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THEORETICAL CALCULATION OF DECAY DATA OF
SHORT-LIVED NUCLIDES FOR JNDC FP DECAY DATA FILE

August 1983

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© Japan Atomic Energy Research Institute, 1983 編集兼発行 日本原子力研究所 印 刷 いばらき印刷㈱ Theoretical Calculation of Decay Data of Short-Lived Nuclides for JNDC FP Decay Data ${\it File}^{1)}$

T. Yoshida*

Japanese Nuclear Data Committee, Tokai Research Establishment, JAERI (Received July 15, 1983)

It is one of unique features of the JNDC FP Decay Data File that theoretical values of \overline{E}_β and \overline{E}_γ , average beta- and gamma-ray energies, are fully adopted for short-lived nuclides. Here, details of the theoretical estimation method of \overline{E}_β and \overline{E}_γ based on 'gross theory' of beta-decay are described and the numerical tables of the estimated decay data for short-lived nuclides are presented. Further, discussion is made for justification of adoption of the theoretical values instead of values derived from decay schemes from the viewpoint of the energy profile of the beta-strength function.

Keywords : Fission Product, Beta Decay, Beta Ray, Gamma Ray, Short-Lived, Gross Theory, Decay Scheme, Strength Function

¹⁾ The work was performed in the evaluation work of the Working Group of Decay Heat, Japanese Nuclear Data Committee.

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JNDC FP 崩壊データファイルのための短寿命核崩壊データの理論計算[†]

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(1983年7月15日受理)

Q値の大きな短寿命核種に対して、放出ベータ線・ガンマ線の平均エネルギー \overline{E}_{β} , \overline{E}_{r} の理論計算値を全面的に採用したことは、JNDC FP Decay Data File の大きな特徴である。本報告では、まずベータ崩壊の大局的理論に基づく \overline{E}_{β} , \overline{E}_{r} の理論的推定法を詳細に説明し、この方法で得られた短寿命核の崩壊データの数値表を示す。更に、測定に基づく崩壊スキームから計算される \overline{E}_{β} , \overline{E}_{r} 値のかわりに、理論値を採用したことについて、ベータ強度関数のエネルギー依存性の検討から、その正当性を明らかにする。

^{†)} 本報告書は、シグマ研究委員会・核構造データ専門部会・崩壊熱評価ワーキング・グループの作業の一環として行われた仕事をまとめたものである。

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1. Introduction

The origin of the fission product decay heat is the beta- and gamma-ray energies released from unstable fission products undergoing beta-decay. The most powerful and widely used tool to evaluate the size of this energy release is the summation calculation method, which is based on summing up of the contributions from all the unstable nuclides produced by fission events. In order to calculate the contribution from each nuclide, it is necessary to know the fission yield, the decay constant (or half-life), the branching ratios, and the average betaand gamma-ray energies $(\overline{\mathbb{E}}_{\mathrm{g}}^{}$, $\overline{\mathbb{E}}_{\mathrm{v}}^{})^{\cdot}$ per one decay event. These data are physical constants inherent to each fission product (hereafter FP), and usually a set of these data for all the important FP nuclides are stored in a peripheral memory to be read by a computer code for use in summation calculations. This kind of data set is called a FP decay data file (or library) for summation calculations. Today not a few sets of FP decay data file are open to the users who are interested in decay heat calculations. 1)-5)

In the 1970's, requirement for the high prediction accuracy of the decay heat at short cooling-times was stressed from the nuclear safety field, and it stimulated experimental and theoretical studies of the FP decay heat around the world. It was one of responses to this requirement that the Japanese Nuclear Data Committee (JNDC) started to compile a new FP decay data file in the middle of the 1970's. This file, completed in 1981 as 'JNDC FP Decay Data File'6), was aimed at improvement of the prediction accuracy of the FP decay heat at short cooling-times. The most serious obstacle to this goal was the fact that the decay data were scarce, or inaccurate even if available, for short-lived FPs which are the dominant contributors to the decay heat at short cooling-time. According to a study by Schmittroth et al. 7), the uncertainty in the $\overline{\mathbb{E}}_{\mathrm{g}}$ and $\overline{\mathbb{E}}_{\mathrm{g}}$ data is responsible for the largest portion of the total error in the calculated decay heat. In order to improve the reliability of the decay data for the 'data-unknown' FPs, the present author proposed a theoretical estimation method of $t_{1/2}$, \overline{E}_{β} and $\overline{E}_{\gamma}^{\ 8)}$ on the basis of a 'gross theory'9),10) of beta-decay. With the same intention several authors presented estimation method of $\overline{\mathbb{E}}_{\mathsf{R}}$ and $\overline{\mathbb{E}}_{\mathsf{V}}$ from different approaches. 11),12) A 'microscopic theory', 13) of beta-decay might be an alternative theoretical basis capable of calculating $\overline{\mathbb{E}}_{\beta}$ and $\overline{\mathbb{E}}_{\gamma}$ for a wide range of nuclides.

The former part of the present report is devoted to a detailed description of the way in which the present author's method is applied to the estimation of $t_{1/2}$, \overline{E}_{β} and \overline{E}_{γ} data to be contained in the JNDC FP Decay Data File. In chapter 2 we review the gross theory of beta-decay and describe the way in which the theory is applied to estimate the unknown parameters relevant to decay heat calculations. As is described in chapter 3, the adoption of the theoretical data drastically improved the consistency between calculated and measured decay heat curves at short cooling-times. The physical interpretation of this improvement is tried in chapter 4.

- 2. Decay Data of Short-Lived FPs and their Theoretical Estimation
- 2.1 Average energies of beta- and gamma-rays emitted per one decay

Before dealing with the theoretical estimation method we review the calculation method of \overline{E}_{β} and \overline{E}_{γ} for data-known nuclides. Figure 1 displays a typical decay scheme of a short-lived nuclide with a relatively large Q_{β} -value. Beta-decay of the parent nucleus (Z,N) populates not only the ground state but also many excited levels having energy ε_{i} with branching ratio a_{i} . At the first stage a beta-ray and an anti-neutrino are emitted and then the populated excited level is de-excited by emitting gamma-rays usually through a cascade process. The average energies of these beta-and gamma-rays per one beta-decay are expressed in terms of the branching ratios a_{i} (here $\Sigma a_{i} = 1$) as

$$\overline{E}_{\beta} = \sum_{i} a_{i} E_{\beta}^{(i)} \qquad (1)$$

$$\overline{E}_{\gamma} = \sum_{i} a_{i} \epsilon_{i}$$
 (2)

where $E_{\beta}^{(i)}$ is the average beta-ray energy associated with a beta-transition to the i-th excited level. By adding this to the average antineutrino energy $E_{\nu}^{(i)}$ we get the energy difference between the ground state of the parent and the i-th excited level of the daughter, say, $E_{\beta}^{(i)} + E_{\nu}^{(i)} = Q_{\beta} - \varepsilon_{i}.$ The partition of $Q_{\beta} - \varepsilon_{i}$ into $E_{\beta}^{(i)}$ and $E_{\nu}^{(i)}$ is given when the type of the beta-transition is fixed. The key quantity a_{i} essential to evaluate the right-hand sides of Eqs. (1) and (2) is given in published decay schemes, which are constructed most commonly on the basis of the beta-gamma intensity analysis.

Here we introduce the concept of the beta-strength function, which plays a quite important role in the following description of this chapter.

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Here we introduce the concept of the beta-strength function, which plays a quite important role in the following description of this chapter.

Let us suppose λ is the decay constant of the parent. Then $\lambda_{\bf i}=a_{\bf i}\cdot\lambda$ becomes a partial decay constant associated with the beta-transition which populates the i-th excited level. In the decay of a short-lived nuclide with a high Q_{β} -value, the density of the final levels is high except at low excitation energy. It is, therefore, often helpful to average $\lambda_{\bf i}$ in a suitable energy interval and to express it as a function of the excitation energy ϵ of the final level. The beta-strength function $S_{\beta}(\epsilon)$ is proportional to $\overline{\lambda}_{\bf i}\cdot\rho/f$, where f is the integrated Fermi function and ρ is the level density at ϵ . The bar on $\lambda_{\bf i}$ indicates that an average should be taken around $\epsilon_{\bf i}$. As f and ρ are known quantities, apart from some ambiguity in ρ , to know $S_{\beta}(\epsilon)$ is essentially equivalent to know $a_{\bf i}$ as long as we are interested in the calculation of \overline{E}_{β} and \overline{E}_{γ} . In this section we denoted the strength function as $S_{\beta}(\epsilon)$. In the following sections, however, it is written as $|M(E_{\beta})|^2$ in accordance with the convention used in the original papers of the gross theory. (See Note 1 below).

2.2 The gross theory of beta-decay

In this section we review the gross theory which is applied to estimate $t_{1/2}$, $\overline{\mathbb{E}}_{\beta}$ and $\overline{\mathbb{E}}_{\gamma}$. For simplicity we restrict the description within the allowed transitions. The energy spectrum of the beta-ray emitted at a transition from the ground state of the parent having a wave function. Ψ to the n-th level with a wave function Ψ_n is expressed as

$$\Pi_{n}(E) dE = \frac{mc^{2}}{\hbar} \frac{G^{2}}{2\pi^{3}} [|(\Psi_{n}, \Omega_{F}\Psi)|^{2} + \frac{C_{A}^{2}}{C_{V}^{2}} |(\Psi_{n}, \Omega_{GT}\Psi)|^{2}]$$

$$\times F(Z + 1, E) pE(E_{n} - E)^{2} dE. \qquad (3)$$

Here the symbols $\Omega_{\rm F}$ and $\Omega_{\rm GT}$ represent the transition operators for the Fermi type and the Gamow-Teller type beta-transitions. The absolute value of the ratio of the axial-vector coupling constant ${\rm C_A}$ to the vector coupling constant ${\rm C_V}$, namely $\left| {\rm C_A}/{\rm C_V} \right|$, is determined experimentally to be 1.239±0.011. The dimensionless number G which appears in the factor on the top of the

Note 1) The energy scale is shifted by Q_{β} from ϵ to E_{g} , namely, $E_{g} = \epsilon - Q_{\beta}$. We resume the notation $S_{\beta}(\epsilon)$ in the final part of this report (Section 4.2).

right hand side of Eq. (3) has a value $(3.001\pm0.002) \times 10^{-12}$, which is reduced from the ft value for a pure Fermi-transition. The Fermi function F(Z,N) is expressed as

$$F(Z,E) = 2(1 + \gamma)(2pR)^{2\gamma-2} \exp(\pi \nu) \frac{|\Gamma(\gamma + i\nu)|^2}{[\Gamma(2\gamma + 1)]^2}$$

where $\gamma=(1-\alpha^2Z^2)^{1/2}$, $\nu=\alpha ZE/p$, $\alpha=1/137$ and R is the nuclear radius. Although we measure the energy and momentum of the electron in a unit of m=c=1.0, we leave the factor \hbar/mc^2 as it is in the following expressions. In the Eq. (3) E_n is the relativistic maximum electron energy emitted at a beta-transition to the n-th excited level; by use of the symbols in Fig. 1 it is equal to $Q_{\beta}-\varepsilon_{n}+1$. The average energy of the beta- and gamma-rays, \overline{E}_{β} and \overline{E}_{γ} and the partial decay constant relevant to a transition to the n-th final level are expressed as

$$\overline{E}_{\beta}^{(n)} = \frac{1}{\lambda_n} \int_{1}^{E_n} (E - 1) \Pi_n(E) dE \dots (4)$$

$$\overline{E}_{\gamma}^{(n)} = Q_{\beta} - E_{n} + 1$$
 (4')

$$\lambda_{n} = \int_{-1}^{E_{n}} \Pi_{n}(E) dE, \qquad (4'')$$

where $\Pi_n(E)$ is given by Eq. (3). In actual situations of the short-lived FPs, where many final levels are energetically accessible, we must sum up λ_n over n to get the total decay constant λ .

$$\lambda = \sum_{n} \lambda_{n}$$

$$= \frac{mc^{2}}{h} \frac{G^{2}}{2\pi^{3}} \sum_{n} \left[\left| (\Psi_{n}, \Omega_{F} \Psi) \right|^{2} + \frac{C_{A}^{2}}{C_{V}^{2}} \left| (\Psi_{n}, \Omega_{GT} \Psi) \right|^{2} \right]$$

$$\times f(E_{n}). \qquad (5)$$

The function $f(E_n)$ which appears in the above expression is called the integrated Fermi function and is written as

Note 2) The number G is related to the vector constant ($|C_V| = 1.405 \times 10^{-49} \text{ erg} \cdot \text{cm}^3$) through an expression $C_V^2 = G^2 \frac{\pi^6}{m^4 c^2}$.

$$f(E_n) = \int_{-1}^{E_n} F(Z + 1, E) pE(E_n - E)^2 dE$$
 (5')

The starting point of the gross theory $^{15)}$ of beta-decay lies in a replacement of the summation over n by an integration with the energy E which is equal to $-(E_n-1)$, as the variable; resultingly,

$$\lambda = \frac{mc^{2}}{\hbar} \frac{G^{2}}{2\pi^{3}} \int_{-Q_{\beta}}^{0} \left[|M_{F}(E_{g})|^{2} + 3 \frac{C_{A}^{2}}{C_{V}^{2}} |M_{GT}(E_{g})|^{2} \right]$$

$$\times f(-E_{g} + 1) dE_{g} \qquad (6)$$

It is a conventional notation of the original papers of the gross theory to use E as energy variable. (E is, in other words, the mass change in the neutral atom before and after the transition.) The symbol $|M_{\omega}(E_g)|^2$ (ω = F or GT) denotes the beta-strength function and is equal to the absolute square of transition matrix element $|(\Psi_n, \Omega_\omega \Psi)|^2$ multiplied by the level density around E in Eq. (6) the factor of 3 of the Gamow-Teller term comes from an assumption that the parent nucleus is unpolarized.

The determination of the energy profile of the beta-strength function constitutes the essential part of the gross theory. Yamada and Takahashi⁹⁾ carried out this with the aid of the sum rules as follows.

$$\int_{-Q_{\beta}}^{\infty} |M_{\omega}(E_{g})|^{2} dE_{g} = \sum_{n}^{\infty} (\Psi, \Omega_{\omega}^{\dagger} \Psi_{n}) (\Psi_{n}, \Omega_{\omega} \Psi)$$

$$= (\Psi, \Omega_{\omega}^{\dagger} \Omega_{\omega} \Psi_{n}) \qquad (7)$$

$$\int_{-Q_{\beta}}^{\infty} |M_{\omega}(E_{g})|^{2} dE_{g} = (\Psi, \Omega^{\dagger}[H, \Omega]\Psi) \qquad (8)$$

$$\int_{-Q_{\beta}}^{\infty} |E_{g}| |M_{\omega}(E_{g})|^{2} dE_{g} = (\Psi, [\Omega^{\dagger}, H][H, \Omega]\Psi) \qquad (9)$$

In order to refine the theory they introduced an one-particle strength function $D_{\omega}(E_{g}, \xi)$ by decomposing the total strength into the contributions from individual nucleons in the nucleus as

$$|M_{\omega}(E_g)|^2 = \int_{\xi_{\min}}^{\xi_{\max}} D_{\omega}(E_g, \xi) \cdot W(E_g, \xi) \frac{dn_1}{d\xi} d\xi , \dots (10)$$

where ξ is the energy of the nucleon undergoing decay, $W(E_g, \xi)$ is a factor representing the effect of the Pauli's exclusion principle, and $\frac{dn_1}{c\xi}$ is the

one particle level density of the initial state.

Here we give, as an example, the form of the one-particle strength function for the Fermi-type transition;

$$D_{F}(E_{g}, \xi) = \frac{\sigma_{c}^{2} + \gamma^{2}}{\pi} \frac{\sigma_{c}^{2}}{\gamma} \frac{1}{(E_{g} - \Delta_{c})^{2} + (\sigma_{c}^{2}/\gamma)^{2}}$$

$$\times \frac{1}{(E_{g} - \Delta_{c})^{2} + \gamma^{2}} \cdot \dots (11)$$

In this case a modified-Lorentz form is assumed and the parameters Δ_c (peak position) and σ_c (peak width) are determined with the aid of the sum rules (8) and (9) in the following way.

$$\int_{-\infty}^{\infty} E_{g} \cdot D_{F}(E_{g}, \xi) dE_{g} = \Delta_{c}$$

$$= \left[\frac{1.44}{(r_{0}/1.2)} \frac{Z}{A^{1/3}} - 0.7825 \right] MeV (8')$$

$$\int_{-\infty}^{\infty} (E_{g} - \Delta_{c})^{2} D_{F}(E_{g}, \xi) dE_{g} = \sigma_{c}^{2}$$

$$= \left[\frac{0.157}{(r_{0}/1.2)} \frac{Z}{A^{1/3}} MeV \right]^{2}, \qquad (9')$$

where Z, r_0 , and A denote the proton number of the parent, the radius of the volume occupied by one nucleon, and the mass number, respectively. The sum rule (7) has already been used to determine the normalization factor of $|M_{\omega}(E_g)|^2$. The expression (8') reduced from the sum rule (8) represents the sum of changes in the Coulomb energy and in the nucleon mass $(p \rightarrow n)$ induced by the decay. The expression (9') gives the peak width of the strength which is brought about by the presence of the isospin impurity; in other words, if the isospin is a good quantum number, the width becomes zero. In the case of the Gamow-Teller transition, we replace σ_c^2 by $\sigma_c^2 + \sigma_N^2$, where σ_N^2 gives the increase of the width induced by incommutability of the Gamow-Teller transition operator $\boldsymbol{\Omega}_{\text{CT}}$ with the spin dependent part of the nuclear force; in the present calculation $\sigma_N^{\ 2}$ is taken to be 12 MeV. $^{10)}$ In the above description we restricted the discussion within the allowed transitions. The gross theory of the forbidden transition was developed by Takahashi 17) and this is taken also into account in the present calculation. In order to apply the theory in

practical problems it is essential to take into account the transitions between one-particle discrete levels. This is accomplished by using of a rather simple one-particle nuclear model. As a result the one-particle strength function is largely modified and becomes a sum of a continuum part and delta-functions representing the discrete transitions. The complete description of the procedure of obtaining the one-particle strength is too bulky to reproduce here. Refer to the original paper for it. Anyway we get the total strength function by integrating the one particle strength according to the formula (1).

