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APPLE-2: AN IMPROVED VERSION OF
APPLE CODE FOR PLOTTING NEUTRON
AND GAMMA RAY SPECTRA AND
REACTION RATES

July 1982

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APPLE-2: An Improved Version of APPLE Code for Plotting Neutron
and Gamma Ray Spectra and Reaction Rates

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A computer code APPLE-2 which plots the spatial distribution of energy spectra of multi-group neutron and/or gamma ray fluxes, and reaction rates has been developed. This code is an improved version of the previously developed APPLE code and has the following features:

- (1) It plots energy spectra of neutron and/or gamma ray fluxes calculated by ANISN, DOT and MORSE.
- (2) It calculates and plots the spatial distribution of neutron and gamma ray fluxes and various types of reaction rates such as nuclear heating rates, operational dose rates, displacement damage rates.
- (3) Input data specification is greatly simplified by the use of standard, response libraries and by close coupling with radiation transport calculation codes.
- (4) Plotting outputs are given in camera ready form.

Keywords: Plotter, Graphical Display, Neutron Flux, Gamma Ray Flux,
Energy Spectra, Reaction Rate, Nuclear Heating Rate,
Radiation Transport Calculation, APPLE-2 code

* Century Research Center Corporation Ltd.

APPLE-2: 中性子束とガンマ線束のスペクトルと
反応率のプロッターコードAPPLEの改良版

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中性子束とガンマ線束のエネルギー群スペクトルと反応率の空間分布をプロットする計算コードAPPLE-2を開発した。本コードは以前に開発したAPPLEコードの改良版であり以下の特徴を有している。

- (1) ANISN, DOTおよびMORSEで計算した中性子束およびガンマ線束のエネルギースペクトルをプロットする。
- (2) 中性子束とガンマ線による各種の反応率, 例えば核発熱率, 運転中の線量率, はじき出し損傷率等の空間分布を計算しプロットする。
- (3) 標準的なレスポンスライブラリーの使用と放射線輸送計算コードとの連動により入力法を大巾に簡単にした。
- (4) プロット結果をそのままレポート等に利用できる。

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1. Introduction

The APPLE-2 code is an improved version of the APPLE code⁽¹⁾ developed in 1976 for plotting the spatial distribution of the reaction rates and the energy spectra of multi-group neutron flux obtained with one-dimensional discrete ordinates transport code ANISN⁽²⁾. The APPLE code has been widely used in the nuclear design of fusion devices^{(3),(4)} and analyses⁽⁵⁾ of integral experiments in the Japan Atomic Energy Research Institute (JAERI) and elsewhere in Japan⁽⁶⁾. The extensive use of the APPLE code made apparent, the complexity of input data preparation and inadequacies of the result such as the difficulty in deriving quantitative information from the overview plot of multigroup neutron flux.

Based on the experiences with the APPLE code, the APPLE-2 code is developed not just as a minor modification of the previous code but as a thoroughly improved code. Additional capabilities of the new code are;

- 1) to plot the energy spectra of neutron and/or gamma ray fluxes calculated by ANISN⁽²⁾, DOT⁽⁷⁾ and MORSE⁽⁸⁾, and
- 2) to calculate and plot reaction rates using the DOT calculated fluxes.

The input data specification is greatly simplified by modifying the output of the radiation transport codes. Also several standard response libraries for fusion reactor neutronics calculations are made available to the users of the cross section sets such as the GICX40 Set.⁽⁹⁾

In addition, all the output graphs are provided in camera ready form.

The function, structure, and input/output descriptions of the code are given in Section 2. Standard response libraries for fusion reactor calculations are described in Section 3. Sufficient number of sample

problems are given in Section 4 to demonstrate the versatile application of the code. Some remarks are given in Section 5.

2. APPLE-2 Code

2.1 Functions and Features

The APPLE-2 code has the following functions which are summarized in Table 2.1:

- (1) It plots multi-group energy spectra of neutron and/or gamma ray fluxes calculated by ANISN, DOT-3.5 and MORSE.
- (2) It gives overview plot of multi-group neutron fluxes calculated by ANISN and DOT-3.5. Scalar neutron flux $\phi(r,E)$ is plotted with the spatial parameter r linearly along the Y-axis, $\log E$ along the X-axis and $\log \phi(r,E)$ in the Z-axis direction.
- (3) It calculates the spatial distribution and region volume integrated values of reaction rates using scalar flux calculated with ANISN⁽²⁾ and DOT-3.5⁽⁷⁾.
- (4) Reaction rate distribution along R or Z direction may be plotted.
- (5) Overview plot of reaction rates or scalar fluxes summed over specified groups may be plotted. $R(r_i, z_j)$ or $\phi(r_i, z_j)$ is plotted with spatial parameters r and z along the X- or the Y-axis in an orthogonal coordinate system.
- (6) Angular flux calculated by ANISN, $\phi(r, \vec{\Omega}, E)$ is rearranged and a shell source at any specified spatial mesh point may be punched out in FIDO format. Thus obtained shell source may be employed in solving deep penetration problems by ANISN, when the entire reactor system is divided into two or more parts and the neutron flux in two adjoining parts are connected by using the shell source.

Notable features of the APPLE-2 code are as follows:

- (a) The input data specification is made as simple as possible by making use of the input data required in the radiation transport

code. For example, geometry related data in ANISN and DOT are transmitted* to APPLE-2 along with scalar flux data so as to reduce duplicity and errors in reproducing these data.

- (b) Most of the input data follow the free form FIDO format developed in the Oak Ridge National Laboratory and used in the ANISN code⁽²⁾. Furthermore, the mixture specifying method used in ANISN is also used in APPLE-2.
- (c) Libraries for some standard response functions required in fusion reactor nuclear design have been prepared and are made available to users of the 42-group neutron, 21-group gamma ray coupled cross section set GICX40⁽⁹⁾. For fluxes calculated with arbitrary cross sections, response functions must be supplied by card input.
- (d) When drawing energy spectra of fluxes calculated with the GICX40 set, there is no need to input energy group structure data as they are built-in in the APPLE-2 code.
- (e) Reaction rates calculated with more than one fluxes may be drawn on a graph for comparison.
- (f) The graphical outputs are devised so that they may be readily used in reports.

* Some modification in the ANISN and DOT output is required.

Table 2.1 Functions of the APPLE-2 Code

Functions	Radiation transport codes		
	ANISN	DOT-3.5	MORSE
(1) Neutron and gamma ray energy spectrum plotting, $\phi(E_g)_{r=r_0}$	○	○	○
(2) Overview plotting of the spatial change of energy spectra, $\phi(r_i, E_g)_{z=z_0}$ or $\phi(z_i, E_g)_{r=r_0}$	○	○	—
(3) Reaction rate, $R(r_i) = \sum_g \sigma_{gi} \cdot N_i \cdot \phi(r_i, E_g)$, $R = \sum_i R(r_i) \cdot V_i$ calculation	○	○	—
(4) Reaction rate, $R(r_i) = \sum_g \sigma_{gi} \cdot N_i \cdot \phi(r_i, E_g)$ plotting	○	○	—
(5) Overview plotting of reaction rates or scalar fluxes, $R(r_i, z_j) = \sum_g N_{ij} \cdot \sigma(E_g) \cdot \phi(r_i, z_j, E_g)$ or $\phi(r_i, z_j) = \sum_{g=NL}^{NH} \phi(r_i, z_j, E_g)$	—	○	—
(6) Shell source punchout	○	—	—

2.2 Program Structure and Computational Flow

The program structure of APPLE-2 is shown in Fig.2.1 together with the Input/Output data flow. As shown in the figure, the APPLE-2 code consists of six major calculational paths which are controlled by the main program APPLE using the identification symbol named IDENT. The IDENT is always read before any part of the input data.

When IDENT = 'FLUX', scalar flux from ANISN, DOT or MORSE is read together with geometrical data.

When IDENT = 'CROS', response cross sections and mixing input data are read and mixture cross sections are calculated if necessary.

When IDENT = 'RCAL', reaction rate calculation input data are read and reaction rates are calculated.

When IDENT = 'RPLT', calculated reaction rates are plotted.

When IDENT = 'SPEC', neutron or gamma ray scalar flux spectra are plotted.

When IDENT = 'SHEL', shell source is calculated from the angular flux calculated by ANISN.

A job terminates when an input card with IDENT = 'END' is read.

As shown in Fig.2.1 the logical numbers required for input-output files and their uses are:

logical 9 + NON.	scalar fluxes (NON = 1,2,.....10);
logical 5.	standard input;
logical 6.	standard output;
logical 7.	standard punch out;
logical 21.	storage device for writing scalar flux input;
logical 23.	storage device for writing input geometrical data;
logical 24.	storage device for writing input mixture data;

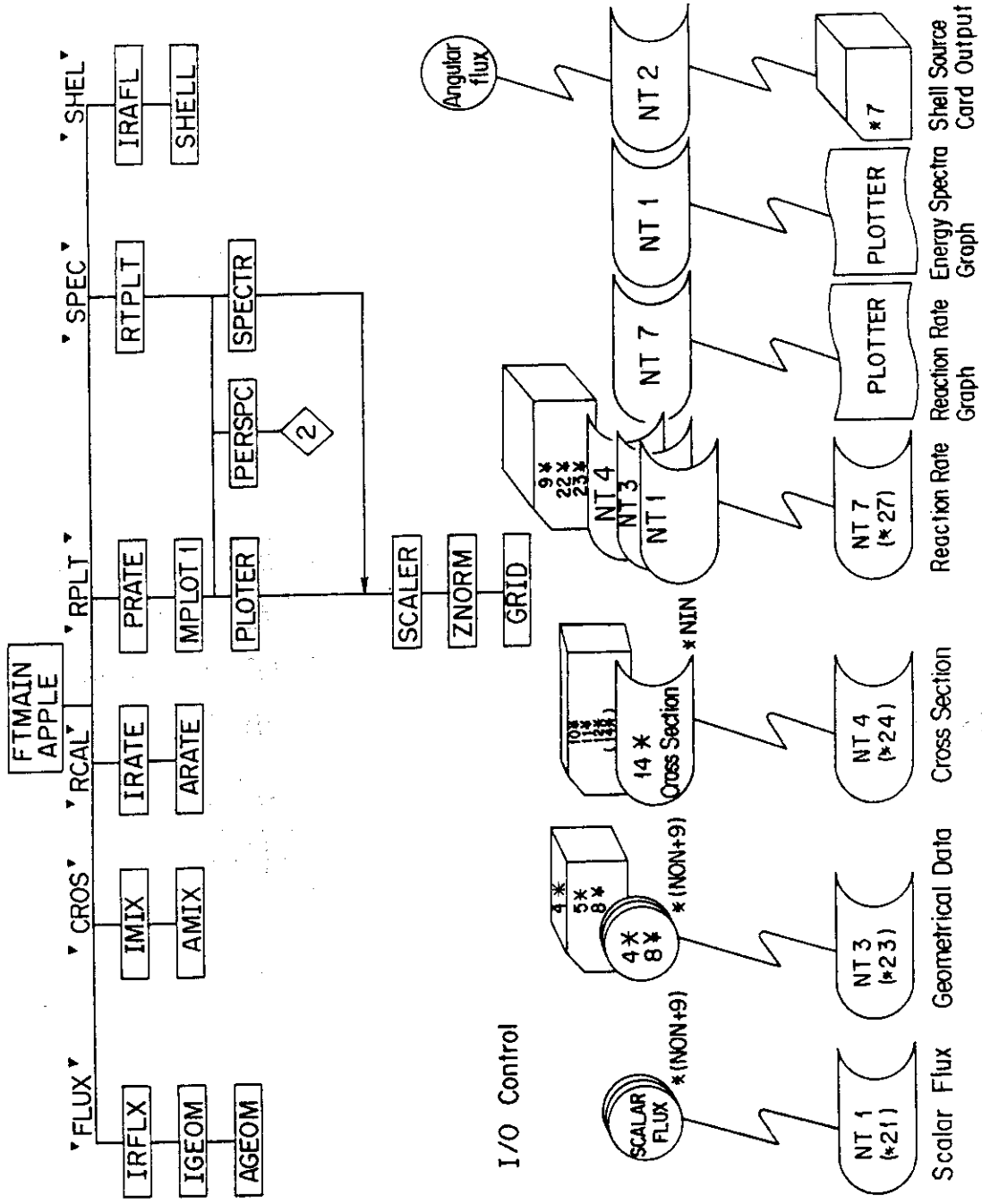


Fig.2.1 Program Structure and Input/Output Data Flow in APPLE-2

Program

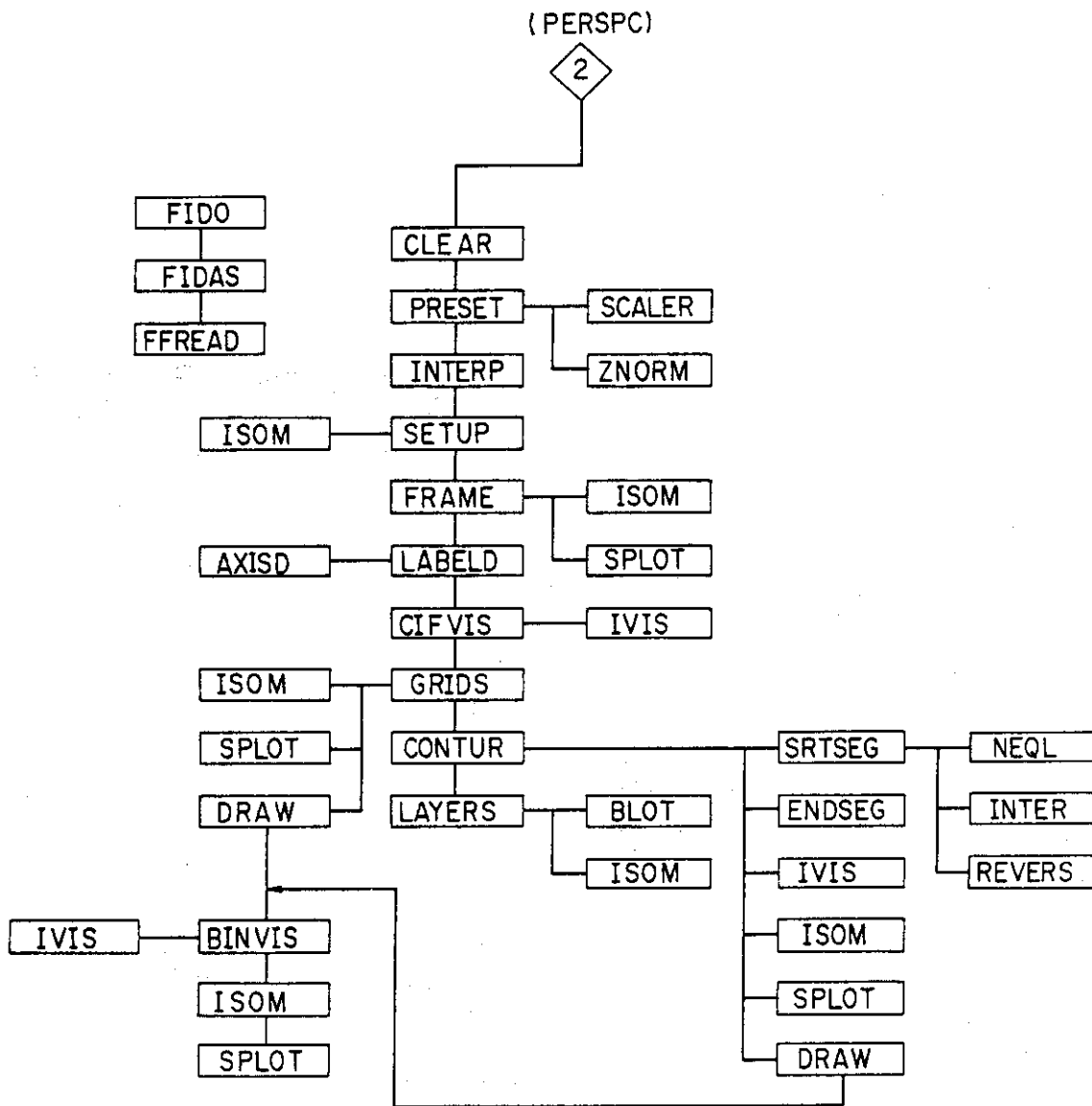


Fig.2.1 Program Structure and Input/Output Data Flow in APPLE-2

Program (continued)

- logical 26. storage device for writing input cross sections;
 logical 27. storage device for writing reaction rates.

If more than two scalar fluxes are used, the logical numbers 10, 11, ..
 ..., 20 may be used and specified in the input data.

2.3 Description of subroutines

Brief descriptions of subroutines included in APPLE-2 are as follows:

I/O and control routines

- APPLE - the main program which sets blank common size, and
 controls calculational flow
- AGEOM - processes geometrical input data (NT3)
- AMIX - mixes cross sections (NT4)
- ARATE - calculates reaction rates
- AZNAT - writes mixture data
- BLOCK DATA - stores standard energy group structures (42N, 100N,
 21G, 54G)
- CCLEAR - sets elements in array to a certain value
- CHAN - transforms dimension of arrays from two to one
- CLEAR - same as above
- DTFPUN - punches out shell sources in ANISN FIDO format
- FFREAD - reads free-form FIDO format⁽²⁾ cards
- FIDAS - same as above
- FIDO - same as above
- FLTFX - transforms a floating point number to a fixed point number
- FTMAIN - sets maximum location and calls the subroutine APPLE
- IGEOM - controls geometrical input data
- IMIX - controls mixing input data

IRAFL - reads angular flux input data from ANISN output
 IRATE - controls reaction rate calculations
 IRFLX - reads scalar flux input data from ANISN, DOT or MORSE(NT1)
 LOCAT - checks location size
 MPLOT1 - controls the plotting of reaction rates
 PRATE - sets work array locations for plotting
 PUNSH - punches out shell source in ANISN FIDO format
 RTPLT - controls the plotting of scalar flux
 SHELL - reads and processes angular flux output from ANISN
 WOT - writes 1, 2, and 3 dimensional arrays
 WOT8 - writes array by 8 columns

General plotting routines

PENSET - exchanges the colour of pens
 SCALER - calculates a factor for normalization
 ZNORM - normalizes flux value
 ENDPLT - ends plotting

Plotting routines for graphic display of reaction rates

GRID - plots grid and titles
 LINTYP - plots dotted or dashed lines
 PLOTFR - plots data and controls calculational flow
 REFER - plots reference table
 SMOOTH - connects data points with smooth curves
 SPECTR - plots scalar flux spectrum
 ZUNORM - normalizes plot value

Plotting routines for overview plot of scalar flux

AXISD - plots axes and their titles
 BINVIS - calculational routine

BLOT - same as above
 CIFVIS - determines hidden parts of grids
 CONTUR - plots contour lines
 DRAW - control routine
 ENDSEG - calculates the end of a contour line
 FRAME - draws frames
 GRIDS - controls plotting of grids
 INTER - interchanges two variables
 INTERP - interpolates input data to determine the values on
 square lattice
 ISOM - calculates coordinates values
 IVIS - determines hidden parts of grids
 LABELD - control routine for drawing axes
 LAYERS - plots numerical values
 NEQL - calculational routine
 PERSPC - controls the overview plotting
 PRESET - normalizes flux values
 REVERS - calculational routine
 SETUP - determines maximum and minimum values
 SPLOT - plotting routine
 SRTSEG - calculational routine

2.4 Variable Descriptions

In the following are described the variables for plotting reaction rates and overview of neutron spectra, which are included in subroutines PLOTER and PERSPC, respectively.

* SUBROUTINE PLOTER

X(NMAX,M) two-dimensional array corresponding to X-axis.

Y(NMAX,M) two-dimensional array corresponding to Y-axis.
 NN(M) number of data in arrays X and Y
 M number of vectors in X and Y
 NMAX maximum number of data in the vectors in X and Y
 NWAY the option for the scaling
 =1 linear X vs. linear Y
 =2 linear X vs. log Y
 =3 log X vs. linear Y
 =4 log X vs. log Y
 BCDY label for Y-axis
 NBCDY number of letters (characters) in BCDY
 BCDX label for X-axis
 NBCDX number of letters in BCDX
 TITLE main title
 NTITLE number of letters in TITLE
 XVECT =.TRUE. X is one-dimensional array
 =.FALSE. X is two-dimensional array
 BOUNDS(M) BOUNDS(1) minimum value for X-axis
 BOUNDS(2) maximum value for X-axis
 BOUNDS(3) minimum value for Y-axis
 BOUNDS(4) maximum value for Y-axis
 XSIZE length of X-axis
 YSIZE length of Y-axis
 NTRA > 0, points are connected by smooth curves
 LOGPO 1 or 3, log scaling is forced on X-axis
 2, log scaling is forced on Y-axis
 LINEIT > 0, fine grids are drawn
 NLABEL > 0, frame is drawn

NSYMB < 0, each vector are selectively drawn as continuous line, dashed line, etc.
 =0, only lines are drawn
 > 0, characteristic symbols are assigned to the data points of each vector
 |NSYMB| > 1 Descriptions for each symbol are written on a graph

BCDL(M) description for each vector

ICENT < 0, Origin of the coordinate system is set to X=0.0, Y=0.0.
 ≠ 0, basic coordinate system is drawn

* SUBROUTINE PERSPC

Z(NROW, NCOL) Z-axis data
 X(NCOL) X-axis data
 Y(NROW) Y-axis data
 IV(~) temporary area
 NN(NCOL) temporary area
 IR number of data for the X-axis
 IC number of data for the Y-axis
 THETA angle (in degrees) down from the Z-axis (see Fig.2.4.5)
 PSI angle (in degrees) around from the X-axis towards the Y-axis (see Fig.2.4.5)
 VIEWPT distance between the view point and the origin of the coordinate system (in cm)
 PWIDTH width of graph (in cm)
 PSIZE length of graph (in cm)
 NCONTR > 0, draw contour lines
 IDE ≥ 0, eliminate hidden lines

KROSS	< 0, Z-axis will be placed cross-wise
LGRID	< 0, suppress grid plot of the surface > 0, number of grids per 1 scale
NFRAME	< 0, do not draw frame = 0, draw only base frame > 0, draw full frame
KOLOR	> 0, change colour of the pen
NWAY	Z-axis scaling (1; linear, 2; log)
NWAYX	X-axis scaling
NWAYY	Y-axis scaling
LOGPO	> 0, force log scaling on Z-axis
LOGPOX	> 0, force log scaling on X-axis
LOGPOY	> 0, force log scaling on Y-axis
BCD	title of graph
NBCD	number of letters in title
BCDZ	label for Z-axis
NBCDZ	number of letters in BCDZ
BCDX	label for X-axis
NBCDX	number of letters in BCDX
BCDY	label for Y-axis
NBCDY	number of letters in BCDY

2.5 Input Instructions

The input data for APPLE-2 may be prepared by using corresponding input cards for ANISN/DOT or by using output cards from ANISN or DOT. Either conventional FIDO (\$ or *) or free-form (\$\$ or **) format⁽³⁾ may be used. Yen symbol ¥ is used in place of dollar symbol \$ in the FACOM M-200 computer used in JAERI.

