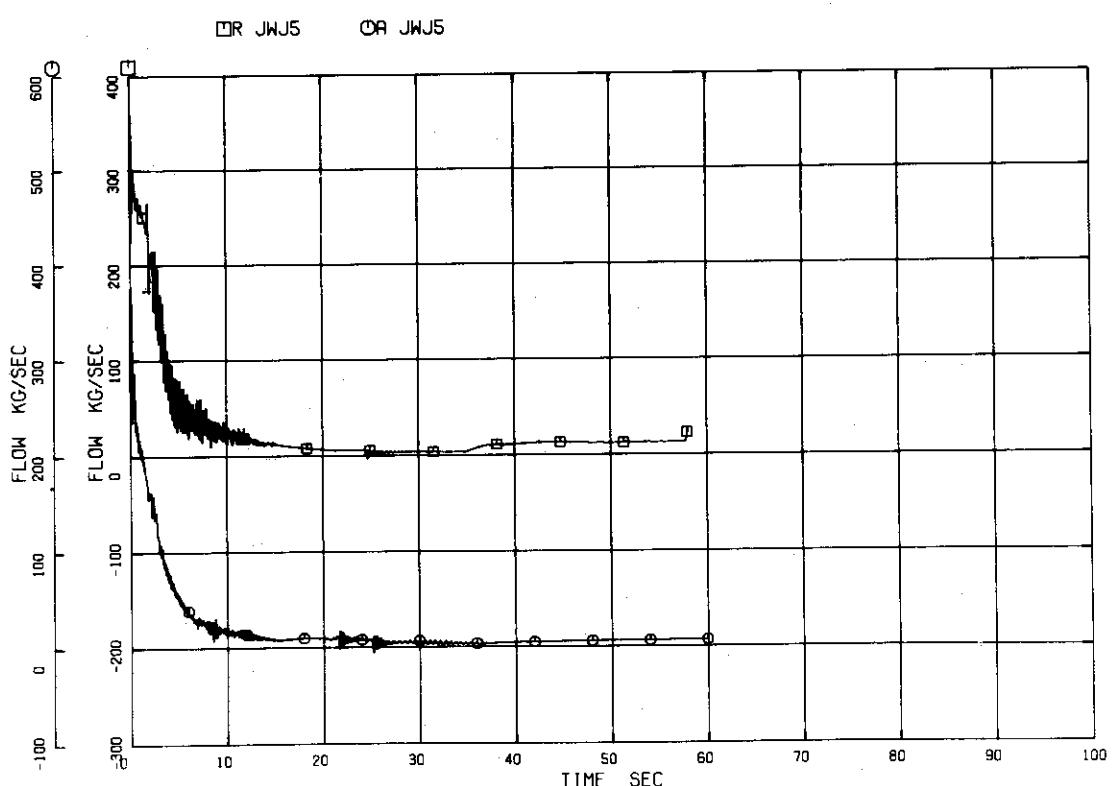


Fig. 5.18 Junction Flow at Steam Generator Outlet

CSNI STANDARD PROBLEM L1-4

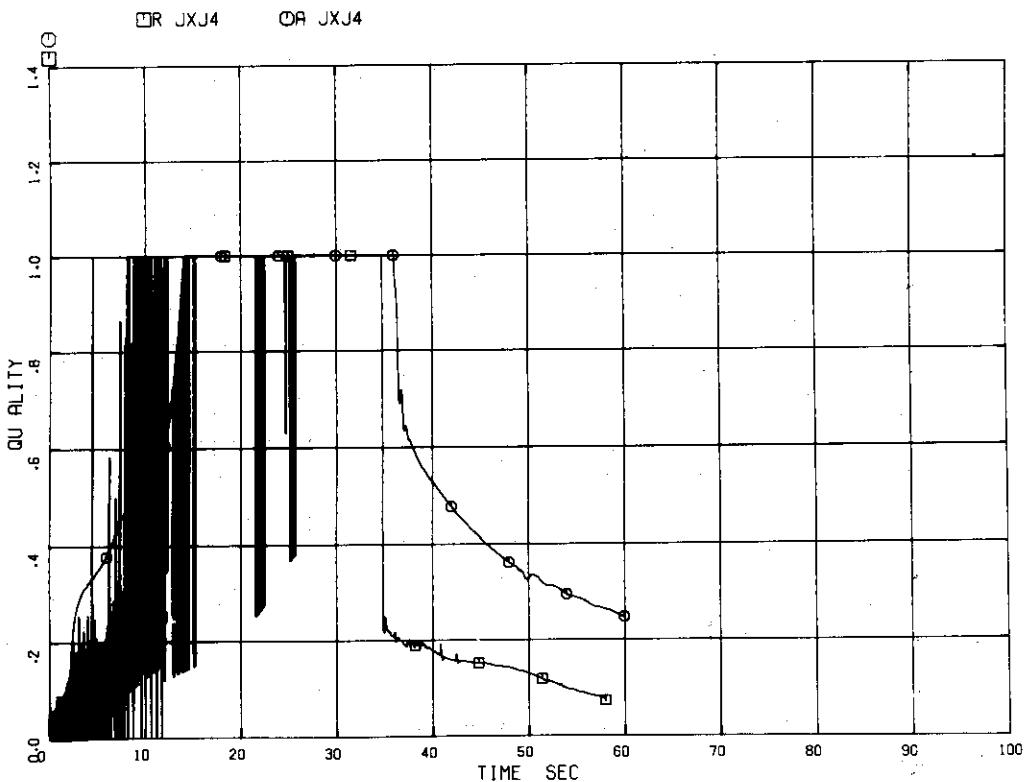


Fig. 5.19 Junction Flow at Steam Generator Top

CSNI STANDARD PROBLEM L1-4

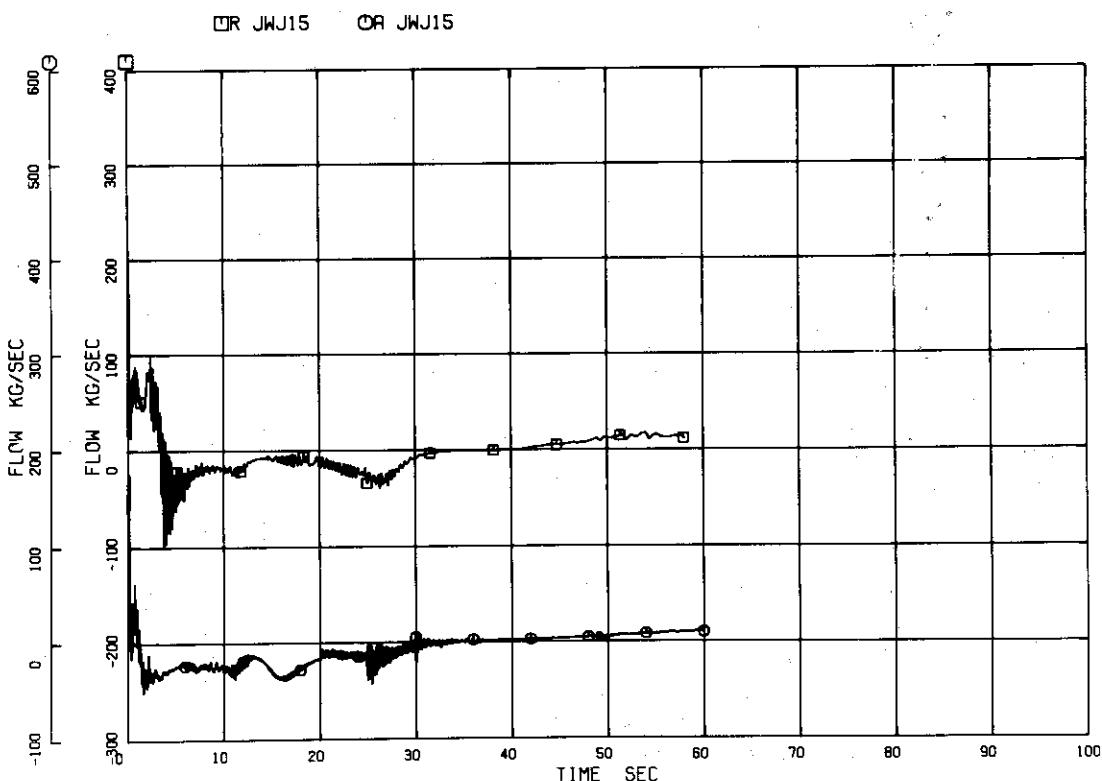


Fig. 5.20 Junction Flow at Upper Plenum Inlet from Intact Loop Hot Leg

CSNI STANDARD PROBLEM L1-4

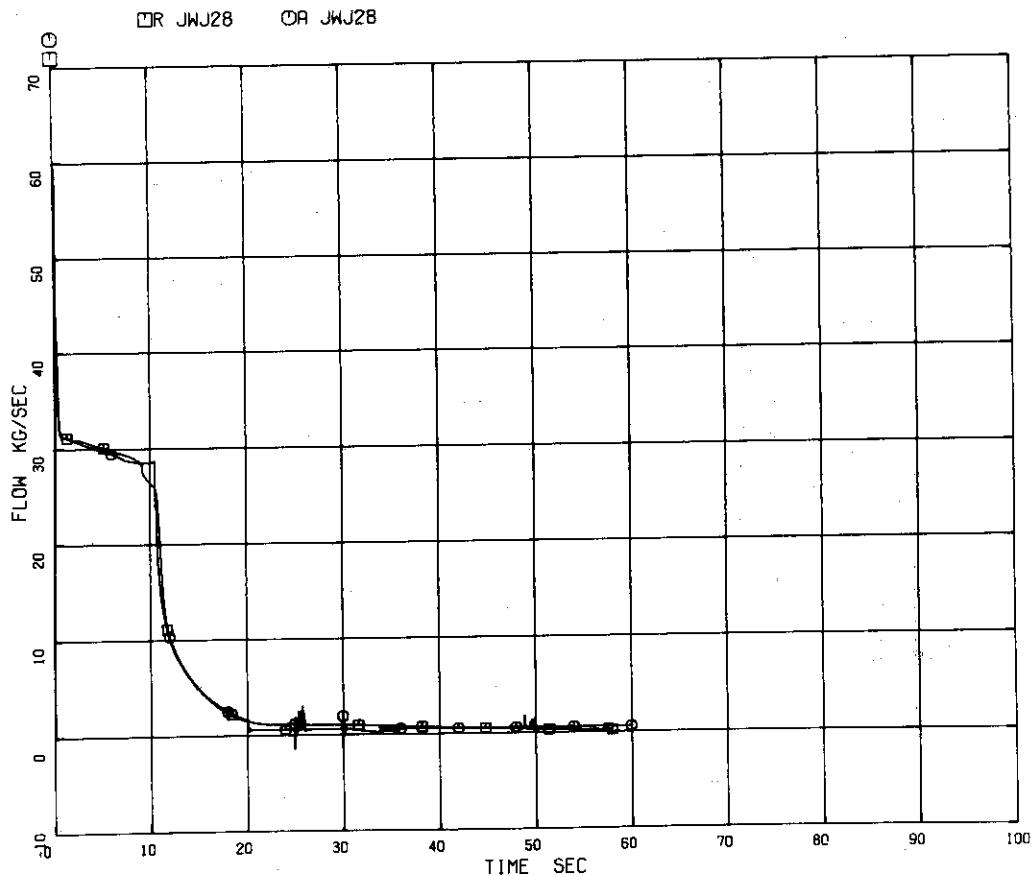


Fig. 5.21 Discharge Flow From Pressurizer Surge Line

CSNI STANDARD PROBLEM L1-4

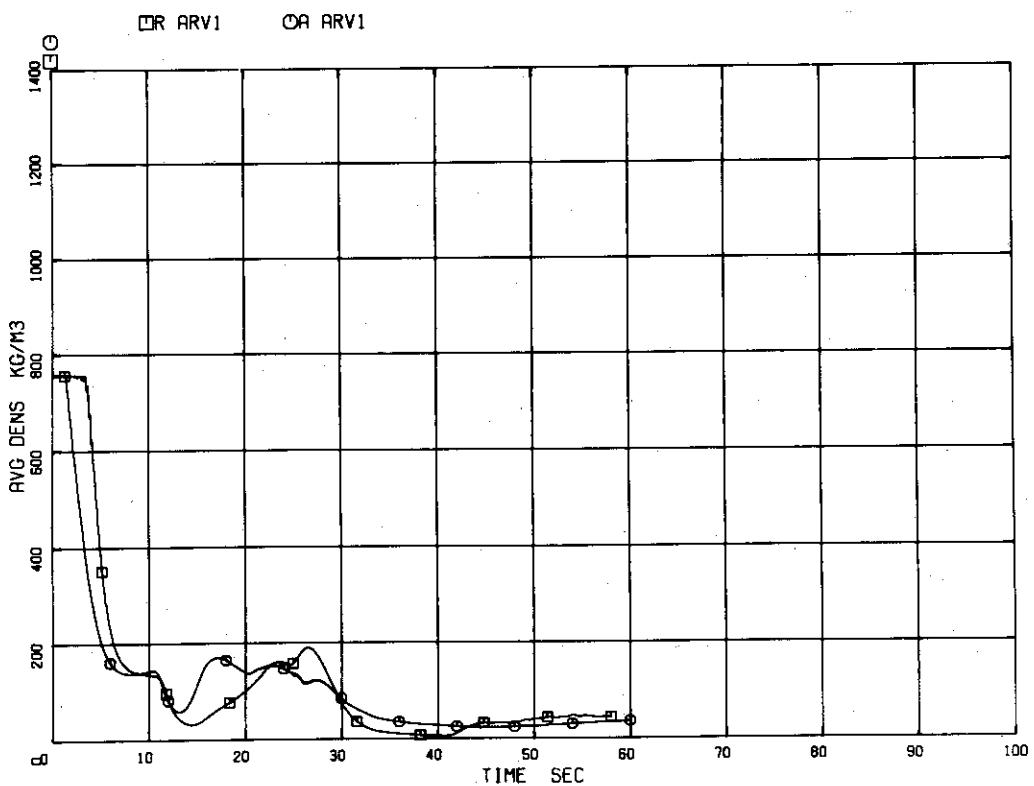


Fig. 5.22 Density in Intact Loop Hot Leg (DE-PC-2)

CSNI STANDARD PROBLEM L1-4

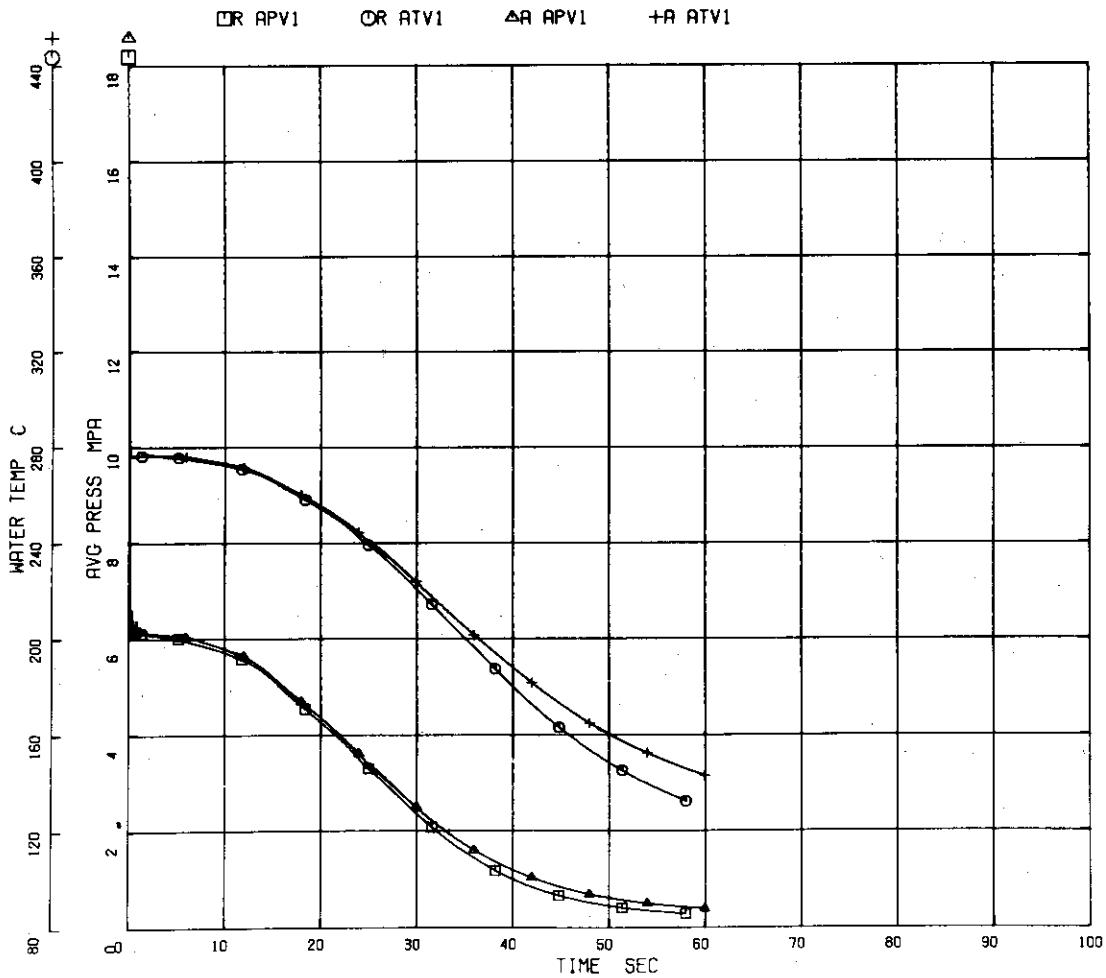


Fig. 5.23 Pressure and Temperature in Intact Loop Hot Leg (PE-PC-2, TE-PC-2)

CSNI STANDARD PROBLEM L1-4

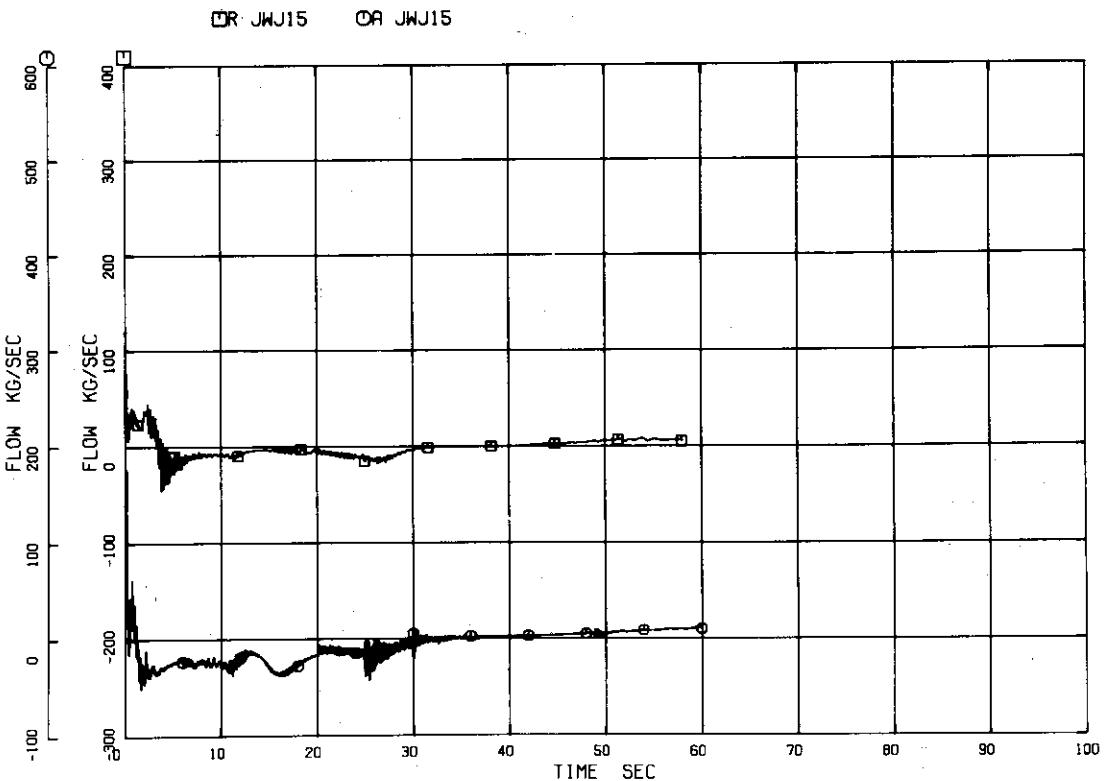


Fig. 5.24 Junction Flow at Upper Plenum Outlet to Intact Loop Hot Leg

CSNI STANDARD PROBLEM L1-4

DR JWJ16 OA JWJ16

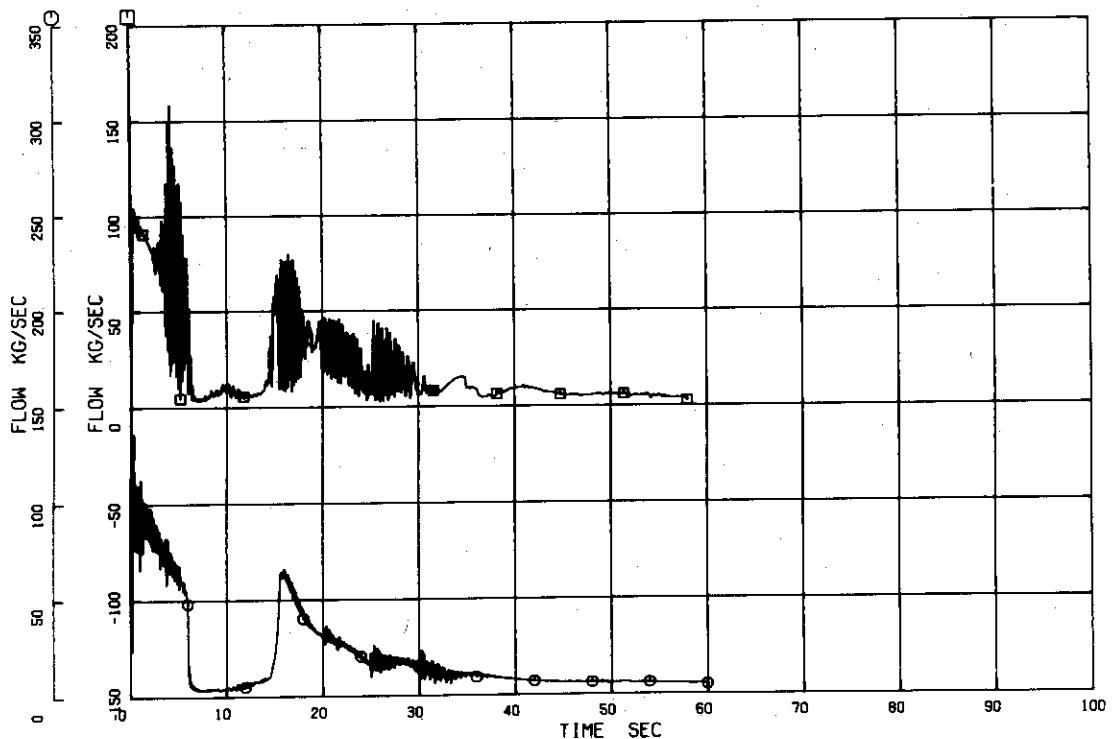


Fig. 5.25 Junction Flow Out of Upper Plenum to Broken Loop Hot Leg

CSNI STANDARD PROBLEM L1-4

DR MLV14 OA MLV14

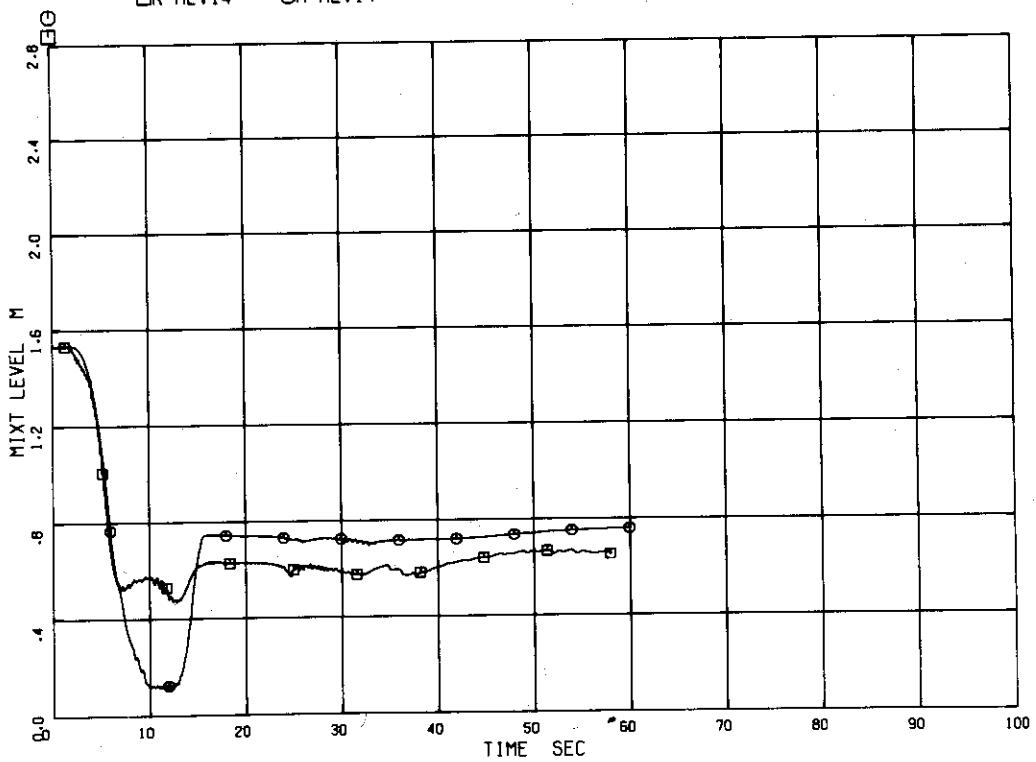


Fig. 5.26 Mixture Level in Upper Plenum

CSNI STANDARD PROBLEM L1-4

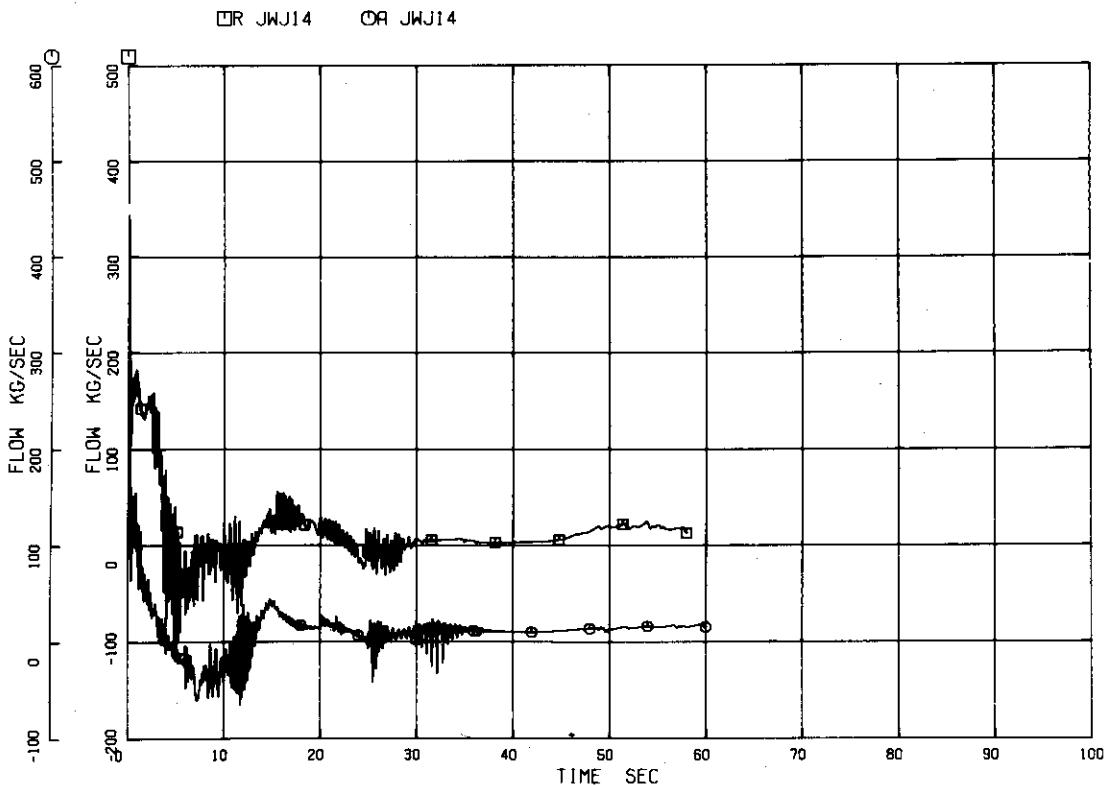


Fig. 5.27 Junction Flow Out of Core Simulator to Upper Plenum

CSNI STANDARD PROBLEM L1-4

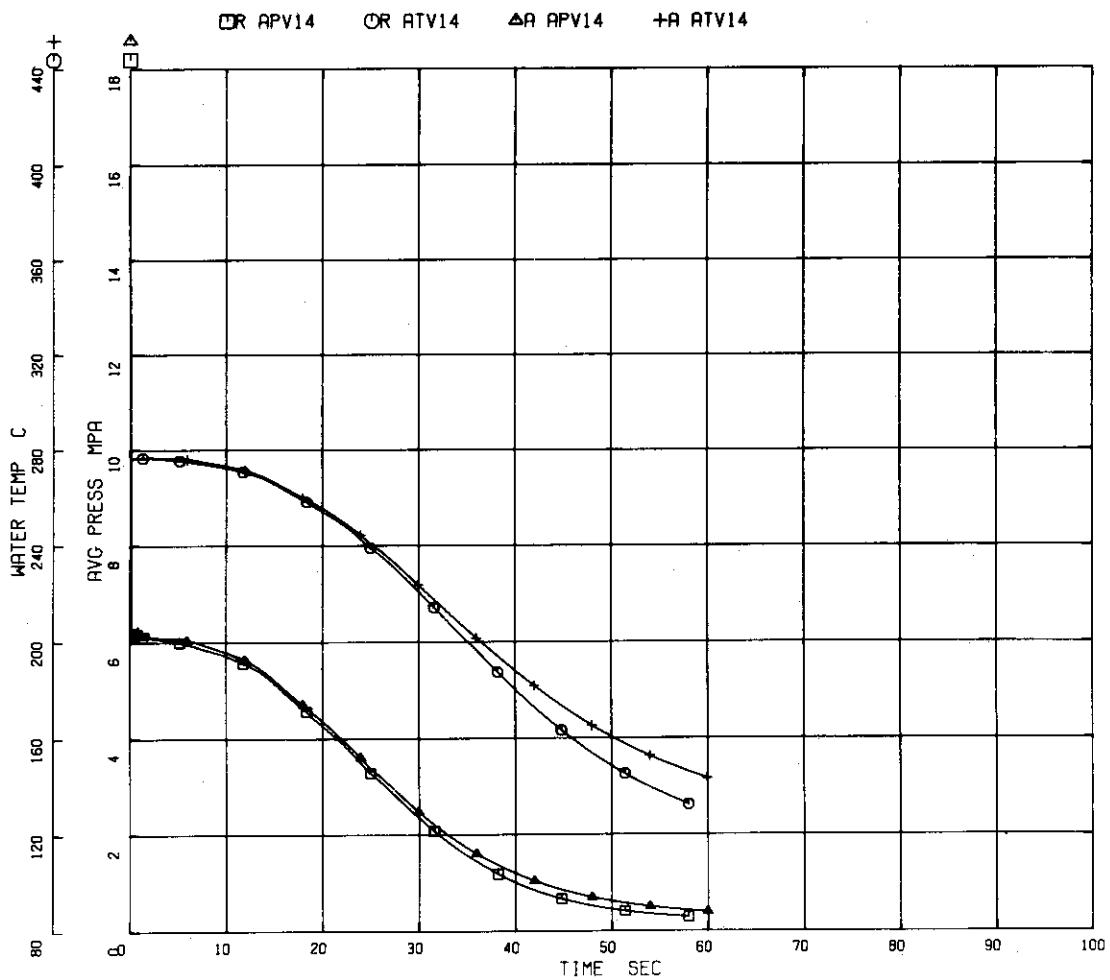


Fig. 5.28 Pressure and Temperature in Upper Plenum (PE-CS-1A, TE-CS-1A)

CSNI STANDARD PROBLEM L1-4

□R JWW13 ○R JWW13

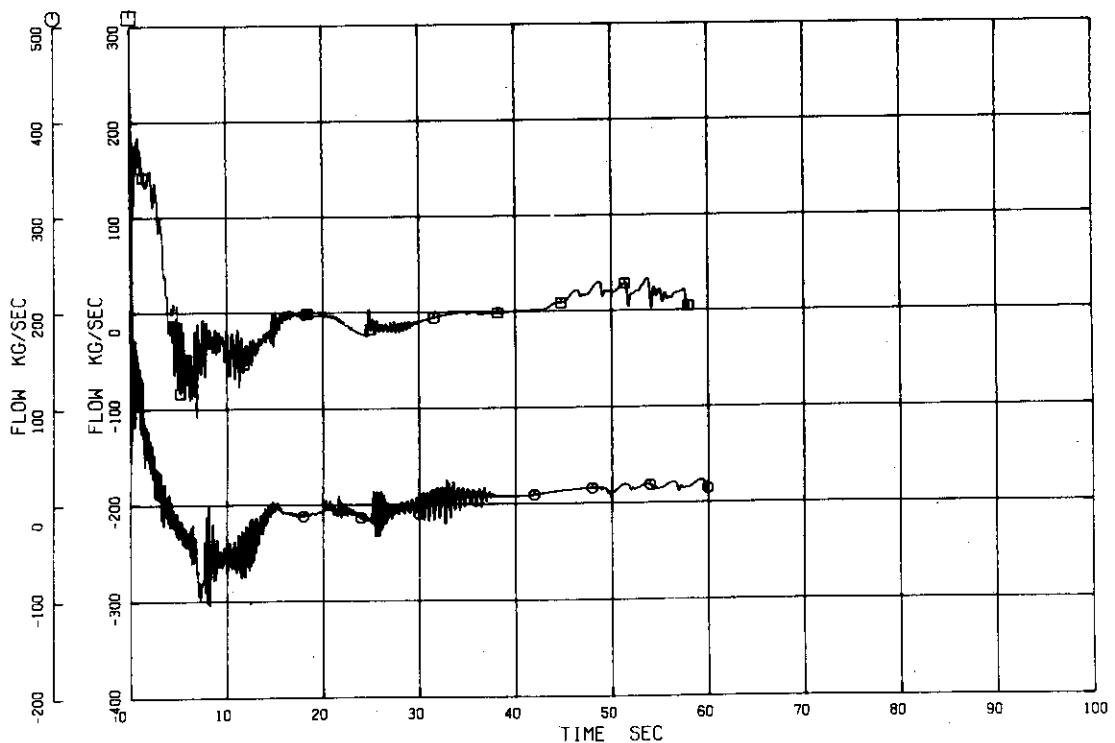


Fig. 5.29 Junction Flow From Lower Plenum to Core Simulator

CSNI STANDARD PROBLEM L1-4

□R JWW14 ○R JWW14

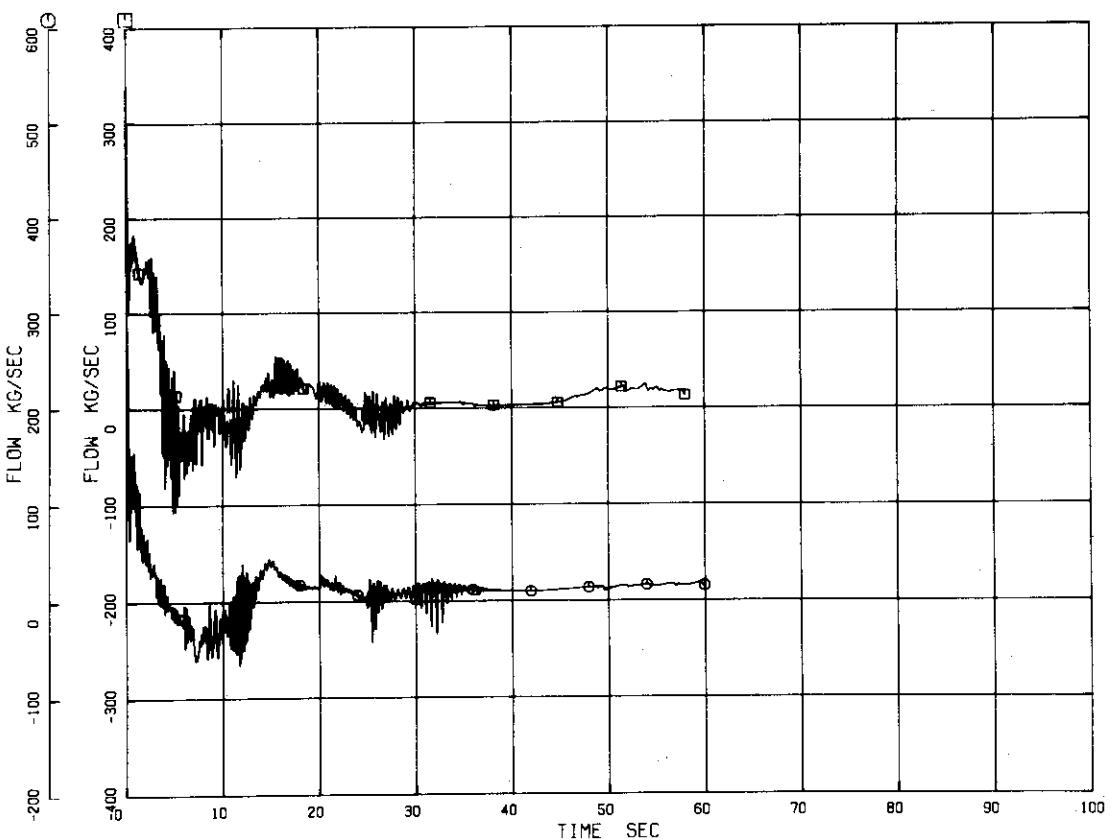


Fig. 5.30 Junction Flow into Upper Plenum Out of Core Simulator

CSNI STANDARD PROBLEM L1-4

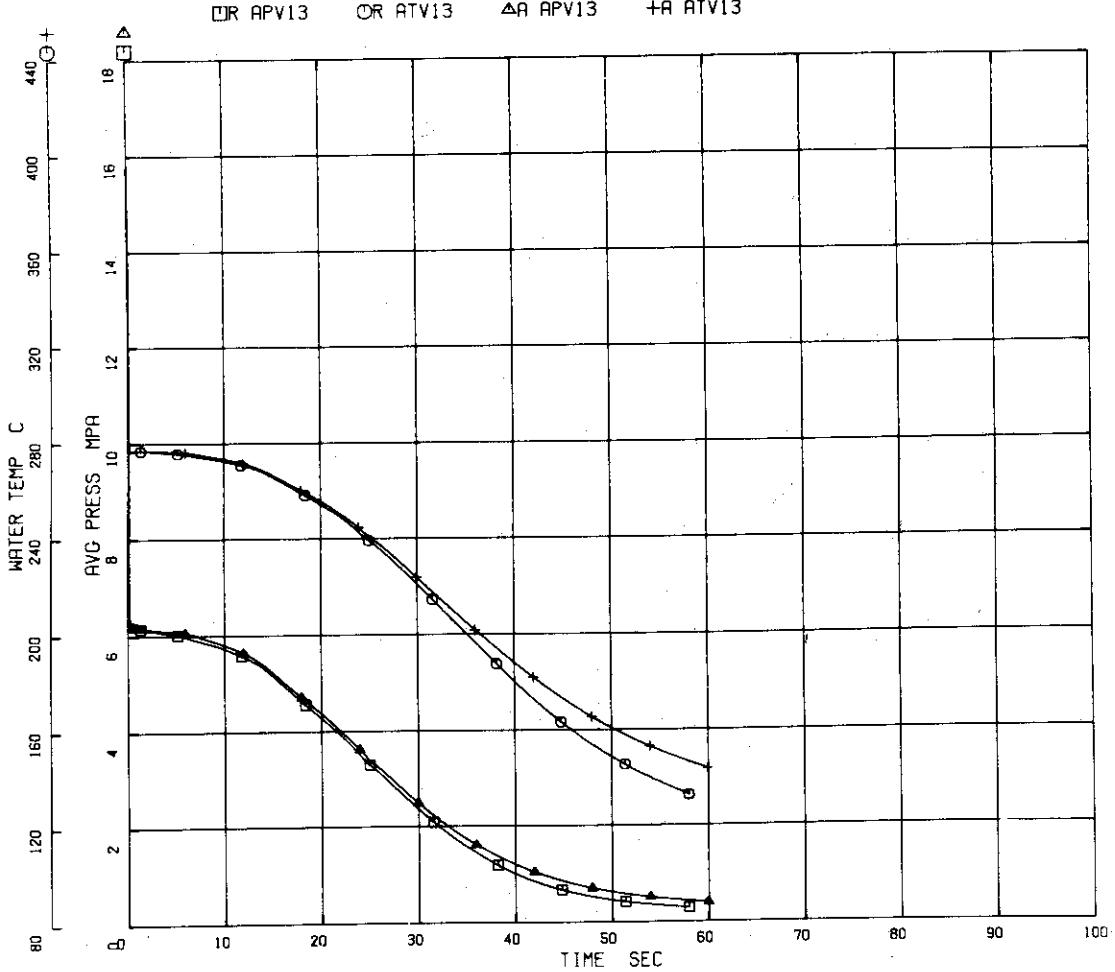


Fig. 5.31 Pressure and Temperature in Core Simulator

CSNI STANDARD PROBLEM L1-4

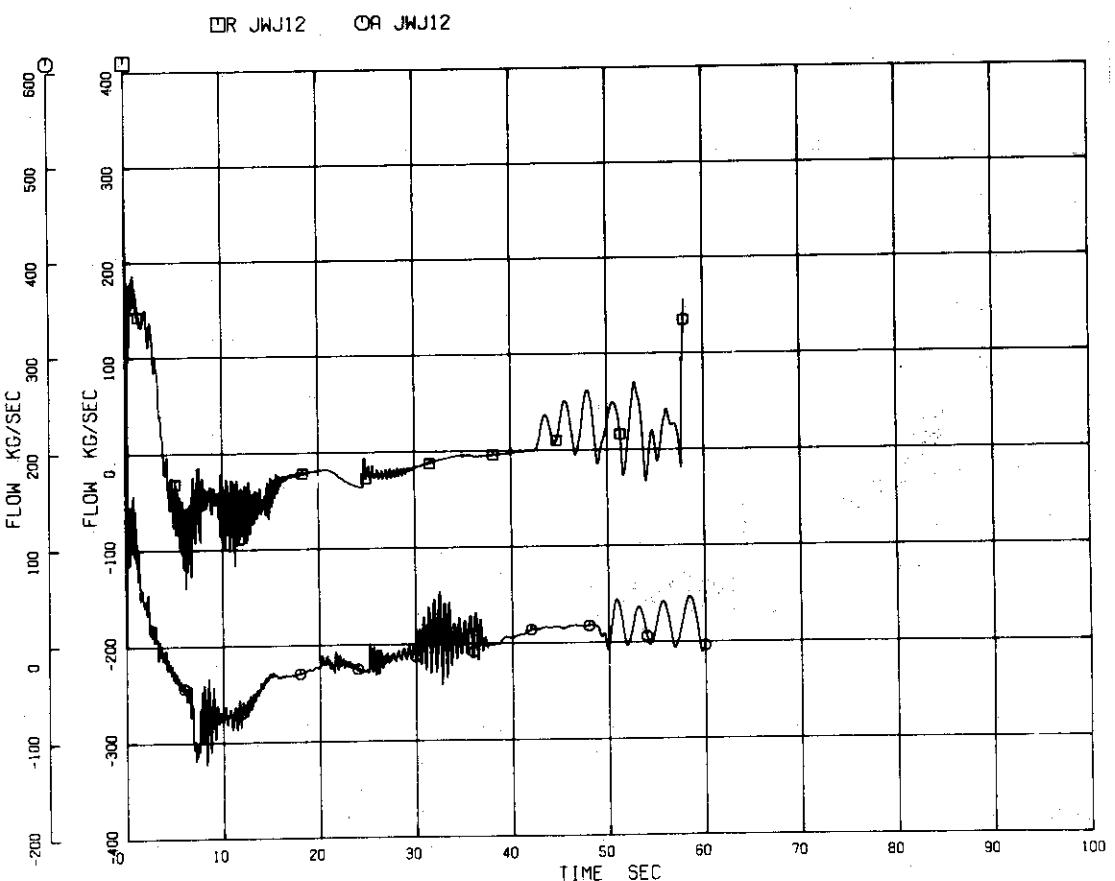


Fig. 5.32 Junction Flow From Downcomer to Lower Plenum

CSNI STANDARD PROBLEM L1-4

□R APV12 □R ATV12 △R APV12 +R ATV12

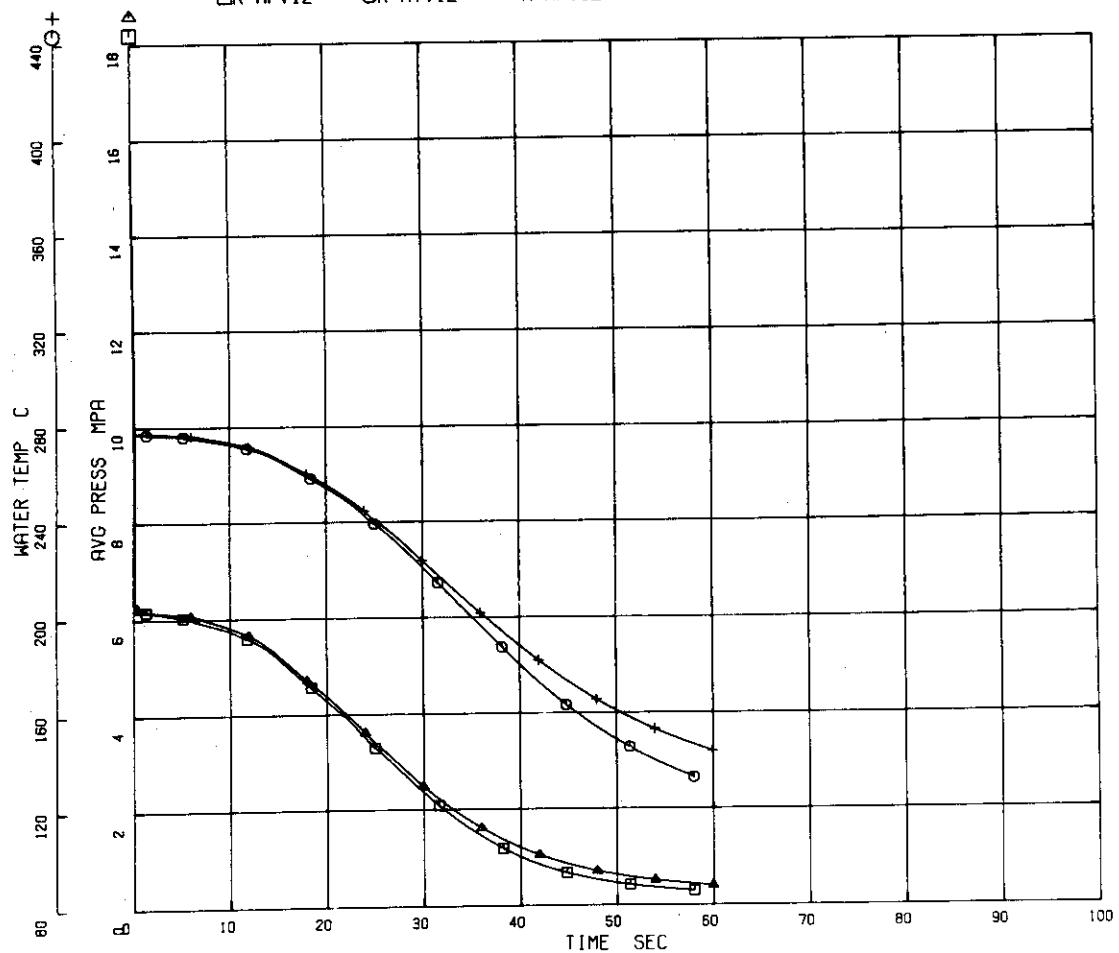


Fig. 5.33 Pressure and Temperature in Lower Plenum (PE-1ST-1A, TE-1ST-1A)
CSNI STANDARD PROBLEM L1-4

□R JWJ11 □R JWJ11

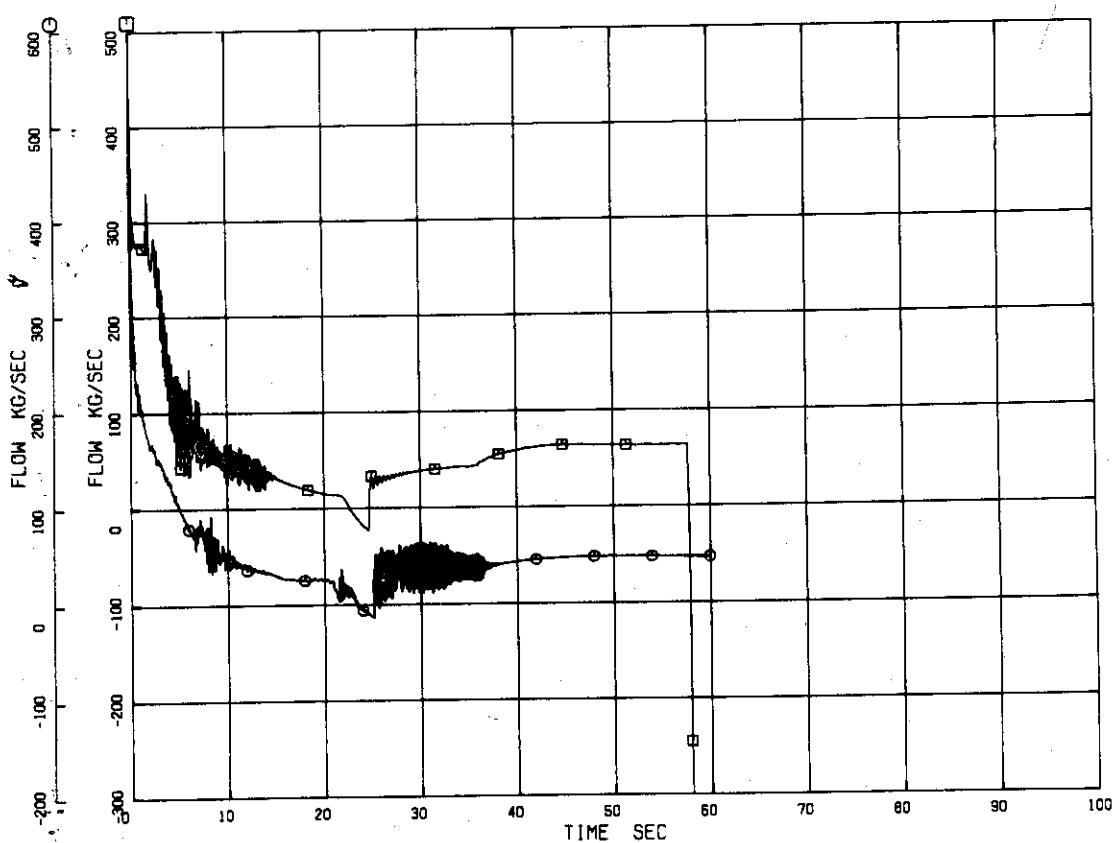


Fig. 5.34 Junction Flow From Intact Loop Cold Leg to Downcomer

CSNI STANDARD PROBLEM L1-4

□R JWJ24 □A JWJ24

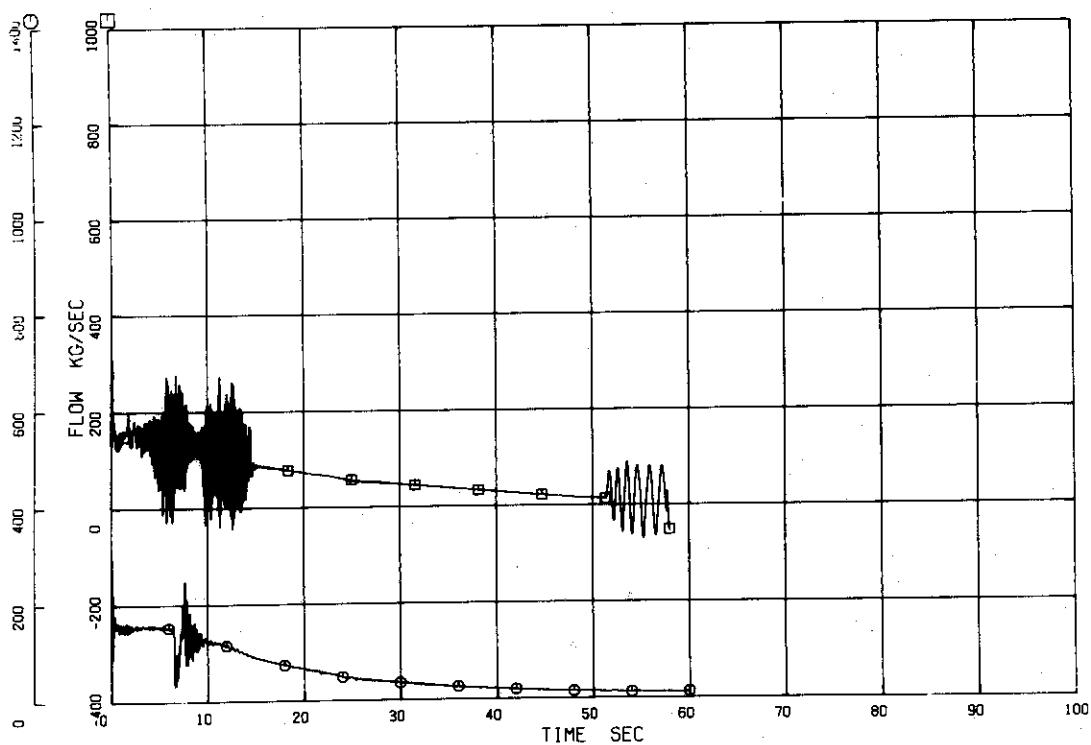


Fig. 5.35 Junction Flow From Downcomer to Broken Loop Cold Leg

CSNI STANDARD PROBLEM L1-4

□R MLV11 □A MLV11

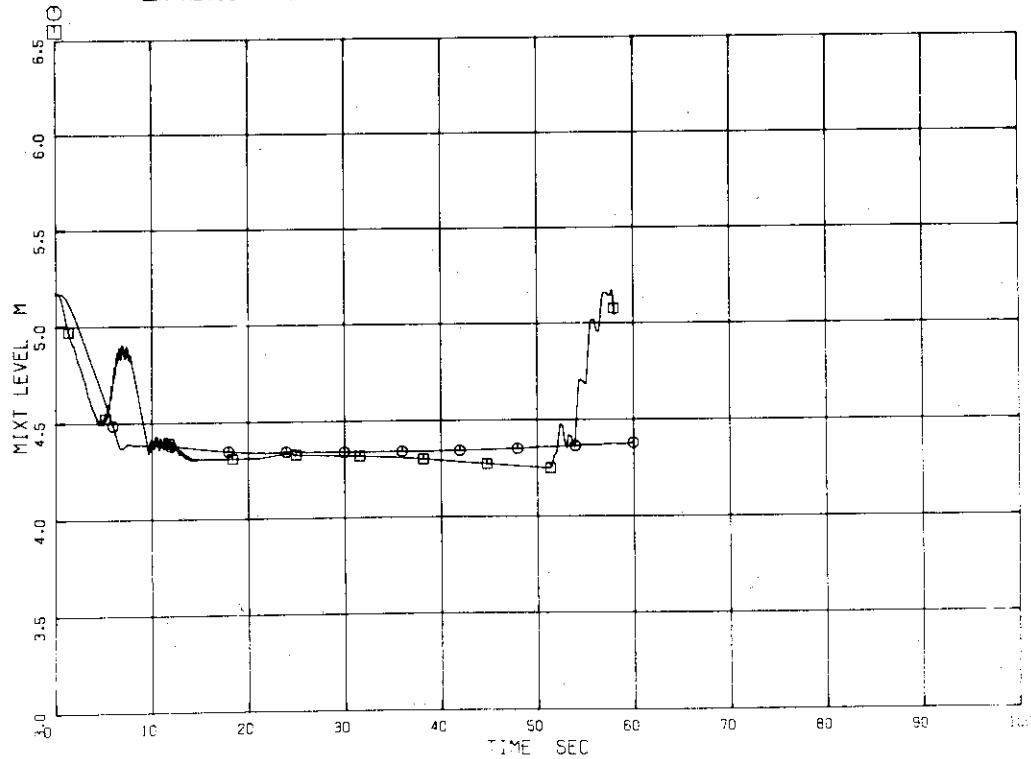


Fig. 5.36 Mixture Level in Downcomer (LE-1ST-2-1~12, LE-2ST-2-1~12)

CSNI STANDARD PROBLEM L1-4

□R ATV11 ○R APV11 △R ATV11 +R APV11

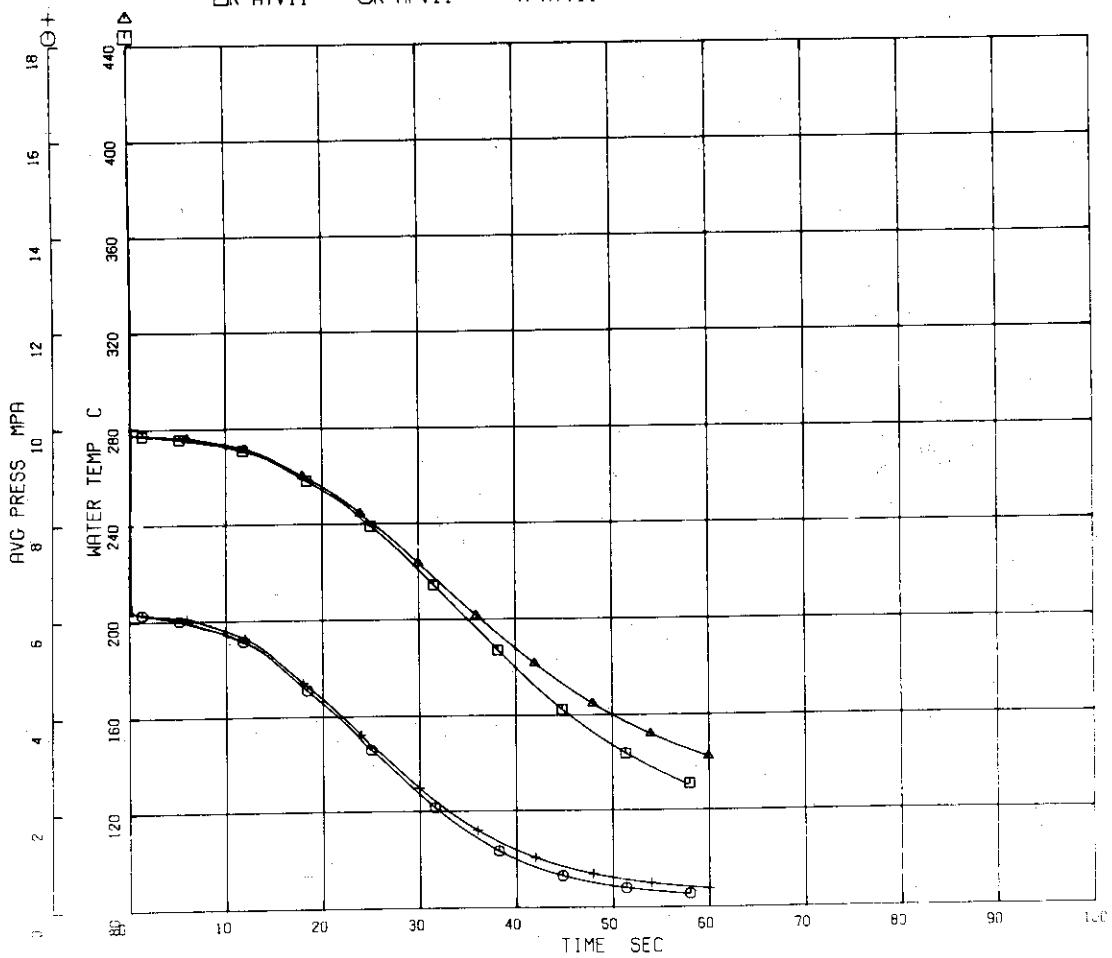


Fig. 5.37 Pressure and Temperature in Downcomer (PE-1ST-3, TE-1ST-1 ~ 6)

CSNI STANDARD PROBLEM L1-4

□R ATV22 ○R APV22 △R ATV22 +R APV22

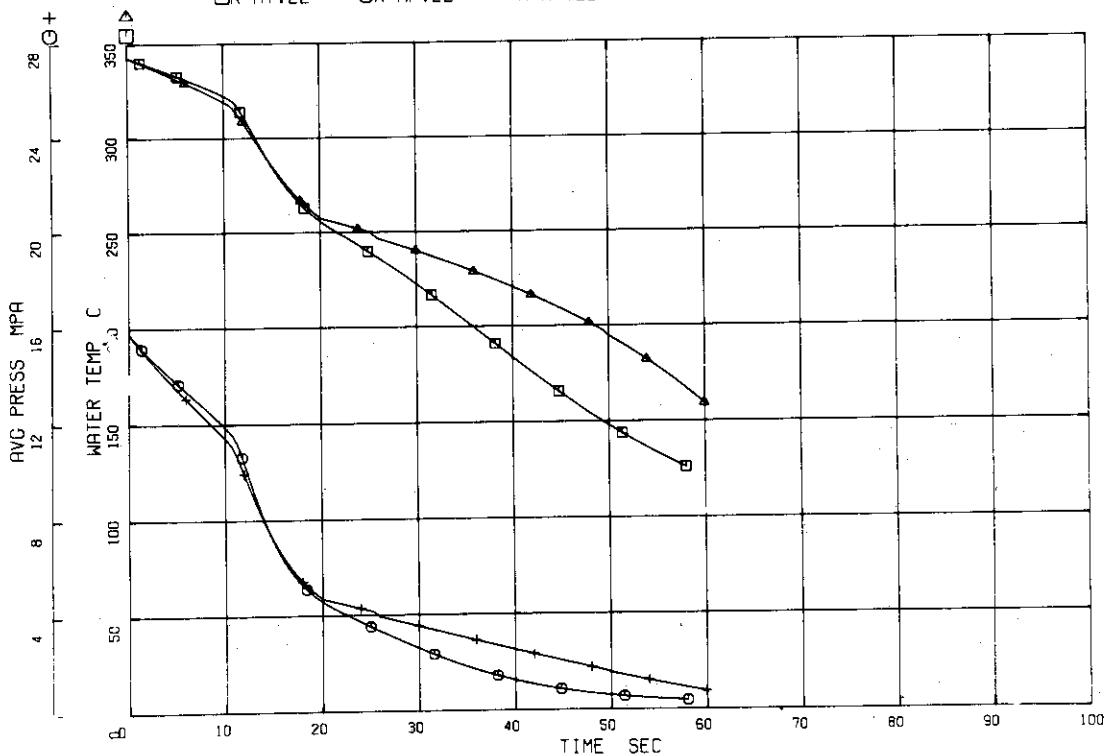


Fig. 5.38 Pressure and Temperature in Pressurizer (PE-PC-4, TE-P139-20)

CSNI STANDARD PROBLEM L1-4

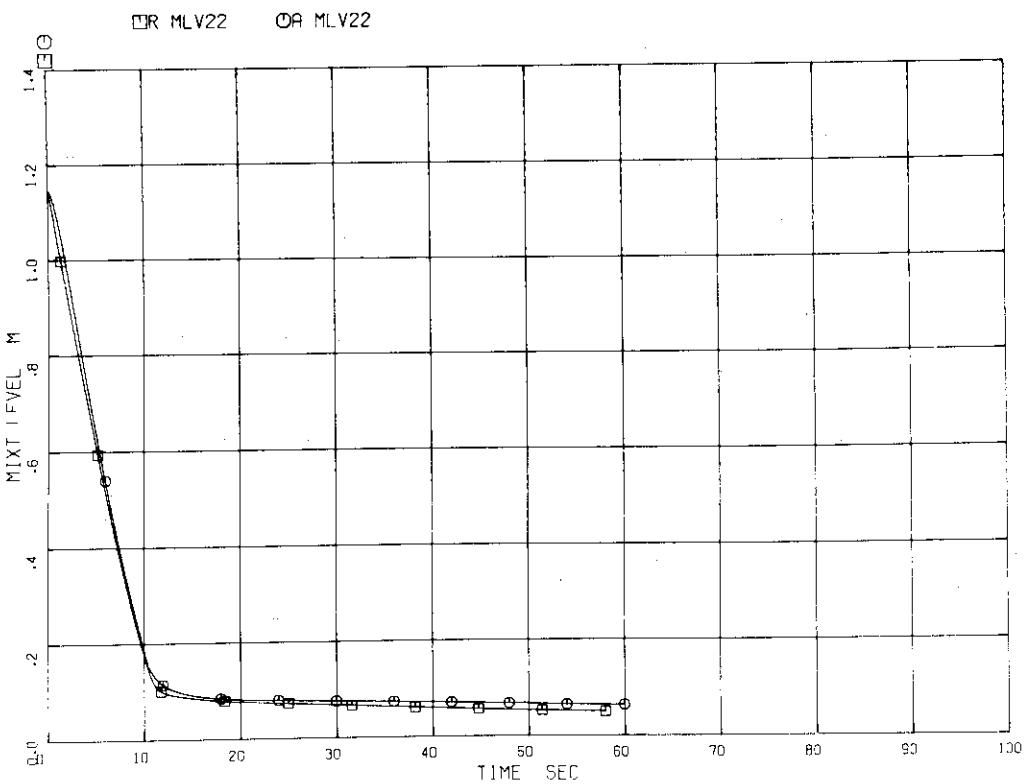


Fig. 5.39 Mixture Level in Pressurizer (LT-P139-6,7,8)