The gross theory expression for the decay constant λ is given by Eq. (6). In the later part we calculate the average beta- and gamma-ray energies per one decay $(\overline{E}_{\beta}, \overline{E}_{\gamma})$ on the basis of the gross theory. A close parallel procedure leads to the gross theory description for these quantities. At first we deal with the calculation of the average beta-ray energy. This quantity \overline{E}_{β} is given by summing up all the contributions from the transitions to the every final levels; namely,

$$\overline{E}_{\beta} = \frac{1}{\lambda} \sum_{n} \widetilde{E}_{\beta}^{(n)}$$

$$= \frac{1}{\lambda} \frac{mc^{2}}{\hbar} \frac{G^{2}}{2\pi^{3}} \sum_{n} \left[\left| (\Psi_{n}, \Omega_{F} \Psi) \right|^{2} + \frac{C_{A}^{2}}{C_{V}^{2}} \left| (\Psi_{n}, \Omega_{GT} \Psi) \right|^{2} \right]$$

$$\times \int_{1}^{E_{n}} (E - 1) F(Z + 1, E) pE(E_{n} - E)^{2} dE, \dots (12)$$

where $\overline{E}_{\beta}^{}$ (n) represents the average beta-ray energy released at a transition feeding the n-th final level as is given by Eq. (4). The partial decay constant λ_n is given by Eq. (5). The translation of this expression into the gross theory form is easily done in a quite parallel way to the case of the decay constant. The only difference is that the integrant, in this case, has an additional factor (E - 1) which does not appear in the expression (6) for λ .

$$\overline{E}_{\beta} = \frac{C}{\lambda} \int_{-Q_{\beta}}^{0} \left[|M_{F}(E_{g})|^{2} + 3 \frac{C_{A}^{2}}{C_{V}^{2}} |M_{GT}(E_{g})|^{2} \right] \\
\times \left[\int_{1}^{-E} g^{+1} (E - 1) F(Z + 1, E) pE(-E_{g} + 1 - E)^{2} dE \right] dE_{g}, ... (13)$$

where the constant C denotes the factor $\frac{mc^2}{\tilde{n}}$ $\frac{G^2}{2\pi^3}$

To derive the expression for the gamma-ray energy \overline{E}_{γ} we assume that the excitation energy of the level populated by the beta-transition is

released solely as gamma-rays; in other words we neglect the effects of the delayed neutron emission and the internal conversion. The expression, then

$$\overline{E}_{\gamma} = \frac{1}{\lambda} \sum_{n} \Omega_{n} \overline{E}_{\gamma}^{(n)}$$

$$= \frac{1}{\lambda} \sum_{n} (Q_{\beta} - E_{n} + 1) \lambda_{n}$$

$$= \frac{1}{\lambda} \frac{mc^{2}}{\overline{n}} \frac{G^{2}}{2\pi^{3}} \sum_{n} \left[|(\Psi_{n}, \Omega_{F}\Psi)|^{2} + \frac{C_{A}^{2}}{C_{V}^{2}} |(\Psi_{n}, \Omega_{GT}\Psi)|^{2} \right]$$

$$\times (Q_{\beta} - E_{n} + 1) f(E_{n}) . \qquad (14)$$

The corresponding expression in the gross theory form is

$$\overline{E}_{\gamma} = \frac{C}{\lambda} \int_{-Q_{\beta}}^{0} \left[|M_{F}(E_{g})|^{2} + 3 \frac{C_{A}^{2}}{C_{V}^{2}} |M_{GT}(E_{g})|^{2} \right]$$

$$\times (Q_{\beta} + E_{g}) f(-E_{g} + 1) dE_{g} . \qquad (15)$$

Before closing this subsection we overview the behavior of the betastrength function. Fig. 2 displays the energy profile of the beta-strength functions for the Fermi, the Gamow-Teller, and the first-forbidden transi-The sharp peak of the Fermi strength is situated at the isobaric analog state, the eigen state of the total isospin T. This is due to the fact that the Fermi transition operator is essentially $T_x + iT_y$ which elevates the z-component of the isospin by unit one. If the total isospin is a good quantum number, the Fermi-strength becomes a delta-function at the isobaric analog state. The thin but finite width of the strength is resulted by the impurity of the isospin. In a classical term this is interpreted as follows. The Coulomb potential within a nucleus is not always uniform. The Coulomb energy change induced by a decay of a neutron into a proton, therefore, depends on the position of the decaying neutron within the nucleus. This gives rise to the spread of the Fermi strength. The Gamow-Teller strength has a broad peak around the isobaric analog state. The wide spread of the peak is caused by incommutability of the Gamow-Teller transition operator with the spin-dependent part of the nuclear force. The strength function of the first-forbidden transition has two peaks with spread widths.

Here it should be noted that only the lower tails of these strengths

are energetically accessible by real beta-transitions. (This is not the case for light nuclides, where the isobaric analog state is accessible energetically). This leads to the fact that the total strength is an increasing function of energy. Though this tendency is largely cancelled out by the presence of f, a decreasing function of the excitation energy, in the expressions for λ , $\overline{\mathbb{E}}_{\beta}$, and $\overline{\mathbb{E}}_{\gamma}$, the high energy part of the total strength plays an important role in the following discussions.

2.3 A preparatory consideration

The essential quantities needed in decay heat calculations, λ , \overline{E}_{β} , \overline{E}_{γ} , are given by the expressions (6), (13) and (15). These quantities, generally, vary sensitively if the transitions to the ground or to the low-lying states are prohibited by some selection rule. In order to consider this effect of the selection rules in the calculation based on expressions (6), (13) and (15), we follow the method of Takahashi et al. 10) and introduce a parameter Q_{00} , which represents the energy of the lowest level to which the transition is allowed by selection rules.

In order to incorpolate the parameter $\boldsymbol{\varrho}_{00}$ into the gross theory, the strength function is modified as

$$|M_{\omega}^{\dagger}(E_{g})|^{2} = \begin{cases} |M_{\omega}(E_{g})|^{2} + \delta(E_{g} + Q_{\beta} - Q_{00}) \int_{-Q_{\beta}}^{-Q_{\beta}+Q_{00}} |\Delta E_{g}^{\dagger}(E_{g} \geq -Q_{\beta} + Q_{00}) \\ 0 & (-Q_{\beta} \leq E_{g} < -Q_{\beta} + Q_{00}) \end{cases}$$
(16)

By this modification the strength distributed over the energy range below \mathbf{Q}_{00} , where the transition is prohibited, is to be concentrated at \mathbf{Q}_{00} in the form of a delta-function. Takahashi et al. applied the same value of \mathbf{Q}_{00} to all the nuclides. In the present study we tried to find the best value of \mathbf{Q}_{00} for each nuclide.

As is described in ref. 8), 19 short-lived FPs were selected from the compilation by Tobias and the parameter Q_{00} was determined for each nuclide so that the calculation should reproduce the Tobias' value of \overline{E}_{β} and \overline{E}_{γ} best. The calculations were performed with the expressions (13) and (15) where $|M_{\omega}(E_g)|^2$ being replaced by the modified one $|M_{\omega}'(E_g)|^2$. Further, the same Q_{00} value was assumed for all the types of the transition, namely, Fermi, Gamow-Teller, and 1-st forbidden transitions. The results are shown in Table I. As is seen here, the gross theory reproduces the experimental values of \overline{E}_{β} and \overline{E}_{γ} quite well owing to the appropriate

selection of Q_{00} for each nuclide. The values of Q_{00} scatter between 0.0 and 2.5 MeV. Figs. 4-6 display the results of the gross theory calculations with these upper and lower values of Q_{00} , 0.0 and 2.5 MeV, and also with $\mathrm{Q}_{00}=1.0$ MeV for FPs having Q values larger than 3 MeV. In these calculations the mass number A is fixed to 90 (for even A nuclides) or to 89 (for odd A nuclides). Most of the experiment-based values of E_{β} and E_{γ} (due to Tobias, Ref. 20)) scatter between two calculated curves of $\mathrm{Q}_{00}=0.0$ MeV and of $\mathrm{Q}_{00}=2.5$ MeV with a few exceptions such as $^{97}\mathrm{Y}$, $^{82}\mathrm{As}$ and $^{92}\mathrm{Rb}$. The curve of $\mathrm{Q}_{00}=1.0$ MeV goes through amid the scattered data points, suggesting that this curve is adoptable as a good estimation of E_{β} and E_{γ} when no further information is available which helps us to find a more reliable value of Q_{00} . The observations in this section suggest that the range 0.0 - 2.5 MeV should be appropriate for the Q_{00} variation from nuclide to nuclide.

2.4 Estimation of average beta- and gamma-ray energies, $\overline{\mathbb{E}}_{\beta}$ and $\overline{\mathbb{E}}_{\gamma}$ The goal of this chapter is to establish a reasonable method to estimate the average beta- and gamma-ray energies released per one decay of a short-lived FP nuclide. In order to use the gross theory for this purpose, we must think out a way to find the appropriate value of the parameter Q_{00} of each nuclide. This section deals with the determination of the Q_{00} value.

There are very many FP nuclides for which only the half-life is known, because the measurement of half-life is easier than the experimental determination of other physical characters of a short-lived nuclide. From a practical point of view, these short-lived FPs play an important role in the FP decay heat shortly after the reactor shut-down. Further, as is discussed in the later part of this report, it is often the case that theoretically estimated values of \overline{E}_β and \overline{E}_γ are more reliable than those based on the experimentally determined decay schemes so long as the decay schemes are incomplete from some aspects.

The half-life $t_{1/2}$ (or the decay constant λ) is a quantity which is quite sensitive to the effect of the selection rules on the ground and low-lying levels, in other words, on the value of Q_{00} . In this respect we can make an assumption that the information about these effects of selection rules is included in the value of $t_{1/2}$ in a implicit way. This leads to an idea to determine the value of Q_{00} on the basis of the measured half-life of each nuclide.

Fig. 7 displays a comparison between calculated and experiment-based $^{20)}$ values of $\overline{\mathrm{E}}_{\beta}$ and $\overline{\mathrm{E}}_{\gamma}$ for 34 FPs with Q_{β} larger than 5 MeV. At the time of calculation, the value of the parameter Q_{00} was determined for each nuclide so that the calculation might reproduce the measured half-life in the best way. In this procedure of determining the value of Q_{00} the domain of the variation of this parameter was taken to be between 0.0 and 2.0 MeV for odd-odd nuclides and between 0.5 and 2.0 MeV for others.

As is seen in the preceding section, the most of the Q_{00} values which were determined so as to reproduce the experimental values of \overline{E}_{β} and \overline{E}_{γ} lie between 0.0 and 2.5 MeV. In the present parameter survay we cut off the upper and the lower ends of this range by 0.5 MeV and adopted the range 0.5 - 2.0 MeV as is mentioned above. An exception is the odd-odd nuclide case, where a range of 0.0 - 2.0 MeV was adopted so that the transition into the ground state should be allowed. Many odd-odd nuclides have ground states of spin-parity 1^+ which can decay to 0^+ ground state of the daughters (even-even) by the Gamow-Teller transition ($|\Delta J|$ = 1, parity change: no).

It is clear from the comparison of Figs. 7 and 8 that the determination of Q_{00} based on measured half-life is quite effective to reproduce Realistic values of \overline{E}_β and \overline{E}_γ . The former shows the results of the Q_{00} optimization mentioned above and the latter corresponds to the case where the value of Q_{00} is fixed to 1.0 MeV for all the nuclides. The values of these figures are normalized so that the sum of \overline{E}_β , \overline{E}_γ and the antineutrino energy should becomes 100.0. The dotted and the solid lines indicate \overline{E}_β and $\overline{E}_\beta+\overline{E}_\gamma$, respectively.

- 3. Data for \overline{E}_{β} , \overline{E}_{γ} and $t_{1/2}$ Adopted in the JNDC File
- 3.1 Estimated \overline{E}_{β} and \overline{E}_{γ} values

The JNDC Decay Heat Evaluation Working Group calculated \overline{E}_{β} and \overline{E}_{γ} for more than 700 nuclides including many short-lived ones on the basis of decay schemes published until 1980. The expressions (1) and (2) were used to derive these values. For short-lived ones among them, the values \overline{E}_{β} and \overline{E}_{γ} were also calculated by the method described in Sec. 4.2. Fig. 9 displays the results for nuclides which have Q_{β} values larger than 3 MeV. Theoretical values based on the method described in Sec. 2.4 and the values from ENDF/B-IV (Δ) and from Tasaka's File (∇) are also shown there. It should be noted that the ENDF/B-IV and the Tasaka's File include estimated data based on relatively simple extrapolation methods. On the other hand, the JNDC data (o) are wholly derived from decay schemes; (i.e.

Fig. 7 displays a comparison between calculated and experiment-based $^{20)}$ values of $\overline{\mathbb{E}}_{\beta}$ and $\overline{\mathbb{E}}_{\gamma}$ for 34 FPs with \mathbb{Q}_{β} larger than 5 MeV. At the time of calculation, the value of the parameter \mathbb{Q}_{00} was determined for each nuclide so that the calculation might reproduce the measured half-life in the best way. In this procedure of determining the value of \mathbb{Q}_{00} the domain of the variation of this parameter was taken to be between 0.0 and 2.0 MeV for odd-odd nuclides and between 0.5 and 2.0 MeV for others.

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all the JNDC values are based on experiments.) A survey of Fig. 9 leads to the following observations; 1). The average beta-energies from the four data sources (JNDC, ENDF/B-IV, Tasaka and theoretical estimation) are consistent each other in a relative sense. 2) For the gamma-ray energy the consistency deteriorates appreciably. 3) As for the gamma-energy (\overline{E}_{γ}) , the JNDC value is quite often the lowest among the four data sources.

A comment is needed here about the second observation above. For simplicity let us assume that the whole beta-strength concentrates on the level at Q_{00} . A shift of Q_{00} by $\Delta\mathsf{Q}_{00}$ results in a change in the average gamma-ray energy by the same amount, namely, by $\Delta\mathsf{Q}_{00}$. On the contrary the average beta-energy changes only by C Q_{00} , where the factor C, having a value smaller than 1.0 (0.3 - 0.5), is the ratio of the beta-ray energy to the sum of beta-ray and anti-neutrino energies. In this respect $\overline{\mathsf{E}}_{\gamma}$ is more sensitive to the assumed value of Q_{00} than the case of $\overline{\mathsf{E}}_{\beta}$. In the estimation calculations of $\overline{\mathsf{E}}_{\beta}$ and $\overline{\mathsf{E}}_{\gamma}$, the assumed values of Q_{00} have fairly large ambiguity in general. Hence the estimated value of $\overline{\mathsf{E}}_{\gamma}$ is more ambiguous than the value of $\overline{\mathsf{E}}_{\beta}$.

- 3.2 Data for \overline{E}_{β} , \overline{E}_{γ} and $t_{1/2}$ for nuclides with no experimental data Among more than 1100 nuclides and isomers whose decay and yield data are stored in the JNDC FP Decay Data File, about 380 nuclides and isomers lack measured decay data. More precisely, neither half-lives nor decay schemes are known for 280 among them, and only half-lives are known for the rest. Theoretical estimation of \overline{E}_{β} , \overline{E}_{γ} and $t_{1/2}$ were carried out for these nuclides with the aid of the gross theory and the results were stored into the JNDC FP Decay Data File.
- 1) Estimation of \overline{E}_{β} and \overline{E}_{γ} for nuclides with no decay data except $t_{1/2}$: For these nuclides the values of \overline{E}_{β} and \overline{E}_{γ} were estimated with the method described in Sec. 2.4. The parameter Q_{00} was optimized so that the best consistency should be attained between calculated and measured half-lives. The variation range of Q_{00} was taken to be $0.0 \le Q_{00} \le 2.0$ MeV for odd-odd nuclides and to be $0.5 \le Q_{00} \le 2.0$ MeV for others. The Q_{β} values were taken from the compilation by Wapstra and Bos, Q_{00} or were calculated by Uno and Yamada's linear type mass formula when Wapstra and Bos give no information. Table II summarizes the values of \overline{E}_{β} , \overline{E}_{γ} , Q_{β} and Q_{00} for the nuclides belonging to this category.
- 2) Estimation of $\overline{\mathbb{E}}_{eta}$, $\overline{\mathbb{E}}_{\gamma}$ and $\mathfrak{t}_{1/2}$ for nuclides with no measured data:

For these nuclides, the estimation method used for the nuclides of category 1) is inapplicable because half-lives are not known. The key parameter \mathbf{Q}_{00} was determined in the following two methods, namely;

- (a) The Q_{00} -value was fixed to 1.0 MeV for all the nuclides.
- (b) Systematic behavior of the values of \mathbf{Q}_{00} was examined in several subdivided mass regions and the value of \mathbf{Q}_{00} was extrapolated to each nuclide in each mass region.

By use of the \mathbf{Q}_{00} values determined in the above two methods, $\overline{\mathbf{E}}_{\beta}$, $\overline{\mathbf{E}}_{\gamma}$ and $\mathbf{t}_{1/2}$ were calculated. There was, however, no essential difference between the two decay heat curves corresponding to the above two methods. This is due to the fact that the contribution from the nuclides of this category is minor even at very short cooling-times. In practice we stored the $\overline{\mathbf{E}}_{\beta}$, $\overline{\mathbf{E}}_{\gamma}$ and $\mathbf{t}_{1/2}$ data based on method (b). The whole results are given in Table III.