IGOM ; geometry type specification
 1 / 2 / 3 = slab / cylinder / sphere (NXMODE = 1)
 0 / 1 / 2 = R-Z / X-Y / R-THETA (NXMODE = 2)

Cards 3.3 (FIDO format) (required only when NXCARD = 1)

4** [NINTI + 1] radial mesh boundaries
 5** [NINTJ + 1] axial mesh boundaries (required when NXMODE = 2)
 8** [NINTI * NINTJ] zone number specification for each mesh point
 (set radial directions first as in DOT input)

T
 (N.B. Card 3.3 may be copied from corresponding DOT input)

4. IDENT = 'CROS'; Cross section and geometrical data input

Card 4.1 (4I3)

IHM ; length of cross section table
 MCR ; number of cross section set
 MS ; cross section mixing table length
 NIN ; logical file numbers for cross section library, when
 cross sections are input from cards, NIN equals 0 or 5.

Cards 4.2 (FIDO format)

10** [MS] ; mixture numbers in mixing table
 11** [MS] ; component numbers in mixing table
 12** [MS] ; atom densities in mixing table

T

Cards 4.3 (FIDO format) (required only when NIN = 0 or 5)

14** [IHM * NGROUP * MCR] ; cross sections for reaction rate
 calculations or response functions

T

5. IDENT = 'RCAL'; Reaction rate calculation input

Card 5.1 (4I3,E12.0)

NFX ; NFX-th scalar flux data in file NT1 to be used(see Fig.2.1 for NT1)
 NGE ; NGE-th geometrical data in file NT3 to be used(see Fig.2.1 for NT3)

ID3 ; number of reaction rates to be calculated

MOPT ; plot option

= 1; reaction rates for each material are plotted

= 2; the sum of the reaction rates is plotted

= 3; both MOPT=1 and 2 are plotted

CF ; conversion factor to be multiplied to the reaction rates

(if not specified CF=1.0)

Cards 5.2 (FIDO format)

9YY [NZONE] ; material or mixture numbers by zone

22YY[ID3] ; material numbers for reaction rate calculations

23YY[ID3] ; cross section table positions for reaction rate calculations

^T
Card 5.3 (9A8)

ACT [ID3] ; labels of the reaction rates to be plotted

6. IDENT = 'RPLT' ; reaction rate (or scalar flux)* plotting input

Card 6.1 (2I3,A4)

NPLT(1) ; plot control option

= 1; reaction rate plotting for ANISN

= 2; reaction rate plotting for DOT along a fixed radial row or axial column

= 3; overview plotting of reaction rate for DOT

NPLT(2) ; (required when NPLT(1) ≥ 2)

when NPLT(1) = 2, radial or axial mesh point number along which reaction rates are plotted

when NPLT(1) = 3, reaction rate material number for plotting

NPLT(2) = 1 ~ ID3

* Scalar flux is plotted when response function is 1 or 0

TYPE ; (required only when NPLT(1) = 2)
 specifies radial or axial plotting type

= 'RADIAL' ; reaction rate is plotted in the axial
 (Z or θ) direction along NPLT(2)-th radial
 row (R-Z or R- θ geometry)

= 'Z' ; reaction rate is plotted in the radial
 direction along NPLT(2)-th axial column
 (R-Z geometry)

= 'THETA' ; reaction rate is plotted in the radial
 direction along NPLT(2)-th θ -mesh
 (R- θ geometry)

= 'X' ; reaction rate is plotted in the Y-direction
 along NPLT(2)-th X row (X-Y geometry)

= 'Y' ; reaction rate is plotted in the X-direction
 along NPLT(2)-th Y column (X-Y geometry)

Cards 6.2 (required when NPLT(1) = 1 or 2)

Card 6.2.1 (2F12.4)

XSIZE ; plot size in X-direction, unit in cm.

(default value = 15.0)

YSIZE ; plot size in Y-direction, unit in cm.

(default value = 20.0)

Card 6.2.2 (20A4) BCDZ ; title heading

Card 6.2.3 (20A4) BCDX ; X-axis title

Card 6.2.4 (20A4) BCDY ; Y-axis title

Card 6.3 (required when NPLT(1) > 2, when overview is plotted)

Card 7.5 described later

Card 7.7 described later

7. IDENT = 'SPEC' ; input data for neutron or gamma ray energy
 spectrum plotting

Card 7.1 (6I3)

NPLT1 = 2 ; neutron or gamma ray energy spectra plotting at
specified mesh points

= 3 ; neutron* energy spectra plotting along radial row
or axial column

ISTEPC ; the NON number of scalar flux data for plotting
specified in IDENT=FLUX card (same as NFX in card 5.1)

ISTEPR ; the NON number of geometrical data used for plotting
(same as NGE in card 5.1)

NORG > 0 ; number of neutron energy groups
< 0 ; number of gamma ray energy groups

NCARD = 0 ; neutron or gamma ray energy group structure in BLOCK
DATA will be used (see Section III for built-in
structures)

= 1 ; the energy boundaries of groups are input by cards

ID3 ; number of mesh points at which the energy spectra are
plotted (≤ 24)

Card 7.2 (2I3) (required when NXMODE = 2 in Card 3.1 or DOT flux
spectra are plotted)

MSH ; number of axial column or radial row along which
spectra are plotted

MXY = 1 ; spectra is plotted along the radial direction
= 2 ; spectra is plotted along the axial direction

Cards 7.3 (6E12.0) (required when NCARD = 1)

X [ABS(NORG) + 1] ; neutron or gamma ray energy group boundaries
from high to low in eV.

Card 7.4 (14I3) (required when NPLT1 = 2)

* the program cannot plot overview energy spectra of gamma ray flux
in neutron and gamma ray coupled problem.

NSOS [ID3] ; number of mesh points at which energy spectra are plotted

Card 7.5 (6I3,5E12.0) (required when NPLT1 = 3)

1. IDE ≥ 0 ; eliminate hidden lines
 < 0 ; give perspective drawing
2. KROSS < 0 ; place the Z-axis cross-wise
3. LGRID > 0 ; number of grids per 1 scale
 < 0 ; suppress grid plot of the surface
4. NFRAME > 0 ; draw full frame
 $= 0$; draw only base frame
 < 0 ; do not draw frame
5. KOLOR > 0 ; change colour of the pen
6. KONTR ; the range of plotting. If the maximum value is given by 10^N , the values larger than $10^{N-KONTR}$ will be plotted
7. THETA ; angle (in degrees) down from the Z-axis (suggested value 45.0)
8. PSI ; angle (in degrees) around from the X-axis towards the Y-axis (suggested value 45.0)
9. VIEWPT ; distance between viewpoint and the origin of the coordinate system (suggested value 1000.0 cm)
10. PWIDTH ; width of the plot (less than 23.0 cm)
11. PSIZE ; length of the plot (in cm)

Cards 7.6 (required when NPLT1 = 2)

Card 7.6.1 (2F12.4)

XSIZE ; plot size in X-direction (if 0, XSIZE = 15.0 cm)

YSIZE ; plot size in Y-direction (if 0, YSIZE = 20.0 cm)

Card 7.6.2 (20A4)

BCDZ ; title heading

BCDX ; X-axis title

BCDY ; Y-axis title

Card 7.7 (20A4) (required when NPLT1 = 3)

BCD ; title heading for overview plot

8. IDENT = 'SHEL' ; input data for shell source punch out for ANISN calculations

Card 8.1 (3I3)

NGROUP ; number of groups

NINTI ; number of spatial mesh points

NDIR ; number of discrete directions

= ISN+1 for plane or sphere,

= (ISN * (ISN + 4)) / 4 for cylinder,

where ISN is the order of S_N used in the angular flux calculation

Card 8.2 (I3)

MBDRY ; the mesh interval number at which the shell source is punched out

Cards 2 ~ 6 may be input repeatedly so as to allow reaction rates plotting in different models on a same graph for comparison.

IDENT cards of a kind must be given sequential NON numbers.

IDENT = 'END' card will terminate the job.

2.5.2 Input file record format

The APPLE-2 code reads scalar flux, angular flux, response libraries and other data from files prepared beforehand. The record format of the files are described below.

(a) Scalar flux record format of ANISN output

The output subroutine FINPR of the ANISN code has been slightly modified to transmit relevant data to APPLE-2 together with scalar flux

data. The modified portion of the FINPR subroutine is listed in Fig.2.4.1. As shown in the figure, the input parameter ID2 must be made equal to -3 in order to transmit relevant data to APPLE-2.

The record format is as follows:

Record 1

IGM ; number of energy groups
 IM ; number of spatial mesh intervals
 IZM ; number of zones
 IGE ; number of geometry type specification
 1-slab ; 2-cylinder; 3-sphere

Record 2

RA [IM+1] ; interval boundaries
 MA [IM] ; zone numbers by interval
 V [IM] ; volumes by interval

Record 3

(XN(J,I),J=1,IM) ; scalar flux in IGM loops

These data are read by subroutine IRFLX of the APPLE-2 code.

(b) Scalar flux record format of DOT output

Subroutines OUTER, TPSAVE and TPXF of the DOT code have been modified to transmit relevant data to APPLE-2 with scalar flux data. The modified portions of the subroutines are listed in Fig.2.4.2. As shown in the figure, the initial portion of the scalar flux data written on NFLSV is modified to transmit the data in the following record format to be read by the subroutine IRFLX of the APPLE-3.

Record 1

IGM ; number of energy groups
 IM ; number of radial mesh interval
 JM ; number of axial mesh interval

IZM ; number of zones

IGE ; number of geometry type specification

0 / 1 / 2 = R-Z / X-Y / R-THETA

Record 2

RA [IM+1] ; radial interval boundaries

ZA [JM+1] ; axial interval boundaries

MA [IM*JM] ; zone numbers by interval

V [IM*JM] ; volumes by interval

Record 3

((XN(I,J),I=1,IM), J=1,JM) ; scalar flux in IGM loops

(c) Scalar flux record format by MORSE output

The subroutine NRUN of the MORSE-GG code⁽⁸⁾ is modified to write the scalar flux of some region (using track length estimator) or some positions (using point detector estimator). The record format of the data read by subroutine IRFLX of the APPLE-2 is as follows:

Record 1

NNE ; number of neutron groups

NGROUP ; number of total groups

NINTI ; number of estimators multiplied by 3

Record 2

EFIRST ; the upper bound energy of the first neutron group

EGTOP ; the upper bound energy of the first gamma ray group

Y(I),I=1,NGROUP; the lower bound energy of neutron and

gamma ray energy groups from high to low

Record 3

Y(J),J=1,NGROUP ; scalar flux

Record 4

Y(J),J=1,NGROUP ; fractional standard deviation (f.s.d.) of

the scalar flux

Records 3 and 4 are in NINTI loops (are read repeatedly for NINTI times).

(d) Angular flux record from ANISN

The angular flux are written by the modified version of the SUMARY subroutine of the ANISN code which is listed in Fig.2.4.4. As shown in Fig.2.4.4, the input parameter ID1 must be made equal to -1 in order to write angular flux on a file for the transmission to APPLE-2.

Record 1 angular flux

((XND(I,M), I = 1, NINTI + 1), M = 1, NDIR)

Record 1 is in NGROUP loops.

(e) Response function libraries record format

Some standard response function libraries for fusion reactor calculations are provided for the user of the GICX40 cross section set⁽⁹⁾ and DLC-2D⁽¹⁰⁾ structured cross section set. The content of the libraries will be described in the next section. The record format of the libraries are as follows:

Record 1 (3I3)

IHM ; length of cross section (response) table

NGP ; number of groups

MCR ; number of cross section set in the library

Record 2 (FIDO format)

14** [IHM * NGP * MCR] ; cross section (or response function values

T ; end of the library

```

0092 IF(IGMNEW.NE.IGMNEU.AND.JJ1.EQ.1) GO TO 800
0093 IF(IDAT1.NE.0)REWIND NT3
0094 IF(IDAT1.EQ.2)REWIND NT1
0095 IF(NACTPR.EQ.1) CALL ACTPRT(XNXNKN(1),XNXNKN(NXADRS),IM,IGM,ID3,
      * IZP,IIG,J,I,KK,E2,E3,T3,1)
0096 IF(ID4.GE.0)GO TO 1
0097 DO 42 I=1,ID3
0098 42 CALL PUNSH(T5(1,I),IM)
0099 1 CONTINUE
0100 IF(IDAT1.EQ.2)GO TO 26
0101 IF(ID1.LT.2)GO TO 18
0102 DO 43 I=1,IGM
0103 43 CALL PUNSH(XN(1,I),IM)
0104 160 FORMAT(12A4,8X/1X,2H3*,69X,4HFLUX,3X,1H0)
0105 18 IF(ID1.GT.-2) GO TO 110
0106 NFX=10
0107 REWIND NFX
0108 IF(ID1.EQ.-2) GO TO 104
0109 WRITE(NFX) IGM,IM,IZM,IGE
0110 104 CONTINUE
0111 WRITE(NFX) (RA(I),I=1,IP),(MA(I),I=1,IM),(V(I),I=1,IM)
0112 DO 105 I=1,IGM
0113 105 WRITE(NFX) (XN(J,I),J=1,IM)
0114 WRITE(6,600) IGM,IM,NFX
0115 REWIND NFX
C 18 WRITE (NOU,170) T
0116 110 WRITE (NOU,170) T
      *** PRINT FLUX IF IN CORE
0117 WRITE (NOU,60)
0118 60 FORMAT(12HO TOTAL FLUX)
0119 IF(IIBOUD.EQ.1) REWIND 20
C IF(IIBOUD.EQ.1) CALL NWSUB4(D(LXND),IP,MM,XNXNKN,IGM,NT4)
IF(IIBOUD.EQ.1) CALL NWSUB4(D(LXND),IP,MM,XNXNKN,IGM,NT4,D(LW))
0120 IF(IIBOUD.NE.1) GO TO 3333
0121 REWIND 20
0122 CALL NWSUB1(XNXNKN,IP,IGM)
0123 GO TO 3334
0124 3333 CONTINUE
0125 CALL WOT(XN,IGM,IM,1,'INT.','GRP.',0)
0126 3334 CONTINUE
0127 IF(IISPTM.EQ.1) CALL NWSUB2(XN,IP,IGM,IM,XNXNKN)
0128 CALL WOTYT(XN,IGM,IM,1,IGMNEU)
0129 CALL WOTYT(XN,IGM,IM,IGMNEU+1,IGM)
0130 19 IF(IDAT1.EQ.1)GO TO 22
0131 C *** PRINT DIST. SOURCE IF ANY AND IN CORE
0132 IF(IGM.EQ.0)GO TO 23
0133 WRITE (NOU,170) T
0134 WRITE (NOU,70)
0135 70 FORMAT(20HO DISTRIBUTED SOURCE)
0136 CALL WOT(Q,IGM,IM,1,'INT.','GRP.',0)
0137 GO TO 24
C *** PRINT SHELL SOURCE IF ANY AND IN CORE
0138 23 IF(IPM.EQ.0)GO TO 24
0139 WRITE (NOU,170) T
0140 IF(IPM.GT.1)GO TO 25
0141 WRITE (NOU,80) IPP
0142 80 FORMAT(27HO SHELL SOURCE IN INTERVAL I3)
0143 CALL WOT(PA,IGM,MM,1,'ANGL','GRP.',0)
0144 GO TO 24
0145 25 WRITE (NOU,90)
0146 90 FORMAT(14HO SHELL SOURCE)
0147 CALL WOT(PA,IM,MM,IGM,'ANGL','INT.','GRP.')
0148 GO TO 24
0149 26 IF(ID1.GT.-2) GO TO 120
0150 NFX=10
0151 REWIND NFX
0152 IF(ID1.EQ.-2) GO TO 114
0153 WRITE(NFX) IGM,IM,IZM,IGE
0154 114 CONTINUE
0155 WRITE(NFX) (RA(I),I=1,IP),(MA(I),I=1,IM),(V(I),I=1,IM)
0156 DO 115 I=1,IGM
0157 READ (NT1) (X(J,I),J=1,IM)
0158 WRITE(NFX) (X(J,I),J=1,IM)
0159 IF(ISCT.GT.0) READ (NT1)
0160 115 CONTINUE
0161 WRITE(6,600) IGM,IM,NFX
0162 REWIND NT1
0163 REWIND NFX
0164 600 FORMAT(1H1////,5X,'*** SCALAR FLUX ('I3,' GROUPS,'I4,
      1 ' INTERVALS ) WAS WRITTEN ON MT='I3,' ***')
C 26 I02=0
0165 120 I02=0
0166 29 I01=MINO(IGM-I02,8)
0167 WRITE (NOU,170) T
0168 WRITE (NOU,140) I02
0169 140 FORMAT(32HO TOTAL FLUX - G=GROUP NO. N=I3)
0170 DO 31 I=1,I01
0171 READ (NT1) (X(J,I),J=1,IM)
0172 31 IF(ISCT.GT.0)READ (NT1)
0173 CALL WOT(X,I01,IM,1,'INT.','G=N+',0)
0174 I03=I01+IM

```

modified
portion

modified
portion

Fig.2.4.1 Modification of Subroutine FINPR of the ANISN Code for the Data Transmission to APPLE-2

```

ISN 00001      SUBROUTINE OUTER (A0,A7,B0,B2,B4,A1,M3,B6,CO,FO,G2,I7,K6,MO,M2,M4,OUTRO010
1 M5,M6,M7,N2,N4,P2,P4,SO,S2,S4,T7,VO,V7,W0,W1,W2,X0,JMG,X1,X2,Z5,OUTRO020
2 F2,A5,P3,S3,J3,BSR,BST,E0,E1,E2,E3,E4,E5,E6,E7,F5,F6,F7,ITLP,OUTRO030
3 ITMT,IMJMP,NOMAP,ISIZE1,ISIZE2,IGG,ALBDOR,ALBDOT,ALBDOB,IIGM,IMP,OUTRO040
4 JMP,IMAFIX,JSC,CBAN,IZB,D1,D2,D3,D4,D5,D6,BSL,BSB,ISIZE3,V1,V2,OUTRO050
5 V3,V4,V5,NOMG,A)OUTRO060
C              OUTRO070
C***** OUTER CONTROLS AN OUTER ITERATION, READS DISTRIBUTED SOURCE,OUTRO080
C***** BOUNDARY SOURCE(S), FIRST COLLISION SOURCE, AND COMPUTESOUTRO090
C***** DOWNSCATTER AND UPSCATTER SOURCESOUTRO100
C              OUTRO110
ISN 00002      COMMONOUTRO120
1 NINP,NOUT,NCR1,NFLUX1,NSCRAT,NAFT,NBSO,NFLSV,NPSO,NZBT,NBFT,NGAMOUTRO130
ISN 00003      COMMON ALA,AV,AVP,AVR,B05,B06,B07,CNT,CTL,CVT,DEN,DENOM,DISCR,OUTRO140
1 D01,D02,D03,D04,EQ,EGA,EQB,EQC,EQR,EGS,EVA,EVB,EVP,EVPP,EV1,EV2,OUTRO150
2 E01,E02,E03,E04,E05,F,GBAR,IAFP,IBB,IBL,IBR,IBT,IFOT,IGEP,IGK,OUTRO160
3 IGP,IGV,IG1,IHG,II,IMJM,IP,IT,ITEMP,ITP,IZP,ITEMP1,ITEMP2,JP,KO1,OUTRO170
4 KO2,KO3,KO4,KO5,KO6,KO7,LAP,LAPP,LAR,LC,MBAR,MJMK,ML,MM,MMAFLX,OUTRO180
5 MMDN,MMIFLX,MMIM,MMIP,MMJFLX,MMJM,MMLT,MMRT,MMUP,NB,NBAR,NGOTO,OUTRO190
6 NOM,NOMA,NUM,PBAR,PO2,PO7,SBAR,SIM,SIMJM,SJM,SBAR1,SK7,SUMW1,OUTRO200
7 SUMW2,TC,TEMP,T1,TEMP1,TEMP2,TEMP3,TEMP4,TO6,T10,T11,T12,T15,T16,OUTRO210
8 T17,UP,UP1,UP2,VBL,VHL,VLL,VNL,VRL,VTL,VVL,VO7,V10,V11,V12,V13,OUTRO220
9 V14OUTRO230
ISN 00004      COMMON ID(18),OUTRO240
1 A01,A02,A03,A04,IGE,IZM,IM,JM,IO4,EV,EVM,EPS,B01,B02,B03,B04,OUTRO250
2 M07,FXT,MT,M01,MCR,MTP,I2,J2,S02,S03,IGM,IHT,IHS,ITL,S01,M05,M06,OUTRO260
3 S04,D05,G07,G05,G06,LAL,LAH,POD,EPSA,IAFT,IZC,IMG,ISC,IS2,IS3,OUTRO270
4 ITI,IP1,IP2,IP3,IP4,IP5,IB1,IB2,IB3,IB4,IB5,IB6,IZ1,IZ2,IZ3,IZ4,OUTRO280
5 IZ5,IZ6,J11,J12,J13,J14,J15,J16OUTRO290
ISN 00005      COMMON LLL(2),LCO,LS2,LB2,LB4,LN2,LA0,LA1,LA5,LA7,LB0,LB6,LS3,OUTRO300
1 LJ3,LP3,LBSR,LBST,LBSS,LBSL,LBSB,LFO,LF2,LG2,LIO,L11,L12,L13,OUTRO310
2 LI7,LK6,LK7,LMO,LM2,LM3,LM4,LMS,LM6,LM7,LN4,LP2,LP4,LRO,LR1,LR2,OUTRO320
3 LR3,LR4,LR5,LS0,LS4,LT7,LV0,LV7,LW0,LW1,LW2,LZ0,LZ1,LZ2,LZ3,LZ4,OUTRO330
4 LZ5,LX0,LX1,LX2,LE0,LE1,LE2,LE3,LE4,LE5,LE6,LE7,LF5,LF6,LF7,LMB,OUTRO340
5 LM9,LABDR,LABDT,LABDB,LJMG,LJSC,LCBAN,LIZB,LD1,LD2,LD3,LD4,LD5,OUTRO350
6 LD6,LV1,LV2,LV3,LV4,LV5,LV6,LC1,LC2,LC3,LC4,LC5,LC6,LA5,OUTRO360
ISN 00006      DIMENSION A(1)OUTRO370
C              OUTRO380
ISN 00007      DIMENSION P3(1),JSC(1),E0(1),E1(1),E2(1),E3(1),E4(1),E5(1),E6(1),OUTRO390
1 E7(1),F5(1),F6(1),F7(1),JMG(1),X1(1),X2(1),A0(1),A7(1),I7(1),OUTRO400
2 K6(1),M2(1),M4(1),M5(1),A1(1),M3(1),M6(1),M7(1),T7(1),V7(1),OUTRO410
3 W0(1),W1(1),W2(1),X0(1),Z5(1),B0(1),B2(1),B4(1),B6(1),FO(1),OUTRO420
4 G2(1),MO(1),N4(1),P2(1),P4(1),S0(1),S2(1),VO(1),V1(1),V2(1),OUTRO430
5 V3(1),V4(1),V5(1),F2(1),A5(1),CO(ITLP,1),BSR(1),BST(1),BSL(1),OUTRO440
6 BSB(1),S3(IMJMP,1),J3(IMJMP,KO4,1),N2(IMJMP,1),S4(IMJMP,1),OUTRO450
7 ALBDOR(JMP,1),ALBDOT(IMP,1),ALBDOB(IMP,1),CBAN(IMJMP,1),IZB(1),OUTRO460
8 D1(1),D2(1),D3(1),D4(1),D5(1),D6(1),NOMG(1)OUTRO470
ISN 00008      INTEGER S02,A02,A03,B01,B02,B03,B04,D05,E04,FXT,GBAR,G07,PBAR,OUTRO480
1 SBAR,SBAR1,T15,T16,T17,UP,A04,PO2,GOLDOUTRO490
ISN 00009      REAL K6,M5,M7,NBAR,N2,N4,NUM,M3,J3OUTRO500
ISN 00010      CALL TIMSTR (1)OUTRO510
ISN 00011      CALL TIMON (1)OUTRO520
ISN 00012      CALL REWND(NFLSV)OUTRO530
ISN 00013      WRITE(NFLSV) IGM,IM,JM,IZM,IGE
ISN 00014      CALL WANDR4(NFLSV,A(LRO),IP,A(LZO),JP,A(LMO),IMJM,A(LVO),IMJM,1)
C
ISN 00015      IF(IZ4.GT.0) CALL REWND(IZ4)OUTRO540
ISN 00016      IF(I04.EQ.6) CALL REWND(NPSO)OUTRO550
ISN 00017      IF(IB5.NE.0 .OR. IB6.NE.0) REWIND NBFTOUTRO555
ISN 00018      IGV=1OUTRO560
C***** SECTION --24 FIXED SOURCE *****OUTRO570
ISN 00019      UP1=0.0OUTRO580
ISN 00020      124 CONTINUEOUTRO590
ISN 00021      KO1=A03OUTRO600
ISN 00022      IF(IB4.NE.1) GO TO 3724OUTRO610
ISN 00023      KO1 = I7(IGV)OUTRO620
ISN 00024      NOMA=(KO1*(KO1+3))/2OUTRO630
ISN 00025      3724 IF(I04.NE.1) GO TO 3324OUTRO640
ISN 00026      3324 IF(K02)3224,324,3224OUTRO650
ISN 00027      3224 DO 224 I=1,NOMOUTRO660
ISN 00028      S4(I,1)=0.0OUTRO670
ISN 00029      224 CONTINUEOUTRO680
ISN 00030      324 CALL WANDR2(NCR1,CO(1,1),ITL*MT,S2(1),MJMK,2)OUTRO690
ISN 00031      IF(I04.NE.6) GO TO 424OUTRO700
ISN 00032      CALL WANDR2(NPSO,S2(1),IMJM,S4(1,1),NOM,2)OUTRO710
ISN 00033      424 IF(I04.EQ.0.OR.I04.EQ.6) GO TO 8024OUTRO720
ISN 00034      DO 624 I=1,IMJMOUTRO730
ISN 00035      624 S2(I)=0.0OUTRO740
ISN 00036      8024 IF(IB1.EQ.0.OR.I04.EQ.5) GO TO 724OUTRO750
ISN 00037      DO 8004 L = 1,IB1OUTRO760
ISN 00038      D1(L) = 0.0OUTRO770
ISN 00039      8004 CONTINUEOUTRO780
ISN 00040      8003 DO 8000 IJ=1,IMJMOUTRO790
ISN 00041      ITEMP=MO(IJ)OUTRO800