CSNI STANDARD PROBLEM L1-4

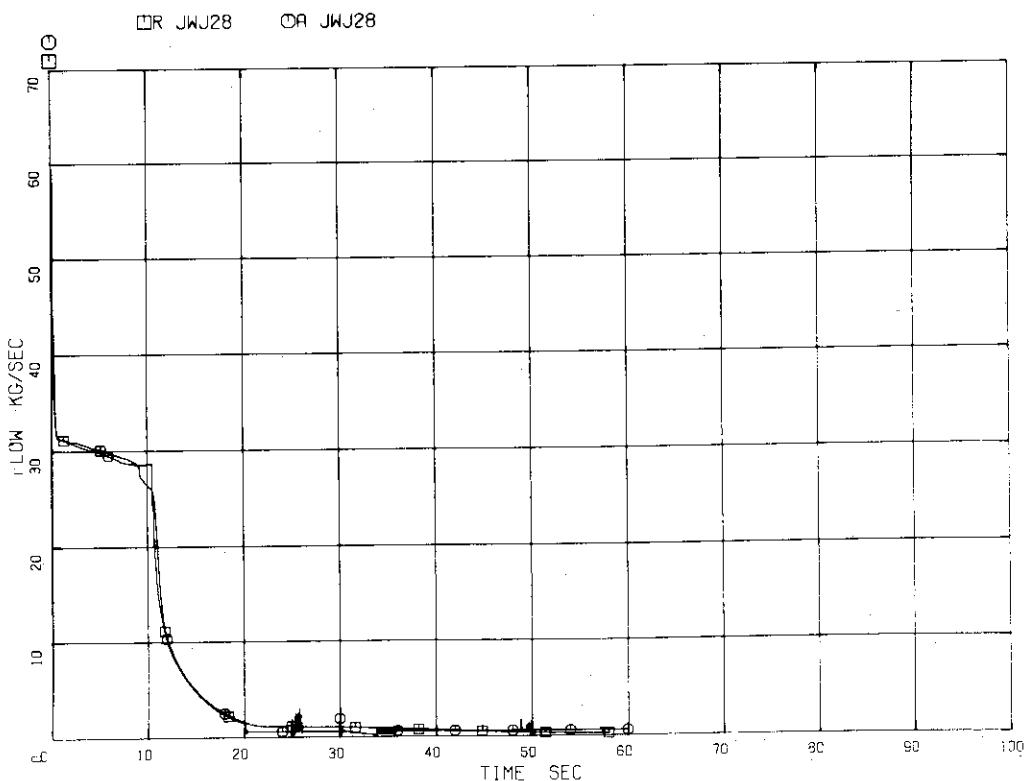


Fig. 5.40 Discharge Flow From Pressurizer Surge Line Outlet

CSNI STANDARD PROBLEM LI-4

JWJ27 JWJ27

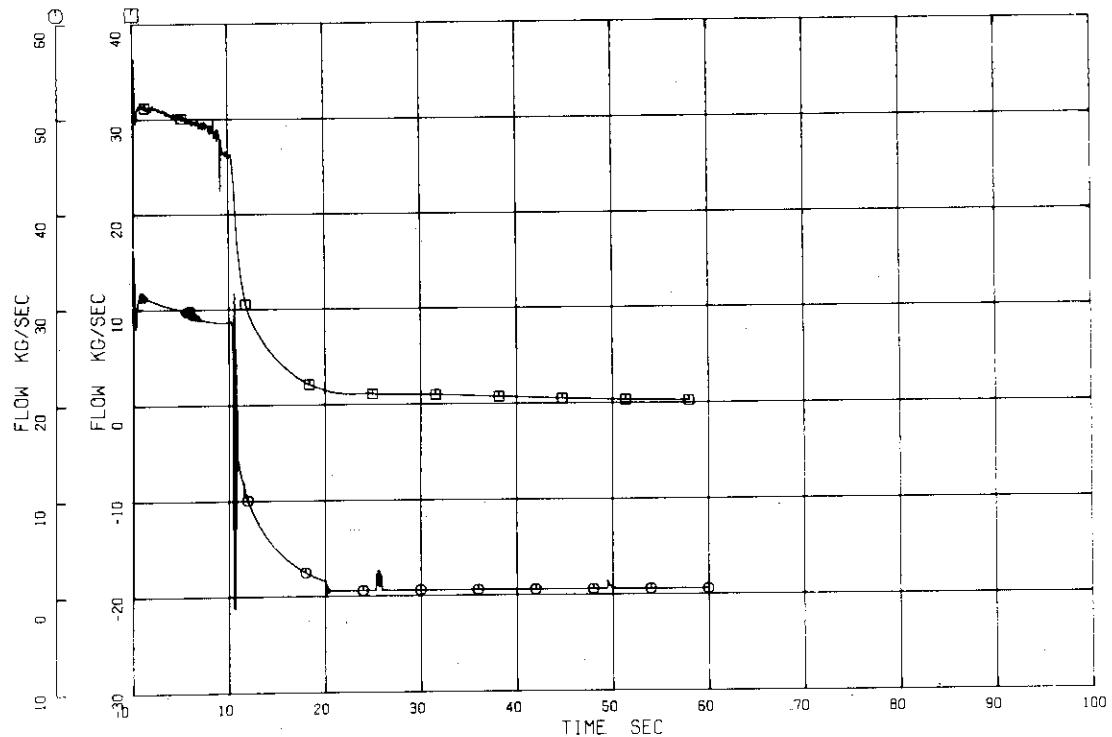


Fig. 5.41 Junction Flow at Pressurizer Surge Line Inlet

●—● RELAP-4J PMP 1 ○—○ RELAP-4J PUMP 2 △—△ ALARM-P1 PUMP 1 & 2

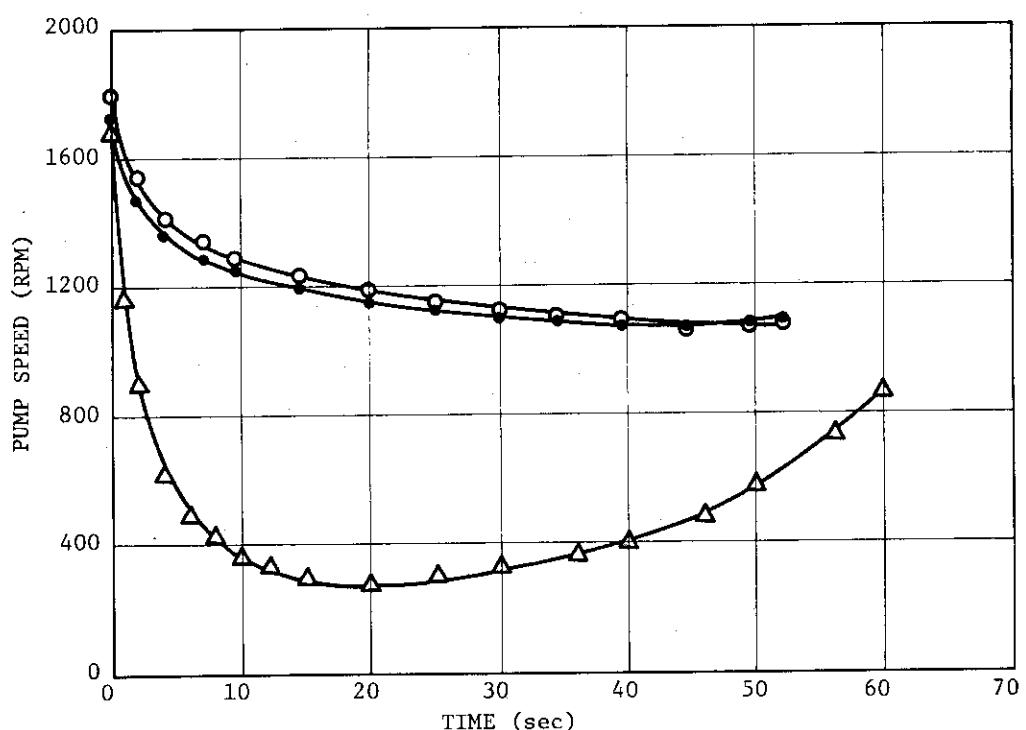


Fig. 5.42 Pump Speed

CSNI STANDARD PROBLEM L1-4

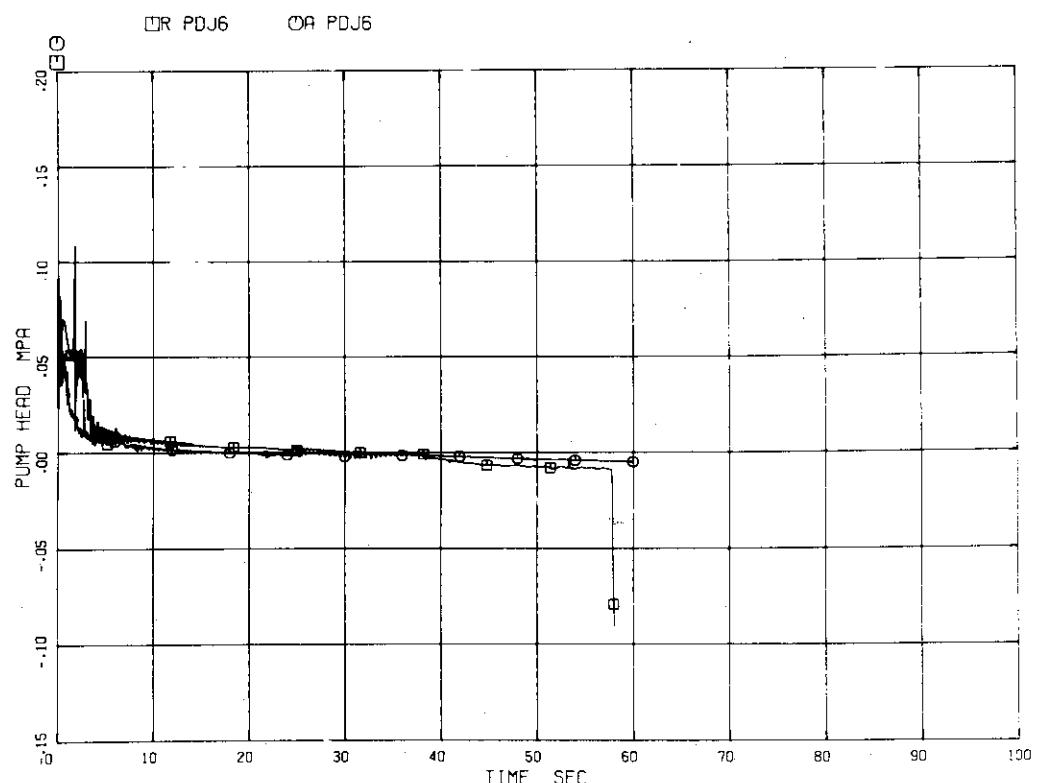


Fig. 5.43(a) Pump No.1 Head (PdE-PC-1)

CSNI STANDARD PROBLEM L1-4

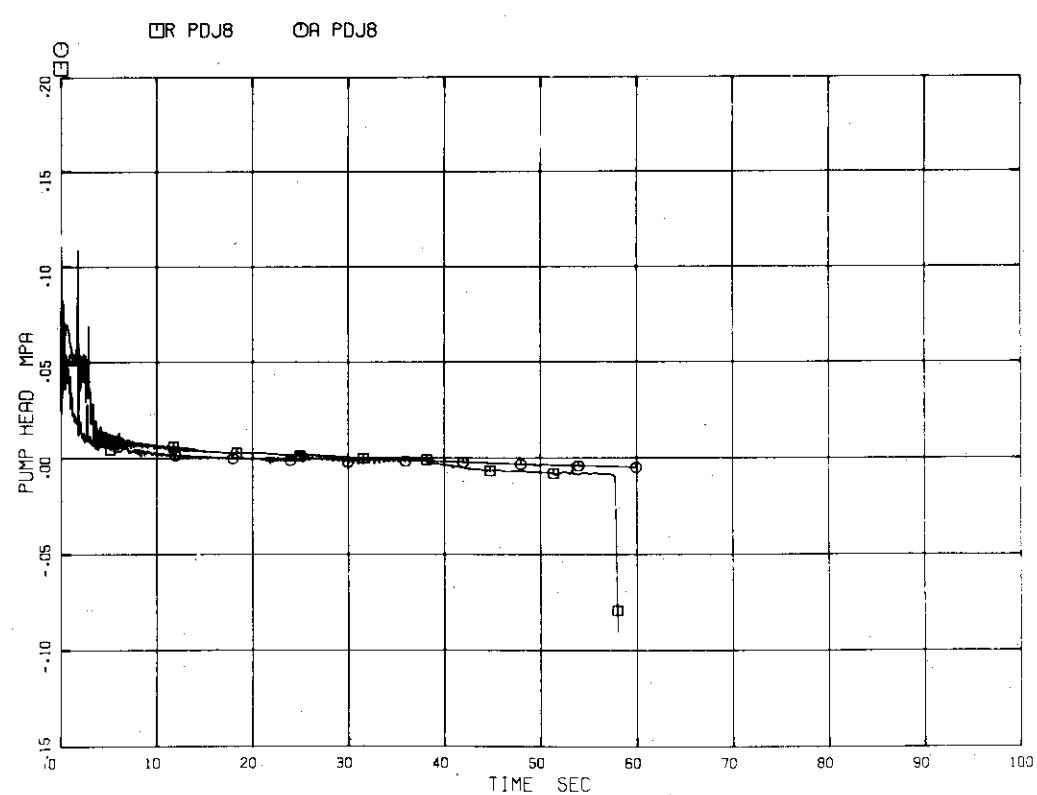


Fig. 5.43(b) Pump No.1 Head (PdE-PC-1)

CSNI STANDARD PROBLEM L1-4

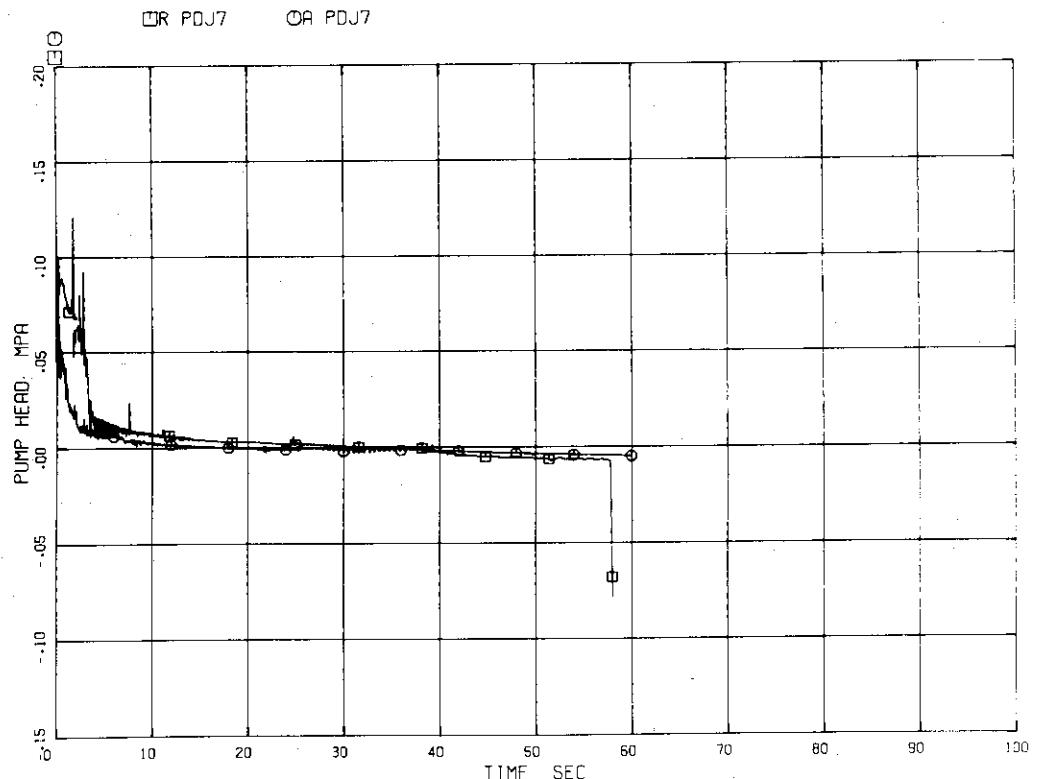


Fig. 5.44(a) Pump No.2 Head (PdE-PC-2)

CSNI STANDARD PROBLEM L1-4

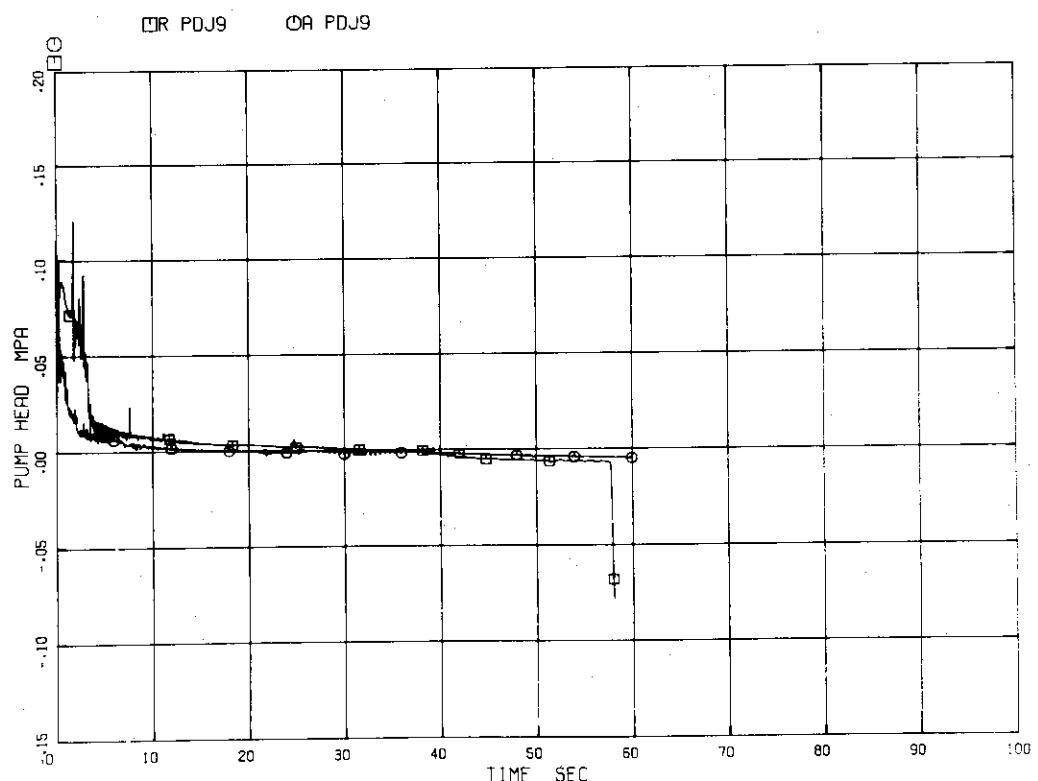


Fig. 5.44(b) Pump No.2 Head (PdE-PC-2)

CSNI STANDARD PROBLEM L1-4

□R APV26 □R ATV26 △R RPV31 +R ATV31

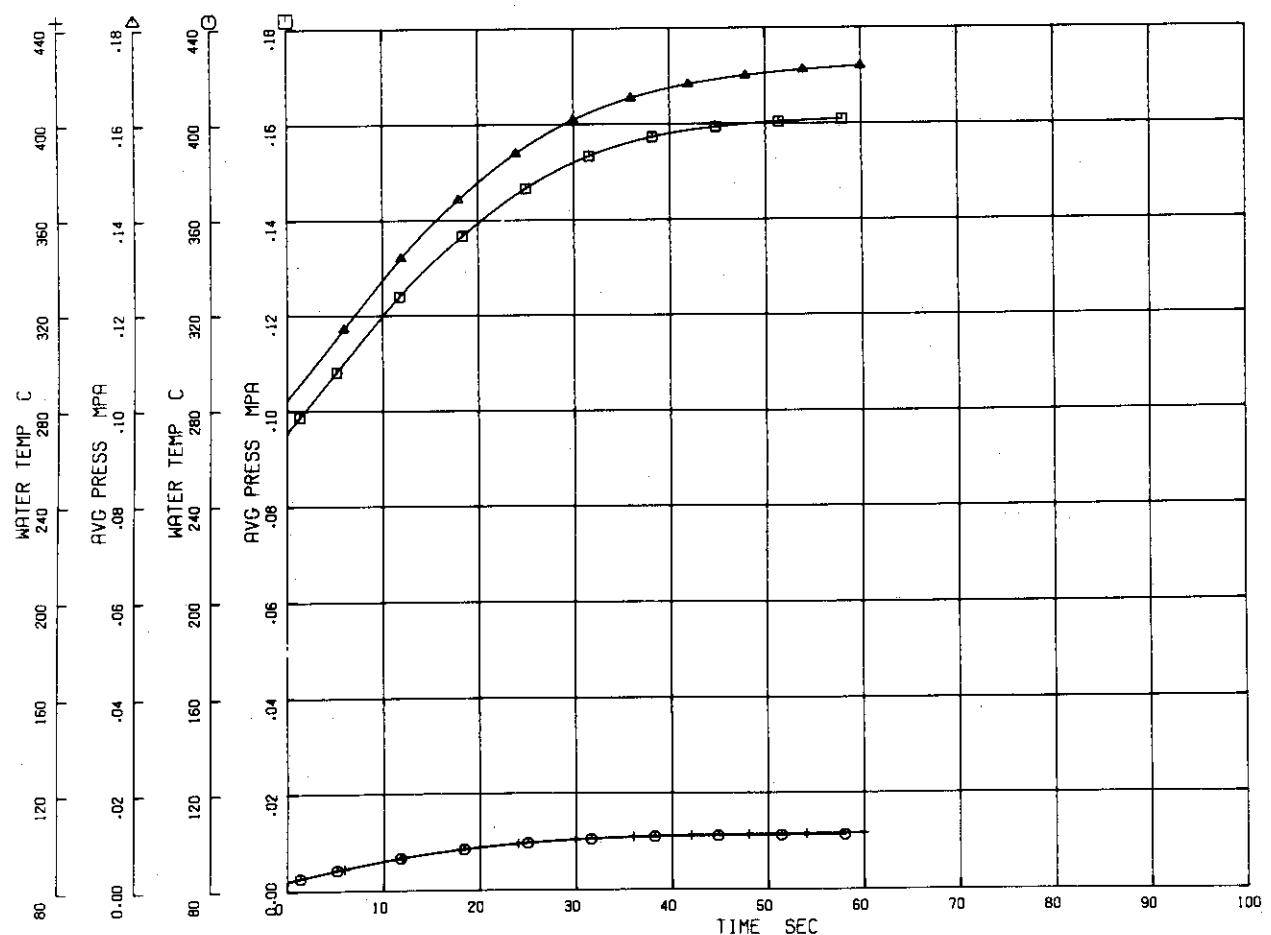


Fig. 5.45 Pressure and Temperature in Suppression Tank

CSNI STANDARD PROBLEM L1-4

□R MLV26 □R MLV31

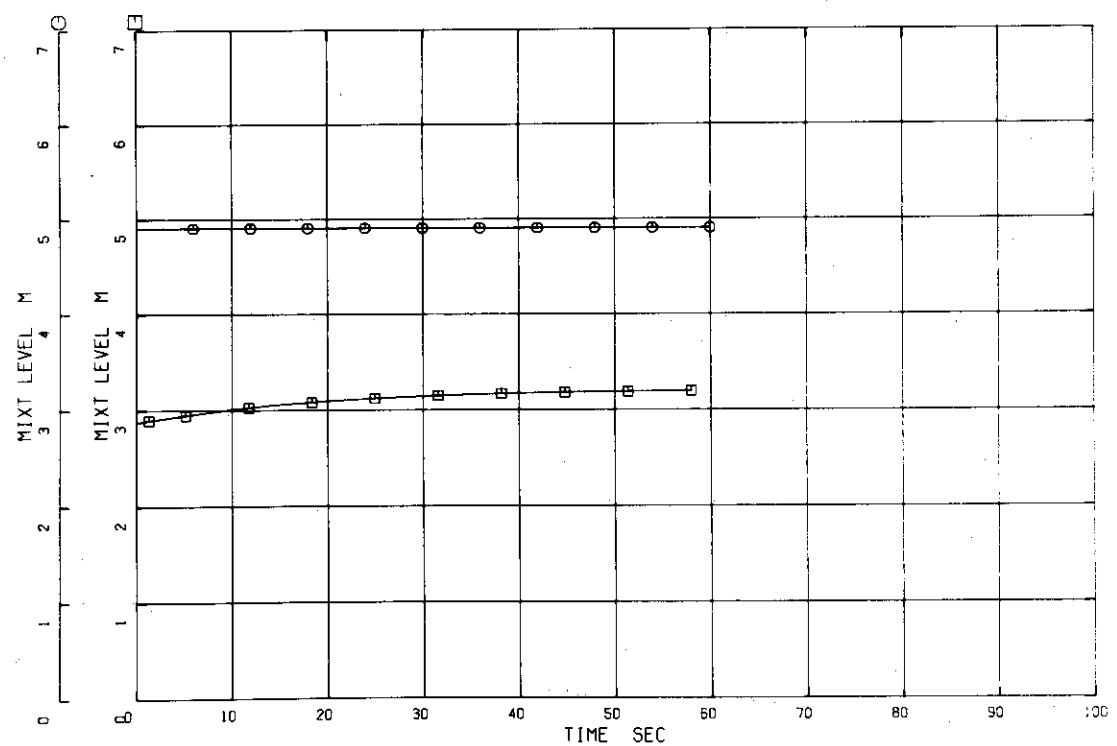


Fig. 5.46 Mixture Level in Suppression Tank

CSNI STANDARD PROBLEM L1-4

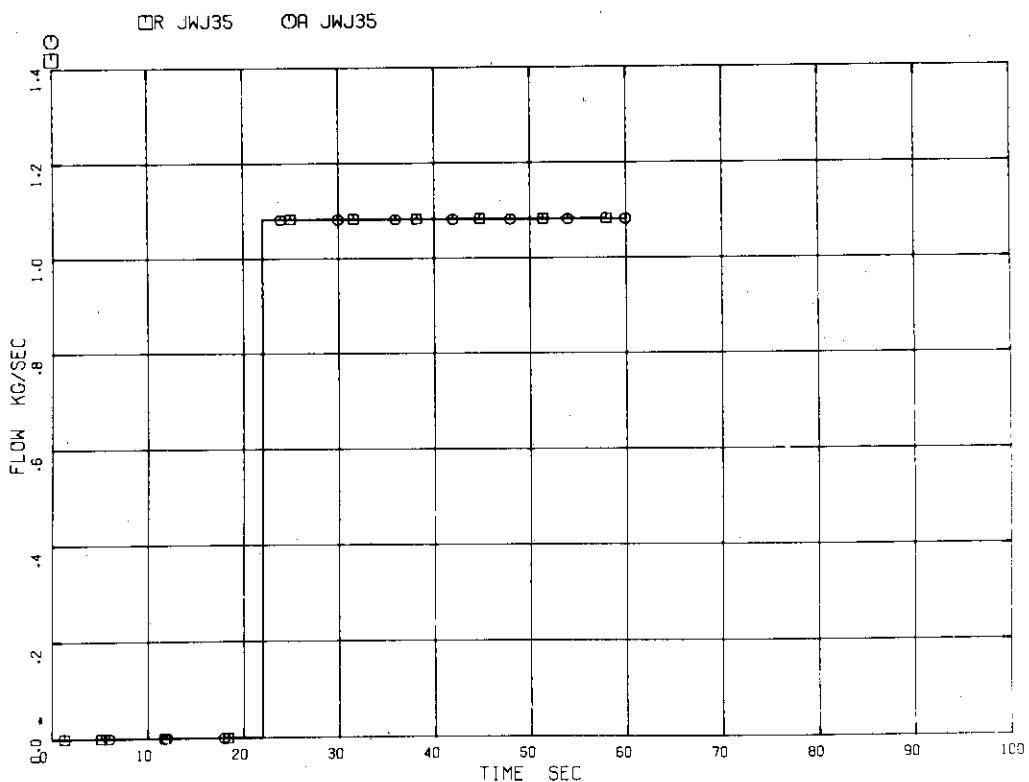


Fig. 5.47 HPIS Injection Flow

CSNI STANDARD PROBLEM L1-4

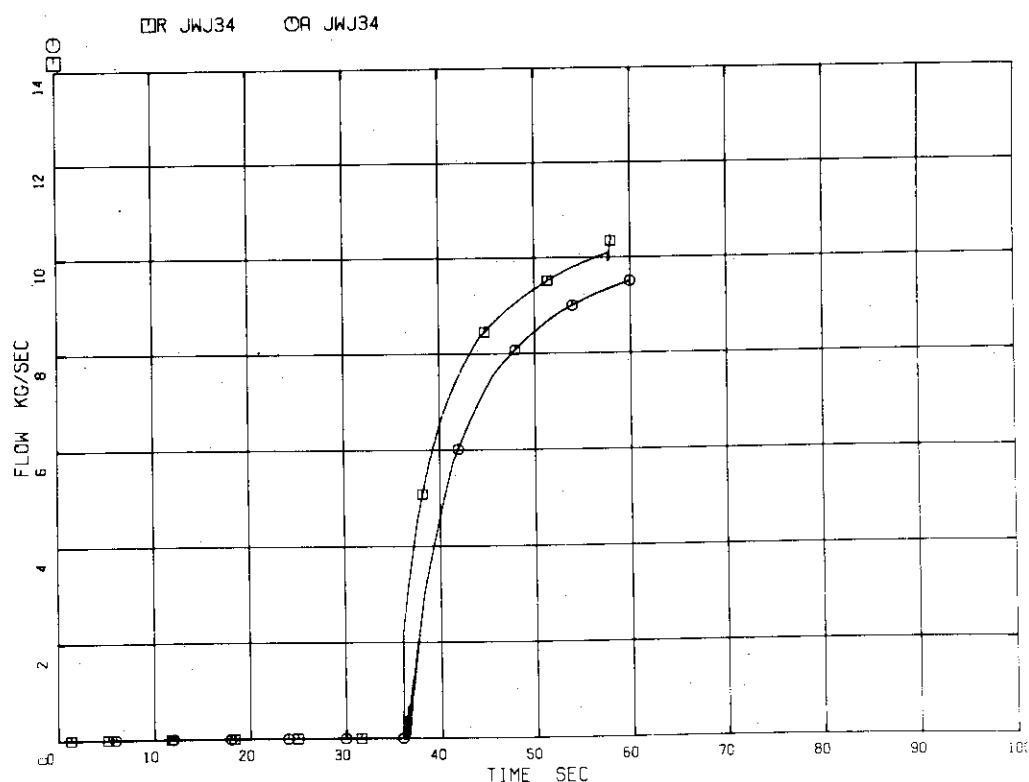


Fig. 5.48 LPIS Injection Flow

CSNI STANDARD PROBLEM L1-4

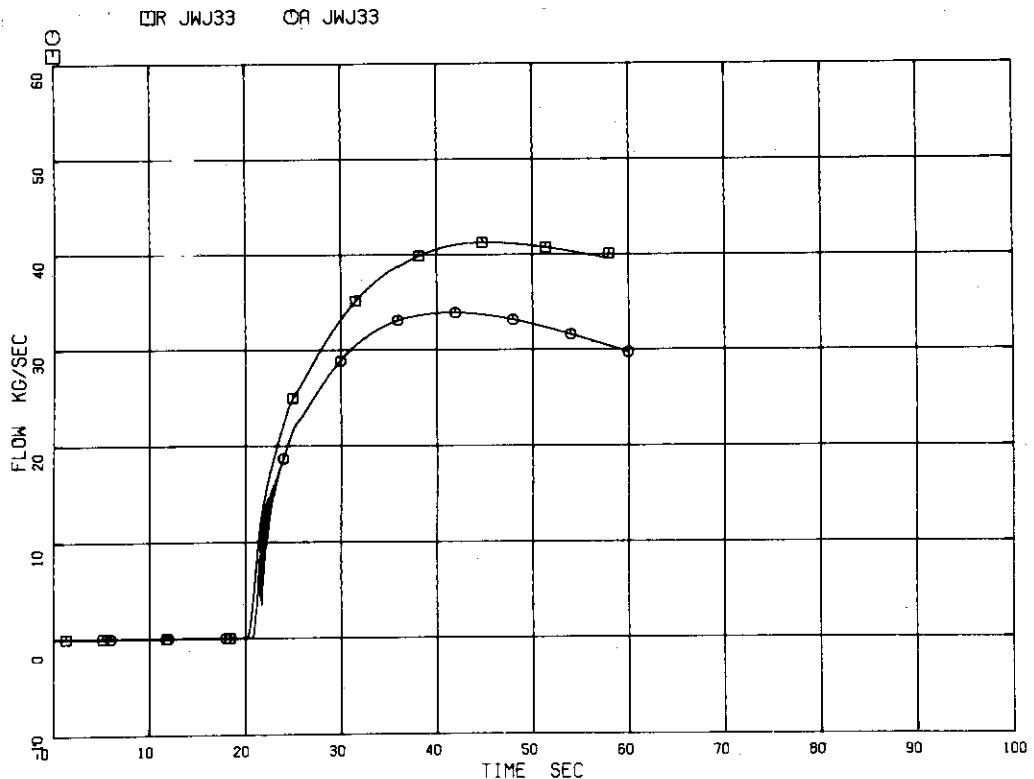


Fig. 5.49 Accumulator Injection Flow Rate

CSNI STANDARD PROBLEM L1-4

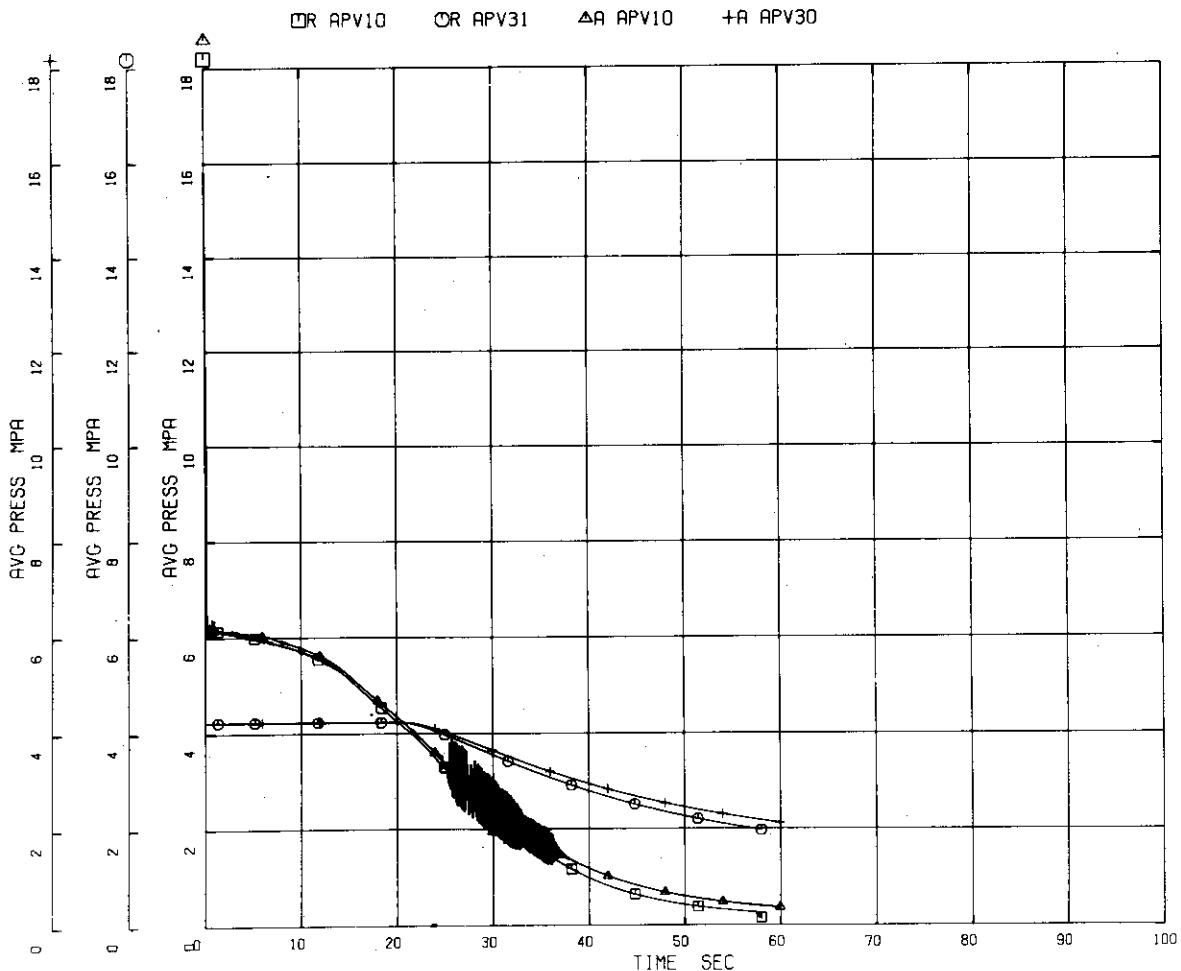


Fig. 5.50 Pressure in Accumulator and Cold Leg of Intact Loop

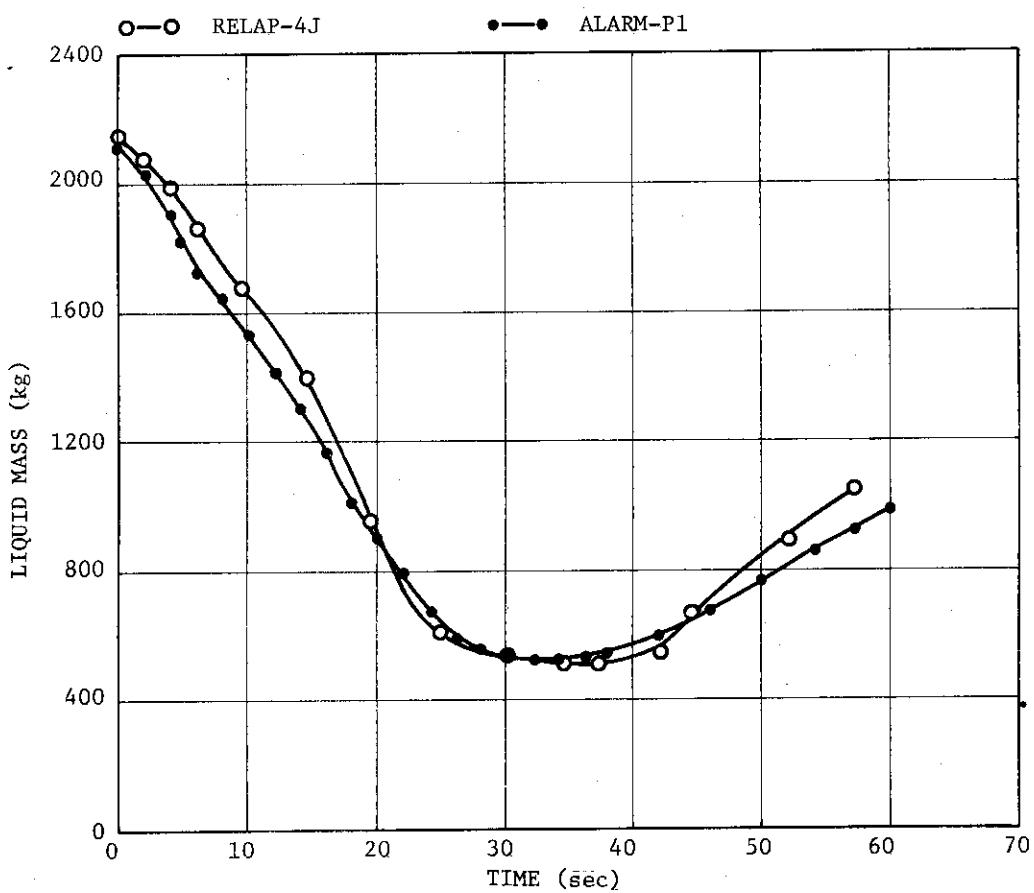


Fig. 5.51 Mass Inventory in Reactor Vessel

6. CONCLUSIONS

LOFT L1-4 experimental result was predicted by the LOFT analysis group and the code development group at JAERI with the use of RELAP-4J and ALARM-P1, respectively. For those analyses, input data were prepared by the analysis group and used for both analyses. Therefore any difference appeared in the analyses should be resulted from difference in code performance characteristics.

The present analysis leads to the following conclusions on LOFT L1-4 experiment and calculation model.

- (1) Predicted coolant behavior by RELAP-4J and ALARM-P1 is generally in excellent agreement despite the fact that several differences exist in computational models employed in the codes.
- (2) Major difference appears in coolant flow rate across the pump, i.e. ALARM-P1 predicts faster coastdown and smaller flow rate than RELAP-4J. The faster coastdown results in smaller pump head and it leads to earlier flow reversal in intact loop hot leg and core. The earlier flow reversal induces earlier back flow from steam generator inlet. The effect of earlier flow reversal and earlier back flow is felt by density in broken loop hot leg as the increase of coolant density. Although the timing of the density increase is earlier in ALARM-P1 results, qualitative agreement with RELAP-4J is satisfactory.
- (3) Due to the differences in the models, following differences are observed in predicted results.
 - (a) Explicit method used in ALARM-P1 seems to result in unstable calculation at a T shaped junction such as reflood assist line outlet when one of the two volumes connected by the junction is filled with subcooled water. This type of oscillation occurs at both reflood assist line outlets in broken loop cold leg and hot leg.
 - (b) Junction flow calculation in ALARM-P1 becomes unstable when mixture level assumed in upstream volume connected to the junction approaches the junction elevation. Thus ALARM-P1 analysis results in sudden change in junction quality and sudden flow rate change.
- (4) Computational models employed in RELAP-4J and ALARM-P1 need to be modified in common to better predict coolant behavior in the following components.

- (a) Coolant flow in downcomer predicted by RELAP-4J and ALARM-P1 seems unreasonable since counter current two phase flow is not well modeled in both codes. Thus modification is necessary.
 - (b) Heat transfer to and from steam generator secondary was not assumed in the present analysis. Although the effect of steam generator secondary is not significant during blowdown phase, steam generator plays an important role in determining coolant behavior during reflooding phase. Thus steam generator should be considered in future analysis.
 - (c) Suppression tank was simulated by one volume in RELAP-4J and ALARM-P1. It turned out that pressure rise due to vent pipe air clearance was not well predicted. Therefore further improvement is necessary including pressure rise due to compressed air in suppression tank.
- (5) Following instrumentations are suggested in future LOFT experiment.
- (a) Coolant condition (pressure, temperature, density) in reflood assist lines.
 - (b) Liquid level in steam generator.
 - (c) Emergency coolant condition in injection line.

Based on conclusions described above, future study on L1-4 experiment will be focused on improving computational models and its application to future LOFT analysis including nuclear test series.

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JAERI-M 7329

Appendix 1. Input Data List of RELAP-4J Analysis

LISTING OF INPUT DATA FOR CASE 1

```

1   *LOFT(L1=4) ANALYSIS
2   *
3   *      PROBLEM DIMENSIONS
4   *
5   010001 -2 9 7 7 28 2 0 33 2 1 1 3 2 2 1 0 0          * L1=4 INPUT
6   010002 -2 9 7 7 31 2 0 35 2 2 1 2 2 2 1 0 0          * L1=4 INPUT
7   CARD ABOVE IS REPLACEMENT CARD.
8   *
9   *      PROBLEM CONSTANT
10  010002 0.0 1.0
11  *
12  *      UNIT OPTION
13  010005 0 0           * INPUT=FT.LB  OUTPUT=FT.LB
14  *
15  *      EDIT VARIABLES
16  *
17  020000 AP 1 AP IV AP 15 AP 21 AP 22 AH 1 AR 10 AR 15 AH 21
18  *
19  *      TIME STEP
20  *
21  030010 20 2 2 0 0 0.0002 0.00001 0.1
22  030020 20 10 1 0 0 0.0005 0.00075 0.8
23  030030 10 20 1 0 0 0.001 0.0001 2.0
24  030040 5 10 4 0 0.01 0.00065 7.0
25  030050 5 50 4 0 0.001 0.00005 20.0
26  030060 5 50 4 0 0.01 0.00005 20.0
27  030070 5 50 2 0 0.01 0.0005 54.0
28  *
29  *      TRIM CONTROLS
30  *
31  040010 1 1 0 0 75.0 0.0           * END PROBLEM ON ELAPSED TIME
32  040020 1 -4 1 0 27.0 0.0           * END PROBLEM ON LOW PRESSURE IN VOL 1
33  040030 1 1 0 0 0.0 0.0           * ACTION 2 ON ELAP. TIME (PUMP)
34  040040 3 1 C 0 0.0 0.0           * ACTION 3 ON ELAP. TIME (LEAK)
35  040050 4 -4 29 0 612.4 0.6       * ACTION 4 ON ELAP. TIME (ACC)
36  040060 5 1 0 0 34.0 0.0           * ACTION 5 ON ELAP. TIME (LP15)
37  040070 6 1 0 0 22.0 0.0           * ACTION 6 ON ELAP. TIME (HPS)
38  *
39  *      VOLUME DATA
40  *
41  050011 0 3 2235.4 535.0 -1.0 4.92 0.932 0.932 0 0.6827 .932 -0.466
42  050021 0 0 2244.9 536.0 -1.0 2.42 0.932 0.932 0 0.6827 .932 -0.466
43  050031 0 0 2243.7 537.0 -1.0 5.85 1.26 1.26 0 0.6827 .932 -0.466
44  050041 0 0 2240.7 536.0 -1.0 24.9 11.25 11.25 0 1.6262 .0335 0.312
45  050051 0 0 2233.2 535.0 -1.0 24.9 11.25 11.25 0 1.6262 .0335 0.312
46  050061 0 0 2271.2 534.0 -1.0 6.17 5.57 5.53 0 0.6827 .932 -4.633
47  050071 0 0 2285.2 535.0 -1.0 6.055 4.947 4.947 0 0.6827 .932 -4.633
48  050081 0 0 2285.1 535.0 -1.0 6.035 4.937 4.937 0 0.6827 .932 -4.633
49  050091 0 0 2244.3 535.0 -1.0 4.02 0.932 0.932 0 0.6827 .932 -0.466
50  050101 0 0 2294.4 535.0 -1.0 5.29 0.932 0.932 0 0.6827 .932 -0.466
51  050111 0 0 2239.2 537.0 -1.0 33.3 16.963 16.963 0 1.363 .162 -13.96
52  050121 0 0 2236.5 537.0 -1.0 22.71 2.703 2.703 0 8.402 3.271 -16.365
53  050131 0 0 2233.1 536.0 -1.0 32.3 11.587 11.587 0 2.788 1.884 -13.662
54  050141 1 0 2281.2 535.0 -1.0 10.1 5.028 5.028 0 2.483 1.778 -2.075
55  050151 0 0 2295.4 535.0 -1.0 5.793 0.932 0.932 0 0.6827 .932 -0.466
56  050161 0 0 2283.9 535.0 -1.0 6.448 2.523 2.523 0 0.09 .339 -0.169
57  050171 0 0 2292.4 530.0 -1.0 11.89 9.476 9.476 0 1.137 1.203 2.354
58  050181 0 0 2255.4 530.0 -1.0 11.89 9.476 9.476 0 1.137 1.203 2.354
59  050191 0 0 2288.5 525.0 -1.0 1.764 6.80 6.80 0 0.276 .593 -4.445
60  050201 0 0 2285.4 527.0 -1.0 0.556 4.148 4.148 0 0.09 .339 -4.148
61  050211 0 0 2294.4 527.0 -1.0 4.893 0.932 0.932 0 0.6827 .932 -0.466
62  050221 0 0 2282.8 649.0 -0.0 34.0 5.5884 3.758 0 6.044 2.78 3.786
63  050231 0 0 2284.4 572.0 -1.0 0.228 3.382 3.382 0 0.0156 .161 0.466
64  050241 0 0 2284.5 535.0 -1.0 5.655 2.828 2.828 0 0.418 .729 -0.3646
65  050251 0 0 2293.9 530.0 -1.0 6.792 1.993 1.993 0 0.418 .729 0.466
66  050261 1 0 2 13.8 143.0 0.0 5709.9 16.094 9.42 0 230.0 17.1 -13.55
67  050271 0 0 2266.4 572.0 -1.0 0.144 .3386 .3386 0 0.09 .3386 -0.169
68  050281 0 0 2283.6 608.0 -1.0 0.224 0.664 0.664 0 0.0155 .140 3.707
69  *
70  *      INJECTION LINE NEAR VESSEL
71  *
72  050291 0 0 2294.4 690.0 -1.0 1.2 0.1458 0.1458 0 0.06681 0.29167 0.466
73  *
74  *      INJECTION LINE NEAR ACC TANK
75  *
76  050301 0 0 613.4 92.0 -1. 11.6 2.528 2.528 0 0.06681 0.29167 0.6118
77  *
78  *      ACC TANK
79  *
80  050311 2 0 613.4 92.0 0.0 130.0 9.58 6.5586 0 13.57 4.1567 0.6118
81  *
82  *
83  *      BUBBLE DATA
84  *
85  060011 0.8 3.0
86  060021 0.8 -3.0
87  *
88  *      JUNCTION DATA
89  *
90  080011 1 2 0 0 391.7 0.6827 0.0 ,0 0.0 0.0 0 1 2 0 0.0 0.0 1 0
91  080021 2 3 0 0 591.7 0.6827 0.0 ,0 0.0 0.0 0 1 2 0 0.0 0.0 1 0
92  080031 3 4 0 0 591.7 0.5564 0.734 ,0 0.0 0.0 0 1 2 0 0.0 0.0 1 0
93  080041 4 5 0 0 591.7 1.63 10.03 ,0 0.0 0.0 0 1 2 0 0.0 0.0 1 0
94  080051 5 6 0 0 591.7 0.5564 0.897 ,0 0.0 0.0 0 1 2 0 0.0 0.0 1 0
95  080061 6 7 1 0 295.0 0.6827 -4.167 ,0 0.0 0.0 0 1 2 0 0.0 0.0 1 0
96  080071 6 8 2 0 295.0 0.6827 -4.167 ,0 0.0 0.0 0 1 2 0 0.0 0.0 1 0
97  080081 7 9 1 0 295.9 0.3941 0.0 ,0 0.0 0.0 0 1 2 0 0.0 0.0 1 0
98  080091 8 10 2 0 295.8 0.3941 0.0 ,0 0.0 0.0 0 1 2 0 0.0 0.0 1 0
99  080101 9 10 0 0 591.7 0.6827 0.0 ,0 0.0 0.0 0 1 2 0 0.0 0.0 1 0
100 080111 10 11 0 0 591.7 0.6827 0.0 ,0 0.0 0.0 0 1 2 0 0.0 0.0 1 0
101 080121 11 12 0 0 591.7 1.84 -13.96 ,0 0.0 0.0 0 1 2 0 0.0 0.0 1 0
102 080131 12 13 0 0 591.7 2.826 -13.662 ,0 0.0 0.0 0 1 2 0 0.0 0.0 1 0
103 080141 13 14 0 0 591.7 0.5144 -2.075 ,0 0.0 0.0 0 1 2 0 0.0 0.0 1 0
104 080151 14 1 0 0 591.7 0.6827 0.0 ,0 0.0 0.0 0 1 2 0 0.0 0.0 1 0
105 080161 14 15 0 0 0.0 0.0 0.6827 0.0 ,0 0.0 0.0 0 1 3 0 0.0 0.0 1 0
106 080171 24 15 0 0 0.0 0.0 0.4176 0.0 ,0 0.5 0.5 0 1 2 0 0.0 0.0 1 0
107 080181 15 16 0 0 0.0 0.0 0.0 0.09 0.0 ,0 0.0 0.0 0 1 3 0 0.0 0.0 1 0
108 080191 16 17 0 0 0.0 0.0 0.09 2.354 ,0 1.52 1.09 0 1 2 0 0.0 0.0 1 0
109 080201 17 18 0 0 0.0 0.0 0.206 31.228 ,0 7.02 7.02 0 1 2 0 0.0 0.0 1 0
110 080211 18 19 0 0 0.0 0.0 0.0 2.354 ,0 1.09 1.52 0 1 2 0 0.0 0.0 1 0
111 080221 19 20 0 0 0.0 0.0 0.0 0.09 -3.979 ,0 17.1 17.1 0 1 2 0 0.0 0.0 1 0
112 080231 20 24 0 1 0.0 0.09 0.0 ,0 0.0 0.0 0 1 3 0 0.0 0.0 0.57 1 0 1
113 080241 21 21 0 0 0.0 0.0 0.6827 0.0 ,0 0.6 0.0 0 1 3 0 0.0 0.0 0.0 1 0
114 080251 25 21 0 0 0.0 0.0 0.4176 0.466 ,0 0.5 0.5 0 1 2 0 0.0 0.0 1 0
115 080261 21 27 0 0 0.0 0.0 0.09 0.0 ,0 0.0 0.0 0 1 3 0 0.0 0.0 0.0 1 0
116 080271 22 28 0 0 0.0 0.0 0.0504 4.181 ,0 0.0 0.0 0 1 3 0 0.0 0.0 0.57 1 0 1
117 080281 23 2 0 0 0.0 0.0 0.0 0.0156 0.466 ,0 0.95 0.44 0 1 2 0 0.0 0.0 0.57 1 0 1
118 080291 27 26 0 1 0.0 0.09 0.0 ,0 0.0 0.0 0 1 3 0 0.0 0.0 0.57 1 0 1
119 080301 28 23 0 0 0.0 0.0 0.0156 3.778 ,0 9.0 9.0 0 1 2 0 0.0 0.0 0.57 1 0 1
120  *
121  *      ACC INJECTION
122  *
123  080311 29 10 0 0 0.0 0.0645 0.466 .0 1.0 0.0 1 0 2 0 0.0 0.57 0 0 1
124  *
125  *      ACC CHECK VALVE
126  *
127  080321 30 29 0 2 0.0 0.0645 0.6118 0. 34.2 34.2 0 0 2 0 0.0 0.2866 0.57 0 0
128  *
129  *      ACCOUNTLET PIPING

```

130 *
 131 * 080331 31 30 C 0 0.0 0.06661 3.1398 0.0 38.6 0.0 1 0 2 0 0.0 0.57 0 0
 132 *
 133 *
 134 *
 135 * LPIS INJECTION
 136 *
 137 080341 0 29 1 0 0.0 0.0645 0.5389 .0 1.0 0.0 1 0 2 0 0.0 0.57 0 0 1
 138 *
 139 * HPIS INJECTION
 140 *
 141 080351 0 29 2 0 0.0 0.0645 0.5389 +0 1.0 0.0 1 0 2 0 0.0 0.57 0 0 1
 142 * PUMP CURVE INPUT INDICATORS
 143 100000 C 0 0 0
 144 100000 16 0 0 16
 CARD ABOVE IS REPLACEMENT CARD.
 145 *
 146 * PUMP DESCRIPTION
 147 *
 148 090011 1 3 1 1 3530, 0.6515 3000, 330, 443, 386, 46.02 110.7
 149 090011 1 3 1 1 3530, 0.6515 5000, 330, 443, 294, 46.02 110.7
 CARD ABOVE IS REPLACEMENT CARD.
 150 090011 1 3 1 1 3530, 0.6515 3000, 408.95 465, 340, 38.75 40.0522
 CARD ABOVE IS REPLACEMENT CARD.
 151 090021 1 3 1 1 3530, 0.6515 5000, 330, 443, 386, 46.02 110.7
 152 090021 1 3 1 1 3530, 0.6515 3000, 330, 443, 294, 46.02 110.7
 CARD ABOVE IS REPLACEMENT CARD.
 153 090021 1 3 1 1 3530, 0.50E2322 3000, 408.95 465, 340, 38.75 46.529
 CARD ABOVE IS REPLACEMENT CARD.
 154 *
 155 * PUMP HEAD MULTIPLIER
 156 *
 157 091001 -11 0, 0, .1 0, .15, .05, .24, .8, .3, .96, .6, .98
 158 091002 .6, .97, .8, .9, .8, .96, .5, 1, 0,
 159 *
 160 * PUMP TORQUE MULTIPLIER
 161 *
 162 092001 -7 0, 0, .1 0, .15, .05, .24, .56, .8, .56, .96, .45, 1, 0,
 163 *
 164 * PUMP HEAD AND TORQUE DATA
 165 *
 166 101011 1 1 6 0, 1.4036, 1.19061, 1.3036, .38963 1.3186
 167 101012 .59396, 1.2328, .7302, 1.1336 1, 1.0078
 168 101021 1 2 3 0, .67, .2, .5, .4, .22
 169 101022 .57554, .74432, .7583, .77348, .3776
 170 101023 .86313, .6326, 1, 1.0078
 171 101031 1 3 6 -.1, 2.4722, .80574, 2.0474, -.6069, 1.831
 172 101032 -.40683, 1.674, .200171, 1.4705 0, 1.4036
 173 101041 1 4 8 -.1, 2.4722, .82297, 1.9986, -.61332, 1.5897
 174 101042 -.45534, 1.3779, -.27109, 1.1949, -.17716, 1.0605
 175 101043 .0, .90973, 1.0155, 0, .394273
 176 101051 1 5 7 .25, .2, .28, .4, .34
 177 101052 .4118, .2768, .59763, .4584, .763467, .7492
 178 101053 1, .9465
 179 102061 1 6 10 0, .934279, .941099, .9229, .186509, .6863
 180 102062 .271762, .875, .455872, .8433, .574406, .6835
 181 102063 .740576, .9465, .766119, .8469, .871471, .6838
 182 102064 1, .9465
 183 102071 1 7 6 -.1, .8, -.63, -.6, -.3
 184 102072 .4, -.105, .2, .15, .0, .25
 185 102081 1 8 6 -.1, .8, .97, .6, .95
 186 102082 .4, .58, .2, .8, .0, .67
 187 102091 2 1 6 0, .6032, .1939, .6325, .393, .7369
 188 102092 .59552, .6331, .79782, .9229, 1, .9672
 189 102101 2 2 7 0, .67, .4, .25, .5, .15
 190 102102 .737255, .524566, .768049, .606594, .86723, .74366
 191 102103 1, .9672
 192 102111 2 3 6 -.1, 1.9443, -.80095, 1.394, -.00638, 1.0975
 193 102112 .40686, .872, .199224, .6646, 0, .6532
 194 102121 2 4 8 -.1, 1.9343, -.42234, 1.8308, -.63371, 1.6624
 195 102122 .45534, .557, .267023, 1.4362, -.176107, 1.3879
 196 102123 .68931, .3481, 0, 1.23361
 197 102131 2 5 6 0, .45, .4, .25, .5, 0,
 198 102132 1, .3669
 199 102141 2 6 10 0, 1.23361, .990643, 1.1965, .188569, 1.1096
 200 102142 .27347, 1.0416, .456649, .6958, .574448, .7807
 201 102143 1, .6134, .763852, .5849, .870057, .4877
 202 102144 .3569
 203 102151 2 7 4 -.1, .3, -.3, -.9, -.1, -.5, -.5
 204 102152 0, -.45, .25, .8, .08, -.8
 205 102161 2 8 4 -.1, .1, -.25, .8, .08, -.8
 206 102162 0, .67
 207 104011 1 1 7 0, 0, .1, .83, .2, 1.04, .5, 1.02, .7, 1.01, .9, .94, 1, 1,
 208 104021 1 2 8 0, 0, .1, .83, .2, 0, .3, 1.49, .21, .3, .67, .9, .8, 1, 1,
 209 104031 1 3 10 -.1, -.15, -.9, -.1, .24, -.6, -.17, -.7, -.2, .36, -.6, -.27, -.5, 2.91
 210 104042 -.6, -.2, .67, -.25, -.1, .69, -.1, -.5, 0, 0,
 211 104041 1 4 10 -.1, -.15, -.4, -.78, -.6, -.5, -.7, -.31, -.6, -.17, -.5, -.05
 212 104042 -.35, 0, -.2, .65, -.1, .06, 0, .11
 213 104051 1 5 6 0, 0, 2, -.34, .4, -.65, -.1, -.93, .8, -.19, 1, -.1, -.47
 214 104061 1 6 10 0, .11, .1, .13, .25, .13, .4, .13, .5, .07, .6, -.04, .7, -.23
 215 104062 .8, -.51, .7, -.91, 1, -.1, 1.47
 216 104071 1 7 2 -.1, 0, .5, 0
 217 104081 1 8 2 0, .1, 0, .5, 0
 218 104091 2 1 6 0, .6632, .193, .6325, .393, .7369
 219 104092 .59352, .6331, .79782, .9229, 1, .9672
 220 104101 2 2 7 0, .67, .4, .25, .5, .15
 221 104102 .737255, .526566, .768049, .606594, .86723, .74366
 222 104103 1, .9672
 223 104111 2 3 6 -.1, 1.9443, -.80095, 1.394, -.00638, 1.0975
 224 104112 .40686, .872, .199224, .6646, 0, .6532
 225 104121 2 4 8 -.1, 1.9343, -.42234, 1.8308, -.63371, 1.6624
 226 104122 .45534, .557, .267023, 1.4362, -.176107, 1.3879
 227 104123 .68931, 1.3481, 0, 1.23361
 228 104131 2 5 4 0, .45, .4, .25, .5, 0, 1, .3569
 229 104141 2 6 10 0, 1.23361, .990643, 1.1965, .188569, 1.1096
 230 104142 .27347, 1.0416, .456649, .6958, .574448, .7807
 231 104143 .73816, .6134, .763852, .5849, .870057, .4877
 232 104144 1, .3569
 233 104151 2 7 4 -.1, -.1, -.3, .7, -.1, -.5, 0, -.45
 234 104161 2 8 4 -.1, -.1, -.25, -.9, -.08, -.8, 0, -.67
 235 *
 236 * VALVE DATA
 237 110010 -3 0.0 0.0 0.0 0.0
 238 *
 239 * CHECK VALVE DATA FOR ACC INJECTION
 240 *
 241 110020 -4 C+C C+C C+C
 242 *
 243 * LEAK TABLE
 244 *
 245 120100 3 2 27.0 0.0 0.0 0.02 1.0 100.0 1.0
 246 120100 3 2 53.0 0.0 0.0 0.02 1.0 100.0 1.0
 CARD ABOVE IS REPLACEMENT CARD.
 247 *
 248 * FILL TABLE (LPIS)
 249 *
 250 130100 14 5 1 1 100, 78, *LPIS INJECTION
 251 130101 0, 2667, 20, 2589, 40, 2491, 60, 2326, 80, 2186, 100, 2047,
 130102 120, 1660, 140, 1659, 160, 1411, 160, 1116, 200, 729, 220, 263.6
 252 130103 226, 0, 5000.0 0.0
 253 *
 254 * FILL TABLE (HPIS)

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256 *
257 130260 2 6 1 1 105, TR. SPHTS INJECTION
258 130261 0 1 266.7 3600. 266.7
259 *
260 *
261 150011 0 11 1 0 0.0 820.3 432.5 0.0 0.0
262 150021 0 22 2 0 0.0 64.3 14.1 0.0 0.0
263 1701C1 1 1 1 0 0.0 0.50 0.0
264 170261 1 1 1 0 0.0 0.25 0.0
265 *
266 * THERMAL PROPERTIES
267 1801C1 -2 0 0.0 55364 * THERMAL CONDUCTIVITY
268 1801C2 212. 9.574 2372. 19.294
269 1901C1 -13 0 0.0 55364 * HEAT CAPACITY
270 1901D2 170. 44.46941 250. 44.37946 400. 44.68772
271 1901D3 800. 45.39201 800. 46.90036 1000. 48.84151
272 1901D4 1230. 50.99036 1400. 53.15849 1500. 55.14803
273 1901D5 1860. 56.76590 2000. 57.74932 2200. 58.06550
274 1901D6 2400. 57.36161
275 *