3.3 Adoption of theoretical data for high-Q $_{\rm B}$ nuclides with experimental data For 88 short-lived nuclides listed in Table IV, theoretically estimated values of $\overline{\rm E}_{\rm B}$ and $\overline{\rm E}_{\rm Y}$ were finally adopted, though these nuclides have experimental information on their beta- and gamma-decay schemes which enable us to calculate $\overline{\rm E}_{\rm B}$ and $\overline{\rm E}_{\rm Y}$ apart from their reliability. A justification for this preferential adoption of the theoretical data in place of the experiment-based data will be dealt with in Chapter 4. The method to obtain the theoretical values of $\overline{\rm E}_{\rm B}$ and $\overline{\rm E}_{\rm Y}$ is the same as that for the nuclides of category 1) of Sec. 3.2; namely, the optimization of the parameter ${\rm Q}_{00}$ with the aid of the measured half-life. Table IV summarizes the theoretical (T) and experiment-based (E) values of $\overline{\rm E}_{\rm B}$ and $\overline{\rm E}_{\rm Y}$, the measured half-lives used to determine ${\rm Q}_{00}$, the resultant value of ${\rm Q}_{00}$ and the calculated half-lives. This table also gives fractional contribution from each nuclide in the ${\rm Calculate}$ decay heat shortly after a burst irradiation of thermal neutrons.

Before ending this chapter we review briefly the consequence of this adoption of the theoretical data though detailed descriptions are given in Ref. 25). Figs. 10 and 11 display the beta- and gamma-ray components of the ^{235}U decay heat after an instantaneous irradiation of thermal neutrons. Adoption of the theoretically estimated values of $\overline{\text{E}}_{\beta}$ and $\overline{\text{E}}_{\gamma}$ for the above 88 nuclides drastically improves the consistency between the calculated and the measured decay heat (from A to B). LaVauve et al. successfully tried to remove an apparent disagreement between measured and

calculated decay heat curves at short cooling time by introducing the JNDC values of $\overline{\mathbb{E}}_\beta$ and $\overline{\mathbb{E}}_\gamma$ into the ENDF/B-V data base. Their results are shown in Fig. 12. Remarkable change brought about by the introduction of the JNDC data seems to come mostly from the 88 nuclides described above in their result, too. In the next chapter we see the reason why the theoretical values lead to a success in interpreting the measured decay heat at short cooling-times.

- 4. Problems in Deriving \overline{E}_{β} and \overline{E}_{γ} from Decay Schemes
- 4.1 Incompleteness of decay schemes for short-lived nuclides

A quite suggestive numerical experiment was carried out by J. C. Hardy et al. ³¹⁾ They generated numerically a hypothetical beta-gamma decay scheme of a fictional nuclide 'pandemonium' under the following conditions.

- 1) Atomic and mass numbers and spin-parity are taken to be the same as Gd-145, namely z=64, A=145, $I^{II}=1/2^{+}$ and further $Q_{EC}=5$ MeV.
- 2) The level density of the daughter nuclide (Z = 63, A = 145) takes after the Gilbert-Cameron's level density formula.
- 3) Level spacings obey the Wigner's statistics.
- 4) The Gamow-Teller transition probability to each level obeys the random Porter-Thomas distribution.
- 5) The beta-transition matrix is assumed to be independent of the excitation energy.

Then the Ge(Li)-detector response to the gamma-rays from the decaying 'pandemonium' was generated under realistic conditions for resolution, efficiency, etc. The resultant response data were analysed with a peak analysis code SAMPO. As a result of this gedanken-experiment it was proved that a sizable portion of the total gamma-ray intensity remained undetected. From this observation they concluded that the decay schemes constructed on the basis of the peak analysis and the intensity balance of gamma-rays are incomplete in general for short-lived high-Q-value nuclides. They do not describe this incompleteness of decay schemes in detail. It is easy to see, however, that the incompleteness manifests itself in the high excitationenergy side where the level density is high and the gamma decay structure is complicated. When the high energy part of a decay scheme is oversimplified or missing, the beta-strength function is underestimated at high energy. This inevitably introduces a systematic bias into the values of $\overline{\mathbb{E}}_{\mathsf{R}}$ and $\overline{\mathbb{E}}$. This must be the origin of the overestimation of the beta decayheat and the underestimation of the gamma decay-heat at short cooling

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times, which was depicted in section 3.3.

Fig. 13 displays a decay scheme of 93 Kr, which is taken from the Tables of Isotopes 7th edition. 22) This nuclide, situated near the light peaks of the fission yield curves of U and Pu, has a relatively high $Q_{\!\scriptscriptstyle R}\!-\!$ value $(7.3 \text{ MeV}^{22}) - 8.7 \text{ MeV}^{6})$ and a short beta half-life. The excited levels are identified, however, only up to 4.9392 MeV and 98.1 % of the total beta-intensity is allotted below this highest level. It seems unreal that there is no beta-intensity between 5 and 7 MeV. Actually 1.9 % of the beta-intensity is given to the delayed neutron window around 7 MeV. This intensity happened to be detected owing to the existence of the delayed neutron, which played a role of a probe, so to speak. It is, therefore, doubtless that a non-negligible amount of beta-intensity should exist between 5 and 7 MeV, and also above 7 MeV. The $\overline{\mathbb{E}}_{\beta}$ value is overestimated and the $\overline{\mathbb{E}}_{_{\mathbf{y}}}$ value is underestimated when they are derived from this decay scheme which lacks beta-intensities to unknown highly excited levels. This example of 93 Kr is not a exceptional one but represents a defect common to high-Qg-value decay schemes. As another example, let examine the case of 95 Sr, which has a Q_8 -value of 6.09 MeV 22) (Fig. 14). In this case no beta-intensity is given above 4.2677 MeV. The \overline{E}_{β} and \overline{E}_{γ} values are as follows.

	\overline{E}_{β} (Be	ta-energy)	$\overline{\overline{E}}_{\gamma}$ (Ga	mma-energy)
	Decay scheme	Gross theory	Decay scheme	Gross theory
93 _{Kr}	2.89	2.73	2.28	2.76
95 _{Sr}	2.27	1.59	1.03	2.44
			(all	in MeV unit)

When being derived from decay schemes, \overline{E}_{β} is larger and \overline{E}_{γ} is smaller in comparison with the gross theory values as is expected from the above discussion. It should be kept in mind, however, that the gross theory does not always give the best estimates of \overline{E}_{β} and \overline{E}_{γ} for each individual nuclide, because this theory describes overall properties of wide range of nuclides from its nature.

Observations in this section can be summarized in the following way.

The published decay schemes of short-lived FPs miss a non-negligible amount of the beta-intensity to unknown highly-excited levels. This leads

to an overestimation of \overline{E}_{β} and, equivalently, to an underestimation of \overline{E}_{γ} . In this defect of the published decay schemes we find the reason why the recently completed libraries such as the preliminary version of the JNDC file, ENDF/B-V³⁰⁾ and UKFPDD-2³²⁾ failed in reproducing the beta- and gamma-ray components of decay heat at short cooling-times.

4.2 Beta-strength function and decay heat

In section 4.1 we dealt with incompleteness of high- Q_{β} -value decay schemes and with its consequences on derived \overline{E}_{β} and \overline{E}_{γ} values. In this section a quite simple strength function model is introduced in order to make the discussion more quantitative.

In recent years information on the beta-strength functions has been accumulated by using of specially designed instrumentations. $^{33)-35)}$ Fig. 15 displays beta-strength functions of short-lived FPs measured by K. H. Johansen et al. $^{34)}$ Difference between the open and the solid circles comes from the uncertainty in assumed $\rm Q_{\beta}$ -values. Very roughly speaking we can fit these curves with an exponential function $\rm e^{E/\alpha}$. The value of α ranges from 0.5 to 2.0 MeV. This observation will be made use in the later part of this section.

The average gamma-ray energy \overline{E}_{γ} can be expressed as (15) in terms of the strength functions. We use an energy variable E (equivalent to ϵ used in chapter 2) instead of E_g . They are related as $E=Q_{\beta}+E_g$. Then, we have

$$\overline{E}_{\gamma} = \frac{C}{\lambda} \int_{0}^{Q_{\beta}} |M(E - Q_{\beta})|^{2} E \int_{0}^{Q_{\beta}-E+1} F(Z + 1, W) (W^{2} - 1)^{1/2} W(Q_{\beta} - E + 1 - W)^{2} dW dE,$$
(17)

where the integrated Fermi function f is rewritten explicitly using the expression (5'). We confine the following discussion within the allowed transition. Hence the Fermi function F(Z,W) is written in non-relativistic approximation as 36

$$F(Z, W) = \frac{2\pi y}{1 - \exp(-2\pi y)}, \quad y = \frac{Z}{137} W(W^2 - 1)^{-1/2}$$

Further, by using of an approximation $F(Z, W) \simeq 2\pi y$, the integrant of the second integral becomes $W^2(Q_R - E + 1 - W)^2$ and analytically integrable. The result is $(X^5 + 5X^4 + 10X^3)/30$ with $X = Q_\beta - E$. By rewriting $|M(E - Q_\beta)|^2$ as $S_\beta(E)$, we get a simple expression for average gamma-ray

energy;

$$\overline{E}_{\gamma} = \frac{c}{30\lambda} \int_{0}^{Q_{\beta}} S_{\beta}(E) E(X^{5} + 5X^{4} + 10X^{3}) dE . \qquad (18)$$

It is shown that the above approximations for the Fermi function introduce no serious error except heavy nuclides like actinides. ³⁷⁾ By using of the expression (18), the consequences of the missing beta-intensity to the highly excited levels will be examined.

Let us suppose two types of the energy dependence of the beta-strength function; linear type $S_{\beta} \propto E$ and exponential type $S_{\beta} \propto e^{E/\alpha}$. In order to see the effect of the missing beta-intensity, or the missing strength, we introduce a modified strength function $S_{\beta}(E,q)$, which has no strength above a critical energy q,

$$S_{\beta}(E, q) = \begin{cases} C_s E \text{ or } C_s e^{E/\alpha} \text{ for } 0 \le E \le q \\ \\ 0 \text{ for } q \le E \le Q_{\beta} \end{cases}.$$

The function $S_{\beta}(E,Q_{\beta})$ represents a situation in which the strength is fully known up to the maximum excitation energy. We write the average gamma-ray energy as $\overline{E}_{\gamma}(q)$ which is calculated with the strength $S_{\beta}(E,q)$;

$$\frac{\int_{0}^{Q_{\beta}} s_{\beta}(E, q) E(X^{5} + 5X^{4} + 10X^{3}) dE}{\int_{0}^{Q_{\beta}} s_{\beta}(E, q) (X^{5} + 5X^{4} + 10X^{3}) dE} \qquad(19)$$

$$(X = Q_{\beta} - E) .$$

The ratio $\overline{\mathbb{E}}_{\gamma}(q)/\overline{\mathbb{E}}_{\gamma}(\mathbb{Q}_{\beta})$ gives a measure of the underestimation of $\overline{\mathbb{E}}_{\gamma}$ caused by missing of beta-intensity above the energy q. Fig. 16 displays this ratio as a function of q on the basis of three types of assumed strength functions; E, $e^{E/1.5}$ and e^E . The experimental background of taking the value of α to be 1.5 and 1.0 MeV is as follows.

- 1) As was observed at the beginning of this section the value of α ranges from 0.5 to 2.0 MeV.
- 2) The ratio $\overline{E}_{\gamma}/Q_{\beta}$ should fall within 0.25 0.35, which is a typical value of this ratio from the viewpoint of the microscopic and integral measurements. (See Table V)

Among the values of α which fulfil the above criteria, two typical values,

1.5 and 1.0 MeV, were adopted for the present discussion. As is seen from Table V, $\overline{E}_{\gamma}/Q_{\beta}$ is too large for large Q_{β} nuclides when $S_{\beta} \stackrel{\text{\tiny c}}{=} e^E$ is used. From this respect, $S_{\beta} \stackrel{\text{\tiny c}}{=} e^{E/1.5}$ is preferable. (See footnote 3)

Let us examine the curve in Fig. 16, which corresponds to $Q_{\rm g}$ = 8 MeV and $S_g \propto e^{E/1.5}$. If the beta transition to levels above 5 MeV is missed, the \overline{E}_{γ} value is underestimated by 10 %. This reaches 20 % when the intensity is missing above 4 MeV. The underestimation becomes larger if we take e^{E} as S_{g} . A survey of published decay schemes of short-lived FPs (typically refer to the Tables of Isotopes 22) leads to an observation that beta-intensity is not given above 3 - 5 MeV for most high- $Q_{\hat{B}}$ nuclides. By combining this observation with the above result from the simple strength-function calculation, we come to a conclusion that the value of \overline{E}_{γ} is open to underestimation by 10 - 30 % for nuclides with Q_{β} -values larger than 5 - 6 MeV. On the contrary the \overline{E}_{γ} and \overline{E}_{β} values calculated with the gross theory reflect properly the effect of the large beta-strength at high energy, which increases \overline{E}_{γ} and decreases \overline{E}_{β} . This is the reason why the introduction of gross theory values drastically improved the reproducibility of the measured beta- and gamma-ray components of the decay heat at short cooling-times.

5. Concluding Remarks

The method of theoretical estimation of the average energies \overline{E}_{β} and \overline{E}_{γ} was described in detail. It is a notable feature of the JNDC FP Decay Data File that these estimated values are fully adopted for short-lived FPs with high Q_{β} -values ($Q_{\beta} \gtrsim 5$ MeV) in place of the values derived from the published decay schemes. Discussions were made in favor of this preferential selection of the theoretical values. In the course of the discussions the following things were known.

- Note 3) Several authors assumed a level-density-proportional behavior for the beta-strength function. Roughly speaking, this assumption corresponds to taking the α value as 0.5-0.9 in the expression $S_{\beta} \stackrel{\sim}{=} e^{E/\alpha}$. This selection, however, leads to serious overestimation of $\overline{E}_{\gamma}/Q_{\beta}$ ratio (larger than 0.4). Further, this ratio increases too rapidly as a function of Q_{β} . From this respect, the level-density proportional assumption is not acceptable.
- Note 4) Here consideration was made only for \overline{E}_{γ} . It is easy to see, however, \overline{E}_{β} is overestimated when \overline{E}_{γ} is underestimated, for they are closely related by the energy conservation.

1.5 and 1.0 MeV, were adopted for the present discussion. As is seen from Table V, $\overline{E}_{\gamma}/Q_{\beta}$ is too large for large Q_{β} nuclides when $S_{\beta} \cong e^E$ is used. From this respect, $S_{\beta} \cong e^{E/1.5}$ is preferable. (See footnote 3)

Let us examine the curve in Fig. 16, which corresponds to $Q_{\hat{B}}$ = 8 MeV and $S_g \propto e^{E/1.5}$. If the beta transition to levels above 5 MeV is missed, the $\overline{\mathbb{E}}_{\gamma}$ value is underestimated by 10 %. This reaches 20 % when the intensity is missing above 4 MeV. The underestimation becomes larger if we take e^{E} as S_{R} . A survey of published decay schemes of short-lived FPs (typically refer to the Tables of Isotopes 22) leads to an observation that beta-intensity is not given above 3 - 5 MeV for most high-Q $_{\mbox{\scriptsize B}}$ nuclides. By combining this observation with the above result from the simple strength-function calculation, we come to a conclusion that the value of $\overline{\mathbb{E}}_{\gamma}$ is open to underestimation by 10 - 30 % for nuclides with \mathbb{Q}_{β} -values larger than 5 - 6 MeV. On the contrary the \overline{E}_{γ} and \overline{E}_{β} values calculated with the gross theory reflect properly the effect of the large beta-strength at high energy, which increases \overline{E}_{γ} and decreases \overline{E}_{β} . This is the reason why the introduction of gross theory values drastically improved the reproducibility of the measured beta- and gamma-ray components of the decay heat at short cooling-times.

5. Concluding Remarks

The method of theoretical estimation of the average energies \overline{E}_β and \overline{E}_γ was described in detail. It is a notable feature of the JNDC FP Decay Data File that these estimated values are fully adopted for short-lived FPs with high Q_β -values (Q_β \geq 5 MeV) in place of the values derived from the published decay schemes. Discussions were made in favor of this preferential selection of the theoretical values. In the course of the discussions the following things were known.

- Note 3) Several authors assumed a level-density-proportional behavior for the beta-strength function. Roughly speaking, this assumption corresponds to taking the α value as 0.5 0.9 in the expression $S_{\beta} \stackrel{\sim}{=} e^{E/\alpha}$. This selection, however, leads to serious overestimation of $\overline{E}_{\gamma}/Q_{\beta}$ ratio (larger than 0.4). Further, this ratio increases too rapidly as a function of Q_{β} . From this respect, the level-density proportional assumption is not acceptable.
- Note 4) Here consideration was made only for \overline{E}_{γ} . It is easy to see, however, \overline{E}_{β} is overestimated when \overline{E}_{γ} is underestimated, for they are closely related by the energy conservation.

- 1) The beta-strength function increases with the excitation energy of the final state. In calculations of \overline{E}_{β} , \overline{E}_{γ} and $t_{1/2}$, the effect of this increasing trend of S_{β} is cancelled out to a large extent by the presence of the Fermi-function which decreases rapidly with the energy. In order to calculate the average energies \overline{E}_{β} and \overline{E}_{γ} accurately, however, it is quite important to take the effect of the increasing strength into account.
- 2) Published decay schemes of high Q_{β} -value nuclides are usually constructed on the basis of the intensity balance of gamma-ray spectra. Generally speaking, there exist quite many types of gamma-rays emitted at the time of beta-decay of a high- Q_{β} nuclide because the structure of the high energy final levels is complex and dense. A sizable portion of these gamma-rays remain undetected due to weakness of their intensity. It also happens that some gamma-rays are not placed in appropriate positions in the decay scheme although they are detected. These lead to missing of high energy levels, in other words, to missing of beta-strength at high energy. This is the reason why \overline{E}_{β} is overestimated and \overline{E}_{γ} is underestimated when they are derived from decay schemes.
- 3) Full adoption of the theoretical values of \overline{E}_{β} and \overline{E}_{γ} drastically improved the agreement between calculation and measurement for both beta-and gamma-ray components of decay heat at short cooling-times. This fact indicates that the gross theory predicts reasonably well the energy behavior of the beta-strength function on an average over some range of nuclides.

Acknowledgments

The author expresses deep thanks to Profs. R. Nakasima and M. Yamada for their valuable comments, and to Dr. Z. Matumoto for critical reading of the manuscript. He is much indebted also to Drs. M. Akiyama, K. Tasaka and Mr. H. Ihara.