```

2 cards added

Fig.2.4.2 Modification of Subroutines OUTER, TPSAVE, TPXF of the DOT-3.5 Code for the Data Transmission to APPLE-2


```

ISN 00001      SUBROUTINE TPSAVE(N2,IMJM,IGM,IGG,IFOT,J3,NOM,B2,B4,MMIM,MMJM,ITI,TPSV0010
                1 NOMG)                                TPSV0020
C                                                       TPSV0030
C***** TPSAVE WRITES SCALAR FLUXES, MOMENTS AND SYSTEM BOUNDARY TPSV0040
C***** ANGULAR FLUXES ON NFLSV                        TPSV0050
C                                                       TPSV0060
ISN 00002      COMMON NINP,NOUT,NCR1,NFLUX1,NSCRAT,NAFT,NBSO,NFLSV,NPSO TPSV0070
ISN 00003      DIMENSION N2(IMJM,IGG),J3(NOM,IGG),B2(9),B4(9),NOMG(1) TPSV0080
ISN 00004      REAL N2,J3                                TPSV0090
ISN 00005      1234 REWIND NFLUX1                        TPSV0100
CRG           REWIND NFLSV                               this statement is deleted TPSV0110
ISN 00006      DO 1236 IIG =1,IGM                       TPSV0120
ISN 00007      IGI = IIG                                TPSV0130
ISN 00008      IF(IFOT.EQ.0) GO TO 1233                 TPSV0140
ISN 00009      IGI = 1                                  TPSV0150
ISN 00010      IF(NFLUX1.EQ.NFLSV) GO TO 1237           TPSV0160
ISN 00011      CALL WANDR4(NFLUX1,N2(1,IG1),IMJM,J3(1,IG1),NOMG(IIG),B2(1),MMJM, TPSV0170
                1B4(1),MMIM,2)                          TPSV0180
ISN 00012      GO TO 1235                                TPSV0190
ISN 00013      1233 CALL WANDR2(NFLUX1,B2(1),MMJM,B4(1),MMIM,2) TPSV0200
ISN 00014      1235 CALL WANDR4 (NFLSV,N2(1,IG1),IMJM,J3(1,IG1),NOM,B2(1),MMJM,B4(1), TPSV0210
                1MMIM,1)                                TPSV0220
ISN 00015      1236 CONTINUE                            TPSV0230
ISN 00016      1237 RETURN                              TPSV0240
ISN 00017      END                                      TPSV0250

ISN 00001      SUBROUTINE TPXF(NFLUX,NFLUX1,N2,J3,B2,B4,UF,IGRP,FO,FN,N20,J30, TPXF0010
                1 B20,B40,FI,FJ,ICF,IUCF,IK,JK,IKJK,NOM,NOMA,IEDIT,NOUT,NPSO,A) TPXF0020
ISN 00002      COMMON/CPYBU/X(1),LIMX,LBEGIN,LFP,LE,LIGRP,LFN,LFO,LN20,LJ30, TPXF0030
                1 LB20,LB40,LSP,L1,L2,L3,L4,L5,L6,LAST,IAO4,IAO3, NOM1,NOMA1, TPXF0040
                2 IB01,IB02,IB03,IB04,JZ1,JZ2,ML,IMK,JMK,IMJMK,IGMA,MMJKI,MMIKI, TPXF0050
                3 IFLUX,IGMI,IAO3I,IAO4I,ISRCE,IGIXS,DUMBU(4) TPXF0060
ISN 00003      DIMENSION A(1)                          TPXF0070
ISN 00004      DIMENSION N2(1),J3(IKJK,1),B2(1),B4(1),IGRP(1),FO(1),FN(1),N20(1), TPXF0080
                1 J30(IKJK,1),B20(1),B40(1),FI(IK,1),FJ(JK,1),UF(1),Q0(1) TPXF0090
ISN 00005      REAL N2,N20,J3,J30                      TPXF0100
C                                                       TPXF0110
ISN 00006      IF(ICF.EQ.3)                            GO TO 11
ISN 00007      REWIND IFLUX
ISN 00008      CALL WANDRO(IFLUX,2) this statement is inserted
ISN 00009      11 CONTINUE
ISN 00010      REWIND NFLUX1                            TPXF0120
ISN 00011      MMJK=IAO4*JMK                            TPXF0130
ISN 00012      MMIK=IAO4*IMK                            TPXF0140
ISN 00013      IF(IUCF.GT.0) CALL WANDRO(NPSO,IGMA)    TPXF0150
ISN 00014      DO 12 I=1,IGMA                          TPXF0160
ISN 00015      12 IF(IGRP(I).LE.0) IGRP(I)=I          TPXF0170
C***** SEARCH FOR FLUX GROUP TO USE *****
ISN 00016      IGT=0                                    TPXF0180
ISN 00017      DO 100 IIG=1,IGMA                       TPXF0190
ISN 00018      IGR=IGRP(IIG)                           TPXF0200
ISN 00019      80 IF(IGRO.EQ.IGOT) GO TO 90            TPXF0210
ISN 00020      IGT=IGOT+1                              TPXF0220
                TPXF0230

```

Fig.2.4.2 Modification of Subroutines OUTER, TPSAVE, TPXF of the DOT-3.5 Code for the Data Transmission to APPLE-2 (Continued)

```

C ** ENERGY WIDTH
ISN 00215 EDELTA = EPREV-E(IEP)
C ** LETHARGY
ISN 00216 RATIOE = EPREV/E(IEP)
ISN 00217 UDELTA = ALOG(RATIOE)
ISN 00218 EPREV = E(IEP)
ISN 00219 1980 CONTINUE
ISN 00220 DO 1977 I=ID11, ID12, NE
ISN 00221 IF(NFOUT) 1977, 1982, 1983
C1982 E(I) = E(I)*EDELTA
1982 E(I) = E(I)*EDELTA*FACTR
GO TO 1977
1983 E(I) = E(I)*EDELTA/UDELTA
1977 CONTINUE
WRITE (IO, 1070) (E(I), I=ID11, ID12, NE)
1070 FORMAT (17X, 1P10E10.3)
DO 1978 I=ID11, ID12, NE
IF(NFOUT) 1978, 1984, 1985
1984 E(I) = E(I)/EDELTA/FACTR
C1984 E(I) = E(I)/EDELTA
GO TO 1978
1985 E(I) = E(I)/EDELTA*UDELTA
1978 CONTINUE
C * * OUTPUT FOR FLUX * * *
J = ID1
DO 2030 I=ID11, ID12, NE
FNE(IE, J) = E(I)
J = J+1
2030 CONTINUE
ID11 = ID11 + NEND
ID12 = ID12 + NEND
WRITE (IO, 1080) (E(I), I=ID11, ID12, NE)
1080 FORMAT (17X, 10(F9.3, 1X))
J = ID1
DO 2040 I=ID11, ID12, NE
FSD(IE, J) = E(I)
J = J+1
2040 CONTINUE
ENE(IE) = E(IEP)
205 WRITE (IO, 1090) E(IEP)
1090 FORMAT (1X, 1PE11.3)
C * * PUNCH OUT ENERGY BOUNDARIES * *
ISN 00251 NFX = 10
ISN 00252 REWIND NFX
ISN 00253 WRITE(NFX) NNE, NE, ND
ISN 00254 WRITE(NFX) EFIRST, EGTOP, (ENE(IE), IE=1, NE)
ISN 00255 DO 2050 ID=1, ND
ISN 00256 WRITE(NFX) (FNE(IE, ID), IE=1, NE)
ISN 00257 WRITE(NFX) (FSD(IE, ID), IE=1, NE)
ISN 00258 2050 CONTINUE
ISN 00259 ENDFILE NFX
ISN 00260 REWIND NFX
ISN 00261 2010 FORMAT(12I6)
ISN 00262 2020 FORMAT(6E12.5)
ISN 00263 210 IF (NT) 375, 375, 215
ISN 00264 215 NRM = (NRESP-1)/10 + 1
ISN 00265 NTM = (NT-1)/17 + 1
ISN 00266 IHP = IH1
C * * OUTPUT SQT AND SQT2 IN THE FOLLOWING LOOP
ISN 00267 DO 275 I=1, ND
ISN 00268 DO 275 INR=1, NRM
ISN 00269 IR1 = (INR-1)*10 + 1
ISN 00270 IF (INR-NRM) 220, 225, 225
ISN 00271 220 IR2 = IR1 + 9
ISN 00272 GO TO 230
ISN 00273 225 IR2 = NRESP
ISN 00274 230 DO 275 INT=1, NTM
ISN 00275 IST = LOCQTE - 19
ISN 00276 WRITE (IO, 1100) IHP, I, (NUMB(IPR), IPR=IST, LOCQTE)
ISN 00277 1100 FORMAT (A1, 11HDETECTOR NO, I3, 5X, 32HRESPONSE (RESPONSE, TIME, DETECTOR
1), 1X, 20A4)
IF (NT-8) 235, 235, 240
235 IHP = IH2
240 IT1 = (INT-1)*17 + 1
IF (INT-NTM) 245, 250, 250
245 IT2 = IT1 + 16
GO TO 255
250 IT2 = NT
255 IF (INT-1) 260, 260, 265
260 AGS = E(LOCXD + 4*ND + I)
GO TO 270
265 ISUB = LOCT + (I-1)*NT + IT1 - 1
AGS = E(ISUB)
270 WRITE (IO, 1110) (IR, IR=IR1, IR2)
1110 FORMAT (4X, 9H RESPONSE, 10I10)

```

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Fig.2.4.3 Modification of Subroutine NRUN of the MORSE Code for the Data Transmission to APPLE-2

```

ISN 00001      SUBROUTINE SUMMARY(XKI,FD,XN, VE,W,DSN,MA,MZ,CRX,Q,PA,DF,I2,CA,CF,ANS30040
1CT,CS,V,AA,TAB,WD,XND,FXS,FIS,SNN,SFS,OTS,APS,FRT,TXN,DEN,RFL,RCT,ANS30050
2RLK,XLL,XLK,XBB,RXN,IG1,I1,IH1,IGM1,M1,IM1) ANS30060
C *** SUMMARY PRINTS ANGULAR FLUXES AND COMPUTES SUMMARY TABLES ANS30070
ISN 00002      DIMENSION XKI(1),FD(1),XN(I1,1), VE(1),W(1),DSN(1),MA(1),MZ(1) ANS30080
1,CRX(IH1,IGM1,1),Q(I1,1),PA(M1,IM1,1),DF(1),CA(1),CF(1),CT(1), ANS30090
2 CS(1),V(1),AA(1),TAB(1),WD(1),XND(I2,1),FXS(IG1,1),FIS(IG1,1), ANS30100
3 SNN(IG1,1),SFS(IG1,1),OTS(IG1,1),APS(IG1,1),XLK(IG1,1),XBB(IG1,1) ANS30110
4,RXN(IG1,1),RFL(IG1,1),RCT(IG1,1),RLK(IG1,1),XLL(IG1,1),FRT(IG1,1) ANS30120
5, TXN(IG1,1),DEN(IG1,1) ANS30130
ISN 00003      COMMON /BULKBU/ ANS30140
* D(1),LIM1,LXKI,LFD,LXN,LR,LVE,LW,LDSN,LMA,LMZ,LMB,LMC,LXMD, ANS30150
1LMTT,LCRX,LFIX,LFLT,LQ,LPA,LJ5,LRM,LDF,LJ3,LJ4,LIGT,LART,LALFT, ANS30160
2LFGP,LFGG,LEND,LV,LAA,LWD,LMR,LPNC,LXJ,LCH,LCA,LCF,LCT,LCS,LTAB, ANS30170
3LXND,LSA,LSAT,LRAV,LRA,LXNN,LXNE,LXNR,LXNA,LSR,LST,LQG,LFG,LSG, ANS30180
4LXKE,LXNI,LXNO,LT3,LT5,LDA,LDB,LDC,LDS,LB,IGMP,IGMM,IIGG,NERR,IMJT ANS30190
5,IHG,IMP,MP,NDS,NUS,SDG,SCG,AG,XNLGG,XNLG,SNG,ALA,ASR,EAM,EPG,EG, ANS30200
6E1,E2,E3,E4,E5,E6,E7,EB,E9,E10,E11,E12,E13,E14,E15,E16,E17,E18,E19 ANS30210
7,E20,ESC,ESM,EVP,EVPP,FTP,IC,ICVT,IGP,IG,IHP,IIC,IIG,IP,I2P,I01, ANS30220
8I02,I03,I04,I05,I06,I07,I08,I09,I00,JT,LC,MG,MI,ML,MM,NFN,XITR, ANS30230
9XLAP,XLAPP,XLAR,XLA,XNIG,XNII,ZZ1,ZZ2,ZZ3,XNB,XKEP,XXIP,IH,I,K,L, ANS30240
AM,J,N,NN,ISV, ANS30250
BID,ITH,ISCT,ISN,IGE,IBL,IBR,IZM,IM,IEVT,IGM,IHT,IHS,IHM,MS,MCR,MTP ANS30260
C,MT,IDFM,IPVT,IGM,IPM,IPP,IIM,ID1,ID2,ID3,IDA,ICM,IDAT1,IDAT2,IFG, ANS30270
DIFLU,IFN,IPRT,IXTR, ANS30280
EEV,EVM,EPS,BF,DY,DZ,DFM1,XNF,PV,RYF,XLAL,XLAH,EQL,XNPM, ANS30290
FT(12),NIN,NOU,NT1,NT2,NT3,NT4,NT5,NT6,NT7 ANS30300
ISN 00004      COMMON/NEWOP1/ IIBOUD,IISPTM,IIANLL,NNXNN(4),YGRENE(101), ANS30301
* NOANNO,HOANLL(10),AWSEDR(21) ANS30302
COMMON/NEWOP2/ XNXNN(30000) ANS30303
ISN 00005      IF(ID1.GE.0.OR.ID1.EQ.-2) GO TO 80
ISN 00006      NTX=11
ISN 00007      REWIND NTX
ISN 00008      WRITE(6,2220)
ISN 00009      2220 FORMAT(1H1)
ISN 00010      80 CONTINUE
ISN 00011      DO 1 IIG=1,IGM ANS30310
ISN 00012      IIGG=IIG ANS30320
ISN 00013      READ (NT4)((XND(I,M),I=1,IP),M=1,MM) ANS30330
ISN 00014      IF(ID1.GE.0.OR.ID1.EQ.-2) GO TO 81
ISN 00015      WRITE(NTX)((XND(I,M),I=1,IP),M=1,MM)
ISN 00016      WRITE(6,2222) IIG,NTX,IP,MM
ISN 00017      2222 FORMAT(1H ,5X,'GRP.',I4,' ANGULAR FLUX WAS WRITTEN ON MT=',I3,5X,
ISN 00018      * '( MESH POINTS =',I4,3X,'DIRECTIONS =',I3,')')
ISN 00019      GO TO 2
ISN 00020      81 CONTINUE
ISN 00021      C IF(ID1.EQ.0 .OR. ID1.EQ.2)GO TO 2 ANS30340
IF(ID1.LE.0 .OR. ID1.EQ.2)GO TO 2
C *** PRINT ANGULAR FLUX ANS30350
ISN 00022      IF(IIG.NE.1) GO TO 3333 ANS30351
ISN 00023      WRITE (NOU,10)IIG ANS30360
ISN 00024      GO TO 3334 ANS30361
ISN 00025      3333 CONTINUE ANS30362
ISN 00026      WRITE(NOU,3335) IIG ANS30363
ISN 00027      3335 FORMAT(////,1X,' FLUX BY ANGLE AND POINT FOR GROUP ',I3) ANS30364
ISN 00028      3334 CONTINUE ANS30365
ISN 00029      10 FORMAT(37H1 FLUX BY ANGLE AND POINT FOR GROUP I3) ANS30370
ISN 00030      IF(IIANLL.EQ.1) GO TO 4444 ANS30371
ISN 00031      CALL WOT(XND,MM,IP,1,'PNT.','ANGL',0) ANS30380
ISN 00032      GO TO 4445 ANS30381
ISN 00033      4444 CONTINUE ANS30382
ISN 00034      CALL NWSUB3(XND,IP,MM,XNXNN) ANS30383
ISN 00035      4445 CONTINUE ANS30384
ISN 00036      2 IF(IDAT1.EQ.0)GO TO 3 ANS30390
ISN 00037      IIGG=1 ANS30400
ISN 00038      READ (NT3) ((CRX(IH,1,M),IH=1,IHP),M=1,MT) ANS30410
ISN 00039      I01=MP*IMP ANS30420
ISN 00040      IF(IEVT.EQ.0)READ (NT3) (Q(I,1),I=1,I01) ANS30430
C *** COMPUTE SUMMARY TABLES ANS30440
ISN 00041      3 IH=IHM ANS30450
ISN 00042      4 K=IIG+IHS-IH ANS30460
ISN 00043      IF(K.LE.0)GO TO 5 ANS30470
ISN 00044      IF(K.GT.IGM)GO TO 6 ANS30480
ISN 00045      IF(IDAT1.NE.2)GO TO 7 ANS30490
ISN 00046      K=1 ANS30500
ISN 00047      READ (NT1) (XN(I,1),I=1,IM) ANS30510
ISN 00048      IF(ISCT.GT.0)READ (NT1) ANS30520
ISN 00049      7 DO 8 I=1,IM ANS30530
ISN 00050      J=MA(I) ANS30540
ISN 00051      L=IABS(MZ(J)) ANS30550
ISN 00052      J=MINO(J,IZM) ANS30560
ISN 00053      E4=V(I) ANS30570
ISN 00054      IF(IDFM.GT.0)E4=E4*DF(I) ANS30580
ISN 00055      IF(IH.NE.IHS)GO TO 39 ANS30590

```

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Fig.2.4.4 Modification of Subroutine SUMMARY of the ANISN Code for Angular Flux Data Transmission

2.5.3 Input Notes and Descriptions

(a) Overview plot of scalar neutron flux

The overview plot mentioned here is the graph of spatial distribution of neutron spectra. For the overview plot, IDENT = FLUX and SPEC input data are necessary. The Z-axis corresponds to values of neutron flux (in log scale), X-axis corresponds to energy (log scale) and Y-axis corresponds to position (linear scale). Origin of the coordinate system will be at the point corresponding to the lowest energy and first mesh point.

As shown in Fig.2.4.5, the angle between Z-axis and the viewpoint vector is THETA and the rotation angle of the plane including viewpoint vector around from the X-axis towards the Y-axis is PSI. For example, if THETA = 0° , the overview from Z-axis direction will be given. By changing the value of PSI, the position of origin, X-axis and Y-axis may be changed. VIEWPT is the distance of the viewpoint from the origin. Suggested values are THETA = 45.0, PSI = 45.0 and VIEWPT = 1000.0.

When the plotting machine allows the exchange of the colour of the pen, pen No.1 (black pen) draws hidden parts of the overview, pen No.2 (red pen) the surface, and pen No.3 (blue pen) the frame and contour lines.

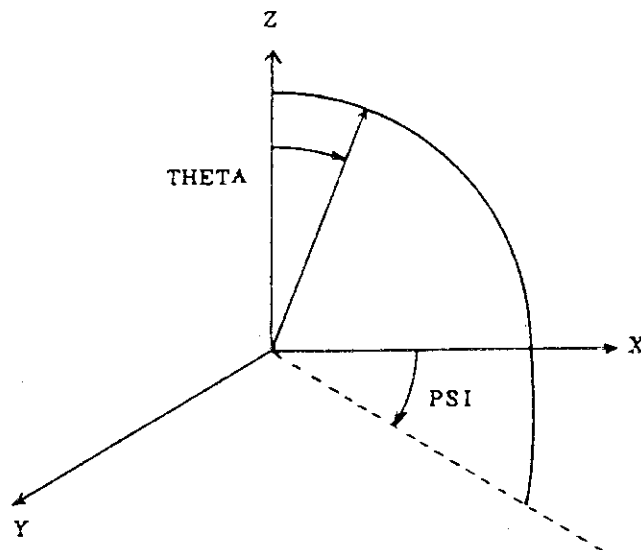


Fig.2.4.5 Angles for Overview Plotting

(b) Calculation and plotting of reaction rates

Reaction rates for each interval, zone and for the whole system are calculated. The plot symbol of reaction rate is given at the midpoint of each interval and the plotted symbols are connected by straight line. The points may be connected by smooth curve by changing NTRA specified in SUBROUTINE MLOT1 to a positive value.