Appendix 2. Input Data List of ALARM-P1 Analysis

ALARM-P (VERSION 1) PWR LOSS OF COOLANT ANALYSIS PROGRAM
***** LISTING OF INPUT DATA *****

| NO. |1....2....3....4....5....6....7....8 | LFT00000 |
|-----|---|----------|
| 1 | /* | LFT00010 |
| 2 | /* LOFT(L1-4) ANALYSIS BY ALARM-P1 | LFT00020 |
| 3 | /* CSNI STANDARD PROBLEM NO.5 BY ALARM-P1(MOD1) | LFT00030 |
| 4 | /* | LFT00040 |
| 5 | /* PROBLEM DIMENSION | LFT00050 |
| 6 | /* | LFT00060 |
| 7 | /* -3 18 6 9 31 1 35 2 1 3 0 2 1 0 1 1 0 0 0 | LFT00070 |
| 8 | /* | LFT00080 |
| 9 | /* EDIT VARIABLE | LFT00090 |
| 10 | /* | LFT00100 |
| 11 | AP NI AP N10 AP N15 AP N21 AP N22 AR NI AR N10 AR N15 AR N21 | LFT00110 |
| 12 | AP N14 AP N11 AP N9 JW J31 JW J11 JW J10 JW J12 AP N28 AP N30 | LFT00115 |
| 13 | /* | LFT00120 |
| 14 | /* TIME STEP CONTROL | LFT00130 |
| 15 | /* | LFT00140 |
| 16 | 500 10 1 1000 0.00001 0.05 | LFT00150 |
| 17 | 200 30 1 200 0.00005 0.30 | LFT00160 |
| 18 | 500 20 1 100 0.0001 1.00 | LFT00170 |
| 19 | 200 10 1 20 0.0005 5.00 | LFT00180 |
| 20 | 500 10 1 10 0.001 20.00 | LFT00190 |
| 21 | 500 20 1 10 0.001 80.00 | LFT00200 |
| 22 | /* TRIP CONTROL | LFT00210 |
| 23 | /* | LFT00220 |
| 24 | 1 1 0 0 60.0 0.0 | LFT00230 |
| 25 | 1 -4 1 0 1,899E4 0.0 | LFT00240 |
| 26 | /* (TWO PUMPS) | LFT00250 |
| 27 | 41 1 0 0 0.0 0.0 | LFT00260 |
| 28 | 62 1 0 0 0.0 0.0 | LFT00270 |
| 29 | /* (LPIS INJECTION --- FILL SYSTEMS) | LFT00271 |
| 30 | 51 1 0 0 36.0 0.0 | LFT00272 |
| 31 | /* (HPIS INJECTION --- FILL SYSTEMS) | LFT00273 |
| 32 | 52 1 0 0 22.0 0.0 | LFT00274 |
| 33 | /* (ACC INJECTION --- FILL SYSTEMS) | LFT00275 |
| 34 | 6 -4 28 0 43.14E4 0.0 | LFT00276 |
| 35 | 7 1 0 0 0.0 0.0 | LFT00277 |
| 36 | 8 1 0 0 0.0 0.0 | LFT00278 |
| 37 | /* VOLUME DATA | LFT00280 |
| 38 | /* | LFT00290 |
| 39 | /* | LFT00300 |
| 40 | /* | LFT00310 |
| 41 | 0 0 160.7172995E+4 279.444 -1.0 0.13933 0.2840736 | LFT00320 |
| 42 | 0.2840736 0.06342 0.2840736 -0.1420368 0.0 | LFT00330 |
| 43 | 0 0 160.6821378E+4 280.000 -1.0 0.06853 0.2840736 | LFT00340 |
| 44 | 0.2840736 0.06342 0.2840736 -0.1420368 0.0 | LFT00350 |
| 45 | 0 0 160.5977496E+4 280.556 -1.0 0.16267 0.384048 | LFT00360 |
| 46 | 0.384048 0.06342 0.2840736 -0.1420368 0.0 | LFT00370 |
| 47 | 1 0 160.3516174E+4 280.000 -1.0 0.70517 3.429 | LFT00380 |
| 48 | 3.429 0.15107 0.0102108 0.0950976 3.56 | LFT00390 |
| 49 | 0 0 159.8593530E+4 279.444 -1.0 0.70517 3.429 | LFT00400 |
| 50 | 3.429 0.15107 0.0102108 0.0950976 3.56 | LFT00400 |

ALARM-P (VERSION 1) PWR LOSS OF COOLANT ANALYSIS PROGRAM
***** LISTING OF INPUT DATA *****

| NO. |1....2....3....4....5....6....7....8 | LFT00410 |
|-----|--|----------|
| 51 | 0 0 159.7046413E+4 278.889 -1.0 0.17473 1.685544 | LFT00420 |
| 52 | 1,685544 0.06342 0.2840736 -1.4121384 0.0 | LFT00430 |
| 53 | 0 1 160.6962025E+4 279.444 -1.0 0.19413 1.5200376 | LFT00440 |
| 54 | 1,5200376 0.06342 0.2840736 -1.4121384 0.0 | LFT00450 |
| 55 | 177.437 | |
| 56 | 0 1 160.6962025E+4 279.444 -1.0 0.22753 1.5200376 | LFT00460 |
| 57 | 1,5200376 0.06342 0.2840736 -1.4121384 0.0 | LFT00465 |
| 58 | 177.437 | |
| 59 | 0 161.3823727E+4 279.444 -1.0 0.11385 0.2840736 | LFT00470 |
| 60 | 0.2840736 0.06342 0.2840736 -0.1420368 0.0 | LFT00480 |
| 61 | 0 0 161.3502109E+4 279.444 -1.0 0.14981 0.2840736 | LFT00490 |
| 62 | 0.2840736 0.06342 0.2840736 -0.1420368 0.0 | LFT00500 |
| 63 | 1 0 161.4084697E+4 280.556 -1.0 0.94206 5.1703224 | LFT00510 |
| 64 | 5.1703224 0.18236 0.0493776 -0.25900 0.0 | LFT00520 |
| 65 | 0 0 161.4978902E+4 290.556 -1.0 0.64315 0.8238744 | LFT00530 |
| 66 | 0.8238744 0.18005 0.9970008 -0.988052 0.0 | LFT00540 |
| 67 | 0 0 161.2587749E+4 290.000 -1.0 0.91474 3.5317176 | LFT00550 |
| 68 | 3.5317176 0.25901 0.5742432 -0.1641776 0.0 | LFT00560 |
| 69 | 1 0 160.8438818E+4 279.444 -1.0 0.30869 1.5325344 | LFT00570 |
| 70 | 1.5325344 0.23067 0.5419344 -0.63246 0.0 | LFT00580 |
| 71 | 0 0 160.7172995E+4 279.444 -1.0 0.16406 0.2840736 | LFT00590 |
| 72 | 0.2840736 0.06342 0.2840736 -0.1420368 0.0 | LFT00600 |
| 73 | 0 0 160.6118143E+4 279.444 -1.0 0.01269 0.7690104 | LFT00610 |
| 74 | 0.7690104 0.08836 0.1032272 -0.0515112 0.0 | LFT00620 |
| 75 | 0 0 160.5063291E+4 276.667 -1.0 0.33672 2.8682648 | LFT00630 |
| 76 | 2.8682648 0.10363 0.3666744 0.7174992 0.0 | LFT00640 |
| 77 | 0 0 160.7172995E+4 276.667 -1.0 0.33672 2.8682648 | LFT00650 |
| 78 | 2.8682648 0.10363 0.3666744 0.7174992 0.0 | LFT00660 |
| 79 | 0 0 160.9353023E+4 273.889 -1.0 0.04996 2.07264 | LFT00670 |
| 80 | 2.07264 0.02356 0.1807464 -0.134836 0.0 | LFT00680 |
| 81 | 0 0 160.7172995E+4 272.222 -1.0 0.01575 1.2631104 | LFT00690 |
| 82 | 1.2631104 0.08836 0.103333 -0.12643104 0.0 | LFT00700 |
| 83 | 0 0 161.3502109E+4 280.556 -1.0 0.13857 0.2840736 | LFT00710 |
| 84 | 0.2840736 0.06342 0.2840736 -0.1420368 0.0 | LFT00720 |
| 85 | 1 0 160.5344585E+4 342.778 0.0 0.96288 1.703344 | LFT00730 |
| 86 | 1.1454584 0.36520 0.647344 1.1539724 0.0 | LFT00740 |
| 87 | 0 0 160.6469760E+4 300.000 -1.0 0.00634 1.0308336 | LFT00750 |
| 88 | 1.0308336 0.00145 0.0429768 0.1420368 0.0 | LFT00760 |
| 89 | 0 0 160.6540084E+4 276.667 -1.0 0.16576 0.8619744 | LFT00770 |
| 90 | 0.8619744 0.02883 0.2221992 -0.11113008 0.0 | LFT00780 |
| 91 | 0 0 161.2869158E+4 276.667 -1.0 0.19235 0.6074664 | LFT00790 |
| 92 | 0.6074664 0.02883 0.2221992 0.1420368 0.0 | LFT00800 |
| 93 | 0 0 159.3811533E+4 272.222 -1.0 0.00405 0.10320928 | LFT00830 |
| 94 | 0.10320928 0.00836 0.10320928 -0.0515112 0.0 | LFT00832 |
| 95 | 0 0 160.5907172E+4 320.000 -1.0 0.00634 0.2023472 | LFT00834 |
| 96 | 0.2023472 0.00144 0.042672 1.1298936 0.0 | LFT00836 |
| 97 | /* ECLS | LFT00844 |
| 98 | /* (VOL=2) ACC LINE NEAR COLD-LEG | LFT00845 |
| 99 | 0 0 161.3379359E+4 234.444 -1.0 0.03398 0.04443984 | LFT00846 |
| 100 | 0.04443984 0.006207 0.08890 0.1420368 0.0 | LFT00847 |

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ALARM-P (VERSION 1) PWR LOSS OF COOLANT ANALYSIS PROGRAM

***** LISTING OF INPUT DATA *****

NO.*....1....*....2....*....3....*....4....*....5....*....6....*....7....*....8

101 /* (VUL=29) ACC LINE NEAR ACC TANK (CONTAINS STANDPIPE) LFT00848
 102 0 43.1384276E+4 33.333 -1.0 0.3285 0.7705344 LFT00849
 103 0.7705344 0.006207 0.08890 0.18647664 0.0 LFT00850
 104 /* (VUL=30) ACC TANK LFT00851
 105 1 0 43.1384276E+4 33.333 0.0 3.6816 2.919984 LFT00852
 106 1.999 1.2607 1.267 0.18647664 0.0 LFT00853
 107 0 1.0E0/876E+4 83.889 0.0 104.809 4.9054512 LFT00854
 108 2.871216 21.367 5.21208 -4.13004 0.0 LFT00855
 109 /* LFT00856
 110 /* BUBBLE DATA LFT00860
 111 /* 0.8 0.9144 LFT00870
 112 /* LFT00880
 113 /* PUMP DATA LFT00890
 114 /* LFT00900
 115 /* LFT00910
 116 11 12 13 17 11 7 10 17 2 LFT00920
 117 0.0 1.0E-5 620.775 124.648 0.3154 369.661 10.232 0.363 0.0 LFT00930
 118 /* LFT00940
 119 /* HEAD LFT00950
 120 /* LFT00960
 121 -1.0 2.4722 -0.80574 2.0474 -0.8069 1.631 LFT00970
 122 -0.40683 1.624 -0.200171 1.4705 0.0 1.4036 LFT00980
 123 0.19081 1.3636 0.38963 1.3386 0.59396 1.2328 LFT00990
 124 0.7902 1.1336 1.0 1.0078 LFT01000
 125 /* LFT01010
 126 -1.0 -1.0 -0.80 -0.97 -0.60 -0.50 LFT01020
 127 -0.40 -0.05 -0.20 0.15 0.0 0.25 LFT01030
 128 0.20 0.26 0.40 0.34 0.4118 0.2768 LFT01040
 129 0.59763 0.4584 0.763467 0.6992 1.0 0.9465 LFT01050
 130 /* LFT01060
 131 -1.0 -1.0 -0.80 -0.97 -0.60 -0.95 LFT01070
 132 -0.40 -0.86 -0.20 -0.60 0.0 -0.67 LFT01080
 133 0.20 -0.50 0.40 -0.25 0.57556 0.0 LFT01090
 134 0.74432 0.2583 0.77346 0.3778 0.86313 0.6326 LFT01100
 135 1.0 1.0078 LFT01110
 136 /* LFT01120
 137 -1.0 2.4722 -0.82297 1.9968 -0.63332 1.5897 LFT01130
 138 -0.45534 1.3279 -0.27109 1.1949 -0.17716 1.0605 LFT01140
 139 -0.09073 1.0156 0.0 0.934279 0.091099 0.9229 LFT01150
 140 0.186509 0.8963 0.271762 0.675 0.455872 0.8433 LFT01160
 141 0.574406 0.8355 0.760576 0.6466 0.766619 0.8469 LFT01170
 142 0.871471 0.8838 1.0 0.9465 LFT01180
 143 /* LFT01190
 144 /* TURWUE LFT01200
 145 /* LFT01210
 146 -1.0 1.9843 -0.80096 1.394 -0.60638 1.0975 LFT01220
 147 -0.40686 0.6422 -0.19928 0.6648 0.0 0.6032 LFT01230
 148 0.1930 0.6325 0.393 0.7369 0.59552 0.8331 LFT01240
 149 0.79782 0.9292 1.0 0.9672 LFT01250
 150 /* LFT01260

ALARM-P (VERSION 1) PWR LOSS OF COOLANT ANALYSIS PROGRAM

***** LISTING OF INPUT DATA *****

NO.*....1....*....2....*....3....*....4....*....5....*....6....*....7....*....8

151 -1.0 -1.0 -0.30 -0.90 -0.10 -0.50 LFT01270
 152 0.0 -0.45 0.40 -0.25 0.30 0.0 LFT01280
 153 1.0 0.5569 LFT01290
 154 /* LFT01300
 155 -1.0 -1.0 -0.25 -0.90 -0.08 -0.80 LFT01310
 156 0.0 -0.07 0.40 -0.25 0.30 0.15 LFT01320
 157 0.737255 0.526586 0.768049 0.606594 0.86723 0.74366 LFT01330
 158 1.0 0.9872 LFT01340
 159 /* LFT01350
 160 -1.0 1.9843 -0.82234 1.8308 -0.63731 1.6824 LFT01360
 161 -0.45853 1.3577 -0.267023 1.4362 -0.176107 1.3879 LFTG1370
 162 -0.08931 1.3881 0.0 1.23361 0.090843 1.1965 LFT01380
 163 0.188569 1.1096 0.27347 1.0416 0.458669 0.8956 LFTC1390
 164 0.574448 0.7807 0.73816 0.6134 0.76832 0.5849 LFT01400
 165 0.870057 0.4877 1.0 0.3569 LFTG1410
 166 /* LFTG1420
 167 0.0 0.0 1.E+8 0.0 LFTG1430
 168 /* LFTD1440
 169 /* JUNCTION DATA LFTD1450
 170 /* LFTD1460
 171 1 2 0 0 0 1 268.400 0.06342 0.0 0.0 LFTC1470
 172 1.0E-5 1.0E-5 0.0 0.85 0.0 LFTD1480
 173 2 3 0 0 0 1 268.400 0.06342 0.0 0.0 LFTC1490
 174 1.0E-5 1.0E-5 0.0 0.85 0.0 LFTD1500
 175 3 4 0 0 0 1 268.400 0.05169 0.2420112 0.0 LFTG1510
 176 1.0E-5 1.0E-5 0.0 0.85 0.0 LFTD1520
 177 4 5 0 0 0 1 268.400 0.15143 3.057144 0.0 LFTG1530
 178 5 6 0 0 0 1 268.400 0.05169 0.2734056 0.0 LFTC1540
 179 1.0E-5 1.0E-5 0.0 0.85 0.0 LFTD1550
 180 6 7 -1 0 0 1 134.200 0.06342 -1.2701016 0.0 LFTG1560
 181 1.0E-5 1.0E-5 0.0 0.85 0.0 LFTD1570
 182 6 8 -2 0 0 1 134.200 0.06342 -1.2701016 0.0 LFTG1580
 183 1.0E-5 1.0E-5 0.0 0.85 0.0 LFTD1590
 184 7 9 1 0 0 1 134.200 0.03661 0.0 0.0 LFTG1600
 185 1.0E-5 1.0E-5 0.0 0.85 0.0 LFTC1610
 186 8 9 2 0 0 1 134.200 0.03661 0.0 0.0 LFTG1620
 187 1.0E-5 1.0E-5 0.0 0.85 0.0 LFTD1630
 188 9 10 0 0 0 1 268.400 0.06342 0.0 0.0 LFTG1640
 189 1.0E-5 1.0E-5 0.0 0.85 0.0 LFTD1650
 190 10 11 0 0 0 1 268.400 0.06342 0.0 0.0 LFTG1660
 191 1.0E-5 1.0E-5 0.0 0.85 0.0 LFTD1670
 192 11 12 0 0 0 1 268.400 0.17094 -4.255008 0.0 LFTG1680
 193 1.0E-5 1.0E-5 0.0 0.85 0.0 LFTD1690
 194 12 13 0 0 0 1 268.400 0.26254 -4.161776 0.0 LFTG1700
 195 1.0E-5 1.0E-5 0.0 0.85 0.0 LFTD1710
 196 13 14 0 0 0 1 268.400 0.04779 -0.63246 0.0 LFTG1720
 197 1.0E-5 1.0E-5 0.0 0.85 0.0 LFTD1730
 198 14 1 0 0 0 1 268.400 0.06342 0.0 0.0 LFTG1740
 199 1.0E-5 1.0E-5 0.0 0.85 0.0 LFTD1750
 200 .. LFTG1760

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ALARM-P (VERSION 1) PWR LOSS OF COOLANT ANALYSIS PROGRAM

***** LISTING OF INPUT DATA *****

| NO. | 1 | 2 | 3 | 4 | 5 | 6 | 7 | 8 |
|-----|------|---------------------------------|-----|-----|------|------|------|------------|
| 201 | 14 | 15 | 0 | 0 | 0 | 1 | 0.0 | 0.06342 |
| 202 | 0.0 | 0.0 | 0 | 0 | 0.85 | 0.0 | 0.0 | LFT01770 |
| 203 | 24 | 15 | 0 | 0 | 0 | 1 | 0.0 | 0.03880 |
| 204 | 0.0 | 0.5 | 0.0 | 0.0 | 0.85 | 0.0 | 0.0 | LFT01780 |
| 205 | 15 | 16 | 0 | 0 | 0 | 1 | 0.0 | 0.00836 |
| 206 | 0.0 | 0.0 | 0 | 0 | 0.85 | 0.0 | 0.0 | LFT01790 |
| 207 | 16 | 17 | 0 | 0 | 0 | 1 | 0.0 | 0.00836 |
| 208 | 17 | 18 | 0 | 0 | 0 | 1 | 0.0 | 0.7174992 |
| 209 | 17 | 18 | 0 | 0 | 0 | 1 | 0.0 | 0.03914 |
| 210 | 18 | 19 | 0 | 0 | 0 | 1 | 0.0 | 3.4222944 |
| 211 | 18 | 19 | 0 | 0 | 0 | 1 | 0.0 | 0.00836 |
| 212 | 19 | 20 | 0 | 0 | 0 | 1 | 0.0 | 0.7174992 |
| 213 | 19 | 20 | 0 | 0 | 0 | 1 | 0.0 | -1.2127992 |
| 214 | 20 | 21 | 0 | 0 | 0 | 1 | 0.0 | 0.00836 |
| 215 | 20 | 21 | 0 | 0 | 0 | 1 | 0.0 | 0.0 |
| 216 | 21 | 22 | 0 | 0 | 0 | 1 | 0.0 | 0.00836 |
| 217 | 11 | 21 | 0 | 0 | 0 | 1 | 0.0 | 0.05342 |
| 218 | 21 | 22 | 0 | 0 | 0 | 1 | 0.0 | 0.05342 |
| 219 | 25 | 21 | 0 | 0 | 0 | 1 | 0.0 | 0.03880 |
| 220 | 25 | 21 | 0 | 0 | 0.5 | 0 | 0.0 | 0.1420368 |
| 221 | 21 | 26 | 0 | 0 | 0 | 1 | 0.0 | 0.00836 |
| 222 | 26 | 0 | 0 | 0 | 0.0 | 1 | 0.0 | 0.0 |
| 223 | 22 | 27 | 0 | 0 | 0 | 1 | 0.0 | 1.2743688 |
| 224 | 27 | 0 | 0 | 0 | 0.0 | 1 | 0.0 | 0.00468 |
| 225 | 23 | 2 | 0 | 0 | 0 | 1 | 0.0 | 0.00145 |
| 226 | 26 | 31 | 0 | 0 | 0.95 | 0.44 | 0.0 | 0.1420368 |
| 227 | 26 | 31 | 0 | 0 | 0 | 1 | 0.0 | 0.00836 |
| 228 | 27 | 23 | 0 | 0 | 0 | 1 | 0.0 | 0.0 |
| 229 | 27 | 23 | 0 | 0 | 0 | 1 | 0.0 | 0.00145 |
| 230 | 28 | 10 | 0 | 0 | 9.00 | 9.00 | 0.0 | 0.00836 |
| 231 | /* | ECC WATER INLET JUNCTION (J=31) | | | | | | LFT02034 |
| 232 | 28 | 10 | 0 | 0 | 2 | 1 | 0.0 | 0.00599 |
| 233 | 28 | 10 | 0 | 0 | 0.0 | 0.85 | -1.0 | LFT02035 |
| 234 | /* | (ACC CHECK VALVE) (J=32) | | | | | | LFT02037 |
| 235 | 29 | 28 | 0 | 1 | 0 | 1 | 0.0 | 0.00399 |
| 236 | 30 | 29 | 0 | 1 | 0 | 1 | 0.0 | 0.18647664 |
| 237 | 30 | 29 | 0 | 1 | 0 | 1 | 0.0 | 0.00399 |
| 238 | 30 | 29 | 0 | 1 | 0 | 1 | 0.0 | 0.00621 |
| 239 | 30 | 29 | 0 | 1 | 0 | 1 | 0.0 | 0.95701104 |
| 240 | /* | LPIIS FILL JUNCTION (J=34) | | | | | | LFT02036 |
| 241 | 0 | 28 | 1 | 0 | 1 | 0.0 | 0.0 | 0.00599 |
| 242 | 0 | 28 | 1 | 0 | 1 | 0.0 | 0.0 | 0.1642567 |
| 243 | /* | LPIIS FILL JUNCTION (J=35) | | | | | | LFT02045 |
| 244 | 0 | 28 | 2 | 0 | 1 | 0.0 | 0.0 | 0.00599 |
| 245 | 0 | 28 | 2 | 0 | 1 | 0.0 | 0.0 | 0.1642567 |
| 246 | 1.00 | 2 | 0 | 1 | 0.0 | 0.0 | 0.85 | 0.60 |
| 247 | /* | CHECK VALVE DATA | | | | | | LFT02054 |
| 248 | /* | CHECK VALVE DATA | | | | | | LFT02055 |
| 249 | /* | CHECK VALVE DATA | | | | | | LFT02056 |
| 250 | =6 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | | LFT02057 |

ALARM-P (VERSION 1) PWR LOSS OF COOLANT ANALYSIS PROGRAM

***** LISTING OF INPUT DATA *****

| NO. | 1 | 2 | 3 | 4 | 5 | 6 | 7 | 8 |
|-----|----------|--------------------------------|-----------|----------|------------|----------|-----|----------|
| 251 | -7 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | | LFT02060 |
| 252 | -6 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | | LFT02065 |
| 253 | /* | FILL TABLE DATA | | | | | | LFT02090 |
| 254 | /* | (LPIIS INJECTION) | | | | | | LFT02091 |
| 255 | 8 | 1 | 7.03E+4 | 26.0 | | | | LFT02092 |
| 256 | 0.0 | 10.81 | 28124.0 | 10.0 | 56248.0 | 8.861 | | LFT02093 |
| 257 | 86372.0 | 7.541 | 112496.0 | 5.719 | 140620.0 | 2.954 | | LFT02094 |
| 258 | 160307.0 | 0.0 | 100.E+4 | 0.0 | | | | LFT02095 |
| 259 | 160307.0 | 0.0 | 100.E+4 | 0.0 | | | | LFT02096 |
| 260 | /* | (MPIS INJECTION) | | | | | | LFT02097 |
| 261 | 2 | 1 | 7.03E+4 | 26.0 | | | | LFT02098 |
| 262 | 70.31 | 1.081 | 2109300.0 | 1.081 | | | | LFT02099 |
| 263 | /* | HEAT SLAB DATA | | | | | | LFT02100 |
| 264 | /* | HEAT SLAB DATA | | | | | | LFT02105 |
| 265 | 0 | 11 | 1 | 0.0 | 76.206 | 13.6644 | 0.0 | 0.0 |
| 266 | /* | SLAB GEOMETRY DATA | | | | | | LFT02130 |
| 267 | /* | SLAB GEOMETRY DATA | | | | | | LFT02140 |
| 268 | 1 | 1 | 0 | 1 | 0.2560 | 0.0 | 0.0 | LFT02150 |
| 269 | /* | MATERIAL THERMAL PROPERTY DATA | | | | | | LFT02160 |
| 270 | /* | MATERIAL THERMAL PROPERTY DATA | | | | | | LFT02170 |
| 271 | /* | SS304 THERMAL CONDUCTIVITY | | | | | | LFT02180 |
| 272 | /* | SS304 THERMAL CONDUCTIVITY | | | | | | LFT02190 |
| 273 | /* | SS304 THERMAL CONDUCTIVITY | | | | | | LFT02200 |
| 274 | /* | SS304 THERMAL CONDUCTIVITY | | | | | | LFT02210 |
| 275 | 2 | | | | | | | LFT02220 |
| 276 | 100.0 | 3.95725E-3 | | 1300.0 | 7.97485E-3 | | | LFT02230 |
| 277 | /* | SS304 HEAT CAPACITY | | | | | | LFT02240 |
| 278 | /* | SS304 HEAT CAPACITY | | | | | | LFT02250 |
| 279 | /* | END OF DATA | | | | | | LFT02260 |
| 280 | /* | END OF DATA | | | | | | LFT02270 |
| 281 | 13 | | | | | | | LFT02280 |
| 282 | 76.667 | 712.1265 | 121.111 | 710.0256 | 204.444 | 712.5495 | | LFT02290 |
| 283 | 313.556 | 727.0415 | 426.667 | 751.3452 | 537.778 | 782.2920 | | LFT02290 |
| 284 | 648.889 | 816.7132 | 760.000 | 851.4400 | 871.111 | 883.3022 | | LFT02300 |
| 285 | 982.222 | 909.1364 | 1093.333 | 923.7688 | 1204.444 | 930.0322 | | LFT02310 |
| 286 | 1313.556 | 918.7380 | | | | | | LFT02320 |
| 287 | /* | GAP CONDUCTANCE DATA | | | | | | LFT02330 |
| 288 | /* | GAP CONDUCTANCE DATA | | | | | | LFT02340 |
| 289 | /* | END OF DATA | | | | | | LFT02350 |
| 290 | 2 | 0.0 | 0.0 | 1000.0 | 0.0 | | | LFT02360 |
| 291 | /* | END OF DATA | | | | | | LFT02370 |
| 292 | /* | END OF DATA | | | | | | LFT02380 |
| 293 | /* | END OF DATA | | | | | | LFT02390 |

END OF INPUT DATA

Appendix 3. Output Data List of RELAP4J Analysis

** RELAP4J ANALYSIS FOR STANDARD PROBLEM NO.5 L1=4:JAERI **

PUMP SPEED

| TIME | PUMP1 | PUMP2 |
|--------|--------------|--------------|
| SEC | RPM | RPM |
| 0.0 | 1.694400E+03 | 1.787000E+03 |
| 0.020 | 1.691210E+03 | 1.784170E+03 |
| 0.040 | 1.689640E+03 | 1.781450E+03 |
| 0.060 | 1.687170E+03 | 1.778600E+03 |
| 0.080 | 1.684710E+03 | 1.775780E+03 |
| 0.100 | 1.682260E+03 | 1.772900E+03 |
| 0.200 | 1.669510E+03 | 1.759200E+03 |
| 0.300 | 1.657430E+03 | 1.745500E+03 |
| 0.400 | 1.645140E+03 | 1.731170E+03 |
| 0.500 | 1.633070E+03 | 1.758480E+03 |
| 0.600 | 1.621200E+03 | 1.705440E+03 |
| 0.700 | 1.609500E+03 | 1.692590E+03 |
| 0.800 | 1.597960E+03 | 1.679930E+03 |
| 1.000 | 1.575250E+03 | 1.655010E+03 |
| 1.200 | 1.553220E+03 | 1.630730E+03 |
| 1.400 | 1.531860E+03 | 1.607130E+03 |
| 1.600 | 1.511010E+03 | 1.584310E+03 |
| 1.800 | 1.492830E+03 | 1.563760E+03 |
| 2.000 | 1.474640E+03 | 1.542750E+03 |
| 2.500 | 1.431250E+03 | 1.495110E+03 |
| 3.000 | 1.396690E+03 | 1.455270E+03 |
| 3.500 | 1.376640E+03 | 1.430150E+03 |
| 4.000 | 1.362740E+03 | 1.414150E+03 |
| 4.500 | 1.349780E+03 | 1.400030E+03 |
| 5.000 | 1.338020E+03 | 1.386990E+03 |
| 5.500 | 1.327380E+03 | 1.375030E+03 |
| 6.000 | 1.317030E+03 | 1.363480E+03 |
| 6.500 | 1.307480E+03 | 1.352740E+03 |
| 7.000 | 1.298260E+03 | 1.342390E+03 |
| 7.500 | 1.259590E+03 | 1.298490E+03 |
| 12.000 | 1.228990E+03 | 1.263540E+03 |
| 14.500 | 1.204470E+03 | 1.235310E+03 |
| 17.000 | 1.183570E+03 | 1.211410E+03 |
| 19.500 | 1.165830E+03 | 1.190990E+03 |
| 20.000 | 1.152600E+03 | 1.187240E+03 |
| 22.500 | 1.147670E+03 | 1.169850E+03 |
| 25.000 | 1.133670E+03 | 1.153610E+03 |
| 27.500 | 1.120900E+03 | 1.138980E+03 |
| 30.000 | 1.108850E+03 | 1.124950E+03 |
| 32.000 | 1.100170E+03 | 1.114640E+03 |
| 34.500 | 1.090660E+03 | 1.102850E+03 |
| 37.000 | 1.082770E+03 | 1.091840E+03 |
| 39.500 | 1.077430E+03 | 1.082820E+03 |
| 42.000 | 1.076890E+03 | 1.087840E+03 |
| 44.500 | 1.080080E+03 | 1.077970E+03 |
| 47.000 | 1.085340E+03 | 1.078860E+03 |
| 49.500 | 1.091690E+03 | 1.080770E+03 |
| 52.000 | 1.099860E+03 | 1.084260E+03 |
| 54.500 | 1.108100E+03 | 1.087980E+03 |
| 57.000 | 1.116660E+03 | 1.092010E+03 |
| 57.967 | 1.129510E+03 | 1.101680E+03 |

** RELAP4J ANALYSIS FOR STANDARD PROBLEM NO.5 L1=4:JAERI **

TEMPERATURE

| TIME | AT14 | AT10 | AT21 | AT15 | AT11 | AT23 | AT26 | (TE=CS-1) (TE=PC-1) (TE=BL-1) (TE=BL-2) (TE=1ST-1, TE=1ST-4, TE=1ST-7, TE=1ST-9, TE=1ST-13, TE=2ST-1, TE=2ST-4, TE=2ST-7) | | | | | |
|-------|---------------|---------------|---------------|---------------|---------------|---------------|---------------|---|---|---|---|---|---|
| | | | | | | | | C | C | C | C | C | C |
| 0.0 | 2.794444E+02 | 2.794444E+02 | 2.805556E+02 | 2.794444E+02 | 2.805556E+02 | 2.544444E+02 | 6.388889E+01 | | | | | | |
| 0.070 | 2.777475E+02 | 2.775198E+02 | 2.785500E+02 | 2.777598E+02 | 2.787030E+02 | 2.529229E+02 | 8.401756E+01 | | | | | | |
| 0.140 | 2.764648E+02 | 2.762382E+02 | 2.773900E+02 | 2.763934E+02 | 2.774384E+02 | 2.520335E+02 | 9.413144E+01 | | | | | | |
| 0.210 | 2.763504E+02 | 2.761885E+02 | 2.771558E+02 | 2.762475E+02 | 2.774034E+02 | 2.520547E+02 | 8.420654E+01 | | | | | | |
| 0.280 | 2.763643E+02 | 2.761907E+02 | 2.774039E+02 | 2.762372E+02 | 2.774094E+02 | 2.5210121E+02 | 8.427279E+01 | | | | | | |
| 0.350 | 2.763634E+02 | 2.761883E+02 | 2.772576E+02 | 2.762321E+02 | 2.774384E+02 | 2.5212422E+02 | 8.433821E+01 | | | | | | |
| 0.420 | 2.763961E+02 | 2.761927E+02 | 2.773934E+02 | 2.762457E+02 | 2.774796E+02 | 2.5212431E+02 | 8.440331E+01 | | | | | | |
| 0.490 | 2.762425E+02 | 2.761924E+02 | 2.774529E+02 | 2.76261RE+02 | 2.774761E+02 | 2.5212066E+02 | 8.446838E+01 | | | | | | |
| 0.560 | 2.763374E+02 | 2.761927E+02 | 2.771342E+02 | 2.762626E+02 | 2.774866E+02 | 2.5212066E+02 | 8.453309E+01 | | | | | | |
| 0.630 | 2.764445E+02 | 2.761906E+02 | 2.774056E+02 | 2.762638E+02 | 2.774359E+02 | 2.521239E+02 | 8.459763E+01 | | | | | | |
| 0.700 | 2.765607E+02 | 2.761897E+02 | 2.771187E+02 | 2.762707E+02 | 2.774311E+02 | 2.5211295E+02 | 8.466702E+01 | | | | | | |
| 0.770 | 2.764834E+02 | 2.761884E+02 | 2.7722091E+02 | 2.762844E+02 | 2.77332E+02 | 2.5212015E+02 | 8.472598E+01 | | | | | | |
| 0.840 | 2.765082E+02 | 2.76176E+02 | 2.771650E+02 | 2.763017E+02 | 2.773427E+02 | 2.5211945E+02 | 8.478990E+01 | | | | | | |
| 0.910 | 2.765276E+02 | 2.761877E+02 | 2.770601E+02 | 2.763115E+02 | 2.773106E+02 | 2.521190E+02 | 8.485319E+01 | | | | | | |
| 0.980 | 2.765452E+02 | 2.761901E+02 | 2.772208E+02 | 2.763246E+02 | 2.772496E+02 | 2.5211745E+02 | 8.491648E+01 | | | | | | |
| 1.050 | 2.765595E+02 | 2.761938E+02 | 2.769082E+02 | 2.763345E+02 | 2.772344E+02 | 2.5211711E+02 | 8.497944E+01 | | | | | | |
| 1.120 | 2.765738E+02 | 2.761959E+02 | 2.771146E+02 | 2.763439E+02 | 2.771160E+02 | 2.521157E+02 | 8.502222E+01 | | | | | | |
| 1.190 | 2.765819E+02 | 2.762077E+02 | 2.767653E+02 | 2.763535E+02 | 2.771153E+02 | 2.521158E+02 | 8.510444E+01 | | | | | | |
| 1.260 | 2.765919E+02 | 2.762186E+02 | 2.769333E+02 | 2.767633E+02 | 2.771109E+02 | 2.521159E+02 | 8.516729E+01 | | | | | | |
| 1.330 | 2.766019E+02 | 2.762239E+02 | 2.768012E+02 | 2.767353E+02 | 2.770838E+02 | 2.521126E+02 | 8.522988E+01 | | | | | | |
| 1.400 | 2.766114E+02 | 2.762497E+02 | 2.768812E+02 | 2.768341E+02 | 2.7703161E+02 | 2.521116E+02 | 8.529191E+01 | | | | | | |
| 1.470 | 2.766199E+02 | 2.762701E+02 | 2.767584E+02 | 2.763941E+02 | 2.7701108E+02 | 2.5211085E+02 | 8.5354101E+01 | | | | | | |
| 1.540 | 2.766281E+02 | 2.762938E+02 | 2.768161E+02 | 2.766425E+02 | 2.769692E+02 | 2.5210949E+02 | 8.5416151E+01 | | | | | | |
| 1.610 | 2.766357E+02 | 2.763234E+02 | 2.768681E+02 | 2.767410E+02 | 2.769479E+02 | 2.5211112E+02 | 8.5478151E+01 | | | | | | |
| 1.680 | 2.766432E+02 | 2.763556E+02 | 2.766950E+02 | 2.766235E+02 | 2.769237E+02 | 2.521134E+02 | 8.5540028E+01 | | | | | | |
| 1.750 | 2.766508E+02 | 2.764013E+02 | 2.766290E+02 | 2.764342E+02 | 2.769309E+02 | 2.521167E+02 | 8.560146E+01 | | | | | | |
| 1.820 | 2.766588E+02 | 2.764388E+02 | 2.765930E+02 | 2.764444E+02 | 2.769184E+02 | 2.521145E+02 | 8.566372E+01 | | | | | | |
| 1.890 | 2.766651E+02 | 2.764923E+02 | 2.7675451E+02 | 2.764517E+02 | 2.769365E+02 | 2.521098E+02 | 8.572580E+01 | | | | | | |
| 1.960 | 2.766693E+02 | 2.765411E+02 | 2.768824E+02 | 2.765410E+02 | 2.768938E+02 | 2.521076E+02 | 8.578771E+01 | | | | | | |
| 2.030 | 2.766603E+02 | 2.766786E+02 | 2.766525E+02 | 2.766458E+02 | 2.767629E+02 | 2.521069E+02 | 8.595555E+01 | | | | | | |
| 2.500 | 2.766457E+02 | 2.766808E+02 | 2.7656312E+02 | 2.766730E+02 | 2.7661092E+02 | 2.521092E+02 | 8.461733E+01 | | | | | | |
| 2.850 | 2.7663577E+02 | 2.7662390E+02 | 2.765501E+02 | 2.7653303E+02 | 2.7655535E+02 | 2.520972E+02 | 8.465660E+01 | | | | | | |
| 3.200 | 2.7663016E+02 | 2.765759E+02 | 2.765867E+02 | 2.765867E+02 | 2.7664327E+02 | 2.5210688E+02 | 8.468988E+01 | | | | | | |
| 3.550 | 2.7661734E+02 | 2.759438E+02 | 2.7650513E+02 | 2.762920E+02 | 2.767242E+02 | 2.5209316E+02 | 8.4716892E+01 | | | | | | |
| 3.900 | 2.759737E+02 | 2.761544E+02 | 2.755227E+02 | 2.758172E+02 | 2.761795E+02 | 2.520950E+02 | 8.4746618E+01 | | | | | | |
| 4.250 | 2.758396E+02 | 2.755589E+02 | 2.7562349E+02 | 2.760173E+02 | 2.760049E+02 | 2.520847E+02 | 8.4776190E+01 | | | | | | |
| 4.600 | 2.7579001E+02 | 2.761771E+02 | 2.746727E+02 | 2.755331E+02 | 2.760231E+02 | 2.521037E+02 | 8.4805966E+01 | | | | | | |
| 4.950 | 2.7566087E+02 | 2.754194E+02 | 2.755090E+02 | 2.756251E+02 | 2.757636E+02 | 2.520674E+02 | 8.4834673E+01 | | | | | | |
| 5.300 | 2.7535995E+02 | 2.751271E+02 | 2.771588E+02 | 2.757256E+02 | 2.754343E+02 | 2.520842E+02 | 8.4863309E+01 | | | | | | |
| 5.650 | 2.7525282E+02 | 2.754579E+02 | 2.753888E+02 | 2.753784E+02 | 2.755480E+02 | 2.520974E+02 | 8.4891591E+01 | | | | | | |

JAERI-M 7329

** RELAP4J ANALYSIS FOR STANDARD PROBLEM NO.5 L1-4:JAERI **

TEMPERATURE

| | (TE-CS-1) | (TE-PC-1) | (TE-BL-1) | (TE-BL-2) | (TE-1ST-1, | TE-P120-62 | TE-SV-6 | |
|--------|--------------|---------------|---------------|---------------|---------------|---------------|---------------|---------------|
| TIME | AT14 | AT10 | AT21 | AT15 | AT11 | AT29 | AT26 | |
| SEC | C | C | C | C | C | C | C | |
| 6.000 | 1.751259E+02 | 2.756644E+02 | 2.760180E+02 | 2.75100RE+02 | 2.750087E+02 | 2.521070E+02 | 8.919360E+01 | |
| 6.500 | 2.747976E+02 | 2.749768E+02 | 2.747639E+02 | 2.747537E+02 | 2.749082E+02 | 2.520442E+02 | 8.946847E+01 | |
| 6.700 | 2.746274E+02 | 2.746435E+02 | 2.746127E+02 | 2.746031E+02 | 2.746159E+02 | 2.520956E+02 | 8.974014E+01 | |
| 7.000 | 2.744729E+02 | 2.744574E+02 | 2.738476E+02 | 2.744579E+02 | 2.742433E+02 | 2.520572E+02 | 9.001227E+01 | |
| 7.300 | 2.741466E+02 | 2.741918E+02 | 2.741036E+02 | 2.738290E+02 | 2.740193E+02 | 2.520733E+02 | 9.054999E+01 | |
| 7.400 | 2.738632E+02 | 2.737866E+02 | 2.737391E+02 | 2.737313E+02 | 2.738214E+02 | 2.520747E+02 | 9.041651E+01 | |
| 7.700 | 2.737536E+02 | 2.737220E+02 | 2.736676E+02 | 2.735396E+02 | 2.735839E+02 | 2.520637E+02 | 9.08173E+01 | |
| 8.100 | 2.735345E+02 | 2.734939E+02 | 2.733391E+02 | 2.732871E+02 | 2.733631E+02 | 2.520266E+02 | 9.134693E+01 | |
| 8.400 | 2.733346E+02 | 2.732349E+02 | 2.729355E+02 | 2.728210E+02 | 2.731149E+02 | 2.520618E+02 | 9.160577E+01 | |
| 8.700 | 2.730177E+02 | 2.729665E+02 | 2.729314E+02 | 2.729320E+02 | 2.730114E+02 | 2.520618E+02 | 9.160577E+01 | |
| 9.000 | 2.728449E+02 | 2.727702E+02 | 2.727317E+02 | 2.727505E+02 | 2.727523E+02 | 2.520556E+02 | 9.186344E+01 | |
| 9.400 | 2.727247E+02 | 2.727111E+02 | 2.727098E+02 | 2.7275532E+02 | 2.727020E+02 | 2.520620E+02 | 9.211760E+01 | |
| 9.700 | 2.726610E+02 | 2.726202E+02 | 2.726404E+02 | 2.7272520E+02 | 2.7270741E+02 | 2.520553E+02 | 9.236528E+01 | |
| 10.000 | 2.725426E+02 | 2.719204E+02 | 2.719395E+02 | 2.718942E+02 | 2.718489E+02 | 2.520492E+02 | 9.260857E+01 | |
| 10.300 | 2.715436E+02 | 2.713246E+02 | 2.713098E+02 | 2.715330E+02 | 2.717869E+02 | 2.520374E+02 | 9.284772E+01 | |
| 10.600 | 2.712477E+02 | 2.711322E+02 | 2.711300E+02 | 2.712481E+02 | 2.709116E+02 | 2.707682E+02 | 2.020362E+02 | 9.331241E+01 |
| 11.000 | 2.709356E+02 | 2.709500E+02 | 2.709521E+02 | 2.706694E+02 | 2.707534E+02 | 2.520228E+02 | 9.353935E+01 | |
| 11.300 | 2.705212E+02 | 2.705212E+02 | 2.705212E+02 | 2.705212E+02 | 2.705212E+02 | 2.520206E+02 | 9.376232E+01 | |
| 11.700 | 2.701342E+02 | 2.699304E+02 | 2.695355E+02 | 2.701031E+02 | 2.703431E+02 | 2.520228E+02 | 9.398025E+01 | |
| 12.000 | 2.697353E+02 | 2.695808E+02 | 2.696006E+02 | 2.697059E+02 | 2.698450E+02 | 2.520342E+02 | 9.419505E+01 | |
| 12.300 | 2.695053E+02 | 2.694171E+02 | 2.694171E+02 | 2.694791E+02 | 2.694214E+02 | 2.520155E+02 | 9.449505E+01 | |
| 12.600 | 2.692970E+02 | 2.691970E+02 | 2.691970E+02 | 2.692631E+02 | 2.693858E+02 | 2.520262E+02 | 9.440457E+01 | |
| 13.000 | 2.687679E+02 | 2.686944E+02 | 2.686944E+02 | 2.687662E+02 | 2.688239E+02 | 2.520089E+02 | 9.446100E+01 | |
| 13.300 | 2.682466E+02 | 2.678662E+02 | 2.678246E+02 | 2.683204E+02 | 2.675737E+02 | 2.520240E+02 | 9.440987E+01 | |
| 13.600 | 2.676759E+02 | 2.673424E+02 | 2.673424E+02 | 2.675737E+02 | 2.670639E+02 | 2.669447E+02 | 9.500272E+01 | |
| 14.000 | 2.661979E+02 | 2.661662E+02 | 2.661662E+02 | 2.662952E+02 | 2.6657171E+02 | 2.661910E+02 | 9.519079E+01 | |
| 14.300 | 2.658948E+02 | 2.656964E+02 | 2.656964E+02 | 2.659285E+02 | 2.6597171E+02 | 2.656110E+02 | 9.537315E+01 | |
| 14.700 | 2.653393E+02 | 2.651714E+02 | 2.651714E+02 | 2.6565154E+02 | 2.6586661E+02 | 2.654377E+02 | 9.551952E+01 | |
| 15.000 | 2.648744E+02 | 2.6465178E+02 | 2.6465178E+02 | 2.6463792E+02 | 2.6461820E+02 | 2.6466941E+02 | 9.5551137E+01 | |
| 15.300 | 2.645171E+02 | 2.643176E+02 | 2.643176E+02 | 2.6453557E+02 | 2.6439122E+02 | 2.6419259E+02 | 9.572620E+01 | |
| 15.600 | 2.642830E+02 | 2.642337E+02 | 2.642337E+02 | 2.643748E+02 | 2.643748E+02 | 2.6422727E+02 | 2.1918950E+02 | 9.6067330E+01 |
| 16.000 | 2.639264E+02 | 2.639264E+02 | 2.639264E+02 | 2.642104E+02 | 2.642104E+02 | 2.6423425E+02 | 9.623425E+01 | |
| 16.300 | 2.635702E+02 | 2.635214E+02 | 2.635214E+02 | 2.6363035E+02 | 2.6363035E+02 | 2.635854E+02 | 9.639895E+01 | |
| 16.600 | 2.632170E+02 | 2.629717E+02 | 2.629717E+02 | 2.630272E+02 | 2.639878E+02 | 2.618550E+02 | 9.656153E+01 | |
| 17.000 | 2.628531E+02 | 2.625717E+02 | 2.625717E+02 | 2.6295767E+02 | 2.6300272E+02 | 2.625130E+02 | 9.672185E+01 | |
| 17.300 | 2.624910E+02 | 2.597919E+02 | 2.597919E+02 | 2.598070E+02 | 2.598786E+02 | 2.518351E+02 | 9.687948E+01 | |
| 17.600 | 2.621307E+02 | 2.597917E+02 | 2.597917E+02 | 2.598095E+02 | 2.598205E+02 | 2.5182155E+02 | 9.697984E+01 | |
| 18.000 | 2.617707E+02 | 2.573016E+02 | 2.57316CE+02 | 2.574151E+02 | 2.574562E+02 | 2.515070E+02 | 9.703546E+01 | |
| 18.300 | 2.614534E+02 | 2.564417E+02 | 2.564417E+02 | 2.565345E+02 | 2.565345E+02 | 2.517925E+02 | 9.718871E+01 | |
| 18.600 | 2.611703E+02 | 2.555153E+02 | 2.555153E+02 | 2.560656E+02 | 2.565033LE+02 | 2.511779E+02 | 9.733958E+01 | |
| 19.000 | 2.608466E+02 | 2.5463174E+02 | 2.5463174E+02 | 2.546678E+02 | 2.549231E+02 | 2.549650E+02 | 9.748800E+01 | |

** RELAP4J ANALYSIS FOR STANDARD PROBLEM NO.5 L1-4:JAERI **

TEMPERATURE

| | (TE-CS-1) | (TE-PC-1) | (TE-BL-1) | (TE-BL-2) | (TE-1ST-1, | TE-P120-62 | TE-SV-6 |
|--------|---------------|---------------|---------------|---------------|---------------|--------------|--------------|
| TIME | AT14 | AT10 | AT21 | AT15 | AT11 | AT29 | AT26 |
| SEC | C | C | C | C | C | C | C |
| 20.000 | 2.541491E+02 | 2.539749E+02 | 2.539367E+02 | 2.541057E+02 | 2.541197E+02 | 2.51744RE+02 | 9.763395E+01 |
| 20.300 | 2.534515E+02 | 2.531275E+02 | 2.529855E+02 | 2.527870F+02 | 2.532701E+02 | 2.513173E+02 | 9.777740E+01 |
| 20.700 | 2.523263E+02 | 2.522149E+02 | 2.521535E+02 | 2.522221E+02 | 2.524142E+02 | 2.466516E+02 | 9.791838E+01 |
| 21.000 | 2.514846E+02 | 2.514130E+02 | 2.512377E+02 | 2.515145E+02 | 2.515145E+02 | 2.342382E+02 | 9.805686E+01 |
| 21.300 | 2.505856E+02 | 2.505856E+02 | 2.505272E+02 | 2.505893E+02 | 2.505664E+02 | 2.147757E+02 | 9.819289E+01 |
| 21.700 | 2.497864E+02 | 2.493995E+02 | 2.494651E+02 | 2.495591E+02 | 2.497374E+02 | 1.917393E+02 | 9.832648E+01 |
| 22.000 | 2.486755E+02 | 2.484610E+02 | 2.484851E+02 | 2.484937E+02 | 2.484851E+02 | 1.678957E+02 | 9.8457E+01 |
| 22.300 | 2.476112E+02 | 2.474644E+02 | 2.474644E+02 | 2.480105E+02 | 2.477043E+02 | 1.446924E+02 | 9.856618E+01 |
| 22.600 | 2.465075E+02 | 2.464414E+02 | 2.464331E+02 | 2.464574E+02 | 2.464574E+02 | 1.242023E+02 | 9.871206E+01 |
| 23.000 | 2.453570E+02 | 2.452857E+02 | 2.452857E+02 | 2.454163E+02 | 2.454163E+02 | 1.065572E+02 | 9.883509E+01 |
| 23.300 | 2.440615E+02 | 2.439526E+02 | 2.439526E+02 | 2.443935E+02 | 2.443935E+02 | 9.163244E+02 | 9.895516E+01 |
| 23.600 | 2.4242163E+02 | 2.4242163E+02 | 2.4242163E+02 | 2.4242163E+02 | 2.4242163E+02 | 7.921369E+01 | 9.907214E+01 |
| 24.000 | 2.414612E+02 | 2.414246E+02 | 2.414246E+02 | 2.414307E+02 | 2.414246E+02 | 6.402472E+01 | 9.918597E+01 |
| 24.300 | 2.404015E+02 | 2.404015E+02 | 2.39901E+02 | 2.404325E+02 | 2.404542E+02 | 6.077727E+01 | 9.929663E+01 |
| 24.700 | 2.394373E+02 | 2.391723E+02 | 2.38493E+02 | 2.395439E+02 | 2.391567E+02 | 5.423071E+01 | 9.940444E+01 |
| 25.000 | 2.38161C+02 | 2.372260E+02 | 2.372260E+02 | 2.387089E+02 | 2.388195E+02 | 4.911859E+01 | 9.950993E+01 |
| 25.300 | 2.369044E+02 | 2.357162E+02 | 2.356930E+02 | 2.373792E+02 | 2.371792E+02 | 4.516389E+01 | 9.961304E+01 |
| 25.600 | 2.356044E+02 | 2.354765E+02 | 2.354765E+02 | 2.359765E+02 | 2.3584835E+02 | 4.211729E+01 | 9.971352E+01 |
| 26.000 | 2.343842E+02 | 2.341934E+02 | 2.341934E+02 | 2.345801E+02 | 2.345801E+02 | 3.978203E+01 | 9.981145E+01 |
| 26.300 | 2.332825E+02 | 2.332104E+02 | 2.332104E+02 | 2.332599E+02 | 2.3341601E+02 | 3.800235E+01 | 9.990702E+01 |
| 26.600 | 2.320802E+02 | 2.3189067E+02 | 2.321042E+02 | 2.325792E+02 | 2.3234554E+02 | 3.655472E+01 | 1.000003E+02 |
| 27.000 | 2.311172E+02 | 2.311172E+02 | 2.30801E+02 | 2.310104E+02 | 2.310737E+02 | 3.554087E+01 | 1.000019E+02 |
| 27.300 | 2.304515E+02 | 2.302416E+02 | 2.294974E+02 | 2.296166E+02 | 2.295858E+02 | 3.488521E+01 | 1.001801E+02 |
| 27.600 | 2.2984963E+02 | 2.294201E+02 | 2.291553E+02 | 2.297841E+02 | 2.298077E+02 | 3.432064E+01 | 1.002666E+02 |
| 28.000 | 2.2970846E+02 | 2.295049E+02 | 2.295049E+02 | 2.297698E+02 | 2.297698E+02 | 3.390553E+01 | 1.003506E+02 |
| 28.400 | 2.295570E+02 | 2.294331E+02 | 2.294331E+02 | 2.2961246E+02 | 2.295790E+02 | 3.360099E+01 | 1.004328E+02 |
| 28.700 | 2.293570E+02 | 2.292104E+02 | 2.292104E+02 | 2.294007E+02 | 2.2942903E+02 | 3.337882E+01 | 1.005124E+02 |
| 29.000 | 2.291432E+02 | 2.290317E+02 | 2.290317E+02 | 2.2928608E+02 | 2.2928791E+02 | 3.321755E+01 | 1.005898E+02 |
| 29.300 | 2.289157E+02 | 2.287433E+02 | 2.287433E+02 | 2.291171E+02 | 2.2914564E+02 | 3.310102E+01 | 1.006647E+02 |
| 29.600 | 2.287152E+02 | 2.285317E+02 | 2.285317E+02 | 2.290104E+02 | 2.290308E+02 | 3.301715E+01 | 1.007374E+02 |
| 30.000 | 2.285053E+02 | 2.283210E+02 | 2.283210E+02 | | | | |

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** RELAP4J ANALYSIS FOR STANDARD PROBLEM NO. 11-4:JAERI **

TEMPERATURE

| (TE=CS=1) | (TE=PC=1) | (TE=BL-1) | (TE=BL-2) | (TE=1ST=1, TE=1ST=4, TE=1ST=7, TE=1ST=9, TE=1ST=13, TE=2ST=1, TE=2ST=4, TE=2ST=7) | TE=P12U-62 | TE=SV=6 | |
|-----------|---------------|--------------|---------------|--|--------------|--------------|---------------|
| TIME | AT14 | AT10 | AT21 | AT15 | AT11 | AT29 | AT26 |
| SEC | C | C | C | C | C | C | C |
| 34.000 | 2.042480E+02 | 1.071936E+02 | 2.037550E+02 | 2.041766E+02 | 2.041075E+02 | 3.281339E+01 | 1.014027E+02 |
| 34.350 | 2.028108E+02 | 1.054102E+02 | 2.023074E+02 | 2.027509E+02 | 2.026671E+02 | 3.281257E+01 | 1.014517E+02 |
| 34.700 | 2.013976E+02 | 1.037936E+02 | 2.008695E+02 | 2.013524E+02 | 2.012359E+02 | 3.281233E+01 | 1.014989E+02 |
| 35.050 | 2.000405E+02 | 1.017980E+02 | 1.995276E+02 | 1.999633E+02 | 1.998195E+02 | 3.281304E+01 | 1.015855E+02 |
| 35.400 | 1.987009E+02 | 9.989639E+01 | 1.981283E+02 | 1.986263E+02 | 1.985195E+02 | 3.281380E+01 | 1.016311E+02 |
| 35.750 | 1.973232E+02 | 9.626829E+01 | 1.975146E+02 | 1.972594E+02 | 1.971341E+02 | 3.276906E+01 | 1.016724E+02 |
| 36.100 | 1.959558E+02 | 9.675722E+01 | 1.953247E+02 | 1.958962E+02 | 1.957179E+02 | 3.276906E+01 | 1.016724E+02 |
| 36.450 | 1.945021E+02 | 9.523921E+01 | 1.938558E+02 | 1.944369E+02 | 1.942651E+02 | 3.261671E+01 | 1.017123E+02 |
| 36.800 | 1.930401E+02 | 9.392767E+01 | 1.923706E+02 | 1.929730E+02 | 1.927305E+02 | 3.249134E+01 | 1.017508E+02 |
| 37.150 | 1.915643E+02 | 9.289101E+01 | 1.908700E+02 | 1.914935E+02 | 1.913040E+02 | 3.238352E+01 | 1.017860E+02 |
| 37.500 | 9.101015E+02 | 9.169566E+01 | 1.893709E+02 | 1.903616E+02 | 1.893205E+02 | 3.228972E+01 | 1.018236E+02 |
| 37.850 | 1.886612E+02 | 9.101738E+01 | 1.878974E+02 | 1.882886E+02 | 1.883608E+02 | 3.220898E+01 | 1.018552E+02 |
| 38.200 | 1.872023E+02 | 9.027367E+01 | 1.866054E+02 | 1.871264E+02 | 1.868635E+02 | 3.214182E+01 | 1.018913E+02 |
| 38.550 | 1.855778E+02 | 9.495404E+01 | 1.849432E+02 | 1.856985E+02 | 1.854358E+02 | 3.208339E+01 | 1.019231E+02 |
| 38.900 | 1.843685E+02 | 8.656594E+01 | 1.834898E+02 | 1.842998E+02 | 1.840040E+02 | 3.203336E+01 | 1.019536E+02 |
| 39.250 | 1.829687E+02 | 8.778158E+01 | 1.8202479E+02 | 1.828924E+02 | 1.825806E+02 | 3.198983E+01 | 1.019828E+02 |
| 39.600 | 1.815855E+02 | 8.705397E+01 | 1.8061278E+02 | 1.8181109E+02 | 1.811636E+02 | 3.195221E+01 | 1.020109E+02 |
| 39.950 | 1.802201E+02 | 8.576590E+01 | 1.777910E+02 | 1.787963E+02 | 1.783805E+02 | 3.192880E+01 | 1.020363E+02 |
| 40.300 | 1.786652E+02 | 8.523639E+01 | 1.763399E+02 | 1.774727E+02 | 1.770212E+02 | 3.184231E+01 | 1.020848E+02 |
| 40.650 | 1.775296E+02 | 8.485645E+01 | 1.750000E+02 | 1.761498E+02 | 1.756563E+02 | 3.183947E+01 | 1.021120E+02 |
| 41.000 | 1.762042E+02 | 8.441446E+01 | 1.736511E+02 | 1.7491182E+02 | 1.743259E+02 | 3.181926E+01 | 1.021347E+02 |
| 41.350 | 1.749026E+02 | 8.400446E+01 | 1.713651E+02 | 1.7474182E+02 | 1.741325E+02 | 3.180097E+01 | 1.021655E+02 |
| 41.700 | 1.736322E+02 | 8.359742E+01 | 1.723200E+02 | 1.735593E+02 | 1.730175E+02 | 3.179097E+01 | 1.0217173E+02 |
| 42.050 | 1.723777E+02 | 8.359944E+01 | 1.709774E+02 | 1.723038E+02 | 1.717261E+02 | 3.178416E+01 | 1.021773E+02 |
| 42.400 | 1.711436E+02 | 8.323183E+01 | 1.696919E+02 | 1.707238E+02 | 1.704512E+02 | 3.176886E+01 | 1.022164E+02 |
| 42.750 | 1.699066E+02 | 8.297655E+01 | 1.683989E+02 | 1.699306E+02 | 1.691895E+02 | 3.175487E+01 | 1.022348E+02 |
| 43.100 | 1.686879E+02 | 8.259045E+01 | 1.671473E+02 | 1.686233E+02 | 1.679632E+02 | 3.174193E+01 | 1.022552E+02 |
| 43.450 | 1.675057E+02 | 8.218389E+01 | 1.659100E+02 | 1.674441E+02 | 1.667441E+02 | 3.171515E+01 | 1.022695E+02 |
| 43.800 | 1.663525E+02 | 8.178039E+01 | 1.646738E+02 | 1.662940E+02 | 1.655284E+02 | 3.170573E+01 | 1.022858E+02 |
| 44.150 | 1.652095E+02 | 8.142467E+01 | 1.636523E+02 | 1.651546E+02 | 1.643346E+02 | 3.167573E+01 | 1.023015E+02 |
| 44.500 | 1.640943E+02 | 8.107056E+01 | 1.622359E+02 | 1.640131E+02 | 1.621758E+02 | 3.165932E+01 | 1.023165E+02 |
| 44.850 | 1.629649E+02 | 8.066650E+01 | 1.610994E+02 | 1.628747E+02 | 1.620496E+02 | 3.160942E+01 | 1.023304E+02 |
| 45.200 | 1.616078E+02 | 8.038446E+01 | 1.599652E+02 | 1.617602E+02 | 1.609401E+02 | 3.163495E+01 | 1.023448E+02 |
| 45.550 | 1.6067319E+02 | 7.964359E+01 | 1.588817E+02 | 1.606846E+02 | 1.605933E+02 | 3.167721E+01 | 1.023648E+02 |
| 45.900 | 1.596977E+02 | 7.904758E+01 | 1.577212E+02 | 1.596443E+02 | 1.587295E+02 | 3.167137E+01 | 1.023581E+02 |
| 46.250 | 1.586702E+02 | 7.859159E+01 | 1.566019E+02 | 1.586221E+02 | 1.576403E+02 | 3.166598E+01 | 1.023709E+02 |
| 46.600 | 1.576492E+02 | 7.812287E+01 | 1.555033E+02 | 1.576058E+02 | 1.565880E+02 | 3.166059E+01 | 1.023931E+02 |
| 46.950 | 1.565993E+02 | 7.762559E+01 | 1.546576E+02 | 1.565516E+02 | 1.555811E+02 | 3.165559E+01 | 1.024060E+02 |
| 47.300 | 1.555507E+02 | 7.704873E+01 | 1.534083E+02 | 1.555259E+02 | 1.545759E+02 | 3.165076E+01 | 1.024046E+02 |
| 47.650 | 1.545700E+02 | 7.644544E+01 | 1.523814E+02 | 1.545227E+02 | 1.535723E+02 | 3.164680E+01 | 1.024166E+02 |