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TABLE I Average beta- and gamma-ray energies from short-lived FPs (Parameter Q_{00} determined to reproduce the experimental values) [Upper = experimental (Ref. 4); lower.= calculated]

A	z	Element	Even-Odd	Beta-Particle Energy (MeV)	Gamma-Ray Energy (MeV)	Q00	Q Value (MeV)
76	31	Ga	0~0	1.675 1.684	2.808 2.794	2.0	6.610
80	33	As	0-0	2.468 2.471	0.55 4 0.578	0.2	5.999
82	33	As	0~0	3.137 2.952	0.336 0.760	0.0	7.146
86	35	Br	0-0	1.765 1.783	3.296 3.266	2.5	7.296
87	35	Br	о-е	2.087 2.076	1.727 1.737	1.3	6.362
89	36	Kr	e-o	1.231 1.215	2.072 2.109	1.9	4.971
90	37	Rb	0-0	1.789 1.803	2.559 2.550	1.7	6.624
91	36	Kr	e-0	2.000 2.030	0.748 0.764	0.4	5.298
91	37	Rb	o-e	1.320 1.299	2.871 2.804	2.5	5.844
92	36	Kr	e-e	2.700 2.601	0.751 0.927	0.0	6.615
92	37	Rb	0-0	3.714 3.127	0.260 1.467	0.0	8.216
93	38	Sr	e-o	0.784 0.795	2.135 2.075	2.0	4.054
95	39	Y	о-е	1.713 1.732	0.523 0.527	0.3	4.464
97	39	Y	o~e	1.612ª 2.075	0.935 1.501	1.0	6.135
100	41	Nb ^m	0-0	2.023 2.035	1.942 1.978	1.0	6.538
116	47	Ag	0-0	2.185 2.222	0.710 0.7 44	0.0	5.710
132	51	Sb	0-0	1.664 1.698	2.006 2.007	0.9	5.922
134	51	Sb	o -o	2.879 2.802	2.026 2.295	0.0	8,482
136	53	1	0-0	1.808 1.839	1.911 1.920	0.7	6.137

^{*}The ENDF/B-IV file gives 2.162 MeV.

NUCLIDE EBETA E-GAMMA Q-VALUE HALF-LIFE NUCLIDE E-BETA (MEV)	Table	II e	Average	β- and Υ-	y-ray Energies for	t _{1/2} -known	Nuclides	s (Gross	Theory)	
J 68M 0.197 0.956 1.414 225.000 BR 88 2.454 3.210 46.000 RB 88 1.193 2.494 5 2.494 5 2.404 2.404 5 2.400 2.480 2.452 0.494 5 2.404 5 2.404 5 2.404 5 2.404 2.404 5 2.400 2.480 2.400 2.481 3.210 8 8 2.126 3.210 3 2.404 3.210 3	UCL ID	-BET (MEV	-GAMM.	-VALU	ALF-LIF (SEC)	UCLID	-BET (MEV	-GAMM (MEV)		HALF-LIFE (SEC)
J. 70M 1.650 2.167 6.310 46.000 RB 88 1.193 2.494 8 J. 70 2.697 6.279 6.770 4.500 SE 89 3.126 1.894 8 J. 70 2.687 6.720 4.500 BR 89 2.3126 1.894 8 J. 70 2.798 6.770 10.200 BR 89 2.3126 1.894 8 J. 70 2.748 6.770 27.100 BR 90 1.544 2.632 1.662 1.660 8 9 1.544 2.642 1.660 8 9 1.544 2.642 1.660 8 9 1.546 2.642 1.660 8 9 1.544 2.642 1.660 8 9 1.546 2.646 6 2.666 6 2.666 6 2.666 6 2.666 6 2.666 6 2.666 6 2.666 2.666 6 2.666 6	J 68	.19	. 95	. 41	25.00	ص ص	. 45	. 21	. 60	6.30
1 2.697 0.295 6.170 4.500 SE 89 3.126 1.894 8 4 76 1.288 5.401 6.5000 SE 89 3.126 1.623 8 4 76 1.128 8.401 5.620 9 2.047 2.621 10 4 76 1.249 6.770 2.7100 RB 90 1.571 2.759 6 2.042 3.046 2.048 3.046 2.048 3.040 3.089 3.042 </td <td>J 70</td> <td>.65</td> <td>.16</td> <td>.31</td> <td>46.00</td> <td>80</td> <td>.19</td> <td>67.</td> <td>.30</td> <td>00</td>	J 70	.65	.16	.31	46.00	80	.19	67.	.30	00
7 7 1.288 7.4.01 5.400 495.000 BR 89 2.373 2.728 8 8 7 5 2.143 0.870 5.620 10.200 BR 90 3.084 2.633 7 8 7 6 1.746 2.496 6.770 27.100 BR 90 1.571 2.535 7 8 7 7 2.0435 1.171 6.910 1.400 RB 90 1.571 2.759 6 8 7 7 2.0535 1.072 6.010 1.600 RB 90 1.571 2.759 6 8 7 7 2.0536 1.030 RB 90 1.571 2.759 6 8 7 7 2.0538 1.000 RB 91 3.417 2.156 1.017 8 8 2.016 2.161 8.140 5.090 RR 91 3.417 2.156 1.017 8 8 2.016 2.161 8.140 5.090 RR 92 4.000 3.105 1.017 8.000 1.017 8.000 1.017 8.000 1.017 8.000 1.017	7 (69.	.29	.17	.50	ω	1.12	.89	.63	0 41
75 2.143 0.870 5.620 10.200 SE 90 2.904 2.633 77 47 4 76 1.398 0.754 3.780 2.700 RB 900 1.574 2.652 10 4 7 7 2.645 1.71 6.910 1.400 RB 900 1.574 2.656 6 6 6 6 6 6 6 6 6 6 6 6 6 6 6 6 6 6	7	.28	(†	07	95.00	م ھ	.37	1	70.	38
1,398 0.754 3,980 5.700 BR 90 3.089 3.662 10 4 76 1.746 2.740 27.100 RB 90 1.571 2.759 6 4 77 2.653 1.711 6.710 1.400 RB 90 1.541 2.759 6 4 78 2.258 1.032 6.010 1.600 RR 91 3.126 1.213 9 4 79 2.013 8.660 1.000 RR 91 1.417 2.139 9 4 79 2.013 8.660 1.000 RR 91 1.475 2.139 9 4 80 2.014 8.660 1.000 RR 91 1.475 2.139 1.2 4 80 2.015 8.700 RR 92 4.006 3.199 1.2 5 80 2.472 8.700 RR 92 4.006 3.199 1.2 8 80 2.423 1.250 1.250 RR 93 2.425 1.575 8 8 80 2.425	^	.14	87	-62	0.20	9	.90	.63	.47	9
A 76 1.746 2.496 6 770 27.100 RB 90M 1.571 2.759 6 A 77 2.635 1.171 6.910 1.400 RB 90M 1.544 2.666 6 A 78 2.258 1.032 6.010 1.600 RR 91 3.712 2.136 9 A 78 2.258 1.032 6.010 1.600 RR 91 2.055 1.617 6 A 78 2.901 2.140 3.000 RR 91 2.055 1.617 6 A 80 3.016 2.917 8.660 1.000 RR 92 2.262 1.078 5 A 80 3.122 3.548 9.900 1.660 KR 92 2.262 1.078 5 A 80 3.122 3.548 9.900 1.660 KR 92 2.262 1.078 5 A 80 3.122 3.548 9.900 1.660 KR 92 2.262 1.078 6 A 80 3.122 3.548 <td>7</td> <td>39</td> <td>7.5</td> <td>.98</td> <td>5.70</td> <td>ο.</td> <td>.08</td> <td>.66</td> <td>0.33</td> <td>92</td>	7	39	7.5	.98	5.70	ο.	.08	.66	0.33	92
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A 80 3.122 3.548 9.900 1.660 KR 92 2.262 1.078 6 S 80 0.815 0.620 2.630 24.500 KR 93 2.727 2.757 8 S 80 2.479 0.259 5.700 16.500 KR 93 2.727 2.757 8 A 81 2.726 1.187 7.230 10.100 KR 94 2.947 1.480 7.675 10.600 KR 94 2.947 1.480 7.655 10.650 10.600 KR 94 2.947 1.480 10.655 10.650 10.660 KR 94 2.947 1.480 10.655 10.650 10.650 10.650 10.650 10.650 10.655 <td>A 7</td> <td>.61</td> <td>• 06</td> <td>.76</td> <td>00.</td> <td>٥-</td> <td>00.</td> <td>.19</td> <td>2.01</td> <td>0.36</td>	A 7	.61	• 06	.76	00.	٥-	00.	.19	2.01	0.36
E 80 0.815 0.620 2.630 24.500 RB 92 2.856 1.566 7 S 80 2.479 0.259 5.700 16.500 RB 93 2.727 2.757 8 B 81 2.726 4.131 12.300 10.100 RB 93 2.727 2.757 8 B 82 3.796 4.131 12.300 0.600 RB 94 2.994 3.655 10 E 82 1.449 0.765 4.400 4.600 RB 94 2.994 3.655 10 S 82 1.449 0.765 4.400 4.600 RB 94 2.994 3.655 10 S 82 1.449 0.765 4.400 21.000 RB 95 3.102 1.887 8 S 82 1.954 2.763 7.400 1.900 SR 95 3.102 1.887 8 S 83 2.689 2.444 7.400 1.900 SR 96 1.962 0.959 S 83 2.689 2.444 7.400 1.900 SR 96 1.962 0.959 S 83 2.689 2.444 7.400 1.900 SR 96 1.962 0.959 S 84 2.546 6.700 1.900 S.800 Y 97 2.472 1.231 6 S 85 2.836 5.100 2.900 PR 8 3.711 2.923 10 S 86 3.317 3.778 10.180 0.900 Y 98 3.216 2.041 8 S 86 1.350 1.964 5.100 16.700 Y 98 3.216 2.041 8 S 87 2.079 2.444 7.200 5.600 PR 8 9 3.644 2.656 10 S 88 3.317 3.778 10.410 5.500 PR 8 9 3.041 2.106 8 S 88 3.317 3.778 10.410 5.600 PR 8 9 3.041 2.106 8 S 88 3.317 3.778 10.410 6.500 PR 8 9 3.041 2.107 8 S 88 3.317 3.778 10.410 6.500 PR 8 9 3.041 2.107 5 S 88 3.317 3.778 10.410 6.500 PR 8 9 3.041 2.107 5 S 88 3.404 1.716 7.000 PR 8 3.216 2.106 BR 8 3.216 2.	Α 38	. 12	. 54	06.	1.66	8	.26	.07	6.08	8.5
S 80 2.479 0.259 5.700 16.500 KR 93 2.727 2.757 B A 81 2.784 1.187 7.230 1.230 RB 93 2.147 2.675 7 E 81 2.724 1.187 7.230 10.100 RB 93 2.147 2.675 7 E 82 3.796 4.131 12.300 4.600 RB 94 2.994 3.655 10 S 82 1.990 2.954 7.400 4.600 RB 94 2.994 3.655 10 S 82 1.990 2.954 7.400 4.600 RB 95 3.055 3.355 10 S 82 1.990 2.954 7.400 13.000 SR 95 1.992 2.442 6 S 82 2.000 0.900 1.900 SR 95 1.962 0.959 2.442 6 S 83 2.689 2.444 7.400 1.200 Y Y 9 1.501 1.231 1.231 1.231 <td>ш 83</td> <td>.81</td> <td>. 62</td> <td>-63</td> <td>4.50</td> <td>9</td> <td>.85</td> <td>.56</td> <td>.77</td> <td>.50</td>	ш 83	.81	. 62	-63	4.50	9	.85	.56	.77	.50
A 81 2.784 1.187 7.230 1.230 RB 93 2.147 2.675 7 E 81 2.126 0.881 5.600 10.100 KR 94 2.947 1.480 7 A 82 3.796 4.400 4.600 KR 94 2.994 3.655 10 E 82 1.449 0.765 4.400 4.600 KR 95 3.055 3.355 10 S 82 1.954 2.763 4.400 4.600 RB 95 3.102 1.887 8 S 82 1.954 7.400 13.000 SR 95 3.102 1.887 8 S 83 2.689 2.444 7.400 1.900 SR 95 1.593 2.442 A 83 3.881 3.745 14.100 SR 96 3.821 3.042 10 B 84 2.546 2.400 0.993 5.314 14.100 SR 97 2.472 1.231 6 S 84 2.546 2.760 4.700	so ex	25.	.25	.70	6.50	٥ د	.72	.75	.70	. 28
E 81 2.126 0.881 5.600 10.100 KR 94 2.947 1.480 7 0.600 RB 94 2.994 3.655 10 0.600 KR 95 3.796 4.131 12.300 0.600 KR 95 3.055 3.355 10 0.600 KR 95 3.055 3.355 10 0.600 KR 95 3.055 3.355 10 0.600 L4.600 KR 95 3.055 3.355 10 0.600 C.954 7.400 21.000 SR 95 3.102 1.887 8 3.82M 1.954 2.743 11.000 0.310 SR 96 3.821 3.042 6 83 2.444 7.400 1.900 SR 96 1.962 0.959 5 83 2.000 0.993 5.314 14.100 SR 96 1.962 0.959 5 83 2.000 0.993 5.314 14.100 SR 96 1.962 0.959 5 88 2.000 0.993 5.314 14.100 SR 97 2.472 1.231 6 2.84 2.854 3.405 9.780 5.800 Y 97 2.472 1.231 6 2.85 3.005 9.100 2.080 KB 98 3.711 2.923 10 2.88 3.317 3.778 10.180 0.900 Y 98 3.216 2.051 9.051 5 88 3.317 3.778 10.180 0.900 Y 98 3.216 2.051 9.051 5 88 3.440 3.473 10.410 0.730 SR 99 3.041 2.1051 5 88 3.440 3.473 10.410 0.730 SF 99 3.041 2.105	Α Ω	. 78	.18	. 23	1.23	9	. 14	.67	.45	.82
A 82 3.796 4.131 12.300 0.600 RB 94 2.994 3.655 10 E 82 1.449 0.765 4.400 4.600 KR 95 3.055 3.355 10 S 82 1.990 2.954 7.400 21.000 SR 95 1.593 2.442 6 S 82 3.881 3.743 11.000 0.310 SR 96 1.962 0.959 5 S 83 2.689 2.444 7.400 1.200 Y 97 2.472 1.231 7 E 84 2.546 2.460 6.700 1.200 Y 97 2.472 1.231 7 S 84 2.346 5.314 14.100 SR 94 2.472 1.231 7 2.472 1.231 7 S 84 2.346 5.310 5.800 Y 97 2.472 1.231 7 2 2.472 1.231 2 2.472 1.231 2 2 2.833 1.472 <td>ш œ</td> <td>.12</td> <td>.88</td> <td>9.</td> <td>0.10</td> <td>o. ∝</td> <td>76.</td> <td>. 48</td> <td>.50</td> <td>.20</td>	ш œ	.12	.88	9.	0.10	o. ∝	76.	. 48	.50	.20
E 82 1.449 0.765 4.400 4.600 KR 95 3.055 3.355 10 S 82 1.990 2.954 7.400 21.000 SR 95 3.102 1.887 8 S 82 1.990 2.954 7.400 13.000 SR 95 3.102 1.887 8 S 83 3.881 3.743 11.000 0.310 SR 96 1.962 0.959 5 S 83 2.689 2.444 7.400 1.900 SR 96 1.962 0.959 5 S 84 2.860 6.700 1.200 Y 97 2.472 1.231 6 S 84 2.834 3.465 6.700 1.200 Y 97 2.472 1.231 6 S 85 2.834 3.405 9.780 5.800 Y 97M 2.683 1.472 7 S 86 3.317 3.778 10.180 0.900 Y 98 3.216 2.041 8 S 86 3.317 3.778 10.180 0.900 Y 98 3.216 2.041 8 S 86 1.964 5.100 16.700 RB 99 3.664 2.656 10 S 87 3.440 3.473 10.410 0.730 SR 99 3.041 2.106 8 S 88 2.404 1.716 7.200 55.600 NB100N 1.564 2.831 6 E 88 2.404 1.716 7.000 1.530 SR 99 2.375 1.147 6 E 88 2.404 1.716 7.000 1.530 SR 99 2.375 1.167 5	8	62.	. 13	.30	9.	9 9	66.	. 65	0.14	.76
S 82 1.990 2.954 7.400 21.000 RB 95 3.102 1.887 B 8	ω ω	77.	. 76	07.	09.7	o a	.05	.35	0.00	7.8
S 82M 1.954 2.763 7.400 13.000 SR 95 1.593 2.442 6 A 83 3.881 3.743 11.000 0.310 RB 96 3.821 3.084 10 E 83 2.689 2.444 7.400 1.900 SR 96 1.962 0.959 5 S 83 2.089 0.993 5.314 14.100 SR 97 2.603 1.501 7 E 84 2.546 2.460 6.700 1.200 Y 97 2.472 1.231 6 S 84 2.834 3.405 9.780 5.800 Y 97M 2.683 1.472 7 S 85 2.836 3.005 9.100 2.080 RB 98 3.711 2.923 10 E 85 1.630 2.388 6.100 32.800 Y 98 3.216 2.041 8 E 86 1.350 1.964 5.100 16.700 Y 98 3.216 2.041 8 E 86 1.350 1.964 5.100 16.700 Y 98 3.216 2.050 9 E 86 3.317 3.778 10.410 0.730 SR 99 3.041 2.106 8 E 87 2.079 2.644 7.270 5.600 NB100N 1.564 2.831 6 E 88 2.404 1.716 7.000 1.530 2.810 2.950 7.000 1.991 5	S 82	66.	.95	.40	1.00	В	.10	.88	. 59	.38
A 83 3.881 3.743 11.000 0.310 RB 96 3.821 3.084 10 E 83 2.689 2.444 7.400 1.900 SR 96 1.962 0.959 5 S 83 2.089 2.444 7.400 1.900 SR 96 1.962 0.959 5 S 83 2.000 0.993 5.314 14.100 S 8 97 2.603 1.501 7 E 84 2.546 2.460 6.700 1.200	S 82	.95	.76	7 t C	3.00	٥ س	59	77.	.09	07.
E 83 2.689 2.444 7.400 1.900 SR 96 1.962 0.959 5 SR 97 2.000 0.993 5.314 14.100 SR 97 2.603 1.501 7 7 2.000 0.993 5.314 14.100 SR 97 2.603 1.501 7 7 2.000 0.993 5.314 14.100 Y 97 2.472 1.231 6 1.200 Y 97 2.460 6.700 1.200 Y 97 2.472 1.231 6 1.200 SR 98 3.711 2.923 10 1.472 7 1.200 SR 98 3.711 2.923 10 1.472 1.200 SR 98 3.711 2.923 10 1.051 5 1.051	A 8	.88	7.4	1.00	.31	В	82	.08	0.30	0.20
S 83 2.000 0.993 5.314 14.100 SR 97 2.603 1.501 7 7 2.546 2.460 6.700 1.200 Y 97 2.472 1.231 6 1.200 Y 97 2.472 1.231 6 1.200 Y 97 2.472 1.231 6 1.200 Y 97 2.450 1.472 7 2.834 3.405 9.780 5.800 Y 97M 2.683 1.472 7 2.836 3.005 9.100 32.800 SR 98 3.711 2.923 10 1.850 1.350 1.964 5.100 16.700 Y 98 3.216 2.041 8 1.350 1.964 5.100 16.700 Y 98M 2.989 2.596 9 1.864 2.656 10 1.947 2.936 7.300 55.700 RB 99 3.664 2.656 10 1.947 2.079 2.644 7.270 5.600 W 1.564 2.831 6 1.813 2.410 6.500 55.600 N 1.564 2.831 6 1.091 5 1.091 5	ш	. 68	77	77.	1.90	٥ د	96.	.95	.36	.01
E 84 2.546 2.460 6.700 1.200 Y 97 2.472 1.231 6 S 84 2.834 3.405 9.780 5.800 Y 97M 2.683 1.472 7 S 85 2.836 3.005 9.100 2.080 RB 98 3.711 2.923 10 E 85 1.630 2.388 6.100 32.800 Y 98 3.711 2.923 10 S 86 3.317 3.778 10.180 0.900 Y 98 3.216 2.041 B E 86 1.350 1.964 5.100 16.700 Y 98 3.216 2.041 B E 86 1.947 2.936 7.300 55.700 RB 99 3.664 2.656 10 S 87 3.440 3.473 10.410 0.730 SR 99 3.041 2.106 B E 87 2.079 2.644 7.270 5.600 NB100N 1.564 2.831 6 E 88 2.404 1.716 7.000 1.530 ZR101 2.160 1.091 5	S S	00.	66	.31	4.10	o œ	.60	.50	.20	77.
S 84 2.834 3.405 9.780 5.800 Y 97M 2.683 1.472 7 2.834 2.835 3.005 9.100 2.080 RB 98 3.711 2.923 10 2.835 2.836 3.005 9.100 32.800 SR 98 2.139 1.051 5 5 8 8 3.317 3.778 10.180 0.900 Y 98 3.216 2.041 8 E 86 1.350 1.964 5.100 16.700 Y 98M 2.989 2.596 9 R 86 1.947 2.936 7.300 55.700 RB 99 3.664 2.656 10 S 8 7 3.440 3.473 10.410 0.730 SR 99 3.041 2.106 8 E 87 2.079 2.644 7.270 5.600 WB100N 1.564 2.831 6 E 88 2.404 1.716 7.000 1.530 2.8101 2.160 1.091 5	ω	. 54	46	.70	. 20	<u></u>	.47	. 23	.67	.70
S 85 2.836 3.005 9.100 2.080 RB 98 3.711 2.923 10 E 85 1.630 2.388 6.100 32.800 SR 98 2.139 1.051 5 S 86 3.317 3.778 10.180 0.900 Y 98 3.216 2.041 8 E 86 1.350 1.964 5.100 16.700 Y 98M 2.989 2.596 9 R 86 1.947 2.936 7.300 55.700 RB 99 3.664 2.656 10 S 87 3.440 3.473 10.410 0.730 SR 99 3.041 2.106 B E 87 2.079 2.644 7.270 5.600 Y 99 2.375 1.147 6 R 87 1.813 2.410 6.500 55.600 NB100N 1.564 2.831 6 E 88 2.404 1.716 7.000 1.530 2.8101 2.160 1.091 5	s S	.83	07.	.78	.80	26	.68	27.	.17	.13
E 85 1.630 2.388 6.100 32.800 SR 98 2.139 1.051 5 S 86 3.317 3.778 10.180 0.900 Y 98 3.216 2.041 8 E 86 1.350 1.964 5.100 16.700 Y 98M 2.989 2.596 9 R 86 1.947 2.936 7.300 55.700 RB 99 3.664 2.656 10 S 87 3.440 3.473 10.410 0.730 SR 99 3.041 2.106 8 E 87 2.079 2.644 7.270 5.600 Y 99 2.375 1.147 6 R 87 1.813 2.410 6.500 55.600 NB100N 1.564 2.831 6 E 88 2.404 1.716 7.000 1.530 ZR101 2.160 1.091 5	S S	.83	00.	. 10	2.08	В	.71	.92	0.85	.10
S 86 3.317 3.778 10.180 0.900 Y 98 3.216 2.041 8 E 86 1.350 1.964 5.100 16.700 Y 98M 2.989 2.596 9 R 86 1.947 2.936 7.300 55.700 RB 99 3.664 2.656 10 S 87 3.440 3.473 10.410 0.730 SR 99 2.375 1.147 6 R 87 1.813 2.410 6.500 55.600 NB100N 1.564 2.831 6 E 88 2.404 1.716 7.000 1.530 ZR101 2.160 1.091 5	m ee	. 63	.38	.10	2.80	٥ ٢	.13	.05	5.81	.66
E 86 1.350 1.964 5.100 16.700 Y 98M 2.989 2.596 9 R 86 1.947 2.936 7.300 55.700 RB 99 3.664 2.656 10 S 87 3.440 3.473 10.410 0.730 SR 99 3.041 2.106 B 8 E 87 2.079 2.644 7.270 5.600 Y 99 2.375 1.147 6 R 87 1.813 2.410 6.500 55.600 NB100N 1.564 2.831 6 E 88 2.404 1.716 7.000 1.530 ZR101 2.160 1.091 5	S	.31	.77	0.18	06.	٥	.21	.04	.98	.65
R 86 1.947 2.936 7.300 55.700 RB 99 3.664 2.656 10 S 87 3.440 3.473 10.410 0.730 SR 99 3.041 2.106 B E 87 2.079 2.644 7.270 5.600 Y 99 2.375 1.147 6 R 87 1.813 2.410 6.500 55.600 NB100N 1.564 2.831 6 E 88 2.404 1.716 7.000 1.530 2R101 2.160 1.091 5	m &	.35	96.	7,	6.70	98	.98	.59	0.8	00.
S 87 3.440 3.473 10.410 0.730 SR 99 3.041 2.106 8 E 87 2.079 2.644 7.270 5.600 Y 99 2.375 1.147 6 R 87 1.813 2.410 6.500 55.600 NB100N 1.564 2.831 6 E 88 2.404 1.716 7.000 1.530 ZR101 2.160 1.091 5	∞ ∞	76.	.93	ĕ.	5.70	В	99.	.65	00.0	.06
E 87 2.079 2.644 7.270 5.600 Y 99 2.375 1.147 6 R 87 1.813 2.410 6.500 55.600 NB100N 1.564 2.831 6 E 88 2.404 1.716 7.000 1.530 ZR101 2.160 1.091 5	S S	77-	47	. 4.	. 7.3	ه ۳	70	.10	00.	.60
E 88 2.404 1.716 7.000 1.530 ZR101 2.160 1.091 5	m eo	-07	79.	.27	5.60	66	.37	.14	.39	07.
E 88 2.404 1.716 7.000 1.530 2R101 2.160 1.091 5	eo ≃∶	8	. 41	.50	5.60	B100	. 56	.83	.43	00.
	ED	7,	.71	ĕ	.5	R 10	.16	8	.90	07.