For the plotting of reaction rates, IDENT = FLUX, CROS, RCAL, RPLT data are required. By repeating IDENT = RCAL input data, any number of reaction rates for different neutron fluxes with same number of energy groups and same number of mesh points, may be plotted on a graph.

The implication of IDENT = CROS data for reading cross section input and making mixing table and IDENT = RCAL data for reaction rate plotting is quite similar to their counter-parts in ANISN. There are following options for choosing the material numbers ID22 for reaction-rates calculations which are input as 22¥ data of IDENT = RCAL.

(i) ID22 > 0,

(a) ID22 ≤ MCR, i.e. when ID22 is equal to one of the component numbers input as 11\$ data, the reaction rate for the component element (nuclide)

$$R_i^m = \sum_g \sigma_g^m N^m \phi_{gi}$$

is calculated and plotted. Here,

g ; energy group number,

m ; element number,

i ; spatial mesh number,

σ ; microscopic cross section (14 * data),

N ; atom density (12 * data),

φ ; neutron flux.

(b) ID22 > MCR, i.e. when ID22 is equal to one of the mixture number specified as 10% data, the reaction rate of the mixture

$$R_i = \sum_m \sum_g \sigma_g^m N^m \phi_{gi}$$

is calculated and plotted.

(ii) ID22 < 0,

$$R_i^m = \sum_g \sigma_g^m \phi_{gi}$$

is calculated and plotted. In this case, $N^m = 1.0$ so that cross section input (14 * data) may be macroscopic.

(c) Restrictions

Variable dimensioning is employed in APPLE. There is no practical limitation in the number of reaction rates to be calculated and plotted on a graph, but a same type of plot symbol will appear for every 17th reaction rate curves.

If a problem requiring larger core size than 50 kW is to be solved, two cards in the FTMAIN routine of APPLE specifying blank common requirements should be changed:

```
COMMON  D(XXXXX)
        LIMM = XXXXX
```

2.6 Output Descriptions

Most of the output list from the APPLE-2 code is self evident and does not need particular explanation. The output are summarized as follows:

(i) List of the input cards.

(ii) Input data are rearranged and explained in more detail.

Such as the meaning of the input parameters are described or the zone map is printed for the DOT flux processing.

When a response function library is used, the content list of the library is printed.

(iii) Reaction rate distribution along the specified axial or radial direction and the region integrated values of reaction rate is printed.

(iv) Neutron or gamma ray spectra value to be plotted are listed.

A sample of output listing is shown in Fig.4.3.6.

3. Response Function Libraries for Fusion Reactor Calculations

The nuclear characteristic values required in fusion reactor design are mostly in the form of reaction rate, i.e. the product of neutron or gamma ray flux and response function integrated over energy, or the volume integrated reaction rates.

The four libraries of response functions for fusion reactor calculations provided for the use with the APPLE-2 code are introduced in this Section. The record format of the libraries has been described in 2.4.2(e).

3.1 XS63 Library

This library is in the 42-group neutron, 21-group gamma ray energy group structure so that it may be used with the GICX40 cross section set⁽⁹⁾. The group structures of the GICX40 set are given in Tables A.1.1 and A.1.2. The following 17 response functions are stored in this order.

1. Response to obtain 14 MeV neutron flux ($n \cdot \text{cm}^{-2} \cdot \text{s}^{-1}$)
2. Response to obtain neutron flux with energy greater than 0.1 MeV ($n \cdot \text{cm}^{-2} \cdot \text{s}^{-1}$)
3. Response to obtain total neutron flux ($n \cdot \text{cm}^{-2} \cdot \text{s}^{-1}$)
4. Response to obtain total gamma ray flux ($\gamma \cdot \text{cm}^{-2} \cdot \text{s}^{-1}$)
5. ${}^6\text{Li}(n, \alpha)t$ reaction cross section (barn)
6. ${}^7\text{Li}(n, n'\alpha)t$ reaction cross section (barn)
7. Displacement damage cross section of SS-316 ($10^{-24} \cdot \text{dpa}$)
8. Displacement damage cross section of copper ($10^{-24} \cdot \text{dpa}$)
9. Flux to dose conversion factor ($\text{mrem} \cdot \text{h}^{-1}$)
10. Neutron flux to dose conversion factor ($\text{mrem} \cdot \text{h}^{-1}$)
11. Gamma ray flux to dose conversion factor ($\text{mR} \cdot \text{h}^{-1}$)
12. ${}^{235}\text{U}$ fission cross section (barn)

13. ^{238}U fission cross section (barn)
14. ^{232}Th fission cross section (barn)
15. ^{237}Np fission cross section (barn)
16. $^{58}\text{Ni}(n,p)^{58}\text{Co}$ reaction cross section (barn)
17. $^{58}\text{Fe}(n,\gamma)^{59}\text{Fe}$ reaction cross section (barn)

The content of the library is listed in Appendix A.1. The XS63 library is used in the sample problem in 4.1.

3.2 GICXRMA Library

This library provides kerma factors to be used with the GICX40 cross section set for the nuclear heating calculations. It has neutron and gamma ray kerma factors in 42-group and 21-group structures of the GICX40 set. It also has total kerma factors. Neutron, gamma ray and the total kerma factors are stored for each of the 40 nuclides included in the GICX40 set, in the same order as in the GICX40. The 40 nuclides are listed in Table A.2.1. A part of the library is listed in Appendix A.2. Its use is demonstrated in the sample problem 4.2.

3.3 GFLXDOSE Library

This library includes gamma ray flux to dose rate conversion factors in the 54 group structure (shown in Table A.3.1) of the GROUPIN gamma ray cross section set for decay gamma ray transport calculations. The GROUPIN cross section set is included in the THIDA code system⁽¹¹⁾ for induced activation calculations. This library is used to calculate and plot the dose rate as shown in the sample problem in 4.3. It is listed in Appendix A.3.

3.4 XS100 Library

The XS100 library includes fission cross sections of ^{235}U , ^{238}U , ^{232}Th and ^{237}Np , and two tritium producing reaction cross sections $^6\text{Li}(n,\alpha)\text{t}$ and $^7\text{Li}(n,\alpha)\text{t}$. The 100-group neutron energy group structure is the same as the DLC-2D cross section set⁽¹⁰⁾, and is shown in Table A.4.1. This library is used in the analysis of integral experiments conducted in JAERI⁽⁵⁾.

4. Sample Problems

Four sample problems are described in this section to demonstrate the versatile capabilities of the APPLE-2 code. They are characterized as follows:

- 4.1 Sample problem for ANISN flux using XS63 library
- 4.2 Sample problem for ANISN flux using GICXKRMA library
- 4.3 Sample problem for DOT flux using GFLXDOSE library
- 4.4 Sample problem for MORSE energy spectra plotting

4.1 Sample Problem 4.1 for ANISN Flux Using XS63 Library

The sample problem 4.1 gives various nuclear characteristic values, neutron and gamma ray spectra calculated in a simplified model of a fusion reactor shown in Fig.4.1.1. The infinite cylinder model includes a 100 cm radius plasma column surrounded by water layer 100 cm thick. The 14 MeV neutrons are generated uniformly in the plasma region. A 10 cm thick SS316 annulus is placed behind the water layer.

Neutron and gamma ray scalar fluxes in the calculational model were calculated by the ANISN code⁽²⁾ using the 42-group neutron, 21-group gamma ray cross section set GICX40⁽⁹⁾. The scalar fluxes and other relevant data were written on a disk file (or a magnetic tape) by the modified FINPR subroutine (see Fig.2.4.1) for the transmission to the APPLE-2 code.

The input data for this problem is listed in Fig.4.1.2. In the figure, the fifth card shows that a response library containing 17 responses is read from the logical file 1. The XS63 library described in 3.1 is allocated to the logical file 1. The job control cards of this problem by the FACOM M-200 machine in JAERI is shown in Fig.4.1.3.

Operational dose rates, neutron and gamma ray fluxes, radiation

damage rates and activation reaction rates in the model are calculated and plotted by the APPLE-2 code. All the results are normalized to unit neutron source. The plotted graphs are shown in Figs.4.1.4~4.1.6. Neutron and gamma ray energy spectra at three locations are plotted and shown in Figs.4.1.7 and 4.1.8. The overview plot of the neutron spectra is shown in Fig.4.1.9.

4.2 Sample Problem 4.2 for ANISN Flux Using GICXKRMA Library

The sample problem 4.2 gives epoxy dose rate and nuclear heating rate in the calculational model of Fig.4.1.1. Epoxy dose rate is the amount absorbed in an epoxy sample per one year if the sample is brought to the position. One 14 MeV neutron is assumed to be generated every second. Nuclear heating rate is given in the unit of $\text{MeV}\cdot\text{cm}^{-3}\cdot\text{s}^{-1}$.

The input cards for this problem is listed in Fig.4.2.1. The fifth card in the figure shows that a response library containing 40 cross section sets with three components in each set is read from the logical file 3. The GICXKRMA library described in 3.2 is assigned to the logical file 3. Therefore the mixing table begins from 41 in the 10YY data. In the mixing table, the mixtures 41 and 44 corresponds to epoxy and water. Table A.2.1 shows the list of 40 nuclides in the GICXKRMA library which is the same as that of the GICX40 set.

Plotter output of operational dose rate and nuclear heating rate are shown in Figs.4.2.2 and 4.2.3, respectively.

4.3 Sample Problem 4.3 for DOT Flux Using GFLXDOSE Library

The sample problem 4.3 gives the activation dose rate distribution calculated in a disk geometry shown in Fig.4.3.1. The disk is made of lithium oxide (Li_2O) and stainless steel structure. The 14 MeV neutrons

are generated from a point source located on the Z axis 20 cm from the disk.

The gamma ray source 1 day after shutdown was obtained using the THIDA code system⁽¹¹⁾ for activation calculation. Using the source and the 54-Group gamma ray cross section set GROUFIN⁽¹¹⁾, the gamma ray flux is calculated by the DOT code⁽⁷⁾ and stored in a disk file (or a magnetic tape) by the modified subroutines OUTER, TPSAVE and TPXF (see Fig.2.4.2) for the transmission to the APPLE-2 code.

The input data for this problem is listed in Fig.4.3.2. In the figure, the fifth card shows that a response library containing one response is read from the logical file 1, where the GFLXDOSE library described in 3.3 is allocated. The dose rate distribution is calculated and plotted. The dose rate is plotted in the axial direction along $R = 13$ cm (or the 7th radial mesh interval) and shown in Fig.4.3.3. The overview of the dose rate distribution is shown in Fig.4.3.4. The gamma ray spectra at $Z = 23$ cm and 39 cm along $R = 13$ cm are shown in Fig.4.3.5.

The output list for the sample problem 4.3 is given in Fig.4.3.6. The output list rewrites the input data with explanations. The zone map is shown in the second page of the output list. Reaction rates integrated over the whole system, zones and mesh intervals are given from the bottom of the second page of the output. Gamma ray spectra values are listed in the fourth page.

4.4 Sample problem 4.4 for MORSE Flux Energy Spectra Plotting

Neutron and gamma ray energy spectra at four locations calculated by the MORSE code are plotted in this sample. Energy group structure, group fluxes and fractional standard deviation (fsd) values were written

by the modified NRUN subroutine of the MORSE code (see Fig.2.4.3). The APPLE-2 code reads these data from the logical file 10 as shown in the second card of the input data list in Fig.4.4.1. The NON value in the IDENT=FLUX card is 1 so the flux data are read from the logical file NON+9=10. The neutron and gamma ray spectra at 4 locations are plotted and are given in Figs.4.4.2 and 4.4.3, respectively. In both figures, the flux values have error bars which denote the extent of statistical deviation (one fsd).

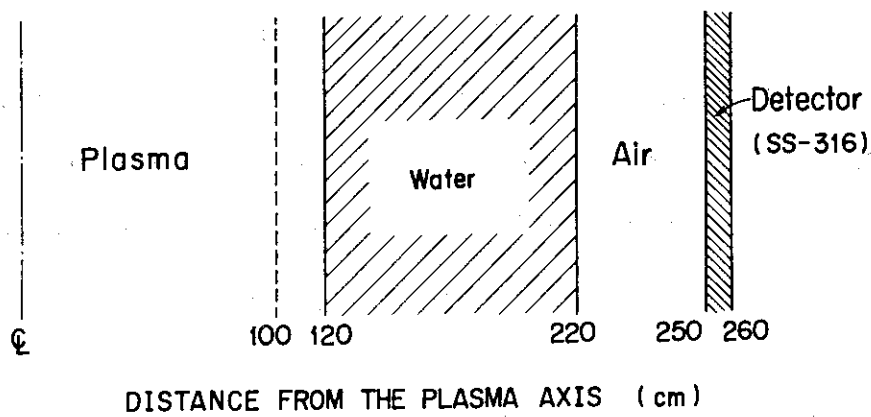


Fig.4.1.1 A Simplified Model of a Fusion Reactor

```

*** APPLE INPUT DATA CARD IMAGE LIST ***
-----1-----2-----3-----4-----5-----6-----7-----8
1 OPERATIONAL DOSE RATE SAMPLE PROBLEM <APPLE?> 00000100
2 FLUX 1 00000110
3 1 0 00000200
4 CRGS 1 00000300
5 1 17 11 1 00000400
6 10** 3R18 4R19 4R20 00000500
7 11** 9 10 11 1 2 3 4 7 8 16 17 00000600
8 12** F1 T 00000700
9 RCAL 1 00000800
10 1 1 3 1 1.0 00000900
11 9** F12 00001000
12 22** 9 10 11 00001100
13 23** F1 T 00001200
14 TOTAL NEUTRON GAMMA 00001300
15 RPLT 1 00001400
16 1 00001410
17 15.0 20.0 00001500
18 OPERATIONAL DOSE RATE (WATER) 00001600
19 DISTANCE FROM THE PLASMA AXIS (CM) 00001700
20 MREM PER HOUR PER D-T NEUTRON 00001800
21 RCAL 2 00001900
22 1 1 4 1 1.0 00002000
23 9** F19 00002100
24 22** 1 2 3 4 00002200
25 23** F1 T 00002300
26 14MEV N..1MEV N.TOTAL N.TOTALGAM 00002400
27 RPLT 2 00002500
28 1 00002510
29 15.0 20.0 00002600
30 NEUTRON AND GAMMA RAY FLUXES (WATER) 00002700
31 DISTANCE FROM THE PLASMA AXIS (CM) 00002800
32 NEUTRON AND GAMMA FLUX (PER CM**3 SEC) 00002900
33 RCAL 3 00003000
34 1 1 4 1 1.0 00003100
35 9** F20 00003200
36 22** 7 8 16 17 00003300
37 23** F1 T 00003400
38 SS DPA CU DPA N158NP FE58NG 00003500
39 RPLT 3 00003600
40 1 00003610
41 15.0 20.0 00003700
42 RADIATION DAMAGE AND ACTIVATION (WATER) 00003800
43 DISTANCE FROM THE PLASMA AXIS (CM) 00003900
44 DPA RATES AND REACTION RATES 00004000
45 SPEC 1 00004100
46 2 1 1 42 0 3 00004200
47 4 54105 00004300
48 15.0 20.0 00004400
49 NEUTRON ENERGY SPECTRA (WATER) 00004500
50 NEUTRON ENERGY (EV) 00004600
-----1-----2-----3-----4-----5-----6-----7-----8

```

```

*** APPLE INPUT DATA CARD IMAGE LIST ***
-----1-----2-----3-----4-----5-----6-----7-----8
51 NEUTRON FLUX PER UNIT LETHARGY 00004700
52 R=120CM R=170CM R=250CM 00004800
53 SPEC 2 00004900
54 2 1 1-21 0 3 00005000
55 4 54105 00005100
56 15.0 20.0 00005200
57 GAMMA ENERGY SPECTRA (WATER) 00005300
58 GAMMA ENERGY (EV) 00005400
59 GAMMA FLUX PER UNIT LETHARGY 00005500
60 R=120CM R=170CM R=250CM 00005600
61 SPEC 3 00005700
62 3 1 1 42 0 00005800
63 -1 1 10 1 1 0 45.0 60.0 1000.0 20.0 25.00005900
64 NEUTRON ENERGY SPECTRA (WATER) 00006000
65 END 0 00006100
-----1-----2-----3-----4-----5-----6-----7-----8

```

Fig.4.1.2 Input Data List for Sample Problem 4.1

```

//JCLG JOB
// EXEC JCLG
//SYSIN DD DATA,DLM='++'
// JUSER XXXXXXXX,YA.SEKI,XXXX.XXX
   T.4W.1C.2I.3P.0   GRP OPN
   OPTP PASSWORD=XXXXXXX
//*****
//*  APPLE: REACTION RATE OR ENERGY SPECTRA PLOTTING.          */
//*  READ FILE.                                                  */
//*  SCALAR FLUX FILE : ANISN OR DOT3.5 OR MORSE                */
//*  REACTION RATE CROSS SECTION : XS63 OR XS100 OR GICXKRMA    */
//*  J2372.APPLE.CNTL(APPLE)                                     */
//*****
//GO EXEC LMGO,LM='J2372.APPLEPNL'
//FT06F001 DD DCB=(BLKSIZE=137)
// EXPAND DISK,DDN=FT21F001
// EXPAND DISK,DDN=FT23F001
// EXPAND DISK,DDN=FT24F001
// EXPAND DISK,DDN=FT27F001
// EXPAND GRNLP,SYSOUT=H
// EXPAND DISKTO,DDN=FT10F001,DSN='J2372.SPTR03'
// EXPAND DISKTO,DDN=FT01F001,DSN='J2372.APPLE',Q='.DATA(XS63)'
// EXPAND DISKTO,DDN=FT02F001,DSN='J2372.APPLE',Q='.DATA(XS100)'
// EXPAND DISKTO,DDN=FT03F001,DSN='J2372.GICXKRMA'
// EXPAND DISKTO,DDN=SYSIN,DSN='J2372.APPLE',Q='.DATA(SS316)'
++
//