** RELAP4J ANALYSIS FOR STANDARD PROBLEM NO. 5 11-4:JAERI **

TEMPERATURE

| (TE=CS=1) | (TE=PC=1) | (TE=BL-1) | (TE=BL-2) | (TE=1ST=1, TE=1ST=4, TE=1ST=7, TE=1ST=9, TE=1ST=13, TE=2ST=1, TE=2ST=4, TE=2ST=7) | TE=P12U-62 | TE=SV=6 | |
|-----------|---------------|--------------|--------------|--|--------------|---------------|---------------|
| TIME | AT14 | AT10 | AT21 | AT15 | AT11 | AT29 | AT26 |
| SEC | C | C | C | C | C | C | C |
| 48.000 | 1.536092E+02 | 7.581135E+01 | 1.513607E+02 | 1.535588E+02 | 1.525672E+02 | 3.1641525E+01 | 1.0244871E+02 |
| 48.350 | 1.526906E+02 | 7.519337E+01 | 1.503337E+02 | 1.526365E+02 | 1.515655E+02 | 3.163707E+01 | 1.0244668E+02 |
| 48.700 | 1.518717E+02 | 7.464652E+01 | 1.493116E+02 | 1.517470E+02 | 1.505919E+02 | 3.163271E+01 | 1.0244668E+02 |
| 49.050 | 1.510444E+02 | 7.413338E+01 | 1.483430E+02 | 1.508107E+02 | 1.496754E+02 | 3.162453E+01 | 1.0244558E+02 |
| 49.400 | 1.499620E+02 | 7.361027E+01 | 1.473751E+02 | 1.493977E+02 | 1.487657E+02 | 3.162440E+01 | 1.0244646E+02 |
| 49.750 | 1.4909723E+02 | 7.304439E+01 | 1.464055E+02 | 1.490113E+02 | 1.478498E+02 | 3.161737E+01 | 1.0244731E+02 |
| 50.100 | 1.482043E+02 | 7.251704E+01 | 1.454557E+02 | 1.481274E+02 | 1.464921E+02 | 3.161544E+01 | 1.0244810E+02 |
| 50.450 | 1.473384E+02 | 7.199660E+01 | 1.445119E+02 | 1.472748E+02 | 1.460372E+02 | 3.161254E+01 | 1.0244850E+02 |
| 50.800 | 1.464908E+02 | 7.147280E+01 | 1.435990E+02 | 1.464932E+02 | 1.451387E+02 | 3.160860E+01 | 1.0245038E+02 |
| 51.150 | 1.457024E+02 | 7.097766E+01 | 1.426650E+02 | 1.448459E+02 | 1.430010E+02 | 3.160493E+01 | 1.025037E+02 |
| 51.500 | 1.4494204E+02 | 7.059410E+01 | 1.406090E+02 | 1.4488659E+02 | 1.436089E+02 | 3.160895E+01 | 1.025170E+02 |
| 51.850 | 1.439447E+02 | 7.016623E+01 | 1.415519E+02 | 1.438594E+02 | 1.426820E+02 | 3.159698E+01 | 1.025224E+02 |
| 52.200 | 1.432198E+02 | 6.967649E+01 | 1.402195E+02 | 1.431506E+02 | 1.419355E+02 | 3.159213E+01 | 1.0252785E+02 |
| 52.550 | 1.425555E+02 | 6.906093E+01 | 1.389834E+02 | 1.423689E+02 | 1.415659E+02 | 3.158694E+01 | 1.025343E+02 |
| 52.900 | 1.417128E+02 | 6.856549E+01 | 1.395853E+02 | 1.416426E+02 | 1.402975E+02 | 3.158693E+01 | 1.025394E+02 |
| 53.250 | 1.410298E+02 | 6.813874E+01 | 1.364207E+02 | 1.409774E+02 | 1.395647E+02 | 3.158162E+01 | 1.025445E+02 |
| 53.600 | 1.402318E+02 | 6.776336E+01 | 1.372556E+02 | 1.403094E+02 | 1.387191E+02 | 3.157815E+01 | 1.025495E+02 |
| 53.950 | 1.397046E+02 | 6.742239E+01 | 1.372309E+02 | 1.396265E+02 | 1.379702E+02 | 3.157408E+01 | 1.025544E+02 |
| 54.300 | 1.388399E+02 | 6.698487E+01 | 1.338617E+02 | 1.387514E+02 | 1.373753E+02 | 3.157062E+01 | 1.025591E+02 |
| 54.650 | 1.383186E+02 | 6.654195E+01 | 1.347144E+02 | 1.382285E+02 | 1.365900E+02 | 3.156422E+01 | 1.025636E+02 |
| 55.000 | 1.374776E+02 | 6.615599E+01 | 1.351473E+02 | 1.376198E+02 | 1.358120E+02 | 3.156337E+01 | 1.025681E+02 |
| 55.350 | 1.365667E+02 | 6.575766E+01 | 1.352517E+02 | 1.369183E+02 | 1.351910E+02 | 3.155946E+01 | 1.025684E+02 |
| 55.700 | 1.363044E+02 | 6.537784E+01 | 1.314620E+02 | 1.363208E+02 | 1.344859E+02 | 3.155291E+01 | 1.025765E+02 |
| 56.050 | 1.357429E+02 | 6.505845E+01 | 1.326795E+02 | 1.353776E+02 | 1.335723E+02 | 3.154782E+01 | 1.025808E+02 |
| 56.400 | 1.351054E+02 | 6.477930E+01 | 1.323091E+02 | 1.350134E+02 | 1.335005E+02 | 3.154094E+01 | 1.025846E+02 |
| 56.750 | 1.345163E+02 | 6.445220E+01 | 1.294107E+02 | 1.344361E+02 | 1.323849E+02 | 3.154600E+01 | 1.025844E+02 |
| 57.100 | 1.339202E+02 | 6.413045E+01 | 1.291134E+02 | 1.334412E+02 | 1.316827E+02 | 3.154271E+01 | 1.025844E+02 |
| 57.450 | 1.333603E+02 | 6.384823E+01 | 1.299717E+02 | 1.332759E+02 | 1.307668E+02 | 3.153931E+01 | 1.025842E+02 |
| 57.800 | 1.327657E+02 | 6.240665E+01 | 1.300119E+02 | 1.327066E+02 | 1.306084E+02 | 3.153956E+01 | 1.025957E+02 |

JAERI-M 7329

** RELAXATION ANALYSIS FOR STANDARD PROBLEM NO. 3 [I-4.1AERT] **

| PRESSURE | | | | | | MIXTURE LEVEL | | | |
|------------|---------------|---------------|---------------|--------------|--------------|----------------|--------------|--------------|--|
| (PE=CS-1A) | (PE=PC-4) | (PE=SV-18) | (PT=P120-43) | (PE=BL-1) | | (LE=1ST-(1,2)) | (LT=P139-6) | (LT=P138-58) | |
| TIME | AP14 | AP22 | AP26 | AP31 | AP21 | AML11 | AML22 | AML26 | |
| SEC | MPA | MPA | MPA | MPA | MPA | M | M | M | |
| 0.0 | 1.57627E+01 | 1.5737238E+01 | 9.510546E-02 | 4.227370E+00 | 1.581233E+01 | 5.170070E+00 | 1.145382E+00 | 2.871076E+00 | |
| 0.070 | 1.3e33913E+00 | 1.5724154E+01 | 9.544187E+00 | 4.227364E+00 | 9.980870E+00 | 5.170070E+00 | 1.143656E+00 | 2.873136E+00 | |
| 0.140 | 6.5h956E+00 | 1.56883E+01 | 9.570455E+00 | 4.227370E+00 | 6.59280E+00 | 5.170070E+00 | 1.135224E+00 | 2.874559E+00 | |
| 0.210 | 6.1785L+00 | 1.565158E+01 | 9.593817E+00 | 4.227365E+00 | 6.164642E+00 | 5.170070E+00 | 1.130737E+00 | 2.876155E+00 | |
| 0.280 | 6.17347E+00 | 1.561409E+01 | 9.611288E+00 | 4.227368E+00 | 6.169703E+00 | 5.163364E+00 | 1.131910E+00 | 2.877215E+00 | |
| 0.350 | 6.123210E+00 | 1.558593E+01 | 9.628571E+00 | 4.227367E+00 | 6.155968E+00 | 5.167290E+00 | 1.110281E+00 | 2.878256E+00 | |
| 0.420 | 6.154117E+00 | 1.555292E+01 | 9.648580E+00 | 4.227367E+00 | 6.169172E+00 | 5.167070E+00 | 1.102030E+00 | 2.879305E+00 | |
| 0.490 | 6.175941E+00 | 1.551618E+01 | 9.661605E+00 | 4.227368E+00 | 6.174312E+00 | 5.164412E+00 | 1.099365E+00 | 2.880345E+00 | |
| 0.560 | 6.151048E+00 | 1.548426E+01 | 9.681260E+00 | 4.227365E+00 | 6.144403E+00 | 5.168797E+00 | 1.085630E+00 | 2.881380E+00 | |
| 0.630 | 6.171939E+00 | 1.545411E+01 | 9.697446E+00 | 4.227369E+00 | 6.169496E+00 | 5.110202E+00 | 1.077159E+00 | 2.882412E+00 | |
| 0.700 | 6.112454E+00 | 1.541768E+01 | 9.714622E+00 | 4.227365E+00 | 6.142940E+00 | 5.108690E+00 | 1.066897E+00 | 2.883440E+00 | |
| 0.770 | 6.122655E+00 | 1.535464E+01 | 9.733117E+00 | 4.227369E+00 | 6.147286E+00 | 5.070554E+00 | 1.052587E+00 | 2.885661E+00 | |
| 0.840 | 6.138843E+00 | 1.535208E+01 | 9.748804E+00 | 4.227365E+00 | 6.137467E+00 | 5.035504E+00 | 1.044350E+00 | 2.886692E+00 | |
| 0.910 | 6.144777E+00 | 1.535202E+01 | 9.768105E+00 | 4.227369E+00 | 6.137467E+00 | 5.025099E+00 | 1.034099E+00 | 2.887502E+00 | |
| 0.980 | 6.164165E+00 | 1.536271E+01 | 9.782822E+00 | 4.227366E+00 | 6.132235E+00 | 5.324025E+00 | 1.027878E+00 | 2.888507E+00 | |
| 1.050 | 6.145230E+00 | 1.536746E+01 | 9.797340E+00 | 4.227366E+00 | 6.132235E+00 | 5.004794E+00 | 1.019564E+00 | 2.889509E+00 | |
| 1.120 | 6.135813E+00 | 1.532255E+01 | 9.812612E+00 | 4.227366E+00 | 6.142501E+00 | 5.004794E+00 | 1.019564E+00 | 2.890508E+00 | |
| 1.190 | 6.130753E+00 | 1.531970E+01 | 9.813639E+00 | 4.227367E+00 | 6.181316E+00 | 4.994396E+00 | 1.011456E+00 | 2.891505E+00 | |
| 1.260 | 6.124238E+00 | 1.530525E+01 | 9.820555E+00 | 4.227368E+00 | 6.130674E+00 | 4.976506E+00 | 1.003557E+00 | 2.891505E+00 | |
| 1.330 | 6.127224E+00 | 1.531705E+01 | 9.847486E+00 | 4.227366E+00 | 6.113229E+00 | 4.967760E+00 | 9.953539E+00 | 2.892501E+00 | |
| 1.400 | 6.110495E+00 | 1.530495E+01 | 9.884403E+00 | 4.227368E+00 | 6.120733E+00 | 4.953508E+00 | 9.873639E+00 | 2.893496E+00 | |
| 1.470 | 6.112943E+00 | 1.530477E+01 | 9.901343E+00 | 4.227366E+00 | 6.109278E+00 | 4.942749E+00 | 9.794042E+00 | 2.894490E+00 | |
| 1.540 | 6.120240E+00 | 1.526485E+01 | 9.918185E+00 | 4.227368E+00 | 6.114708E+00 | 4.928984E+00 | 9.717235E+00 | 2.895483E+00 | |
| 1.610 | 6.130114E+00 | 1.507042E+01 | 9.935235E+00 | 4.227366E+00 | 6.102727E+00 | 4.918460E+00 | 9.635755E+00 | 2.896476E+00 | |
| 1.680 | 6.162042E+00 | 1.494559E+01 | 9.952187E+00 | 4.227368E+00 | 6.103373E+00 | 4.905842E+00 | 9.559527E+00 | 2.897467E+00 | |
| 1.750 | 6.128681E+00 | 1.494592E+01 | 9.961655E+00 | 4.227366E+00 | 6.097217E+00 | 4.904235E+00 | 9.479984E+00 | 2.898459E+00 | |
| 1.820 | 6.109977E+00 | 1.494277E+01 | 9.986196E+00 | 4.227368E+00 | 6.125394E+00 | 4.898020E+00 | 9.402237E+00 | 2.899453E+00 | |
| 1.890 | 6.104304E+00 | 1.494893E+01 | 1.000330E+01 | 4.227367E+00 | 6.108879E+00 | 4.895182E+00 | 9.324475E+00 | 2.900452E+00 | |
| 1.960 | 6.105373E+00 | 1.494703E+01 | 1.002040E+01 | 4.227367E+00 | 6.120856E+00 | 4.882390E+00 | 9.245414E+00 | 2.901449E+00 | |
| 2.030 | 6.107824E+00 | 1.494797E+01 | 1.006047E+01 | 4.227366E+00 | 6.075546E+00 | 4.840359E+00 | 9.037131E+00 | 2.904150E+00 | |
| 2.100 | 6.101293E+00 | 1.494515E+01 | 1.015241E+01 | 4.227367E+00 | 6.090914E+00 | 4.792556E+00 | 8.654648E+00 | 2.999039E+00 | |
| 2.170 | 6.071939E+00 | 1.495251E+01 | 1.023840E+01 | 4.227367E+00 | 6.089873E+00 | 4.736633E+00 | 8.279494E+00 | 2.914033E+00 | |
| 2.240 | 6.073796E+00 | 1.494363E+01 | 1.032464E+01 | 4.227367E+00 | 6.026638E+00 | 4.677795E+00 | 7.917060E+00 | 2.918952E+00 | |
| 2.310 | 6.054066E+00 | 1.492928E+01 | 1.041645E+01 | 4.227367E+00 | 6.043606E+00 | 4.617933E+00 | 7.543948E+00 | 2.923781E+00 | |
| 2.380 | 6.035363E+00 | 1.491253E+01 | 1.046655E+01 | 4.227367E+00 | 5.994849E+00 | 4.570188E+00 | 7.178492E+00 | 2.928598E+00 | |
| 2.450 | 6.024054E+00 | 1.490425E+01 | 1.056303E+01 | 4.227367E+00 | 6.360607E+00 | 4.521460E+00 | 6.822495E+00 | 2.933412E+00 | |
| 2.520 | 6.013046E+00 | 1.488646E+01 | 1.0646966E+01 | 4.227367E+00 | 5.917123E+00 | 4.515562E+00 | 6.471761E+00 | 2.938206E+00 | |
| 2.590 | 6.007247E+00 | 1.487322E+01 | 1.075629E+01 | 4.227367E+00 | 5.993612E+00 | 4.511718E+00 | 6.126303E+00 | 2.942959E+00 | |
| 2.660 | 5.982742E+00 | 1.486139E+01 | 1.084224E+01 | 4.227367E+00 | 6.146707E+00 | 4.502606E+00 | 5.788224E+00 | 2.947636E+00 | |
| 2.730 | 5.962515E+00 | 1.484639E+01 | 1.092728E+01 | 4.227367E+00 | 5.868933E+00 | 4.468881E+00 | 5.452086E+01 | 2.952239E+00 | |
| 2.800 | 5.942515E+00 | 1.483612E+01 | 1.07252E+01 | 4.227367E+00 | 6.040527E+00 | 4.713116E+00 | 5.122402E+01 | 2.956747E+00 | |
| 2.870 | 5.923515E+00 | 1.482320E+01 | 1.07973E+01 | 4.22737E+00 | 5.919195E+00 | 4.81466E+00 | 4.80236E+01 | 2.961200E+00 | |
| 2.940 | 5.904515E+00 | 1.481254E+01 | 1.084471E+01 | 4.227367E+00 | 5.841770E+00 | 4.859043E+00 | 4.652227E+01 | 2.970103E+00 | |
| 3.010 | 5.885515E+00 | 1.480199E+01 | 1.081310E+01 | 4.227367E+00 | 5.816033E+00 | 4.882959E+00 | 3.854922E+01 | 2.974549E+00 | |
| 3.080 | 5.866493E+00 | 1.478852E+01 | 1.078520E+01 | 4.227367E+00 | 5.886530E+00 | 4.847579E+00 | 3.548856E+01 | 2.978995E+00 | |
| 3.150 | 5.843392E+00 | 1.477413E+01 | 1.073722E+01 | 4.227367E+00 | 5.820103E+00 | 4.761612E+00 | 3.245637E+01 | 2.983436E+00 | |
| 3.220 | 5.823392E+00 | 1.476130E+01 | 1.061522E+01 | 4.227367E+00 | 5.820708E+00 | 4.667798E+00 | 2.946853E+01 | 2.987850E+00 | |

** RELAP4U ANALYSIS FOR STANDARD PROBLEM NO.3 (I-4:JAEP) **

| PRESSURE | | | | | | | MIXTURE LEVEL | | |
|----------|--------------|--------------|--------------|---------------|--------------|--------------|---------------------------|--------------|--|
| TIME | (P-E-C5-1A) | (P-E-PC-4) | (P-E-SV-18) | (P-T-P120-43) | (P-E-BL-1) | | (LE-1ST-(1,2), LT-P139-6) | (LT-P138-58) | |
| | AM14 | AM27 | AP26 | AP31 | AP21 | AML11 | AML22 | AML26 | |
| SEC | MPA | MPA | MPA | MPA | MPA | MPA | M | M | |
| 8,400 | 5.796007E+00 | 1.234519E+01 | 1.369416E-01 | 4.227367E+00 | 5.760626E+00 | 4.570806E+00 | 2.654012E-01 | 2.992308E+00 | |
| 9,130 | 5.765526E+00 | 1.221033E+01 | 1.177979E-01 | 4.227367E+00 | 5.767700E+00 | 4.474140E+00 | 2.374302E-01 | 2.996725E+00 | |
| 9,500 | 5.752904E+00 | 1.202773E+01 | 1.165359E-01 | 4.227367E+00 | 5.701631E+00 | 4.384970E+00 | 2.113765E-01 | 3.001052E+00 | |
| 9,850 | 5.725500E+00 | 1.195604E+01 | 1.190523E-01 | 4.227367E+00 | 5.664833E+00 | 4.412737E+00 | 1.856744E-01 | 3.005332E+00 | |
| 10,200 | 5.703792E+00 | 1.174004E+01 | 1.203344E-01 | 4.227367E+00 | 5.689272E+00 | 4.365860E+00 | 1.608764E-01 | 3.009532E+00 | |
| 10,550 | 5.672684E+00 | 1.145573E+01 | 1.211564E-01 | 4.227367E+00 | 5.783300E+00 | 4.390005E+00 | 1.371581E-01 | 3.013454E+00 | |
| 10,900 | 5.637541E+00 | 1.114034E+01 | 1.219705E+01 | 4.227367E+00 | 5.480234E+00 | 4.424016E+00 | 1.142614E-01 | 3.017470E+00 | |
| 11,250 | 5.611161E+00 | 1.116474E+01 | 1.227727E+01 | 4.227367E+00 | 5.481842E+00 | 4.379110E+00 | 1.093917E-01 | 3.021261E+00 | |
| 11,600 | 5.576453E+00 | 1.077732E+01 | 1.235374E+01 | 4.227367E+00 | 5.482377E+00 | 4.387385E+00 | 1.023464E-01 | 3.022040E+00 | |
| 11,950 | 5.548389E+00 | 1.038338E+01 | 1.242452E+01 | 4.227367E+00 | 5.495500E+00 | 4.379153E+00 | 9.877777E-02 | 3.028753E+00 | |
| 12,300 | 5.519111E+00 | 1.097477E+01 | 1.251133E+01 | 4.227367E+00 | 5.401124E+00 | 4.380134E+00 | 9.599397E-02 | 3.032859E+00 | |
| 12,650 | 5.490388E+00 | 9.529333E+00 | 1.260989E+01 | 4.227367E+00 | 5.394886E+00 | 4.373326E+00 | 9.387866E-02 | 3.035921E+00 | |
| 13,000 | 5.461367E+00 | 9.105733E+00 | 1.266573E+01 | 4.227367E+00 | 5.396621E+00 | 4.338008E+00 | 9.214341E-02 | 3.039377E+00 | |
| 13,350 | 5.432346E+00 | 8.702106E+00 | 1.274007E+01 | 4.227367E+00 | 5.283797E+00 | 4.339137E+00 | 9.076822E-02 | 3.042717E+00 | |
| 13,700 | 5.355830E+00 | 8.314643E+00 | 1.281332E+01 | 4.227367E+00 | 5.160999E+00 | 4.315564E+00 | 8.935932E-02 | 3.040950E+00 | |
| 14,050 | 5.295935E+00 | 7.915737E+00 | 1.288484E+01 | 4.227367E+00 | 5.193391E+00 | 4.301814E+00 | 8.864639E-02 | 3.040940E+00 | |
| 14,400 | 5.247232E+00 | 7.610223E+00 | 1.295406E+01 | 4.227367E+00 | 5.130711E+00 | 4.316837E+00 | 8.748540E-02 | 3.051939E+00 | |
| 14,750 | 5.202347E+00 | 7.290538E+00 | 1.302180E+01 | 4.227367E+00 | 5.161179E+00 | 4.311656E+00 | 8.665659E-02 | 3.054717E+00 | |
| 15,100 | 5.151274E+00 | 6.919130E+00 | 1.308773E+01 | 4.227367E+00 | 5.097273E+00 | 4.310648E+00 | 8.557634E+00 | 3.057364E+00 | |
| 15,450 | 5.068252E+00 | 6.714104E+00 | 1.315246E+01 | 4.227367E+00 | 5.035331E+00 | 4.310258E+00 | 8.471509E+00 | 3.059942E+00 | |
| 15,800 | 5.004214E+00 | 6.457644E+00 | 1.315131E+01 | 4.227367E+00 | 4.972268E+00 | 4.309577E+00 | 8.394899E+00 | 3.062481E+00 | |
| 16,150 | 4.936141E+00 | 6.219946E+00 | 1.317944E+01 | 4.227367E+00 | 4.908196E+00 | 4.310424E+00 | 8.320505E+00 | 3.064969E+00 | |
| 16,500 | 4.887242E+00 | 5.962948E+00 | 1.334197E+01 | 4.227367E+00 | 4.844961E+00 | 4.310538E+00 | 8.247272E+00 | 3.067498E+00 | |
| 16,850 | 4.829100E+00 | 5.779740E+00 | 1.340401E+01 | 4.227367E+00 | 4.782944E+00 | 4.309901E+00 | 8.178649E+00 | 3.069996E+00 | |
| 17,200 | 4.771951E+00 | 5.613109E+00 | 1.346557E+01 | 4.227367E+00 | 4.721334E+00 | 4.309788E+00 | 8.117635E+00 | 3.072472E+00 | |
| 17,550 | 4.698251E+00 | 5.442336E+00 | 1.352665E+01 | 4.227367E+00 | 4.660096E+00 | 4.310053E+00 | 8.066443E+00 | 3.074942E+00 | |
| 17,900 | 4.624254E+00 | 5.286221E+00 | 1.358722E+01 | 4.227367E+00 | 4.599928E+00 | 4.310378E+00 | 8.011332E+00 | 3.077396E+00 | |
| 18,250 | 4.570129E+00 | 5.112494E+00 | 1.364722E+01 | 4.227367E+00 | 4.539744E+00 | 4.310423E+00 | 7.953348E+00 | 3.079428E+00 | |
| 18,600 | 4.501404E+00 | 5.007408E+00 | 1.370656E+01 | 4.227367E+00 | 4.479803E+00 | 4.310678E+00 | 7.905951E+00 | 3.082223E+00 | |
| 18,950 | 4.436332E+00 | 4.884056E+00 | 1.376530E+01 | 4.227367E+00 | 4.419805E+00 | 4.310778E+00 | 7.858400E+00 | 3.084595E+00 | |
| 19,300 | 4.373183E+00 | 4.769944E+00 | 1.382341E+01 | 4.227367E+00 | 4.359630E+00 | 4.310837E+00 | 7.822089E+00 | 3.086940E+00 | |
| 19,650 | 4.320064E+00 | 4.661320E+00 | 1.388083E+01 | 4.227367E+00 | 4.299741E+00 | 4.311226E+00 | 7.776721E+00 | 3.089253E+00 | |
| 20,000 | 4.262101E+00 | 4.565712E+00 | 1.393755E+01 | 4.227367E+00 | 4.240014E+00 | 4.311494E+00 | 7.749349E+00 | 3.091539E+00 | |
| 20,350 | 4.213210E+00 | 4.473759E+00 | 1.399355E+01 | 4.227165E+00 | 4.180488E+00 | 4.311707E+00 | 7.702655E+00 | 3.093791E+00 | |
| 20,700 | 4.156293E+00 | 4.387481E+00 | 1.404828E+01 | 4.227479E+00 | 4.121272E+00 | 4.312164E+00 | 7.674677E+00 | 3.096509E+00 | |
| 21,050 | 4.076246E+00 | 4.306385E+00 | 1.410334E+01 | 4.218159E+00 | 4.062102E+00 | 4.333109E+00 | 7.636705E+00 | 3.098194E+00 | |
| 21,400 | 4.014997E+00 | 4.229603E+00 | 1.415712E+01 | 4.206855E+00 | 4.002057E+00 | 4.314704E+00 | 7.612191E+00 | 3.100344E+00 | |
| 21,750 | 3.961713E+00 | 4.156174E+00 | 4.120171E+01 | 4.191729E+00 | 3.940036E+00 | 4.317434E+00 | 7.582751E+00 | 3.102274E+00 | |
| 22,100 | 3.903858E+00 | 4.084952E+00 | 4.142624E+01 | 4.173874E+00 | 3.875075E+00 | 4.320690E+00 | 7.556511E+00 | 3.104686E+00 | |
| 22,450 | 3.817552E+00 | 4.011866E+00 | 4.143195E+01 | 4.150166E+00 | 3.806764E+00 | 4.323667E+00 | 7.518785E+00 | 3.108276E+00 | |
| 22,800 | 3.766463E+00 | 3.946085E+00 | 4.136459E+01 | 4.132520E+00 | 3.735234E+00 | 4.326567E+00 | 7.490124E+00 | 3.108768E+00 | |
| 23,150 | 3.673212E+00 | 3.876842E+00 | 4.144248E+01 | 4.109616E+00 | 3.660616E+00 | 4.329108E+00 | 7.464232E+00 | 3.110486E+00 | |
| 23,500 | 3.593263E+00 | 3.807286E+00 | 4.146297E+01 | 4.083544E+00 | 3.583904E+00 | 4.335751E+00 | 7.436322E+00 | 3.112265E+00 | |
| 23,850 | 3.515277E+00 | 3.737181E+00 | 4.155109E+01 | 4.061252E+00 | 3.504464E+00 | 4.335767E+00 | 7.388465E+00 | 3.114657E+00 | |
| 24,200 | 3.445218E+00 | 3.666285E+00 | 4.155710E+01 | 4.033767E+00 | 3.423699E+00 | 4.337485E+00 | 7.349639E+00 | 3.118290E+00 | |
| 24,550 | 3.355045E+00 | 3.594336E+00 | 4.160247E+01 | 4.000462E+00 | 3.410030E+00 | 4.337485E+00 | 7.311892E+00 | 3.120072E+00 | |
| 24,900 | 3.298192E+00 | 3.523598E+00 | 4.164646E+01 | 3.978748E+00 | 3.281293E+00 | 4.325535E+00 | 7.281350E+00 | 3.121802E+00 | |

JAERI-M 7329

** RFLAP4J ANALYSIS FOR STANDARD PROBLEM NO.5 L1=4:JAERI **

MIXTURE LEVEL

| PRESSURE | | | | | | (LE-1ST-(1,2), (LT-P139-6) (LT-P138-58) | | |
|------------|--------------|---------------|--------------|---------------|--------------|---|---------------|--------------|
| (PE-CS-1A) | (PE-PC-4) | (PE-SV-18) | (PT-P120-43) | (PE-BL-1) | | LE-2ST-(1,2) | LE-2ST-(1,2) | |
| TIME | AP14 | AP22 | AP26 | AP31 | AP21 | AML11 | AML22 | AML26 |
| SEC | MPA | MPA | MPA | MPA | MPA | M | M | M |
| 25.600 | 5.179326E+00 | 3.389062E+00 | 1.473287E+01 | 3.921632E+00 | 3.169397E+00 | 4.326846E+00 | 7.257545E+02 | 3.123494E+00 |
| 25.950 | 3.117641E+00 | 3.324554E+00 | 1.477451E+01 | 3.892891E+00 | 3.104495E+00 | 4.325167E+00 | 7.219537E+02 | 3.125142E+00 |
| 26.300 | 3.059215E+00 | 3.260679E+00 | 1.441523E+01 | 3.863915E+00 | 3.038852E+00 | 4.328497E+00 | 7.194399E+02 | 3.126754E+00 |
| 26.650 | 3.961682E+00 | 3.197393E+00 | 1.449550E+01 | 3.829371E+00 | 3.096963E+00 | 4.328802E+00 | 7.164010E+02 | 3.129338E+00 |
| 27.000 | 2.917112E+00 | 3.142911E+00 | 1.439415E+01 | 3.803299E+00 | 3.095845E+00 | 4.324996E+00 | 7.140588E+02 | 3.129897E+00 |
| 27.350 | 2.854111E+00 | 3.070617E+00 | 1.446323E+01 | 3.775707E+00 | 2.837691E+00 | 4.328471E+00 | 7.105871E+02 | 3.131433E+00 |
| 27.700 | 2.785926E+00 | 3.007726E+00 | 1.446693E+01 | 3.745966E+00 | 2.770166E+00 | 4.322406E+00 | 7.075593E+02 | 3.132947E+00 |
| 28.050 | 2.720594E+00 | 2.945144E+00 | 1.500664E+01 | 3.716106E+00 | 2.703531E+00 | 4.324664E+00 | 7.051539E+02 | 3.134491E+00 |
| 28.400 | 2.645912E+00 | 2.882204E+00 | 1.504725E+01 | 3.686158E+00 | 2.635314E+00 | 4.324012E+00 | 7.010539E+02 | 3.135913E+00 |
| 28.750 | 2.577632E+00 | 2.820714E+00 | 1.507720E+01 | 3.6565153E+00 | 2.567666E+00 | 4.323059E+00 | 6.985736E+02 | 3.137362E+00 |
| 29.100 | 2.517517E+00 | 2.758862E+00 | 1.511120E+01 | 3.626120E+00 | 2.501610E+00 | 4.322263E+00 | 6.961005E+02 | 3.138787E+00 |
| 29.450 | 2.449072E+00 | 2.693390E+00 | 1.514545E+01 | 3.598090E+00 | 2.436214E+00 | 4.321594E+00 | 6.918552E+02 | 3.140186E+00 |
| 29.800 | 2.386715E+00 | 2.626185E+00 | 1.517682E+01 | 3.565098E+00 | 2.371353E+00 | 4.320809E+00 | 6.892784E+02 | 3.141559E+00 |
| 30.150 | 2.323797E+00 | 2.557007E+00 | 1.520825E+01 | 3.536153E+00 | 2.307207E+00 | 4.320002E+00 | 6.868193E+02 | 3.142904E+00 |
| 30.500 | 2.260346E+00 | 2.5110456E+00 | 1.523885E+01 | 3.505299E+00 | 2.244194E+00 | 4.319340E+00 | 6.830096E+02 | 3.144225E+00 |
| 30.850 | 2.191994E+00 | 2.456914E+00 | 1.526884E+01 | 3.476557E+00 | 2.182487E+00 | 4.318763E+00 | 6.806193E+02 | 3.145519E+00 |
| 31.200 | 2.139129E+00 | 2.399841E+00 | 1.529761E+01 | 3.446594E+00 | 2.121734E+00 | 4.318140E+00 | 5.768056E+02 | 3.146788E+00 |
| 31.550 | 2.087316E+00 | 2.340429E+00 | 1.532578E+01 | 3.417495E+00 | 2.062185E+00 | 4.317546E+00 | 6.731267E+02 | 3.148030E+00 |
| 31.900 | 2.021585E+00 | 2.283939E+00 | 1.535317E+01 | 3.393517E+00 | 2.003885E+00 | 4.316924E+00 | 6.706006E+02 | 3.149425E+00 |
| 32.250 | 1.953144E+00 | 2.227475E+00 | 1.537976E+01 | 3.359127E+00 | 1.946605E+00 | 4.316214E+00 | 6.683317E+02 | 3.150431E+00 |
| 32.600 | 1.873124E+00 | 2.172905E+00 | 1.540578E+01 | 3.310222E+00 | 1.890722E+00 | 4.315551E+00 | 6.637745E+02 | 3.151589E+00 |
| 32.950 | 1.815248E+00 | 2.118649E+00 | 1.543059E+01 | 3.301592E+00 | 1.836255E+00 | 4.313425E+00 | 6.612957E+02 | 3.152717E+00 |
| 33.300 | 1.749462E+00 | 2.064377E+00 | 1.545482E+01 | 3.273164E+00 | 1.784616E+00 | 4.311408E+00 | 6.583096E+02 | 3.153816E+00 |
| 33.650 | 1.687344E+00 | 2.013244E+00 | 1.547828E+01 | 3.245010E+00 | 1.730872E+00 | 4.311321E+00 | 6.554979E+02 | 3.154888E+00 |
| 34.000 | 1.624153E+00 | 1.962078E+00 | 1.550093E+01 | 3.217105E+00 | 1.680086E+00 | 4.312557E+00 | 6.521120E+02 | 3.155933E+00 |
| 34.350 | 1.564741E+00 | 1.911801E+00 | 1.552290E+01 | 3.182947E+00 | 1.630646E+00 | 4.311176E+00 | 6.500553E+02 | 3.156957E+00 |
| 34.700 | 1.507014E+00 | 1.862016E+00 | 1.555413E+01 | 3.152116E+00 | 1.582665E+00 | 4.310971E+00 | 6.453590E+02 | 3.157962E+00 |
| 35.050 | 1.455506E+00 | 1.814657E+00 | 1.558647E+01 | 3.135054E+00 | 1.538895E+00 | 4.310862E+00 | 6.429854E+02 | 3.158951E+00 |
| 35.400 | 1.413920E+00 | 1.775753E+00 | 1.561875E+01 | 3.108305E+00 | 1.494235E+00 | 4.303362E+00 | 6.411351E+02 | 3.159927E+00 |
| 35.750 | 1.374436E+00 | 1.724860E+00 | 1.564040E+01 | 3.081868E+00 | 1.451524E+00 | 4.303070E+00 | 6.365061E+02 | 3.160890E+00 |
| 36.100 | 1.342693E+00 | 1.678105E+00 | 1.567293E+01 | 3.055761E+00 | 1.407576E+00 | 4.303720E+00 | 6.3354522E+02 | 3.161837E+00 |
| 36.450 | 1.313272E+00 | 1.634655E+00 | 1.569412E+01 | 3.030000E+00 | 1.364186E+00 | 4.3036380E+00 | 6.307790E+02 | 3.162768E+00 |
| 36.800 | 1.286394E+00 | 1.591574E+00 | 1.569584E+01 | 3.004542E+00 | 1.321110E+00 | 4.3030520E+00 | 6.286466E+02 | 3.163680E+00 |
| 37.150 | 1.261717E+00 | 1.550135E+00 | 1.567608E+01 | 2.979386E+00 | 1.278675E+00 | 4.3030996E+00 | 6.270157E+02 | 3.164572E+00 |
| 37.500 | 1.237341E+00 | 1.510166E+00 | 1.569263E+01 | 2.954531E+00 | 1.237356E+00 | 4.303082E+00 | 6.221636E+02 | 3.165442E+00 |
| 37.850 | 1.214548E+00 | 1.484912E+00 | 1.570860E+01 | 2.929981E+00 | 1.197773E+00 | 4.301396E+00 | 6.200754E+02 | 3.166289E+00 |
| 38.200 | 1.194474E+00 | 1.462981E+00 | 1.571239E+01 | 2.905735E+00 | 1.158708E+00 | 4.300098E+00 | 6.186164E+02 | 3.167113E+00 |
| 38.550 | 1.175250E+00 | 1.441790E+00 | 1.573881E+01 | 2.881792E+00 | 1.121403E+00 | 4.298713E+00 | 6.137805E+02 | 3.167133E+00 |
| 38.900 | 1.157066E+00 | 1.420408E+00 | 1.575307E+01 | 2.858158E+00 | 1.085262E+00 | 4.297292E+00 | 6.115740E+02 | 3.168690E+00 |
| 39.250 | 1.140336E+00 | 1.398556E+00 | 1.576680E+01 | 2.834631E+00 | 1.050319E+00 | 4.295771F+00 | 6.104265E+02 | 3.169446E+00 |
| 39.600 | 1.124662E+00 | 1.374267E+00 | 1.578217E+01 | 2.810086E+00 | 1.016425E+00 | 4.294286E+00 | 6.056645E+02 | 3.170183E+00 |
| 39.950 | 1.110330E+00 | 1.351035E+00 | 1.579721E+01 | 2.787949E+00 | 9.838376E+01 | 4.292907E+00 | 6.051060E+02 | 3.170933E+00 |
| 40.300 | 9.762211E+01 | 1.214234E+00 | 1.580496E+01 | 2.766652E+00 | 9.527959E+01 | 4.291525E+00 | 6.025526E+02 | 3.171609E+00 |
| 40.650 | 9.468234E+01 | 1.181539E+00 | 1.581676E+01 | 2.746592E+00 | 9.218749E+01 | 4.290044E+00 | 5.976398E+02 | 3.172301E+00 |
| 41.000 | 9.176634E+01 | 1.149766E+00 | 1.582813E+01 | 2.722794E+00 | 8.92049E+01 | 4.288334E+00 | 5.959930E+02 | 3.172980E+00 |
| 41.350 | 8.900257E+01 | 1.118442E+00 | 1.583902E+01 | 2.701297E+00 | 8.640307E+01 | 4.287663E+00 | 5.951383E+02 | 3.173645E+00 |
| 41.700 | 8.633434E+01 | 1.084861E+00 | 1.585049E+01 | 2.680101E+00 | 8.370705E+01 | 4.285329E+00 | 5.949506E+02 | 3.174299E+00 |
| 42.050 | 8.382271E+01 | 1.059749E+00 | 1.586956E+01 | 2.659204E+00 | 8.109436E+01 | 4.283770E+00 | 5.885049E+02 | 3.174940E+00 |

** RFLAP4J ANALYSIS FOR STANDARD PROBLEM NO.5 L1=4:JAERI **

MIXTURE LEVEL

| PRESSURE | | | | | | (LE-1ST-(1,2), (LT-P139-6) (LT-P138-58) | | |
|------------|--------------|---------------|--------------|--------------|--------------|---|---------------|---------------|
| (PE-CS-1A) | (PE-PC-4) | (PE-SV-18) | (PT-P120-43) | (PE-BL-1) | | LE-2ST-(1,2) | LE-2ST-(1,2) | |
| TIME | AP14 | AP22 | AP26 | AP31 | AP21 | AML11 | AML22 | AML26 |
| SEC | MPA | MPA | MPA | MPA | MPA | M | M | M |
| 42.400 | 8.137904E-01 | 1.0301529E+00 | 1.586940E+01 | 2.638604E+00 | 7.857922E+01 | 4.282204E+00 | 5.877588E+02 | 3.175570E+00 |
| 42.750 | 8.177742E-01 | 1.004206E+00 | 1.587880E+01 | 2.618297E+00 | 7.614946E+01 | 4.280505E+00 | 5.825155E+02 | 3.176188E+00 |
| 43.100 | 7.444724E-01 | 9.777720E+00 | 1.587886E+01 | 2.598828E+00 | 7.385646E+01 | 4.279255E+00 | 5.810693E+02 | 3.176794E+00 |
| 43.450 | 7.450511E-01 | 9.523070E+00 | 1.589661E+01 | 2.578656E+00 | 7.164603E+01 | 4.277935E+00 | 5.805823E+02 | 3.177386E+00 |
| 43.800 | 7.242608E+00 | 9.275791E+00 | 1.590506E+01 | 2.559321E+00 | 6.984809E+01 | 4.276610E+00 | 5.779515E+02 | 3.177911E+00 |
| 44.150 | 7.145191E+00 | 9.024212E+00 | 1.591520E+01 | 2.542107E+00 | 6.821021E+01 | 4.274125E+00 | 5.743933E+02 | 3.178905E+00 |
| 44.500 | 6.945555E+00 | 8.767579E+00 | 1.592664E+01 | 2.502470E+00 | 6.532267E+01 | 4.271315E+00 | 5.6951912E+02 | 3.179442E+00 |
| 44.850 | 6.755147E+00 | 8.513945E+00 | 1.593559E+01 | 2.484135E+00 | 6.172348E+01 | 4.269729E+00 | 5.657554E+02 | 3.180174E+00 |
| 45.200 | 6.573433E+00 | 8.263348E+00 | 1.594246E+01 | 2.466671E+00 | 5.997977E+01 | 4.267349E+00 | 5.617591E+02 | 3.180493E+00 |
| 45.550 | 6.403736E+00 | 8.012173E+00 | 1.594974E+01 | 2.448270E+00 | 5.827942E+01 | 4.265179E+00 | 5.5617907E+02 | 3.181199E+00 |
| 45.900 | 6.247573E+00 | 7.761926E+00 | 1.595622E+01 | 2.431027E+00 | 5.661931E+01 | 4.263865E+00 | 5.468065E+02 | 3.1817541E+00 |
| 46.250 | 6.111091E+00 | 7.5163421E+00 | 1.595952E+01 | 2.413989E+00 | 5.480249E+01 | 4.262523E+00 | 5.416632E+02 | 3.182166E+00 |
| 46.600 | 4.464137E+00 | 7.245736E+00 | 1.596520E+01 | 2.392836E+00 | 4.432299E+01 | 4.255213E+00 | 5.344398E+02 | 3.182630E+00 |
| 47.000 | 3.796213E+00 | 7.002571E+00 | 1.597151E+01 | 2.37375 | | | | |

** RELAP4J ANALYSIS FOR STANDARD PROBLEM NO.5 L1=4(JAERI) **

| DENSITY | | | | | | VOLUMETRIC FLOW | | |
|---------|---------------|--------------|---------------|--------------|--------------|-----------------|--------------|---------------|
| TIME | (DE-PC-1) | (DE-PC-2) | (DE-PC-3) | (DE-BL-1) | (DE-BL-2) | (FT-P120-36-1) | (FT-P120-85) | (FT-P128-104) |
| SEC | MG/M3 | MG/M3 | MG/M3 | MG/M3 | MG/M3 | LITER/SEC | LITER/SEC | LITER/SEC |
| 0.0 | 7.660482E+01 | 7.659596E+01 | 7.6617455E+01 | 7.641611E+01 | 7.659596E+01 | 0.0 | 0.0 | 0.0 |
| 0.070 | 7.608131E+01 | 7.611174E+01 | 7.615932E+01 | 7.589533E+01 | 7.613309E+01 | 9.592824E+03 | 0.0 | 0.0 |
| 0.140 | 7.573313E+01 | 7.573691E+01 | 7.576130E+01 | 7.556330E+01 | 7.575324E+01 | -1.813551E+02 | 0.0 | 0.0 |
| 0.210 | 7.571944E+01 | 7.570412E+01 | 7.556976E+01 | 7.492057E+01 | 7.571528E+01 | 2.473350E+02 | 0.0 | 0.0 |
| 0.280 | 7.572004E+01 | 7.570380E+01 | 7.558297E+01 | 7.513130E+01 | 7.571091E+01 | -2.903970E+02 | 0.0 | 0.0 |
| 0.350 | 7.571920E+01 | 7.569592E+01 | 7.572928E+01 | 7.425484E+01 | 7.570577E+01 | 3.073668E+02 | 0.0 | 0.0 |
| 0.420 | 7.571985E+01 | 7.570132E+01 | 7.571706E+01 | 7.353102E+01 | 7.570595E+01 | -2.989956E+02 | 0.0 | 0.0 |
| 0.490 | 7.571957E+01 | 7.570359E+01 | 7.570307E+01 | 7.216323E+01 | 7.570623E+01 | 2.674633E+02 | 0.0 | 0.0 |
| 0.560 | 7.571975E+01 | 7.569866E+01 | 7.557398E+01 | 7.015046E+01 | 7.570233E+01 | -2.164912E+02 | 0.0 | 0.0 |
| 0.630 | 7.571953E+01 | 7.569262E+01 | 7.505367E+01 | 7.918876E+01 | 7.569825E+01 | 1.513366E+02 | 0.0 | 0.0 |
| 0.700 | 7.571961E+01 | 7.569597E+01 | 7.4531516E+01 | 6.711422E+01 | 7.569555E+01 | -7.772333E+03 | 0.0 | 0.0 |
| 0.770 | 7.571940E+01 | 7.569497E+01 | 7.440348E+01 | 6.574388E+01 | 7.569446E+01 | 2.185953E+04 | 0.0 | 0.0 |
| 0.840 | 7.571903E+01 | 7.569201E+01 | 7.416719E+01 | 6.418426E+01 | 7.569396E+01 | 6.863653E+03 | 0.0 | 0.0 |
| 0.910 | 7.571822E+01 | 7.568980E+01 | 7.347878E+01 | 6.282902E+01 | 7.567049E+01 | -1.272122E+02 | 0.0 | 0.0 |
| 0.980 | 7.571704E+01 | 7.568455E+01 | 7.274113E+01 | 6.201611E+01 | 7.566981E+01 | 1.697925E+02 | 0.0 | 0.0 |
| 1.050 | 7.571594E+01 | 7.568649E+01 | 7.224648E+01 | 6.066274E+01 | 7.568710E+01 | -1.946492E+02 | 0.0 | 0.0 |
| 1.120 | 7.571398E+01 | 7.568373E+01 | 7.171765E+01 | 6.022156E+01 | 7.568413E+01 | 2.016504E+02 | 0.0 | 0.0 |
| 1.190 | 7.571176E+01 | 7.568124E+01 | 7.086618E+01 | 5.935568E+01 | 7.568127E+01 | -1.912004E+02 | 0.0 | 0.0 |
| 1.260 | 7.570893E+01 | 7.567884E+01 | 7.002209E+01 | 5.916452E+01 | 7.567840E+01 | 1.673300E+02 | 0.0 | 0.0 |
| 1.330 | 7.570569E+01 | 7.567682E+01 | 6.918244E+01 | 5.862386E+01 | 7.567571E+01 | -1.322577E+02 | 0.0 | 0.0 |
| 1.400 | 7.570165E+01 | 7.567530E+01 | 6.829218E+01 | 5.851124E+01 | 7.567315E+01 | 9.012229E+03 | 0.0 | 0.0 |
| 1.470 | 7.567322E+01 | 7.567315E+01 | 6.738659E+01 | 5.823641E+01 | 7.567049E+01 | -4.501211E+03 | 0.0 | 0.0 |
| 1.540 | 7.569208E+01 | 7.567146E+01 | 6.651005E+01 | 5.813045E+01 | 7.566796E+01 | 4.895012E+03 | 0.0 | 0.0 |
| 1.610 | 7.568679E+01 | 7.565967E+01 | 6.568089E+01 | 5.791523E+01 | 7.566541E+01 | 3.916549E+03 | 0.0 | 0.0 |
| 1.680 | 7.568059E+01 | 7.566719E+01 | 6.454838E+01 | 5.818709E+01 | 7.566299E+01 | -7.209335E+03 | 0.0 | 0.0 |
| 1.750 | 7.567307E+01 | 7.566614E+01 | 6.288344E+01 | 5.903496E+01 | 7.566073E+01 | 6.632630E+03 | 0.0 | 0.0 |
| 1.820 | 7.566049E+01 | 7.566334E+01 | 6.265027E+01 | 6.081300E+01 | 7.566585E+01 | -1.100100E+02 | 0.0 | 0.0 |
| 1.890 | 7.565625E+01 | 7.565257E+01 | 6.2446254E+01 | 5.513434E+01 | 7.565569E+01 | 1.139951E+02 | 0.0 | 0.0 |
| 1.960 | 7.565017E+01 | 7.566176E+01 | 6.085043E+01 | 6.110529E+01 | 7.565638E+01 | -1.083661E+02 | 0.0 | 0.0 |
| 2.150 | 7.559170E+01 | 7.566191E+01 | 5.918664E+01 | 5.789305E+01 | 7.565658E+01 | -2.139176E+03 | 0.0 | 0.0 |
| 2.500 | 7.371691E+01 | 7.561941E+01 | 5.628256E+01 | 5.850250E+01 | 7.566213E+01 | 5.530642E+03 | 0.0 | 0.0 |
| 2.850 | 6.933204E+01 | 7.562854E+01 | 5.219495E+01 | 5.763385E+01 | 7.564952E+01 | 1.396908E+05 | 0.0 | 0.0 |
| 3.200 | 6.854131E+01 | 7.567556E+01 | 4.820973E+01 | 5.420313E+01 | 7.490535E+01 | -2.168045E+03 | 0.0 | 0.0 |
| 3.550 | 6.366818E+01 | 7.322709E+01 | 4.684224E+01 | 5.462212E+01 | 7.551257E+01 | 3.368890E+04 | 0.0 | 0.0 |
| 3.900 | 6.2551110E+01 | 6.802071E+01 | 4.358675E+01 | 5.367178E+01 | 7.366036E+01 | 8.027052E+04 | 0.0 | 0.0 |
| 4.250 | 5.866767E+01 | 5.618926E+01 | 4.2446254E+01 | 5.513434E+01 | 7.565569E+01 | -2.493517E+04 | 0.0 | 0.0 |
| 4.600 | 5.726479E+01 | 4.797000E+01 | 3.99979E+01 | 5.131935E+01 | 7.296161E+01 | -2.612655E+04 | 0.0 | 0.0 |
| 4.950 | 5.542565E+01 | 3.934458E+01 | 3.825679E+01 | 4.897941E+01 | 7.286608E+01 | 1.253115E+04 | 0.0 | 0.0 |
| 5.300 | 5.322135E+01 | 3.162862E+01 | 3.760224E+01 | 4.837572E+01 | 7.182424E+01 | 7.328357E+03 | 0.0 | 0.0 |
| 5.650 | 5.285966E+01 | 2.690701E+01 | 5.535808E+01 | 3.996651E+01 | 6.688546E+01 | -5.081646E+05 | 0.0 | 0.0 |
| 6.000 | 5.212721E+01 | 2.290678E+01 | 3.388540E+01 | 3.819852E+01 | 6.254775E+01 | -1.837673E+05 | 0.0 | 0.0 |
| 6.350 | 4.906336E+01 | 1.981370E+01 | 3.253263E+01 | 3.615645E+01 | 5.306777E+01 | 2.114239E+05 | 0.0 | 0.0 |
| 6.700 | 4.715979E+01 | 1.777581E+01 | 3.130855E+01 | 3.946655E+01 | 4.387024E+01 | 3.587932E+06 | 0.0 | 0.0 |
| 7.050 | 4.54021CE+01 | 1.642853E+01 | 3.002298E+01 | 3.883669E+01 | 3.510030E+01 | -6.9265557E+06 | 0.0 | 0.0 |
| 7.400 | 4.362467E+01 | 1.552458E+01 | 2.862222E+01 | 4.112408E+01 | 2.779718E+01 | -2.965774E+07 | 0.0 | 0.0 |
| 7.750 | 4.185779E+01 | 1.491139E+01 | 2.737061E+01 | 4.090699E+01 | 2.196775E+01 | 1.905731E+06 | 0.0 | 0.0 |
| 8.100 | 4.066176E+01 | 1.446059E+01 | 2.629194E+01 | 4.323277E+01 | 1.761940E+01 | -9.86526E+08 | 0.0 | 0.0 |
| 8.450 | 3.883396E+01 | 1.415247E+01 | 2.522535E+01 | 4.378218E+01 | 1.456559E+01 | -4.245461E+07 | 0.0 | 0.0 |

** RELAP4J ANALYSIS FOR STANDARD PROBLEM NO.5 L1=4(JAERI) **

| DENSITY | | | | | | VOLUMETRIC FLOW | | |
|---------|--------------|--------------|--------------|---------------|---------------|-----------------|--------------|---------------|
| TIME | (DE-PC-1) | (DE-PC-2) | (DE-PC-3) | (DE-BL-1) | (DE-BL-2) | (FT-P120-36-1) | (FT-P120-85) | (FT-P128-104) |
| SEC | MG/M3 | MG/M3 | MG/M3 | MG/M3 | MG/M3 | LITER/SEC | LITER/SEC | LITER/SEC |
| 8.800 | 3.791584E+01 | 1.394978E+01 | 2.437448E+01 | 4.353849E+01 | 1.329883E+01 | 4.705040E+08 | 0.0 | 0.0 |
| 9.150 | 3.658205E+01 | 1.379950E+01 | 2.310111E+01 | 4.308652E+01 | 1.239121E+01 | 6.752582E+08 | 0.0 | 0.0 |
| 9.500 | 3.531197E+01 | 1.370325E+01 | 2.252399E+01 | 4.252702E+01 | 1.189422E+01 | 8.582824E+09 | 0.0 | 0.0 |
| 9.850 | 3.447542E+01 | 1.359509E+01 | 2.160363E+01 | 3.524426E+01 | 1.171637E+01 | -9.480666E+09 | 0.0 | 0.0 |
| 10.200 | 3.302357E+01 | 1.349956E+01 | 2.078694E+01 | 3.511267E+01 | 1.145626E+01 | 2.026266E+09 | 0.0 | 0.0 |
| 10.550 | 3.162410E+01 | 1.341140E+01 | 1.988389E+01 | 3.195486E+01 | 1.158359E+01 | 1.671202E+09 | 0.0 | 0.0 |
| 10.900 | 3.007061E+01 | 1.318494E+01 | 1.910181E+01 | 2.843871E+01 | 1.169245E+01 | 5.39230E+10 | 0.0 | 0.0 |
| 11.250 | 2.908984E+01 | 1.293642E+01 | 1.841013E+01 | 2.889474E+01 | 1.167621E+01 | -1.120247E+10 | 0.0 | 0.0 |
| 11.600 | 2.807948E+01 | 1.052321E+01 | 1.749274E+01 | 2.926571E+01 | 9.550796E+02 | 5.674620E+00 | 0.0 | 0.0 |
| 11.950 | 2.662975E+01 | 4.843904E+01 | 1.618090E+01 | 2.807608E+01 | 9.174030E+02 | -5.653349E+11 | 0.0 | 0.0 |
| 12.300 | 2.362126E+01 | 5.778760E+01 | 1.617650E+01 | 2.474676E+01 | 8.278788E+02 | -4.174377E+11 | 0.0 | 0.0 |
| 12.650 | 2.030379E+01 | 5.454305E+01 | 1.594040E+01 | 2.391159E+01 | 7.306230E+02 | -1.508387E+11 | 0.0 | 0.0 |
| 13.000 | 2.347439E+01 | 4.553700E+01 | 1.479040E+01 | 2.605230E+01 | 6.494913E+02 | 1.140496E+12 | 0.0 | 0.0 |
| 13.350 | 2.289509E+01 | 3.915345E+02 | 6.831674E+02 | 2.0033245E+02 | 5.793056E+02 | -9.069642E+13 | 0.0 | 0.0 |
| 13.700 | 2.151374E+01 | 3.509245E+02 | 6.149757E+02 | 1.780766E+02 | 5.925365E+02 | -2.747640E+12 | 0.0 | 0.0 |
| 14.050 | 2.061443E+01 | 3.267342E+02 | 6.248692E+02 | 1.320624E+02 | 7.047268E+02 | -8.885751E+12 | 0.0 | 0.0 |
| 14.400 | 1.969010E+01 | 3.171722E+02 | 6.081951E+02 | 1.202486E+02 | 7.047877E+01 | -9.354304E+13 | 0.0 | 0.0 |
| 14.750 | 1.866747E+01 | 3.265454E+02 | 6.160135E+02 | 1.518783E+02 | 6.639444E+02 | -1.469692E+12 | 0.0 | 0.0 |
| 15.100 | 1.765006E+01 | 3.489606E+02 | 1.093915E+02 | 1.453961E+02 | 1.0483525E+02 | -2.020700E+12 | 0.0 | 0.0 |
| 15.450 | 1.659171E+01 | 3.422929E+02 | 1.027205E+02 | 1.441736E+02 | 1.020814E+02 | -1.498284E+12 | 0.0 | 0.0 |
| 15.800 | 1.593344E+01 | 4.390520E+02 | 9.949045E+02 | 1.205623E+02 | 1.306624E+01 | -1.346492E+12 | 0.0 | 0.0 |
| 16.150 | 1.512942E+01 | 4.839677E+02 | 9.403568E+02 | 1.394810E+02 | 1.427782E+01 | -1.278756E+12 | 0.0 | 0.0 |
| 16.500 | 1.436266E+01 | 5.463149E+02 | 6.346187E+02 | 1.386337E+02 | 1.405285E+01 | -5.586188E+12 | 0.0 | 0.0 |
| 16.850 | 1.371072E+01 | 5.774104E+02 | 6.128466E+02 | 1.397222E+02 | 1.387220E+01 | -4.924647E+13 | 0.0 | 0.0 |
| 20.000 | 8.711772E+02 | 1.071132E+01 | 5.51421 | | | | | |

** RELAP4J ANALYSIS FOR STANDARD PROBLEM NO.5 L1-4:JAERI **

| DENSITY | | | | | | VOLUMETRIC FLOW | | |
|---------|--------------|--------------|---------------|--------------|---------------|-----------------|---------------|---------------|
| TIME | (DE-PC-1) | (DE-PC-2) | (DE-PC-3) | (DE-BL-1) | (DE-BL-2) | (FT-P120-36-1) | (FT-P120-85) | (FT-P128-104) |
| SEC | ADE10 | ADE1 | ADE6 | ADE21 | ADE15 | JW33 | JW34 | JW35 |
| MG/M3 | MG/M3 | MG/M3 | MG/M3 | MG/M3 | MG/M3 | LITER/SEC | LITER/SEC | LITER/SEC |
| 25.600 | 8.488530E-01 | 1.751099E-01 | 2.593612E-02 | 7.470166E-02 | 7.975048E-02 | 2.609910E+01 | 0.0 | 1.085379E+00 |
| 25.950 | 8.585972E-01 | 1.839680E-01 | 2.485101E-02 | 7.404139E-02 | 8.257687E-02 | 2.671486E+01 | 0.0 | 1.085379E+00 |
| 26.300 | 8.679909E-01 | 1.886349E-01 | 2.387260E-02 | 7.332669E-02 | 8.595313E-02 | 2.733186E+01 | 0.0 | 1.085379E+00 |
| 26.650 | 8.768926E-01 | 1.895377E-01 | 2.296731E-02 | 7.299826E-02 | 8.819598E-02 | 2.794022E+01 | 0.0 | 1.085379E+00 |
| 27.000 | 8.848529E-01 | 1.854630E-01 | 2.205567E-02 | 7.288169E-02 | 8.629760E-02 | 2.855533E+01 | 0.0 | 1.085379E+00 |
| 27.350 | 8.917257E-01 | 1.860186E-01 | 2.110221E-02 | 7.270948E-02 | 8.327545E-02 | 2.918117E+01 | 0.0 | 1.085379E+00 |
| 27.700 | 8.980587E-01 | 1.646030E-01 | 2.016170E-02 | 7.262965E-02 | 8.067419E-02 | 2.979112E+01 | 0.0 | 1.085379E+00 |
| 28.050 | 9.038114E-01 | 1.516605E-01 | 1.926639E-02 | 7.245607E-02 | 7.732680E-02 | 3.037852E+01 | 0.0 | 1.085379E+00 |
| 28.400 | 9.091184E-01 | 1.377596E-01 | 1.840973E-02 | 7.229709E-02 | 7.433798E-02 | 3.094546E+01 | 0.0 | 1.085379E+00 |
| 28.750 | 9.139437E-01 | 1.231287E-01 | 1.758218E-02 | 7.220610E-02 | 7.165027E-02 | 3.150028E+01 | 0.0 | 1.085379E+00 |
| 29.100 | 9.183178E-01 | 1.085765E-01 | 1.673450E-02 | 7.216618E-02 | 6.737139E-02 | 3.203656E+01 | 0.0 | 1.085379E+00 |
| 29.450 | 9.222841E-01 | 9.470290E-02 | 1.601869E-02 | 7.211841E-02 | 6.490333E-02 | 3.255502E+01 | 0.0 | 1.085379E+00 |
| 29.800 | 9.259948E-01 | 8.128384E-02 | 7.258179E-02 | 7.201677E-02 | 6.039117E-02 | 3.305416E+01 | 0.0 | 1.085379E+00 |
| 30.150 | 9.291970E-01 | 6.924795E-02 | 1.459032E-02 | 7.187839E-02 | 5.1639629E-02 | 3.353459E+01 | 0.0 | 1.085379E+00 |
| 30.500 | 9.323016E-01 | 5.894331E-02 | 7.176730E-02 | 5.176730E-02 | 5.176730E-02 | 3.399681E+01 | 0.0 | 1.085379E+00 |
| 30.850 | 9.351153E-01 | 4.998779E-02 | 1.330695E-02 | 1.330695E-02 | 1.330695E-02 | 3.443933E+01 | 0.0 | 1.085379E+00 |
| 31.200 | 9.376680E-01 | 4.247958E-02 | 1.272132E-02 | 1.272132E-02 | 1.272132E-02 | 3.480422E+01 | 0.0 | 1.085379E+00 |
| 31.550 | 9.401603E-01 | 3.521566E-02 | 1.217320E-02 | 1.217320E-02 | 1.217320E-02 | 3.527269E+01 | 0.0 | 1.085379E+00 |
| 31.900 | 9.429626E-01 | 3.102419E-02 | 1.165962E-02 | 1.165962E-02 | 1.165962E-02 | 3.566042E+01 | 0.0 | 1.085379E+00 |
| 32.250 | 9.449580E-02 | 2.673542E-02 | 1.117851E-02 | 1.117851E-02 | 1.117851E-02 | 3.603232E+01 | 0.0 | 1.085379E+00 |
| 32.600 | 9.465777E-02 | 2.322202E-02 | 1.072819E-02 | 1.072819E-02 | 1.072819E-02 | 3.639815E+01 | 0.0 | 1.085379E+00 |
| 32.950 | 9.485103E-02 | 2.039604E-02 | 1.030656E-02 | 7.071374E-02 | 3.363637E-02 | 3.672490E+01 | 0.0 | 1.085379E+00 |
| 33.300 | 9.502656E-02 | 1.814201E-02 | 9.909514E-02 | 7.048980E-02 | 7.301244E-02 | 3.704495E+01 | 0.0 | 1.085379E+00 |
| 33.650 | 9.516473E-02 | 1.636686E-02 | 9.534347E-02 | 7.026336E-02 | 6.098208E-02 | 3.735142E+01 | 0.0 | 1.085379E+00 |
| 34.000 | 9.534035E-02 | 1.498939E-02 | 9.179971E-02 | 7.004209E-02 | 6.482019E-02 | 3.764335E+01 | 0.0 | 1.085379E+00 |
| 34.350 | 9.545991E-02 | 1.393995E-02 | 8.845049E-02 | 6.991434E-02 | 4.822564E-02 | 3.791949E+01 | 0.0 | 1.085379E+00 |
| 34.700 | 9.557912E-02 | 1.315538E-02 | 8.652829E-02 | 6.959675E-02 | 5.092200E-02 | 3.811797E+01 | 0.0 | 1.085379E+00 |
| 35.050 | 9.572452E-02 | 1.220552E-02 | 8.375939E-02 | 6.979815E-02 | 4.752473E-02 | 3.840294E+01 | 0.0 | 1.085379E+00 |
| 35.400 | 9.585912E-02 | 1.133447E-02 | 8.077702E-02 | 6.939755E-02 | 4.149208E-02 | 3.841665E+01 | 0.0 | 1.085379E+00 |
| 35.750 | 9.597127E-02 | 1.067671E-02 | 7.1313538E-02 | 6.923292E-02 | 3.897347E-02 | 3.882490E+01 | 0.0 | 1.085379E+00 |
| 36.100 | 9.607328E-02 | 1.012042E-02 | 1.548178E-02 | 6.889420E-02 | 3.680870E-02 | 3.894647E+01 | 7.4046608E+00 | 1.085379E+00 |
| 36.450 | 9.618145E-02 | 9.470689E-02 | 1.756735E-02 | 6.868521E-02 | 3.060487E-02 | 3.913968E+01 | 2.9496666E+00 | 1.085379E+00 |
| 36.800 | 9.627279E-02 | 9.095965E-02 | 1.931015E-02 | 6.865980E-02 | 2.506365E-02 | 3.933579E+01 | 3.473881E+00 | 1.085379E+00 |
| 37.150 | 9.634335E-02 | 8.430548E-02 | 2.076426E-02 | 6.866194E-02 | 2.303061E-02 | 3.952730E+01 | 3.957173E+00 | 1.085379E+00 |
| 37.500 | 9.640365E-02 | 7.998215E-02 | 2.190484E-02 | 6.878477E-02 | 2.266221E-02 | 3.971341E+01 | 4.427293E+00 | 1.085379E+00 |
| 37.850 | 9.646677E-02 | 7.556620E-02 | 2.256415E-02 | 6.886474E-02 | 2.076242E-02 | 3.988127E+01 | 4.800480E+00 | 1.085379E+00 |
| 38.200 | 9.651616E-02 | 7.182240E-02 | 2.305095E-02 | 6.895594E-02 | 2.107802E-02 | 4.006493E+01 | 5.141286E+00 | 1.085379E+00 |
| 38.550 | 9.657008E-02 | 6.827590E-02 | 2.327874E-02 | 6.927021E-02 | 2.154754E-02 | 4.019818E+01 | 5.471023E+00 | 1.085379E+00 |
| 38.900 | 9.662560E-02 | 6.502247E-02 | 2.331163E-02 | 6.938029E-02 | 2.352804E-02 | 4.033630E+01 | 5.777670E+00 | 1.085379E+00 |
| 39.250 | 9.667439E-02 | 6.212311E-02 | 2.320887E-02 | 6.945097E-02 | 2.490102E-02 | 4.047161E+01 | 6.029329E+00 | 1.085379E+00 |
| 39.600 | 9.671739E-02 | 5.965265E-02 | 2.310274E-02 | 6.950303E-02 | 2.475270E-02 | 4.052233E+01 | 6.277279E+00 | 1.085379E+00 |
| 39.950 | 9.676185E-02 | 5.740377E-02 | 2.296708E-02 | 6.958305E-02 | 2.393390E-02 | 4.070208E+01 | 6.514303E+00 | 1.085379E+00 |
| 40.300 | 9.680204E-02 | 5.549771E-02 | 2.284217E-02 | 6.975975E-02 | 2.311747E-02 | 4.080399E+01 | 6.746584E+00 | 1.085379E+00 |
| 40.650 | 9.683377E-02 | 5.383662E-02 | 2.274562E-02 | 6.982346E-02 | 2.329733E-02 | 4.089587E+01 | 6.928207E+00 | 1.085379E+00 |
| 41.000 | 9.686179E-02 | 5.163785E-02 | 2.246756E-02 | 6.996263E-02 | 2.314612E-02 | 4.098758E+01 | 7.104806E+00 | 1.085379E+00 |
| 41.350 | 9.689904E-02 | 6.913439E-02 | 2.237517E-02 | 6.971775E-02 | 2.367667E-02 | 4.106250E+01 | 7.271252E+00 | 1.085379E+00 |
| 41.700 | 9.691707E-02 | 8.982223E-02 | 2.230406E-02 | 6.970469E-02 | 3.728200E-02 | 4.112965E+01 | 7.431623E+00 | 1.085379E+00 |
| 42.050 | 9.694181E-02 | 1.227204E-02 | 2.230160E-02 | 6.952942E-02 | 3.780957E-02 | 4.118854E+01 | 7.585224E+00 | 1.085379E+00 |