HALF-LIFE 10.400 1.700 3.100 3.760 2.000 0.480 1.500 0.390 5.000 3.210 2.400 2.320 2.100 1.300 3.760 0.940 0.840 5.600 0.990 2.500 0.576 0.270 168.000 1.470 1.040 0.850 (SEC) E-GAMMA Q-VALUE (MEV) 6.590 7.000 5.500 6.615 6.059 7.350 5.700 4.000 7.000 2.298 9.170 .140 1.455 5.632 8.060 8.210 6.486 9.310 9.390 ,322 .410 007.6 .132 5.050 7.2406.0708.400 11.043 11.359 11.087 11.087 11.087 11.087 11.089 11 2.256 3.272 1.790 2.620 2.605 E-BETA (MEV) 2.284 2.480 1.532 2.953 2.313 2.234 2.245 2.245 2.364 2.364 2.364 2.364 3.366 2.410 2.295 2.781 NUCLIDE IN132 SB132 SN133 SN134 SB134 SB134 AG116M PD117 PD117 PD117 PD118 AG118 AG122 IN122 IN122 IN122 IN125 IN126 IN126 IN126 IN127 CD128 IN127 IN127 IN127 IN127 IN127 IN127 IN128 IN127 IN128 IN127 HALF-LIFE 1.000 0.800 4.800 1092.000 3.000 1.000 3.500 3.500 5.000 1.400 15.900 3.000 28.500 3.000 63.000 4.650 (SEC) E-GAMMA Q-VALUE (MEV) 8.800 2.200 5.620 6.940 5.400 3.3400 6.300 6.200 4.200 8.000 8.000 7.200 7.200 5.200 4.300 2.500 5.600 7.200 6.700 5.200 8.300 4.570 8.850 5.450 (cont'd) (MEV) 1.134 0.894 2.134 3.376 0.585 2.678 2.365 2.549 0.746 2.933 1.393 0.986 2.993 1.099 2.170 0.486 1.461 1.461 0.982 0.725 .156 .416 0.962 E-BETA (MEV) 1.686 3.096 1.250 2.832 2.832 1.144 3.125 2.510 0.623 1.244 2.499 1.244 1.244 1.232 1.232 1.232 1.682 2.144 2.317 2.249 2.144 1.682 2.249 2.263 1.444 1.682 657-1.114 2.477 2.249 1.733 2.742 1.435 0.662 2.967 2.111 ___ Table NUCLIDE NB103 M0103 2R104 NB104 M0104 1C104 NB105 M0105 M0105 TC106 MO107 TC107 TC108 TC108 TC108 RV110 RV111 RV1111 RV1112 RV1112 NB101 Y 102 ZR102 NB102 NB102M RH113 RH114 PD115 PD116 AG116

Table	le II	(cont'd)							
NUCLIDE	E-BETA (MEV)	E-GAMMA (MEV)	Q-VALUE (MEV)	HALF-LIFE (SEC)	NUCLIDE	E-BETA (MEV)	E-GAMMA (MEV)	Q-VALUE (MEV)	HALF-LIFE (SEC)
I 136	.76	76.	.00	85.100	CE151	77.	.87	.76	.02
M	.76	76.	.01	4.80	S	. 23	.70	.50	00
M	.17	.60	7.	.80	PM152N	1.054	6		1080.000
13	.27	94.	ς,		S	.51	. 58	00.	000.07
E 13	76	.06	κ,	1.40					
S 13	.08	.68	W)	00.					
\$13	. 28	.73	7.	4.00					
13	.05	.32	۰.	3.8	[cl] (o+oM	f. livos ai	you in thi	se oldet a	
E13	00.	.23	٥.	.50		is cavil-i	nali-lives given in this table	א נמטופ מרפ	e medsured
1 4	.76	.32	٥.	.60	val	values. The	The key parame	parameter Qon was	s searched
\$14	.42	.79	٦,	7.0	for	for and fived co		on that the amore	though the
14	- 42	.77	7	77	101	מווח וואבר		נר חוב אוחס	
E14	.04	. 48	۲.	.73	tion	ıı should∙r	eproduce t	hese half-	should reproduce these half-lives in the
S14	. 27	.13	7	9.	4	the second	أعياطينياطيا	hoot was for individual modified	1000: +00+)
E 1 4	.75	-97	0.	- 24	מטח	t way lui	illa i V sada i	Hactides	(אבב ובעו)
S14	77.	.78	۲,	71	Ave	Average energies were	jies were c	alculated	calculated on the basis
£14	.22	.72	٠,	.30	4.0	these A	values		
S143	. 93	. 21	۰,	. 78	5	or cuese 400 values			
€14	, W.	17.	۵.	.80					
E 14	. 60	.92	٠,	.15					
\$14	.64	.19	Ξ,	00.					
A14	76.	.70	٥.	.85					
A 14	33	60.	Š	.10					
XE145	2.291	1.827	6.300	0.900					
514	0.	. 58	τ.	ω.					
A 1 4	7.5	. 15	₹.	3.79					
A14	. 45	.80	~	30					
S 1 4	. 63	. 19	Ÿ	4.1 1.4					
A14	.15	.77	٥.	. 18					
A14	.18	.34	٠,	.50					
\$14	. 21	. 58	۶.	. 21					
A14	.85	.30	s.	.70					
A14	.63	.93	•						
A14	.34	.83	٥.	۷,					
A14	17	.36	7.050	.29					
R15	0.	, 0.7	۲.	۲,					

Average 8-and Y-ray Energies for tyg-unknown Nuclides (Gross Theory) Table III

NUCLIDE	E-BETA (MEV)	Е-GАММА (МЕV)	Q-VALUE (MEV)	HALF-LIFE* (SEC)	NUCLIDE	E-BETA (MEV)	E-GAMM/	A Q-VALUE (MEV)	HALF-LIFE (SEC)
CR 66	3.863	69.	.87	.26	7 0	.16	.42	. 22	.08
۸ د	.73	.64	.58	.17	I 7	.68	. 19	7.02	43
E 6	.26	.04	.03	.66	7 1	5.	.20	69.	98
0 6	.90	.37	.65	.78	7 0	. 25	.74	4.73	0.6
R 6	.93	.13	. 45	.11	1 7	82	.21	34	7.5
∨	53	. 45	.97	21	7 0	. 68	60	6.93	9.5
E 6	.70	85	.73	.70	7	13	7.1	3,45	70
0 6	0.5	1.249	7.828	2,286	CO 76	5.866	6.371	18.570	0.036
R 6	.39	.00	.25	.13	I 7	.37	. 52	8.75	43
N 0	.07	.05	5.65	.10	7 0	.11	. 50	0.20	. 57
e V	. 72	.21	7.13	.46	7 I	.48	.08	. 52	15
9 0	.68	.80	.65	.73	7 0	. 26	.50	8.51	. 26
1 6	.66	. 58	2.25	.10	7 I	.92	.87	0.20	19
2 2	.98	.07	67.	.10	7 0	83	.05	.18	7 6
E 6	70.	.23	62.0	.38	7 0	7.0	26.	9.85	5 4
0	. 56	.61	.20	.90	188	.30	96.	4.05	0.3
9 I	32	. 93	4.05	. 29	3	.32	α	.71	2.
ж 	0.8	. 53	. 15	.05	83	.75	.24	7.22	. 12
≻ ι Ζ ι	77.	. 56	6.91	90.	ອ ດ	.82	.45	3.58	.09
, '	. 32	.46	8.56	. 53	eo Z	.03	.71	1.25	.26
· 0	, 15	. 20	.98	.34	В В	.98	.53	5.99	.02
<u> </u>	- 24	.71	3.60	. 23	U 8	.68	.06	4.91	12
~	. 57	.91	. 52	.05	S Ω	23	. 18	.13	12
E 7	07.	. 71	1.97	.20	z ω	.10	.95	2.63	16
\	. 10	. 16	0.83	36	z x	. 62	.29	3.03	.06
- - -	82	. 24	.35	3.20	A 8	. 22	.63	3.57	. 22
7 0	.37	. 63	3.81	.71	A 8	.50	.30	3.81	.09
, , ,	90.	.87	7,46	. 18	E 83	.02	.18	.71	77.
- - -	. 60	69.	4.37	.17	2	.26	.68	4.70	0.3
/ I	83	.91	. 12	. 84	A 88	79.	.17	.95	.12
\ r	.03	66.	7.52	.79	я 8	.36	.63	9.84	28
~ α μ	٥	0,	- 67	0.	щ 83	.53	. 58	1.13	32
\	/1	. 98	2.88	. 13	т 83	00.	00.	.50	11
\	. 28	.61	.65	. 26	S	7.5	. 22	2.21	. 4.1
\ 0	χ. 8	.77	5.20	83	SB	97	76.	2.39	.17
`	`	~	•						