```

Fig.4.1.3 List of Job Control Cards for Sample Problem 4.1

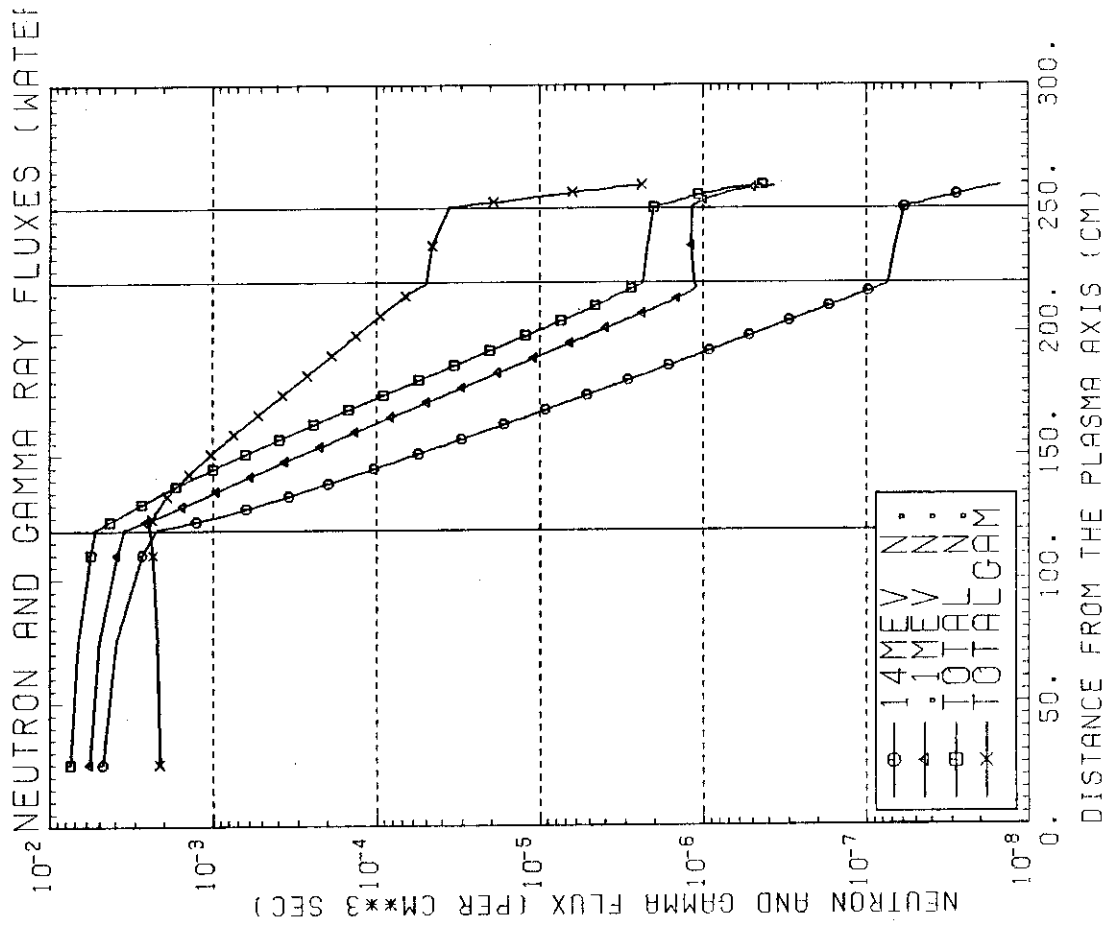


Fig.4.1.5 Plotter Output of Neutron and Gamma Ray Fluxes

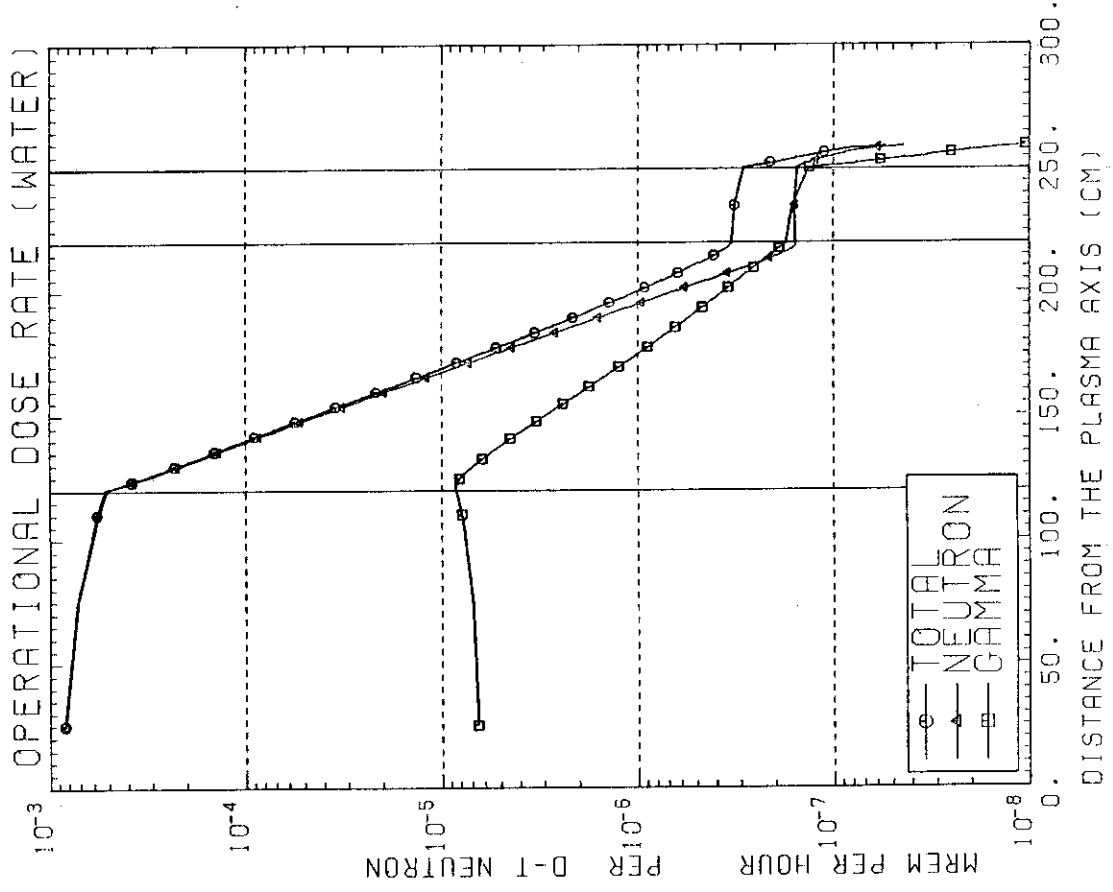


Fig.4.1.4 Plotter Output of Operational Dose Rate

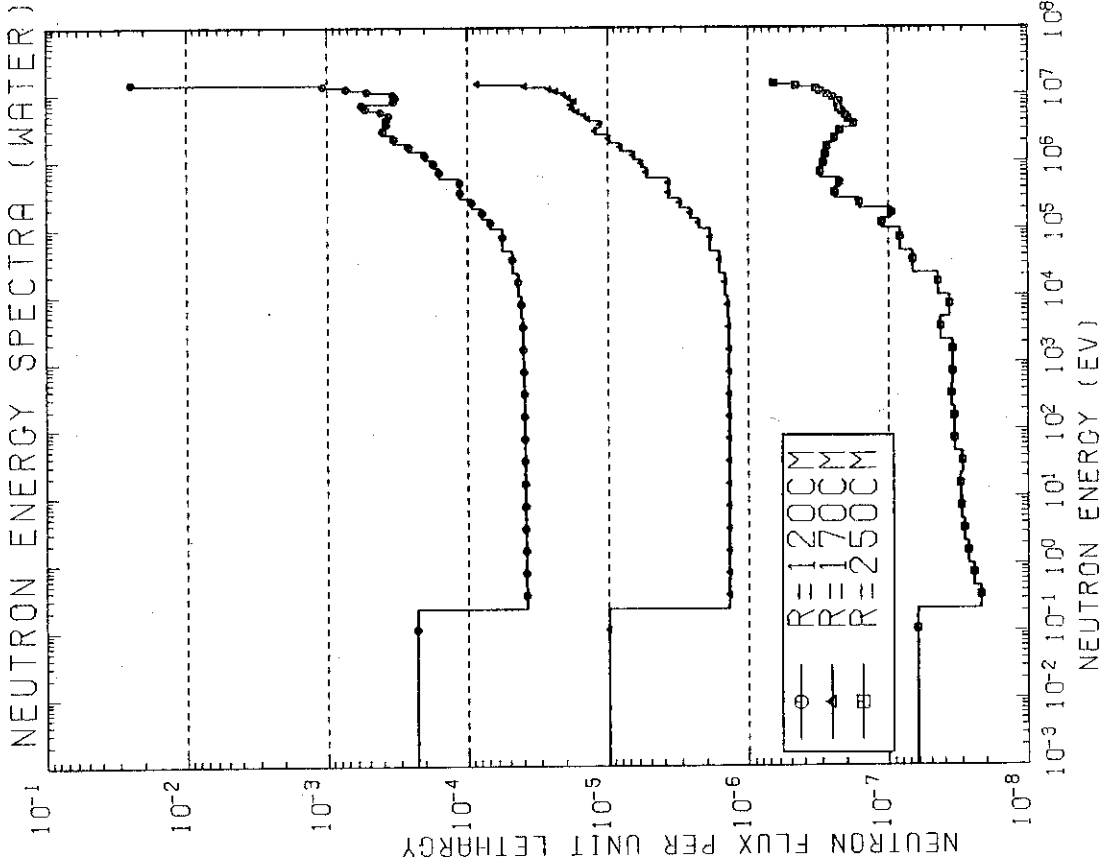


Fig.4.1.7 Plotter Output of Neutron Spectra at 3 Locations

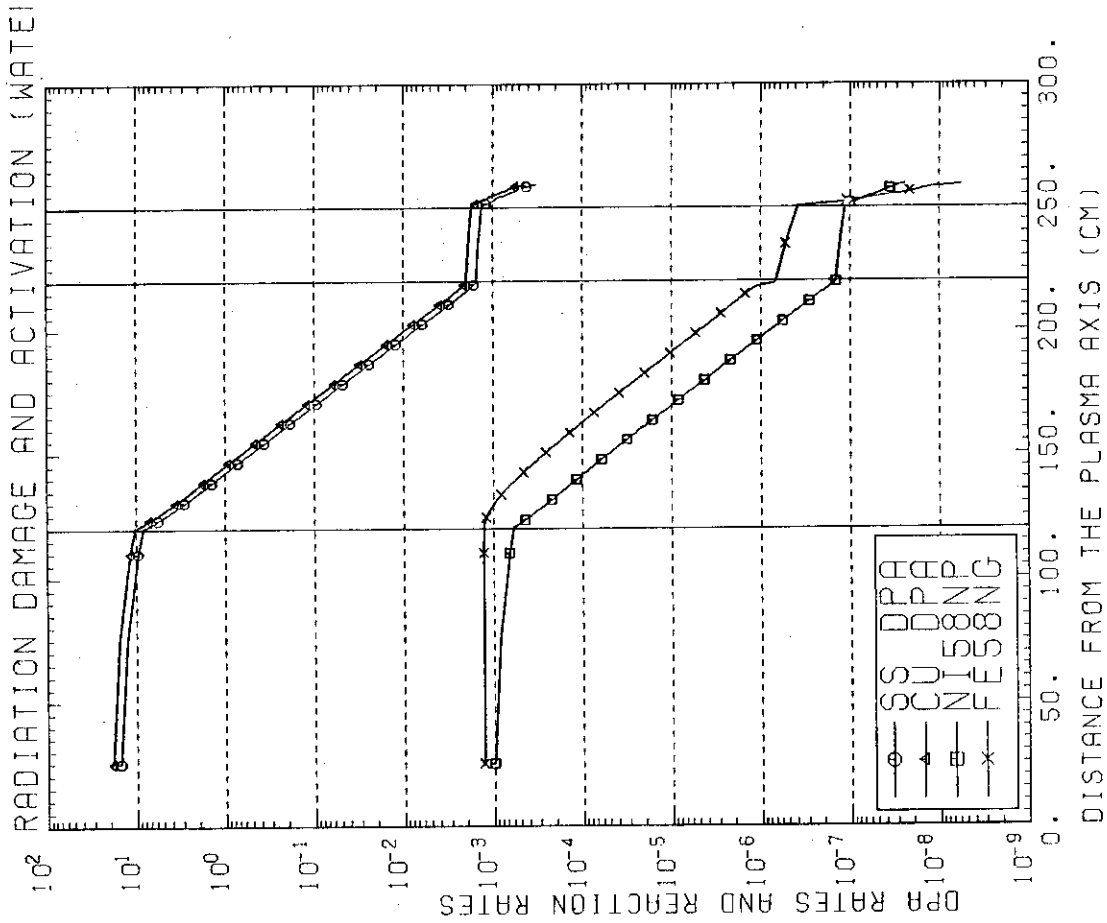


Fig.4.1.6 Plotter Output of Damage Rates and Activation Reaction Rates

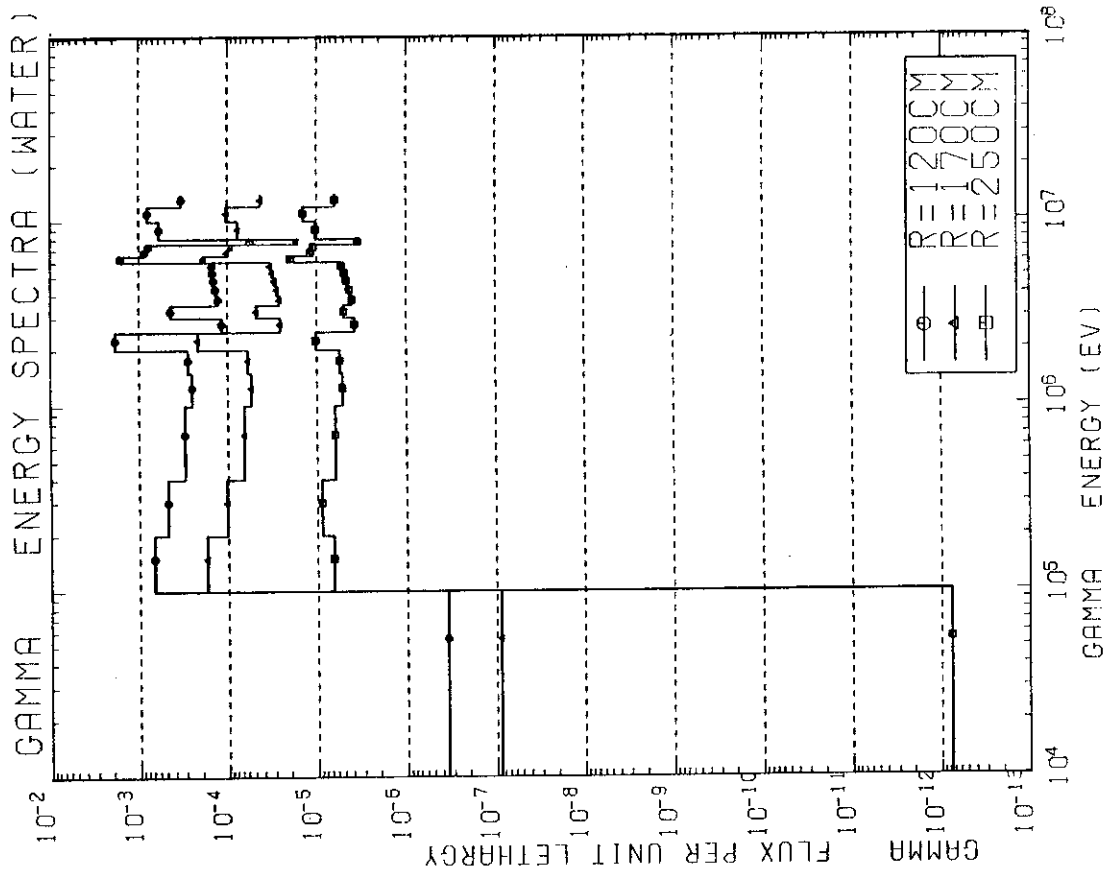


Fig.4.1.8 Plotter Output of Gamma Ray Spectra at 3 Locations

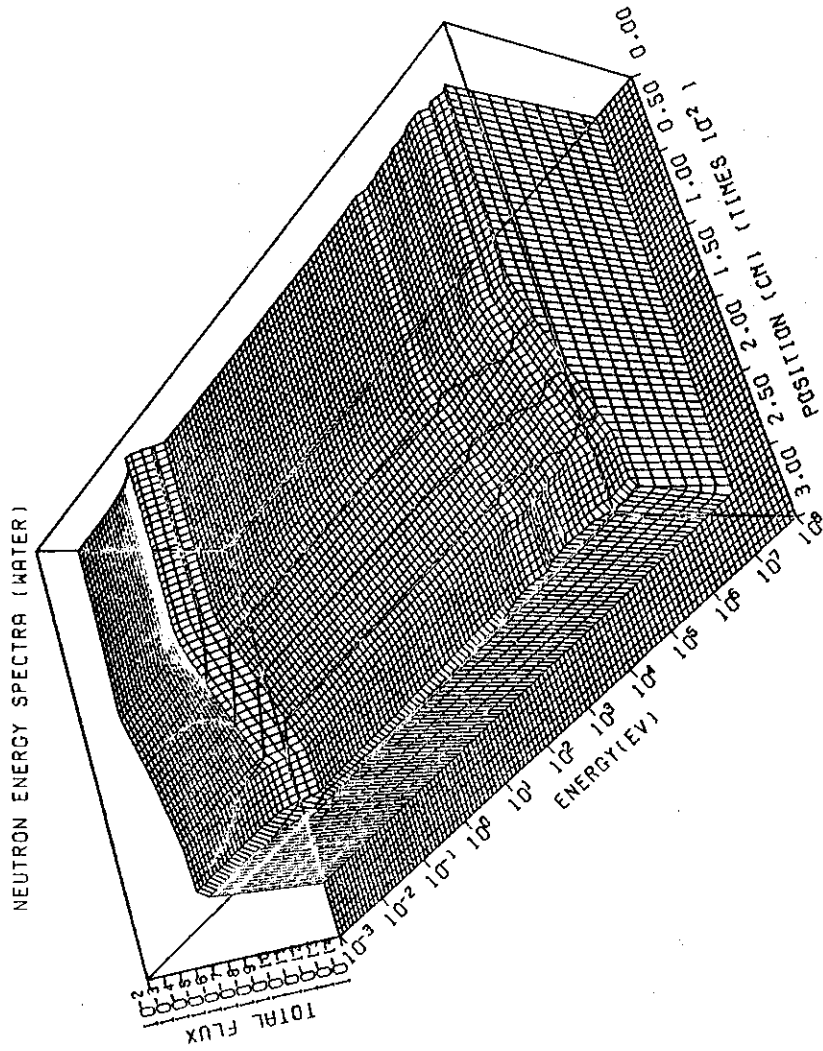


Fig.4.1.9 Overview Plot of Neutron Spectra

```

*** APPLE INPUT DATA CARD IMAGE LIST ***
-----1-----2-----3-----4-----5-----6-----7-----8
1  EPOXY DOSE RATE SAMPLE PROBLEM          <APPLE2>          00000100
2  FLUX 1                                     00000110
3  1 0                                         00000200
4  CROSS 1                                    00000300
5  3 40 25 3                                  00000400
6  10** 3R41 3R42 4R43 2R44 45 5R46 8R47     00000500
7  11** 3 4 11 1 2 4 7 8 9 10 4 11 20 4 11 17 27 43 3 4 10 11 00000600
8  17 25 27 39                                00000700
9  12** 3.65-2 7.3-3 4.745-2 5.118-3 6.385-2 3.448-2 1.255-3 1.575-2 00000800
10 9.848-3 5.909-2 3.35-2 6.7-2 3.296-2 3.391-2 1.331-2 3.031-3 2.394-3 00000900
11 0.4 6.02-6 4.57-2 7.05-4 1.40-2 3.29-3 5.63-4 2.57-3 1.44-2 00001000
12  I                                         00001100
13 RCAL 1                                     00001200
14 1 1 3 1 0.50085                           00001300
15 2** F41                                    00001400
16 22** 3R41                                  00001500
17 23** 1 2 3                                00001600
18  I                                         00001700
19 NEUTRON GAMMA TOTAL                       00001800
20 RPLT 1                                     00001900
21 1                                           00002000
22 15.0 20.0                                 00002100
23 EPOXY DOSE RATE (WATER)                   00002200
24 DISTANCE FROM THE PLASMA AXIS (CM)        00002300
25 DOSE RATE (RAD/YEAR/D-T NEUTRON)         00002400
26 RCAL 2                                     00002500
27 1 1 6 1                                    00002600
28 9** 41 44 41 43                           00002700
29 22** 3R44 3R43                             00002800
30 23** 1 2 3 103                            00002900
31  I                                         00003000
32 NEUTRON GAMMA TOTAL                       00003100
33 RPLT 2                                     00003200
34 1                                           00003300
35 15.0 20.0                                 00003400
36 NUCLEAR HEATING (WATER)                   00003500
37 DISTANCE FROM THE PLASMA AXIS (CM)        00003600
38 HEATING RATE (MEV/D-T NEUTRON)           00003700
39 END 0                                       00003800
-----1-----2-----3-----4-----5-----6-----7-----8

```

Fig.4.2.1 Input Data List for Sample Problem 4.2

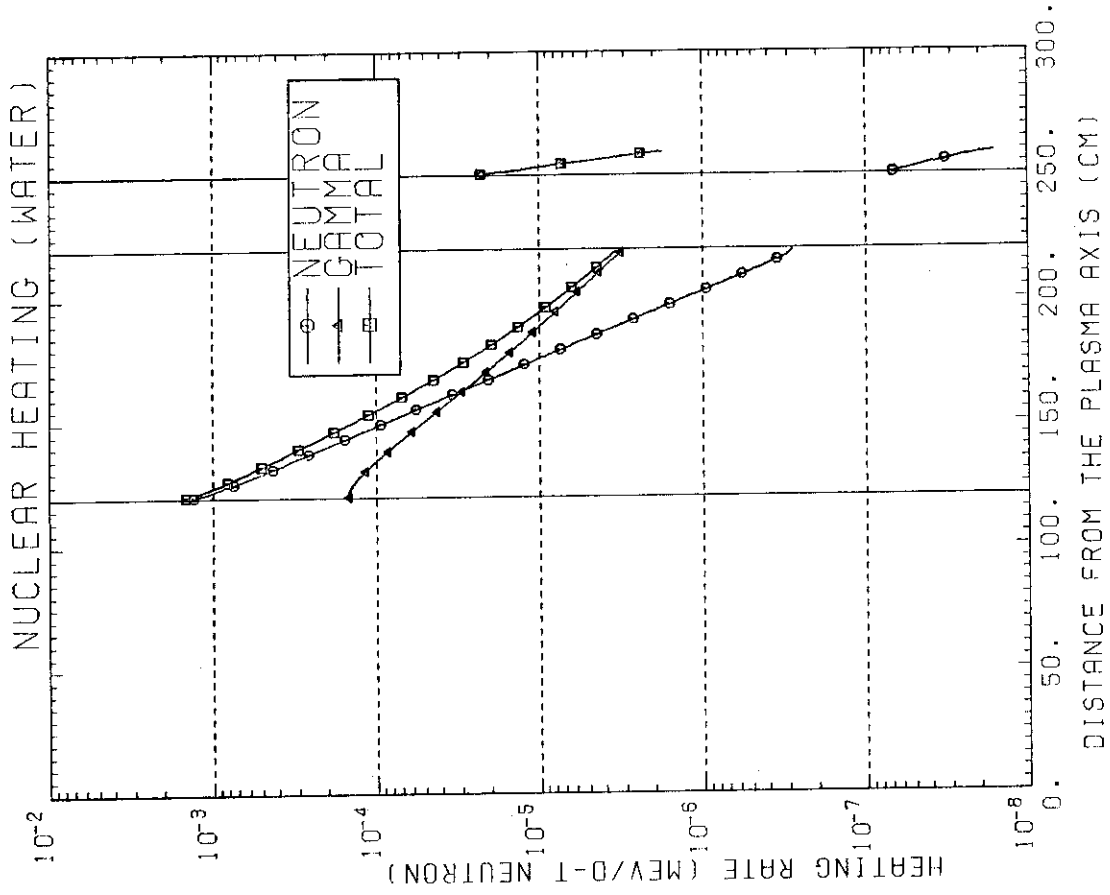


Fig.4.2.3 Plotter Output of Nuclear Heating Rate

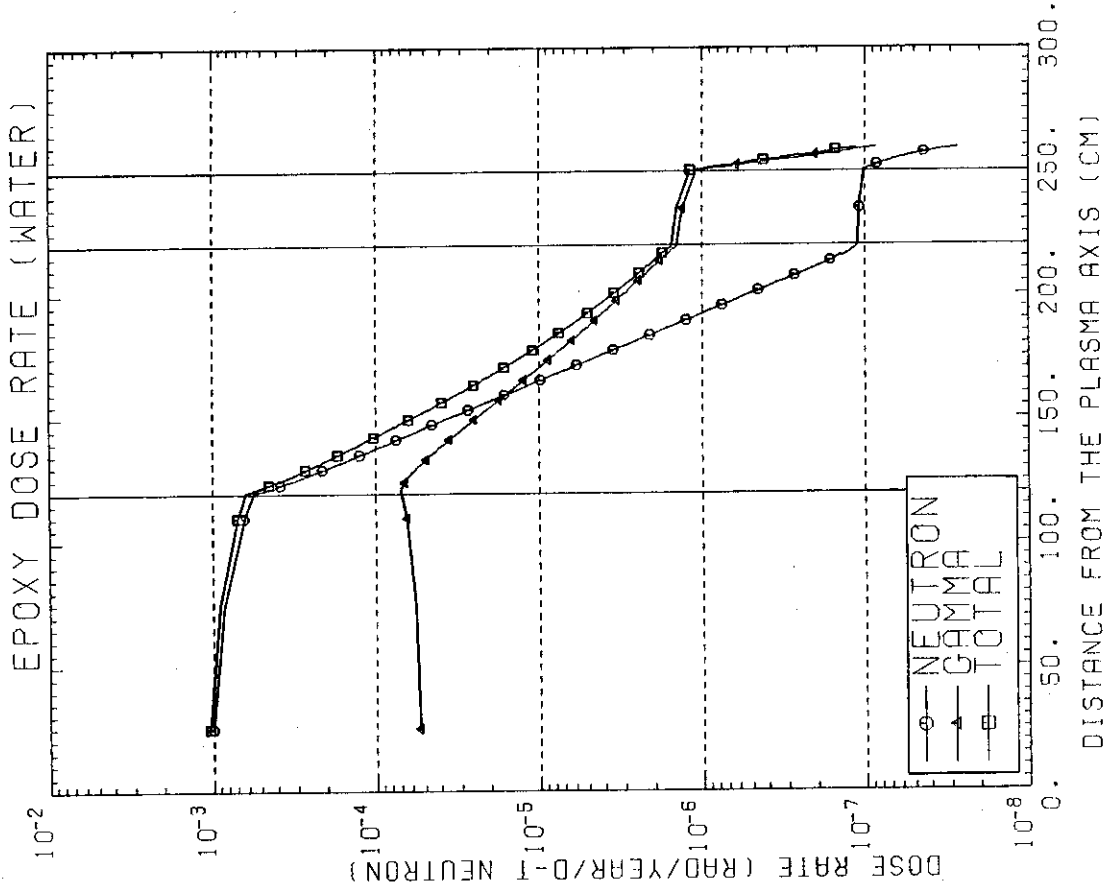


Fig.4.2.2 Plotter Output of Epoxy Dose Rate

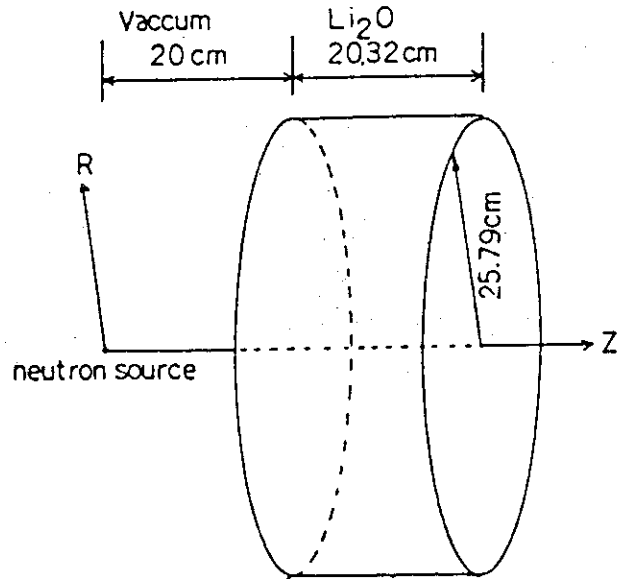


Fig.4.3.1 A Disk Model for Induced Activation Calculation

```

*** APPLE INPUT DATA CARD IMAGE LIST ***
-----1-----2-----3-----4-----5-----6-----7-----8
1  *LIU20 RZ - LI2O20.32CM P5-S16 1ST SRC                <APPLE2>      00000100
2  FLUX 1                                                  00000200
3    2 1 1.0                                              00000300
4    S4 13 12 2 1                                         00000400
5    5** 0.0 0.25 9I20.0 40.0                            00000500
6    4** 12I0.0 25.79                                     00000600
7    8** 39R1 117R2                                       00000700
8    T                                                    00000800
9    CROS 1                                               00000900
10   1 1 1 1                                             00001000
11  10** 1                                               00001100
12  11** 1                                               00001200
13  12** F1 T                                           00001300
14  RCAL 1                                               00001400
15   1 1 1 1 0.0508                                     00001500
16   9** F1                                              00001600
17  22** 1                                               00001700
18  23** F1 T                                           00001800
19  1 DAY                                               00001900
20  RPLT 1                                               00002000
21   2 7RADIAL                                           00002100
22   15.0 20.0                                           00002200
23   SHUTDOWN DOSE RATE (R=13 CM)                       00002300
24   DISTANCE FROM MID PLANE (CM)                       00002400
25   DOSE RATE (MREM/HOUR)                              00002500
26  RPLT 1                                               00002600
27   3 1                                                 00002700
28   -1 1 10 1 1 0 45.0 60.0 10000.0 20.0 25.00002800
29   SHUTDOWN DOSE RATE (MREM/HOUR)                   00002900
30  SPEC 1                                               00003000
31   2 1 1-54 0 2                                       00003100
32   7 2                                                 00003200
33   4 12                                                00003300
34   15.0 20.0                                          00003400
35   GAMMA RAY ENERGY SPECTRA (R=13 CM)             00003500
36   GAMMA ENERGY (EV)                               00003600
37   GAMMA FLUX PER UNIT LETHARGY                    00003700
38   Z = 23CMZ = 39CM                                  00003800
39  END 0                                               00004000
-----1-----2-----3-----4-----5-----6-----7-----8