** RELAP4J ANALYSIS FOR STANDARD PROBLEM NO.5 L1-4:JAERI **

| DENSITY | | | | | | VOLUMETRIC FLOW | | |
|---------|------------------|--------------|--------------|--------------|--------------|-----------------|--------------|---------------|
| TIME | (DE-PC-1) | (DE-PC-2) | (DE-PC-3) | (DE-BL-1) | (DE-BL-2) | (FT-P120-36-1) | (FT-P120-85) | (FT-P128-104) |
| SEC | ADE10 | ADE1 | ADE6 | ADE21 | ADE15 | JW33 | JW34 | JW35 |
| MG/M3 | MG/M3 | MG/M3 | MG/M3 | MG/M3 | MG/M3 | LITER/SEC | LITER/SEC | LITER/SEC |
| 42.400 | 9.696427E-01 | 1.623747E-02 | 2.222021E-02 | 6.934008E-02 | 3.799408E-02 | 4.174037E+01 | 7.724105E+00 | 1.085379E+00 |
| 42.750 | 9.697397E-01 | 2.047594E-02 | 1.917901E-02 | 6.912137E-02 | 3.790859E-02 | 4.128878E+01 | 7.858096E+00 | 1.085379E+00 |
| 43.100 | 9.700311E-01 | 2.360191E-02 | 2.178204E-02 | 6.894495E-02 | 3.701844E-02 | 4.132059E+01 | 7.984618E+00 | 1.085379E+00 |
| 43.450 | 9.702882E-01 | 2.632328E-02 | 2.150404E-02 | 6.882934E-02 | 3.617497E-02 | 4.134717E+01 | 8.106348E+00 | 1.085379E+00 |
| 43.800 | 9.705334E-01 | 2.884963E-02 | 2.126858E-02 | 6.878231E-02 | 3.573553E-02 | 4.137100E+01 | 8.225529E+00 | 1.085379E+00 |
| 44.150 | 9.707943E-01 | 3.099310E-02 | 2.095350E-02 | 6.865813E-02 | 3.523344E-02 | 4.139147E+01 | 8.338474E+00 | 1.085379E+00 |
| 44.500 | 9.710496E-01 | 3.221148E-02 | 2.063399E-02 | 6.859049E-02 | 3.468757E-02 | 4.140657E+01 | 8.420444E+00 | 1.085379E+00 |
| 44.850 | 9.713209E-01 | 3.249486E-02 | 2.030500E-02 | 6.849721E-02 | 3.416242E-02 | 4.141212E+01 | 8.497723E+00 | 1.085379E+00 |
| 45.200 | 9.715107E-01 | 3.206571E-02 | 1.994362E-02 | 6.849711E-02 | 3.223812E-02 | 4.141199E+01 | 8.571571E+00 | 1.085379E+00 |
| 45.550 | 9.717822E-01 | 3.171229E-02 | 1.957141E-02 | 6.840647E-02 | 3.103002E-02 | 4.140642E+01 | 8.642884E+00 | 1.085379E+00 |
| 45.900 | 9.721538E-01 | 3.177596E-02 | 1.929011E-02 | 6.825673E-02 | 3.083882E-02 | 4.139702E+01 | 8.712757E+00 | 1.085379E+00 |
| 46.250 | 9.724521E-01 | 3.170716E-02 | 1.921707E-02 | 6.825607E-02 | 3.072031E-02 | 4.139400E+01 | 8.781362E+00 | 1.085379E+00 |
| 46.600 | 9.727261E-01 | 3.164170E-02 | 1.887592E-02 | 6.804616E-02 | 3.074182E-02 | 4.117772E+01 | 8.844242E+00 | 1.085379E+00 |
| 46.950 | 9.730150E-01 | 3.128240E-02 | 1.862807E-02 | 6.792321E-02 | 3.024992E-02 | 4.117376E+01 | 8.902198E+00 | 1.085379E+00 |
| 47.300 | 9.732374E-01 | 3.122646E-02 | 1.797742E-02 | 6.749363E-02 | 3.001235E-02 | 4.113394E+01 | 8.964982E+00 | 1.085379E+00 |
| 47.650 | 9.737157E-01 | 3.124832E-02 | 1.763735E-02 | 6.749739E-02 | 2.999625E-02 | 4.103505E+01 | 9.026086E+00 | 1.085379E+00 |
| 48.000 | 9.741124E-01</td | | | | | | | |

JAERI-M 7329

** RELAP4J ANALYSIS FOR STANDARD PROBLEM NO.5 L1=4:JAERI **

MASS FLOW PER SYSTEM VOLUME

| | INTACT LOOP COLD LEG FLOW | INTACT LOOP HOT LEG FLOW | INTACT LOOP HOT LEG FLOW AT VENTURE | INTACT LOOP COLD LEG FLOW AT S.G. | SHROKEN LOOP COLD LEG FLOW OUTLET | BROKEN LOOP HOT LEG FLOW | CORE SIMULA- TOR FLOW | R.V., DOWNCO- MER FLOW AT STALK NO.1 AND NO.2 |
|-------|---------------------------------|-----------------------------|---|---|--|-----------------------------|--------------------------|--|
| TIME | JW11 | JW15 | JW2 | JW5 | JW16 | JW24 | JW14 | JW12 |
| SEC. | KG/M3 | KG/M3 | KG/M3 | KG/M3 | KG/M3 | KG/M3 | KG/M3 | KG/M3 |
| 0.0 | 2.683447E+02 | 2.683447E+02 | 2.683447E+02 | 2.683447E+02 | 0.0 | 2.683447E+02 | 2.683447E+02 | 2.683447E+02 |
| 0.070 | 4.023734E+02 | 1.613758E+02 | 1.967638E+02 | 2.441728E+02 | 7.753485E+01 | 1.967838E+02 | 2.238093E+02 | 1.463988E+02 |
| 0.140 | 2.907433E+02 | 1.243326E+02 | 1.950753E+02 | 2.034796E+02 | 5.007496E+01 | 1.950753E+02 | 1.582912E+02 | 9.464758E+01 |
| 0.210 | 2.763164E+02 | 2.550998E+01 | 2.646101E+02 | 2.525180E+02 | 9.323384E+01 | 2.646101E+02 | 1.114859E+02 | 9.738074E+01 |
| 0.280 | 2.897256E+02 | 3.628727E+01 | 1.115292E+02 | 2.908164E+02 | 1.009660E+02 | 1.113292E+02 | 1.389613E+02 | 1.395988E+02 |
| 0.350 | 2.862234E+02 | 3.554861E+01 | 1.466726E+02 | 8.897114E+01 | 9.611849E+01 | 1.466724E+02 | 1.308623E+02 | 1.280451E+02 |
| 0.420 | 4.183929E+02 | 4.162757E+01 | 1.698253E+02 | 8.181661E+02 | 1.043928E+02 | 1.698253E+02 | 1.653433E+02 | 1.436153E+02 |
| 0.490 | 2.789011E+02 | 6.661123E+01 | 1.079378E+02 | 7.7811122E+01 | 9.739996E+01 | 1.079478E+02 | 1.639119E+02 | 1.641545E+02 |
| 0.560 | 2.748596E+02 | 7.845272E+01 | 7.018693E+02 | 5.698482E+02 | 9.307223E+01 | 7.016939E+02 | 1.713650E+02 | 1.739393E+02 |
| 0.630 | 2.747419E+02 | 7.752250E+01 | 7.809214E+02 | 5.585930E+02 | 9.449558E+01 | 7.809241E+02 | 1.722527E+02 | 1.756769E+02 |
| 0.700 | 2.732713E+02 | 7.570528E+01 | 1.067697E+02 | 5.458007E+02 | 9.271288E+01 | 1.067947E+02 | 1.682467E+02 | 1.686594E+02 |
| 0.770 | 2.735480E+02 | 6.999829E+01 | 1.317004E+02 | 7.085321E+02 | 9.736816E+01 | 1.317003E+02 | 1.665687E+02 | 1.660256E+02 |
| 0.840 | 2.759686E+02 | 5.4483335E+01 | 1.395931E+02 | 6.376446E+02 | 9.583484E+01 | 1.395931E+02 | 1.601513E+02 | 1.585287E+02 |
| 0.910 | 2.762971E+02 | 6.501917E+01 | 1.329199E+02 | 5.544576E+02 | 9.392636E+01 | 1.329199E+02 | 1.583499E+02 | 1.574675E+02 |
| 0.980 | 2.755615E+02 | 6.46488492E+01 | 1.160411E+02 | 5.294095E+02 | 9.487438E+01 | 1.163611E+02 | 1.594930E+02 | 1.589194E+02 |
| 1.050 | 2.749084E+02 | 5.509453E+01 | 1.0124559E+02 | 5.698482E+02 | 9.358645E+01 | 1.0124559E+02 | 1.586490E+02 | 1.593356E+02 |
| 1.120 | 2.759556E+02 | 9.1111529E+01 | 6.578080E+02 | 9.276863E+01 | 9.1111529E+01 | 1.569811E+02 | 1.588376E+02 | 1.588376E+02 |
| 1.190 | 2.746977E+02 | 5.854497E+01 | 8.449098E+02 | 5.919085E+02 | 9.189453E+01 | 8.449098E+01 | 1.504615E+02 | 1.515243E+02 |
| 1.260 | 2.733958E+02 | 5.512126E+01 | 8.122774E+02 | 5.523067E+02 | 9.109494E+01 | 5.122724E+02 | 1.462772E+02 | 1.471864E+02 |
| 1.330 | 2.719296E+02 | 5.141660E+01 | 7.848459E+02 | 4.937040E+02 | 9.056663E+01 | 7.984896E+01 | 1.420573E+02 | 1.427684E+02 |
| 1.400 | 2.701105E+02 | 4.669674E+01 | 7.945205E+02 | 4.666107E+02 | 9.023200E+01 | 7.926520E+02 | 1.371103E+02 | 1.378907E+02 |
| 1.470 | 2.582050E+02 | 4.453387E+01 | 7.816192E+02 | 4.488763E+02 | 8.967016E+01 | 7.816192E+02 | 1.339850E+02 | 1.343388E+02 |
| 1.540 | 2.665594E+02 | 5.476785E+01 | 7.771705E+02 | 4.331360E+02 | 8.896664E+01 | 7.771705E+02 | 1.325858E+02 | 1.331903E+02 |
| 1.610 | 2.721102E+02 | 4.324299E+01 | 7.750056E+02 | 3.924256E+02 | 8.835164E+01 | 7.750056E+02 | 1.315074E+02 | 1.319035E+02 |
| 1.680 | 2.892238E+02 | 4.498122E+01 | 7.770998E+02 | 3.238782E+02 | 8.788470E+01 | 7.770998E+02 | 1.3278649E+02 | 1.330907E+02 |
| 1.750 | 3.163520E+02 | 4.071118E+01 | 7.769981E+02 | 2.6523769E+02 | 8.704428E+01 | 7.884910E+01 | 1.356115E+02 | 1.359475E+02 |
| 1.820 | 3.165280E+02 | 5.466224E+01 | 8.182021E+02 | 6.647319E+02 | 8.621202E+01 | 5.182021E+02 | 1.404504E+02 | 1.409238E+02 |
| 1.890 | 2.956556E+02 | 6.471122E+01 | 6.717523E+02 | 9.505388E+01 | 8.545601E+01 | 8.737523E+01 | 1.420126E+02 | 1.419897E+02 |
| 1.960 | 2.661798E+02 | 7.8606938E+01 | 9.510565E+01 | 1.021866E+02 | 2.108514E+02 | 8.197295E+01 | 1.021866E+02 | 1.532836E+02 |
| 2.030 | 2.849084E+02 | 7.570484E+01 | 1.021866E+02 | 9.493976E+01 | 9.232494E+02 | 9.493976E+01 | 9.649330E+01 | 1.368123E+02 |
| 2.100 | 2.824727E+02 | 5.493959E+01 | 1.021866E+02 | 9.493959E+01 | 8.745689E+01 | 8.745689E+01 | 1.433737E+02 | 8.969394E+01 |
| 2.170 | 2.008617E+02 | 1.7651567E+01 | 7.194802E+02 | 9.860539E+01 | 8.497402E+01 | 7.194802E+02 | 1.404085E+01 | 1.404085E+01 |
| 2.240 | 1.990227E+02 | -5.847371E+01 | 7.194802E+02 | 9.860539E+01 | 8.497402E+01 | 7.194802E+02 | 1.404085E+01 | 1.404085E+01 |
| 2.310 | 1.496176E+02 | -4.610597E+01 | 4.5458319E+01 | 1.149516E+01 | 8.994594E+01 | 4.5458319E+01 | 1.538724E+01 | 1.538724E+01 |
| 2.380 | 8.775276E+01 | -5.325118E+01 | 9.376192E+01 | 2.8232055E+01 | 1.196506E+01 | 9.376192E+01 | 3.149067E+01 | 3.149067E+01 |
| 3.000 | 1.140639E+02 | -1.948719E+01 | 1.539154E+01 | 7.141722E+01 | 2.965755E+01 | 1.539154E+01 | 7.832795E+01 | 7.832795E+01 |
| 4.250 | 1.237505E+02 | -5.307245E+01 | 2.612986E+01 | 9.503688E+01 | 4.716137E+01 | 2.612986E+01 | -5.169028E+01 | -5.233121E+00 |
| 4.600 | 1.101916E+02 | -6.020789E+01 | 1.582380E+01 | 3.158822E+01 | 1.038936E+02 | 4.552357E+01 | -6.6076743E+01 | -6.6076743E+01 |
| 4.950 | 5.730867E+01 | -2.152422E+01 | 1.197785E+01 | 4.706145E+01 | 1.014291E+01 | 1.197785E+01 | 4.056896E+01 | 4.056896E+01 |
| 5.300 | 1.041735E+02 | -4.387305E+01 | 6.160170E+01 | 6.748322E+01 | 6.041271E+01 | 6.160170E+01 | -3.372734E+01 | -3.793432E+01 |
| 5.650 | 1.244565E+02 | -4.924423E+01 | 7.753000E+01 | 2.575907E+01 | 7.249197E+01 | 7.753000E+01 | -5.247072E+01 | -9.914674E+01 |
| 6.000 | 6.990227E+02 | -1.761567E+01 | 1.1635519E+01 | 7.194802E+01 | 6.079350E+01 | 7.194802E+01 | -6.572171E+01 | -6.185791E+01 |
| 6.350 | 8.775276E+01 | -5.325118E+01 | 9.376192E+01 | 2.8232055E+01 | 1.196506E+01 | 9.376192E+01 | 3.149067E+01 | 3.149067E+01 |
| 6.700 | 6.032713E+01 | -2.743735E+01 | 9.456839E+00 | 2.369935E+01 | 5.662216E+00 | 9.456839E+00 | -6.159639E+00 | -6.919417E+00 |
| 7.050 | 1.116511E+02 | -1.221622E+01 | 1.595674E+01 | 2.658083E+01 | 3.800445E+01 | 1.595674E+01 | -1.089753E+01 | -7.510681E+01 |
| 7.400 | 7.132543E+01 | -1.751091E+01 | 1.395455E+01 | 2.015175E+01 | 3.795931E+01 | 1.395455E+01 | -1.061333E+01 | -1.529592E+01 |
| 7.750 | 6.931026E+01 | -1.916333E+01 | 1.147891E+01 | 2.392595E+01 | 5.8213638E+01 | 1.147891E+01 | 1.036883E+01 | 9.205721E+01 |
| 8.100 | 6.737592E+01 | -1.844922E+01 | 1.182861E+01 | 3.732593E+01 | 6.002068E+01 | 1.182861E+01 | 1.786213E+01 | 5.768203E+01 |
| 8.450 | 4.849588E+01 | -1.766789E+01 | 3.702411E+01 | 3.702411E+01 | 7.040580E+00 | 1.132801E+01 | -2.309291E+01 | -4.652040E+01 |

** RELAP4J ANALYSIS FOR STANDARD PROBLEM NO.5 L1=4:JAERI **

MASS FLOW PER SYSTEM VOLUME

| | INTACT LOOP COLD LEG FLOW | INTACT LOOP HOT LEG FLOW | INTACT LOOP HOT LEG FLOW AT VENTURE | INTACT LOOP COLD LEG FLOW AT S.G. | BROKEN LOOP COLD LEG FLOW OUTLET | BROKEN LOOP HOT LEG FLOW | CORE SIMULA- TOR FLOW | R.V., DOWNCO- MER FLOW AT STALK NO.1 AND NO.2 |
|--------|---------------------------------|-----------------------------|---|---|---|-----------------------------|--------------------------|--|
| TIME | JW11 | JW15 | JW2 | JW5 | JW16 | JW24 | JW14 | JW12 |
| SEC. | KG/M3 | KG/M3 | KG/M3 | KG/M3 | KG/M3 | KG/M3 | KG/M3 | KG/M3 |
| 8.800 | 5.059806E+01 | -1.817721E+01 | 1.26265506E+01 | 3.6655788E+01 | 7.7225585E+01 | 1.26265506E+01 | -1.258151E+01 | -4.473332E+01 |
| 9.150 | 4.499377E+01 | -1.900493E+01 | 5.554901E+01 | 2.3824975E+01 | 6.417377E+01 | 9.554901E+01 | -1.443802E+01 | -4.502688E+01 |
| 9.500 | 5.361735E+01 | -1.615662E+01 | 1.128162E+01 | 2.441269E+01 | 8.968045E+00 | 1.128162E+01 | -3.772407E+00 | -4.232758E+01 |
| 9.850 | 3.336158E+01 | -1.937770E+01 | 7.969870E+01 | 2.143432E+01 | 9.740798E+00 | 7.969870E+01 | -1.440443E+01 | -2.180178E+01 |
| 10.200 | 4.999867E+01 | -2.135133E+01 | 5.7984595E+01 | 2.292191E+01 | 1.258555E+01 | 5.7984595E+01 | -5.355735E+01 | -8.524385E+01 |
| 10.550 | 5.413314E+01 | -1.6387380E+01 | 9.148777E+01 | 1.844777E+01 | 6.184777E+01 | 9.144777E+01 | -1.581807E+01 | -5.355498E+01 |
| 10.900 | 4.870813E+01 | -2.554050E+01 | 2.311939E+01 | 2.601084E+01 | 6.079587E+01 | 2.311939E+01 | -5.72171E+01 | -6.185791E+01 |
| 11.250 | 2.606279E+01 | -1.844989E+01 | 8.688155E+01 | 1.576291E+01 | 6.255140E+01 | 4.763394E+01 | -2.106100E+01 | -6.532461E+01 |
| 11.600 | 4.291808E+01 | -1.827273E+01 | 4.763394E+01 | 1.576291E+01 | 6.255140E+01 | 4.763394E+01 | -2.150452E+01 | -6.650428E+01 |
| 11.950 | 5.171658E+01 | -2.028252E+01 | 9.227257E+01 | 1.810666E+01 | 5.888155E+01 | 9.227257E+01 | -3.631636E+01 | -6.903717E+01 |
| 12.300 | 2.910831E+01 | -1.593538E+01 | 1.372367E+01 | 1.319883E+01 | 5.688452E+01 | 3.172666E+01 | -5.647488E+01 | -6.007488E+01 |
| 12.650 | 6.216288E+01 | -1.159678E+01 | 1.682444E+01 | 1.551536E+01 | 5.809351E+01 | 1.682444E+01 | -1.701342E+01 | -3.397556E+ |

** RELAP4J ANALYSIS FOR STANDARD PROBLEM NO.5 L1-4:JAERI **

MASS FLOW PER SYSTEM VOLUME

| | INTACT LOOP COLD LEG FLOW | INTACT LOOP HOT LEG FLOW | INTACT LOOP HOT LEG FLOW AT VENTURE | INTACT LOOP COLD LEG FLOW AT S.G. | BROKEN LOOP COLD LEG FLOW | BROKEN LOOP HOT LEG FLOW | CORE SIMULA- TOR FLOW | R.V. DOWNCO- MER FLOW AT STALK NO.1 AND NO.2 |
|--------|---------------------------------|-----------------------------|---|---|---------------------------------|-----------------------------|--------------------------|---|
| TIME | JW11 | JW15 | JX2 | JW5 | JW16 | JW24 | JW14 | JW12 |
| SEC. | KG/M3 | KG/M3 | KG/M3 | KG/M3 | KG/M3 | KG/M3 | KG/M3 | KG/M3 |
| 25.800 | 2.391952E+01 | -2.668004E+01 | -3.021475E+01 | 1.083571E+00 | 6.497657E+00 | -3.021475E+01 | 1.797428E+01 | -2.085236E+01 |
| 25.950 | 2.732318E+01 | -3.353939E+01 | -3.102111E+01 | 2.394636E+00 | 2.542062E+00 | -3.102113E+01 | 1.280462E+01 | -2.332835E+01 |
| 26.300 | 3.186824E+01 | -3.991156E+01 | -3.009233E+01 | 3.304120E+00 | 2.876075E+00 | -3.600233E+01 | 1.182595E+01 | -2.613817E+01 |
| 26.650 | 3.519777E+01 | -3.446003E+01 | -3.215761E+01 | 4.688957E+00 | 1.445728E+01 | -3.215761E+01 | 8.733454E+01 | -2.517458E+01 |
| 27.000 | 3.211018E+01 | -2.411773E+01 | -2.023957E+01 | 3.490521E+00 | 3.041781E+01 | -2.023957E+01 | 4.418477E+01 | -1.802191E+01 |
| 27.350 | 3.200974E+01 | -2.124259E+01 | -1.354546E+01 | 2.947379E+00 | 2.771694E+01 | -1.354546E+01 | 1.435051E+01 | -2.384536E+01 |
| 27.700 | 3.288639E+01 | -2.790908E+01 | -8.833768E+00 | 9.977473E+00 | 1.554323E+01 | -8.830768E+00 | 1.228456E+01 | -2.181394E+01 |
| 28.050 | 3.430233E+01 | -1.896235E+01 | -1.041252E+01 | 2.395302E+00 | 1.675406E+01 | -8.104125E+00 | 1.298896E+01 | -2.347718E+01 |
| 28.400 | 3.568232E+01 | -1.604684E+01 | -8.893125E+00 | 3.691121E+00 | 2.566741E+01 | -6.839135E+00 | 1.701646E+01 | -2.287268E+01 |
| 28.750 | 3.643001E+01 | -1.745908E+01 | -5.473325E+00 | 3.806057E+00 | 1.406498E+01 | -5.473325E+00 | 8.844429E+00 | -2.235537E+01 |
| 29.100 | 3.709238E+01 | -1.443951E+01 | -2.141671E+01 | 3.808260E+00 | 5.527252E+00 | -2.141671E+01 | 1.442326E+00 | -7.059577E+01 |
| 29.450 | 3.749254E+01 | -6.219887E+00 | -1.791754E+00 | 3.734063E+00 | 2.266763E+01 | -1.791754E+00 | 2.460508E+01 | -1.859814E+01 |
| 29.800 | 3.803518E+01 | -9.393536E+00 | -1.093404E+00 | 3.708253E+00 | 8.074691E+00 | -1.093404E+00 | 4.413377E+00 | -1.651966E+01 |
| 30.150 | 3.863172E+01 | -7.722341E+00 | -2.776296E+03 | 3.724454E+00 | 6.188636E+00 | -2.784296E+03 | 5.850255E+00 | -1.555965E+01 |
| 30.500 | 3.918555E+01 | -5.535091E+00 | -5.859037E+01 | 3.745817E+00 | 1.292561E+01 | -5.859037E+01 | 3.202159E+01 | -1.493894E+01 |
| 30.850 | 3.952139E+01 | -4.583125E+00 | -1.002551E+02 | 3.719289E+00 | 7.038175E+00 | -1.002551E+02 | 4.591101E+01 | -1.377071E+01 |
| 31.200 | 3.991262E+01 | -2.984749E+00 | -1.020170E+01 | 3.678824E+00 | 7.201563E+00 | -1.020170E+01 | 4.501121E+01 | -1.289694E+01 |
| 31.550 | 4.018611E+01 | -3.271118E+01 | -5.034464E+01 | 3.641784E+00 | 8.293950E+00 | -5.034464E+01 | 5.683097E+00 | -1.261609E+01 |
| 31.900 | 4.064881E+01 | -2.793546E+00 | -4.832175E+01 | 3.534419E+00 | 7.385829E+00 | -4.832175E+01 | 4.568135E+00 | -1.032433E+01 |
| 32.250 | 4.076256E+01 | -2.391046E+00 | -2.882065E+00 | 3.486201E+00 | 7.658260E+00 | -2.882065E+00 | 2.821518E+01 | -5.124001E+00 |
| 32.600 | 4.096631E+01 | -2.017448E+01 | -3.049754E+01 | 3.432567E+00 | 8.932622E+00 | -3.049754E+01 | 5.461165E+00 | -8.943972E+00 |
| 32.950 | 4.122435E+01 | -1.907927E+00 | -3.367335E+01 | 3.393647E+00 | 1.068194E+01 | -3.367335E+01 | 4.942171E+00 | -8.031448E+00 |
| 33.300 | 4.156802E+01 | -1.416735E+01 | -3.820351E+01 | 3.383715E+00 | 1.237709E+01 | -3.820351E+01 | 5.664166E+00 | -7.241384E+00 |
| 33.650 | 4.192550E+01 | -1.167961E+01 | -4.576715E+01 | 3.389772E+00 | 1.369618E+01 | -4.576715E+01 | 5.780633E+00 | -6.551433E+00 |
| 34.000 | 4.225218E+01 | -1.056642E+01 | -5.332292E+01 | 3.408423E+00 | 1.466710E+01 | -5.332292E+01 | 5.970075E+00 | -5.739666E+00 |
| 34.350 | 4.252172E+01 | -6.795765E+01 | -6.244171E+00 | 4.491107E+01 | 1.530706E+01 | -6.244171E+00 | 6.121026E+00 | -5.019974E+00 |
| 34.700 | 4.283311E+01 | -4.620694E+01 | -7.269754E+01 | 3.472894E+01 | 5.134309E+01 | -7.269754E+01 | 6.197645E+00 | -4.347010E+00 |
| 35.050 | 4.284690E+01 | -7.794738E+01 | -4.735108E+01 | 4.040083E+01 | 9.402526E+01 | -4.735108E+01 | 5.137938E+00 | -4.047882E+00 |
| 35.400 | 4.322474E+01 | -6.465355E+01 | -5.263232E+01 | 5.302272E+00 | 9.045840E+01 | -5.263232E+01 | 4.748588E+00 | -4.690128E+00 |
| 35.750 | 4.335940E+01 | -5.711351E+01 | -5.456436E+01 | 6.650944E+00 | 9.494078E+01 | -5.456436E+01 | 4.3991159E+00 | -4.412999E+00 |
| 36.100 | 4.449211E+01 | -6.173705E+01 | -9.193536E+01 | 7.960025E+00 | 8.309469E+01 | -9.193536E+01 | 3.085961E+00 | -5.942095E+00 |
| 36.450 | 4.793135E+01 | -6.763700E+01 | -9.413563E+01 | 8.593752E+00 | 5.425821E+01 | -9.413563E+01 | 3.0367115E+00 | -5.580503E+00 |
| 36.800 | 4.854490E+01 | -5.235529E+01 | -9.463206E+01 | 9.423137E+00 | 4.893712E+01 | -9.463206E+01 | 2.914714E+00 | -5.292343E+00 |
| 37.150 | 5.144606E+01 | -3.397471E+01 | -5.475178E+01 | 1.035634E+01 | 5.288912E+01 | -5.475178E+01 | 2.862619E+00 | -5.095458E+00 |
| 37.500 | 5.252498E+01 | -5.365939E+01 | -4.461716E+01 | 1.167722E+01 | 5.234737E+01 | -4.461716E+01 | 2.183629E+00 | -5.263435E+00 |
| 37.850 | 5.399230E+01 | -4.735108E+01 | -5.421693E+01 | 1.058181E+01 | 4.938908E+01 | -5.421693E+01 | 2.464687E+00 | -4.820541E+00 |
| 38.200 | 5.517535E+01 | -4.228131E+01 | -4.859486E+01 | 1.084508E+01 | 6.829156E+01 | -4.859486E+01 | 2.878559E+00 | -3.893183E+00 |
| 38.550 | 5.554948E+01 | -4.637114E+01 | -4.351377E+01 | 1.055748E+01 | 6.666847E+01 | -4.351377E+01 | 2.571111E+00 | -3.826144E+00 |
| 38.900 | 5.638238E+01 | -4.575566E+01 | -4.162206E+01 | 1.064723E+01 | 7.247744E+01 | -4.162206E+01 | 2.484899E+00 | -3.666099E+00 |
| 39.250 | 5.726494E+01 | -3.814773E+01 | -4.667072E+01 | 1.091623E+01 | 8.163774E+01 | -4.667072E+01 | 2.679333E+00 | -3.182055E+00 |
| 39.600 | 5.820727E+01 | -3.362692E+01 | -4.888803E+01 | 1.090422E+01 | 9.249666E+01 | -4.888803E+01 | 2.805323E+00 | -2.708059E+00 |
| 39.950 | 5.890721E+01 | -2.524114E+01 | -5.376424E+01 | 1.100747E+01 | 9.290375E+01 | -5.376424E+01 | 2.857616E+00 | -2.389688E+00 |
| 40.300 | 5.959946E+01 | -1.701235E+01 | -5.195271E+01 | 1.126441E+01 | 9.606035E+01 | -5.195271E+01 | 2.943639E+00 | -2.031310E+00 |
| 40.650 | 6.051890E+01 | -8.523625E+02 | -6.559307E+01 | 1.154121E+01 | 9.767215E+01 | -6.559307E+01 | 3.034103E+00 | -1.690499E+00 |
| 41.000 | 6.055209E+01 | -1.470713E+01 | -7.502649E+01 | 1.162553E+01 | 7.502649E+01 | -7.502649E+01 | 3.10761RE+01 | -1.902135E+00 |
| 41.350 | 6.132597E+01 | -6.802127E+01 | -1.204750E+01 | 1.162534E+01 | 7.623239E+01 | -1.204750E+01 | 3.232488E+00 | -8.456188E+01 |
| 41.700 | 6.175808E+01 | -1.695754E+01 | -4.615577E+01 | 1.229553E+01 | 9.445169E+01 | -4.615577E+01 | 3.442556E+00 | -6.167087E+01 |
| 42.050 | 6.224291E+01 | -2.180443E+00 | -1.170957E+01 | 1.258034E+01 | 9.044562E+00 | -1.170957E+01 | 3.523083E+00 | -3.023549E+01 |

** RELAP4J ANALYSIS FOR STANDARD PROBLEM NO.5 L1-4:JAERI **

| | INTACT LOOP COLD LEG FLOW | INTACT LOOP HOT LEG FLOW | INTACT LOOP HOT LEG FLOW AT VENTURE | INTACT LOOP COLD LEG FLOW AT S.G. | BROKEN LOOP COLD LEG FLOW | BROKEN LOOP HOT LEG FLOW | CORE SIMULA- TOR FLOW | R.V. DOWNCO- MER FLOW AT STALK NO.1 AND NO.2 |
|--------|---------------------------------|-----------------------------|---|---|---------------------------------|-----------------------------|--------------------------|---|
| TIME | JW11 | JW15 | JX2 | JW5 | JW16 | JW24 | JW14 | JW12 |
| SEC. | KG/M3 | KG/M3 | KG/M3 | KG/M3 | KG/M3 | KG/M3 | KG/M3 | KG/M3 |
| 42.400 | 6.272922E+01 | 1.374935E+00 | 1.283234E+01 | 8.709595E+00 | 1.574935E+00 | 3.636796E+00 | -2.933411E+02 | |
| 42.750 | 6.297994E+01 | 3.706000E+01 | 2.199642E+01 | 1.302346E+01 | 8.093408E+00 | 2.190682E+00 | 6.383242E+00 | 4.253471E+00 |
| 43.100 | 6.329230E+01 | 3.493243E+00 | 2.635293E+00 | 1.288922E+00 | 7.314159E+00 | 2.635293E+00 | 3.670382E+00 | 2.165436E+01 |
| 43.450 | 6.355162E+01 | 4.089262E+01 | 3.271821E+00 | 1.291644E+01 | 7.229473E+00 | 3.271821E+00 | 3.936067E+00 | 3.578920E+01 |
| 43.800 | 6.390623E+01 | 4.895827E+00 | 4.284264E+00 | 1.305316E+01 | 7.124661E+00 | 4.284264E+00 | 4.388667E+00 | 3.243946E+01 |
| 44.150 | 6.423370E+01 | 5.355121E+00 | 4.850503E+00 | 1.318355E+01 | 7.167865E+00 | 4.850503E+00 | 4.898075E+00 | 1.841376E+01 |
| 44.500 | 6.437062E+01 | 5.318133E+00 | 5.419749E+00 | 1.319510E+01 | 6.287433E+00 | 5.419749E+00 | 5.332116E+00 | 7.472293E+00 |
| 44.850 | 6.437301E+01 | 5.125355E+00 | 5.701777E+00 | 1.304261E+01 | 5.383241E+00 | 5.701777E+00 | 5.714960E+00 | 1.396494E+01 |
| 45.200 | 6.418178E+01 | 5.283353E+00 | 5.853335E+00 | 1.281121E+01 | 5.590428E+00 | 5.853335E+00 | 6.278550E+00 | 3.522040E+01 |
| 45.550 | 6.412554E+01 | 5.613533E+00 | 6.161916E+00 | 1.265431E+01 | 5.613943E+00 | 6.161916E+00 | 7.187296E+00 | 5.068231E+01 |
| 45.900 | 6.419713E+01 | 6.162364E+00 | 6.462339E+00 | 1.256456E+01 | 5.696736E+00 | 6.462339E+00 | 8.766707E+00 | 4.525423E+01 |
| 46.250 | 6.436310E+01 | 7.117739E+00 | 7.278376E+00 | 1.275901E+01 | 5.767824E+00 | 7.278376E+00 | 1.043512E+01 | 2.248466E+01 |
| 46.600 | 6.437911E+01 | 7.705207E+00 | 7.767288E+00 | 1.284008E+01 | 5.707135E+01 | 7.767288E+00 | 1.203508E+01 | 3.825786E+00 |
| 46.950 | 6.427619E+01 | 6.400334E+01 | 7.247363E+00 | 1.259914E+01 | 5.306 | | | |

JAERI-M 7329

** RELAP4J ANALYSIS FOR STANDARD PROBLEM NO.5 L1-4:JAERI **

DIFFERENTIAL PRESSURE

| (PDE-PC-1) | (PDE-PC-2) | (PDE-P139-30) | (PDE-RL-1) | (PDE-RL-2) | (PDF-BL-3) | (PDE-BL-4) | (PDE-BL-5) | (PDE-BL-7) | |
|------------|---------------|---------------|---------------|---------------|---------------|---------------|--------------|--------------|---------------|
| TIME | AP9-AP6 | AP3-AP6 | AP10-AP1 | AP15-AP16 | AP21-AP27 | AP27-AP26 | AP20-AP26 | AP19-AP20 | AP16-AP19 |
| SEC | MPA | MPA | MPA | MPA | MPA | MPA | MPA | MPA | MPA |
| 0.0 | 1.647114E-01 | 8.752425E-02 | 6.202534E+02 | 1.033743E-02 | 1.429636E-01 | 1.532426E+01 | 1.565520E+01 | 2.136423E-02 | -3.170278E-02 |
| 0.070 | -1.502462E-01 | 4.834510E-01 | -6.152024E-01 | -6.197166E-01 | 3.883638E+00 | 6.012739E+00 | 5.171487E+00 | 5.161226E+00 | 2.698510E-01 |
| 0.140 | 1.430128E-01 | 3.565540E-01 | -2.141946E-01 | 6.077026E-01 | 6.555747E-01 | 5.841493E+00 | 4.569742E+00 | 1.732049E+00 | 1.568793E-01 |
| 0.210 | 1.190798E-01 | 1.615861E-01 | -1.445501E-02 | 2.161242E-01 | 7.988290E-01 | 5.231657E+00 | 3.440903E+00 | 2.175118E+00 | 2.813122E-01 |
| 0.280 | 1.161464E-01 | 9.711864E-02 | -5.767897E-02 | 1.549218E-01 | 7.977525E-01 | 5.237588E+00 | 3.440101E+00 | 2.411153E+00 | 3.062079E-01 |
| 0.350 | 1.103888E-01 | 9.771575E-02 | -6.696222E-02 | 1.0991102E-01 | 7.991102E-01 | 5.236372E+00 | 3.174723E+00 | 2.450150E+00 | 3.017619E-01 |
| 0.420 | 1.150286E-01 | 6.417670E-02 | 1.010126E-02 | 1.481122E-01 | 8.030303E-01 | 5.227517E+00 | 3.171119E+00 | 2.458729E+00 | 2.754769E-01 |
| 0.490 | 1.163586E-01 | 6.455942E-02 | -2.456092E-01 | 8.000161E-01 | 8.077575E+00 | 5.2463952E+00 | 2.447955E+00 | 2.839766E-01 | |
| 0.560 | 1.154182E-01 | 7.472760E-02 | 1.479595E-02 | 1.408030E-01 | 8.055259E-01 | 5.242075E+00 | 3.173923E+00 | 2.472823E+00 | 2.642815E-01 |
| 0.630 | 1.132938E-01 | 6.1664133E-02 | 6.170570E-02 | 9.705708E-01 | 8.066225E-01 | 5.249694E+00 | 3.173335E+00 | 2.475509E+00 | 2.817158E-01 |
| 0.700 | 1.141685E-01 | 9.208045E-02 | 7.4242493E-02 | 1.015573E-01 | 8.032593E-01 | 5.242534E+00 | 3.171597E+00 | 2.478800E+00 | 2.673551E-01 |
| 0.770 | 1.074723E-01 | 8.5115194E-02 | 5.4471535E-02 | 1.366506E-01 | 8.085831E-01 | 5.247076E+00 | 3.166551E+00 | 2.480822E+00 | 2.754612E-01 |
| 0.840 | 1.001399E-01 | 6.4604670E-02 | 2.4771535E-02 | 1.076248E-01 | 8.086585E-01 | 5.242905E+00 | 3.160485E+00 | 2.485065E+00 | 2.932526E-01 |
| 0.910 | 9.636467E-02 | 5.803755E-02 | 2.940446E-01 | 1.473767E-01 | 8.097446E-01 | 5.242086E+00 | 3.164688E+00 | 2.486887E+00 | 2.512750E-01 |
| 0.980 | 9.384271E-02 | 5.139643E-02 | -9.464342E-02 | 1.463473E-01 | 8.103030E-01 | 5.241685E+00 | 3.150785E+00 | 2.488509E+00 | 2.628861E-01 |
| 1.050 | 9.122815E-02 | 4.825544E-02 | -8.302404E-02 | 1.663627E-01 | 8.117476E-01 | 5.242075E+00 | 3.144651E+00 | 2.492007E+00 | 2.608793E-01 |
| 1.120 | 8.394693E-02 | 4.781614E-02 | -3.614108E-02 | 1.359488E-01 | 8.193939E-01 | 5.245355E+00 | 3.140814E+00 | 2.494972E+00 | 2.613367E-01 |
| 1.190 | 8.359446E-02 | 5.244499E-02 | 2.130516E-02 | 1.347207E-01 | 8.215100E-01 | 5.198471E-00 | 3.139123E+00 | 2.497208E+00 | 2.595754E-01 |
| 1.260 | 8.274208E-02 | 5.393619E-02 | 6.1946497E-02 | 1.2954495E-01 | 8.216670E-01 | 5.191146E-00 | 3.138054E+00 | 2.496819E+00 | 2.582722E-01 |
| 1.330 | 8.272974E-02 | 5.645042E-02 | 8.9470114E-02 | 1.2742959E-01 | 8.222959E-01 | 5.192209E-00 | 3.136986E+00 | 2.500228E+00 | 2.558875E-01 |
| 1.400 | 8.252983E-02 | 5.901327E-02 | 8.223553E-02 | 1.2644940E-01 | 8.224239E-01 | 5.192496E-00 | 3.135824E+00 | 2.501543E+00 | 2.554754E-01 |
| 1.470 | 8.340210E-02 | 5.715953E-02 | 1.0748446E-01 | 8.230623E-01 | 8.224148E-01 | 5.188116E-00 | 3.136595E+00 | 2.502813E+00 | 2.525071E-01 |
| 1.540 | 8.471269E-02 | 6.775132E-02 | 1.138288E-02 | 1.212519E-01 | 8.215159E-01 | 5.190581E-00 | 3.133297E+00 | 2.504003E+00 | 2.508436E-01 |
| 1.610 | 9.541031E-02 | 6.455971E-02 | 1.9119427E-02 | 1.191104E-01 | 8.195785E-01 | 5.187777E+00 | 3.131868E+00 | 2.505148E+00 | 2.490393E-01 |
| 1.680 | 1.1646428E-02 | 6.120314E-02 | 2.740586E-02 | 1.179576E-01 | 8.175250E-01 | 5.182334E+00 | 3.130215E+00 | 2.506267E+00 | 2.481453E-01 |
| 1.750 | 1.465020E-02 | 7.458741E-02 | 3.616525E-02 | 1.145900E-01 | 8.124651E-01 | 5.172784E-00 | 3.127282E+00 | 2.507493E+00 | 2.502929E-01 |
| 1.820 | 3.811097E-02 | 6.208425E-02 | 6.064393E-02 | 1.126669E-01 | 8.106709E-01 | 5.158515E-00 | 3.127408E+00 | 2.508772E+00 | 2.519085E-01 |
| 1.890 | 4.035588E-02 | 1.492297E-02 | 1.454021E-02 | 1.095362E-01 | 8.017823E-01 | 5.126465E-00 | 3.109956E+00 | 2.525261E+00 | 2.515127E-01 |
| 1.960 | 8.259959E-02 | 5.351147E-02 | 1.319133E-02 | 1.051313E-01 | 8.007141E-01 | 5.119464E-00 | 3.109227E+00 | 2.511227E+00 | 2.518177E-01 |
| 2.150 | 8.305008E-02 | 6.179207E-02 | 1.142274E-02 | 1.024739E-01 | 8.007464E-01 | 5.175439E-00 | 3.107931E+00 | 2.514068E+00 | 2.492603E-01 |
| 2.500 | 5.307749E-02 | 1.215542E-02 | 1.138288E-02 | 1.212519E-01 | 8.007140E-01 | 5.170779E-00 | 3.112485E+00 | 2.524531E+00 | 2.421887E-01 |
| 2.850 | 4.600339E-02 | 1.165515E-02 | -8.905157E-02 | 8.006774E-01 | 8.066144E-01 | 5.170779E+00 | 3.113016E+00 | 2.524892E+00 | 2.328811E-01 |
| 3.200 | 7.646910E-02 | 5.593374E-02 | 7.117178E-02 | 8.711642E-01 | 8.052987E-01 | 5.169576E+00 | 3.103168E+00 | 2.519899E+00 | 2.319368E-01 |
| 3.550 | 2.264071E-02 | 5.711842E-02 | 1.146252E-02 | 9.964155E-02 | 8.266720E-01 | 5.127187E-00 | 3.091395E+00 | 2.534910E+00 | 2.319368E-01 |
| 3.900 | 3.697543E-02 | 5.711941E-02 | -1.948171E-02 | 8.303274E-02 | 8.229145E-01 | 5.166998E+00 | 3.077671E+00 | 2.535977E+00 | 2.164898E-01 |
| 4.250 | -2.123269E-02 | 3.117177E-02 | 4.6470728E-02 | 3.1424242E-02 | 8.243080E-01 | 5.130469E+00 | 3.076206E+00 | 2.534432E+00 | 2.892526E-01 |
| 4.600 | 4.348724E-02 | 4.607506E-02 | 2.477157E-02 | 5.642478E-02 | 8.247605E-01 | 5.130469E+00 | 3.076206E+00 | 2.534432E+00 | 2.892526E-01 |
| 4.950 | 1.614439E-02 | 2.950481E-02 | -1.034945E-02 | 8.007763E-02 | 8.276536E-01 | 5.105839E+00 | 3.029305E+00 | 2.555234E+00 | 2.349804E-01 |
| 5.300 | 3.031620E-02 | 3.617424E-02 | -5.853592E-02 | 9.085367E-02 | 8.222735E-01 | 5.125511E+00 | 3.021220E+00 | 2.555743E+00 | 2.462379E-01 |
| 5.650 | 2.416163E-02 | 3.157148E-02 | 1.212737E-02 | 8.235677E-02 | 8.674974E-01 | 4.863329E+00 | 2.994972E+00 | 2.558795E-01 | |
| 6.000 | 5.514797E-02 | 3.117721E-02 | 1.655175E-02 | 8.361023E-02 | 8.769540E-01 | 5.050744E+00 | 2.912280E+00 | 2.246305E-01 | |
| 6.350 | 3.834190E-02 | 2.221209E-02 | 1.746536E-02 | 6.390553E-02 | 8.5945647E-01 | 4.948990E+00 | 2.959574E+00 | 2.564012E+00 | 2.257392E-01 |
| 6.700 | 1.388417E-02 | 1.155564E-02 | 9.316371E-02 | 6.747181E-02 | 8.466329E-01 | 4.954064E+00 | 2.956954E+00 | 2.566954E+00 | 2.287901E-01 |
| 7.050 | 7.179127E-03 | 1.572932E-02 | 1.393553E-02 | 5.782726E-02 | 8.362974E-01 | 4.892808E-01 | 2.926079E-00 | 2.570762E+00 | 2.305211E-01 |
| 7.400 | 1.935876E-02 | 1.256613E-02 | 1.533259E-02 | 4.094484E-02 | 8.293631E-01 | 4.922625E+00 | 2.910476E+00 | 2.576322E+00 | 2.221197E-01 |
| 7.750 | 1.584004E-02 | 2.853925E-02 | -1.775715E-02 | 3.394124E-02 | 8.297616E-01 | 4.865903E+00 | 2.895489E+00 | 2.584127E+00 | 2.127859E-01 |
| 8.100 | 9.965675E-03 | 1.708069E-02 | 3.422722E-02 | 3.363955E-02 | 8.183970E-01 | 4.887037E+00 | 2.877930E+00 | 2.594115E+00 | 2.109656E-01 |
| 8.450 | 6.937916E-03 | 2.277116E-02 | -1.987167E-02 | 2.472774E-02 | 8.184314E-01 | 4.858764E+00 | 2.866818E+00 | 2.606818E+00 | 1.954319E-01 |

** RELAP4J ANALYSIS FOR STANDARD PROBLEM NO.5 L1-4:JAERI **

DIFFERENTIAL PRESSURE

| (PDE-PC-1) | (PDE-PC-2) | (PDE-P139-30) | (PDE-RL-1) | (PDE-RL-2) | (PDF-BL-3) | (PDE-BL-4) | (PDE-BL-5) | (PDE-BL-7) | |
|------------|---------------|---------------|-----------------|---------------|--------------|--------------|--------------|--------------|--------------|
| TIME | AP9-AP6 | AP3-AP6 | AP10-AP1 | AP15-AP16 | AP21-AP27 | AP27-AP26 | AP20-AP26 | AP19-AP20 | AP16-AP19 |
| SEC | MPA | MPA | MPA | MPA | MPA | MPA | MPA | MPA | MPA |
| 8.800 | -5.754244E-03 | -2.632397E-03 | -1.690413E-03 | -2.710314E-02 | 8.138539E-01 | 4.829830E+00 | 2.829837E+00 | 2.612604E+00 | 1.965541E-01 |
| 9.150 | 1.962409E-02 | 2.197494E-02 | -4.363038E-02 | 2.605164E-02 | 8.198666E-01 | 4.830034E+00 | 2.796861E+00 | 2.638371E+00 | 1.895389E-01 |
| 9.500 | 2.288650E-02 | 7.902237E-02 | -9.375784E-02 | 2.361633E-02 | 8.377396E-01 | 4.795184E+00 | 2.785951E+00 | 2.656109E+00 | 1.968966E-01 |
| 9.850 | 1.355480E-02 | 1.464742E-02 | 2.156751E-02 | 2.804840E-02 | 8.360422E-01 | 4.716349E+00 | 2.769933E+00 | 2.690395E+00 | 1.926038E-01 |
| 10.200 | 1.535450E-02 | 1.534685E-02 | 6.462400E-02 | 2.804840E-02 | 8.307510E-01 | 4.637619E-00 | 4.794455E+00 | 2.707480E+00 | 1.939555E-01 |
| 10.550 | 1.925128E-02 | 1.074744E-02 | 1.797474E-02 | 3.097510E-02 | 8.307510E-01 | 4.637619E-00 | 4.744749E+00 | 2.656705E+00 | 2.166857E-01 |
| 10.900 | -6.279145E-03 | -1.374955E-02 | -1.65645751E-02 | 3.078798E-02 | 8.307715E-01 | 4.637715E-00 | 4.717715E+00 | 2.621090E+00 | 2.120510E-01 |
| 11.250 | -9.259712E-02 | 3.025164E-02 | 1.207127 | | | | | | |

JAERI-M-7329

** RELAP4J ANALYSIS FOR STANDARD PROBLEM NO.5 L1-4:JAERI **

DIFFERENTIAL PRESSURE

| (PDE-PC-1) | (PDE-PC-2) | (PDE-P139-30) | (PDE-BL-1) | (PDE-BL-2) | (PDF-BL-3) | (PDE-BL-4) | (PDE-BL-5) | (PDE-BL-7) | |
|------------|----------------|---------------|----------------|---------------|---------------|---------------|---------------|---------------|--------------|
| TIME | AP9-AP6 | AP3-AP6 | AP10-AP1 | AP15-AP16 | AP21-AP27 | AP27-AP26 | AP20-AP26 | AP19-AP20 | AP16-AP19 |
| SEC | MPA | MPA | MPA | MPA | MPA | MPA | MPA | MPA | MPA |
| 25.600 | 3.986727E-03 | 7.594940E-03 | -3.827284E-03 | 6.430936E-02 | 6.131562E-01 | 2.408912E+00 | 1.141374E+00 | 1.651269E+00 | 1.871407E-01 |
| 25.950 | 4.759314E-03 | 6.003175E-03 | -4.665159E-03 | 6.387039E-02 | 6.403092E-01 | 2.375244E+00 | 1.109244E+00 | 1.616166E+00 | 1.737051E-01 |
| 26.300 | 3.486385E-03 | 1.149377E-02 | -1.617327E-02 | 7.195160E-02 | 5.951199E-01 | 2.295510E+00 | 1.076174E+00 | 1.580128E+00 | 1.775367E-01 |
| 26.650 | 1.526437E-03 | 1.329848E-02 | -9.613117E-03 | 7.540191E-02 | 5.941475E-01 | 2.226756E+00 | 1.043134E+00 | 1.5446163E+00 | 2.047193E-01 |
| 27.000 | 1.557946E-03 | 7.067956E-03 | -8.639422E-03 | 7.237717E-02 | 5.925548E-01 | 2.164313E+00 | 1.010758E+00 | 1.5099381E+00 | 1.948715E-01 |
| 27.350 | 2.303791E-03 | 4.150749E-02 | -2.079181E-03 | 5.873074E-02 | 5.897349E-01 | 2.086629E+00 | 9.803232E-01 | 1.476731E+00 | 1.575179E-01 |
| 27.700 | 2.667023E-03 | 4.164955E-03 | 1.432388E-03 | 5.286191E-02 | 5.854599E-01 | 2.035008E+00 | 9.502739E-01 | 1.445985E+00 | 1.552226E-01 |
| 28.050 | 2.304632E-03 | 4.411766E-03 | -3.285930E-03 | 4.955025E-02 | 5.973603E-01 | 1.973636E+00 | 9.207516E-01 | 1.413725E+00 | 1.501159E-01 |
| 28.400 | 1.821864E-03 | 5.4931247E-03 | -4.420896E-03 | 5.956421E-02 | 5.72880E-01 | 1.912011E+00 | 8.925030E-01 | 1.355788E+00 | 1.503790E-01 |
| 28.750 | 1.456669E-03 | 6.090091E-03 | -6.014150E-03 | 5.412853E-02 | 5.647592E-01 | 1.864485E+00 | 8.644895E-01 | 1.355504E+00 | 1.781810E-01 |
| 29.100 | 1.119184E-03 | 6.744500E-03 | -3.661535E-03 | 4.966548E-02 | 5.554546E-01 | 1.795043E+00 | 8.366030E-01 | 1.324526E+00 | 1.436017E-01 |
| 29.450 | 7.113744E-04 | 6.880952E-03 | -7.433551E-03 | 5.194782E-02 | 5.449980E-01 | 1.739771E+00 | 8.129331E+00 | 1.408077E-01 | 1.408077E-01 |
| 29.800 | 3.206615E-04 | 7.311522E-03 | -3.403738E-03 | 4.290220E-02 | 5.334101E-01 | 1.664155E+00 | 7.817822E-01 | 1.262156E+00 | 1.326266E-01 |
| 30.150 | 4.350567E-05 | 6.7373213E-03 | -3.061285E-03 | 4.452577E-02 | 5.238172E-01 | 1.631076E+00 | 7.231344E+00 | 1.325197E-01 | 1.325197E-01 |
| 30.500 | -2.185907E-04 | 7.025675E-04 | -9.038962E-04 | 4.077280E-02 | 5.176462E-01 | 1.5747163E+00 | 7.303851E-01 | 1.220970E+00 | 1.229928E-01 |
| 30.850 | -3.071081E-04 | 7.664287E-03 | -7.333404E-03 | 5.167074E-02 | 5.114100E-01 | 1.515392E+00 | 7.029716E-01 | 1.170386E+00 | 1.252758E-01 |
| 31.200 | -4.526272E-04 | 7.521060E-03 | -7.842322E-03 | 5.336151E-02 | 5.050833E-01 | 1.443675E+00 | 6.831238E-01 | 1.139565E+00 | 1.191445E-01 |
| 31.550 | -5.170769E-04 | 7.846675E-03 | -8.555990E-03 | 5.255585E-02 | 4.996439E-01 | 1.492335E+00 | 6.611116E-01 | 1.108036E+00 | 1.195799E-01 |
| 31.900 | -5.529989E-04 | 7.9466717E-03 | -8.541177E-03 | 5.336091E-02 | 4.9455314E-01 | 1.355822E+00 | 6.405583E-01 | 1.075601E+00 | 1.145352E-01 |
| 32.250 | -6.609030E-04 | 8.287479E-03 | -8.5151370E-03 | 5.209093E-02 | 4.880001E-01 | 1.304804E+00 | 6.216057E-01 | 1.041830E+00 | 1.104608E+01 |
| 32.600 | -7.186163E-04 | 8.339222E-03 | -9.551749E-03 | 5.3124215E-02 | 4.8017733E-01 | 1.2568495E+00 | 6.024183E-01 | 1.007574E+00 | 1.073417E+01 |
| 32.950 | -8.152990E-04 | 8.495513E-03 | -9.748541E-03 | 5.1515494E-02 | 4.717273E-01 | 1.207417E+00 | 5.9745194E-01 | 1.058263E+00 | 1.058263E+01 |
| 33.300 | -9.4633301E-04 | 8.711841E-03 | -9.748263E-03 | 4.060499E-02 | 4.636588E-01 | 1.164809E+00 | 5.556537E-01 | 9.409998E-01 | 1.063679E-01 |
| 33.650 | -1.086006E-03 | 8.4951559E-03 | -9.791115E-03 | 5.162203E-02 | 4.554356E-01 | 1.1206535E+00 | 5.310200E-01 | 9.062501E-01 | 1.080958E-01 |
| 34.000 | -1.255823E-03 | 9.038197E-03 | -9.492516E-03 | 4.835869E-02 | 4.470774E-01 | 1.077999E+00 | 5.047326E-01 | 8.761460E-01 | 1.095942E-01 |
| 34.350 | -1.464482E-03 | 9.235492E-03 | -1.126554E-02 | 4.112056E-02 | 4.365279E-01 | 1.036794E+00 | 4.796240E-01 | 8.488531E-01 | 1.104844E-01 |
| 34.700 | -1.662648E-03 | 9.401313E-03 | -1.143536E-02 | 5.199418E-02 | 4.300833E-01 | 9.971403E-01 | 4.547226E-01 | 8.263292E-01 | 1.102675E-01 |
| 35.050 | -1.169092E-03 | 9.856651E-03 | -1.191437E-02 | 4.720806E-02 | 4.202003E-01 | 9.612341E-01 | 4.273496E-01 | 8.123165E-01 | 1.106379E-01 |
| 35.400 | -6.979132E-04 | 1.078333E-02 | -1.157195E-02 | 4.0437579E-02 | 4.155331E-01 | 8.674531E-01 | 4.076103E-01 | 8.007103E-01 | 1.050095E-01 |
| 35.750 | -1.417552E-03 | 1.065880E-02 | -1.190741E-02 | 5.2662923E-02 | 4.051028E-01 | 8.501745E-01 | 3.916211E-01 | 7.867695E-01 | 9.699694E-02 |
| 36.100 | -1.949811E-03 | 1.154845E-02 | -1.194466E-02 | 3.215754E-02 | 4.036997E-01 | 8.479334E-01 | 3.749512E-01 | 7.703630E-01 | 9.147151E-02 |
| 36.450 | -2.383162E-03 | 1.093054E-02 | -1.379303E-02 | 2.717081E-02 | 4.061649E-01 | 8.612422E-01 | 3.591346E-01 | 7.523659E-01 | 8.625347E-02 |
| 36.800 | -2.926616E-03 | 1.053679E-02 | -1.387272E-02 | 2.727376E-02 | 3.978069E-01 | 7.667142E-01 | 3.449111E-01 | 7.341204E-01 | 8.011069E-02 |
| 37.150 | -3.847167E-03 | 1.012965E-02 | -1.414646E-02 | 2.702359E-02 | 3.917291E-01 | 7.216474E-01 | 3.211714E-01 | 7.134635E-01 | 7.460911E-02 |
| 37.500 | -3.598634E-03 | 1.090111E-02 | -1.616302E-02 | 2.006002E-02 | 3.638336E-01 | 6.965050E-01 | 3.170578E-01 | 6.866577E-01 | 7.145769E-02 |
| 37.850 | -3.203765E-03 | 1.195415E-02 | -1.523124E-02 | 2.013137E-02 | 3.745666E-01 | 6.641202E-01 | 3.043338E-01 | 6.550645E-01 | 6.960148E-02 |
| 38.200 | -5.750178E-03 | 1.090322E-02 | -1.610448E-02 | 2.111149E-02 | 3.636349E-01 | 6.378329E-01 | 2.907755E-01 | 6.412685E-01 | 6.70540E-02 |
| 38.550 | -6.028583E-03 | 1.139540E-02 | -1.6564735E-02 | 2.336123E-02 | 3.518513E-01 | 6.121614E-01 | 2.761712E-01 | 6.144586E-01 | 6.716352E-02 |
| 38.900 | -6.501738E-03 | 1.102712E-02 | -1.731342E-02 | 2.549818E-02 | 3.519380E-01 | 6.161740E-01 | 2.617404E-01 | 5.929877E-01 | 6.732958E-02 |
| 39.250 | -6.290563E-03 | 1.130474E-02 | -1.721342E-02 | 2.716747E-02 | 3.260384E-01 | 5.661248E-01 | 2.470551E-01 | 5.712733E-01 | 6.751129E-02 |
| 39.600 | -7.840156E-03 | 1.113570E-02 | -1.837272E-02 | 2.932340E-02 | 3.122663E-01 | 5.363556E-01 | 2.311918E-01 | 5.507406E-01 | 6.775162E-02 |
| 39.950 | -8.260696E-03 | 1.132577E-02 | -1.963797E-02 | 3.068325E-02 | 3.1696555E-01 | 5.094950E-01 | 2.170438E-01 | 5.317819E-01 | 6.817960E-02 |
| 40.300 | -8.839501E-03 | 1.153213E-02 | -2.107452E-02 | 3.111711E-02 | 3.111711E-01 | 5.710347E-01 | 2.035911E-01 | 5.143854E-01 | 6.763743E-02 |
| 40.650 | -9.4765735E-03 | 1.175029E-02 | -2.193926E-02 | 3.109961E-02 | 3.125825E-01 | 5.088511E-01 | 1.924075E-01 | 5.024752E-01 | 6.667240E-02 |
| 41.000 | -8.769640E-03 | 1.274959E-02 | -2.114143E-02 | 3.023635E-02 | 3.249837E-01 | 4.057981E-01 | 1.695793F-01 | 4.928260E-01 | 6.551103E-02 |
| 41.350 | -1.076144E-02 | 1.224773E-02 | -2.256250E-02 | 2.905324E-02 | 3.222584E-01 | 4.833204E-01 | 1.545639E-01 | 4.822577E-01 | 6.364669E-02 |
| 41.700 | -1.133063E-02 | 1.237744E-02 | -2.327953E-02 | 2.7727049E-02 | 3.175217E-01 | 3.610534E-01 | 4.197711E-01 | 4.720159E-01 | 6.181777E-02 |
| 42.050 | -1.208710E-02 | 1.245615E-02 | -2.460505E-02 | 2.610662E-02 | 3.110K84E-01 | 3.412587E-01 | 1.312353E-01 | 4.614601E-01 | 5.943739E-02 |

** RELAP4J ANALYSIS FOR STANDARD PROBLEM NO.5 L1-4:JAERI **

DIFFERENTIAL PRESSURE

| (PDE-PC-1) | (PDE-PC-2) | (PDE-P139-30) | (PDE-BL-1) | (PDE-BL-2) | (PDF-BL-3) | (PDE-BL-4) | (PDE-BL-5) | (PDE-BL-7) | |
|------------|---------------|---------------|---------------|--------------|--------------|--------------|--------------|--------------|--------------|
| TIME | AP9-AP6 | AP3-AP6 | AP10-AP1 | AP15-AP16 | AP21-AP27 | AP27-AP26 | AP20-AP26 | AP19-AP20 | AP16-AP19 |
| SEC | MPA | MPA | MPA | MPA | MPA | MPA | MPA | MPA | MPA |
| 42.400 | -1.283146E-02 | -2.199262E-02 | 2.462674E-02 | 3.035235E-01 | 3.235747E-01 | 1.217654E-01 | 4.507910E-01 | 5.690150E-02 | |
| 42.750 | -1.306683E-02 | 1.273296E-02 | -2.532085E-02 | 2.225086E-02 | 2.950275E-01 | 3.076789E-01 | 1.132546E-01 | 4.383783E-01 | 5.428209E-02 |
| 43.100 | -1.340936E-02 | 1.244535E-02 | -2.533560E-02 | 2.054244E-02 | 2.860932E-01 | 3.097454E-01 | 1.053988E-01 | 4.288672E-01 | 5.190300E-02 |
| 43.450 | -1.375076E-02 | 1.246565E-02 | -2.572056E-02 | 1.914597E-02 | 2.766234E-01 | 2.608138E-01 | 9.298983E-02 | 4.231133E-01 | 4.972129E-02 |
| 43.800 | -1.442229E-02 | 1.246974E-02 | -2.667633E-02 | 1.804021E-02 | 2.691314E-01 | 2.665765E-01 | 9.226551E-02 | 4.162177E-01 | 4.763637E-02 |
| 44.150 | -1.510410E-02 | 1.279128E-02 | -2.751517E-02 | 1.701539E-02 | 2.654324E-01 | 2.620520E-01 | 9.284173E-02 | 4.093745E-01 | 4.570R86E-02 |
| 44.500 | -1.545525E-02 | 1.290393E-02 | -2.771435E-02 | 1.592688E-02 | 2.629426E-01 | 2.319673E-01 | 9.236145E-02 | 4.035070E-01 | |