*) Gross theory calculated value

Tab	Table III	(cont'd	£						
NUCLIDE	E-BETA (MEV)	E-GAMMA (MEV)	A Q-VALUE (MEV)	HALF-LIFE (SEC)	NUCLIDE	E-BETA (MEV)	E-GAMMA (MEV)	Q-VALUE (MEV)	HALF-LIFE (SEC)
E 9	. 11	. 14	2.88	.13	B10	. 15	. 26	.10	.70
BR 93	3.554	3.672	11.280	0.298	M0109	2.675	1.876	7,743	1.722
F 9	.18	.30	1.18	10	811	.84	.50	. 71	.60
ر م	.01	.66	3.20	.24	811	.92	.74	.14	.32
Б 9	. 55	64.	4.12	.07	011	. 19	.15	.05	.01
۵ م	. 59	.71	1.40	.27	811	.39	. 56	06.	.43
Б 9	. 61	.61	2.35	.06	011	60.	. 41	. 14	69.
ο. Ο.	7.0	.82	4.27	14	C11	. 48	.50	6.98	8.
٥ م	0.7	. 56	8.20	67	B11	17	. 18	.10	.20
٥- ح	83	66.	1.17	.24	011	5.5	.354	6.97	66.
۰ ح	67	.85	.34	. 25	C11	.34	.790	.01	.98
9	.29	. 53	2.65	.12	011	. 43	.802	0.21	.37
810	76.	. 18	79.0	.13	c11	.73	.822	7.81	. 56
810	.27	.67	3.75	.17	011	.92	.578	7.95	.50
R 10	. 53	. 27	6.83	.19	C11	.57	.257	96.	.57
810	.03	. 12	. 72	.18	011	47	.844	4.26	. 18
R 10	46	99.	0.11	. 42	011	. 59	866.	77	.27
10	69.	.52	0.77	18	C11	66	.16	. 68	.87
R 10	0.1	.57	8.12	.50	U11	.53	.80	.40	.12
810	.36	iu.	7.5	11	H11	0.5	.05	. 60	.60
810	69.	76.	0.86	. 28	011	.17	.73	8.63	.33
10	.03	86.	. 55	00.	C11	69.	67.	7 7 7	77.
R 10	. 45	.46	.87	.30	011	.84	.98	.17	.18
R10	. 43	.85	9.22	.26	C 1 1	.17	.39	.27	.60
70	67.	5	. 26	. 56	011	69.	.02	7.95	. 42
R 10	80.	.38	2.08	.15	C 1 1	.87	.83	.15	.30
10	. 32	.37	2	3.	U11	60.	. 11	8	.30
R 10	99	- 76	7	. 93	H11	60.	64.	23	. 52
10	8 1	ω.	34	.32	U11	. 92	.31	69	85
R 10	. 13	60.	5.85	. 42	H111	27	. 59	.07	.54
10	99.	80	99.	. 29	011	, 11	, 33	.07	.95
R10	φ, 8	. 20	.68	. 92	U12	.36	. 26	.51	.30
B 10	8	8.	96.	. 45	H122	. 26	.83	.91	0.99
<i>S</i> 2′. ∝	. 56	.33	86.9	00.	012	. 34	.81	- 65	.24
B10	82.	.10	82	.64	H12	. 67	.85	73	.57
K10	.58	?	0.00	.42	012	.33	.63	.83	. 16

Tat	Table III	(cont'd)	1)		;				
NUCL IDE	E-BETA (MEV)	E-GAMMA (MEV)	A Q-VALUE (MEV)	HALF-LIFE (SEC)	NUCLIDE	E-BETA (MEV)	E-GAMMA (MEV)	Q-VALUE (MEV)	HALF-LIFE (SEC)
U12	.68	. 45	34	.70	E 1 4	ŗ	*	c	,
RH122	3.370	3.070	10.370	0.758	142	2.695	M 100 M	9.700	7.77
012	. 65	- 92	4.71	.30	E14	6	Ö		. r
H12	06.	.14	67.	.93	E 14	5	7	· -	, 4
D 1 2	67.	.85	.38	.05	514	7	6	7	
U12	90.	.68	37	.36	A14	.0	. 5		; a
H12	67	32	.88	. 56	A14	. 78	30.	. 2	, ,
D12 012	986.	-07	5.5	.77	E 15	80.	7	. 5	. ~
612	60.	. 62	.36	.36	\$15	.75	M	7	
012	70.	60.	.98	.32	A15	.98	0	74	10
612	5.0	.81	. 54	.76	A15	0.	5.4	. ~	, ,
D12	90.	. 34	66.	. 24	A15	.20	9	Υ.	_
D 1 2	. 35	.27	.52	.23	A15	52	. 6		, ,
612	66.	. 43	66.	.03	A 15	K)	80		, 0
612	. вв	. 18	.51	9.	E 15	1.6	, ,	3 - 3 ⊀	77.0
012	.07	00,	67	.10	R15	7.5			0 +
D12	. 76	. 50	58	.57	A 15	5	80	- 0	
612	19	69.	- 67	.67	E 15	89,		, 0	7 . 7
012	30	. 22	7.37	.25	R15	7.0	20.	. 0	
015	89	.21	.60	.10	015	96	62		3 5
613	30	.02	4.24	.11	A 15	. 6	49	. ~) · (
013	. 25	. 22	6.28	7 7 .	A15	. 61	6.7		
013	. 51	. 26	.90	.23	E15	69	9.5	, 0	; o
710	. 40	89	9.30	.20	815	87	4.1	7	ס כ
0 T Z	ۍ	69.	.31	.16	E15	.01	.57	1.0	, w.
7 7 7 7 7 7 7 7 7 7 7 7 7 7 7 7 7 7 7 7	٠ ر	. t	8.16	19	R15	.07	. 4.8) C
7 6	, ,	ري. د د	. 17	.07	015	.36	83	10	,,,
7 F	,	<u></u>	4.57	60.	415	.02	.63	17	0
7 T Z	.61	.42	. 23	.68	E15	4	17		,,,
7 T Z	. 97	.83	.36	.52	315	14	6.8	, 6	1 4
יור מר	``.	, δ	.13	. 21)15	12	7.6		7000
٠. ا	.01	99.	8.27	.34	115	31	8	C	α
0 t ∪	9.0	``	. 24	.81	E 15	7.3	C	7	7 × 1
7 7 7 7 7 7 7 7 7 7 7 7 7 7 7 7 7 7 7 7		.68	60.	.61	3.15	38	83	α,	- α) «
0 T T	. 5.	. 55.	.67	99.	115	66	1.4	0.4	7.90
7 7	??	~	. 52	10	115	4.5	8	5.6	9 9
						ĺ	ł		

Table	le III	(cont'd)							
NUCLIDE	E-BETA (MEV)	E-GAMMA	Q-VALUE (MEV)	HALF-LIFE (SEC)	NUCLIDE	E-BETA (MEV)	E-GAMMA (HFW)	Q-VALUE (MEV)	HALF-LIFE (SEC)
15	0.9	77	30	5 2	16	79	5.9	64	30
. 5	5 5	15	90	9	1,6	08	20	00	0,7
15	58	92	9	8.1	EU166	1.838	2.395	6.680	7.960
1.5	56	16	8	23.27	16	17	80	69	16.07
15	0.7	5.5	7	8,80	16	76	61	66	10
15	77	33	5.4	67	116	33	10	45	32
15	90	66	7	7.	16	02	97	32	3,23
15	78	16	2	9.10	16	2	21	88	67
Α.	12	68	7	12	116	14	7.5	56	8.37
16	93	7.0	2	2	116	77	41	96	65
4	63	7	7	17	116	16	7	72	60
7	10	20	Ö	7	116	52	9	Ω.	5.39
16	96	50	õ	5	316	17	85	72	71.24
16	8	8	ω,	7	16	3.1	5.4	4.8	3.00
7	16	8	œ	õ	116	.27	6	14	9
1	7	8	5	2.8	16	.91	99.	1,	86
Ξ,	2	7	~	3	316	3.5	6.	20	8.82
ĭ	4	/	S	6.3	/16	86	63	8	10
Ã	7	7	ò	9	117	\$9.	3	6	7
7	0	Ö	M	Ň	117	7	ř	~	Ö
Ξ	M	ω	~	8.8)17	.9	극	5	Ö
~	4	Ö	1	4	317	54.	Ξ.	.6	ĭ.
Ę	4	~	ω	0	(17	79.	.6	'n	7.2(
Ξ	M	0	-7	M)17	36.	~	ň.	3.0
Ξ	Ý.	M	2	'n	317	.55	÷.	ŏ.	1.7
Ξ	Ŋ	0	^	16.1	717	2.	6	<u>؞</u>	40.13
$\overline{}$	6	9		M	017	7	š.	4	3.5
7	۲.	Ś	۲.	4	017	7	جَ.	~	ŏ.
Ę	M	6	\sim	Ξ.	817	'n	~	7	6
7	ω,	0	۲,	۷.	71.	ò	۲.	Ň.	Ň.
Ξ	ν.	7	φ.	18.7	01.	ŏ.	ø.	Ó	7.4
2	۲.	۰,	S.	Ý					•
PM165	2.579	2.221	8.041	0.860	Note) Ha	Note) Half-lives a	are not mea	asured for	are not measured for the nuclides
7	٥.	٥.	٧.	۰.		+ 4+	42410	Lalen 12tel	
1	ω.	٠, ۲	•	٥.	91	given in unis cabi	is cante.	calculated	ndii-iives
01	۲,	α,	α,	7.	Y. C.	amalisted-here	here.		
					3	1 1 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2	,		

Average β -, γ -ray Energies and Related Parameters for 88 Nuclides with Experimental Information Table IV

	Q _B		H B	(MeV)	, 10.11		E	(MeV)		% contr. to 235U decay heat	r. to lecay	Calcula	Calculation Parameters	ers
	(меv)	JNDC(T)	JNDC(E)	ENDF/B-IV	ENDF/B-V	JNDC(T)	JNDC(E)	ENDF/B-IV	ENDF/B~V	tc= 20 sec	tc= 100 sec	t _{1/2} :input (sec)	t _{1/2} :calc'd (sec)	Q00 (MeV)
Cu68 ^m	5.341	0.20	0.19	ı	ı	96.0	0.98	l	ı			225	208	2.0
Cu70m	6.310	1.65	1.58	-	ı	2.17	2.93	1	1			46	97	1.7
Cu70	6.170	2.70	2.57	I		0.30	0.58	1	I			4.5	16	0.0
Ga74	5.400	1.29	1.02	1.07	1.99	2.40	3.05	3.04	0.95			495	182	2.0
Ga76	6.770	1.75	1.81	1.68	1.92	2.50	2.79	2.81	2.79			271	272	1.8
As 80	5.700	2.48	2.32	2.52	2.46	0.26	0.61	0.61	0.61			16.5	22.3	0.0
Ge 81	5.600	2.13	2.49	2.06	2.27	0.88	0.12	1.19	0.51			10.1	12.3	0.5
As82 ^m	7.417	1.95	1.86	1.82	1.81	2.76	3,16	2.99	3.10			. 13	12.9	1.9
As 82	=	1.99	3.25	3.21	3.16	2.95	0.48	0.29	0,40			21	13.4	2.0
As 83	5.460	2.00	1.26	1.68	1.83	0.99	2.75	0.98	1.31	0.4	:	14.1	14.5	0.7
As84	9.554	2.83	3.99	3.76	3.41	3.41	1.58	2.10	2.76			5.8	2.1	2.0
Se 85	6.100	1.63	1.70	2.06	2.18	2.39	2.24	1.29	1.40	6.0	6.0	32.8	18.1	2.0
Se86	5.100	1,35	1.15	1.42	1.55	1.96	2.35	1.02	1.07	1.3		16.7	16.1	1.8
Br86	7.300	1.95	1.74	1.78	1.78	2.94	3.64	3.32	3.30	1.1	3.7	55.7	13.9	2.0
Se87	7.270	2.08	2.49	2.50	2.54	2.64	1.96	1.74	1.71	0.5		5.6	5.1	2.0
Br87	6.500	1.81	1.54	2.14	64.7	2.41	3.86	1.73	1.55	1.6	3.4	55.6	11.0	2.0
Se88	7.000	2.40	2.38	2.10	2.39	1.72	1.72	1.63	1.47			15.2	15.3	1.2
Br 88	8,600	2.45	2.62	3.07	2.54	3.21	3.06	1.88	3.00	3.1	9.0	16.3	41.4	2.0
Rb 88	5.309	1.19	2.09	2.08	2.06	2.49	0.64	0.67	99.0			1068	164	2.0
Br90	10.330	3.09	4.39	3,36	3.21	3.66	1.13	2.32	2.62			1.96	1.18	2.0
Rb90m	6.467	1.54	1.29	1.11	1.36	2.67	3.35	3.62	3.10		1.0	258	31.8	2.0
Rb90	6.360	1.57	1.89	1.66	2.20	2.76	2.16	2.66	1.06	0.4	4.6	153	36.3	2.0
Kr91	6.200	2.06	1.99	2.58	1.94	1.62	1,73	0.72	1.73	3.1		8.57	8.48	1.1
Rb91	5.700	1.48	1.52	1.33	1.50	2.30	2.22	2.73	2.26	2.8	7.0	58.2	26.3	2.0
										1				

0.0 2.0 2.0 4.0 9.0 0.0 0.5 0.0 Calculation Parameters /2:calc'd 979.0 2.32 4.54 2.20 1.87 4.17 27.9 24.0 16,1 72.4 31.9 11.7 6.9 3.98 $t_{1/2}$:input (sec) 1.015 0.108 0.65 99.0 1.29 2.00 160.8 10.4 1.5 36.7 28.5 3.0 1092 % contr. to 235U decay 2.5 tc= 100 sec 0.5 heat tc= 20 s ENDF/B-2.48 1.38 4.68 1.53 1.94 1.09 1.88 1.95 2.24 1.49 0.81 1.32 1.40 1.80 ENDF/B-IV 3.53 1.40 1.99 3.16 1.50 1.94 1,65 2.00 2.27 0.75 2.04 1,41 1.36 1.840.94 1.92 (MeV) JNDC(E) 1.68 0.87 1,16 1,33 1.25 0.17 0.49 0.35 1.84 0.150.80 2,21 0.06 0.72 1.03 0.91 1.49 1,80 1.81 0.81 |¤> 27 1.28 JNDC(T) 0.49 1.04 83 43 2.76 1.50 1.47 1.23 2.92 1.05 2.60 2.04 1.15 1.09 2.68 2.37 2.99 2.44 96.0 1,57 ij ENDF/B-V 1.68 1,88 2,62 2.42 2.15 4.15 2,53 2.61 2.19 2.21 2,47 2.37 1.67 2.41 2.61 1.81 ENDF/B-IV 1.19 2.62 2.48 1.35 1.96 2.19 1.30 2.32 2.84 2.09 2.06 2.40 3.46 2.76 2.03 1.94 1.35 2,35 2.16 3.64 1.692.40 (MeV) t 2.38 2.48 1.68 1.35 1.94 3.29 JNDC(E) 2.53 2.50 2.26 1.98 2.54 2.40 2.15 3.81 3.95 2.89 2.27 . स JNDC(T) 2.31 1.40 0.79 2.52 2.16 1.24 2,24 2.20 2.68 2.14 3.22 2,23 1.29 2.25 2.73 1.59 1.96 2.60 2.47 3.71 2.99 2.26 2.86 2.15 7.128 5.360 7.338 6.670 5.810 8.980 6,390 5.900 5.620 5.400 8,000 5.400 7.000 7,200 10.850 9.080 6.090 6.23 9 Rh110^m Tc108Mo105 Ag118 TC104 Rh110 Zr101^m86Y Rb98 Sr98Sr96Sr97Rb92 86X 797

Table IV (cont'd)