```

Fig.4.3.2 Input Data List for Sample Problem 4.3

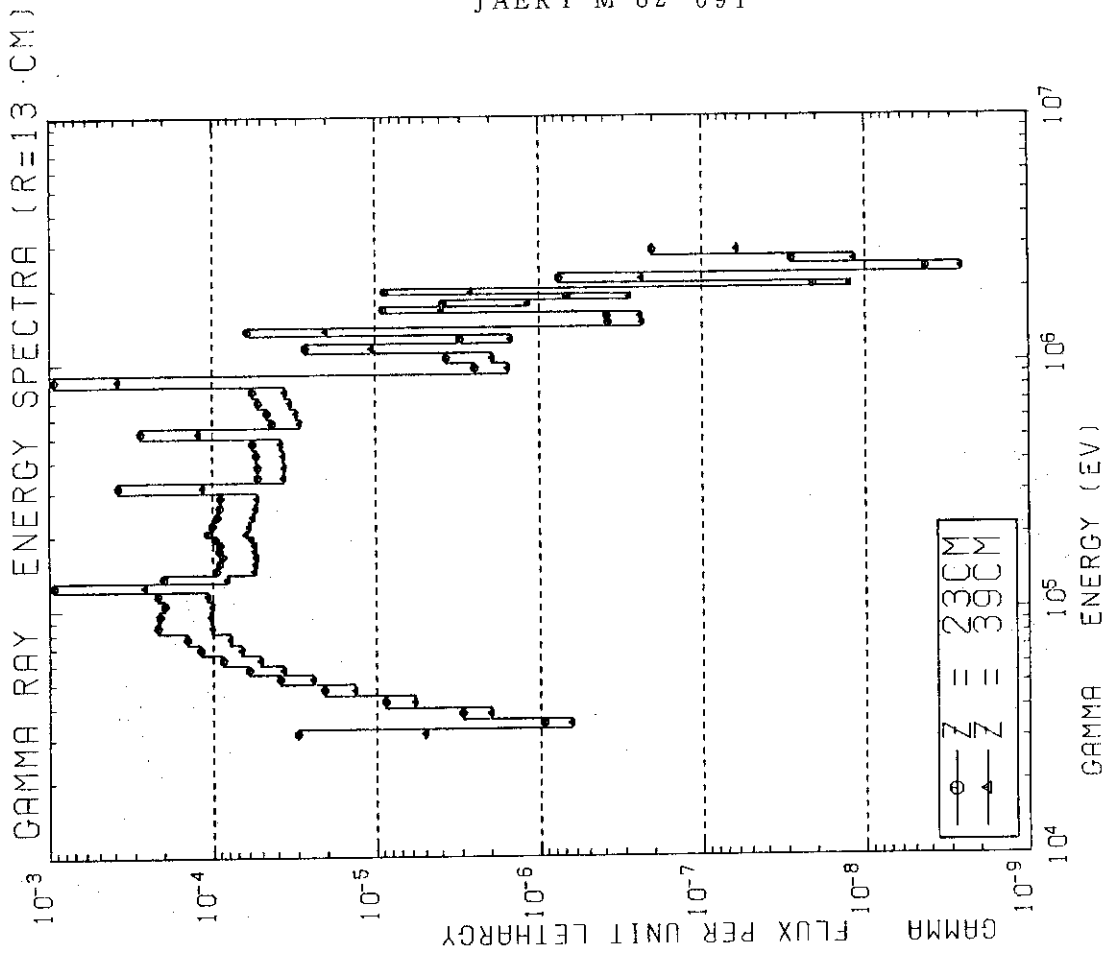


Fig.4.3.5 Plotter Output of Gamma Ray Spectra

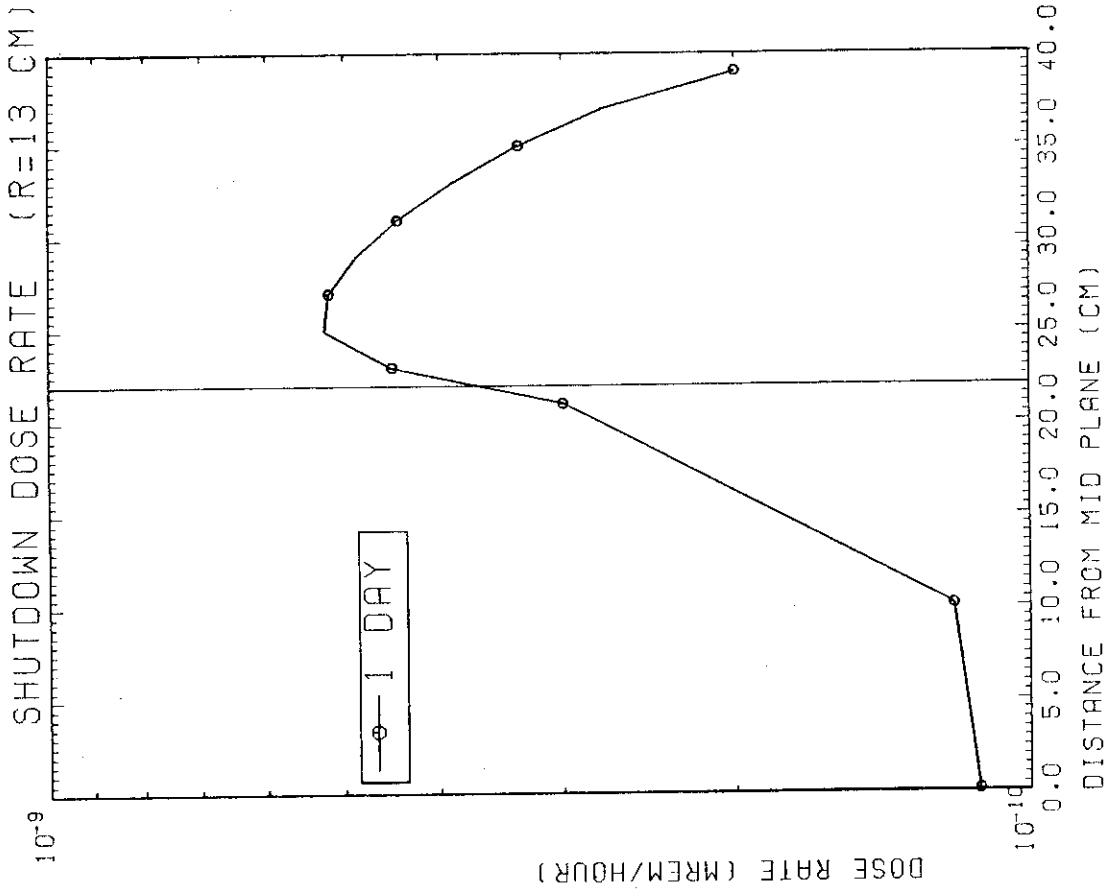


Fig.4.3.3 Plotter Output of the Axial Dose Rate Distribution Along R=13 cm

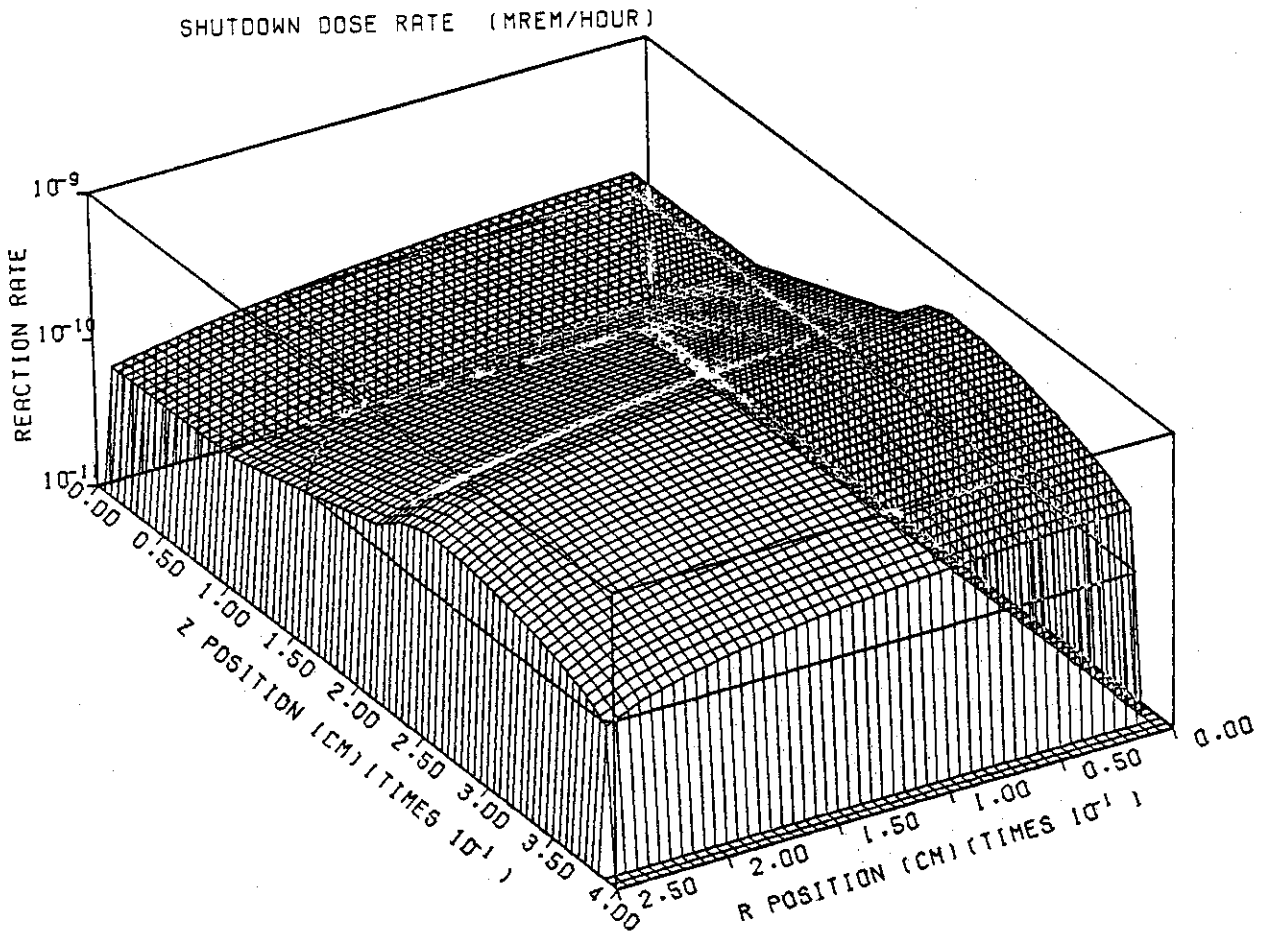


Fig.4.3.4 Overview Plot of Dose Rate Distribution

*LIU20 RZ - LI2020.32CM P5-S16 1ST SRC

<APPLE2>

READ IDENTIFICATION TYPE.FLUX FILE NO. 1

SCALAR FLUX INPUT MODE
 1/ANISN 2/DO3.5 3/MORSE 2
 0/FILE 1/CARD GEOMETRICAL DATA 1
 NORMALIZATION FACTOR 1.0000E+00

SCALAR FLUX INPUT PARAMETER
 READ BY UNIT 10
 NUMBER OF GROUPS 54
 NUMBER OF RADIAL MESH INTERVAL 13
 NUMBER OF AXIAL MESH INTERVAL 12
 NUMBER OF ZONE 2
 NUMBER OF GEOMETRY TYPE 5

5* ARRAY 13 ENTRIES READ

4* ARRAY 14 ENTRIES READ

8* ARRAY 156 ENTRIES READ

OT

RADIAL MESH POINTS (CM)									
0.0	1.984	3.968	5.952	7.935	9.919	11.903	13.887	15.871	17.855
19.838	21.822	23.806	25.790						

AXIAL MESH POINTS (CM)									
0.0	0.250	20.000	22.000	24.000	26.000	28.000	30.000	32.000	34.000
36.000	38.000	40.000							

UNCOLLIDED FLUX ZONE MAP - - -

ZONE NUMBER BY INTERVAL

12... 222222222222
 11... 222222222222
 10... 222222222222
 9... 222222222222
 8... 222222222222
 7... 222222222222
 6... 222222222222
 5... 222222222222
 4... 222222222222
 3... 111111111111
 2... 111111111111
 1... 111111111111

YZT

XPR 1234567890123
 000000001111

SYMBOL = 1 2

NUMBER = 1 2

READ IDENTIFICATION TYPE.CROS FILE NO. 1

10* ARRAY 1 ENTRIES READ

11* ARRAY 1 ENTRIES READ

12* ARRAY 1 ENTRIES READ

OT

REACTION NO. 1 CONVERSION FACTOR FOR DOSE RATE (MREM/HOUR)

14* ARRAY 54 ENTRIES READ

OT

Fig.4.3.6 Output List of Sample Problem 4.3

READ IDENTIFICATION TYPE:RCAL FILE NO. 1

NFX FLUX NO. 1
 NGE GEOMETRY NO. 1
 ID3 TABLE LENGTH 1
 MOPT PLOT OPTION 1
 CF CONVERSION FACTOR 5.08000E-02

9# ARRAY 2 ENTRIES READ
 22# ARRAY 1 ENTRIES READ
 23# ARRAY 1 ENTRIES READ

OT

MATERIAL NAME TABLE
 ACT. 1 1 DAY

TOTAL ACTIVITIES

ACT. 1
 1 2.73943E-06

ACTIVITIES BY ZONE

ZONE ACT. 1
 1 8.32928E-07
 2 1.90742E-06

ACTIVITIES BY INTERVAL

Z-MESH 1 AXIAL 1.25000E-01

R-MESH RADI 1 DAY
 1 9.91921E-01 1.39024E-10
 2 2.97576E+00 1.35824E-10
 3 4.95961E+00 1.32264E-10
 4 6.94345E+00 1.28379E-10
 5 8.92729E+00 1.23815E-10
 6 1.09111E+01 1.18592E-10
 7 1.28950E+01 1.12711E-10
 8 1.48788E+01 1.06248E-10
 9 1.68627E+01 9.92610E-11
 10 1.88465E+01 9.18070E-11
 11 2.08303E+01 8.37607E-11
 12 2.28142E+01 7.37323E-11
 13 2.47980E+01 6.63736E-11

READ IDENTIFICATION TYPE:RPLT FILE NO. 1

REACTION RATE PLOT OPTION PARAMETERS

NWAY = 2
 NTRA = 0
 LOGPO = 2
 LINEIT = 1
 NLABEL = 0
 NSYMB = 2
 ICENT = 1

MAIN TITLE (ARATE) SHUTDOWN DOSE RATE (R=13 CM)
 X TITLE DISTANCE FROM MID PLANE (CM)
 Y TITLE DOSE RATE (MREM/HOUR)

MATERIAL NAME OF PLOT LINE
 1 1 DAY

Zone = 1 1 1 2 2 2 2 2 2 2
 2 2

ID23 = 1

Fig.4.3.6 Output List of Sample Problem 4.3 (continued)

ZONEB= 2.2000E+01
 READ IDENTIFICATION TYPE,RPLT FILE NO. 1
 OVERVIEW PLOTTING OF REACTION RATES OR SCALAR FLUXES
 MAIN TITLE SHUTDOWN DOSE RATE (MREM/HOUR)
 IDE ELIMINATE HIDDEN LINES -1
 CROSS Z-AXIS WILL BE PLACED CROSS-WISE 1
 LGRID GRID PLOT OPTION 10
 NFRAME FRAME 1
 KOLOR CHANGE COLOUR OF THE PEN 1
 KONTR THE RANGE OF PLOTTING (10**N-KONTR) 0
 THETA ANGLE DOWN FROM THE Z-AXIS 0.450E+02
 PSI ANGLE AROUND FROM THE X-AXIS TOWARDS THE Y-AXIS 0.600E+02
 VIEWPT DISTANCE BETWEEN VIEWPOINT AND ORIGIN 0.100E+05
 PWIDTH WIDTH OF THE PLOT 0.200E+02
 PSIZE LENGTH OF THE PLOT 0.250E+02

READ IDENTIFICATION TYPE,SPEC FILE NO. 1

NEUTRON OR GAMMA ENERGY SPECTRA PLOTTING
 SPECTRA OPTION 2-0 OR 3-0 2
 NUMBER OF SCALAR FLUX DATA 1
 NUMBER OF GEOMETRICAL DATA 1
 NEUTRON OR GAMMA GROUPS -54
 ENERGY GROUPS READ OPTION 0
 NUMBER OF 2-0 MESH POINTS 2
 NUMBER OF GROUPS 54
 NUMBER OF RADIAL MESH POINTS 13
 NUMBER OF AXIAL MESH POINTS 12

2-D SPECTRA MESH POINTS
 4 12

PLOT OPTION PARAMETERS

NWAY 4
 NTRA 0
 LOGPO 3
 LINEIT 1
 NLABEL 0
 NSYMB 2
 ISENT 1

MAIN TITLE (ARATE) GAMMA RAY ENERGY SPECTRA (R=13 CM)
 X TITLE GAMMA ENERGY (EV)
 Y TITLE GAMMA FLUX PER UNIT LETHARGY
 MATERIAL NAME OF PLOT LINE
 Z = 23CM
 Z = 39CM

DELTA U -- ALOG(E(I)/E(I+1)) ---

9.531E-02	8.701E-02	1.054E-01	1.178E-01	1.054E-01	9.531E-02	8.701E-02	9.531E-02	1.008E-01
1.054E-01	1.054E-01	9.531E-02	8.701E-02	8.004E-02	7.411E-02	6.899E-02	6.454E-02	6.062E-02
5.407E-02	5.129E-02	4.879E-02	9.097E-02	8.338E-02	7.696E-02	1.054E-01	9.531E-02	8.701E-02
1.178E-01	1.054E-01	9.531E-02	8.701E-02	9.531E-02	1.008E-01	1.040E-01	1.054E-01	1.054E-01
8.701E-02	8.004E-02	7.411E-02	6.899E-02	6.454E-02	6.062E-02	5.716E-02	5.407E-02	5.129E-02
9.097E-02	8.338E-02	7.696E-02	1.054E-01					

SCALING OF X-AXIS

XMIN= 4.000E+00 XMAX= 7.000E+00 DX= 5.080E-01

3.000E+04	3.300E+04	3.600E+04	4.000E+04	4.500E+04	5.000E+04	5.500E+04	6.000E+04	6.600E+04
8.100E+04	9.000E+04	1.000E+05	1.100E+05	1.200E+05	1.300E+05	1.400E+05	1.500E+05	1.600E+05
1.800E+05	1.900E+05	2.000E+05	2.100E+05	2.300E+05	2.500E+05	2.700E+05	3.000E+05	3.300E+05
4.000E+05	4.500E+05	5.000E+05	5.500E+05	6.000E+05	6.600E+05	7.300E+05	8.100E+05	9.000E+05
1.100E+06	1.200E+06	1.300E+06	1.400E+06	1.500E+06	1.600E+06	1.700E+06	1.800E+06	1.900E+06
2.100E+06	2.300E+06	2.500E+06	2.700E+06	3.000E+06				

SCALING OF Y-AXIS

YMIN= -9.000E+00 YMAX= -3.000E+00 DY= 7.620E-01

1	2.997E-05	9.426E-07	2.967E-06	8.755E-06	2.078E-05	3.863E-05	5.987E-05	8.630E-05	1.182E-04
	2.173E-04	2.103E-04	1.948E-04	2.160E-04	9.365E-04	1.985E-04	9.405E-05	9.036E-05	8.642E-05
	8.963E-05	9.554E-05	1.067E-04	9.991E-05	9.304E-05	8.947E-05	8.868E-05	3.733E-04	5.223E-05
	5.352E-05	5.651E-05	2.741E-04	4.280E-05	4.608E-05	5.203E-05	5.628E-05	9.312E-04	2.474E-06
	2.670E-05	3.048E-06	6.056E-05	3.765E-07	3.811E-07	8.964E-06	3.861E-06	6.788E-07	8.725E-06
	7.553E-07	4.288E-09	2.833E-08	2.021E-07					
2	5.009E-06	6.424E-07	2.000E-06	5.803E-06	1.347E-05	2.434E-05	3.682E-05	5.096E-05	6.636E-05
	1.003E-07	1.024E-04	1.002E-04	1.072E-04	2.598E-04	8.086E-05	5.530E-05	5.444E-05	5.347E-05
	5.515E-05	5.743E-05	6.189E-05	5.944E-05	5.648E-05	5.448E-05	5.326E-05	1.144E-04	3.632E-05
	3.662E-05	3.801E-05	1.218E-04	2.895E-05	3.059E-05	3.334E-05	3.589E-05	3.799E-04	1.560E-06
	1.050E-05	1.486E-06	2.013E-05	2.336E-07	2.406E-07	3.929E-06	1.173E-06	2.810E-07	2.602E-06
	2.366E-07	2.611E-09	1.181E-08	6.145E-08					