Appendix 4. Output Data List of ALARM-P1 Analysis

| PWR LOSS OF COOLANT ANALYSIS PROGRAM | | | | | | | | | | | | |
|--|----------------------|----------------------|----------------------|----------------------|----------------------|-----------------------|-----------------------|------------------------|------------------------|--------------------------------------|--|-------------|
| CSNI STANDARD PROBLEM NO.5 BY ALARM-P1(MOD1) | | | | | | | | | | | | |
| TIME SEC | Avg Press Vol 14 MPA | Avg Press Vol 21 MPA | Avg Press Vol 22 MPA | Avg Press Vol 30 MPA | Avg Press Vol 31 MPA | Avg Dense Vol 1 MG/M3 | Avg Dense Vol 6 MG/M3 | Avg Dense Vol 10 MG/M3 | Avg Dense Vol 15 MG/M3 | PWR LOSS OF COOLANT ANALYSIS PROGRAM | CSNI STANDARD PROBLEM NO.5 BY ALARM-P1(MOD1) | PAGE |
| 0.0 | 0.157630+02 | 0.158120+02 | 0.157320+02 | 0.422740+01 | 0.102000+00 | 0.766240+00 | 0.767020+00 | 0.766320+00 | 0.766240+00 | 0.157630+02 | 0.158120+02 | 0.157320+02 |
| 0.500000+02 | 0.157590+02 | 0.158110+02 | 0.157320+02 | 0.422740+01 | 0.102020+00 | 0.766230+00 | 0.767010+00 | 0.766200+00 | 0.766250+00 | 0.157590+02 | 0.158110+02 | 0.157320+02 |
| 0.100000+02 | 0.157570+02 | 0.158100+02 | 0.157320+02 | 0.422740+01 | 0.102040+00 | 0.766180+00 | 0.766970+00 | 0.765110+00 | 0.766120+00 | 0.157570+02 | 0.158100+02 | 0.157320+02 |
| 0.150000+02 | 0.157540+02 | 0.158070+02 | 0.157320+02 | 0.422740+01 | 0.102060+00 | 0.765250+00 | 0.766380+00 | 0.766000+00 | 0.766450+00 | 0.157540+02 | 0.158070+02 | 0.157320+02 |
| 0.200000+02 | 0.157500+02 | 0.158040+02 | 0.157320+02 | 0.422740+01 | 0.102080+00 | 0.764700+00 | 0.766450+00 | 0.764410+00 | 0.764320+00 | 0.157500+02 | 0.158040+02 | 0.157320+02 |
| 0.250000+02 | 0.157470+02 | 0.158010+02 | 0.157320+02 | 0.422740+01 | 0.102110+00 | 0.764510+00 | 0.765750+00 | 0.765710+00 | 0.763780+00 | 0.157470+02 | 0.158010+02 | 0.157320+02 |
| 0.300000+02 | 0.157440+02 | 0.157980+02 | 0.157320+02 | 0.422740+01 | 0.102140+00 | 0.763790+00 | 0.765600+00 | 0.764060+00 | 0.763700+00 | 0.157440+02 | 0.157980+02 | 0.157320+02 |
| 0.350000+02 | 0.157410+02 | 0.157950+02 | 0.157320+02 | 0.422740+01 | 0.102160+00 | 0.763170+00 | 0.764890+00 | 0.764170+00 | 0.764290+00 | 0.157410+02 | 0.157950+02 | 0.157320+02 |
| 0.400000+02 | 0.157380+02 | 0.157920+02 | 0.157320+02 | 0.422740+01 | 0.102180+00 | 0.762180+00 | 0.764080+00 | 0.762410+00 | 0.764290+00 | 0.157380+02 | 0.157920+02 | 0.157320+02 |
| 0.450000+02 | 0.157350+02 | 0.157890+02 | 0.157320+02 | 0.422740+01 | 0.102200+00 | 0.761590+00 | 0.762230+00 | 0.762020+00 | 0.762240+00 | 0.157350+02 | 0.157890+02 | 0.157320+02 |
| 0.500000+02 | 0.157320+02 | 0.157860+02 | 0.157320+02 | 0.422740+01 | 0.102220+00 | 0.761580+00 | 0.762220+00 | 0.762010+00 | 0.762230+00 | 0.157320+02 | 0.157860+02 | 0.157320+02 |
| 0.600000+02 | 0.106350+02 | 0.106300+02 | 0.157270+02 | 0.422740+01 | 0.102280+00 | 0.761580+00 | 0.763240+00 | 0.761700+00 | 0.761830+00 | 0.106350+02 | 0.106300+02 | 0.157270+02 |
| 0.700000+02 | 0.106320+02 | 0.956100+01 | 0.157240+02 | 0.422740+01 | 0.102320+00 | 0.760950+00 | 0.761550+00 | 0.760590+00 | 0.761570+00 | 0.106320+02 | 0.956100+01 | 0.157240+02 |
| 0.800000+02 | 0.956020+01 | 0.941370+01 | 0.157200+02 | 0.422740+01 | 0.102370+00 | 0.760590+00 | 0.761060+00 | 0.760460+00 | 0.760840+00 | 0.956020+01 | 0.941370+01 | 0.157200+02 |
| 0.900000+02 | 0.871730+01 | 0.927610+01 | 0.157150+02 | 0.422740+01 | 0.102410+00 | 0.759630+00 | 0.760860+00 | 0.761030+00 | 0.759960+00 | 0.871730+01 | 0.927610+01 | 0.157150+02 |
| 0.100000+02 | 0.881120+01 | 0.861640+01 | 0.157100+02 | 0.422740+01 | 0.102450+00 | 0.759920+00 | 0.759720+00 | 0.759600+00 | 0.759950+00 | 0.881120+01 | 0.861640+01 | 0.157100+02 |
| 0.110000+02 | 0.798730+01 | 0.762860+01 | 0.157040+02 | 0.422740+01 | 0.102490+00 | 0.758900+00 | 0.759530+00 | 0.759100+00 | 0.759500+00 | 0.798730+01 | 0.762860+01 | 0.157040+02 |
| 0.120000+02 | 0.731100+01 | 0.737430+01 | 0.157000+02 | 0.422740+01 | 0.102530+00 | 0.758430+00 | 0.759530+00 | 0.759540+00 | 0.758250+00 | 0.731100+01 | 0.737430+01 | 0.157000+02 |
| 0.130000+02 | 0.727780+01 | 0.709720+01 | 0.156920+02 | 0.422740+01 | 0.102560+00 | 0.758520+00 | 0.758320+00 | 0.758100+00 | 0.758300+00 | 0.727780+01 | 0.709720+01 | 0.156920+02 |
| 0.140000+02 | 0.698570+01 | 0.684480+01 | 0.156880+02 | 0.422740+01 | 0.102600+00 | 0.757870+00 | 0.758110+00 | 0.758300+00 | 0.758320+00 | 0.698570+01 | 0.684480+01 | 0.156880+02 |
| 0.150000+02 | 0.621750+01 | 0.612020+01 | 0.156800+02 | 0.422740+01 | 0.102630+00 | 0.757520+00 | 0.757520+00 | 0.757510+00 | 0.757520+00 | 0.621750+01 | 0.612020+01 | 0.156800+02 |
| 0.160000+02 | 0.615780+01 | 0.604070+01 | 0.156740+02 | 0.422740+01 | 0.102660+00 | 0.757070+00 | 0.757730+00 | 0.756680+00 | 0.757720+00 | 0.615780+01 | 0.604070+01 | 0.156740+02 |
| 0.170000+02 | 0.606560+01 | 0.581860+01 | 0.156660+02 | 0.422740+01 | 0.102690+00 | 0.757290+00 | 0.757270+00 | 0.757260+00 | 0.757270+00 | 0.606560+01 | 0.581860+01 | 0.156660+02 |
| 0.180000+02 | 0.606580+01 | 0.618400+01 | 0.156630+02 | 0.422740+01 | 0.102720+00 | 0.756930+00 | 0.757520+00 | 0.757450+00 | 0.757450+00 | 0.606580+01 | 0.618400+01 | 0.156630+02 |
| 0.190000+02 | 0.620270+01 | 0.617100+01 | 0.156580+02 | 0.422740+01 | 0.102750+00 | 0.757100+00 | 0.757490+00 | 0.757730+00 | 0.757760+00 | 0.620270+01 | 0.617100+01 | 0.156580+02 |
| 0.200000+02 | 0.613340+01 | 0.616660+01 | 0.156530+02 | 0.422740+01 | 0.102780+00 | 0.756760+00 | 0.757210+00 | 0.757630+00 | 0.757320+00 | 0.613340+01 | 0.616660+01 | 0.156530+02 |
| 0.210000+02 | 0.606640+01 | 0.615420+01 | 0.156470+02 | 0.422740+01 | 0.102800+00 | 0.756580+00 | 0.757820+00 | 0.757690+00 | 0.757715+00 | 0.606640+01 | 0.615420+01 | 0.156470+02 |
| 0.220000+02 | 0.612150+01 | 0.615010+01 | 0.156420+02 | 0.422740+01 | 0.102830+00 | 0.756710+00 | 0.757660+00 | 0.757600+00 | 0.757530+00 | 0.612150+01 | 0.615010+01 | 0.156420+02 |
| 0.230000+02 | 0.612130+01 | 0.615010+01 | 0.156420+02 | 0.422740+01 | 0.102860+00 | 0.756710+00 | 0.757810+00 | 0.757610+00 | 0.757620+00 | 0.612130+01 | 0.615010+01 | 0.156420+02 |
| 0.240000+02 | 0.612230+01 | 0.615040+01 | 0.156370+02 | 0.422740+01 | 0.102880+00 | 0.757590+00 | 0.757910+00 | 0.757390+00 | 0.757360+00 | 0.612230+01 | 0.615040+01 | 0.156370+02 |
| 0.250000+02 | 0.612230+01 | 0.615040+01 | 0.156340+02 | 0.422740+01 | 0.102900+00 | 0.757590+00 | 0.757910+00 | 0.757430+00 | 0.757460+00 | 0.612230+01 | 0.615040+01 | 0.156340+02 |
| 0.260000+02 | 0.612270+01 | 0.615120+01 | 0.156280+02 | 0.422740+01 | 0.102920+00 | 0.757620+00 | 0.757720+00 | 0.757710+00 | 0.757720+00 | 0.612270+01 | 0.615120+01 | 0.156280+02 |
| 0.270000+02 | 0.612070+01 | 0.615140+01 | 0.156280+02 | 0.422740+01 | 0.102940+00 | 0.757680+00 | 0.757740+00 | 0.757740+00 | 0.757740+00 | 0.612070+01 | 0.615140+01 | 0.156280+02 |
| 0.280000+02 | 0.606670+01 | 0.614100+01 | 0.156180+02 | 0.422740+01 | 0.102960+00 | 0.756880+00 | 0.756880+00 | 0.757440+00 | 0.757440+00 | 0.606670+01 | 0.614100+01 | 0.156180+02 |
| 0.290000+02 | 0.606710+01 | 0.614070+01 | 0.156170+02 | 0.422740+01 | 0.102980+00 | 0.756890+00 | 0.756890+00 | 0.757760+00 | 0.757760+00 | 0.606710+01 | 0.614070+01 | 0.156170+02 |
| 0.300000+02 | 0.606700+01 | 0.614040+01 | 0.156160+02 | 0.422740+01 | 0.103000+00 | 0.756920+00 | 0.756920+00 | 0.757720+00 | 0.757720+00 | 0.606700+01 | 0.614040+01 | 0.156160+02 |
| 0.310000+02 | 0.606770+01 | 0.615150+01 | 0.156120+02 | 0.422740+01 | 0.103020+00 | 0.757300+00 | 0.757300+00 | 0.757320+00 | 0.757320+00 | 0.606770+01 | 0.615150+01 | 0.156120+02 |
| 0.320000+02 | 0.606780+01 | 0.615120+01 | 0.156100+02 | 0.422740+01 | 0.103040+00 | 0.757370+00 | 0.757370+00 | 0.757300+00 | 0.757300+00 | 0.606780+01 | 0.615120+01 | 0.156100+02 |
| 0.330000+02 | 0.606820+01 | 0.615090+01 | 0.156070+02 | 0.422740+01 | 0.103060+00 | 0.757370+00 | 0.757370+00 | 0.757300+00 | 0.757300+00 | 0.606820+01 | 0.615090+01 | 0.156070+02 |
| 0.340000+02 | 0.606840+01 | 0.615090+01 | 0.156050+02 | 0.422740+01 | 0.103090+00 | 0.757390+00 | 0.757390+00 | 0.757300+00 | 0.757300+00 | 0.606840+01 | 0.615090+01 | 0.156050+02 |
| 0.350000+02 | 0.606840+01 | 0.615070+01 | 0.156050+02 | 0.422740+01 | 0.103110+00 | 0.757390+00 | 0.757390+00 | 0.757300+00 | 0.757300+00 | 0.606840+01 | 0.615070+01 | 0.156050+02 |
| 0.360000+02 | 0.606840+01 | 0.615040+01 | 0.156020+02 | 0.422740+01 | 0.103130+00 | 0.757420+00 | 0.757420+00 | 0.757300+00 | 0.757300+00 | 0.606840+01 | 0.615040+01 | 0.156020+02 |
| 0.370000+02 | 0.606850+01 | 0.609600+01 | 0.156000+02 | 0.422740+01 | 0.103130+00 | 0.757420+00 | 0.757420+00 | 0.757300+00 | 0.757300+00 | 0.606850+01 | 0.609600+01 | 0.156000+02 |
| 0.380000+02 | 0.606860+01 | 0.607830+01 | 0.156960+02 | 0.422740+01 | 0.103160+00 | 0.757420+00 | 0.757420+00 | 0.757300+00 | 0.757300+00 | 0.606860+01 | 0.607830+01 | 0.156960+02 |
| 0.390000+02 | 0.606810+01 | 0.607170+01 | 0.156910+02 | 0.422740+01 | 0.103180+00 | 0.757420+00 | 0.757420+00 | 0.757300+00 | 0.757300+00 | 0.606810+01 | 0.607170+01 | 0.156910+02 |
| 0.400000+02 | 0.606780+01 | 0.607340+01 | 0.156870+02 | 0.422740+01 | 0.103180+00 | 0.757420+00 | 0.757420+00 | 0.757300+00 | 0.757300+00 | 0.606780+01 | 0.607340+01 | 0.156870+02 |
| 0.410000+02 | 0.606810+01 | 0.607510+01 | 0.156840+02 | 0.422740+01 | 0.103180+00 | 0.757420+00 | 0.757420+00 | 0.757300+00 | 0.757300+00 | 0.606810+01 | 0.607510+01 | 0.156840+02 |
| 0.420000+02 | 0.606820+01 | 0.607500+01 | 0.156810+02 | 0.422740+01 | 0.103180+00 | 0.757420+00 | 0.757420+00 | 0.757300+00 | 0.757300+00 | 0.606820+01 | 0.607500+01 | 0.156 |

ALARM-P (MOD1(VERSION 01) DATE 77.06.30) PWR LOSS OF COOLANT ANALYSIS PROGRAM
 CSNI STANDARD PROBLEM NO.5 BY ALARM-P1(MOD1)

| TIME SEC | Avg Press | Avg Press | Avg Press | Avg Press | Avg Dense | Avg Dense | Avg Dense | Avg Dense |
|-------------|-------------|-------------|-------------|-------------|-------------|-------------|--------------|--------------|
| VOL 14 MPA | VOL 21 MPA | VOL 22 MPA | VOL 30 MPA | VOL 31 MPA | VOL 1 MG/M3 | VOL 6 MG/M3 | VOL 10 MG/M3 | VOL 15 MG/M3 |
| 0.55000D+01 | 0.60513D+01 | 0.60421D+01 | 0.13241D+02 | 0.42274D+01 | 0.11593D+00 | 0.17764D+00 | 0.43629D+00 | 0.67686D+00 |
| 0.60000D+01 | 0.60925D+01 | 0.60233D+01 | 0.13038D+02 | 0.42274D+01 | 0.11721D+00 | 0.14975D+00 | 0.40923D+00 | 0.65418D+00 |
| 0.65000D+01 | 0.60191D+01 | 0.60278D+01 | 0.12837D+02 | 0.42274D+01 | 0.11850D+00 | 0.14887D+00 | 0.38551D+00 | 0.63131D+00 |
| 0.70000D+01 | 0.59967D+01 | 0.59731D+01 | 0.12634D+02 | 0.42274D+01 | 0.11978D+00 | 0.14233D+00 | 0.36130D+00 | 0.59975D+00 |
| 0.75000D+01 | 0.59533D+01 | 0.59713D+01 | 0.12428D+02 | 0.42274D+01 | 0.12103D+00 | 0.13874D+00 | 0.34145D+00 | 0.56836D+00 |
| 0.80000D+01 | 0.59521D+01 | 0.58796D+01 | 0.12222D+02 | 0.42274D+01 | 0.12231D+00 | 0.13798D+00 | 0.32311D+00 | 0.54983D+00 |
| 0.85000D+01 | 0.58926D+01 | 0.58740D+01 | 0.12017D+02 | 0.42274D+01 | 0.12359D+00 | 0.13838D+00 | 0.30707D+00 | 0.51830D+00 |
| 0.90000D+01 | 0.58617D+01 | 0.58613D+01 | 0.11812D+02 | 0.42274D+01 | 0.12486D+00 | 0.12923D+00 | 0.29376D+00 | 0.49334D+00 |
| 0.95000D+01 | 0.58252D+01 | 0.58074D+01 | 0.11606D+02 | 0.42274D+01 | 0.12612D+00 | 0.14087D+00 | 0.27895D+00 | 0.47200D+00 |
| 1.00000D+02 | 0.57864D+01 | 0.57699D+01 | 0.11398D+02 | 0.42274D+01 | 0.12735D+00 | 0.14230D+00 | 0.26620D+00 | 0.45124D+00 |
| 0.10500D+02 | 0.57479D+01 | 0.57372D+01 | 0.11348D+02 | 0.42274D+01 | 0.12860D+00 | 0.12549D+00 | 0.43120D+00 | 0.43334D+01 |
| 0.11000D+02 | 0.57201D+01 | 0.56940D+01 | 0.11282D+02 | 0.42274D+01 | 0.12981D+00 | 0.13343D+00 | 0.42565D+00 | 0.41209D+01 |
| 0.11500D+02 | 0.56821D+01 | 0.56621D+01 | 0.11036D+02 | 0.42274D+01 | 0.13101D+00 | 0.10931D+00 | 0.23122D+00 | 0.39282D+00 |
| 0.12000D+02 | 0.56002D+01 | 0.56023D+01 | 0.99614D+01 | 0.42274D+01 | 0.13218D+00 | 0.13793D+00 | 0.22120D+00 | 0.37470D+00 |
| 0.12500D+02 | 0.55820D+01 | 0.55512D+01 | 0.98554D+01 | 0.42274D+01 | 0.13333D+00 | 0.13563D+01 | 0.21114D+00 | 0.35512D+00 |
| 0.13000D+02 | 0.55172D+01 | 0.54926D+01 | 0.98460D+01 | 0.42274D+01 | 0.13446D+00 | 0.13480D+01 | 0.20241D+00 | 0.33671D+00 |
| 0.13500D+02 | 0.54496D+01 | 0.54272D+01 | 0.98390D+01 | 0.42274D+01 | 0.13556D+00 | 0.16889D+01 | 0.19349D+00 | 0.31807D+00 |
| 0.14000D+02 | 0.53781D+01 | 0.53538D+01 | 0.97422D+01 | 0.42274D+01 | 0.13663D+00 | 0.71484D+01 | 0.18467D+00 | 0.29969D+00 |
| 0.14500D+02 | 0.52962D+01 | 0.52730D+01 | 0.97525D+01 | 0.42274D+01 | 0.13768D+00 | 0.90237D+01 | 0.17617D+00 | 0.28174D+00 |
| 0.15000D+02 | 0.52082D+01 | 0.51837D+01 | 0.97649D+01 | 0.42274D+01 | 0.13870D+00 | 0.11509D+00 | 0.16797D+00 | 0.26453D+00 |
| 0.15500D+02 | 0.51187D+01 | 0.50938D+01 | 0.97770D+01 | 0.42274D+01 | 0.13969D+00 | 0.14014D+00 | 0.16048D+00 | 0.24839D+00 |
| 0.16000D+02 | 0.50298D+01 | 0.50078D+01 | 0.96448D+01 | 0.42274D+01 | 0.14064D+00 | 0.15728D+00 | 0.15355D+00 | 0.23384D+00 |
| 0.16500D+02 | 0.49433D+01 | 0.49209D+01 | 0.61474D+01 | 0.42274D+01 | 0.14158D+00 | 0.16699D+00 | 0.14684D+00 | 0.22024D+00 |
| 0.17000D+02 | 0.48860D+01 | 0.48348D+01 | 0.58734D+01 | 0.42274D+01 | 0.14250D+00 | 0.16995D+00 | 0.14029D+00 | 0.20744D+00 |
| 0.17500D+02 | 0.47744D+01 | 0.47199D+01 | 0.56256D+01 | 0.42274D+01 | 0.14342D+00 | 0.16864D+00 | 0.13390D+00 | 0.19537D+00 |
| 0.18000D+02 | 0.46888D+01 | 0.46662D+01 | 0.54020D+01 | 0.42274D+01 | 0.14432D+00 | 0.16426D+00 | 0.12761D+00 | 0.18407D+00 |
| 0.18500D+02 | 0.46059D+01 | 0.45831D+01 | 0.51998D+01 | 0.42274D+01 | 0.14523D+00 | 0.12783D+00 | 0.12113D+00 | 0.17340D+00 |
| 0.19000D+02 | 0.45241D+01 | 0.45008D+01 | 0.50170D+01 | 0.42274D+01 | 0.14609D+00 | 0.15100D+00 | 0.11524D+00 | 0.17660D+00 |
| 0.19500D+02 | 0.44408D+01 | 0.44178D+01 | 0.48527D+01 | 0.42274D+01 | 0.14695D+00 | 0.14478D+00 | 0.10917D+00 | 0.16789D+00 |
| 0.20000D+02 | 0.43571D+01 | 0.43341D+01 | 0.47470D+01 | 0.42274D+01 | 0.14781D+00 | 0.13909D+00 | 0.10321D+00 | 0.15951D+00 |

ALARM-P (MOD1(VERSION 01) DATE 77.06.30) PWR LOSS OF COOLANT ANALYSIS PROGRAM
 CSNI STANDARD PROBLEM NO.5 BY ALARM-P1(MOD1)

| TIME SEC | Avg Press | Avg Press | Avg Press | Avg Press | Avg Dense | Avg Dense | Avg Dense | Avg Dense |
|-------------|-------------|-------------|-------------|--------------|-------------|-------------|--------------|--------------|
| VOL 14 MPA | VOL 21 MPA | VOL 22 MPA | VOL 30 MPA | VOL 31 MPA | VOL 1 MG/M3 | VOL 6 MG/M3 | VOL 10 MG/M3 | VOL 15 MG/M3 |
| 0.20900D+02 | 0.42466D+01 | 0.42427D+01 | 0.14864D+00 | 0.13791D+00 | 0.97349D-01 | 0.15195D+00 | 0.15271D+00 | |
| 0.21000D+02 | 0.41811D+01 | 0.41565D+01 | 0.14884D+01 | 0.42266D+01 | 0.14946D+00 | 0.14227D+00 | 0.91730D-01 | 0.14209D+00 |
| 0.21200D+02 | 0.40800D+01 | 0.40545D+01 | 0.14932D+01 | 0.42177D+01 | 0.15026D+00 | 0.14740D+00 | 0.85470D-01 | 0.12894D+00 |
| 0.22000D+02 | 0.39927D+01 | 0.39711D+01 | 0.14880D+01 | 0.42013D+01 | 0.15104D+00 | 0.14997D+00 | 0.80165D-01 | 0.11911D+00 |
| 0.22200D+02 | 0.39913D+01 | 0.39708D+01 | 0.14829D+01 | 0.42194D+01 | 0.15181D+00 | 0.15215D+00 | 0.73039D-01 | 0.18964D+00 |
| 0.23000D+02 | 0.38038D+01 | 0.37740D+01 | 0.14755D+01 | 0.42274D+01 | 0.15255D+00 | 0.15262D+00 | 0.69992D-01 | 0.24847D+00 |
| 0.23900D+02 | 0.37019D+01 | 0.36840D+01 | 0.14244D+01 | 0.41244D+01 | 0.15327D+00 | 0.15067D+00 | 0.64830D-01 | 0.12189D+00 |
| 0.24000D+02 | 0.35970D+01 | 0.35775D+01 | 0.40931D+01 | 0.40931D+01 | 0.15398D+00 | 0.15404D+00 | 0.59741D-01 | 0.47358D+00 |
| 0.24900D+02 | 0.34846D+01 | 0.34698D+01 | 0.40227D+01 | 0.40597D+01 | 0.15465D+00 | 0.14049D+00 | 0.54795D-01 | 0.61903D+00 |
| 0.25000D+02 | 0.33720D+01 | 0.33397D+01 | 0.41711D+01 | 0.40245D+01 | 0.15531D+00 | 0.13475D+00 | 0.50252D-01 | 0.77981D+00 |
| 0.25500D+02 | 0.32917D+01 | 0.32842D+01 | 0.40562D+01 | 0.39880D+01 | 0.15594D+00 | 0.12850D+00 | 0.47757D-01 | 0.82633D+00 |
| 0.26000D+02 | 0.32121D+01 | 0.31963D+01 | 0.39526D+01 | 0.39911D+01 | 0.15655D+00 | 0.11786D+00 | 0.44851D-01 | 0.84220D+00 |
| 0.26500D+02 | 0.31213D+01 | 0.31050D+01 | 0.38880D+01 | 0.39138D+01 | 0.15715D+00 | 0.11785D+00 | 0.42170D-01 | 0.85534D+00 |
| 0.27000D+02 | 0.30313D+01 | 0.30124D+01 | 0.38291D+01 | 0.38760D+01 | 0.15773D+00 | 0.12057D+00 | 0.36663D-01 | 0.87703D+00 |
| 0.27500D+02 | 0.29375D+01 | 0.29185D+01 | 0.37776D+01 | 0.38377D+01 | 0.15830D+00 | 0.12170D+00 | 0.33861D-01 | 0.88630D+00 |
| 0.28000D+02 | 0.28412D+01 | 0.28237D+01 | 0.37261D+01 | 0.37990D+01 | 0.15884D+00 | 0.11813D+00 | 0.33861D-01 | 0.75249D+00 |
| 0.28500D+02 | 0.27454D+01 | 0.27285D+01 | 0.36747D+01 | 0.37600D+01 | 0.15937D+00 | 0.11132D+00 | 0.31175D-01 | 0.89376D+00 |
| 0.29000D+02 | 0.26536D+01 | 0.26356D+01 | 0.36233D+01 | 0.37208D+01 | 0.15988D+00 | 0.10146D+00 | 0.28616D-01 | 0.90046D+00 |
| 0.29500D+02 | 0.25639D+01 | 0.25437D+01 | 0.35719D+01 | 0.361815D+01 | 0.16037D+00 | 0.92693D+00 | 0.26174D+01 | 0.90677D+00 |
| 0.30000D+02 | 0.24696D+01 | 0.24453D+01 | 0.35208D+01 | 0.36342D+01 | 0.16085D+00 | 0.84310D+01 | 0.23819D+01 | 0.69823D+00 |
| 0.30500D+02 | 0.23816D+01 | 0.23616D+01 | 0.34696D+01 | 0.36303D+01 | 0.16131D+00 | 0.74686D+01 | 0.21697D+01 | 0.62299D+00 |
| 0.31000D+02 | 0.23068D+01 | 0.22924D+01 | 0.34186D+01 | 0.35646D+01 | 0.16175D+00 | 0.68370D+01 | 0.19737D+01 | 0.58598D+00 |
| 0.31500D+02 | 0.22199D+01 | 0.22199D+01 | 0.33676D+01 | 0.35225D+01 | 0.16218D+00 | 0.62834D+01 | 0.18501D+01 | 0.54998D+00 |
| 0.32000D+02 | 0.21512D+01 | 0.21244D+01 | 0.33167D+01 | 0.34866D+01 | 0.16259D+00 | 0.58247D+01 | 0.16593D+01 | 0.50806D+00 |
| 0.32500D+02 | 0.20724D+01 | 0.20629D+01 | 0.32658D+01 | 0.34848D+01 | 0.16298D+00 | 0.53981D+01 | 0.15221D+01 | 0.49346D+00 |
| 0.33000D+02 | 0.19951D+01 | 0.19776D+01 | 0.32130D+01 | 0.34170D+01 | 0.16336D+00 | 0.48757D+01 | 0.13992D+01 | 0.41982D+00 |
| 0.33500D+02 | 0.19229D+01 | 0.19050D+01 | 0.31643D+01 | 0.33733D+01 | 0.16373D+00 | 0.44308D+01 | 0.12930D+01 | 0.39658D+00 |
| 0.34000D+02 | 0.18527D+01 | 0.18324D+01 | 0.31363D+01 | 0.33365D+01 | 0.16408D+00 | 0.41794D+01 | 0.11983D+01 | 0.34293D+00 |
| 0.34500D+02 | 0.17852D+01 | 0.17693D+01 | 0.31036D+01 | 0.33001D+01 | 0.16442D+00 | 0.39682D+01 | 0.11131D+01 | 0.38643D+00 |
| 0.35000D+02 | 0.17217D+01 | 0.17053D+01 | 0.30712D+01 | 0.32642D+01 | 0.16479D+00 | 0.36780D+01 | 0.10176D+01 | 0.36369D+00 |
| 0.35500D+02 | 0.16659D+01 | 0.16439D+01 | 0.29622D+01 | 0.32288D+01 | 0.16506D+00 | 0.32624D+01 | 0.09157D+01 | 0.34979D+00 |
| 0.36000D+02 | 0.16196D+01 | 0.15856D+01 | 0.29121D+01 | 0.31940D+01 | 0.16536D+00 | 0.35108D+01 | 0.91572D+02 | 0.95162D+00 |
| 0.36500D+02 | 0.15741D+01 | 0.15288D+01 | 0.28121D+01 | 0.31262D+01 | 0.16593D+00 | 0.32495D+01 | 0.88232D+02 | 0.95564D+00 |
| 0.37000D+02 | 0.15484D+01 | 0.14731D+01 | 0.27622D+01 | 0.30793D+01 | 0.16622D+00 | 0.31437D+01 | 0.85758D+02 | 0.95754D+00 |
| 0.37500D+02 | 0.15262D+01 | 0.14193D+01 | 0.27175D+01 | 0.30607D+01 | 0.16646D+00 | 0.30597D+01 | 0.89795D+02 | 0.95922D+00 |
| 0.38000D+02 | 0.15083D+01 | 0.13832D+01 | 0.26715D+01 | 0.30221D+01 | 0.16680D+00 | 0.29806D+01 | 0.82902D+02 | 0.96078D+00 |
| 0.38500D+02 | 0.14944D+01 | 0.13136D+01 | 0.26269D+01 | 0.30289D+01 | 0.16667D+00 | 0.29976D+01 | 0.81689D+02 | 0.96228D+00 |
| 0.39000D+02 | 0.14827D+01 | 0.12868D+01 | 0.26134D+01 | 0.29976D+01 | 0.16695D+00 | 0.29103D+01 | 0.81436D+02 | 0.96428D+00 |
| 0.39500D+02 | 0.14716D+01 | 0.12416D+01 | 0.22225D+01 | 0.29366D+01 | 0.16718D+00 | 0.28489D+01 | 0.79574D+02 | 0.96834D+00 |
| 0.40000D+02 | 0.14615D+01 | 0.12178D+01 | 0.25134D+01 | 0.29396D+01 | 0.16740D+00 | 0.27832D+01 | 0.79688D+02 | 0.96487D+00 |
| 0.40500D+02 | 0.14510D+01 | 0.11945D+01 | 0.24667D+01 | 0.29077D+01 | 0.16761D+00 | 0.27167D+01 | 0.79755D+02 | 0.96898D+00 |
| 0.41000D+02 | 0.14410D+01 | 0.10753 | | | | | | |

ALARM-P (MOD1(VERSION 01) DATE 77.06.30) PWR LOSS OF COOLANT ANALYSIS PROGRAM
 CSNI STANDARD PROBLEM NO.5 BY ALARM-P1(MOD1)

| TIME SEC | Avg Press | Avg Press | Avg Press | Avg Press | Avg Dense | Avg Dense | Avg Dense | Avg Dense | |
|-------------|-------------|-------------|--------------|-------------|-------------|-------------|--------------|--------------|-------------|
| VOL 14 MPA | VOL 21 MPA | VOL 22 MPA | VOL 30 MPA | VOL 31 MPA | VOL 1 MG/M3 | VOL 6 MG/M3 | VOL 10 MG/M3 | VOL 15 MG/M3 | |
| 0.455000+02 | 0.81839D+00 | 0.79671D+00 | 0.19896D+01 | 0.26421D+01 | 0.16934D+00 | 0.23301D-01 | 0.94998D-02 | 0.97279D+00 | 0.23779D-01 |
| 0.460000+02 | 0.79243D+00 | 0.77054D+00 | 0.19431D+01 | 0.26188D+01 | 0.16948D+00 | 0.23359D-01 | 0.94492D+02 | 0.97319D+00 | 0.23753D+01 |
| 0.465000+02 | 0.76766D+00 | 0.74557D+00 | 0.18966D+01 | 0.23952D+01 | 0.16961D+00 | 0.23340D-01 | 0.93949D+02 | 0.97335D+00 | 0.23836D+01 |
| 0.470000+02 | 0.74407D+00 | 0.72177D+00 | 0.18505D+01 | 0.23572D+01 | 0.16974D+00 | 0.23811D-01 | 0.93417D+02 | 0.97388D+00 | 0.26000D+01 |
| 0.475000+02 | 0.72136D+00 | 0.69904D+00 | 0.18046D+01 | 0.23501D+01 | 0.16966D+00 | 0.24093D-01 | 0.92879D+02 | 0.97421D+00 | 0.24231D+01 |
| 0.480000+02 | 0.70011D+00 | 0.67736D+00 | 0.17590D+01 | 0.23283D+01 | 0.16998D+00 | 0.24942D+01 | 0.92342D+02 | 0.97452D+00 | 0.24510D+01 |
| 0.485000+02 | 0.67973D+00 | 0.65669D+00 | 0.17137D+01 | 0.23069D+01 | 0.17010D+00 | 0.25005D-01 | 0.91759D+02 | 0.97482D+00 | 0.24610D+01 |
| 0.490000+02 | 0.66098D+00 | 0.63636D+00 | 0.16686D+01 | 0.22860D+01 | 0.17024D+00 | 0.25190D-01 | 0.91129D+02 | 0.97508D+00 | 0.25159D+01 |
| 0.495000+02 | 0.64272D+00 | 0.61819D+00 | 0.16120D+01 | 0.22654D+01 | 0.17032D+00 | 0.25967D-01 | 0.90780D+02 | 0.97533D+00 | 0.25517D+01 |
| 0.500000+02 | 0.62490D+00 | 0.60085D+00 | 0.15467D+01 | 0.22452D+01 | 0.17040D+00 | 0.25157D-01 | 0.90905D+02 | 0.97547D+00 | 0.24611D+01 |
| 0.505000+02 | 0.60804D+00 | 0.58397D+00 | 0.15009D+01 | 0.22455D+01 | 0.17052D+00 | 0.25578D-01 | 0.90223D+02 | 0.97576D+00 | 0.25162D+01 |
| 0.510000+02 | 0.59218D+00 | 0.56741D+00 | 0.15674D+01 | 0.22450D+01 | 0.17062D+00 | 0.26740D-01 | 0.97680D+02 | 0.97604D+00 | 0.25935D+01 |
| 0.515000+02 | 0.57693D+00 | 0.55126D+00 | 0.14141D+01 | 0.23872D+01 | 0.17071D+00 | 0.27631D+01 | 0.97650D+02 | 0.97625D+00 | 0.26642D+01 |
| 0.520000+02 | 0.56168D+00 | 0.53628D+00 | 0.13713D+01 | 0.23686D+01 | 0.17080D+00 | 0.28234D+01 | 0.97123D+02 | 0.97644D+00 | 0.27164D+01 |
| 0.525000+02 | 0.54748D+00 | 0.52023D+00 | 0.13289D+01 | 0.23504D+01 | 0.17089D+00 | 0.28390D+01 | 0.86419D+02 | 0.97668D+00 | 0.27251D+01 |
| 0.530000+02 | 0.53415D+00 | 0.50836D+00 | 0.12860D+01 | 0.23329D+01 | 0.17097D+00 | 0.28542D+01 | 0.85442D+02 | 0.97692D+00 | 0.27621D+01 |
| 0.535000+02 | 0.52150D+00 | 0.49499D+00 | 0.12450D+01 | 0.23150D+01 | 0.17106D+00 | 0.29556D+01 | 0.84547D+02 | 0.97713D+00 | 0.28182D+01 |
| 0.540000+02 | 0.50930D+00 | 0.48204D+00 | 0.12030D+01 | 0.22978D+01 | 0.17113D+00 | 0.30434D+01 | 0.83999D+02 | 0.97729D+00 | 0.28874D+01 |
| 0.545000+02 | 0.49711D+00 | 0.57003D+00 | 0.11630D+01 | 0.22809D+01 | 0.17121D+00 | 0.30923D+01 | 0.83700D+02 | 0.97745D+00 | 0.29296D+01 |
| 0.550000+02 | 0.48578D+00 | 0.49584D+00 | 0.11226D+01 | 0.22644D+01 | 0.17129D+00 | 0.31135D+01 | 0.83170D+02 | 0.97763D+00 | 0.29504D+01 |
| 0.555000+02 | 0.47495D+00 | 0.46756D+00 | 0.10827D+01 | 0.22482D+01 | 0.17136D+00 | 0.31608D+01 | 0.82487D+02 | 0.97780D+00 | 0.29766D+01 |
| 0.560000+02 | 0.46475D+00 | 0.43676D+00 | 0.10452D+01 | 0.22323D+01 | 0.17143D+00 | 0.31965D+01 | 0.81792D+02 | 0.97796D+00 | 0.30148D+01 |
| 0.565000+02 | 0.45500D+00 | 0.42614D+00 | 0.10042D+01 | 0.22167D+01 | 0.17150D+00 | 0.32866D+01 | 0.81304D+02 | 0.97809D+00 | 0.30124D+01 |
| 0.570000+02 | 0.44497D+00 | 0.41634D+00 | 0.96577D+00 | 0.22014D+01 | 0.17156D+00 | 0.33725D+01 | 0.81121D+02 | 0.97820D+00 | 0.31248D+01 |
| 0.575000+02 | 0.43390D+00 | 0.40666D+00 | 0.92760D+00 | 0.21864D+01 | 0.17163D+00 | 0.33526D+01 | 0.80735D+02 | 0.97832D+00 | 0.31340D+01 |
| 0.580000+02 | 0.42693D+00 | 0.39797D+00 | 0.889019D+00 | 0.21711D+01 | 0.17169D+00 | 0.33978D+01 | 0.80206D+02 | 0.97845D+00 | 0.31553D+01 |
| 0.585000+02 | 0.41843D+00 | 0.38927D+00 | 0.85341D+00 | 0.21572D+01 | 0.17175D+00 | 0.33937D+01 | 0.80299D+02 | 0.97859D+00 | 0.31714D+01 |
| 0.590000+02 | 0.41041D+00 | 0.38158D+00 | 0.81721D+00 | 0.21430D+01 | 0.17181D+00 | 0.34481D+01 | 0.79040D+02 | 0.97869D+00 | 0.32074D+01 |
| 0.595000+02 | 0.40283D+00 | 0.37193D+00 | 0.78181D+00 | 0.21291D+01 | 0.17187D+00 | 0.35913D+01 | 0.78818D+02 | 0.97877D+00 | 0.32092D+01 |
| 0.600000+02 | 0.39458D+00 | 0.36427D+00 | 0.74705D+00 | 0.21154D+01 | 0.17193D+00 | 0.36182D+01 | 0.78498D+02 | 0.97886D+00 | 0.33182D+01 |

ALARM-P (MOD1(VERSION V1) DATE 77.06.30) PWR LOSS OF COOLANT ANALYSIS PROGRAM PAGE
 CSNI STANDARD PROBLEM NO.5 BY ALARM-P1(MOD1)

| TIME SEC | Avg Dense | Mix Level | Mix Level | Avg Temp |
|--------------|-------------|-------------|-------------|-------------|-------------|-------------|-------------|-------------|-------------|-------------|
| VOL 21 MG/M3 | VOL 12 M | VOL 22 M | VOL 31 M | VOL 10 C | VOL 11 C | VOL 14 C | VOL 15 C | VOL 21 C | VOL 21 C | |
| 0.0 | 0.76444D+00 | 0.51703D+01 | 0.11454D+01 | 0.28712D+01 | 0.27944D+03 | 0.28056D+03 | 0.27944D+03 | 0.28056D+03 | 0.27944D+03 | 0.27944D+03 |
| 0.500000+02 | 0.76158D+00 | 0.51703D+01 | 0.11454D+01 | 0.49055D+01 | 0.27973D+03 | 0.28033D+03 | 0.27956D+03 | 0.27945D+03 | 0.27949D+03 | 0.27949D+03 |
| 0.100000+01 | 0.76419D+00 | 0.51703D+01 | 0.11454D+01 | 0.49055D+01 | 0.27900D+03 | 0.28015D+03 | 0.27938D+03 | 0.27940D+03 | 0.27943D+03 | 0.27943D+03 |
| 0.150000+01 | 0.76203D+00 | 0.51703D+01 | 0.11454D+01 | 0.49055D+01 | 0.27915D+03 | 0.28014D+03 | 0.27896D+03 | 0.27897D+03 | 0.27897D+03 | 0.27897D+03 |
| 0.200000+01 | 0.76450D+00 | 0.51703D+01 | 0.11454D+01 | 0.49055D+01 | 0.27873D+03 | 0.28004D+03 | 0.27889D+03 | 0.27874D+03 | 0.28005D+03 | 0.27884D+03 |
| 0.250000+01 | 0.76450D+00 | 0.51703D+01 | 0.11454D+01 | 0.49055D+01 | 0.27873D+03 | 0.27884D+03 | 0.27874D+03 | 0.27874D+03 | 0.27884D+03 | 0.27884D+03 |
| 0.300000+01 | 0.76342D+00 | 0.51703D+01 | 0.11454D+01 | 0.49055D+01 | 0.27860D+03 | 0.27874D+03 | 0.27864D+03 | 0.27864D+03 | 0.27864D+03 | 0.27864D+03 |
| 0.350000+01 | 0.76147D+00 | 0.51703D+01 | 0.11454D+01 | 0.49055D+01 | 0.27860D+03 | 0.27874D+03 | 0.27864D+03 | 0.27864D+03 | 0.27864D+03 | 0.27864D+03 |
| 0.400000+01 | 0.76148D+00 | 0.51703D+01 | 0.11454D+01 | 0.49055D+01 | 0.27861D+03 | 0.27874D+03 | 0.27874D+03 | 0.27874D+03 | 0.27874D+03 | 0.27874D+03 |
| 0.450000+01 | 0.76090D+00 | 0.51703D+01 | 0.11454D+01 | 0.49055D+01 | 0.27872D+03 | 0.27892D+03 | 0.27884D+03 | 0.27884D+03 | 0.27884D+03 | 0.27884D+03 |
| 0.500000+01 | 0.76153D+00 | 0.51703D+01 | 0.11454D+01 | 0.49055D+01 | 0.27876D+03 | 0.27933D+03 | 0.27871D+03 | 0.27871D+03 | 0.27871D+03 | 0.27871D+03 |

ALARM-P (MOD1(VERSION V1) DATE 77.06.30) PWR LOSS OF COOLANT ANALYSIS PROGRAM PAGE
 CSNI STANDARD PROBLEM NO.5 BY ALARM-P1(MOD1)

| TIME SEC | Avg Dense | Mix Level | Mix Level | Avg Temp |
|--------------|-------------|-------------|-------------|-------------|-------------|-------------|-------------|-------------|-------------|-------------|
| VOL 21 MG/M3 | VOL 12 M | VOL 22 M | VOL 31 M | VOL 10 C | VOL 11 C | VOL 14 C | VOL 15 C | VOL 21 C | VOL 21 C | |
| 0.350000+00 | 0.74279D+00 | 0.51701D+01 | 0.11332D+01 | 0.49055D+01 | 0.27613D+03 | 0.27740D+03 | 0.27836D+03 | 0.27627D+03 | 0.27725D+03 | 0.27725D+03 |
| 0.400000+00 | 0.74538D+00 | 0.51699D+01 | 0.11305D+01 | 0.49055D+01 | 0.27603D+03 | 0.27731D+03 | 0.27663D+03 | 0.27730D+03 | 0.27648D+03 | 0.27648D+03 |
| 0.450000+00 | 0.74940D+00 | 0.51676D+01 | 0.11272D+01 | 0.49055D+01 | 0.27605D+03 | 0.27729D+03 | 0.27683D+03 | 0.27749D+03 | 0.27749D+03 | 0.27749D+03 |
| 0.500000+00 | 0.74962D+00 | 0.51691D+01 | 0.11239D+01 | 0.49055D+01 | 0.27610D+03 | 0.27745D+03 | 0.27711D+03 | 0.27711D+03 | 0.27745D+03 | 0.27745D+03 |
| 0.550000+00 | 0.74589D+00 | 0.51662D+01 | 0.11203D+01 | 0.49055D+01 | 0.27610D+03 | 0.27745D+03 | 0.27711D+03 | 0.27711D+03 | 0.27745D+03 | 0.27745D+03 |
| 0.600000+00 | 0.74270D+00 | 0.51672D+01 | 0.11166D+01 | 0.49055D+01 | 0.27610D+03 | 0.27745D+03 | 0.27711D+03 | 0.27711D+03 | 0.27745D+03 | 0.27745D+03 |
| 0.650000+00 | 0.74164D+00 | 0.51684D+01 | 0.11136D+01 | 0.49055D+01 | 0.27610D+03 | 0.27745D+03 | 0.27711D+03 | 0.27711D+03 | 0.27745D+03 | 0.27745D+03 |
| 0.700000+00 | 0.74609D+00 | 0.51684D+01 | 0.11104D+01 | 0.49055D+01 | 0.27610D+03 | 0.27745D+03 | 0.27711D+03 | 0.27711D+03 | 0.27745D+03 | 0.27745D+03 |
| 0.750000+00 | 0.74411D+00 | 0.51662D+01 | 0.11063D+01 | 0.49055D+01 | 0.27610D+03 | 0.27745D+03 | 0.27711D+03 | 0.27711D+03 | 0.27745D+03 | 0.27745D+03 |
| 0.800000+00 | 0.73919D+00 | 0.51595D+01 | 0.11039D+01 | 0.49055D+01 | 0.27597D+03 | 0.27733D+03 | 0.27708D+03 | 0.27733D+03 | 0.27717D+03 | 0.27717D+03 |
| 0.850000+00 | 0.73492D+00 | 0.51568D+01 | 0.10954D+01 | 0.49055D+01 | 0.27597D+03 | 0.27732D+03 | 0.27708D+03 | 0.27726D+03 | 0.27710D+03 | 0.27710D+03 |
| 0.900000+00 | 0.73215D+00 | 0.51538D+01 | 0.10907D+01 | 0.49055D+01 | 0.27600D+03 | 0.27730D+03 | 0.27708D+03 | 0.27726D+03 | 0.27707D+03 | 0.27707D+03 |
| 0.950000+00 | 0.73127D+00 | 0.51506D+01 | 0.10860D+01 | 0.49055D+01 | 0.27600D+03 | 0.27726D+03 | 0.27708D+03 | 0.27726D+03 | 0.27708D+03 | 0.27708D+03 |
| 0.100000+01 | 0.73073D+00 | 0.51469D+01 | 0.10811D+01 | 0.49055D+01 | 0.27599D+03 | 0.27723D+03 | 0.27704D+03 | 0.27721D+03 | 0.27710D+03 | 0.27710D+03 |

| ALARM-P (M001(VERSION 01) DATE 77.06.30) | | | | PWR LOSS OF COOLANT ANALYSIS PROGRAM | | | | | | | | | | | | |
|--|-------------|-------------|-------------|--------------------------------------|-------------|-------------|-------------|-------------|-------------|----------|----------|----------|----------|----------|----------|--|
| CSNI STANDARD PROBLEM NO.5 BY ALARM-P1(M001) | | | | | | | | | | | | | | | | |
| TIME SEC | AVG DENSE | MIX LEVEL | MIX LEVEL | MIX LEVEL | MIX LEVEL | Avg Temp | Avg Temp | Avg Temp | Avg Temp | Avg Temp | Avg Temp | Avg Temp | Avg Temp | Avg Temp | Avg Temp | |
| VOL 21 MG/M3 VOL 11 M VOL 22 M VOL 31 M VOL 10 C VOL 11 C VOL 14 C VOL 15 C VOL 21 C | | | | | | | | | | | | | | | | |
| 0.110000+01 | 0.72455D+00 | 0.51390D+01 | 0.10711D+01 | 0.49055D+01 | 0.27604D+03 | 0.27721D+03 | 0.27651D+03 | 0.27634D+03 | 0.27703D+03 | | | | | | | |
| 0.120000+01 | 0.71712D+00 | 0.51302D+01 | 0.10607D+01 | 0.49055D+01 | 0.27603D+03 | 0.27718D+03 | 0.27652D+03 | 0.27627D+03 | 0.27695D+03 | | | | | | | |
| 0.130000+01 | 0.71731D+00 | 0.51208D+01 | 0.10500D+01 | 0.49055D+01 | 0.27605D+03 | 0.27714D+03 | 0.27653D+03 | 0.27627D+03 | 0.27702D+03 | | | | | | | |
| 0.140000+01 | 0.70898D+00 | 0.51106D+01 | 0.10391D+01 | 0.49055D+01 | 0.27609D+03 | 0.27712D+03 | 0.27655D+03 | 0.27632D+03 | 0.27692D+03 | | | | | | | |
| 0.150000+01 | 0.70374D+00 | 0.51000D+01 | 0.10280D+01 | 0.49055D+01 | 0.27610D+03 | 0.27712D+03 | 0.27663D+03 | 0.27633D+03 | 0.27688D+03 | | | | | | | |
| 0.160000+01 | 0.70594D+00 | 0.50989D+01 | 0.10167D+01 | 0.49055D+01 | 0.27611D+03 | 0.27709D+03 | 0.27659D+03 | 0.27637D+03 | 0.27698D+03 | | | | | | | |
| 0.170000+01 | 0.69870D+00 | 0.50777D+01 | 0.10053D+01 | 0.49055D+01 | 0.27612D+03 | 0.27707D+03 | 0.27663D+03 | 0.27635D+03 | 0.27686D+03 | | | | | | | |
| 0.180000+01 | 0.69405D+00 | 0.50661D+00 | 0.99381D+00 | 0.49055D+01 | 0.27613D+03 | 0.27705D+03 | 0.27666D+03 | 0.27635D+03 | 0.27685D+03 | | | | | | | |
| 0.190000+01 | 0.69224D+00 | 0.50594D+01 | 0.98223D+00 | 0.49055D+01 | 0.27615D+03 | 0.27702D+03 | 0.27669D+03 | 0.27640D+03 | 0.27675D+03 | | | | | | | |
| 0.200000+01 | 0.68436D+00 | 0.50417D+01 | 0.97058U+00 | 0.49055D+01 | 0.27616D+03 | 0.27700D+03 | 0.27674D+03 | 0.27640D+03 | 0.27670D+03 | | | | | | | |
| 0.210000+01 | 0.68454D+00 | 0.50289D+01 | 0.95969D+00 | 0.49055D+01 | 0.27618D+03 | 0.27695D+03 | 0.27679D+03 | 0.27641D+03 | 0.27680D+03 | | | | | | | |
| 0.220000+01 | 0.68078D+00 | 0.50158D+01 | 0.94720D+00 | 0.49055D+01 | 0.27619D+03 | 0.27694D+03 | 0.27678D+03 | 0.27646D+03 | 0.27678D+03 | | | | | | | |
| 0.230000+01 | 0.67613D+00 | 0.50024D+01 | 0.93549D+00 | 0.49055D+01 | 0.27621D+03 | 0.27689D+03 | 0.27675D+03 | 0.27646D+03 | 0.27675D+03 | | | | | | | |
| 0.240000+01 | 0.67294D+00 | 0.49886D+01 | 0.92378U+00 | 0.49055D+01 | 0.27622D+03 | 0.27686D+03 | 0.27677D+03 | 0.27648D+03 | 0.27667D+03 | | | | | | | |
| 0.250000+01 | 0.67058D+00 | 0.49749D+01 | 0.91210D+00 | 0.49055D+01 | 0.27623D+03 | 0.27687D+03 | 0.27672D+03 | 0.27651D+03 | 0.27666D+03 | | | | | | | |
| 0.260000+01 | 0.67024D+00 | 0.49612D+01 | 0.90044D+00 | 0.49055D+01 | 0.27624D+03 | 0.27685D+03 | 0.27668D+03 | 0.27653D+03 | 0.27668D+03 | | | | | | | |
| 0.270000+01 | 0.66863D+00 | 0.49475D+01 | 0.88881D+00 | 0.49055D+01 | 0.27630D+03 | 0.27684D+03 | 0.27669D+03 | 0.27656D+03 | 0.27661D+03 | | | | | | | |
| 0.280000+01 | 0.66608D+00 | 0.49336D+01 | 0.87720D+00 | 0.49055D+01 | 0.27631D+03 | 0.27683D+03 | 0.27668D+03 | 0.27659D+03 | 0.27660D+03 | | | | | | | |
| 0.290000+01 | 0.66370D+00 | 0.49198D+01 | 0.86557D+00 | 0.49055D+01 | 0.27632D+03 | 0.27680D+03 | 0.27666D+03 | 0.27656D+03 | 0.27659D+03 | | | | | | | |
| 0.300000+01 | 0.66227D+00 | 0.49059D+01 | 0.85396D+00 | 0.49055D+01 | 0.27636D+03 | 0.27676D+03 | 0.27662D+03 | 0.27654D+03 | 0.27658D+03 | | | | | | | |
| 0.310000+01 | 0.66093D+00 | 0.48891D+01 | 0.84237D+00 | 0.49055D+01 | 0.27639D+03 | 0.27675D+03 | 0.27664D+03 | 0.27652D+03 | 0.27659D+03 | | | | | | | |
| 0.320000+01 | 0.65914D+00 | 0.48779D+01 | 0.83083U+00 | 0.49055D+01 | 0.27642D+03 | 0.27674D+03 | 0.27660D+03 | 0.27649D+03 | 0.27651D+03 | | | | | | | |
| 0.330000+01 | 0.65959D+00 | 0.48640D+01 | 0.81933U+00 | 0.49055D+01 | 0.27645D+03 | 0.27673D+03 | 0.27659D+03 | 0.27647D+03 | 0.27656D+03 | | | | | | | |
| 0.340000+01 | 0.65959D+00 | 0.48504D+01 | 0.80789D+00 | 0.49055D+01 | 0.27650D+03 | 0.27671D+03 | 0.27657D+03 | 0.27645D+03 | 0.27650D+03 | | | | | | | |
| 0.350000+01 | 0.65886D+00 | 0.48367D+01 | 0.79650D+00 | 0.49055D+01 | 0.27653D+03 | 0.27670D+03 | 0.27651D+03 | 0.27643D+03 | 0.27653D+03 | | | | | | | |
| 0.360000+01 | 0.65815D+00 | 0.48231D+01 | 0.78517D+00 | 0.49055D+01 | 0.27657D+03 | 0.27668D+03 | 0.27658D+03 | 0.27645D+03 | 0.27651D+03 | | | | | | | |
| 0.370000+01 | 0.65782D+00 | 0.48093D+01 | 0.77339U+00 | 0.49055D+01 | 0.27654D+03 | 0.27666D+03 | 0.27664D+03 | 0.27647D+03 | 0.27654D+03 | | | | | | | |
| 0.380000+01 | 0.65694D+00 | 0.47957D+01 | 0.76271D+00 | 0.49055D+01 | 0.27653D+03 | 0.27663D+03 | 0.27662D+03 | 0.27643D+03 | 0.27653D+03 | | | | | | | |
| 0.390000+01 | 0.65753D+00 | 0.47819D+01 | 0.75157D+00 | 0.49055D+01 | 0.27652D+03 | 0.27662D+03 | 0.27664D+03 | 0.27642D+03 | 0.27652D+03 | | | | | | | |
| 0.400000+01 | 0.65528D+00 | 0.47684D+01 | 0.74050D+00 | 0.49055D+01 | 0.27654D+03 | 0.27661D+03 | 0.27666D+03 | 0.27644D+03 | 0.27651D+03 | | | | | | | |
| 0.410000+01 | 0.65585D+00 | 0.47545D+01 | 0.72950D+00 | 0.49055D+01 | 0.27658D+03 | 0.27664D+03 | 0.27664D+03 | 0.27641D+03 | 0.27652D+03 | | | | | | | |
| 0.420000+01 | 0.65416D+00 | 0.47409D+01 | 0.71857U+00 | 0.49055D+01 | 0.27661D+03 | 0.27661D+03 | 0.27664D+03 | 0.27642D+03 | 0.27653D+03 | | | | | | | |
| 0.430000+01 | 0.65350D+00 | 0.47271D+01 | 0.70711D+00 | 0.49055D+01 | 0.27665D+03 | 0.27664D+03 | 0.27664D+03 | 0.27640D+03 | 0.27653D+03 | | | | | | | |
| 0.440000+01 | 0.65313D+00 | 0.47133D+01 | 0.69691L+00 | 0.49055D+01 | 0.27667D+03 | 0.27667D+03 | 0.27665D+03 | 0.27636D+03 | 0.27653D+03 | | | | | | | |
| 0.450000+01 | 0.65309D+00 | 0.46995D+01 | 0.68611H+00 | 0.49055D+01 | 0.27670D+03 | 0.27661D+03 | 0.27657D+03 | 0.27636D+03 | 0.27643D+03 | | | | | | | |
| 0.460000+01 | 0.65302D+00 | 0.46854D+01 | 0.67553D+00 | 0.49055D+01 | 0.27673D+03 | 0.27656D+03 | 0.27648D+03 | 0.27636D+03 | 0.27648D+03 | | | | | | | |
| 0.470000+01 | 0.65154D+00 | 0.46714D+01 | 0.66649D+00 | 0.49055D+01 | 0.27634D+03 | 0.27647D+03 | 0.27651D+03 | 0.27631D+03 | 0.27652D+03 | | | | | | | |
| 0.480000+01 | 0.65082D+00 | 0.46572D+01 | 0.65454D+00 | 0.49055D+01 | 0.27631D+03 | 0.27644D+03 | 0.27652D+03 | 0.27628D+03 | 0.27652D+03 | | | | | | | |
| 0.490000+01 | 0.64999D+00 | 0.46434D+01 | 0.64395D+00 | 0.49055D+01 | 0.27627D+03 | 0.27642D+03 | 0.27650D+03 | 0.27627D+03 | 0.27652D+03 | | | | | | | |
| 0.500000+01 | 0.64932D+00 | 0.46286D+01 | 0.63356D+00 | 0.49055D+01 | 0.27628D+03 | 0.27639D+03 | 0.27622D+03 | 0.27622D+03 | 0.27627D+03 | | | | | | | |

| ALARM-P (M001(VERSION 01) DATE 77.06.30) | | | | PWR LOSS OF COOLANT ANALYSIS PROGRAM | | | | | | | | | | | |
|--|-------------|-------------|-------------|--------------------------------------|-------------|-------------|-------------|-------------|-------------|-------------|-------------|-------------|-------------|-------------|-------------|
| CSNI STANDARD PROBLEM NO.5 BY ALARM-P1(M001) | | | | | | | | | | | | | | | |
| TIME SEC | AVG DENSE | MIX LEVEL | MIX LEVEL | MIX LEVEL | MIX LEVEL | Avg Temp |
| 0.550000+01 | 0.64931D+00 | 0.45545D+01 | 0.58266D+00 | 0.49055D+01 | 0.27614D+03 | 0.27627D+03 | 0.27615D+03 | 0.27612D+03 | 0.27605D+03 |
| 0.600000+01 | 0.63613D+00 | 0.44757D+01 | 0.53339U+00 | 0.49055D+01 | 0.27616D+03 | 0.27611D+03 | 0.27608D+03 | 0.27608D+03 | 0.27580D+03 |
| 0.650000+01 | 0.62632D+00 | 0.43931D+01 | 0.48566D+00 | 0.49055D+01 | 0.27582D+03 | 0.27592D+03 | 0.27592D+03 | 0.27580D+03 |
| 0.700000+01 | 0.60316D+00 | 0.43726D+01 | 0.43927D+00 | 0.49055D+01 | 0.27594D+03 | 0.27581D+03 | 0.27581D+03 | 0.27561D+03 |
| 0.750000+01 | 0.58356D+00 | 0.43589D+01 | 0.43986D+00 | 0.49055D+01 | 0.27591D+03 | 0.27591D+03 | 0.27591D+03 | 0.27571D+03 |
| 0.800000+01 | 0.54329D+00 | 0.43473D+01 | 0.34973D+00 | 0.49055D+01 | 0.27574D+03 | 0.27588D+03 | 0.27574D+03 | 0.275 | | | | | | | |