\bar{B}_{β} (MeV) \bar{B}_{γ} (MeV)	00)	(cont'd)												
ENDF/B—IV ENDF/B—IV <t< td=""><td></td><td></td><td> 퍼 요</td><td>(MeV)</td><td></td><td></td><td> m≻</td><td>(MeV)</td><td>}</td><td>% conf 235U c</td><td>tr. to decay</td><td>Calcul</td><td>ation Parame</td><td>ers</td></t<>			퍼 요	(MeV)			m≻	(MeV)	}	% conf 235U c	tr. to decay	Calcul	ation Parame	ers
2.97 2.94 2.51 1.12 2.91 2.93 0.48 1.57 2.09 2.14 1.26 1.73 1.93 1.15 1.9 1.5 1.6 2.4 1.57 1.9 1.5 1.0 1.5 1.0 1.5 1.0 1.0 2.4 5.40 2.0 1.0	JNDC(T)	. — —	JNDC(E)	ENDF/B-IV	ENE	JNDC(T)	JNDC(E)	ENDF/B-IV			tc= 100	t1/2	t _{1/2} ;calc'	Q ₀₀ (MeV)
1.92 2.17 2.29 1.50 1.73 1.15 <th< td=""><td>3.05</td><td></td><td>3.70</td><td>2.97</td><td>2.94</td><td>2.51</td><td>1.12</td><td>2,91</td><td>2.93</td><td></td><td></td><td>0.48</td><td>1.57</td><td>0.0</td></th<>	3.05		3.70	2.97	2.94	2.51	1.12	2,91	2.93			0.48	1.57	0.0
2.74 2.09 2.14 1.24 1.26 1.86 1.59 1.59 1.57 1.01 2.23 - 2.36 1.66 2.27 - 1.95 2.4 5.40 2.33 2.26 2.29 1.57 1.87 2.20 1.94 2.4 5.40 2.45 1.59 1.91 1.76 0.58 2.24 1.22 11.9 2.45 1.59 1.09 1.79 1.70 0.96 2.32 2.32 2.29 2.29 2.32 3.44 2.20 2.29 2.29 3.44 2.20 2.29 2.29 2.29 3.44 2.89 3.59 <	2.42		1.92	2.17		1.50	1.73	1.93	1.15			10	6.6	0.1
2.23 - 2.36 1.66 2.27 - 1.95 - 2.4 5.40 2.33 2.26 2.29 1.57 1.87 2.20 1.94 - 3.21 6.20 2.45 1.59 1.57 1.87 2.20 1.94 0.38 - 3.21 6.20 1.81 1.53 1.93 1.08 1.70 0.96 - 2.32 9.44 1.81 1.93 1.08 1.70 0.96 - 2.12 11.9 2.47 2.54 2.58 2.03 2.59 0.95 1.53 3.19 2.49 1.96 2.29 0.95 1.53 2.19 1.65 1.53 3.19 2.40 2.54 1.73 0.43 2.29 0.95 1.33 1.65 1.65 1.65 1.65 1.65 1.65 1.65 1.65 1.65 1.65 1.65 1.65 1.65 1.65 1.65 1.65 <t< td=""><td>2.36</td><td></td><td>2.74</td><td>2.09</td><td>2.14</td><td>1.24</td><td>1.26</td><td>1.86</td><td>1.59</td><td></td><td>:</td><td>1.5</td><td>10.1</td><td>0.0</td></t<>	2.36		2.74	2.09	2.14	1.24	1.26	1.86	1.59		:	1.5	10.1	0.0
2.33 2.26 2.29 1.57 1.87 2.20 1.94 3.21 6.20 2.45 1.59 1.11 1.84 0.13 1.76 0.58 12.2 11.9 1.81 1.53 1.93 1.08 1.29 1.70 0.96 2.32 9.44 3.47 - 2.10 0.66 - - 2.1 2.89 2.47 2.54 2.58 2.03 2.53 2.29 0.95 3.76 3.89 2.79 1.96 2.24 1.73 0.43 2.29 0.95 3.76 3.81 2.79 1.96 2.29 0.95 2.29 0.95 3.76 3.81 2.79 1.96 2.29 0.95 3.76 3.81 3.92 3.81 3.92 2.79 2.90 3.95 - 2.92 0.95 3.76 1.63 1.10 0.95 3.76 1.63 2.49 2.90 3.50	2.5		2.23	1	2.36	1.66	2.27	1	1.95			2.4	5.40	0.0
2.45 1.59 2.11 1.84 0.13 1.76 0.58 11.2 11.9 1.81 1.53 1.93 1.08 1.29 1.70 0.56 - - 2.32 9.44 3.47 - - 2.10 0.66 - - - 2.1 2.89 2.47 2.54 2.58 2.03 2.53 2.59 2.29 0.95 - 2.1 2.89 2.79 1.96 2.24 1.73 0.43 2.29 0.95 3.76 3.81 2.79 1.96 2.24 1.73 0.43 2.29 0.95 3.76 3.81 2.79 1.96 2.24 1.73 0.43 2.29 2.95 0.95 3.76 3.81 3.36 2.80 3.12 2.63 3.16 3.06 2.13 3.24 3.86 3.14 2.44 2.80 3.10 2.63 3.14 3.24 3.24 3.24<	2.5	Н	2.33	2.26			1.87	2.20	1.94	:		3.21	6.20	0.0
1.81 1.53 1.93 1.08 1.29 1.70 0.96	1.6	9	2,45	1.59		1.84	0.13	1.76	0.58			12.2	11.9	1.2
3.47 - - 2.10 0.66 - - - 2.1 2.89 2.47 2.54 2.54 2.53 2.59 2.29 2.29 1.53 3.19 2.79 1.96 2.24 1.73 0.43 2.29 0.95 1.37 3.76 3.81 2.18 1.87 2.15 1.44 1.52 2.19 1.65 1.3 3.76 3.81 2.49 - 2.86 3.56 3.56 3.29 - 2.92 0.84 1.40 3.29 - 2.49 0.20 - 2.92 0.84 1.40 3.29 - 2.49 3.06 2.13 0.84 1.40 3.29 - 2.49 3.06 2.13 0.84 1.40 3.29 - 2.49 2.95 0.20 - 2.07 0.84 1.40 3.13 2.89 3.04 2.69 2.24 3.43 3	1:5	4	1.81	1.53	1.93	1.08	1.29	1.70	96.0			2.32	9.44	0.5
2.47 2.54 2.58 2.03 2.53 2.59 2.29 1.53 3.19 2.79 1.96 2.24 1.73 0.43 2.29 0.95 1.65 3.76 3.81 2.18 1.87 2.15 1.44 1.52 2.19 1.65 1.3 3.92 2.49 - 2.86 3.56 3.16 3.06 2.13 0.93 1.65 1.65 3.29 - 2.86 3.56 3.16 3.06 2.13 0.84 1.40 3.29 - 2.49 2.95 0.20 - 2.07 0.84 1.40 3.29 - 2.29 0.20 - 2.07 0.84 1.40 3.24 2.86 1.86 1.81 2.55 1.10 0.99 1.67 3.13 2.89 3.04 2.69 2.24 3.47 0.29 - 1.03 1.17 1.30 1.48 4.66 5.00	2.	17	3.47	ι	t	2.10	99.0	1	1			2.1	2.89	0.0
2.19 1.96 2.24 1.73 0.43 2.29 0.95 3.76 3.81 2.18 1.87 2.15 1.44 1.52 2.19 1.65 1.3 3.76 3.92 2.49 - 2.86 3.56 3.96 - 2.92 0.84 1.65 1.65 3.36 2.80 3.12 2.63 3.16 3.06 2.13 0.84 1.40 3.29 - 2.49 2.95 0.20 - 2.07 0.84 1.40 2.46 2.86 1.86 1.81 2.55 1.10 0.84 1.40 2.46 2.07 2.86 1.81 2.55 1.10 0.59 1.67 2.46 2.07 2.86 1.81 2.24 3.43 3.34 0.59 1.03 2.29 2.26 1.94 3.07 2.47 0.29 1.03 2.27 2.10 1.00 0.3 0.29 1.03 <td>2.</td> <td>74</td> <td>2.47</td> <td>2.54</td> <td></td> <td>2.03</td> <td>2.53</td> <td>•</td> <td>2.29</td> <td></td> <td></td> <td>1.53</td> <td>3,19</td> <td>0.0</td>	2.	74	2.47	2.54		2.03	2.53	•	2.29			1.53	3,19	0.0
2.18 1.87 2.15 1.44 1.52 2.19 1.65 1.65 1.65 3.92 2.49 - 2.86 3.56 3.96 - 2.92 5.6 1.65 1.65 3.36 - 2.86 3.56 3.16 3.06 - 2.92 5.6 1.65 1.65 3.36 2.80 3.12 2.63 3.16 3.06 2.13 0.84 1.40 2.46 2.07 2.86 1.81 2.55 1.10 0.84 1.67 3.13 2.89 3.04 2.69 2.24 3.43 0.59 1.67 1.17 1.30 1.47 2.99 1.63 1.71 1.00 0.29 -1 2.29 2.35 1.63 1.63 1.71 1.00 0.29 -1 1.17 1.30 1.44 4.66 5.00 0.3 1.64 1.47 2.29 2.80 2.73 2.73 2	2.	19	2.79	1.96	2.24	1.73	0.43	2.29	0.95			3.76	3.81	0.8
2.49 - 2.86 3.56 3.96 - 2.92 5.6 1.65 1.65 3.36 2.80 3.12 2.63 3.16 3.06 2.13 0.84 1.40 3.29 - 2.49 2.95 0.20 - 2.07 2.35 1.36 1.81 2.55 1.10 0.99 1.67 1.40 2.46 2.07 2.86 1.86 1.81 2.55 1.10 0.99 1.67 1.67 3.13 2.89 3.04 2.69 2.24 3.43 3.34 0.59 1.67 1.03 1.67 1.67 1.03 1.67 1.67 1.67 1.03 1.67 1.67 1.67 1.67 1.67 1.60 1.	2.	25	2.18	1.87	2.15	1.44	1.52	2.19	1.65			1.3	3.92	0.5
3.36 2.80 3.12 2.63 3.16 3.06 2.13 0.84 1.40 3.29 - 2.49 2.95 0.20 - 2.07 0.84 1.40 2.46 2.07 2.86 1.86 1.81 2.55 1.10 0.99 1.67 3.13 2.89 3.04 2.69 2.24 3.43 3.34 0.59 1.03 2.29 2.35 2.76 2.02 1.94 3.07 2.47 0.29 -1 2.24 3.82 2.76 2.02 1.94 3.07 2.47 0.29 -1 1.17 1.30 1.47 2.39 1.63 1.71 1.00 0.13 1.00 2.24 3.82 3.63 2.90 4.48 4.66 5.00 0.3 0.13 1.00 1.20 1.72 1.38 2.73 2.51 2.01 2.60 0.3 1.47 3.14 2.95 2.80	2.	63	2.49	1	2.86	3.56	3.96	1	2.92			5.6	1,65	2.0
3.29 - 2.49 2.95 0.20 - 2.07 2.5 1.10 2.5 1.10 2.14 2.14 2.46 2.07 2.86 1.86 1.81 2.55 1.10 0.099 1.67 3.13 2.89 3.04 2.69 2.24 3.43 3.34 0.59 1.03 2.29 2.35 2.76 2.02 1.94 3.07 2.47 0.029 -1 2.29 2.35 2.76 2.02 1.94 3.07 2.47 0.029 -1 2.24 3.82 3.63 2.90 4.66 5.00 0.3 1.68 4.64 5.00 0.13 1.00 -1 40.4 1.00 -1 1.00 -1 40.4 -1 1.00 -1 1.00 -1 1.00 -1 1.00 -1 1.00 -1 1.00 -1 1.00 -1 1.00 -1 1.00 -1 1.00 -1 1.00 <td>e,</td> <td>05</td> <td>3.36</td> <td>2.80</td> <td>3.12</td> <td>2.63</td> <td>3.16</td> <td>3.06</td> <td>2.13</td> <td></td> <td></td> <td>0.84</td> <td>1.40</td> <td>0.0</td>	e,	05	3.36	2.80	3.12	2.63	3.16	3.06	2.13			0.84	1.40	0.0
2.46 2.07 2.86 1.81 2.55 1.10 0.99 1.67 3.13 2.89 3.04 2.69 2.24 3.43 3.34 0.576 1.03 2.29 2.35 2.76 2.02 1.94 3.07 2.47 0 0.29 -1 1.17 1.30 1.47 2.39 1.63 1.71 1.00 0 61.0 40.4 40.4 1.20 1.72 1.38 2.90 4.48 4.66 5.00 0.3 1.6 61.0 40.4 1.00 1.20 1.72 1.38 2.73 2.57 2.01 2.60 0.3 1.6 61.0 40.4 1.00 3.10 2.08 2.39 1.86 0.39 2.80 1.98 1.47 1.47 1.44 3.14 2.95 2.80 3.20 2.04 0.00 0.00 0.00 0.00 0.08 0.85 2.45 2.44 1.63	2.	16	3.29	ı		2.95	0.20		2.07			2.5	2.14	2.0
3.13 2.89 3.04 2.69 2.24 3.43 3.34 0.576 1.03 2.29 2.35 2.76 2.02 1.94 3.07 2.47 0.29 -1 1.17 1.30 1.47 2.39 1.63 1.71 1.00 0.3 61.0 40.4 2.24 3.82 3.63 2.90 4.48 4.66 5.00 0.3 1.6 61.0 40.4 1.20 1.72 1.38 2.73 2.57 2.01 2.60 0.3 1.6 1.68 53.4 3.10 2.08 2.39 1.86 0.39 2.80 1.98 1.47 1.47 3.14 2.95 2.80 3.78 2.09 2.04 0.3 1.04 2.45 3.84 3.95 3.78 2.26 0.00 0.00 0.00 0.08 0.08 0.85 2.45 2.44 1.63 2.17 0.74 2.7 0.8 19.2	2.	59	2.46	2.07	2.86	1.86	1.81	2.55	1.10			0.99	1.67	0.5
2.29 2.35 2.76 2.02 1.94 3.07 2.47 0.29 -1 1.17 1.30 1.47 2.39 1.63 1.71 1.00 61.0 61.0 40.4 2.24 3.82 3.63 2.90 4.48 4.66 5.00 0.3 1.6 61.0 61.0 40.4 1.20 1.72 1.38 2.73 2.57 2.01 2.60 0.3 1.68 53.4 3.10 2.08 2.39 1.86 0.39 2.80 1.98 1.47 1.47 3.14 2.95 2.80 3.27 2.03 2.04 0.3 1.04 1.04 2.45 2.44 1.63 2.26 0.00 0	ا بى	90	3.13	2.89	3.04	2.69	2.24	3.43	3.34			0.576	1.03	0.0
1.17 1.30 1.47 2.39 1.63 1.71 1.00 61.0 61.0 40.4 2.24 3.82 3.63 2.90 4.48 4.66 5.00 0.3 1.6 0.13 1.00 1.20 1.72 1.38 2.73 2.57 2.01 2.60 0.3 1.6 1.68 53.4 3.10 2.08 2.39 1.86 0.39 2.80 1.98 0.104 0.3 1.04 2.45 3.84 3.95 3.78 2.26 0.00 0.00 0.00 0.08 0.85 2.45 2.44 1.63 2.40 2.62 0.69 2.17 0.74 2.7 0.8 19.2 9.04 2.31 1.94 2.13 2.94 2.00 1.93 2.00 1.1 1.8 44.8 10.8	2	,71	2.29	2.35		2.02	1.94	3.07	2.47			0.29	7	0.5
2.24 3.82 3.63 2.90 4.48 4.66 5.00 0.3 1.6 0.13 1.00 1.20 1.72 1.38 2.73 2.57 2.01 2.60 0.3 1.6 1.68 53.4 3.10 2.08 2.39 1.86 0.39 2.80 1.98 1.47 1.47 3.14 2.95 2.80 3.27 2.03 2.09 2.04 0.3 1.04 2.45 3.84 3.95 3.78 2.26 0.00 0.00 0.00 0.85 2.45 2.44 1.63 2.40 2.17 0.74 2.7 0.8 19.2 9.04 2.31 1.94 2.13 2.94 2.00 1.93 2.00 1.1 1.8 44.8 10.8	H	91.	1.17	1.30	1.47	2.39	1.63	1.71	1.00			61.0	707	2.0
1.20 1.72 1.38 2.73 2.57 2.01 2.60 0.3 1.6 168 53.4 3.10 2.08 2.39 1.86 0.39 2.80 1.98 1.47 1.47 3.14 2.95 2.80 3.27 2.03 2.09 2.04 0.3 1.04 2.45 3.84 3.95 3.78 2.26 0.00 0.00 0.00 0.85 2.45 2.44 1.63 2.40 2.62 0.69 2.17 0.74 2.7 0.8 19.2 9.04 2.31 1.94 2.13 2.94 2.00 1.93 2.00 1.1 1.8 44.8 10.8	ر. ا	91	2.24	3.82	3.63	2.90	4.48	4.66	5.00			0.13	1.00	0.0
3.10 2.08 2.39 1.86 0.39 2.80 1.98 1.47 1.47 3.14 2.95 2.80 3.27 2.03 2.09 2.04 0.3 1.04 2.45 3.84 3.95 3.78 2.26 0.00 0.00 0.00 0.85 2.45 2.44 1.63 2.40 2.62 0.69 2.17 0.74 2.7 0.8 19.2 9.04 2.31 1.94 2.13 2.94 2.00 1.93 2.00 1.1 1.8 44.8 10.8		20	1.20	1.72		2.73	2.57	2.01	2.60	0.3	1.6	168	53.4	2.0
3.14 2.95 2.80 3.27 2.03 2.09 2.04 0.3 1.04 2.45 3.84 3.95 3.78 2.26 0.00 0.00 0.00 0.85 2.45 2.44 1.63 2.40 2.62 0.69 2.17 0.74 2.7 0.8 19.2 9.04 2.31 1.94 2.13 2.94 2.00 1.93 2.00 1.1 1.8 44.8 10.8	2.	41	3.10	2.08	!	1,86	0.39	2.80	1.98			1.47		
3.84 3.95 3.78 2.26 0.00 0.00 0.00 0.085 2.45 2.44 1.63 2.40 2.62 0.69 2.17 0.74 2.7 0.8 19.2 9.04 2.31 1.94 2.13 2.94 2.00 1.93 2.00 1.1 1.8 44.8 10.8	2.	28	3.14	2.95		3.27	2.03	2.09	2.04	0.3		1.04	2,45	0.0
2.44 1.63 2.40 2.62 0.69 2.17 0.74 2.7 0.8 19.2 9.04 2.31 1.94 2.13 2.94 2.00 1.93 2.00 1.1 1.8 44.8 10.8	2.	78	3.84	3.95	3.78	2.26	00.00	00.0	0.00			0.85	2,45	0.0
2.31 1.94 2.13 2.94 2.00 1.93 2.00 1.1 1.8 44.8 10.8	1.	53	2.44	1.63	2.40	2.62	69.0	2.17	0.74	2.7	0.8	19.2	9.04	2.0
-	1.7	9	2.31	1.94		2.94	2.00	1,93	2.00	1.1	1.8	44.8	10.8	2.0

· T			- (- [į			1						
cers	Q ₀₀ (MeV)	2.0	2.0	2.0	2.0	2.0	2.0	0.5	1.7	0.5	0.0	1.2	0.0	0.0	0.0
tion Paramet	t _{1/2} :calc'd (sec)	10.8	21.0	66.3	74.3	39.7	25.1	5.03	2.48	3.87	5,29	4.23	11.4	11.3	19.1
Calcula	t _{1/2} :input (sec)	85.1	24.5	174	1932	39.5	63.7	1.73	2.49	1.24	1.71	4.21	8.5	0.47	6.2
ecay	tc= 100 sec	4.8	1.2			3.4	8.0		1.8			5.8			
235U d	tc= 20 sec	1.2	2.2			2.6	2.4		3.0	 		2.5	2.1		0.4
		2.38	0.97	0.54	2,36	97.0	2.30	0.78	0.80	1.12	1.17	1.83	1.73	2.04	1.48
(MeV)	ENDF/B-IV	2.21	2.03	2,60	2,33	0.93	2.13	2.27	1.82	1.77	2.54	1.94	2.36	2.67	1.86
¤⊱	JNDC(E)	2.47	0.75	0.53	2.33	0.89	2.22	1.04	0.67	1.19	3.81	1.31	0.72	0.88	0.26
	JNDC(T)	2.94	2.46	0.73	2.68	2.24	2.79	1.49	2.14	0.98	1.79	2.09	1,35	1,36	1.08
	ENDF/B-V	1.97	2.29	0.39	1.20	1.70	1.65	2.35	1.91	1.66	2.50	1.46	2.05	2.21	1.84
(MeV)	ENDF/B-IV	1.81	1.51	1.15	1.26	1.79	1.93	1.57	1.38	1.10	2.04	1.51	1.77	1.93	1.35
[퍼 &		2.54	1.97	0.40	1.25	1.74	1.75	2.36	2.09	1.85	2.62	1.79	2.46	2.74	2.31
	JNDC(T)	1.76	1.27	0.28		1.00	1.43	2.05	1.28	1.76	2.45	1.34		2.18	2.02
0 8	(MeV)	7.000	5.500	5.420	5.340	5.020	6.170	6.150	5.190	5.040	7.280	5.500	6.300	6.300	5.700
		1136	1137	Cs138 ^m	Cs138	Xc139	Cs140		-	1	Cs142	La144		La148	
	\overline{E}_{eta} (MeV)	$\overline{E_{\beta}} \hspace{0.5cm} \text{(MeV)} \hspace{0.5cm} \overline{E_{\beta}} \hspace{0.5cm} \text{(MeV)} \hspace{0.5cm} \overline{E_{\gamma}} \hspace{0.5cm} \text{(MeV)} \hspace{0.5cm} \overline{E_{\gamma}} \hspace{0.5cm} \text{(MeV)} \hspace{0.5cm} \overline{E_{\gamma}} \hspace{0.5cm} \text{(MeV)} \hspace{0.5cm} \overline{E_{\gamma}} \hspace$	$ \begin{array}{c ccccccccccccccccccccccccccccccccccc$	QB EB (MeV) EV (MeV) EV (MeV) EV (MeV) EV (MeV) (MeV)	$ \begin{array}{c c c c c c c c c c c c c c c c c c c $	$ \begin{array}{c c c c c c c c c c c c c c c c c c c $	$ \begin{array}{c c c c c c c c c c c c c c c c c c c $	$ \begin{array}{c c c c c c c c c c c c c c c c c c c $	QB Telement Telement Telement Telement Telement Calculation Paramet (MeV) JNDC(T) JNDC(T)	QB Image: Tell MeV) <	QB Table (MeV) Ta	Qβ Tell (MeV) Eg (MeV) Eg (MeV) Eg (MeV) Eg (MeV) Eg (MeV) Eg (MeV) <	Qg 1.25 (MeV) EV (MeV) EV (MeV) EV (MeV) Pheat Calculation Paramet (MeV) JNDC(T) JNDC(E) ENDF/B-LV INDF/B-LV ENDF/B-LV ENDF/B-LV ENDF/B-LV EV LC= LC= L/2 (sec.) L/2 (sec.) </td <td>Qβ Image Image Calculation Paramet (MeV) JNDC(T) JNDC(E) ENDF/B-LV JNDC(T) JNDC(T)</td> <td>φg Tage (MeV) Feat (MeV) Feat Calculation Paramet (MeV) JMDC(T) JMDC(E) ENDF/B-IV JMDC(T) JMDC(T)<!--</td--></td>	Qβ Image Image Calculation Paramet (MeV) JNDC(T) JNDC(E) ENDF/B-LV JNDC(T) JNDC(T)	φg Tage (MeV) Feat (MeV) Feat Calculation Paramet (MeV) JMDC(T) JMDC(E) ENDF/B-IV JMDC(T) JMDC(T) </td