READ IDENTIFICATION TYPE,END FILE NO. 0

LOCATION REQUESTED ---- 50000
 LOCATION USED ---- 9105
 LOCATION UNUSED ---- 40895

*** PLOT (FPCLS) *** ICHK = 1

Fig.4.3.6 Output List of Sample Problem 4.3 (continued)

```

*** APPLE INPUT DATA CARD IMAGE LIST ***
-----*-----1-----*-----2-----*-----3-----*-----4-----*-----5-----*-----6-----*-----7-----*-----8
1  MORSE ENERGY SPECTRA SAMPLE PROBLEM.                                     <APPLE2>
2  FLUX      1
3  3
4  SPEC      1
5  2  1  1 28  0  4
6  4  5  6  7
7  15.0      20.0
8  NEUTRON ENERGY SPECTRA
9  NEUTRON ENERGY (EV)
10 NEUTRON FLUX PER UNIT LETHARGY
11 D1      D2      D3      D4
12 SPEC    2
13  2  1  1 -7  0  4
14  4  5  6  7
15  15.0      20.0
16  GAMMA ENERGY SPECTRA
17  GAMMA ENERGY (EV)
18  GAMMA FLUX PER UNIT LETHARGY
19 D1      D2      D3      D4
20 END      0
-----*-----1-----*-----2-----*-----3-----*-----4-----*-----5-----*-----6-----*-----7-----*-----8

```

Fig.4.4.1 Input Data List for Sample Problem 4.4

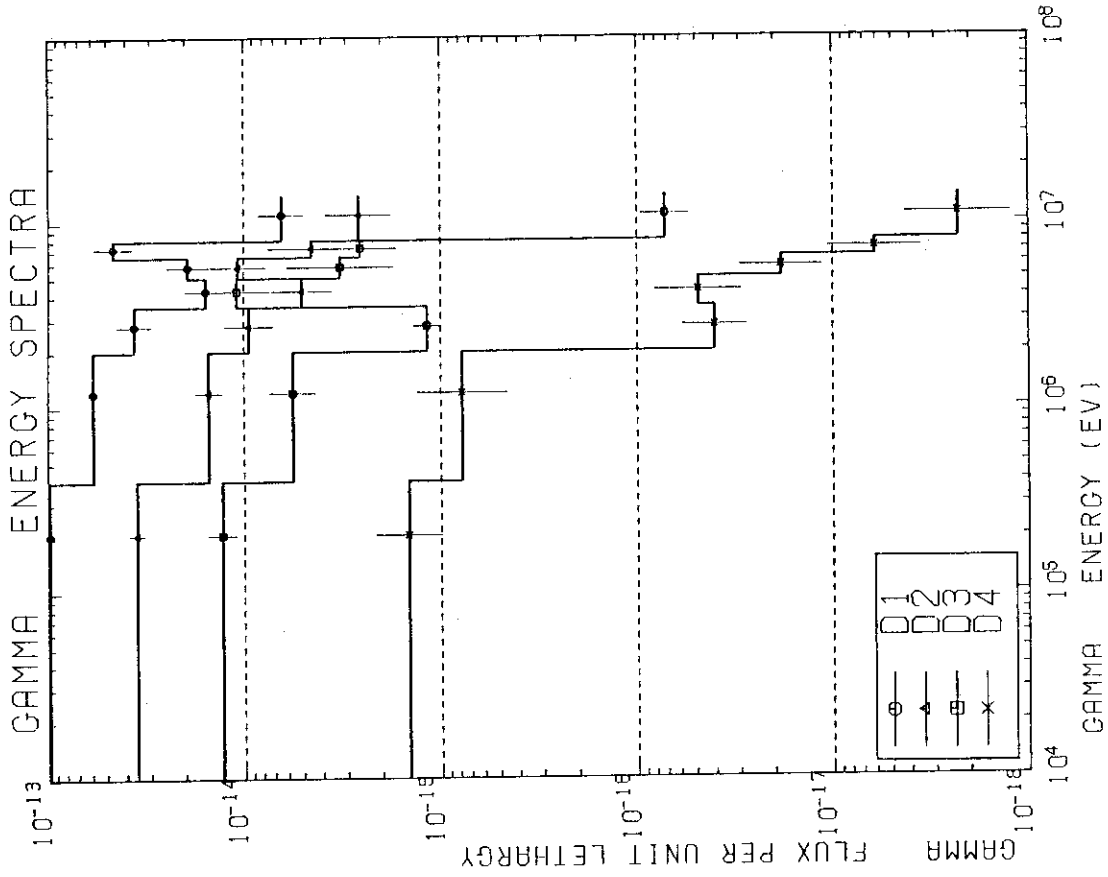


Fig.4.4.3 Plotter Output of Gamma Ray Spectra

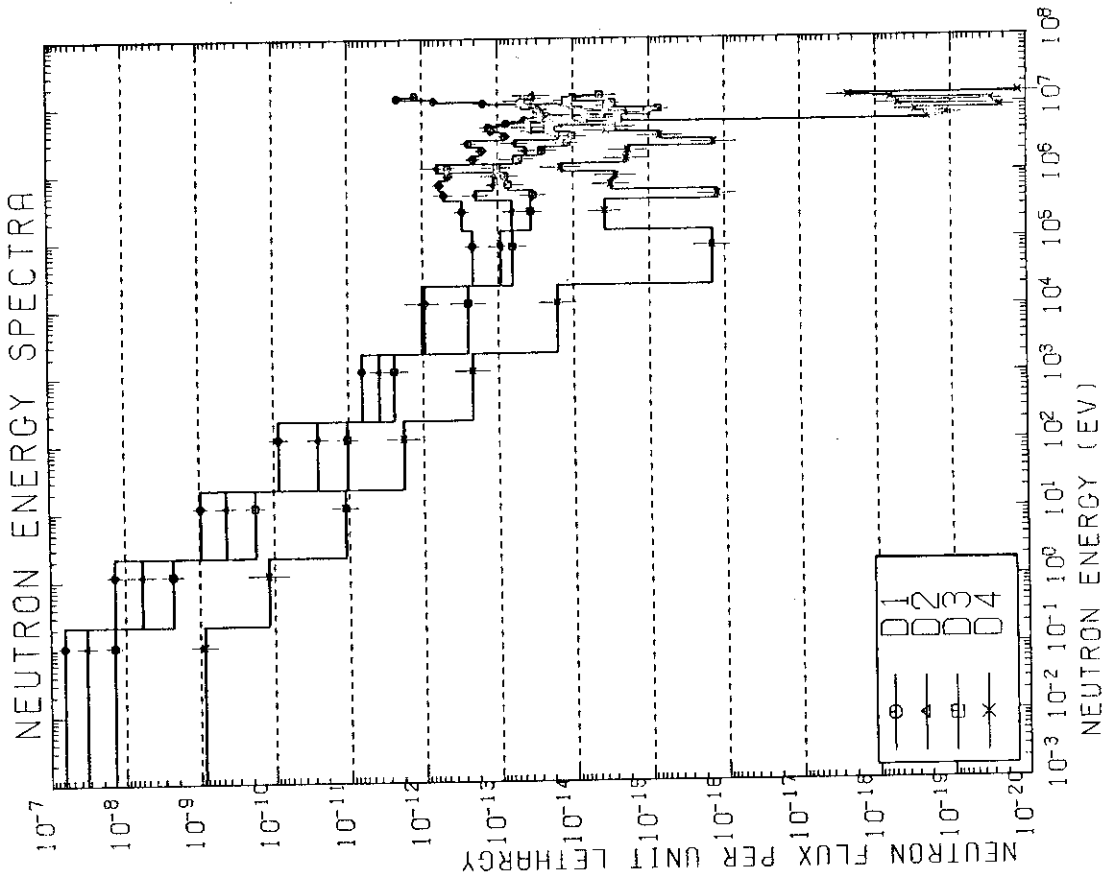


Fig.4.4.2 Plotter Output of Neutron Spectra

5. Concluding Remarks

The main objective for the development of the APPLE-2 code is to simplify the data processing procedure of the fusion reactor neutronics calculations. In order to simplify the input of the code, the output subroutines of radiation transport codes are modified and response libraries compatible with standard cross section sets are provided.

The use of the APPLE-2 code is expected to reduce the manpower required to process the data obtained from ANISN, DOT and MORSE calculations. We hope that such saving in the manpower will off-set the effort required in the development of the APPLE-2 code.

The overview plot routines have been originally obtained from the PERVUE code⁽¹²⁾ made by W.G. Price, Jr.

References

- (1) Yasushi Seki, Hideo Narita and Masahito Igarashi, "Computer Code APPLE for Plotting Spatial Distribution of Neutron Spectra and Reaction-Rates," JAERI-M 6365 (1976) in Japanese.
Also as PSR-111/APPLE in RSIC Computer Code Collection,
Radiation Shielding Information Center, Oak Ridge National
Laboratory (1977)
- (2) W.W. Engle, Jr., "A User's Manual for ANISN, A One Dimensional Discrete Ordinates Transport Code With Anisotropic Scattering," K-1693, Oak Ridge National Laboratory (1967)
- (3) K. Sako et al., "Engineering Aspects of the JAERI Proposal for INTOR(II)," JAERI-M 8518 (1979)
- (4) Y. Seki et al., "Neutronics Design of the Next Tokamak (Swimming Pool Type)," Proc. 3rd Technical Committee Meeting and Workshop on Fusion Reactor Design and Technology, Tokyo, 5-16, October 1981, to be published
- (5) Hiroshi Maekawa, Jyo-ichi Kusano and Yasushi Seki, "Response Distributions of ^6LiF and ^7LiF Thermoluminescence Dosimeters in Lithium Blanket Assemblies," JAERI-M 6811 (1976)
- (6) R-Project Design Team, "Reacting Plasma Experiment Facility, Technical Report[II]," Institute of Plasma Physics Nagoya, November (1981) in Japanese
- (7) W.A. Rhoades and F.R. Mynatt, "The DOT-III Two Dimensional Discrete Ordinates Transport Code," ORNL/TM-4280 (1973)
- (8) E.A. Straker et al., "The MORSE Code — A Multigroup Neutron and Gamma Ray Monte Carlo Transport Code," ORNL-4585 (1970)
- (9) Yasushi Seki and Hiromasa Iida, "Coupled 42-Group Neutron and 21-Group Gamma-Ray Cross Section Sets for Fusion Reactor

- Calculations," JAERI-M 8818 (1980)
- (10) RSIC Data Library Collection, "100-Group Neutron Cross Section Data Based on ENDF/B, DLC-2," Radiation Shielding Information Center, Oak Ridge National Laboratory (1972)
- (11) Hiromasa Iida and Masahito Igarashi, "THIDA-Code System for Calculation of the Exposure Dose Rate Around a Fusion Device," JAERI-M 8019 (1978) in Japanese
- (12) W.G. Price, Jr., "PERVUE: A Program to Plot Perspective Views of Surfaces," PPPL-1304 (1976)

Appendix List of Response Libraries

Complete lists of XS63, GFLXDOSE and XS100 libraries are given as Tables A.1, A.3 and A.4, respectively. Only the initial part of the GICXKRMA library is listed in Table A.2. Energy group structures and nuclides list are also appended.

Appendix A.1 Complete List of XS63 Library

1 63 17										00000100
14**										00000200
REACTION NO. 1	14 MEV NEUTRON FLUX									00000300
1 622										00000400
REACTION NO. 2	NEUTRON FLUX WITH ENERGY GT 0.1 MEV									00000500
24R1 397										00000600
REACTION NO. 3	TOTAL NEUTRON FLUX									00000700
42R1 212										00000800
REACTION NO. 4	TOTAL GAMMA RAY FLUX									00000900
422 21R1										00001000
REACTION NO. 5	LI-6(N,ALPHA)T REACTION RATE									00001100
2.5294-2	2.7750-2	3.0974-2	3.4300-2	3.8447-2						00001200
4.4316-2	5.0658-2	5.8019-2	6.6492-2	7.6484-2	8.7118-2					00001300
9.9839-2	1.2242-1	1.5930-1	2.0238-1	2.3090-1	2.5382-1					00001400
2.6875-1	2.8666-1	3.8706-1	1.059	2.8752	1.2791					00001500
7.2005-1	6.7137-1	8.7341-1	1.2484	1.8176	2.6658					00001600
3.9150	5.7450	8.4442	1.2407+1							00001700
1.8201+1	2.6738+1	3.9271+1								00001800
5.7598+1	8.4605+1	1.2424+2	1.8220+2	2.6760+2	9.4025+2					00001900
21R0.0										00002000
REACTION NO. 6	LI-7(N,N'ALPHA)T REACTION RATE									00002100
3.2338-1	3.5168-1	3.8247-1	4.0062-1	4.1554-1	4.1995-1					00002200
4.2396-1	4.1948-1	3.8405-1	2.9887-1	1.2941-1	4.3060-2					00002300
9.7912-3	1.2312-3	28R0.0								00002400
21R0.0										00002500
REACTION NO. 7	STAINLESS STEEL(SS-316) DISPLACEMENT RATE PER ATOM (DPA)									00002600
2042.5	2848.9	2737.3	2610.0	2465.3	2292.2					00002700
2166.4	2069.3	1963.8	1871.7	1757.7	1642.0					00002800
1412.1	1177.2	863.3	677.6	436.1	351.9					00002900
380.7	362.9	244.4	219.6	241.6	129.5					00003000
110.2	101.1	32.6	26.8	9.9	5.2					00003100
0.14	0.19	0.33	0.36	0.77	0.66					00003200
0.95	1.4	2.0	3.0	4.4	12.3					00003300
21R0.0										00003400
REACTION NO. 8	COPPER DISPLACEMENT RATE PER ATOM (DPA)									00003500
3586.9	3577.5	3636.2	3655.9	3542.5	3253.6					00003600
2897.0	2648.9	2552.0	2367.2	2200.9	1973.3					00003700
1611.5	1236.1	882.0	782.5	697.9	665.6					00003800
584.5	516.1	419.1	349.5	276.5	205.9					00003900
152.0	115.2	65.7	38.9	15.1	9.5					00004000
15.5	1.9	0.25	0.35	0.53	0.78					00004100
0.55	1.7	2.6	3.9	5.7	16.3					00004200
21R0.0										00004300
REACTION NO. 9	TOTAL OF NEUTRON AND GAMMA RAY DOSES (MREM/H)									00004400
17R1.47-1	2R0.115	0.094	2R0.0607	2R0.0354	0.021	0.115				00004500
16R5.42-3	1.19-2	1.03-2	8.79-3	7.86-3	7.49-3	7.12-3				00004600
6.75-3	6.38-3	6.00-3	5.61-3	5.22-3	4.81-3	4.38-3				00004700
3.94-3	3.46-3	2.95-3	2.36-3	1.61-3	7.00-4	2.87-5				00004800
8.49-3										00004900
REACTION NO.10	NEUTRON DOSE (MREM/H)									00005000
17R1.47-1	2R0.115	0.094	2R0.0607	2R0.0354	0.021	0.115				00005100
16R5.42-3	212									00005200
REACTION NO.11	GAMMA RAY DOSE (MREM/H)									00005300
422										00005310
1.19-2	1.03-2	8.79-3	7.86-3	7.49-3	7.12-3	6.75-3				00005400
6.38-3	6.00-3	5.61-3	5.22-3	4.81-3	4.38-3	3.94-3				00005500
3.46-3	2.95-3	2.36-3	1.61-3	7.00-4	2.87-5	8.49-3				00005600
REACTION NO.12	U-235 FISSION RATE									00005601
2.18	2.046	1.797	1.724	1.769	1.799	1.728				00005610
1.517	1.210	1.069	1.103	1.134	1.181	1.250				00005620
1.276	1.258	1.253	1.188	1.140	1.181	1.234				00005630
1.319	1.418	1.535	1.716	2.022	2.428	3.306				00005640
4.865	6.969	10.65	15.24	20.60	29.88	43.21				00005650
59.65	68.99	15.05	21.31	60.97	144.8	233.5				00005660
212										00005670
REACTION NO.13	U-238 FISSION RATE									00005680
1.179	1.083	1.005	.9823	.9777	.9941	.9849				00005780
.9126	.7066	.5693	.5584	.5646	.5553	.5480				00005880
.5416	.3728	.536-2	1.19-2	1.52-3	2.61-4	9.65-5				00005980
5.98-5	5.04-5	4.29-5	4.00-5	6.54-5	8.70-5	1.54-5				00006080
0.000	7.92-5	5.81-4	322							00006180
REACTION NO.14	TH-232 FISSION RATE									00006280
.3715	.3353	.2996	.2831	.2856	.3043	.3318				00006380
.3254	.1728	.1400	.1443	.1440	.1381	.1207				00006480
.1120	8.54-2	9.04-3	462							00006580
REACTION NO.15	NP-237 FISSION RATE									00006680
2.384	2.314	2.304	2.341	2.347	2.309	2.233				00006780
2.091	1.670	1.500	1.515	1.544	1.607	1.683				00006880
1.682	1.623	1.550	1.402	.9902	.4308	.1267				00006980
3.07-2	2.34-2	1.85-2	1.43-2	1.09-2	9.64-3	1.06-2				00007080
8.98-3	7.21-2	3.01-2	4.02-2	1.00-1	4.92-3	1.98-1				00007180
1.67-4	6.98-3	6.45-3	7.02-3	2.91-3	7.04-3	5.61-3				00007280
212										00007380
REACTION NO.16	NI-58(N,P)CO-58 REACTION RATE									00007390
1.82-1	2.34-1	2.82-1	3.14-1	3.31-1	3.35-1	3.31-1				00007391
3.21-1	3.11-1	2.65-1	2.18-1	1.96-1	1.43-1	7.72-2				00007392
3.11-2	9.56-3	2.57-3	2.95-4	3.15-5	1.38-6	4.32-8				00007393
422										00007394
REACTION NO.17	FE-58(N,GAMMA)FE-59 REACTION RATE									00007400
9.13-3	5.14-3	2.89-3	1.63-3	9.49-4	9.11-4	9.38-4				00007401
9.77-4	1.06-3	1.16-3	1.23-3	1.23-3	1.23-3	1.22-3				00007402
1.22-3	1.24-3	1.27-3	1.70-3	2.62-3	2.55-3	2.70-3				00007403
2.87-3	3.26-3	3.95-3	5.30-3	3.72-3	2.32-2	2.82-2				00007404
5.31-4	5.93-4	1.04-3	1.36	7.36-3	1.32-2	2.52-2				00007405
4.28-2	6.75-2	1.03-1	1.53-1	2.27-1	3.34-1	9.58-1				00007406
212										00007410
T										00007480

Table A.1.1 42-Group Neutron Energy Group Structure

Group	Energy Limits	Mid-Point Energy
1	15.000 - 13.720 MeV	14.360 MeV
2	13.720 - 12.549	13.135
3	12.549 - 11.478	12.014
4	11.478 - 10.500	10.989
5	10.500 - 9.314	9.907
6	9.314 - 8.261	8.788
7	8.261 - 7.328	7.795
8	7.328 - 6.500	6.914
9	6.500 - 5.757	6.129
10	5.757 - 5.099	5.428
11	5.099 - 4.516	4.808
12	4.516 - 4.000	4.258
13	4.000 - 3.162	3.581
14	3.162 - 2.500	2.831
15	2.500 - 1.871	2.186
16	1.871 - 1.400	1.636
17	1.400 - 1.058	1.229
18	1.058 - 0.800	0.929
19	0.800 - 0.566	0.683
20	0.566 - 0.400	0.483
21	0.400 - 0.283	0.342
22	0.283 - 0.200	0.242
23	0.200 - 0.141	0.171
24	0.141 - 0.100	0.121
25	100.0 - 46.5 KeV	73.25 KeV
26	46.5 - 21.5	34.0
27	21.5 - 10.0	15.75
28	10.0 - 4.65	7.325
29	4.65 - 2.15	3.40
30	2.15 - 1.00	1.575
31	1.00 - 0.465	0.733
32	0.465 - 0.215	0.340
33	0.215 - 0.100	0.158
34	100.0 - 46.5 eV	73.25 eV
35	46.5 - 21.5	34.0
36	21.5 - 10.0	15.75
37	10.0 - 4.65	7.325
38	4.65 - 2.15	3.40
39	2.15 - 1.00	1.58
40	1.00 - 0.465	0.733
41	0.465 - 0.215	0.340
42	0.215 - 0.001	0.108

Table A.1.2 21-Group Gamma-Ray Energy Group Structure

Group	Energy Limits (MeV)	Mid-Point Energy (MeV)
1	14.0 - 12.0	13.0
2	12.0 - 10.0	11.0
3	10.0 - 8.0	9.0
4	8.0 - 7.5	7.75
5	7.5 - 7.0	7.25
6	7.0 - 6.5	6.75
7	6.5 - 6.0	6.25
8	6.0 - 5.5	5.75
9	5.5 - 5.0	5.25
10	5.0 - 4.5	4.75
11	4.5 - 4.0	4.25
12	4.0 - 3.5	3.75
13	3.5 - 3.0	3.25
14	3.0 - 2.5	2.75
15	2.5 - 2.0	2.25
16	2.0 - 1.5	1.75
17	1.5 - 1.0	1.25
18	1.0 - 0.4	0.7
19	0.4 - 0.2	0.3
20	0.2 - 0.1	0.15
21	0.1 - 0.01	0.055