ALARM-P (MOD1(VERSION 01) DATE 77.06.30) PWR LOSS OF COOLANT ANALYSIS PROGRAM

CSN STANDARD PROBLEM NO.5 BY ALARM-P1(MOD1)

| TIME | SEC | AVG DENSE | MIX LEVEL | MIX LEVEL | MIX LEVEL | Avg Temp | VOL 21 | | | | | | | |
|-------------|-------------|-------------|-------------|-------------|-------------|-------------|-------------|-------------|-------------|-------------|-------------|-------------|-------------|-------------|-------------|-------------|-------------|-------------|-------------|
| | | VOL 21 | MG/M3 | VOL 11 | M | VOL 22 | M | VOL 31 | M | VOL 10 | C | VOL 11 | C | VOL 14 | C | VOL 15 | C | VOL 21 | C |
| 0.240000+02 | 0.908770+01 | 0.434100+01 | 0.812590+01 | 0.490550+01 | 0.254110+03 | 0.254260+03 | 0.254260+03 | 0.254210+03 | 0.254210+03 | 0.253940+03 | 0.253940+03 | 0.253940+03 | 0.253940+03 | 0.253940+03 | 0.253940+03 | 0.253940+03 | 0.253940+03 | 0.253940+03 | 0.253940+03 |
| 0.210000+02 | 0.866380+01 | 0.434050+01 | 0.810600+01 | 0.490550+01 | 0.252810+03 | 0.252980+03 | 0.253020+03 | 0.252980+03 | 0.252980+03 | 0.252980+03 | 0.252980+03 | 0.252980+03 | 0.252980+03 | 0.252980+03 | 0.252980+03 | 0.252980+03 | 0.252980+03 | 0.252980+03 | 0.252980+03 |
| 0.215000+02 | 0.856570+01 | 0.434390+01 | 0.808500+01 | 0.490550+01 | 0.251420+03 | 0.251550+03 | 0.251550+03 | 0.251550+03 | 0.251550+03 | 0.251550+03 | 0.251550+03 | 0.251550+03 | 0.251550+03 | 0.251550+03 | 0.251550+03 | 0.251550+03 | 0.251550+03 | 0.251550+03 | |
| 0.220000+02 | 0.791140+01 | 0.433960+01 | 0.808630+01 | 0.490550+01 | 0.250250+03 | 0.250260+03 | 0.250260+03 | 0.250220+03 | 0.250220+03 | 0.250220+03 | 0.250220+03 | 0.250220+03 | 0.250220+03 | 0.250220+03 | 0.250220+03 | 0.250220+03 | 0.250220+03 | 0.250220+03 | |
| 0.225000+02 | 0.754260+01 | 0.433950+01 | 0.808520+01 | 0.490550+01 | 0.248600+03 | 0.248840+03 | 0.248900+03 | 0.248840+03 | 0.248840+03 | 0.248840+03 | 0.248840+03 | 0.248840+03 | 0.248840+03 | 0.248840+03 | 0.248840+03 | 0.248840+03 | 0.248840+03 | 0.248840+03 | |
| 0.230000+02 | 0.722500+01 | 0.434060+01 | 0.802500+01 | 0.490550+01 | 0.247320+03 | 0.247740+03 | 0.247740+03 | 0.247410+03 | 0.247410+03 | 0.247360+03 | 0.247360+03 | 0.247360+03 | 0.247360+03 | 0.247360+03 | 0.247360+03 | 0.247360+03 | 0.247360+03 | 0.247360+03 | |
| 0.235000+02 | 0.684760+01 | 0.434180+01 | 0.800480+01 | 0.490550+01 | 0.245630+03 | 0.245830+03 | 0.245840+03 | 0.245810+03 | 0.245810+03 | 0.245840+03 | 0.245840+03 | 0.245840+03 | 0.245840+03 | 0.245840+03 | 0.245840+03 | 0.245840+03 | 0.245840+03 | 0.245840+03 | |
| 0.240000+02 | 0.637780+01 | 0.434460+01 | 0.798460+01 | 0.490550+01 | 0.243940+03 | 0.244130+03 | 0.244160+03 | 0.244100+03 | 0.244100+03 | 0.244100+03 | 0.244100+03 | 0.244100+03 | 0.244100+03 | 0.244100+03 | 0.244100+03 | 0.244100+03 | 0.244100+03 | | |
| 0.245000+02 | 0.604020+01 | 0.434800+01 | 0.796450+01 | 0.490550+01 | 0.242190+03 | 0.242310+03 | 0.242300+03 | 0.242300+03 | 0.242300+03 | 0.242300+03 | 0.242300+03 | 0.242300+03 | 0.242300+03 | 0.242300+03 | 0.242300+03 | 0.242300+03 | 0.242300+03 | | |
| 0.250000+02 | 0.559270+01 | 0.435090+01 | 0.794470+01 | 0.490550+01 | 0.240300+03 | 0.240460+03 | 0.240460+03 | 0.240460+03 | 0.240460+03 | 0.240460+03 | 0.240460+03 | 0.240460+03 | 0.240460+03 | 0.240460+03 | 0.240460+03 | 0.240460+03 | 0.240460+03 | | |
| 0.255000+02 | 0.539500+01 | 0.434340+01 | 0.800730+01 | 0.490550+01 | 0.230760+03 | 0.231900+03 | 0.231900+03 | 0.231900+03 | 0.231900+03 | 0.231900+03 | 0.231900+03 | 0.231900+03 | 0.231900+03 | 0.231900+03 | 0.231900+03 | 0.231900+03 | 0.231900+03 | | |
| 0.260000+02 | 0.522230+01 | 0.434090+01 | 0.785900+01 | 0.490550+01 | 0.219760+03 | 0.223770+03 | 0.223770+03 | 0.223770+03 | 0.223770+03 | 0.223770+03 | 0.223770+03 | 0.223770+03 | 0.223770+03 | 0.223770+03 | 0.223770+03 | 0.223770+03 | 0.223770+03 | | |
| 0.265000+02 | 0.494280+01 | 0.434180+01 | 0.782710+01 | 0.490550+01 | 0.208840+03 | 0.212600+03 | 0.212600+03 | 0.212600+03 | 0.212600+03 | 0.212600+03 | 0.212600+03 | 0.212600+03 | 0.212600+03 | 0.212600+03 | 0.212600+03 | 0.212600+03 | | | |
| 0.270000+02 | 0.501900+01 | 0.434030+01 | 0.780570+01 | 0.490550+01 | 0.198940+03 | 0.213410+03 | 0.213440+03 | 0.213440+03 | 0.213440+03 | 0.213440+03 | 0.213440+03 | 0.213440+03 | 0.213440+03 | 0.213440+03 | 0.213440+03 | 0.213440+03 | | | |
| 0.275000+02 | 0.489390+01 | 0.434080+01 | 0.778430+01 | 0.490550+01 | 0.191010+03 | 0.212670+03 | 0.212670+03 | 0.212670+03 | 0.212670+03 | 0.212670+03 | 0.212670+03 | 0.212670+03 | 0.212670+03 | 0.212670+03 | 0.212670+03 | 0.212670+03 | | | |
| 0.280000+02 | 0.476170+01 | 0.434120+01 | 0.776240+01 | 0.490550+01 | 0.181240+03 | 0.205850+03 | 0.205860+03 | 0.205860+03 | 0.205860+03 | 0.205860+03 | 0.205860+03 | 0.205860+03 | 0.205860+03 | 0.205860+03 | 0.205860+03 | 0.205860+03 | | | |
| 0.285000+02 | 0.468570+01 | 0.434060+01 | 0.774160+01 | 0.490550+01 | 0.174740+03 | 0.202910+03 | 0.202910+03 | 0.202910+03 | 0.202910+03 | 0.202910+03 | 0.202910+03 | 0.202910+03 | 0.202910+03 | 0.202910+03 | 0.202910+03 | 0.202910+03 | | | |
| 0.290000+02 | 0.465400+01 | 0.434070+01 | 0.771940+01 | 0.490550+01 | 0.167820+03 | 0.202710+03 | 0.202710+03 | 0.202710+03 | 0.202710+03 | 0.202710+03 | 0.202710+03 | 0.202710+03 | 0.202710+03 | 0.202710+03 | 0.202710+03 | | | | |
| 0.295000+02 | 0.465750+01 | 0.434040+01 | 0.769790+01 | 0.490550+01 | 0.161560+03 | 0.202520+03 | 0.202520+03 | 0.202520+03 | 0.202520+03 | 0.202520+03 | 0.202520+03 | 0.202520+03 | 0.202520+03 | 0.202520+03 | 0.202520+03 | | | | |
| 0.300000+02 | 0.465210+01 | 0.434040+01 | 0.767600+01 | 0.490550+01 | 0.151580+03 | 0.202350+03 | 0.202350+03 | 0.202350+03 | 0.202350+03 | 0.202350+03 | 0.202350+03 | 0.202350+03 | 0.202350+03 | 0.202350+03 | 0.202350+03 | | | | |
| 0.305000+02 | 0.464050+01 | 0.434100+01 | 0.765340+01 | 0.490550+01 | 0.150560+03 | 0.202140+03 | 0.202140+03 | 0.202140+03 | 0.202140+03 | 0.202140+03 | 0.202140+03 | 0.202140+03 | 0.202140+03 | 0.202140+03 | 0.202140+03 | | | | |
| 0.310000+02 | 0.462070+01 | 0.434040+01 | 0.763220+01 | 0.490550+01 | 0.146550+03 | 0.201950+03 | 0.201950+03 | 0.201950+03 | 0.201950+03 | 0.201950+03 | 0.201950+03 | 0.201950+03 | 0.201950+03 | 0.201950+03 | 0.201950+03 | | | | |
| 0.315000+02 | 0.398240+01 | 0.433910+01 | 0.761030+01 | 0.490550+01 | 0.140520+03 | 0.201760+03 | 0.201760+03 | 0.201760+03 | 0.201760+03 | 0.201760+03 | 0.201760+03 | 0.201760+03 | 0.201760+03 | 0.201760+03 | 0.201760+03 | | | | |
| 0.320000+02 | 0.387190+01 | 0.433900+01 | 0.759840+01 | 0.490550+01 | 0.135580+03 | 0.201580+03 | 0.201580+03 | 0.201580+03 | 0.201580+03 | 0.201580+03 | 0.201580+03 | 0.201580+03 | 0.201580+03 | 0.201580+03 | 0.201580+03 | | | | |
| 0.325000+02 | 0.378410+01 | 0.434050+01 | 0.756590+01 | 0.490550+01 | 0.131520+03 | 0.201400+03 | 0.201400+03 | 0.201400+03 | 0.201400+03 | 0.201400+03 | 0.201400+03 | 0.201400+03 | 0.201400+03 | 0.201400+03 | 0.201400+03 | | | | |
| 0.330000+02 | 0.367400+01 | 0.433940+01 | 0.754350+01 | 0.490550+01 | 0.124770+03 | 0.201210+03 | 0.201210+03 | 0.201210+03 | 0.201210+03 | 0.201210+03 | 0.201210+03 | 0.201210+03 | 0.201210+03 | 0.201210+03 | 0.201210+03 | | | | |
| 0.335000+02 | 0.352880+01 | 0.433980+01 | 0.752130+01 | 0.490550+01 | 0.124290+03 | 0.201040+03 | 0.201040+03 | 0.201040+03 | 0.201040+03 | 0.201040+03 | 0.201040+03 | 0.201040+03 | 0.201040+03 | 0.201040+03 | 0.201040+03 | | | | |
| 0.340000+02 | 0.346310+01 | 0.434030+01 | 0.749840+01 | 0.490550+01 | 0.124060+03 | 0.200840+03 | 0.200840+03 | 0.200840+03 | 0.200840+03 | 0.200840+03 | 0.200840+03 | 0.200840+03 | 0.200840+03 | 0.200840+03 | 0.200840+03 | | | | |
| 0.345000+02 | 0.338800+01 | 0.434000+01 | 0.747450+01 | 0.490550+01 | 0.117110+03 | 0.200660+03 | 0.200660+03 | 0.200660+03 | 0.200660+03 | 0.200660+03 | 0.200660+03 | 0.200660+03 | 0.200660+03 | 0.200660+03 | 0.200660+03 | | | | |
| 0.350000+02 | 0.328340+01 | 0.434300+01 | 0.745250+01 | 0.490550+01 | 0.111450+03 | 0.200450+03 | 0.200450+03 | 0.200450+03 | 0.200450+03 | 0.200450+03 | 0.200450+03 | 0.200450+03 | 0.200450+03 | 0.200450+03 | 0.200450+03 | | | | |
| 0.355000+02 | 0.311460+01 | 0.434400+01 | 0.742960+01 | 0.490550+01 | 0.105200+03 | 0.200310+03 | 0.200310+03 | 0.200310+03 | 0.200310+03 | 0.200310+03 | 0.200310+03 | 0.200310+03 | 0.200310+03 | 0.200310+03 | 0.200310+03 | | | | |
| 0.360000+02 | 0.311100+01 | 0.434500+01 | 0.740670+01 | 0.490550+01 | 0.100560+03 | 0.200130+03 | 0.200130+03 | 0.200130+03 | 0.200130+03 | 0.200130+03 | 0.200130+03 | 0.200130+03 | 0.200130+03 | 0.200130+03 | 0.200130+03 | | | | |
| 0.365000+02 | 0.301760+01 | 0.434120+01 | 0.739390+01 | 0.490550+01 | 0.096150+03 | 0.199610+03 | 0.199610+03 | 0.199610+03 | 0.199610+03 | 0.199610+03 | 0.199610+03 | 0.199610+03 | 0.199610+03 | 0.199610+03 | 0.199610+03 | | | | |
| 0.370000+02 | 0.293570+01 | 0.434060+01 | 0.736110+01 | 0.490550+01 | 0.092130+03 | 0.198780+03 | 0.198780+03 | 0.198780+03 | 0.198780+03 | 0.198780+03 | 0.198780+03 | 0.198780+03 | 0.198780+03 | 0.198780+03 | | | | | |
| 0.375000+02 | 0.286220+01 | 0.434380+01 | 0.734170+01 | 0.490550+01 | 0.087960+03 | 0.198440+03 | 0.198440+03 | 0.198440+03 | 0.198440+03 | 0.198440+03 | 0.198440+03 | 0.198440+03 | 0.198440+03 | 0.198440+03 | | | | | |
| 0.380000+02 | 0.281230+01 | 0.434500+01 | 0.731260+01 | 0.490550+01 | 0.084590+03 | 0.198280+03 | 0.198280+03 | 0.198280+03 | 0.198280+03 | 0.198280+03 | 0.198280+03 | 0.198280+03 | 0.198280+03 | 0.198280+03 | | | | | |
| 0.385000+02 | 0.276630+01 | 0.434180+01 | 0.728770+01 | 0.490550+01 | 0.081040+03 | 0.198010+03 | 0.198010+03 | 0.198010+03 | 0.198010+03 | 0.198010+03 | 0.198010+03 | 0.198010+03 | 0.198010+03 | 0.198010+03 | | | | | |
| 0.390000+02 | 0.271340+01 | 0.434120+01 | 0.724360+01 | 0.490550+01 | 0.077400+03 | 0. | | | | | | | | | | | | | |

| ALARM-P (M011(VERSION 01) DATE 77.06.30) PWR LOSS OF COOLANT ANALYSIS PROGRAM | | | | | | | | | | PAGE |
|---|-------------|--------------|---------------|--------------|--------------|--------------|-------------|-------------|-------------|-------------|
| CSNI STANDARD PROBLEM NU.5 BY ALARM-P1(M011) | | | | | | | | | | |
| TIME SEC | Avg TEMP | Avg TEMP | DIFF PRESS | DIFF PRESS | DIFF PRESS | DIFF PRESS | DIFF PRESS | DIFF PRESS | DIFF PRESS | |
| VOL 28 | C | VOL 31 | C | V 6-v 9 MPA | V 3-v 6 MPA | V 1-v10 MPA | V15-v16 MPA | V21-v26 MPA | V26-v31 MPA | V20-v31 MPA |
| 0.0 | 0.25444D+03 | 0.85889D+02 | -0.168710D+00 | 0.87523D-01 | -0.62025D+01 | 0.10338D+01 | 0.19297D+00 | 0.15517D+02 | 0.15648D+02 | |
| 0.10000D+02 | 0.25444D+03 | 0.83879D+02 | -0.14533D+00 | 0.84344D+01 | -0.70711D+01 | 0.16559D+01 | 0.18493D+01 | 0.10615D+02 | 0.53032D+01 | |
| 0.14000D+01 | 0.25330D+03 | 0.83595D+02 | -0.52533D+00 | 0.12789D+00 | -0.12474D+01 | 0.92384D+00 | 0.11818D+01 | 0.14045D+02 | 0.53362D+01 | |
| 0.15000D+01 | 0.25334D+03 | 0.85933D+02 | -0.15993D+00 | 0.84804D+00 | -0.18400D+01 | 0.11589D+01 | 0.20569D+01 | 0.10969D+02 | 0.57448D+01 | |
| 0.20000D+01 | 0.25341D+03 | 0.83932D+02 | -0.54595D+00 | 0.62428D+00 | -0.38161D+00 | 0.96846D+00 | 0.14031D+01 | 0.14340D+02 | 0.55324D+01 | |
| 0.25000D+01 | 0.25414D+03 | 0.85932D+02 | -0.54595D+00 | 0.21115D+00 | -0.10357D+01 | 0.18053D+01 | 0.11963D+02 | 0.35002D+01 | | |
| 0.30000D+01 | 0.25413D+03 | 0.85941D+02 | -0.47816D+00 | -0.13512D+01 | -0.22893D+00 | 0.10836D+01 | 0.13105D+01 | 0.13183D+02 | 0.34189D+01 | |
| 0.35000D+01 | 0.25414D+03 | 0.85925D+02 | -0.10544D+01 | 0.63849D+00 | -0.11737D+01 | 0.11737D+01 | 0.16092D+01 | 0.10113D+02 | 0.54356D+01 | |
| 0.40000D+01 | 0.25367D+03 | 0.85926D+02 | -0.72640D+00 | 0.22592D+01 | 0.19829D+01 | 0.11387D+01 | 0.12236D+01 | 0.11116D+02 | 0.54698D+01 | |
| 0.45000D+01 | 0.25326D+03 | 0.83967D+02 | -0.13625D+00 | 0.13625D+01 | -0.44284D+01 | 0.15857D+01 | 0.10147D+01 | 0.35447D+01 | 0.35447D+01 | |
| 0.50000D+01 | 0.25329D+03 | 0.83976D+02 | -0.56528D+00 | 0.72198D+00 | -0.16153D+01 | 0.11053D+01 | 0.11053D+01 | 0.11053D+01 | 0.35632D+01 | |
| 0.60000D+01 | 0.25365D+03 | 0.83799D+02 | -0.18983D+00 | -0.74730D+00 | -0.39083D+01 | -0.52024D+00 | 0.10676D+01 | 0.49732D+01 | 0.36725D+01 | |
| 0.70000D+01 | 0.25277D+03 | 0.84110D+02 | -0.24992D+00 | 0.88428D+00 | -0.24710D+00 | 0.97470D+00 | 0.18701D+01 | 0.35115D+01 | 0.35115D+01 | |
| 0.80000D+01 | 0.25297D+03 | 0.84426D+02 | -0.95535D+00 | 0.70962D+00 | -0.25004D+00 | 0.22106D+00 | 0.99673D+00 | 0.83126D+01 | 0.35158D+01 | |
| 0.90000D+01 | 0.25231D+03 | 0.84076D+02 | -0.66196D+00 | -0.54547D+00 | -0.13348D+00 | 0.21386D+00 | 0.90610D+00 | 0.82676D+01 | 0.34899D+01 | |
| 0.10000D+00 | 0.25248D+03 | 0.84428D+02 | -0.23955D+00 | 0.84694D+00 | -0.45330D+00 | 0.46030D+00 | 0.66389D+00 | 0.73986D+01 | 0.54449D+01 | |
| 0.11000D+00 | 0.25230D+03 | 0.84472D+02 | -0.32310D+00 | -0.64767D+00 | -0.45495D+00 | 0.80272D+01 | 0.49585D+00 | 0.70302D+01 | 0.33850D+01 | |
| 0.12000D+00 | 0.25272D+03 | 0.84408D+02 | -0.72616D+00 | -0.72185D+00 | -0.31062D+00 | 0.31366D+00 | 0.54051D+00 | 0.67312D+01 | 0.35180D+01 | |
| 0.13000D+00 | 0.25230D+03 | 0.84100D+02 | -0.38675D+00 | 0.10558D+01 | -0.36267D+00 | 0.20130D+00 | 0.59107D+00 | 0.35152D+01 | 0.35152D+01 | |
| 0.14000D+00 | 0.25226D+03 | 0.84112D+02 | -0.53423D+00 | 0.32077D+00 | -0.26463D+00 | 0.13393D+00 | 0.25551D+00 | 0.60907D+01 | 0.35152D+01 | |
| 0.15000D+00 | 0.25235D+03 | 0.84412D+02 | -0.66692D+00 | -0.21155D+00 | -0.95745D+00 | 0.22936D+00 | 0.32149D+00 | 0.60876D+01 | 0.49914D+01 | |
| 0.16000D+00 | 0.25219D+03 | 0.84436D+02 | -0.55937D+00 | 0.43896D+00 | -0.11053D+00 | 0.63459D+00 | 0.24570D+00 | 0.68081D+01 | 0.44668D+01 | |
| 0.17000D+00 | 0.25227D+03 | 0.84414D+02 | -0.14981D+00 | 0.15495D+00 | -0.26269D+00 | 0.43958D+00 | 0.24202D+00 | 0.58399D+01 | 0.44665D+01 | |
| 0.18000D+00 | 0.25212D+03 | 0.84419D+02 | -0.24815D+00 | 0.14238D+00 | -0.37684D+00 | 0.87784D+00 | 0.65729D+00 | 0.54204D+01 | 0.44598D+01 | |
| 0.19000D+00 | 0.25219D+03 | 0.84416D+02 | -0.27895D+00 | 0.14496D+00 | -0.32667D+00 | 0.34401D+00 | 0.77516D+00 | 0.52931D+01 | 0.42442D+01 | |
| 0.20000D+00 | 0.25226D+03 | 0.84417D+02 | -0.27677D+00 | 0.14881D+00 | -0.21458D+00 | 0.39451D+00 | 0.75986D+00 | 0.53019D+01 | 0.40357D+01 | |
| 0.21000D+00 | 0.25217D+03 | 0.84418D+02 | -0.12678D+00 | -0.34135D+00 | -0.26302D+00 | 0.42519D+00 | 0.74713D+00 | 0.53244D+01 | 0.38523D+01 | |
| 0.22000D+00 | 0.25248D+03 | 0.84419D+02 | -0.19189D+00 | -0.27070D+00 | -0.19795D+00 | 0.29866D+00 | 0.37272D+00 | 0.44456D+01 | 0.35300D+01 | |
| 0.23000D+00 | 0.25230D+03 | 0.84419D+02 | -0.16180D+00 | 0.83447D+00 | -0.33151D+00 | 0.23693D+00 | 0.57129D+00 | 0.54980D+01 | 0.32116D+01 | |
| 0.24000D+00 | 0.25270D+03 | 0.84217D+02 | -0.50519Y+00 | 0.16008U+03 | -0.20090U+00 | 0.28098D+00 | 0.28308D+00 | 0.52989D+01 | 0.34847D+01 | |
| 0.25000D+00 | 0.25230D+03 | 0.84226D+02 | -0.30375D+00 | -0.21220D+00 | -0.16727D+00 | 0.29383D+00 | 0.23784D+00 | 0.74626D+00 | 0.54970D+01 | |
| 0.26000D+00 | 0.25227D+03 | 0.84235D+02 | -0.21220D+00 | 0.16727D+00 | -0.23226D+00 | 0.29383D+00 | 0.23784D+00 | 0.74626D+00 | 0.54970D+01 | |
| 0.27000D+00 | 0.25226D+03 | 0.84244D+02 | -0.18643D+00 | 0.16396D+00 | -0.24749D+00 | 0.92334D+00 | 0.74626D+00 | 0.54970D+01 | 0.33361D+01 | |
| 0.28000D+00 | 0.25227D+03 | 0.84253D+02 | -0.13431D+00 | 0.13445D+00 | -0.29969D+00 | 0.16221D+00 | 0.74626D+00 | 0.54970D+01 | 0.33326D+01 | |
| 0.29000D+00 | 0.25225D+03 | 0.84262D+02 | -0.12320D+00 | 0.13432D+00 | -0.21320D+00 | 0.16221D+00 | 0.74626D+00 | 0.54970D+01 | 0.33057D+01 | |
| 0.30000D+00 | 0.25226D+03 | 0.84267D+02 | -0.10512D+00 | 0.13512D+00 | -0.17572D+00 | 0.10924D+00 | 0.75246D+00 | 0.52886D+01 | 0.32866D+01 | |
| ALARM-P (M011(VERSION 01) DATE 77.06.30) PWR LOSS OF COOLANT ANALYSIS PROGRAM | | | | | | | | | | PAGE |
| CSNI STANDARD PROBLEM NU.5 BY ALARM-P1(M011) | | | | | | | | | | |
| TIME SEC | Avg TEMP | Avg TEMP | DIFF PRESS | DIFF PRESS | DIFF PRESS | DIFF PRESS | DIFF PRESS | DIFF PRESS | DIFF PRESS | |
| VOL 28 | C | VOL 31 | C | V 6-v 9 MPA | V 3-v 6 MPA | V 1-v10 MPA | V15-v16 MPA | V21-v26 MPA | V26-v31 MPA | V20-v31 MPA |
| 0.30000D+00 | 0.25272D+03 | 0.84316D+02 | -0.76655D+00 | 0.48235D+01 | 0.25529D+00 | 0.29331D+00 | 0.75979D+00 | 0.52907D+01 | 0.32332D+01 | |
| 0.40000D+00 | 0.25234D+03 | 0.84366D+02 | -0.11180D+01 | 0.83447D+01 | 0.33151D+01 | 0.23693D+00 | 0.57129D+00 | 0.54980D+01 | 0.32116D+01 | |
| 0.45000D+00 | 0.25237D+03 | 0.84440D+02 | -0.13624D+01 | 0.29672D+01 | -0.27252D+01 | 0.39014D+01 | 0.75450D+00 | 0.53041D+01 | 0.32116D+01 | |
| 0.50000D+00 | 0.25231D+03 | 0.84449D+02 | -0.95786D+01 | 0.64659D+01 | -0.35073D+01 | 0.45704D+01 | 0.23237D+01 | 0.53248D+01 | 0.32116D+01 | |
| 0.55000D+00 | 0.25235D+03 | 0.84493D+02 | -0.17617D+01 | 0.37657D+01 | -0.24613D+01 | 0.20507D+00 | 0.74900D+00 | 0.53011D+01 | 0.32117D+01 | |
| 0.60000D+00 | 0.25237D+03 | 0.84532D+02 | -0.16845D+01 | 0.39348D+01 | -0.26297D+01 | 0.66365D+01 | 0.74861D+00 | 0.54966D+01 | 0.32209D+01 | |
| 0.65000D+00 | 0.25234D+03 | 0.84536D+02 | -0.14746D+01 | 0.24076D+01 | -0.41102D+01 | 0.49078D+01 | 0.23114D+00 | 0.75274D+00 | 0.54950D+01 | 0.32121D+01 |
| 0.70000D+00 | 0.25231D+03 | 0.84567D+02 | -0.14746D+01 | 0.19780D+01 | -0.35228D+01 | 0.10228D+01 | 0.75274D+00 | 0.54950D+01 | 0.32121D+01 | |
| 0.75000D+00 | 0.25236D+03 | 0.84570D+02 | -0.17713D+01 | 0.19947D+01 | -0.23064D+01 | 0.29201D+01 | 0.75104D+00 | 0.54890D+01 | 0.32118D+01 | |
| 0.80000D+00 | 0.25234D+03 | 0.84574D+02 | -0.22462D+01 | 0.65162D+01 | -0.36032D+01 | 0.20407D+01 | 0.74852D+00 | 0.54955D+01 | 0.32117D+01 | |
| 0.85000D+00 | 0.25237D+03 | 0.84774D+02 | -0.13382D+01 | 0.15382D+01 | -0.40813D+00 | 0.40890D+00 | 0.15692D+00 | 0.74698D+00 | 0.52883D+01 | 0.32124D+01 |
| 0.90000D+00 | 0.25235D+03 | 0.84803D+02 | -0.13023D+01 | 0.15023D+01 | -0.65252D+00 | 0.59804D+00 | 0.15827D+00 | 0.92234D+01 | 0.52819D+01 | 0.32105D+01 |
| 0.95000D+00 | 0.25235D+03 | 0.84847D+02 | -0.10516D+01 | 0.76363D+01 | -0.33551D+01 | 0.17409D+01 | 0.75253D+00 | 0.52807D+01 | 0.32055D+01 | |
| 1.00000D+01 | 0.25237D+03 | 0.84849CD+02 | -0.90359U+01 | -0.25599U+01 | -0.15356D+02 | 0.49915D+00 | 0.75180D+00 | 0.52833D+01 | 0.32033D+01 | |
| ALARM-P (M011(VERSION 01) DATE 77.06.30) PWR LOSS OF COOLANT ANALYSIS PROGRAM | | | | | | | | | | PAGE |
| CSNI STANDARD PROBLEM NU.5 BY ALARM-P1(M011) | | | | | | | | | | |
| TIME SEC | Avg TEMP | Avg TEMP | DIFF PRESS | DIFF PRESS | DIFF PRESS | DIFF PRESS | DIFF PRESS | DIFF PRESS | DIFF PRESS | |
| VOL 2d | C | VOL 31 | C | V 6-v 9 MPA | V 3-v 6 MPA | V 1-v10 MPA | V15-v16 MPA | V21-v26 MPA | V26-v31 MPA | V20-v31 MPA |
| 0.11000D+01 | 0.25234D+03 | 0.84778D+02 | -0.10518D+00 | 0.62424D+01 | -0.31199D+00 | 0.75473D+00 | 0.52738D+01 | 0.31962D+01 | | |
| 0.12000D+01 | 0.25237D+03 | 0.85066D+02 | -0.17298D+01 | 0.47558D+01 | -0.15878D+01 | 0.71672D+01 | 0.72658D+00 | 0.52640D+01 | 0.31890D+01 | |
| 0.13000D+01 | 0.25237D+03 | 0.84513D+02 | -0.80420D+01 | 0.41457D+01 | -0.33483D+01 | 0.65250D+01 | 0.75797D+00 | 0.52692D+01 | 0.31844D+01 | |
| 0.14000D+01 | 0.25234D+03 | 0.85540D+02 | -0.11438D+01 | 0.14734D+01 | -0.12314D+01 | 0.14764D+00 | 0.75849D+00 | 0.52569D+01 | 0.31794D+01 | |
| 0.15000D+01 | 0.25237D+03 | 0.85532D+02 | -0.14331D+01 | 0.35293D+01 | -0.29179D+01 | 0.11826D+00 | 0.76403D+00 | 0.52491D+01 | 0.31792D+01 | |
| 0.16000D+01 | 0.25237D+03 | 0.85541D+02 | -0.24095D+01 | 0.25762D+01 | -0.20613D+01 | 0.21616D+00 | 0 | | | |

ALARM-P (MOD1(VERSION 01) DATE 77.06.30) PWR LOSS OF COOLANT ANALYSIS PROGRAM
 CSNI STANDARD PROBLEM NO.5 BY ALARM-P1(MOD1)

| TIME SEC | AVG TEMP VOL 28 | AVG TEMP VOL 31 | DIFF PRESS V 6-v 9 MPa | DIFF PRESS V 3-v 6 MPA | DIFF PRESS V 1-v 10 MPa | DIFF PRESS V 15-v 16 MPa | DIFF PRESS V21-v26 MPa | DIFF PRESS V24-v31 MPa | DIFF PRESS V20-v31 MPa |
|-------------|-----------------|-----------------|------------------------|------------------------|-------------------------|--------------------------|------------------------|------------------------|------------------------|
| 0.550000+01 | 0.252422D+03 | 0.887120D+02 | -0.588450D+02 | 0.104010D+01 | -0.403850D+03 | 0.736180D+01 | 0.77263D+00 | 0.51353D+01 | 0.310070D+01 |
| 0.600000+01 | 0.254300D+03 | 0.891200D+02 | -0.706900D+02 | 0.492820D+02 | 0.150350D+02 | 0.681840D+01 | 0.77483D+00 | 0.51372D+01 | 0.308310D+01 |
| 0.650000+01 | 0.254510D+03 | 0.895250D+02 | -0.826180D+02 | 0.161410D+01 | 0.221190D+02 | 0.641130D+01 | 0.76592D+00 | 0.50341D+01 | 0.30542D+01 |
| 0.700000+01 | 0.254630D+03 | 0.899250D+02 | -0.212970D+02 | 0.806700D+02 | 0.991800D+02 | 0.520870D+01 | 0.81927D+00 | 0.50391D+01 | 0.30384D+01 |
| 0.750000+01 | 0.254770D+03 | 0.903140D+02 | -0.849410D+02 | 0.883050D+02 | 0.162730D+01 | 0.135640D+01 | 0.266690D+01 | 0.81240D+00 | 0.50391D+01 |
| 0.800000+01 | 0.255060D+03 | 0.907030D+02 | -0.98239D+02 | 0.186273D+01 | 0.22326D+01 | 0.76621D+00 | 0.49911D+01 | 0.30048D+01 | 0.30542D+01 |
| 0.850000+01 | 0.255220D+03 | 0.910890D+02 | -0.140040D+02 | 0.682390D+02 | 0.18679D+01 | 0.22363D+01 | 0.77320D+00 | 0.49772D+01 | 0.29713D+01 |
| 0.900000+01 | 0.255360D+03 | 0.914880D+02 | -0.32731D+05 | 0.140710D+01 | 0.18679D+01 | 0.22363D+01 | 0.78375D+00 | 0.49527D+01 | 0.29247D+01 |
| 0.950000+01 | 0.255560D+03 | 0.918400D+02 | 0.29368D+02 | 0.10240D+01 | 0.186270D+01 | 0.17204D+01 | 0.80136D+00 | 0.48799D+01 | 0.28696D+01 |
| 0.100000+02 | 0.255910D+03 | 0.922050D+02 | 0.29471D+02 | 0.374700D+02 | 0.10088D+01 | 0.18923D+01 | 0.81753D+00 | 0.48287D+01 | 0.28049D+01 |
| 0.102000+02 | 0.256060D+03 | 0.925610D+02 | 0.25310D+02 | 0.24459D+02 | 0.213735D+01 | 0.82584D+00 | 0.47783D+01 | 0.27340D+01 | 0.27340D+01 |
| 0.110000+02 | 0.256270D+03 | 0.929090D+02 | 0.21218D+02 | 0.15963D+02 | 0.26668D+01 | 0.83450D+01 | 0.47236D+00 | 0.26596D+01 | 0.26596D+01 |
| 0.115000+02 | 0.256560D+03 | 0.93248D+02 | -0.56507D+02 | 0.17754D+02 | 0.16600D+01 | 0.34545D+00 | 0.84517D+00 | 0.46729D+01 | 0.25810D+01 |
| 0.120000+02 | 0.256870D+03 | 0.93578D+02 | -0.37482D+02 | 0.81631D+02 | -0.18476D+01 | 0.29793D+01 | 0.85426D+00 | 0.46158D+01 | 0.25036D+01 |
| 0.125000+02 | 0.256990D+03 | 0.93899D+02 | -0.33932D+02 | 0.33110D+01 | 0.14931D+01 | 0.48033D+01 | 0.86622D+00 | 0.45516D+01 | 0.24423D+01 |
| 0.130000+02 | 0.25729D+03 | 0.94211D+02 | -0.49315D+03 | 0.15067D+01 | 0.18067D+01 | 0.51330D+01 | 0.87842D+00 | 0.44797D+01 | 0.23502D+01 |
| 0.135000+02 | 0.25759D+03 | 0.94514D+02 | -0.51473D+03 | 0.90016D+02 | 0.12020D+01 | 0.60486D+01 | 0.88966D+00 | 0.44020D+01 | 0.22793D+01 |
| 0.140000+02 | 0.25771D+03 | 0.94680D+02 | 0.68367D+03 | 0.91755D+02 | 0.10548D+01 | 0.71608D+01 | 0.89881D+00 | 0.43184D+01 | 0.22422D+01 |
| 0.145000+02 | 0.25787D+03 | 0.95019D+02 | 0.14738D+02 | 0.85170D+02 | 0.93546D+02 | 0.85457D+01 | 0.90287D+00 | 0.42324D+01 | 0.21897D+01 |
| 0.150000+02 | 0.25806D+03 | 0.95367D+02 | -0.50842D+02 | 0.96370D+02 | 0.17700D+02 | 0.11194D+00 | 0.90221D+00 | 0.41648D+01 | 0.21354D+01 |
| 0.155000+02 | 0.25825D+03 | 0.95633D+02 | 0.11124D+02 | 0.77684D+02 | 0.65378D+02 | 0.17462D+00 | 0.89653D+00 | 0.40599D+01 | 0.20696D+01 |
| 0.160000+02 | 0.25840D+03 | 0.95949D+02 | 0.15762D+02 | 0.67110D+02 | 0.12247D+02 | 0.24878D+00 | 0.88595D+00 | 0.39812D+01 | 0.19413D+01 |
| 0.165000+02 | 0.25852D+03 | 0.96137D+02 | 0.14968D+02 | 0.68112D+02 | 0.10044D+01 | 0.24929D+00 | 0.87086D+00 | 0.39082D+01 | 0.18473D+01 |
| 0.170000+02 | 0.25863D+03 | 0.96379D+02 | 0.15844D+02 | 0.17173D+02 | 0.57089D+02 | 0.21272D+00 | 0.85494D+00 | 0.38379D+01 | 0.18095D+01 |
| 0.175000+02 | 0.25871D+03 | 0.96616D+02 | 0.18731D+02 | 0.73064D+02 | 0.68866D+02 | 0.17717D+00 | 0.83658D+00 | 0.37699D+01 | 0.17998D+01 |
| 0.180000+02 | 0.25876D+03 | 0.96662D+02 | 0.19521D+02 | 0.62774D+02 | 0.10112D+01 | 0.15031D+00 | 0.81575D+00 | 0.37023D+01 | 0.17866D+01 |
| 0.185000+02 | 0.25877D+03 | 0.97078D+02 | 0.19725D+02 | 0.61314D+02 | 0.90169D+02 | 0.12949D+00 | 0.80116D+00 | 0.36367D+01 | 0.17711D+01 |
| 0.190000+02 | 0.25873D+03 | 0.97302D+02 | 0.21508D+02 | 0.61787D+02 | 0.97632D+02 | 0.11565D+00 | 0.78499D+00 | 0.35697D+01 | 0.17421D+01 |
| 0.195000+02 | 0.25866D+03 | 0.97521D+02 | 0.19825D+02 | 0.38699D+02 | 0.88113D+02 | 0.10513D+00 | 0.77289D+00 | 0.34979D+01 | 0.17091D+01 |
| 0.200000+02 | 0.25561D+03 | 0.97736D+02 | 0.13301D+02 | 0.61966D+02 | 0.74773D+02 | 0.97385D+01 | 0.76002D+00 | 0.34263D+01 | 0.16739D+01 |

ALARM-P (MOD1(VERSION 01) DATE 77.06.30) PWR LOSS OF COOLANT ANALYSIS PROGRAM
 CSNI STANDARD PROBLEM NO.5 BY ALARM-P1(MOD1)

| TIME SEC | AVG TEMP VOL 28 | AVG TEMP VOL 31 | DIFF PRESS V 6-v 9 MPa | DIFF PRESS V 3-v 6 MPA | DIFF PRESS V 1-v 10 MPa | DIFF PRESS V 15-v 16 MPa | DIFF PRESS V21-v26 MPa | DIFF PRESS V24-v31 MPa | DIFF PRESS V20-v31 MPa |
|-------------|-----------------|-----------------|------------------------|------------------------|-------------------------|--------------------------|------------------------|------------------------|------------------------|
| 0.20500D+02 | 0.25180D+03 | 0.97495D+02 | 0.17773D+02 | 0.80341D+02 | 0.93560D+02 | 0.92106D+01 | 0.74483D+00 | 0.33532D+01 | 0.16353D+01 |
| 0.21000D+02 | 0.25257D+03 | 0.98144D+02 | 0.40040D+02 | 0.57103D+02 | 0.77014D+02 | 0.90503D+01 | 0.72725D+00 | 0.32778D+01 | 0.15929D+01 |
| 0.21500D+02 | 0.25310D+03 | 0.98334D+02 | 0.3741D+02 | 0.66335D+02 | 0.13351D+01 | 0.83623D+01 | 0.71533D+00 | 0.31929D+01 | 0.15443D+01 |
| 0.22000D+02 | 0.25223D+03 | 0.98539D+02 | 0.35687D+02 | 0.61363D+02 | -0.40125D+02 | 0.83048D+01 | 0.69580D+00 | 0.31243D+01 | 0.15033D+01 |
| 0.22500D+02 | 0.25243D+03 | 0.98725D+02 | 0.37420D+02 | 0.79853D+02 | 0.10658D+01 | 0.80544D+01 | 0.67773D+00 | 0.30485D+01 | 0.14598D+01 |
| 0.23000D+02 | 0.25260D+03 | 0.98906D+02 | 0.52996D+02 | 0.50081D+02 | 0.10121D+02 | 0.75809D+01 | 0.65597D+00 | 0.29712D+01 | 0.14159D+01 |
| 0.23500D+02 | 0.25265D+03 | 0.99042D+02 | 0.59942D+02 | 0.52867D+02 | 0.53024D+02 | 0.15363D+01 | 0.71682D+00 | 0.63895D+00 | 0.28917D+01 |
| 0.24000D+02 | 0.25267D+03 | 0.99251D+02 | 0.32473D+02 | 0.97237D+03 | 0.79485D+02 | 0.66318D+02 | 0.21678D+00 | 0.58945D+00 | 0.28106D+01 |
| 0.24500D+02 | 0.25274D+03 | 0.99413D+02 | 0.21446D+02 | 0.52287D+02 | 0.10874D+01 | 0.61487D+01 | 0.58945D+00 | 0.27215D+01 | 0.12744D+01 |
| 0.25000D+02 | 0.25061D+02 | 0.99570D+02 | 0.40506D+02 | 0.29469D+02 | 0.23213D+02 | 0.63973D+01 | 0.57504D+00 | 0.26234D+01 | 0.12244D+01 |
| 0.25500D+02 | 0.25022D+02 | 0.99672D+02 | 0.31546D+02 | 0.29469D+02 | 0.29496D+02 | 0.63345D+00 | 0.55040D+00 | 0.25774D+01 | 0.11778D+01 |
| 0.26000D+02 | 0.25042D+02 | 0.99866D+02 | 0.70743D+02 | 0.20959D+01 | -0.66402D+00 | 0.62622D+01 | 0.53845D+00 | 0.25013D+01 | 0.11411D+01 |
| 0.26500D+02 | 0.25059D+02 | 0.10001D+03 | 0.27592D+02 | 0.63651D+02 | 0.28769D+02 | 0.57797D+01 | 0.52553D+00 | 0.24222D+01 | 0.11014D+01 |
| 0.27000D+02 | 0.25130D+02 | 0.10140D+03 | 0.61206D+02 | 0.12472D+02 | -0.52651D+01 | 0.55674D+01 | 0.51790D+00 | 0.23366D+01 | 0.10579D+01 |
| 0.27500D+02 | 0.25174D+02 | 0.10192D+03 | 0.39882D+02 | 0.30588D+02 | 0.41630D+01 | 0.57193D+01 | 0.50792D+00 | 0.22523D+01 | 0.10132D+01 |
| 0.28000D+02 | 0.25678D+02 | 0.10194D+03 | 0.59343D+02 | 0.44484D+02 | -0.60017D+00 | 0.59488D+01 | 0.49705D+00 | 0.21678D+01 | 0.96908D+00 |
| 0.28500D+02 | 0.25545D+02 | 0.10196D+03 | 0.41093D+02 | 0.22991D+02 | 0.45197D+02 | 0.42246D+01 | 0.59663D+00 | 0.49819D+00 | 0.20814D+01 |
| 0.29000D+02 | 0.25435D+02 | 0.10198D+03 | 0.12598D+02 | 0.39132D+02 | 0.47224D+02 | 0.42246D+01 | 0.59663D+00 | 0.49819D+00 | 0.20814D+01 |
| 0.29500D+02 | 0.25479D+02 | 0.10199D+03 | 0.10410D+03 | 0.74652D+02 | 0.36581D+02 | 0.56439D+00 | 0.46650D+00 | 0.19185D+01 | 0.84349D+00 |
| 0.30000D+02 | 0.25345D+02 | 0.10087D+03 | 0.17737D+02 | 0.63121D+02 | 0.60118D+02 | 0.51145D+01 | 0.45309D+00 | 0.18413D+01 | 0.80517D+00 |
| 0.30500D+02 | 0.25379D+02 | 0.10097D+03 | 0.47660D+02 | 0.62583D+02 | 0.10464D+01 | 0.39407D+01 | 0.44038U+00 | 0.17653D+01 | 0.76457D+00 |
| 0.31000D+02 | 0.25310D+02 | 0.10107D+03 | 0.34564D+02 | 0.10214D+01 | 0.29928D+01 | 0.56631D+01 | 0.42921D+00 | 0.16936D+01 | 0.73353D+00 |
| 0.31500D+02 | 0.25294D+02 | 0.10117D+03 | 0.65945D+02 | 0.12999D+01 | 0.48198D+01 | 0.49467D+01 | 0.41363D+00 | 0.16237D+01 | 0.69960D+00 |
| 0.32000D+02 | 0.25292D+02 | 0.10120D+03 | 0.41582D+02 | 0.46353D+02 | 0.17429D+01 | 0.46353D+01 | 0.40498D+00 | 0.15610D+01 | 0.66692D+00 |
| 0.32500D+02 | 0.25287D+02 | 0.10123D+03 | 0.16027D+02 | 0.91323D+02 | -0.11778D+02 | 0.45087D+01 | 0.39412D+00 | 0.14996D+01 | 0.63552D+00 |
| 0.33000D+02 | 0.25284D+02 | 0.10140D+03 | 0.17459D+02 | 0.54542D+02 | 0.34040D+02 | 0.30403D+01 | 0.38089D+00 | 0.14333D+01 | 0.60730D+00 |
| 0.33500D+02 | 0.25282D+02 | 0.10120D+03 | 0.46329D+02 | 0.36358D+02 | -0.99856D+02 | 0.393957D+01 | 0.37074D+00 | 0.13708D+01 | 0.58016D+00 |
| 0.34000D+02 | 0.25281D+02 | 0.10104D+03 | 0.33639D+02 | 0.53095D+02 | 0.33930D+00 | 0.39890D+01 | 0.13115D+01 | 0.55337D+00 | 0.36599D+00 |
| 0.34500D+02 | 0.25280D+02 | 0.10117D+03 | 0.36332D+02 | 0.48868D+02 | 0.40468D+01 | 0.34861D+01 | 0.29787D+00 | 0.12534D+01 | 0.52787D+00 |
| 0.35000D+02 | 0.25279D+02 | 0.10117D+03 | 0.60737D+02 | 0.48767D+02 | -0.24822D+02 | 0.40382D+01 | 0.34285D+00 | 0.11979D+01 | 0.50199D+00 |
| 0.35500D+02 | 0.25279D+02 | 0.10112D+03 | 0.36967D+02 | 0.67737D+02 | 0.10012D+01 | 0.33450D+00 | 0.11443D+01 | 0.47635D+00 | 0.32947D+00 |
| 0.36000D+02 | 0.25279D+02 | 0.10118D+03 | 0.36373D+02 | 0.45231D+02 | 0.34515D+01 | 0.37487D+01 | 0.32607D+00 | 0.10936D+01 | 0.45212D+00 |
| 0.36500D+02 | 0.25276D+02 | 0.10119D+03 | 0.32299D+02 | 0.77616D+02 | 0.12527D+01 | 0.33747D+01 | 0.31712D+00 | 0.10460D+01 | 0.42915D+00 |
| 0.37000D+02 | 0.25272D+02 | 0.10120D+03 | 0.53479D+02 | 0.55500D+02 | -0.21647D+01 | 0.35478D+01 | 0.30816D+00 | 0.99896D+00 | 0.40681D+00 |
| 0.37500D+02 | 0.25263D+02 | 0.10120D+03 | | | | | | | |

ALARM-P (MUD1(VERSION 01) DATE 77.06.30) PWR LOSS OF COOLANT ANALYSIS PROGRAM
 CSNI STANDARD PROBLEM NO.5 BY ALARM-P1(MUD1)

| TIME SEC | AVG TEMP VOL 28 C | AVG TEMP VOL 31 C | V 6=V 9 MPA | V 3=V 6 MPA | V 1=V10 MPA | V15=V16 MPA | V21=V26 MPA | V26=V31 MPA | V20=V31 MPA |
|-------------|-------------------|-------------------|-------------|-------------|-------------|-------------|-------------|-------------|-------------|
| 0.455000+02 | 0.31650D+02 | 0.10274D+03 | 0.64310U-02 | 0.88299U-02 | 0.15918D-01 | 0.20962D-01 | 0.19701D+00 | 0.43037D+00 | 0.15777D+00 |
| 0.460000+02 | 0.31628D+02 | 0.10276D+03 | 0.66117U-02 | 0.92998U-02 | 0.17535D+01 | 0.20495D+01 | 0.19328D+00 | 0.40779D+00 | 0.14837D+00 |
| 0.465000+02 | 0.31609D+02 | 0.10279D+03 | 0.67973D+00 | 0.10202D+01 | 0.18830D+01 | 0.20048D+01 | 0.18867D+00 | 0.38710D+00 | 0.13999D+00 |
| 0.470000+02 | 0.31592D+02 | 0.10282D+03 | 0.71637U-02 | 0.10699D+01 | 0.19017D+01 | 0.19613D+01 | 0.18450D+00 | 0.36798D+00 | 0.13113D+00 |
| 0.475000+02 | 0.31577D+02 | 0.10284D+03 | 0.74211U-02 | 0.84176U-02 | 0.17580D+01 | 0.19142D+01 | 0.17900D+00 | 0.35018D+00 | 0.12328D+00 |
| 0.480000+02 | 0.31562D+02 | 0.10287D+03 | 0.74734U-02 | 0.65777D+02 | 0.14623D+01 | 0.18686D+01 | 0.17374D+00 | 0.33365D+00 | 0.11593D+00 |
| 0.485000+02 | 0.31549D+02 | 0.10289D+03 | 0.77376U-02 | 0.29288D+01 | 0.16227D+01 | 0.18282D+01 | 0.18826D+00 | 0.31833D+00 | 0.10905D+00 |
| 0.490000+02 | 0.31535D+02 | 0.10291D+03 | 0.81348U-02 | 0.39391D+02 | 0.17970D+01 | 0.18423D+01 | 0.16340D+00 | 0.30288D+00 | 0.10275D+00 |
| 0.495000+02 | 0.31521D+02 | 0.10294D+03 | 0.83813U-02 | 0.14042U-01 | 0.21078D+01 | 0.17788U-01 | 0.16071D+00 | 0.28717D+00 | 0.96877D+01 |
| 0.500000+02 | 0.31509D+02 | 0.10296D+03 | 0.85326U-02 | 0.10449U-01 | 0.15057D+01 | 0.15846D+01 | 0.15057D+00 | 0.27198D+00 | 0.89345D+01 |
| 0.505000+02 | 0.31498D+02 | 0.10298D+03 | 0.88249U-02 | 0.93249U-02 | 0.16131D+01 | 0.15965D+01 | 0.15534D+00 | 0.25412D+00 | 0.81168D+01 |
| 0.510000+02 | 0.31485D+02 | 0.10300D+03 | 0.88333U-02 | 0.96920U-02 | 0.23324D+01 | 0.15632D+01 | 0.15070D+00 | 0.24667D+00 | 0.74640D+01 |
| 0.515000+02 | 0.31471D+02 | 0.10301D+03 | 0.89930U-02 | 0.12820U-01 | 0.17031D+01 | 0.15684D+01 | 0.14448D+00 | 0.23574D+00 | 0.68223D+01 |
| 0.520000+02 | 0.31462D+02 | 0.10303D+03 | 0.88531U-02 | 0.10241D+01 | 0.24481D+01 | 0.15119D+01 | 0.14183D+00 | 0.22365D+00 | 0.62227D+01 |
| 0.525000+02 | 0.31451D+02 | 0.10305D+03 | 0.89099U-02 | 0.12506D+01 | 0.18110D+01 | 0.14768D+01 | 0.13970D+00 | 0.21207D+00 | 0.56687D+01 |
| 0.530000+02 | 0.31444D+02 | 0.10307D+03 | 0.88687D+02 | 0.10531D+01 | 0.19016D+01 | 0.14433D+01 | 0.13529D+00 | 0.20210D+00 | 0.51738D+01 |
| 0.535000+02 | 0.31439D+02 | 0.10309D+03 | 0.91035U-02 | 0.12036D+01 | 0.25513D+01 | 0.14097D+01 | 0.13112D+00 | 0.19219D+00 | 0.47269D+01 |
| 0.540000+02 | 0.31434D+02 | 0.10310D+03 | 0.91712U-02 | 0.11228U+01 | 0.26672D+01 | 0.13746D+01 | 0.12766U+00 | 0.18327D+00 | 0.43155D+01 |
| 0.545000+02 | 0.31411D+02 | 0.10311D+03 | 0.95523U-02 | 0.11146D+01 | 0.24542D+01 | 0.13167D+01 | 0.12454D+00 | 0.17428D+00 | 0.19307D+01 |
| 0.550000+02 | 0.31404D+02 | 0.10313D+03 | 0.95802U-02 | 0.10765U-01 | 0.25999D+01 | 0.12819D+01 | 0.12122D+00 | 0.16604D+00 | 0.35755D+01 |
| 0.555000+02 | 0.31391D+02 | 0.10314D+03 | 0.96009U-02 | 0.11871U-01 | 0.28467D+01 | 0.12433D+01 | 0.11754D+00 | 0.15867D+00 | 0.32514D+01 |
| 0.560000+02 | 0.31381D+02 | 0.10315D+03 | 0.96912U-02 | 0.11171U-01 | 0.27831D+01 | 0.12101D+01 | 0.11371D+00 | 0.15162D+00 | 0.29542D+01 |
| 0.565000+02 | 0.31371D+02 | 0.10317D+03 | 0.96339U-01 | 0.11425D+01 | 0.22036D+01 | 0.11806D+01 | 0.11001U+00 | 0.14461D+00 | 0.26783D+01 |
| 0.570000+02 | 0.31362D+02 | 0.10318D+03 | 0.96180U-01 | 0.14049U-01 | 0.19740D+01 | 0.11180D+01 | 0.10654U+00 | 0.13823D+00 | 0.24172D+01 |
| 0.575000+02 | 0.31353D+02 | 0.10319U+03 | 0.10376U-01 | 0.13067U-01 | 0.30102D+01 | 0.10985D+01 | 0.10470D+00 | 0.13054D+00 | 0.21664D+01 |
| 0.580000+02 | 0.31344D+02 | 0.10320D+03 | 0.10568U-01 | 0.14082U-01 | 0.22397U-01 | 0.10588D+01 | 0.11090D+00 | 0.11531D+00 | 0.19353D+01 |
| 0.585000+02 | 0.31334D+02 | 0.10321D+03 | 0.10538D+01 | 0.12588U-01 | 0.25589D+01 | 0.10272D+01 | 0.10848D+00 | 0.10906D+00 | 0.17169D+01 |
| 0.590000+02 | 0.31325D+02 | 0.10322D+03 | 0.10854U-01 | 0.12327D+01 | 0.23577D+01 | 0.10039D+01 | 0.10344D+00 | 0.10533D+00 | 0.14784D+01 |
| 0.595000+02 | 0.31316D+02 | 0.10324D+03 | 0.11120U-01 | 0.13686U-01 | 0.29451D+01 | 0.99254D+02 | 0.10445D+00 | 0.95808D+01 | 0.10109D+01 |
| 0.600000+02 | 0.31307D+02 | 0.10325D+03 | 0.11317U-01 | 0.13631U-01 | 0.18477D+01 | 0.93243D+02 | 0.11323D+00 | 0.79093D+01 | 0.58886D+02 |

ALARM-P (MUD1(VERSION 01) DATE 77.06.30) PWR LOSS OF COOLANT ANALYSIS PROGRAM
 CSNI STANDARD PROBLEM NO.5 BY ALARM-P1(MUD1)

| TIME SEC | DIFF PRESS VOL 2 V10-V20 MPA | DIFF PRESS VOL 7 V16-V19 MPA | PUMP SPEED VOL 7 KPM | PUMP SPEED VOL 8 KPM | MASS FLOW JUN 11 KG/SEC | MASS FLOW JUN 15 KG/SEC | MASS FLOW JUN 16 KG/SEC | MASS FLOW JUN 14 KG/SEC | MASS FLOW JUN 12 KG/SEC |
|-------------|------------------------------|------------------------------|----------------------|----------------------|-------------------------|-------------------------|-------------------------|-------------------------|-------------------------|
| 0.0 | -0.31702U-01 | 0.16944U+00 | 0.16944U+00 | 0.26840D+03 | 0.26840D+03 | 0.0 | 0.26840D+03 | 0.26840D+03 | 0.26840D+03 |
| 0.500000+02 | 0.59616D+00 | 0.16907D+00 | 0.16907D+00 | 0.28984D+03 | 0.28984D+03 | 0.76775D+00 | 0.26930D+03 | 0.21733D+03 | 0.21733D+03 |
| 0.505000+02 | 0.79236D+01 | 0.15266D+01 | 0.16889D+04 | 0.35973D+03 | 0.25963D+03 | -0.27462D+01 | 0.21949D+03 | -0.35787D+02 | |
| 0.510000+02 | 0.69302D+01 | 0.33712D+00 | 0.16834U+00 | 0.35341D+03 | 0.18127D+03 | -0.20078D+02 | 0.96529D+02 | 0.86390D+01 | |
| 0.515000+02 | 0.20000D+02 | 0.43546D+01 | 0.16800D+04 | 0.16799U-01 | 0.39757D+03 | 0.16532D+03 | 0.49034D+02 | 0.21091D+03 | 0.27876D+02 |
| 0.520000+02 | 0.25000D+02 | 0.47336D+01 | 0.16764D+01 | 0.16764U-01 | 0.38922D+03 | 0.84572D+02 | 0.19991D+03 | 0.15515D+03 | 0.14563D+03 |
| 0.525000+02 | 0.50106D+01 | 0.93557D+00 | 0.16771U-01 | 0.16771U-01 | 0.38922D+03 | 0.16764U-01 | 0.10654U+00 | 0.13823D+00 | 0.32055D+03 |
| 0.530000+02 | 0.30000D+01 | 0.90110D+01 | 0.16739U+00 | 0.16739U+00 | 0.36102D+03 | 0.17074D+02 | 0.25462D+03 | 0.32490D+03 | 0.23329D+03 |
| 0.535000+02 | 0.40000D+01 | 0.46588D+01 | 0.20386D+01 | 0.16708U-01 | 0.18708D+04 | 0.41101D+03 | 0.12340D+03 | 0.80570D+02 | |
| 0.540000+02 | 0.54346D+01 | 0.15768U-01 | 0.16672U+01 | 0.16672U+01 | 0.46422D+03 | 0.10717D+03 | 0.23842D+03 | 0.32842D+03 | 0.22605D+03 |
| 0.545000+02 | 0.54941D+01 | 0.10476D+01 | 0.16638U-01 | 0.16638U-01 | 0.17684D+03 | 0.13106D+03 | 0.24484D+03 | -0.70192D+01 | |
| 0.550000+02 | 0.59233D+01 | 0.33973D+00 | 0.16603U-04 | 0.16603U-04 | 0.12928D+03 | 0.13161D+03 | 0.18498D+03 | -0.22776D+02 | 0.12245D+04 |

ALARM-P (MUD1(VERSION 01) DATE 77.06.30) PWR LOSS OF COOLANT ANALYSIS PROGRAM
 CSNI STANDARD PROBLEM NO.5 BY ALARM-P1(MUD1)

| TIME SEC | DIFF PRESS VOL 2 V10-V20 MPA | DIFF PRESS VOL 7 V16-V19 MPA | PUMP SPEED VOL 8 KPM | MASS FLOW JUN 11 KG/SEC | MASS FLOW JUN 15 KG/SEC | MASS FLOW JUN 16 KG/SEC | MASS FLOW JUN 14 KG/SEC | MASS FLOW JUN 12 KG/SEC |
|-------------|------------------------------|------------------------------|----------------------|-------------------------|-------------------------|-------------------------|-------------------------|-------------------------|
| 0.6 | 0.21364D+01 | 0.13400D+00 | 0.16532D+04 | 0.37579D+03 | 0.17331D+03 | 0.15674D+03 | 0.33162D+03 | 0.18025D+03 |
| 0.700000+02 | 0.46634D+01 | 0.29132D+01 | 0.16464D+04 | 0.16464D+04 | 0.15822D+03 | 0.61819D+02 | 0.23265D+03 | 0.14958D+03 |
| 0.800000+02 | 0.34879D+01 | 0.64955D+00 | 0.16396D+04 | 0.35435D+03 | 0.99822D+02 | 0.39870D+02 | 0.90734D+02 | -0.53815D+01 |
| 0.900000+02 | 0.20300D+01 | 0.33046D+01 | 0.16335U+04 | 0.37818D+03 | 0.16252D+03 | 0.57867D+02 | 0.22422D+03 | 0.17666D+03 |
| 0.100000+00 | 0.42731D+01 | 0.61245D+00 | 0.16266D+04 | 0.16262D+04 | 0.38564D+03 | 0.19614D+03 | 0.93137D+02 | 0.28542D+03 |
| 0.110000+00 | 0.42921D+01 | 0.21466D+01 | 0.16199U+04 | 0.16199U+04 | 0.27190D+03 | 0.14581D+03 | 0.47895D+02 | 0.80570D+02 |
| 0.120000+00 | 0.42412D+01 | 0.23412D+01 | 0.16133U+04 | 0.16133U+04 | 0.36311D+03 | 0.12980D+03 | 0.76240D+02 | 0.18443D+03 |
| 0.130000+00 | 0.41807D+01 | 0.45178D+01 | 0.16062U+04 | 0.16062U+04 | 0.33681D+03 | 0.14000D+03 | 0.75381D+02 | 0.24377D+03 |
| 0.140000+00 | 0.14515D+01 | 0.11248D+01 | 0.16000D+04 | 0.15996U+04 | 0.26765D+03 | 0.13758D+03 | 0.56553D+02 | 0.17137D+03 |
| 0.150000+00 | 0.13304D+01 | 0.27336D+01 | 0.15933U+04 | 0.15929U+04 | 0.27713D+03 | 0.17557D+03 | 0.23163D+02 | 0.21199D+03 |
| 0.160000+00 | 0.11043D+01 | 0.23131D+00 | 0.15868U+04 | 0.15865U+04 | 0.29048D+03 | 0.16672D+03 | 0.46743D+02 | 0.22374D+03 |
| 0.170000+00 | 0.10587D+01 | 0.24577D+01 | 0.15806U+04 | 0.15799U+04 | 0.26550D+03 | 0.13577D+03 | 0.55904D+02 | 0.20901D+03 |
| 0.180000+00 | 0.11767D+01 | 0.17676D+01 | 0.15738U+04 | 0.15738U+04 | 0.17045D+03 | 0.10745D+03 | 0.56183D+02 | 0.17816D+03 |
| 0.190000+00 | 0.13636D+01 | 0.31112D+01 | 0.15674U+04 | 0.15674U+04 | 0.26222D+03 | 0.16062D+03 | 0.78321D+02 | 0.26997D+03 |
| 0.200000+00 | 0.17496D+01 | 0.29116D+01 | 0.15609U+04 | 0.15609U+04 | 0.25714D+03 | 0.66113D+02 | 0.50695D+02 | 0.16056D+03 |
| 0.210000+00 | 0.17483D+01 | 0.29117D+01 | 0.15609U+04 | 0.15541D+04 | 0.24949D+03 | 0.63674D+02 | 0.76110D+02 | 0.10371D+03 |
| 0.220000+00 | 0.19722D+01 | 0.28845D+01 | 0.15483U+04 | 0.15479U+04 | 0.28172D+03 | 0.19230D+02 | 0.12016D+03 | 0.16637D+03 |
| 0.230000+00 | 0.20320D+01 | 0.31393D+01 | 0.15422D+04 | 0.15417D+04 | 0.25676D+03 | 0.22645D+03 | 0.86066D+02 | 0.12796D+03 |
| 0.240000+00 | 0.41212D+01 | 0.32325D+01 | 0.15382D+04 | 0.15356U+04 | 0.25781D+03 | 0.26933D+02 | 0.89930D+02 | 0.12616D+03 |
| 0.250000+00 | 0.22052D+01 | 0.31029D+01 | 0.15301U+04 | 0.15296U+04 | 0.29430D+03 | 0.33643D+02 | 0.16921D+03 | 0.16067D+03 |
| 0.260000+00 | 0.22940D+01 | 0.22940D+01 | 0.15243U+04 | 0.15243U+04 | 0.30110D+03 | 0.16852D+02 | 0.72630D+02 | 0.11364D+03 |
| 0.270000+00 | 0.23355D+01 | 0.26118D+01 | 0.15189U+04 | 0.15179U+04 | 0.27933D+03 | 0.18926D+02 | 0.112228D+03 | 0.15612D+03 |
| 0.280000+00 | 0.23131D+01 | 0.31257D+01 | 0.15126U+04 | 0.15126U+04 | 0.15121D+04 | 0.13386D+01 | 0.99818U+02 | 0.13248D+03 |
| 0.290000+00 | 0.23481D+01 | 0.30277D+01 | 0.15069U+04 | 0.15063D+04 | 0.28086D+03 | 0.37648D+02 | 0.76749D+02</td | |

ALARM-P (MUD1(VERSION 01) DATE 77.06.30) PWR LOSS OF COOLANT ANALYSIS PROGRAM
CSNI STANDARD PROBLEM NO.5 BY ALARM-P1(MUD1)

| TIME SEC | DIFF PRESS | DIFF PRESS | PUMP SPEED | PUMP SPEED | MASS FLOW |
|-------------|-------------|-------------|-------------|-------------|---------------|---------------|---------------|---------------|---------------|
| | V19-V20 MPA | V16-V19 MPA | VOL 7 KHM | VOL 8 KHM | JUN 11 KG/SEC | JUN 15 KG/SEC | JUN 16 KG/SEC | JUN 14 KG/SEC | JUN 12 KG/SEC |
| 0,11000D+01 | 0,24475D+01 | 0,26926D+00 | 0,11413D+04 | 0,11408D+04 | 0,20928D+03 | -0,91050D+01 | 0,10221D+03 | 0,90120D+02 | 0,10188D+03 |
| 0,12000D+01 | 0,24502D+01 | 0,27253D+00 | 0,11085D+04 | 0,11081D+04 | 0,19834D+03 | -0,78417D+03 | 0,10267D+03 | 0,83908D+02 | 0,72461D+02 |
| 0,13000D+01 | 0,24508D+01 | 0,25684D+00 | 0,10778D+04 | 0,10774D+04 | 0,19212D+03 | -0,12185D+02 | 0,10100D+03 | 0,70950D+02 | 0,97090D+02 |
| 0,14000D+01 | 0,24546D+01 | 0,26263D+00 | 0,10488D+04 | 0,10485D+04 | 0,18970D+03 | -0,29143D+02 | 0,96381D+02 | 0,70680D+02 | 0,76065D+02 |
| 0,15000D+01 | 0,24570D+01 | 0,28102D+00 | 0,10213D+04 | 0,10209D+04 | 0,18709D+03 | -0,11688D+02 | 0,37121D+02 | 0,89927D+02 | 0,75189D+02 |
| 0,16000D+01 | 0,24587D+01 | 0,25335D+00 | 0,99490D+03 | 0,99460D+03 | 0,17886D+03 | -0,35477D+02 | 0,95382D+02 | 0,65077D+02 | 0,58752D+02 |
| 0,17000D+01 | 0,24603D+01 | 0,26253D+00 | 0,97004D+03 | 0,96984D+03 | 0,17576D+03 | -0,42680D+02 | 0,83747D+02 | 0,73284D+02 | 0,53171D+02 |
| 0,18000D+01 | 0,24619D+01 | 0,26945D+00 | 0,94652D+03 | 0,94632D+03 | 0,16693D+03 | -0,33531D+02 | 0,79208D+02 | 0,53212D+02 | 0,40840D+02 |
| 0,19000D+01 | 0,24636D+01 | 0,24085D+00 | 0,92409D+03 | 0,92391D+03 | 0,90734D+03 | -0,43109D+02 | 0,91253D+02 | 0,47733D+02 | 0,46892D+02 |
| 0,20000D+01 | 0,24655D+01 | 0,27824D+00 | 0,96251D+03 | 0,96231D+03 | 0,88219D+03 | -0,16882D+03 | 0,16618D+02 | 0,55220D+02 | 0,37023D+02 |
| 0,21000D+01 | 0,24686D+01 | 0,24606D+00 | 0,88823D+03 | 0,88803D+03 | 0,66335D+03 | -0,16795D+03 | 0,32395D+02 | 0,81793D+02 | 0,60777D+02 |
| 0,22000D+01 | 0,24683D+01 | 0,25188D+00 | 0,86347D+03 | 0,86327D+03 | 0,16031D+03 | -0,62504D+02 | 0,89492D+02 | 0,29764D+02 | 0,51277D+02 |
| 0,23000D+01 | 0,24693D+01 | 0,27692D+00 | 0,84543D+03 | 0,84523D+03 | 0,12794D+03 | -0,15954D+03 | 0,36365D+02 | 0,84609D+02 | 0,49214D+02 |
| 0,24000D+01 | 0,24715D+01 | 0,24071D+00 | 0,86289D+03 | 0,86269D+03 | 0,16059D+03 | -0,32636D+02 | 0,81644D+02 | 0,25308D+02 | 0,20970D+02 |
| 0,25000D+01 | 0,24737D+01 | 0,26237D+00 | 0,81163D+03 | 0,81143D+03 | 0,16059D+03 | -0,34517D+02 | 0,73636D+02 | 0,15238D+02 | 0,27070D+02 |
| 0,26000D+01 | 0,24747D+01 | 0,26779D+00 | 0,79571D+03 | 0,79556D+03 | 0,14969D+03 | -0,38330D+02 | 0,68846D+02 | 0,34517D+02 | 0,26307D+02 |
| 0,27000D+01 | 0,24762D+01 | 0,23931D+00 | 0,78027D+03 | 0,78019D+03 | 0,15151D+03 | -0,33189D+02 | 0,74608D+02 | 0,31392D+02 | 0,15353D+02 |
| 0,28000D+01 | 0,24778D+01 | 0,27564D+00 | 0,76559D+03 | 0,76549D+03 | 0,15151D+03 | -0,26888D+02 | 0,78180D+02 | 0,33361D+02 | 0,58975D+01 |
| 0,29000D+01 | 0,24793D+01 | 0,23210D+00 | 0,73508D+03 | 0,73508D+03 | 0,15151D+03 | -0,26988D+02 | 0,78180D+02 | 0,33361D+02 | 0,58975D+01 |
| 0,30000D+01 | 0,24808D+01 | 0,28379D+00 | 0,73216D+03 | 0,73216D+03 | 0,15151D+03 | -0,26988D+02 | 0,31168D+02 | 0,21630D+02 | 0,58975D+01 |
| 0,31000D+01 | 0,24823D+01 | 0,25279D+00 | 0,71241D+03 | 0,71241D+03 | 0,14763D+03 | -0,34357D+02 | 0,59520D+02 | 0,10252D+02 | 0,50018D+01 |
| 0,32000D+01 | 0,24838D+01 | 0,24249D+00 | 0,71171D+03 | 0,71168D+03 | 0,14392D+03 | -0,36565D+02 | 0,81514D+02 | 0,24775D+02 | 0,65739D+01 |
| 0,33000D+01 | 0,24853D+01 | 0,27197D+00 | 0,69598D+03 | 0,69598D+03 | 0,14136D+03 | -0,35996D+02 | 0,73636D+02 | 0,13308D+01 | -0,14735D+02 |
| 0,34000D+01 | 0,24868D+01 | 0,22281D+00 | 0,66881D+03 | 0,66881D+03 | 0,13678D+03 | -0,33330D+02 | 0,68211D+02 | 0,15537D+02 | 0,43355D+01 |
| 0,35000D+01 | 0,24882D+01 | 0,26654D+00 | 0,67686D+03 | 0,67686D+03 | 0,13394D+03 | -0,33707D+02 | 0,78802D+02 | 0,83554D+00 | -0,77791D+01 |
| 0,36000D+01 | 0,24897D+01 | 0,26161D+00 | 0,66657D+03 | 0,66660D+03 | 0,13084D+03 | -0,31181D+02 | 0,72727D+02 | 0,17229D+02 | -0,14686D+01 |
| 0,37000D+01 | 0,24911D+01 | 0,21880D+00 | 0,65554D+03 | 0,65554D+03 | 0,13483D+03 | -0,28751D+02 | 0,68586D+02 | 0,81465D+01 | -0,91957D+01 |
| 0,38000D+01 | 0,24926D+01 | 0,26812D+00 | 0,64552D+03 | 0,64552D+03 | 0,12741D+03 | -0,28044D+02 | 0,75967D+02 | 0,24407D+01 | -0,11944D+02 |
| 0,39000D+01 | 0,24941D+01 | 0,25995D+00 | 0,63557D+03 | 0,63557D+03 | 0,12880D+03 | -0,30565D+02 | 0,66955D+02 | 0,19198D+02 | -0,89096D+01 |
| 0,40000D+01 | 0,24953D+01 | 0,21933D+00 | 0,62255D+03 | 0,62255D+03 | 0,12780D+03 | -0,30193D+02 | 0,72175D+02 | 0,97598D+01 | -0,12626D+02 |
| 0,41000D+01 | 0,24967D+01 | 0,25958D+00 | 0,61674D+03 | 0,61658D+03 | 0,12390D+03 | -0,28173D+02 | 0,71354D+02 | 0,40206D+00 | -0,88035D+01 |
| 0,42000D+01 | 0,24981D+01 | 0,26144D+00 | 0,60863D+03 | 0,60873D+03 | 0,12214D+03 | -0,29295D+02 | 0,64970D+02 | 0,62339D+01 | -0,24014D+02 |
| 0,43000D+01 | 0,24995D+01 | 0,22486D+00 | 0,60035D+03 | 0,59951D+03 | 0,11867D+03 | -0,27658D+02 | 0,71241D+02 | 0,69782D+01 | -0,14190D+02 |
| 0,44000D+01 | 0,25008D+01 | 0,24673D+00 | 0,59522D+03 | 0,59532D+03 | 0,10447D+03 | -0,25557D+02 | 0,70671D+02 | 0,35317D+01 | -0,18401D+02 |
| 0,45000D+01 | 0,25021D+01 | 0,26262D+00 | 0,58578D+03 | 0,57579D+03 | 0,11488D+03 | -0,25023D+02 | 0,61251D+02 | 0,404028D+01 | -0,29327D+02 |
| 0,46000D+01 | 0,25034D+01 | 0,22867D+00 | 0,57683D+03 | 0,57579D+03 | 0,10558D+03 | -0,25533D+02 | 0,65625D+02 | 0,11439D+02 | -0,20908D+02 |
| 0,47000D+01 | 0,25048D+01 | 0,22660D+00 | 0,56597D+03 | 0,56583D+03 | 0,10657D+03 | -0,26655D+02 | 0,66668D+02 | 0,14128D+02 | -0,33001D+02 |
| 0,48000D+01 | 0,25060D+01 | 0,26359D+00 | 0,53626D+03 | 0,53626D+03 | 0,10657D+03 | -0,25008D+02 | 0,59885D+02 | 0,54746D+01 | -0,26352D+02 |
| 0,49000D+01 | 0,25073D+01 | 0,25295D+00 | 0,55595D+03 | 0,55452D+03 | 0,10266D+03 | -0,25008D+02 | 0,23338D+02 | 0,61102D+02 | -0,13586D+02 |
| 0,50000D+01 | 0,25086D+01 | 0,21949D+00 | 0,54951D+03 | 0,54978D+03 | 0,10189D+03 | -0,23384D+02 | 0,30471D+02 | 0,14477D+02 | -0,22903D+02 |

ALARM-P (MUD1(VERSION 01) DATE 77.06.30) PWR LOSS OF COOLANT ANALYSIS PROGRAM
CSNI STANDARD PROBLEM NO.5 BY ALARM-P1(MUD1)

| TIME SEC | DIFF PRESS | DIFF PRESS | PUMP SPEED | PUMP SPEED | MASS FLOW |
|-------------|-------------|-------------|-------------|-------------|---------------|---------------|---------------|---------------|---------------|
| | V19-V20 MPA | V16-V19 MPA | VOL 7 KHM | VOL 8 KHM | JUN 11 KG/SEC | JUN 15 KG/SEC | JUN 16 KG/SEC | JUN 14 KG/SEC | JUN 12 KG/SEC |
| 0,55000D+01 | 0,25148D+01 | 0,24122D+00 | 0,52028D+03 | 0,51179D+03 | 0,88554D+02 | -0,22880D+02 | 0,53435D+02 | -0,17680D+02 | -0,40759D+02 |
| 0,56000D+01 | 0,25210D+01 | 0,25556D+00 | 0,49524D+03 | 0,49492D+03 | 0,78205D+02 | -0,12497D+02 | -0,10310D+02 | -0,44387D+02 | |
| 0,57000D+01 | 0,25226D+01 | 0,23933D+00 | 0,47402D+03 | 0,47058D+03 | 0,70607D+04 | -0,20666D+02 | 0,51441L+01 | -0,18649D+02 | -0,48853D+02 |
| 0,58000D+01 | 0,25237D+01 | 0,23110D+00 | 0,45524D+03 | 0,45150D+03 | 0,78895D+02 | -0,25557D+02 | 0,36634D+01 | -0,52863D+02 | -0,10699D+03 |
| 0,59000D+01 | 0,25250D+01 | 0,23979D+00 | 0,43373D+03 | 0,43418D+03 | 0,76260D+02 | -0,25116D+02 | 0,38116D+01 | -0,44497D+02 | -0,10932D+03 |
| 0,60000D+01 | 0,25257D+01 | 0,23511D+00 | 0,42336D+03 | 0,41937D+03 | 0,71248D+02 | -0,28044D+02 | 0,75967D+02 | -0,24407D+01 | -0,11944D+02 |
| 0,61000D+01 | 0,25266D+01 | 0,25666D+00 | 0,40661D+03 | 0,40467D+03 | 0,69137D+03 | -0,37716D+02 | 0,38372D+02 | -0,40724D+02 | |
| 0,62000D+01 | 0,25273D+01 | 0,18725D+00 | 0,41110D+03 | 0,40467D+03 | 0,37171D+02 | -0,21320D+02 | 0,41118D+01 | -0,22264D+02 | -0,37661D+02 |
| 0,63000D+01 | 0,25280D+01 | 0,18403D+00 | 0,39970D+03 | 0,39468D+03 | 0,37171D+02 | -0,27472D+02 | 0,44225D+01 | -0,38467D+02 | -0,47767D+02 |
| 0,64000D+01 | 0,25284D+01 | 0,17956D+00 | 0,38919D+03 | 0,38460D+03 | 0,34882D+02 | -0,27224D+02 | 0,39198D+01 | -0,46682D+02 | -0,78764D+02 |
| 0,65000D+01 | 0,25287D+01 | 0,17776D+00 | 0,37970D+03 | 0,37440D+03 | 0,34549D+02 | -0,27678D+02 | 0,39340D+01 | -0,20468D+02 | -0,72226D+02 |
| 0,66000D+01 | 0,25291D+01 | 0,18413D+00 | 0,37103D+03 | 0,36356D+03 | 0,42233D+02 | -0,27848D+02 | 0,40829D+01 | -0,23353D+02 | -0,80460D+02 |
| 0,67000D+01 | 0,25298D+01 | 0,19342D+00 | 0,34912D+03 | 0,34334D+03 | 0,39464D+02 | -0,15353D+02 | 0,60871D+01 | -0,16989D+02 | -0,64009D+02 |
| 0,68000D+01 | 0,25304D+01 | 0,22537D+00 | 0,34297D+03 | 0,33731D+03 | 0,34149D+02 | -0,16319D+02 | 0,74912D+01 | -0,19777D+02 | -0,60841D+02 |
| 0,69000D+01 | 0,25314D+01 | 0,27473D+00 | 0,32204D+03 | 0,33135D+03 | 0,35298D+02 | -0,13848D+02 | 0,77318D+01 | -0,50158D+01 | -0,59733D+02 |
| 0,70000D+01 | 0,25320D+01 | 0,27293D+00 | 0,32428D+03 | 0,33208D+03 | 0,35216D+02 | -0,14792D+02 | 0,88476D+01 | -0,15653D+02 | -0,49199D+02 |
| 0,71000D+01 | 0,25324D+01 | 0,26668D+00 | 0,32438D+03 | 0,32724D+03 | 0,34684D+02 | -0,17939D+02 | 0,89416D+01 | -0,30999D+02 | -0,41631D+02 |
| 0,72000D+01 | 0,25328D+01 | 0,26282D+00 | 0,32277D+03 | 0,31657D+03 | 0,32983D+02 | -0,22979D+02 | 0,10457D+02 | -0,34743D+02 | -0,32922D+02 |
| 0,73000D+01 | 0,25330D+01 | 0,25970D+00 | 0,31842D+03 | 0,31237D+03 | 0,30943D+02 | -0,28501D+02 | 0,21235D+02 | -0,36235D+02 | -0,31710D+02 |
| 0,74000D+01 | 0,25339D+01 | 0,25110D+00 | 0,31343D+03 | 0,31488D+03 | 0,30851D+03 | -0,28170D+02 | 0,33052D+02 | 0,57154D+02 | -0,30898D+02 |
| 0,75000D+01 | 0,25342D+01 | 0,38217D+00 | 0,31141D+03 | 0,30494D+03 | 0,26963D+02 | -0,35335D+02 | 0,65113D+02 | -0,28389D+02 | -0,33208D+02 |
| 0,76000D+01 | 0,25348D+01 | 0,39247D+00 | 0,30837D+03 | 0,30181D+03 | 0,26800D+02 | -0,32664D+02 | 0,60018D+02 | -0,20319D+02 | -0,31379D+02 |
| 0,77000D+01 | 0,25352D+01 | 0,23182D+00 | 0,30566D+03 | 0,29900D+03 | 0,26052D+02 | -0,32539D+02 | 0,53636D+02 | -0,20269D+02 | -0,31379D+02 |
| 0,78000D+01 | 0,25356D+01 | 0,22994D+00 | 0,30484D+03 | 0,30329D+03 | 0,25904D+02 | -0,31577D+02 | 0,44952D+02 | -0,20852D+02 | -0,3077 |

ALARM-P (MUD1(VERSION 01) DATE 77.06.30) PWR LOSS OF COOLANT ANALYSIS PROGRAM
 CSNI STANDARD PROBLEM NO.5 BY ALARM-P(MUD1)
 TIME SEC DIFF PRESS DIFF PRESS PUMP SPEED PUMP SPEED MASS FLOW MASS FLOW MASS FLOW MASS FLOW MASS FLOW MASS FLOW
 V19~V20 MPa V16~V19 MPa VOL 7 RPM VOL 8 RPM JUN 11 KG/SEC JUN 15 KG/SEC JUN 16 KG/SEC JUN 14 KG/SEC JUN 12 KG/SEC

| | | | | | | | | | |
|-------------|-------------|-------------|-------------|-------------|--------------|--------------|-------------|--------------|--------------|
| 0.20000D+02 | 0.21443D+01 | 0.29647D+00 | 0.28868D+03 | 0.23386D+02 | -0.11426D+02 | 0.28411D+02 | 0.17009D+02 | -0.17131D+02 | |
| 0.21000D+02 | 0.21061D+01 | 0.24008D+00 | 0.29672D+03 | 0.28869D+03 | 0.15936D+02 | -0.10261D+02 | 0.28061D+02 | 0.18978D+02 | -0.18270D+02 |
| 0.21400D+02 | 0.20455D+01 | 0.23221D+00 | 0.29965D+03 | 0.29146D+03 | 0.32631D+01 | -0.10591D+02 | 0.29424D+02 | 0.14222D+02 | -0.28937D+02 |
| 0.22000D+02 | 0.20242D+01 | 0.22791D+00 | 0.30124D+03 | 0.29291D+03 | 0.10349D+02 | -0.15975D+02 | 0.26889D+02 | 0.15284D+02 | -0.14051D+02 |
| 0.22500D+02 | 0.19835D+01 | 0.22191D+00 | 0.30227D+03 | 0.29348D+03 | 0.18222D+02 | -0.13756D+02 | 0.26045D+02 | 0.92458D+01 | -0.20181D+02 |
| 0.23000D+02 | 0.19415D+01 | 0.21480D+00 | 0.30414D+03 | 0.29567D+03 | 0.10758D+02 | -0.10292D+02 | 0.25274D+02 | 0.10734D+02 | -0.22342D+02 |
| 0.23500D+02 | 0.18974D+01 | 0.20799D+00 | 0.30679D+03 | 0.29828D+03 | -0.19103D+01 | -0.11932D+02 | 0.22830D+02 | 0.86157D+01 | -0.21806D+02 |
| 0.24000D+02 | 0.18501D+01 | 0.19990D+00 | 0.31001D+03 | 0.30142D+03 | -0.14144D+01 | -0.14904D+02 | 0.19785D+02 | 0.62988D+01 | -0.26263D+02 |
| 0.24500D+02 | 0.18002D+01 | 0.19221D+00 | 0.31341D+03 | 0.30475D+03 | -0.90519D+01 | -0.13415D+02 | 0.17479D+02 | 0.33056D+01 | -0.26866D+02 |
| 0.25000D+02 | 0.17478D+01 | 0.18337D+00 | 0.31661D+03 | 0.30796D+03 | -0.13550D+02 | -0.26086D+01 | 0.18413D+02 | -0.56340D+01 | -0.28910D+02 |
| 0.25500D+02 | 0.17079D+01 | 0.18761D+00 | 0.31764D+03 | 0.30495D+03 | -0.30337D+02 | -0.20744D+02 | 0.16526D+02 | -0.24988D+02 | -0.26784D+02 |
| 0.26000D+02 | 0.16689D+01 | 0.18689D+00 | 0.31764D+03 | 0.30848D+03 | 0.14033D+02 | -0.16828D+02 | 0.17035D+02 | 0.52749D+01 | -0.14535D+02 |
| 0.26500D+02 | 0.16297D+01 | 0.17643D+00 | 0.31770D+03 | 0.30889D+03 | 0.54171D+02 | -0.23614D+02 | 0.15937D+02 | -0.46295D+01 | -0.15828D+02 |
| 0.27000D+02 | 0.15841D+01 | 0.16801D+00 | 0.31855D+03 | 0.30970D+03 | 0.10288D+02 | 0.18571D+02 | 0.15252D+02 | 0.76935D+01 | -0.96565D+01 |
| 0.27500D+02 | 0.15353D+01 | 0.16547D+00 | 0.32025D+03 | 0.31137D+03 | 0.20400D+02 | -0.14111D+02 | 0.17445D+02 | 0.88155D+01 | -0.11344D+02 |
| 0.28000D+02 | 0.14854D+01 | 0.16437D+00 | 0.32244D+03 | 0.31590D+03 | 0.28882D+02 | -0.72103D+01 | 0.17808D+02 | 0.78376D+01 | -0.12266D+02 |
| 0.28500D+02 | 0.14363D+01 | 0.16276D+00 | 0.32516D+03 | 0.31616D+03 | 0.20334D+02 | -0.90211D+01 | 0.17179D+02 | 0.57344D+01 | -0.14123D+02 |
| 0.29000D+02 | 0.13894D+01 | 0.15934D+00 | 0.32819D+03 | 0.31919D+03 | 0.38092D+02 | -0.86588D+02 | 0.16543D+02 | 0.61998D+01 | -0.15224D+02 |
| 0.29500D+02 | 0.13453D+01 | 0.15523D+00 | 0.33157D+03 | 0.32255D+03 | 0.36687D+02 | -0.66222D+02 | 0.14617D+02 | 0.28013D+01 | -0.14583D+02 |
| 0.30000D+02 | 0.13039D+01 | 0.14893D+00 | 0.33356D+03 | 0.32632D+03 | 0.31720D+02 | -0.81877D+01 | 0.85183D+01 | -0.13197D+02 | |
| 0.30500D+02 | 0.12611D+01 | 0.15142D+00 | 0.33920D+03 | 0.33019D+03 | 0.62778D+02 | -0.35093D+01 | 0.14447D+02 | -0.31843D+01 | -0.21198D+02 |
| 0.31000D+02 | 0.12202D+01 | 0.15345D+00 | 0.34314D+03 | 0.33408D+03 | 0.40123D+02 | -0.63029D+01 | 0.13102D+02 | -0.22150D+01 | -0.26860D+02 |
| 0.31500D+02 | 0.11797D+01 | 0.15610D+00 | 0.34676D+03 | 0.33772D+03 | 0.47829D+02 | -0.34420D+01 | 0.15592D+02 | 0.13744D+02 | -0.28133D+02 |
| 0.32000D+02 | 0.11394D+01 | 0.15127D+00 | 0.35032D+03 | 0.34413D+03 | 0.29851D+02 | -0.33427D+01 | 0.14324D+02 | 0.97108D+01 | -0.11350D+02 |
| 0.32500D+02 | 0.10969D+01 | 0.15267D+00 | 0.35435D+03 | 0.34535D+03 | 0.17342D+02 | -0.29848D+01 | 0.10380D+02 | 0.14633D+02 | 0.53834D+02 |
| 0.33000D+02 | 0.10609D+01 | 0.15879D+00 | 0.35834D+03 | 0.34993D+03 | 0.39127D+02 | -0.27250D+00 | 0.11995D+02 | 0.18550D+02 | 0.39191D+02 |
| 0.33500D+02 | 0.10217D+01 | 0.15518D+00 | 0.36187D+03 | 0.35280D+03 | 0.25632D+02 | -0.50254D+00 | 0.12600D+02 | 0.17140D+02 | 0.28753D+02 |
| 0.34000D+02 | 0.98184D+00 | 0.11105D+00 | 0.36364D+03 | 0.35666D+03 | 0.37666D+02 | -0.37266D+00 | 0.11550D+02 | 0.17734D+02 | 0.17338D+02 |
| 0.34500D+02 | 0.94196D+00 | 0.10907D+00 | 0.36900D+03 | 0.35997D+03 | 0.46430D+02 | -0.32745D+02 | 0.11453D+02 | 0.14685D+02 | 0.20060D+02 |
| 0.35000D+02 | 0.90424D+00 | 0.10631D+00 | 0.37261D+03 | 0.36357D+03 | 0.25950D+02 | 0.61225D+00 | 0.11484D+02 | 0.13263D+02 | 0.22432D+02 |
| 0.35500D+02 | 0.87085D+00 | 0.10398D+00 | 0.37626D+03 | 0.36723D+03 | 0.45724D+02 | 0.10039D+01 | 0.10463D+02 | 0.11418D+02 | 0.23571D+02 |
| 0.36000D+02 | 0.84037D+00 | 0.99567D+00 | 0.37982D+03 | 0.37078D+03 | 0.39867D+02 | 0.19503D+01 | 0.10872D+02 | 0.12030D+02 | 0.74857D+01 |
| 0.36500D+02 | 0.81213D+00 | 0.95748D+00 | 0.38300D+03 | 0.37396D+03 | 0.40728D+02 | 0.21621D+01 | 0.89894D+01 | 0.11995D+02 | -0.79256D+01 |
| 0.37000D+02 | 0.78385D+00 | 0.93862D+00 | 0.38621D+03 | 0.37717D+03 | 0.38991D+02 | -0.15504D+01 | 0.89694D+01 | 0.16275D+02 | -0.39238D+01 |
| 0.37500D+02 | 0.75554D+00 | 0.91115D+00 | 0.38977D+03 | 0.38074D+03 | 0.40319D+02 | 0.93140D+01 | 0.95609D+01 | 0.11218D+02 | -0.39247D+00 |
| 0.38000D+02 | 0.72810D+00 | 0.88473D+00 | 0.39373D+03 | 0.38471D+03 | 0.40334D+02 | 0.17713D+01 | 0.93485D+01 | 0.10845D+02 | -0.86044D+00 |
| 0.38500D+02 | 0.70124D+00 | 0.84871D+00 | 0.39824D+03 | 0.38932D+03 | 0.41312D+02 | 0.18789D+01 | 0.90018D+01 | 0.10718D+02 | -0.58852D+01 |
| 0.39000D+02 | 0.67559D+00 | 0.81766D+00 | 0.40319D+03 | 0.39919D+03 | 0.47100D+02 | 0.20582D+01 | 0.86938D+01 | 0.10579D+02 | 0.43678D+01 |
| 0.39500D+02 | 0.64988D+00 | 0.78838D+00 | 0.40851D+03 | 0.39952D+03 | 0.42837D+02 | 0.21093D+01 | 0.83785D+01 | 0.10507D+02 | 0.63463D+01 |
| 0.40000D+02 | 0.62626D+00 | 0.76016D+00 | 0.41418D+03 | 0.40521D+03 | 0.43400D+02 | 0.20311D+01 | 0.80350D+01 | 0.10114D+02 | 0.53993D+01 |
| 0.40500D+02 | 0.60323D+00 | 0.73189D+00 | 0.42016D+03 | 0.41121D+03 | 0.44107D+02 | 0.21775D+01 | 0.77896D+01 | 0.99667D+01 | 0.78882D+01 |
| 0.41000D+02 | 0.58112D+00 | 0.70445D+00 | 0.42667D+03 | 0.41754D+03 | 0.44773D+02 | 0.24208D+01 | 0.75622D+01 | 0.98283D+01 | 0.91276D+01 |
| 0.41500D+02 | 0.55956D+00 | 0.67683D+00 | 0.43317D+03 | 0.42426D+03 | 0.45181D+02 | 0.23867D+01 | 0.73218D+01 | 0.97911D+01 | 0.11026D+02 |
| 0.42000D+02 | 0.53889D+00 | 0.64548D+00 | 0.44016D+03 | 0.43127D+03 | 0.45571D+02 | 0.28967D+01 | 0.71415D+01 | 0.99110D+01 | 0.14161D+02 |
| 0.42500D+02 | 0.51895D+00 | 0.61323D+00 | 0.44751D+03 | 0.43864D+03 | 0.46094D+02 | 0.28464D+01 | 0.69916D+01 | 0.10045D+02 | 0.14486D+02 |
| 0.43000D+02 | 0.49975D+00 | 0.61108D+00 | 0.45516D+03 | 0.44631D+03 | 0.46252D+02 | 0.28194D+01 | 0.68400D+01 | 0.10228D+02 | 0.15308D+02 |
| 0.43500D+02 | 0.48144D+00 | 0.59108D+00 | 0.46307D+03 | 0.45524D+03 | 0.46593D+02 | 0.29480D+01 | 0.67230D+01 | 0.10518D+02 | 0.16426D+02 |
| 0.44000D+02 | 0.46339D+00 | 0.57116D+00 | 0.47130D+03 | 0.46224D+03 | 0.46851D+02 | 0.30270D+01 | 0.66116D+01 | 0.10801D+02 | 0.16031D+02 |
| 0.44500D+02 | 0.44717D+00 | 0.55359D+00 | 0.47978D+03 | 0.47098D+03 | 0.47195D+02 | 0.31481D+01 | 0.65331D+01 | 0.11160D+02 | 0.16845D+02 |
| 0.45000D+02 | 0.43124D+00 | 0.53628D+00 | 0.48658D+03 | 0.47980D+03 | 0.47415D+02 | 0.34432D+01 | 0.64729D+01 | 0.11531D+02 | 0.16005D+02 |

ALARM-P (MUD1(VERSION 01) DATE 77.06.30) PWR LOSS OF COOLANT ANALYSIS PROGRAM
 CSNI STANDARD PROBLEM NO.5 BY ALARM-P(MUD1)
 TIME SEC DIFF PRESS DIFF PRESS PUMP SPEED PUMP SPEED MASS FLOW MASS FLOW MASS FLOW MASS FLOW MASS FLOW MASS FLOW
 V19~V20 MPa V16~V19 MPa VOL 7 RPM VOL 8 RPM JUN 11 KG/SEC JUN 15 KG/SEC JUN 16 KG/SEC JUN 14 KG/SEC JUN 12 KG/SEC

| | | | | | | | | | |
|-------------|-------------|-------------|-------------|-------------|---------------|-------------|-------------|-------------|--------------|
| 0.45500D+02 | 0.51951D+01 | 0.49778D+03 | 0.48690D+03 | 0.47658D+02 | 0.35045D+01 | 0.64097D+01 | 0.11840D+02 | 0.15639D+02 | |
| 0.46000D+02 | 0.50383D+01 | 0.50724D+03 | 0.49485D+03 | 0.47793D+02 | 0.37352D+01 | 0.63681D+01 | 0.12294D+02 | 0.17483D+02 | |
| 0.46500D+02 | 0.38721D+00 | 0.48871D+01 | 0.51703D+03 | 0.50830D+03 | 0.47966D+02 | 0.43024D+01 | 0.63671D+01 | 0.12679D+02 | 0.18065D+02 |
| 0.47000D+02 | 0.37374D+00 | 0.47429D+01 | 0.52713D+03 | 0.51843D+03 | 0.48040D+02 | 0.45264D+01 | 0.63522D+01 | 0.13049D+02 | 0.17598D+02 |
| 0.47500D+02 | 0.36083D+00 | 0.46616D+01 | 0.53775D+03 | 0.52886D+03 | 0.48060D+02 | 0.45838D+01 | 0.63359D+01 | 0.13382D+02 | 0.16961D+02 |
| 0.48000D+02 | 0.35884D+00 | 0.46467D+01 | 0.54682D+03 | 0.53960D+03 | 0.48182D+02 | 0.49989D+01 | 0.63190D+01 | 0.13715D+02 | 0.17807D+02 |
| 0.48500D+02 | 0.33348D+00 | 0.43171D+01 | 0.55923D+03 | 0.55058D+03 | 0.48263D+02 | 0.49546D+01 | 0.63050D+01 | 0.13958D+02 | 0.18110D+02 |
| 0.49000D+02 | 0.32512D+00 | 0.42894D+01 | 0.57045D+03 | 0.56181D+03 | 0.48545D+02 | 0.25954D+01 | 0.63827D+01 | 0.13885D+02 | 0.11911D+02 |
| 0.49500D+02 | 0.31424D+00 | 0.41110D+01 | 0.58184D+03 | 0.57320D+03 | 0.49862D+02 | 0.15919D+01 | 0.57139D+01 | 0.11596D+02 | 0.97619D+01 |
| 0.50000D+02 | 0.30711D+00 | 0.39438D+01 | 0.59567D+03 | 0.58623D+03 | 0.49383D+02 | 0.49293D+01 | 0.59094D+01 | 0.11669D+02 | -0.30559D+01 |
| 0.50500D+02 | 0.30295D+00 | 0.38280D+01 | 0.60646D+03 | 0.59786D+03 | 0.49809D+02 | 0.59539D+01 | 0.60095D+01 | 0.13625D+02 | 0.32325D+02 |
| 0.51000D+02 | 0.29121D+00 | 0.37369D+01 | 0.61825D+03 | 0.60966D+03 | 0.49381D+02 | 0.64550D+01 | 0.61310D+01 | 0.14510D+02 | 0.41822D+02 |
| 0.51500D+02 | 0.28338D+00 | 0.36534D+01 | 0.63085D+03 | 0.62206D+03 | 0.49833D+02 | 0.71433D+01 | 0.62021D+01 | 0.15169D+02 | 0.14083D+02 |
| 0.52000D+02 | 0.27556D+00 | 0.35516D+01 | 0.64394D+03 | 0.63488D+03 | 0.49835D+02 | 0.68374D+01 | 0.58670D+01 | 0.13392D+02 | -0.16457D+01 |
| 0.52500D+02 | 0.26880D+00 | 0.34667D+01 | 0.65598D+03 | 0.64745D+03 | 0.49808D+02 | 0.67515D+01 | 0.59367D+01 | 0.14713D+02 | 0.17639D+02 |
| 0.53000D+02 | 0.26041D+00 | 0.33749D+01 | 0.66852D+03 | 0.66000U+03 | 0.49814D+02</ | | | | |

ALARM-P (MOD1/VERSION 01) DATE 77.06.30 PWR LOSS OF COOLANT ANALYSIS PROGRAM
 CSNI STANDARD PROBLEM NO.5 BY ALARM-P1(MOD1)

TIME SEC MASS FLOW MASS FLOW MASS FLOW VOLUME FLOW VOLUME FLOW VOLUME FLOW

JUN 2 KG/SEC JUN 2 KG/SEC JUN 24 KG/SEC JUN 33 L/SEC JUN 34 L/SEC JUN 35 L/SEC

| | | | | | | |
|------------|-------------|-------------|-------------|--------------|-----|-----|
| 0.0 | 0.26840D+03 | 0.26840D+03 | 0.0 | 0.0 | 0.0 | 0.0 |
| 0.5000D+02 | 0.26837D+03 | 0.26835D+03 | 0.36239D+03 | 0.10259D+01 | 0.0 | 0.0 |
| 1.0000D+01 | 0.26779D+03 | 0.26973D+03 | 0.21447D+03 | 0.20092D+01 | 0.0 | 0.0 |
| 1.5000D+01 | 0.23907D+03 | 0.30829D+03 | 0.53364D+03 | 0.29091D+01 | 0.0 | 0.0 |
| 2.0000D+01 | 0.15160D+03 | 0.37615D+03 | 0.31428D+03 | 0.36885D+01 | 0.0 | 0.0 |
| 2.5000D+01 | 0.12693D+03 | 0.35094D+03 | 0.36721D+03 | 0.43144D+01 | 0.0 | 0.0 |
| 3.0000D+01 | 0.93668D+02 | 0.33226D+03 | 0.15952D+03 | 0.47622D+01 | 0.0 | 0.0 |
| 3.5000D+01 | 0.10201D+03 | 0.25874D+03 | 0.13241D+03 | 0.50121D+01 | 0.0 | 0.0 |
| 4.0000D+01 | 0.15549D+03 | 0.26578D+03 | 0.30524D+03 | 0.50542D+01 | 0.0 | 0.0 |
| 4.5000D+01 | 0.18920D+03 | 0.26550D+03 | 0.38595D+03 | 0.48867D+01 | 0.0 | 0.0 |
| 5.0000D+01 | 0.21343D+03 | 0.34670D+03 | 0.30446D+03 | 0.45167D+01 | 0.0 | 0.0 |
| 0.6000D+01 | 0.19899D+03 | 0.28224D+03 | 0.22218D+03 | 0.32393D+01 | 0.0 | 0.0 |
| 0.7000D+01 | 0.19178D+03 | 0.25628D+03 | 0.29546D+03 | 0.14303D+01 | 0.0 | 0.0 |
| 0.8000D+01 | 0.17349D+03 | 0.39949D+03 | 0.28215D+03 | -0.41904D+02 | 0.0 | 0.0 |
| 0.9000D+01 | 0.17822D+03 | 0.28628D+03 | 0.25911D+03 | -0.17465D+01 | 0.0 | 0.0 |
| 1.0000D+01 | 0.20570D+03 | 0.21877D+03 | 0.22916D+03 | -0.27872D+01 | 0.0 | 0.0 |
| 1.1000D+01 | 0.19089D+03 | 0.35394D+03 | 0.22036D+03 | -0.33701D+01 | 0.0 | 0.0 |
| 1.2000D+01 | 0.20198D+03 | 0.23955D+03 | 0.22585D+03 | -0.33997D+01 | 0.0 | 0.0 |
| 1.3000D+01 | 0.17734D+03 | 0.25929D+03 | 0.19444D+03 | 0.28711D+01 | 0.0 | 0.0 |
| 1.4000D+01 | 0.20509D+03 | 0.30850D+03 | 0.16129D+03 | -0.18712D+01 | 0.0 | 0.0 |
| 1.5000D+01 | 0.23714D+03 | 0.23576D+03 | 0.22212D+03 | 0.56400D+02 | 0.0 | 0.0 |
| 1.6000D+01 | 0.24268D+03 | 0.21988D+03 | 0.12517D+03 | 0.12227D+01 | 0.0 | 0.0 |
| 1.7000D+01 | 0.21936D+03 | 0.26123D+03 | 0.93666D+02 | 0.30706D+01 | 0.0 | 0.0 |
| 1.8000D+01 | 0.25117D+03 | 0.27779D+03 | 0.40298D+02 | 0.44142D+01 | 0.0 | 0.0 |
| 1.9000D+01 | 0.25988D+03 | 0.28385D+03 | 0.89330D+02 | 0.50331D+01 | 0.0 | 0.0 |
| 2.0000D+01 | 0.26848D+03 | 0.26889D+03 | 0.93043D+02 | 0.48259D+01 | 0.0 | 0.0 |
| 2.1000D+01 | 0.29233D+03 | 0.24843D+03 | 0.12242D+03 | 0.38266D+01 | 0.0 | 0.0 |
| 2.2000D+01 | 0.29022D+03 | 0.24210D+03 | 0.14443D+03 | 0.21994D+01 | 0.0 | 0.0 |
| 2.3000D+01 | 0.28972D+03 | 0.27279D+03 | 0.14761D+03 | 0.21120D+02 | 0.0 | 0.0 |
| 2.4000D+01 | 0.22463D+03 | 0.30612D+03 | 0.14611D+03 | -0.12378D+01 | 0.0 | 0.0 |
| 2.5000D+01 | 0.20631D+03 | 0.26075D+03 | 0.14664D+03 | 0.24165D+01 | 0.0 | 0.0 |
| 2.6000D+01 | 0.18324D+03 | 0.26744D+03 | 0.15023D+03 | -0.31959D+01 | 0.0 | 0.0 |
| 2.7000D+01 | 0.16727D+03 | 0.28247D+03 | 0.16382D+03 | 0.34552D+01 | 0.0 | 0.0 |
| 2.8000D+01 | 0.14159D+03 | 0.29295D+03 | 0.17316D+03 | -0.31446D+01 | 0.0 | 0.0 |
| 2.9000D+01 | 0.13069D+03 | 0.27866D+03 | 0.17414D+03 | 0.23177D+01 | 0.0 | 0.0 |
| 3.0000D+01 | 0.12737D+03 | 0.24699D+03 | 0.17525D+03 | -0.11104D+01 | 0.0 | 0.0 |

ALARM-P (MOD1/VERSION 01) DATE 77.06.30 PWR LOSS OF COOLANT ANALYSIS PROGRAM
 CSNI STANDARD PROBLEM NO.5 BY ALARM-P1(MOD1)

TIME SEC MASS FLOW MASS FLOW MASS FLOW VOLUME FLOW VOLUME FLOW VOLUME FLOW

JUN 2 KG/SEC JUN 2 KG/SEC JUN 24 KG/SEC JUN 33 L/SEC JUN 34 L/SEC JUN 35 L/SEC

| | | | | | | |
|------------|-------------|-------------|-------------|--------------|-----|-----|
| 0.3500D+00 | 0.16213D+03 | 0.27323D+03 | 0.17703D+03 | 0.50052D+01 | 0.0 | 0.0 |
| 0.4000D+00 | 0.89123D+02 | 0.24949D+03 | 0.17231D+03 | -0.19811D+01 | 0.0 | 0.0 |
| 0.4500D+00 | 0.12444D+03 | 0.23999D+03 | 0.16113D+03 | -0.16266D+01 | 0.0 | 0.0 |
| 0.5000D+00 | 0.83990D+02 | 0.23414D+03 | 0.15265D+03 | 0.50526D+01 | 0.0 | 0.0 |
| 0.5500D+00 | 0.78232D+02 | 0.23570D+03 | 0.15181D+03 | -0.14943D+01 | 0.0 | 0.0 |
| 0.6000D+00 | 0.11012D+03 | 0.23382D+03 | 0.15733D+03 | 0.20991D+01 | 0.0 | 0.0 |
| 0.6500D+00 | 0.66346D+02 | 0.21723D+03 | 0.16268D+03 | 0.49658D+01 | 0.0 | 0.0 |
| 0.7000D+00 | 0.53763D+02 | 0.22666D+03 | 0.16116D+03 | -0.96830D+02 | 0.0 | 0.0 |
| 0.7500D+00 | 0.87718D+02 | 0.22324D+03 | 0.15737D+03 | -0.25154D+01 | 0.0 | 0.0 |
| 0.8000D+00 | 0.90938D+02 | 0.21525D+03 | 0.19414D+03 | 0.47871D+01 | 0.0 | 0.0 |
| 0.8500D+00 | 0.57566D+02 | 0.20242D+03 | 0.14538D+03 | -0.41698D+02 | 0.0 | 0.0 |
| 0.9000D+00 | 0.91671D+02 | 0.21191D+03 | 0.15518D+03 | 0.28645D+01 | 0.0 | 0.0 |
| 0.9500D+00 | 0.51619D+02 | 0.21764D+03 | 0.16141D+03 | 0.44024D+01 | 0.0 | 0.0 |
| 1.0000D+01 | 0.63150D+02 | 0.20441D+03 | 0.19648D+03 | 0.21213D+02 | 0.0 | 0.0 |

ALARM-P (MOD1/VERSION 01) DATE 77.06.30 PWR LOSS OF COOLANT ANALYSIS PROGRAM
 CSNI STANDARD PROBLEM NO.5 BY ALARM-P1(MOD1)

TIME SEC MASS FLOW MASS FLOW MASS FLOW VOLUME FLOW VOLUME FLOW VOLUME FLOW

JUN 2 KG/SEC JUN 2 KG/SEC JUN 24 KG/SEC JUN 33 L/SEC JUN 34 L/SEC JUN 35 L/SEC

| | | | | | | |
|-------------|-------------|-------------|-------------|--------------|-----|-----|
| 0.11000D+01 | 0.61149D+02 | 0.25186D+02 | 0.14342D+03 | 0.39401U+00 | 0.0 | 0.0 |
| 0.12000D+01 | 0.50170D+02 | 0.20904D+02 | 0.15741D+03 | -0.33252D+01 | 0.0 | 0.0 |
| 0.13000D+01 | 0.36217D+02 | 0.19441D+02 | 0.15335D+03 | 0.18148D+01 | 0.0 | 0.0 |
| 0.14000D+01 | 0.33597D+02 | 0.19193D+02 | 0.14331D+03 | 0.27208D+01 | 0.0 | 0.0 |
| 0.15000D+01 | 0.30990D+02 | 0.18313D+02 | 0.16152D+03 | -0.34350D+01 | 0.0 | 0.0 |
| 0.16000D+01 | 0.24809D+02 | 0.17698D+02 | 0.15154D+03 | 0.32234D+01 | 0.0 | 0.0 |
| 0.17000D+01 | 0.25799D+02 | 0.17077D+02 | 0.14469U+03 | 0.12169D+01 | 0.0 | 0.0 |
| 0.18000D+01 | 0.28595D+02 | 0.15631D+02 | 0.16198U+03 | 0.31826D+01 | 0.0 | 0.0 |
| 0.19000D+01 | 0.23833D+02 | 0.15912D+02 | 0.14758U+03 | 0.42899U+01 | 0.0 | 0.0 |
| 0.20000D+01 | 0.24222D+02 | 0.16130D+02 | 0.15038U+03 | 0.28292U+02 | 0.0 | 0.0 |
| 0.21000D+01 | 0.26650D+02 | 0.16165D+02 | 0.15725D+03 | -0.25951D+01 | 0.0 | 0.0 |
| 0.22000D+01 | 0.25046D+02 | 0.13817D+02 | 0.14773D+03 | 0.49024D+01 | 0.0 | 0.0 |
| 0.23000D+01 | 0.25583D+02 | 0.13439D+02 | 0.15392D+03 | -0.13638D+01 | 0.0 | 0.0 |
| 0.24000D+01 | 0.21799D+02 | 0.14607D+02 | 0.15163D+03 | -0.17349D+01 | 0.0 | 0.0 |
| 0.25000D+01 | 0.25130D+02 | 0.13295D+02 | 0.15781D+03 | -0.49972D+01 | 0.0 | 0.0 |
| 0.26000D+01 | 0.22310D+02 | 0.14001D+02 | 0.15293D+03 | 0.23000D+01 | 0.0 | 0.0 |
| 0.27000D+01 | 0.22885D+02 | 0.12600D+02 | 0.15316D+03 | -0.69332D+02 | 0.0 | 0.0 |
| 0.28000D+01 | 0.23188D+02 | 0.11616D+02 | 0.15362D+03 | 0.45652D+01 | 0.0 | 0.0 |
| 0.29000D+01 | 0.22130D+02 | 0.11094D+02 | 0.15221D+03 | -0.29921D+01 | 0.0 | 0.0 |
| 0.30000D+01 | 0.22677D+02 | 0.10447D+02 | 0.15675D+03 | 0.61409D+02 | 0.0 | 0.0 |
| 0.31000D+01 | 0.21084D+02 | 0.10167D+02 | 0.15128D+03 | 0.36527D+01 | 0.0 | 0.0 |
| 0.32000D+01 | 0.20313D+02 | 0.10274D+02 | 0.15714D+03 | -0.33675D+01 | 0.0 | 0.0 |
| 0.33000D+01 | 0.20689D+02 | 0.91131D+02 | 0.15612D+03 | 0.21734D+01 | 0.0 | 0.0 |
| 0.34000D+01 | 0.18797D+02 | 0.93618D+02 | 0.15596D+03 | 0.23567D+01 | 0.0 | 0.0 |
| 0.35000D+01 | 0.19607D+02 | 0.83295D+02 | 0.15386D+03 | -0.33873D+01 | 0.0 | 0.0 |
| 0.36000D+01 | 0.19232D+02 | 0.84263D+02 | 0.15663D+03 | 0.35047D+01 | 0.0 | 0.0 |
| 0.37000D+01 | 0.19055D+02 | 0.83686D+02 | 0.15346D+03 | 0.81455D+02 | 0.0 | 0.0 |
| 0.38000D+01 | 0.19633D+02 | 0.73272D+02 | 0.15701D+03 | -0.30494D+01 | 0.0 | 0.0 |
| 0.39000D+01 | 0.17529D+02 | 0.78403D+02 | 0.15436D+03 | 0.44662D+01 | 0.0 | 0.0 |
| 0.40000D+01 | 0.18379D+02 | 0.73949D+02 | 0.15245D+03 | -0.55400D+02 | 0.0 | 0.0 |
| 0.41000D+01 | 0.17333D+02 | 0.66414D+02 | 0.15629D+03 | -0.23915D+01 | 0.0 | 0.0 |
| 0.42000D+01 | 0.16588D+02 | 0.70695D+02 | 0.15355D+03 | 0.49482D+01 | 0.0 | 0.0 |
| 0.43000D+01 | 0.18177D+02 | 0.65237D+02 | 0.15783D+03 | -0.16042D+01 | 0.0 | 0.0 |
| 0.44000D+01 | 0.16518D+02 | 0.61226D+02 | 0.15163D+03 | -0.14821D+01 | 0.0 | 0.0 |
| 0.45000D+01 | 0.16126D+02 | 0.61440D+02 | 0.15680D+03 | 0.49116D+01 | 0.0 | 0.0 |
| 0.46000D+01 | 0.15291D+02 | 0.59495D+02 | 0.15319D+03 | -0.24835D+01 | 0.0 | 0.0 |
| 0.47000D+01 | 0.16006D+02 | 0.53868D+02 | 0.15503D+03 | -0.41795D+02 | 0.0 | 0.0 |
| 0.48000D+01 | 0.15427D+02 | 0.53257D+02 | 0.15367D+03 | 0.43574D+01 | 0.0 | 0.0 |
| 0.49000D+01 | 0.14349D+02 | 0.53584D+02 | 0.15524D+03 | -0.30955D+01 | 0.0 | 0.0 |
| 0.50000D+01 | 0.14341D+02 | 0.51376D+02 | 0.15268D+03 | 0.10076D+01 | 0.0 | 0.0 |

ALARM-P (MUD1(VERSION 01) DATE 77.06.30) PWR LOSS OF COOLANT ANALYSIS PROGRAM
 CSNI STANDARD PROBLEM NO.5 BY ALARM-P1(MUD1)

| TIME SEC | MASS FLOW | MASS FLOW | MASS FLOW | VOLUME FLOW | VOLUME FLOW | VOLUME FLOW |
|--------------|--------------|---------------|--------------|--------------|--------------|-------------|
| JUN 2 KG/SEC | JUN 5 KG/SEC | JUN 24 KG/SEC | JUN 33 L/SEC | JUN 34 L/SEC | JUN 35 L/SEC | |

| | | | | | | |
|-------------|--------------|-------------|-------------|--------------|-----|-----|
| 0.55000D+01 | 0.12942D+02 | 0.40636D+02 | 0.15119D+03 | -0.33123D+01 | 0.0 | 0.0 |
| 0.60000D+01 | 0.96066D+01 | 0.34131D+02 | 0.15122D+03 | -0.81201D+02 | 0.0 | 0.0 |
| 0.65000D+01 | 0.87930D+01 | 0.27312D+02 | 0.14655D+03 | -0.47900D+01 | 0.0 | 0.0 |
| 0.70000D+01 | 0.48007D+01 | 0.31399D+02 | 0.74043D+02 | 0.13689D+01 | 0.0 | 0.0 |
| 0.75000D+01 | 0.55835D+01 | 0.26579D+02 | 0.16300D+03 | -0.32274D+01 | 0.0 | 0.0 |
| 0.80000D+01 | 0.78679D+01 | 0.18676D+02 | 0.15577D+03 | -0.10550D+01 | 0.0 | 0.0 |
| 0.85000D+01 | 0.53084D+01 | 0.79369D+01 | 0.15920D+03 | -0.46523D+01 | 0.0 | 0.0 |
| 0.90000D+01 | 0.12492D+01 | 0.18240D+02 | 0.12776D+03 | 0.17118D+01 | 0.0 | 0.0 |
| 0.95000D+01 | 0.10436D+01 | 0.17334D+02 | 0.11647D+03 | -0.31245D+01 | 0.0 | 0.0 |
| 0.10000D+02 | -0.11592D+01 | 0.19536D+02 | 0.12116D+03 | -0.12892D+01 | 0.0 | 0.0 |
| 0.10200D+02 | -0.12103D+01 | 0.17772D+02 | 0.11875D+03 | -0.44890D+01 | 0.0 | 0.0 |
| 0.11000D+02 | -0.15908D+01 | 0.14522D+02 | 0.11938D+03 | 0.20533D+01 | 0.0 | 0.0 |
| 0.11200D+02 | 0.25459D+01 | 0.15948D+02 | 0.11943D+03 | -0.30046D+01 | 0.0 | 0.0 |
| 0.12000D+02 | 0.76452D+00 | 0.10032D+02 | 0.11694D+03 | -0.15133D+01 | 0.0 | 0.0 |
| 0.12200D+02 | -0.61702D+00 | 0.98910D+01 | 0.11185D+03 | 0.43015D+01 | 0.0 | 0.0 |
| 0.13000D+02 | -0.83359D+01 | 0.12407D+02 | 0.10481D+03 | 0.23733D+01 | 0.0 | 0.0 |
| 0.13300D+02 | -0.12668D+02 | 0.47388D+01 | 0.10405D+03 | -0.28685D+01 | 0.0 | 0.0 |
| 0.14000D+02 | -0.18863D+02 | 0.90751D+01 | 0.98484D+02 | -0.17262D+01 | 0.0 | 0.0 |
| 0.14200D+02 | -0.27006D+02 | 0.96242D+01 | 0.92653D+02 | -0.40911D+01 | 0.0 | 0.0 |
| 0.15000D+02 | -0.34963D+02 | 0.82531D+01 | 0.88427D+02 | -0.26766D+01 | 0.0 | 0.0 |
| 0.15200D+02 | -0.38305D+02 | 0.75940D+01 | 0.86771D+02 | -0.27172D+01 | 0.0 | 0.0 |
| 0.16000D+02 | -0.36506D+02 | 0.80868D+01 | 0.84910D+02 | -0.19267D+01 | 0.0 | 0.0 |
| 0.16300D+02 | -0.35020D+02 | 0.85796D+01 | 0.81175D+02 | -0.38592D+01 | 0.0 | 0.0 |
| 0.17000D+02 | -0.30125D+02 | 0.88644D+01 | 0.78807D+02 | -0.29604D+01 | 0.0 | 0.0 |
| 0.17500D+02 | -0.22936D+02 | 0.94446D+01 | 0.76789D+02 | -0.25511D+01 | 0.0 | 0.0 |
| 0.18000D+02 | -0.20067D+02 | 0.95964D+01 | 0.73966D+02 | -0.21133D+01 | 0.0 | 0.0 |
| 0.18200D+02 | -0.17762D+02 | 0.98090D+01 | 0.72144D+02 | -0.36074D+01 | 0.0 | 0.0 |
| 0.19000D+02 | -0.16134D+02 | 0.96253D+01 | 0.59494D+02 | 0.32233D+01 | 0.0 | 0.0 |
| 0.19500D+02 | -0.13489D+02 | 0.90677D+01 | 0.57986D+02 | -0.23733D+01 | 0.0 | 0.0 |
| 0.20000D+02 | -0.11744D+02 | 0.89570D+01 | 0.56188D+02 | -0.22867D+01 | 0.0 | 0.0 |

ALARM-P (MUD1(VERSION 01) DATE 77.06.30) PWR LOSS OF COOLANT ANALYSIS PROGRAM
 CSNI STANDARD PROBLEM NO.5 BY ALARM-P1(MUD1)

| TIME SEC | MASS FLOW | MASS FLOW | MASS FLOW | VOLUME FLOW | VOLUME FLOW | VOLUME FLOW |
|--------------|--------------|---------------|--------------|--------------|--------------|-------------|
| JUN 2 KG/SEC | JUN 5 KG/SEC | JUN 24 KG/SEC | JUN 33 L/SEC | JUN 34 L/SEC | JUN 35 L/SEC | |

| | | | | | | |
|-------------|--------------|-------------|-------------|-------------|-------------|-------------|
| 0.20500D+02 | -0.11617D+02 | 0.86911D+01 | 0.64401D+02 | 0.33373D+01 | 0.0 | 0.0 |
| 0.21000D+02 | -0.13288D+02 | 0.10205D+02 | 0.62152D+02 | 0.10209D+01 | 0.0 | 0.0 |
| 0.21300D+02 | -0.12864D+02 | 0.10613D+02 | 0.62306D+02 | 0.12363D+02 | 0.0 | 0.0 |
| 0.22000D+02 | -0.16081D+02 | 0.18482D+02 | 0.56565D+02 | 0.11937D+02 | 0.0 | 0.10840D+01 |
| 0.22500D+02 | -0.12551D+02 | 0.53997D+01 | 0.55757D+02 | 0.21049D+02 | 0.0 | 0.10840D+01 |
| 0.23000D+02 | -0.83960D+01 | 0.71350D+01 | 0.53768D+02 | 0.23134D+02 | 0.0 | 0.10840D+01 |
| 0.23500D+02 | -0.83153D+01 | 0.78285D+01 | 0.51295D+02 | 0.25623D+02 | 0.0 | 0.10840D+01 |
| 0.24000D+02 | -0.11113D+02 | 0.85425D+01 | 0.48195D+02 | 0.28272D+02 | 0.0 | 0.10840D+01 |
| 0.24500D+02 | -0.91671D+02 | 0.79521D+01 | 0.47353D+02 | 0.30506D+02 | 0.0 | 0.10840D+01 |
| 0.25000D+02 | 0.40473D+01 | 0.70510D+01 | 0.46482D+02 | 0.32699D+02 | 0.0 | 0.10840D+01 |
| 0.25500D+02 | 0.28263D+01 | 0.92849D+01 | 0.43691D+02 | 0.34173D+02 | 0.0 | 0.10840D+01 |
| 0.26000D+02 | -0.22846D+02 | 0.68482D+01 | 0.42060D+02 | 0.35244D+02 | 0.0 | 0.10840D+01 |
| 0.26200D+02 | 0.24974D+01 | 0.42380D+02 | 0.36612D+02 | 0.0 | 0.10840D+01 | 0.10840D+01 |
| 0.27000D+02 | -0.15616D+02 | 0.50980D+01 | 0.39463D+02 | 0.38060D+02 | 0.0 | 0.10840D+01 |
| 0.27500D+02 | -0.10141D+02 | 0.44303D+01 | 0.40336D+02 | 0.39418D+02 | 0.0 | 0.10840D+01 |
| 0.28000D+02 | 0.15248D+01 | 0.50188D+01 | 0.39863D+02 | 0.40795D+02 | 0.0 | 0.10840D+01 |
| 0.28500D+02 | -0.11377D+01 | 0.60675D+01 | 0.38190D+02 | 0.42149D+02 | 0.0 | 0.10840D+01 |
| 0.29000D+02 | -0.33674D+01 | 0.64314D+01 | 0.37858D+02 | 0.43443D+02 | 0.0 | 0.10840D+01 |
| 0.29500D+02 | 0.16676D+00 | 0.56787D+01 | 0.36659D+02 | 0.44693D+02 | 0.0 | 0.10840D+01 |
| 0.30000D+02 | -0.79752D+01 | 0.62623D+01 | 0.36199D+02 | 0.45895D+02 | 0.0 | 0.10840D+01 |
| 0.30500D+02 | -0.15432D+01 | 0.67020D+01 | 0.35035D+02 | 0.47060D+02 | 0.0 | 0.10840D+01 |
| 0.31000D+02 | 0.14004D+01 | 0.71762D+01 | 0.34166D+02 | 0.48181D+02 | 0.0 | 0.10840D+01 |
| 0.31500D+02 | 0.12896D+01 | 0.61549D+01 | 0.32096D+02 | 0.49203D+02 | 0.0 | 0.10840D+01 |
| 0.32000D+02 | 0.87735D+01 | 0.34929D+01 | 0.30674D+02 | 0.50186D+02 | 0.0 | 0.10840D+01 |
| 0.32500D+02 | 0.74533D+01 | 0.25231D+01 | 0.31776D+02 | 0.51145D+02 | 0.0 | 0.10840D+01 |
| 0.33000D+02 | 0.19781D+01 | 0.22484D+01 | 0.29617D+02 | 0.52139D+02 | 0.0 | 0.10840D+01 |
| 0.33500D+02 | 0.87572D+00 | 0.26340D+01 | 0.28386D+02 | 0.53049D+02 | 0.0 | 0.10840D+01 |
| 0.34000D+02 | 0.13651D+01 | 0.28487D+01 | 0.28490D+02 | 0.53924D+02 | 0.0 | 0.10840D+01 |
| 0.34500D+02 | 0.12495D+01 | 0.29583D+01 | 0.27734D+02 | 0.54772D+02 | 0.0 | 0.10840D+01 |
| 0.35000D+02 | 0.21120D+01 | 0.29503D+01 | 0.27127D+02 | 0.55593D+02 | 0.0 | 0.10840D+01 |
| 0.35500D+02 | 0.24668D+01 | 0.27656D+01 | 0.26720D+02 | 0.56388D+02 | 0.0 | 0.10840D+01 |
| 0.36000D+02 | 0.20455D+01 | 0.30649D+01 | 0.25517D+02 | 0.57141D+02 | 0.0 | 0.10840D+01 |
| 0.36500D+02 | 0.29277D+01 | 0.34106D+01 | 0.25346D+02 | 0.57857D+02 | 0.0 | 0.10840D+01 |
| 0.37000D+02 | 0.23598D+01 | 0.34879D+01 | 0.24476D+02 | 0.58515D+02 | 0.12003D+01 | 0.10840D+01 |
| 0.37500D+02 | 0.16330D+01 | 0.35975D+01 | 0.23554D+02 | 0.59161D+02 | 0.18210D+01 | 0.10840D+01 |
| 0.38000D+02 | 0.30273D+01 | 0.37172D+01 | 0.22875D+02 | 0.59807D+02 | 0.26491D+01 | 0.10840D+01 |
| 0.38500D+02 | 0.28749D+01 | 0.39918D+01 | 0.22643D+02 | 0.60455D+02 | 0.32598D+02 | 0.10840D+01 |
| 0.39000D+02 | 0.32212D+01 | 0.41432D+01 | 0.22266D+02 | 0.61082D+02 | 0.37420D+01 | 0.10840D+01 |
| 0.39500D+02 | 0.26641D+01 | 0.43142D+01 | 0.21769D+02 | 0.61654D+02 | 0.41996D+01 | 0.10840D+01 |
| 0.40000D+02 | 0.24556D+01 | 0.44351D+01 | 0.21343D+02 | 0.62299D+02 | 0.46339D+01 | 0.10840D+01 |
| 0.40500D+02 | 0.26491D+01 | 0.45669D+01 | 0.20936D+02 | 0.62885D+02 | 0.50649D+01 | 0.10840D+01 |
| 0.41000D+02 | 0.34676D+01 | 0.46864D+01 | 0.20503D+02 | 0.63404D+02 | 0.54685D+01 | 0.10840D+01 |
| 0.41500D+02 | 0.29114D+01 | 0.44927D+01 | 0.20056D+02 | 0.64221D+02 | 0.58222D+01 | 0.10840D+01 |
| 0.42000D+02 | 0.38539D+01 | 0.49918D+01 | 0.19580D+02 | 0.64986D+02 | 0.60620D+01 | 0.10840D+01 |
| 0.42500D+02 | 0.40149D+01 | 0.30097D+01 | 0.19037D+02 | 0.65132D+02 | 0.63042D+01 | 0.10840D+01 |
| 0.43000D+02 | 0.35280D+01 | 0.50592D+01 | 0.18944D+02 | 0.65966D+02 | 0.63330D+01 | 0.10840D+01 |
| 0.43500D+02 | 0.35521D+01 | 0.51768D+01 | 0.18031D+02 | 0.66190D+02 | 0.67519D+01 | 0.10840D+01 |
| 0.44000D+02 | 0.32463D+01 | 0.32629D+01 | 0.17578D+02 | 0.66701D+02 | 0.69574D+01 | 0.10840D+01 |
| 0.44500D+02 | 0.33347D+01 | 0.53294D+01 | 0.17101D+02 | 0.67202D+02 | 0.71553D+01 | 0.10840D+01 |
| 0.45000D+02 | 0.39381D+01 | 0.54486D+01 | 0.16774D+02 | 0.67696D+02 | 0.73470D+01 | 0.10840D+01 |

ALARM-P (MODULE VERSION 01) DATE 77.06.30) PWR LOSS OF COOLANT ANALYSIS PROGRAM
 CSNI STANDARD PROBLEM NO.2 BY ALARM-P1(MOD1)

| TIME SEC | MASS FLOW JUN 2 KG/SEC | MASS FLOW JUN 3 KG/SEC | MASS FLOW JUN 24 KG/SEC | VOLUME FLOW JUN 33 L/SEC | VOLUME FLOW JUN 34 L/SEC | VOLUME FLOW JUN 35 L/SEC |
|--------------|------------------------|------------------------|-------------------------|--------------------------|--------------------------|--------------------------|
| 0.425000D+02 | 0.361240D+01 | 0.551160D+01 | 0.164950D+02 | 0.681820D+02 | 0.752740D+01 | 0.108400D+01 |
| 0.460000D+02 | 0.387250D+01 | 0.595760D+01 | 0.161630D+02 | 0.686630D+02 | 0.766250D+01 | 0.108400D+01 |
| 0.465000D+02 | 0.342150D+01 | 0.567110D+01 | 0.156280D+02 | 0.691380D+02 | 0.778220D+01 | 0.108400D+01 |
| 0.470000D+02 | 0.555140D+01 | 0.575230D+01 | 0.155020D+02 | 0.696030D+02 | 0.789240D+01 | 0.108400D+01 |
| 0.475000D+02 | 0.479450D+01 | 0.582760D+01 | 0.151860D+02 | 0.700610D+02 | 0.800550D+01 | 0.108400D+01 |
| 0.480000D+02 | 0.579390D+01 | 0.588500D+01 | 0.148730D+02 | 0.705390D+02 | 0.811290D+01 | 0.108400D+01 |
| 0.485000D+02 | 0.425120D+01 | 0.593290D+01 | 0.145590D+02 | 0.709630D+02 | 0.820940D+01 | 0.108400D+01 |
| 0.490000D+02 | 0.527350D+01 | 0.588140D+01 | 0.143080D+02 | 0.714430D+02 | 0.839490D+01 | 0.108400D+01 |
| 0.495000D+02 | 0.601630D+01 | 0.622680D+01 | 0.142260D+02 | 0.718430D+02 | 0.84870D+01 | 0.108400D+01 |
| 0.500000D+02 | 0.718720D+01 | 0.683350D+01 | 0.142440D+02 | 0.722700D+02 | 0.84870D+01 | 0.108400D+01 |
| 0.505000D+02 | 0.685350D+01 | 0.60190D+01 | 0.139480D+02 | 0.726490D+02 | 0.856150D+01 | 0.108400D+01 |
| 0.510000D+02 | 0.727980D+01 | 0.610580D+01 | 0.133610D+02 | 0.731230D+02 | 0.864110D+01 | 0.108400D+01 |
| 0.515000D+02 | 0.798130D+01 | 0.625720D+01 | 0.133360D+02 | 0.735590D+02 | 0.872300D+01 | 0.108400D+01 |
| 0.520000D+02 | 0.819710D+01 | 0.637170D+01 | 0.131910D+02 | 0.739860D+02 | 0.879130D+01 | 0.108400D+01 |
| 0.525000D+02 | 0.647860D+01 | 0.619340D+01 | 0.131940D+02 | 0.744070D+02 | 0.886440D+01 | 0.108400D+01 |
| 0.530000D+02 | 0.652190D+01 | 0.619160D+01 | 0.127670D+02 | 0.746310D+02 | 0.892700D+01 | 0.108400D+01 |
| 0.535000D+02 | 0.614250D+01 | 0.627870D+01 | 0.124250D+02 | 0.752360D+02 | 0.897980D+01 | 0.108400D+01 |
| 0.540000D+02 | 0.981240D+01 | 0.639240D+01 | 0.124290D+02 | 0.756860D+02 | 0.903150D+01 | 0.108400D+01 |
| 0.545000D+02 | 0.951960D+01 | 0.641200D+01 | 0.124610D+02 | 0.761090D+02 | 0.908160D+01 | 0.108400D+01 |
| 0.550000D+02 | 0.820200D+01 | 0.539740D+01 | 0.124670D+02 | 0.765320D+02 | 0.913050D+01 | 0.108400D+01 |
| 0.555000D+02 | 0.636600D+01 | 0.639740D+01 | 0.124780D+02 | 0.769550D+02 | 0.917740D+01 | 0.108400D+01 |
| 0.560000D+02 | 0.629980D+01 | 0.644550D+01 | 0.1246720D+02 | 0.773830D+02 | 0.922490D+01 | 0.108400D+01 |
| 0.565000D+02 | 0.873670D+01 | 0.637460D+01 | 0.1111320D+02 | 0.7778170D+02 | 0.927470D+01 | 0.108400D+01 |
| 0.570000D+02 | 0.873070D+01 | 0.663240D+01 | 0.122230D+02 | 0.782480D+02 | 0.931320D+01 | 0.108400D+01 |
| 0.575000D+02 | 0.110010D+02 | 0.661170D+01 | 0.1233420D+02 | 0.786790D+02 | 0.934420D+01 | 0.108400D+01 |
| 0.580000D+02 | 0.908520D+01 | 0.6627760D+01 | 0.122040D+02 | 0.791100D+02 | 0.939550D+01 | 0.108400D+01 |
| 0.585000D+02 | 0.922480D+01 | 0.682790D+01 | 0.114990D+02 | 0.795460D+02 | 0.942900D+01 | 0.108400D+01 |
| 0.590000D+02 | 0.102980D+02 | 0.669020D+01 | 0.111810D+02 | 0.799890D+02 | 0.966870D+01 | 0.108400D+01 |
| 0.595000D+02 | 0.992070D+01 | 0.680490D+01 | 0.118240D+02 | 0.804400D+02 | 0.949560D+01 | 0.108400D+01 |
| 0.600000D+02 | 0.120240D+02 | 0.683210D+01 | 0.130090D+02 | 0.808830D+02 | 0.953860D+01 | 0.108400D+01 |