Appendix A.2 Partial List of GICXKRMA Library

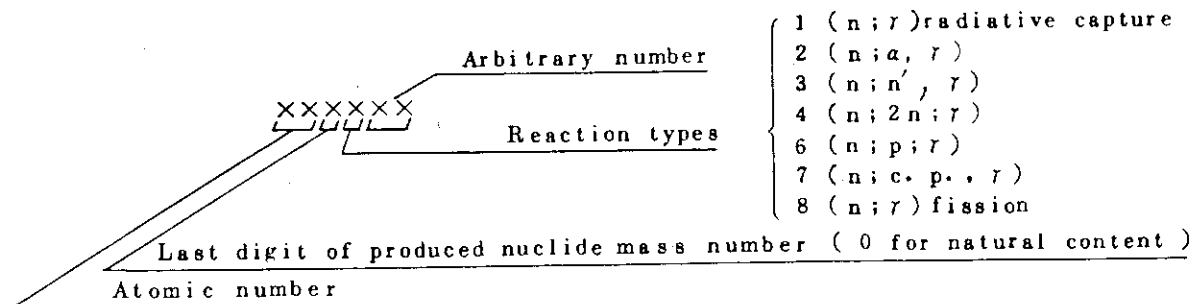
3	63	40					
14*	0.4426E+01	0.0	0.4426E+01	0.4291E+01	0.0	0.4291E+01	
	0.4189E+01	0.0	0.4189E+01	0.4086E+01	0.0	0.4086E+01	
	0.3943E+01	0.0	0.3943E+01	0.3800E+01	0.0	0.3800E+01	
	0.3616E+01	0.0	0.3616E+01	0.3437E+01	0.0	0.3437E+01	
	0.3259E+01	0.0	0.3259E+01	0.3113E+01	0.0	0.3113E+01	
	0.2996E+01	0.0	0.2996E+01	0.2901E+01	0.0	0.2901E+01	
	0.2617E+01	0.0	0.2617E+01	0.2225E+01	0.0	0.2225E+01	
	0.2025E+01	0.0	0.2025E+01	0.1855E+01	0.0	0.1855E+01	
	0.1792E+01	0.0	0.1792E+01	0.1747E+01	0.0	0.1747E+01	
	0.1742E+01	0.0	0.1742E+01	0.2207E+01	0.0	0.2207E+01	
	0.5666E+01	0.0	0.5666E+01	0.1479E+02	0.0	0.1479E+02	
	0.6435E+01	0.0	0.6435E+01	0.3563E+01	0.0	0.3563E+01	
	0.3274E+01	0.0	0.3274E+01	0.4213E+01	0.0	0.4213E+01	
	0.5995E+01	0.0	0.5995E+01	0.8713E+01	0.0	0.8713E+01	
	0.1277E+02	0.0	0.1277E+02	0.1874E+02	0.0	0.1874E+02	
	0.2750E+02	0.0	0.2750E+02	0.4042E+02	0.0	0.4042E+02	
	0.5938E+02	0.0	0.5938E+02	0.8711E+02	0.0	0.8711E+02	
	0.1280E+03	0.0	0.1280E+03	0.1879E+03	0.0	0.1879E+03	
	0.2757E+03	0.0	0.2757E+03	0.4049E+03	0.0	0.4049E+03	
	0.5946E+03	0.0	0.5946E+03	0.8720E+03	0.0	0.8720E+03	
	0.1281E+04	0.0	0.1281E+04	0.2799E+04	0.0	0.2799E+04	
	0.0	0.1459E+01	0.1459E+01	0.0	0.1313E+01	0.1313E+01	
	0.0	0.1167E+01	0.1167E+01	0.0	0.1072E+01	0.1072E+01	
	0.0	0.1033E+01	0.1033E+01	0.0	0.9931E+00	0.9931E+00	
	0.0	0.9521E+00	0.9521E+00	0.0	0.9096E+00	0.9096E+00	
	0.0	0.8652E+00	0.8652E+00	0.0	0.8188E+00	0.8188E+00	
	0.0	0.7702E+00	0.7702E+00	0.0	0.7175E+00	0.7175E+00	
	0.0	0.6614E+00	0.6614E+00	0.0	0.6000E+00	0.6000E+00	
	0.0	0.5319E+00	0.5319E+00	0.0	0.4550E+00	0.4550E+00	
	0.0	0.3665E+00	0.3665E+00	0.0	0.2490E+00	0.2490E+00	
	0.0	0.1080E+00	0.1080E+00	0.0	0.4322E-01	0.4322E-01	
	0.0	0.1153E-01	0.1153E-01	0.3359E+01	0.0	0.3359E+01	
	0.3158E+01	0.0	0.3158E+01	0.3007E+01	0.0	0.3007E+01	
	0.2856E+01	0.0	0.2856E+01	0.2653E+01	0.0	0.2653E+01	
	0.2404E+01	0.0	0.2404E+01	0.2209E+01	0.0	0.2209E+01	
	0.2145E+01	0.0	0.2145E+01	0.2179E+01	0.0	0.2179E+01	
	0.2133E+01	0.0	0.2133E+01	0.1962E+01	0.0	0.1962E+01	
	0.1805E+01	0.0	0.1805E+01	0.1418E+01	0.0	0.1418E+01	
	0.1042E+01	0.0	0.1042E+01	0.7809E+00	0.0	0.7809E+00	
	0.5738E+00	0.0	0.5738E+00	0.4359E+00	0.0	0.4359E+00	
	0.3170E+00	0.0	0.3170E+00	0.2049E+00	0.0	0.2049E+00	
	0.1333E+00	0.0	0.1333E+00	0.1553E+00	0.0	0.1553E+00	
	0.2640E+00	0.0	0.2640E+00	0.3327E-01	0.0	0.3327E-01	
	0.2034E-01	0.0	0.2034E-01	0.1316E-01	0.0	0.1316E-01	
	0.7145E-02	0.0	0.7145E-02	0.4076E-02	0.0	0.4076E-02	
	0.2660E-02	0.0	0.2660E-02	0.2068E-02	0.0	0.2068E-02	
	0.2010E-02	0.0	0.2010E-02	0.2409E-02	0.0	0.2409E-02	
	0.3318E-02	0.0	0.3318E-02	0.4714E-02	0.0	0.4714E-02	
	0.6759E-02	0.0	0.6759E-02	0.9738E-02	0.0	0.9738E-02	
	0.1405E-01	0.0	0.1405E-01	0.2049E-01	0.0	0.2049E-01	
	0.3028E-01	0.0	0.3028E-01	0.4473E-01	0.0	0.4473E-01	
	0.6570E-01	0.0	0.6570E-01	0.9625E-01	0.0	0.9625E-01	
	0.2086E+00	0.0	0.2086E+00	0.0	0.1459E+01	0.1459E+01	
	0.0	0.1313E+01	0.1313E+01	0.0	0.1167E+01	0.1167E+01	
	0.0	0.1072E+01	0.1072E+01	0.0	0.1033E+01	0.1033E+01	
	0.0	0.9931E+00	0.9931E+00	0.0	0.9521E+00	0.9521E+00	
	0.0	0.9096E+00	0.9096E+00	0.0	0.8652E+00	0.8652E+00	
	0.0	0.8188E+00	0.8188E+00	0.0	0.7702E+00	0.7702E+00	
	0.0	0.7175E+00	0.7175E+00	0.0	0.6614E+00	0.6614E+00	
	0.0	0.6000E+00	0.6000E+00	0.0	0.5319E+00	0.5319E+00	
	0.0	0.4550E+00	0.4550E+00	0.0	0.3665E+00	0.3665E+00	
	0.0	0.2490E+00	0.2490E+00	0.0	0.1080E+00	0.1080E+00	
	0.0	0.4322E-01	0.4322E-01	0.0	0.1153E-01	0.1153E-01	
	0.3389E+01	0.0	0.3389E+01	0.2940E+01	0.0	0.2940E+01	
	0.2518E+01	0.0	0.2518E+01	0.2208E+01	0.0	0.2208E+01	
	0.1389E+01	0.0	0.1389E+01	0.1062E+01	0.0	0.1062E+01	
	0.1414E+01	0.0	0.1414E+01	0.6425E+00	0.0	0.6425E+00	
	0.8961E+00	0.0	0.8961E+00	0.7202E+00	0.0	0.7202E+00	
	0.7722E+00	0.0	0.7722E+00	0.8688E+00	0.0	0.8688E+00	
	0.1210E+01	0.0	0.1210E+01	0.7264E+00	0.0	0.7264E+00	
	0.5159E+00	0.0	0.5159E+00	0.4217E+00	0.0	0.4217E+00	
	0.3714E+00	0.0	0.3714E+00	0.3262E+00	0.0	0.3262E+00	
	0.2757E+00	0.0	0.2757E+00	0.2217E+00	0.0	0.2217E+00	
	0.1733E+00	0.0	0.1733E+00	0.1322E+00	0.0	0.1322E+00	
	0.9877E-01	0.0	0.9877E-01	0.7275E-01	0.0	0.7275E-01	
	0.4435E-01	0.0	0.4435E-01	0.2128E-01	0.0	0.2128E-01	
	0.1002E-01	0.0	0.1002E-01	0.4696E-02	0.0	0.4696E-02	
	0.2185E-02	0.0	0.2185E-02	0.1015E-02	0.0	0.1015E-02	
	0.4723E-03	0.0	0.4723E-03	0.2192E-03	0.0	0.2192E-03	
	0.1017E-03	0.0	0.1017E-03	0.4733E-04	0.0	0.4733E-04	
	0.2202E-04	0.0	0.2202E-04	0.1031E-04	0.0	0.1031E-04	
	0.4942E-05	0.0	0.4942E-05	0.2509E-05	0.0	0.2509E-05	
	0.1479E-05	0.0	0.1479E-05	0.1148E-05	0.0	0.1148E-05	
	0.1208E-05	0.0	0.1208E-05	0.2185E-05	0.0	0.2185E-05	
	0.0	0.3456E+01	0.3456E+01	0.0	0.3023E+01	0.3023E+01	
	0.0	0.2608E+01	0.2608E+01	0.0	0.2349E+01	0.2349E+01	
	0.0	0.2245E+01	0.2245E+01	0.0	0.2141E+01	0.2141E+01	

Table A.2.1 List of 40 Nuclides Stored in the GICX40 Set

№	Nuclide	MATNO in ENDF/B-3(4*)	POPOP4 ID Number**for Gamma-ray Producing reactions			MT NO for ANISN input P0~P5
			(n, r)	(n,n'r)	others	
1	⁶ Li	1115	30101	40301	80201,860601	1 ~ 6
2	⁷ Li	1116	30101	40301		7 ~ 12
3	¹² C	1165	60101	60301		13 ~ 18
4	¹⁶ O	1134	70301	86301		19 ~ 24
5	⁴ He	1088	30301	40301		25 ~ 30
6	Nb	1164	404101	400301		31 ~ 36
7	Mo	1111	420101	400301		37 ~ 42
8	Cr	1121	240101	240301		43 ~ 48
9	Ni	1123	280101	280301		49 ~ 54
10	Fe	1180	260101	260301		55 ~ 60
11	¹ H	1148	10101	40301	50204 74401	61 ~ 66
12	² H	1120	13001	40301		67 ~ 72
13	³ He	1146	30101	40301		73 ~ 78
14	⁹ Be	1154	40102	40301		79 ~ 84
15	¹⁰ B	1155	40102	40301		85 ~ 90
16	¹⁴ N	1133	70102	70301		91 ~ 96
17	²⁷ Al	1135	130103	180301		97 ~ 102
18	V	1017	240101	240301		103 ~ 106
19	Cu	1087	290104	280301		109 ~ 114
20	Pb	1136	820102	820301		115 ~ 120
21	²³² Th	1117	928109	928301	925801	121 ~ 126
22	²³⁵ U	1157	925101	925301	925801	127 ~ 132
23	²³⁹ Pu	1159	928109	928301	925801	133 ~ 138
24	²³⁷ Np	1263 *	937101	928301	925801	139 ~ 144
25	Mg	1014	925101	925301		145 ~ 150
26	K	1150	190101	190301	190701	151 ~ 156
27	Ca	1152	200101	200301	200701	157 ~ 162
28	¹¹ B	1160 *	60101	60301		163 ~ 168
29	Cl	1149 *	170101	170301		169 ~ 174
30	Na	1156 *	110101	113301		175 ~ 180
31	Cd	1281 *	480101	-		181 ~ 186
32	Ta	1285 *	730101	740301		187 ~ 192
33	¹⁸² W	1128 *	730103	740301		193 ~ 198
34	¹⁸³ W	1129 *	730103	740301		199 ~ 204
35	¹⁸⁴ W	1130 *	730103	740301		205 ~ 210
36	¹⁸⁶ W	1131 *	740103	740301		211 ~ 216
37	F	1277 *	90102	86302		217 ~ 222
38	²³⁸ U	1262 *	928109	928301	925801	223 ~ 228
39	Si	1194 *	140105	140301		229 ~ 234
40	Ti	1286 *	220102	220302		235 ~ 240

* The data in ENDF/B-4 are used.

** ID number used in POPOP4 library has five or six digits. They indicate the following meaning



Appendix A.3 Complete List of GFLXDOSE Library

```

1 54 1
14**
REACTION NO. 1 CONVERSION FACTOR FOR DOSE RATE (MREM/HOUR)
0.13266E-03 0.13612E-03 0.12570E-03 0.11531E-03 0.10746E-03 0.10232E-03 00007000
0.97182E-04 0.91994E-04 0.86807E-04 0.81605E-04 0.76397E-04 0.71168E-04 00007010
0.65913E-04 0.60626E-04 0.55299E-04 0.49927E-04 0.44770E-04 0.40115E-04 00007020
0.35973E-04 0.32356E-04 0.29278E-04 0.26468E-04 0.23648E-04 0.20820E-04 000007100
0.18269E-04 0.16288E-04 0.14595E-04 0.12909E-04 0.11513E-04 0.10405E-04 000007200
0.93080E-05 0.84939E-05 0.79561E-05 0.74239E-05 0.68973E-05 0.63776E-05 000007300
0.58663E-05 0.53647E-05 0.48750E-05 0.43997E-05 0.39426E-05 0.35085E-05 000007400
0.31047E-05 0.27578E-05 0.24894E-05 0.22983E-05 0.21809E-05 0.21296E-05 000007500
0.21408E-05 0.22251E-05 0.24143E-05 0.26973E-05 0.30287E-05 0.34423E-05 000007600
000007700
000007800
000007900
00008000
    
```

Table A.3.1 54-Group Gamma Ray Energy Group Structure

	E(MeV)		E(MeV)
1	3.0 ~ 2.7	28	0.3 ~ 0.27
2	2.7 ~ 2.5	29	0.27 ~ 0.25
3	2.5 ~ 2.3	30	0.25 ~ 0.23
4	2.3 ~ 2.1	31	0.23 ~ 0.21
5	2.1 ~ 2.0	32	0.21 ~ 0.20
6	2.0 ~ 1.9	33	0.20 ~ 0.19
7	1.9 ~ 1.8	34	0.19 ~ 0.18
8	1.8 ~ 1.7	35	0.18 ~ 0.17
9	1.7 ~ 1.6	36	0.17 ~ 0.16
10	1.6 ~ 1.5	37	0.16 ~ 0.15
11	1.5 ~ 1.4	38	0.15 ~ 0.14
12	1.4 ~ 1.3	39	0.14 ~ 0.13
13	1.3 ~ 1.2	40	0.13 ~ 0.12
14	1.2 ~ 1.1	41	0.12 ~ 0.11
15	1.1 ~ 1.0	42	0.11 ~ 0.10
16	1.0 ~ 0.9	43	0.10 ~ 0.09
17	0.9 ~ 0.81	44	0.09 ~ 0.081
18	0.81 ~ 0.73	45	0.081 ~ 0.073
19	0.73 ~ 0.66	46	0.073 ~ 0.066
20	0.66 ~ 0.6	47	0.066 ~ 0.06
21	0.6 ~ 0.55	48	0.06 ~ 0.055
22	0.55 ~ 0.5	49	0.055 ~ 0.05
23	0.5 ~ 0.45	50	0.05 ~ 0.045
24	0.45 ~ 0.4	51	0.045 ~ 0.04
25	0.4 ~ 0.36	52	0.04 ~ 0.036
26	0.36 ~ 0.33	53	0.036 ~ 0.033
27	0.33 ~ 0.3	54	0.033 ~ 0.03

Table A.4.1 100-Group Neutron Energy Group Structure

Group	Group Limits			E(Mid Point)		
	E(Top)		E(Low)			
1	1.4918	(+7)*	1.3499	(+7)	1.4208	(+7)
2	1.3499	(+7)	1.2214	(+7)	1.2856	(+7)
3	1.2214	(+7)	1.1052	(+7)	1.1633	(+7)
4	1.1052	(+7)	1.0000	(+7)	1.0526	(+7)
5	1.0000	(+7)	9.0484	(+6)	9.5242	(+6)
6	9.0484	(+6)	8.1873	(+6)	8.6178	(+6)
7	8.1873	(+6)	7.4082	(+6)	7.7977	(+6)
8	7.4082	(+6)	6.7032	(+6)	7.0557	(+6)
9	6.7032	(+6)	6.0653	(+6)	6.3843	(+6)
10	6.0653	(+6)	5.4881	(+6)	5.7767	(+6)
11	5.4881	(+6)	4.9659	(+6)	5.2270	(+6)
12	4.9659	(+6)	4.4933	(+6)	4.7296	(+6)
13	4.4933	(+6)	4.0657	(+6)	4.2795	(+6)
14	4.0657	(+6)	3.6788	(+6)	3.8722	(+6)
15	3.6788	(+6)	3.3287	(+6)	3.5038	(+6)
16	3.3287	(+6)	3.0119	(+6)	3.1703	(+6)
17	3.0119	(+6)	2.7253	(+6)	2.8686	(+6)
18	2.7253	(+6)	2.4660	(+6)	2.5956	(+6)
19	2.4660	(+6)	2.2313	(+6)	2.3486	(+6)
20	2.2313	(+6)	2.0910	(+6)	2.1251	(+6)
21	2.0910	(+6)	1.8268	(+6)	1.9229	(+6)
22	1.8268	(+6)	1.6350	(+6)	1.7399	(+6)
23	1.6350	(+6)	1.4957	(+6)	1.5743	(+6)
24	1.4957	(+6)	1.3534	(+6)	1.4245	(+6)
25	1.3534	(+6)	1.2246	(+6)	1.2890	(+6)
26	1.2246	(+6)	1.1080	(+6)	1.1663	(+6)
27	1.1080	(+6)	1.0026	(+6)	1.0553	(+6)
28	1.0026	(+6)	9.0718	(+5)	9.5488	(+5)
29	9.0718	(+5)	8.2085	(+5)	8.6401	(+5)
30	8.2085	(+5)	7.4274	(+5)	7.8179	(+5)
31	7.4274	(+5)	6.7206	(+5)	7.0740	(+5)
32	6.7206	(+5)	6.0810	(+5)	6.4008	(+5)
33	6.0810	(+5)	5.5023	(+5)	5.7917	(+5)
34	5.5023	(+5)	4.9787	(+5)	5.2405	(+5)
35	4.9787	(+5)	4.5049	(+5)	4.7418	(+5)
36	4.5049	(+5)	4.0762	(+5)	4.2906	(+5)
37	4.0762	(+5)	3.6883	(+5)	3.8827	(+5)
38	3.6883	(+5)	3.3373	(+5)	3.5128	(+5)
39	3.3373	(+5)	3.0197	(+5)	3.1785	(+5)
40	3.0197	(+5)	2.7324	(+5)	2.8761	(+5)
41	2.7324	(+5)	2.4724	(+5)	2.6024	(+5)
42	2.4724	(+5)	2.2371	(+5)	2.3547	(+5)
43	2.2371	(+5)	2.0242	(+5)	2.1306	(+5)
44	2.0242	(+5)	1.8316	(+5)	1.9279	(+5)
45	1.8316	(+5)	1.6573	(+5)	1.7444	(+5)
46	1.6573	(+5)	1.4996	(+5)	1.5784	(+5)
47	1.4996	(+5)	1.3569	(+5)	1.4282	(+5)
48	1.3569	(+5)	1.2277	(+5)	1.2923	(+5)
49	1.2277	(+5)	1.1109	(+5)	1.1693	(+5)
50	1.1109	(+5)	8.6517	(+4)	9.8803	(+4)

Table A.4.1 continued

Group	Group Limits				E(Mid Point)	
	E(Top)		E(Low)			
51	8.6517	(+4)	6.7379	(+4)	7.6948	(+4)
52	6.7379	(+4)	5.2475	(+4)	5.9927	(+4)
53	5.2475	(+4)	4.0868	(+4)	4.6671	(+4)
54	4.0868	(+4)	3.1828	(+4)	3.6348	(+4)
55	3.1828	(+4)	2.4788	(+4)	2.8308	(+4)
56	2.4788	(+4)	1.9305	(+4)	2.2046	(+4)
57	1.9305	(+4)	1.5034	(+4)	1.7169	(+4)
58	1.5034	(+4)	1.1709	(+4)	1.3372	(+4)
59	1.1709	(+4)	9.1188	(+3)	1.0414	(+4)
60	9.1188	(+3)	7.1017	(+3)	8.1103	(+3)
61	7.1017	(+3)	5.5308	(+3)	6.3163	(+3)
62	5.5308	(+3)	4.3074	(+3)	4.9191	(+3)
63	4.3074	(+3)	3.3546	(+3)	3.8310	(+3)
64	3.3546	(+3)	2.6126	(+3)	2.9836	(+3)
65	2.6126	(+3)	2.0347	(+3)	2.3236	(+3)
66	2.0347	(+3)	1.5846	(+3)	1.8096	(+3)
67	1.5846	(+3)	1.2341	(+3)	1.4094	(+3)
68	1.2341	(+3)	9.6112	(+2)	1.0976	(+3)
69	9.6112	(+2)	7.4852	(+2)	8.5482	(+2)
70	7.4852	(+2)	5.8295	(+2)	6.6573	(+2)
71	5.8295	(+2)	4.5733	(+2)	5.1847	(+2)
72	4.5733	(+2)	3.5358	(+2)	4.0379	(+2)
73	3.5358	(+2)	2.7536	(+2)	3.1447	(+2)
74	2.7536	(+2)	2.1445	(+2)	2.4491	(+2)
75	2.1445	(+2)	1.6702	(+2)	1.9074	(+2)
76	1.6702	(+2)	1.3007	(+2)	1.4855	(+2)
77	1.3007	(+2)	1.0130	(+2)	1.1569	(+2)
78	1.0130	(+2)	7.8893	(+1)	9.0097	(+1)
79	7.8893	(+1)	6.1442	(+1)	7.0168	(+1)
80	6.1442	(+1)	4.7851	(+1)	5.4647	(+1)
81	4.7851	(+1)	3.7267	(+1)	4.2559	(+1)
82	3.7267	(+1)	2.9023	(+1)	3.3145	(+1)
83	2.9023	(+1)	2.2603	(+1)	2.5813	(+1)
84	2.2603	(+1)	1.7603	(+1)	2.0103	(+1)
85	1.7603	(+1)	1.3710	(+1)	1.5657	(+1)
86	1.3710	(+1)	1.0677	(+1)	1.2193	(+1)
87	1.0667	(+1)	8.3153	(+0)	9.4962	(+0)
88	8.3153	(+0)	6.4760	(+0)	7.3956	(+0)
89	6.4760	(+0)	5.0435	(+0)	5.7597	(+0)
90	5.0435	(+0)	3.9279	(+0)	4.4857	(+0)
91	3.9279	(+0)	3.0590	(+0)	3.4934	(+0)
92	3.0590	(+0)	2.3824	(+0)	2.7207	(+0)
93	2.3824	(+0)	1.8554	(+0)	2.1189	(+0)
94	1.8554	(+0)	1.4450	(+0)	1.6502	(+0)
95	1.4450	(+0)	1.1254	(+0)	1.2852	(+0)
96	1.1254	(+0)	8.7643	(-1)	1.0009	(+0)
97	8.7643	(-1)	6.8256	(-1)	7.7949	(-1)
98	6.8256	(-1)	5.3158	(-1)	6.0707	(-1)
99	5.3158	(-1)	4.1399	(-1)	4.7279	(-1)
100	4.1399	(-1)	2.5000	(-2)	2.1950	(-1)

*($\pm n$) represents ($10^{\pm n}$)