Table V Values of $\overline{E}_{\gamma}/\textbf{Q}_{\beta}$ for three assumed beta-strength functions

		$Q_{\beta} = 6 \text{ MeV}$	$Q_{\beta} = 8 \text{ MeV}$	$Q_{\beta} = 10 \text{ MeV}$
	S _β ∝ E	0.27	0.27	0.26
Present simple	$S_{\beta} \propto e^{E/1.5}$	0.25	0.29	0.34
calc.	S _β ∝ e ^E	0.33	0.40	0.48
Tasak	a, Ref. 5)	0.29	0.29	0.29
Tobia	s, Ref. 20)	0.33	0.33	0.33
Yamam	oto, Ref. 38)	~0.25 for 1	ight and ~0.35	for heavy peaks

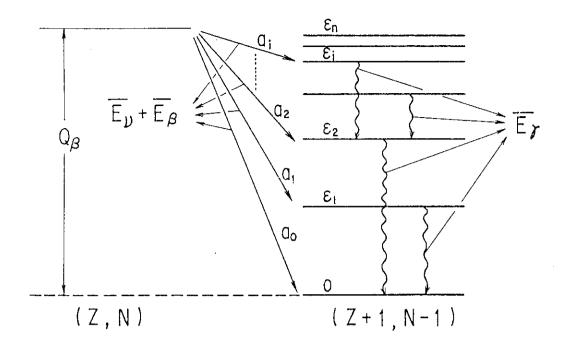


Fig. 1 Schematic display of beta- and gamma-decay process from a parent (Z, N) to the daughter (Z + 1, N - 1)

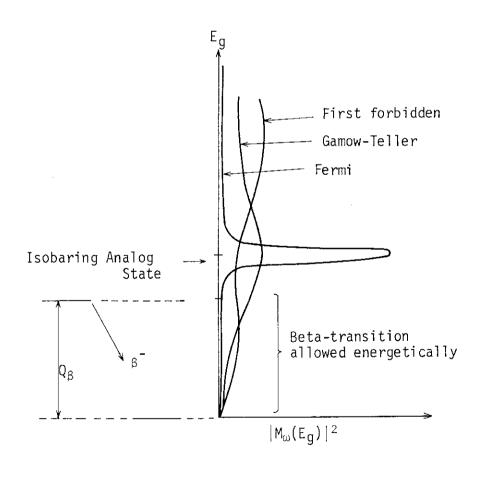


Fig. 2 Schematic view of beta-strength function

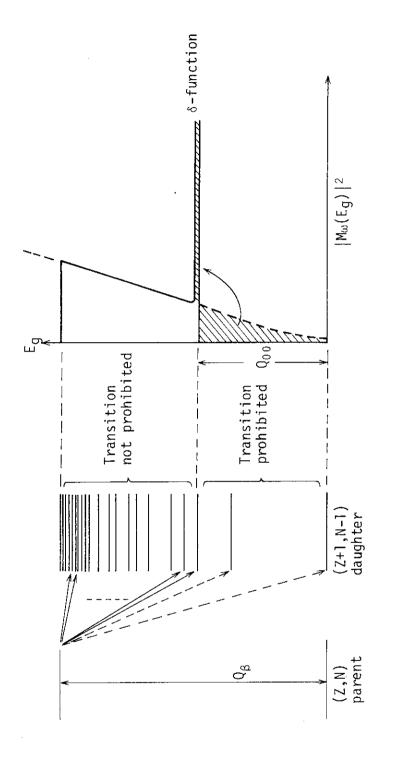


Fig. 3 Introduction of a parameter $Q_{0\,0}$

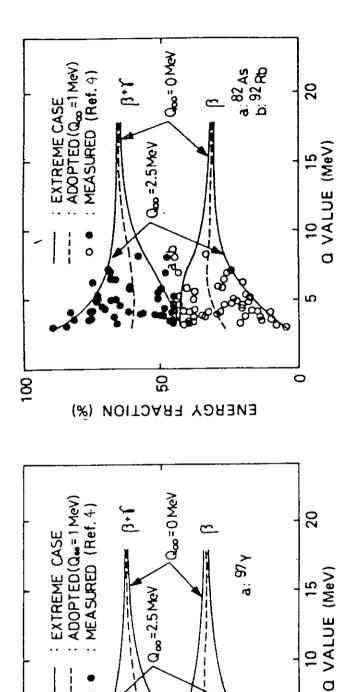


Fig. 5 Percentage of average beta-particle and gamma-ray energies from odd-odd fission products, and comparison of calculation with experiment (Ref. 4). (Total decay energy * 100%, calculated at A = 90.)

Fig.4 Percentage of average beta-particle and gamma-ray energies from odd-A fission products, and comparison of calculation with experiment (Ref. 4). (Total decay energy = 100%, calculated at $A \approx 89$.)

20

ENERGY FRACTION (%)

5

88

0

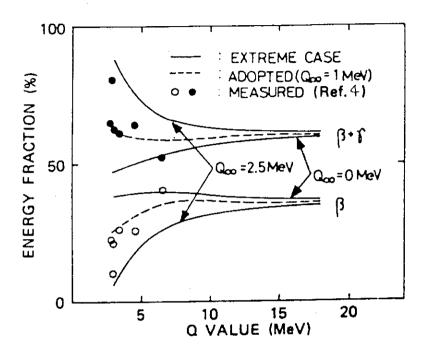
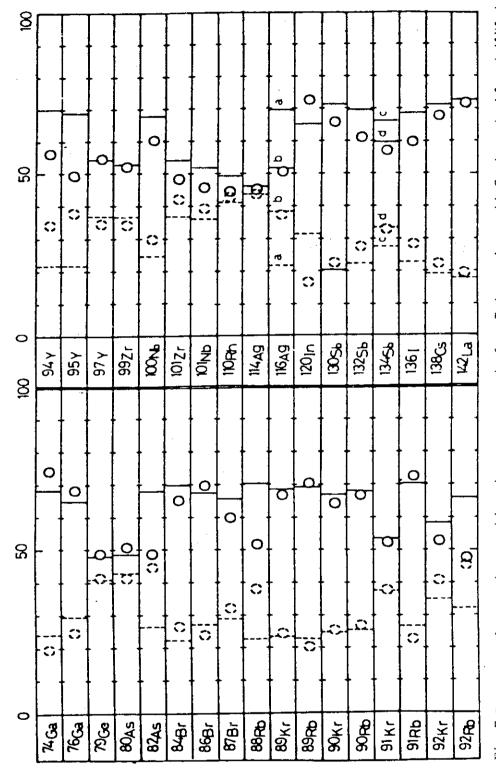


Fig. 6 Percentage of average beta-particle and gamma-ray energies from even-even fission products, and comparison of calculation with experiment (Ref. 4). (Total decay energy = 100%, calculated at A = 90.)



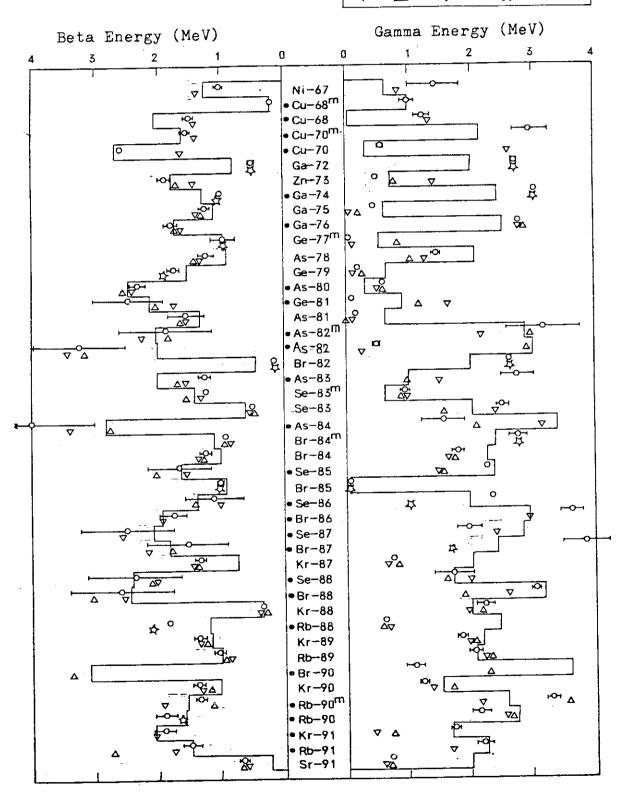
Here, a dot = beta energy, a solid = beta-particle plus gamma-ray energy, a circle = experimental value (Refs. 4 and 2), and a line = calculated value. Lines a and c are based on t_1/t_2 from Ref. 4 and b and d from Ref. 39. (Total decay energy = 100%.) Fig. 7 Percentage of average beta-particle and gamma-ray energies from fission products, with Q_{∞} determined from half-life data.

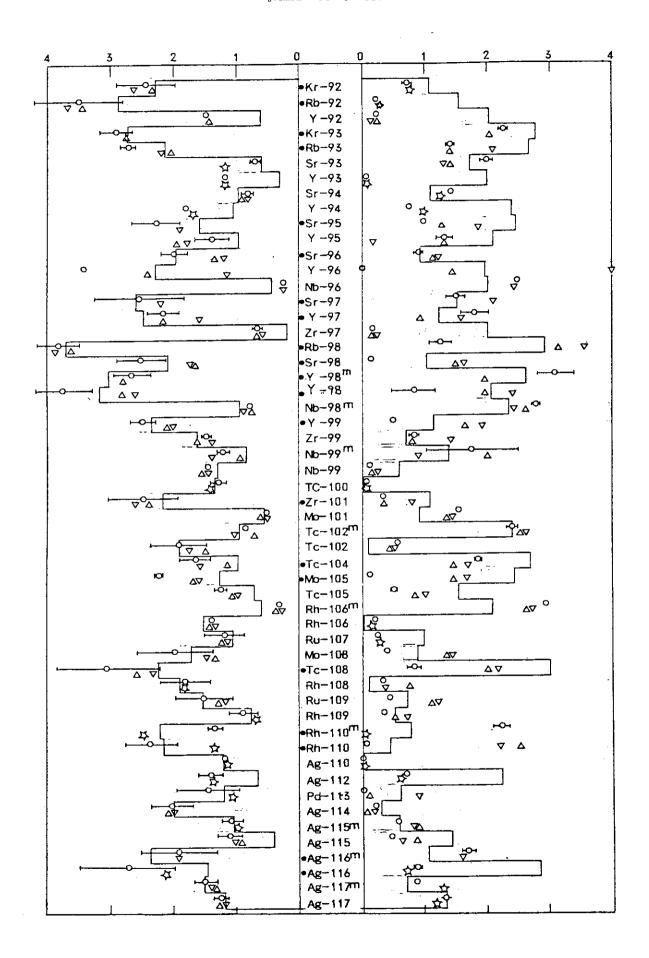
8																	
		† - -	† †	+			+	† 			0	0				0	0
20	0	0	0	0		0	0 0	9	၉	0			0	0	0		
	0			Ω.	C						0	0	-0	C	-52	С	0
0 001	7,76	λ56	97γ	99Zr	3400	10121	qNiQ	10gh	11449	116Ag	120jn	13051	132Sb	13/ch	1361	138_{Cs}	142/14
	0	0				0	0	Ó		0	0	0	0		0		
50			0 0	0 0	00				0 0					0		0 0	'α;
	٥	0				O	O	O		0	C	C	O		O		
0	74Ga	76 _{Cs}	79 _{Ge}	80 _{AS}	82 _{AS}	84Br	86Br	87Br	Ф-	89Kr	89Ptb	90Kr	90Pb	91Kr	91Rb	92Kr	92Rb

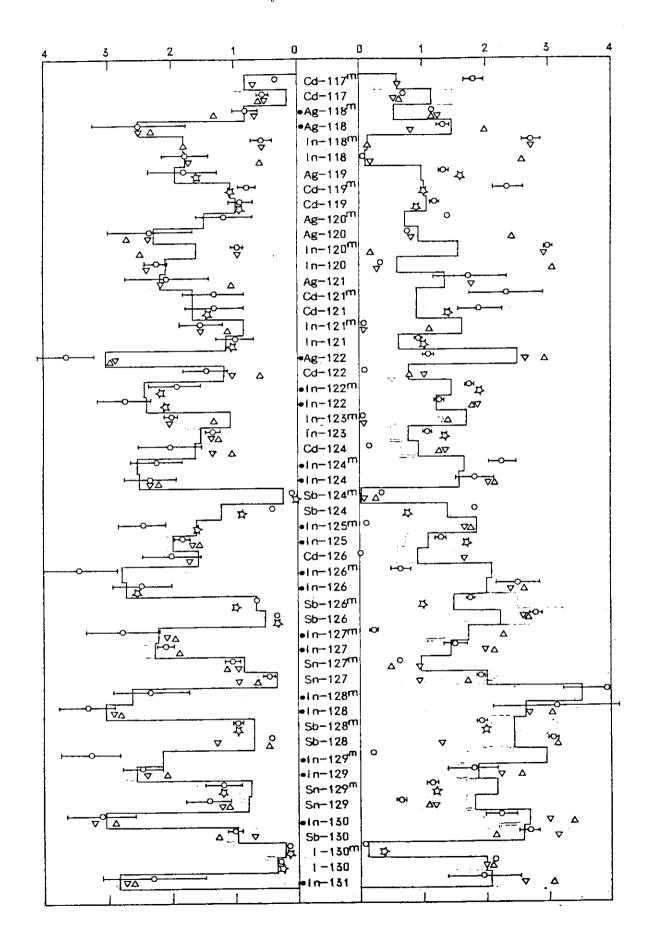
Fig. 8 Percentage of average beta-particle and gamma-ray energies from fission products, Q_{∞} fixed to 1.0 MeV. Here, a dot = beta energy, a solid = beta-particle plus gamma-ray energy, a circle = experimental value (Refs. 4 and 2), and a line = calculated value. (Total decay energy = 100%.)

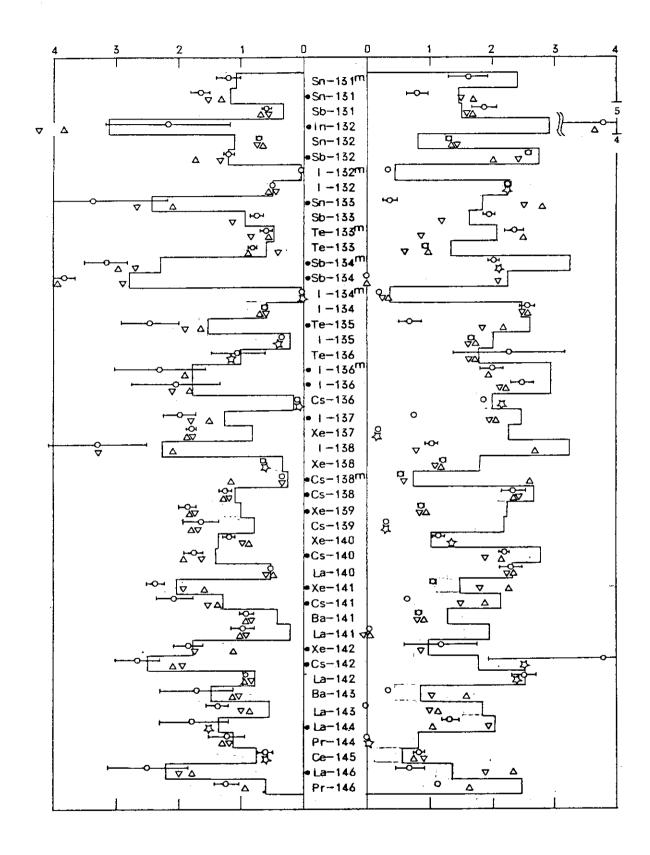
Fig.9 Calculated beta- and gamma-ray energies released from short-lived FPs. Also shown in circles, triangles, and stars, are library values.

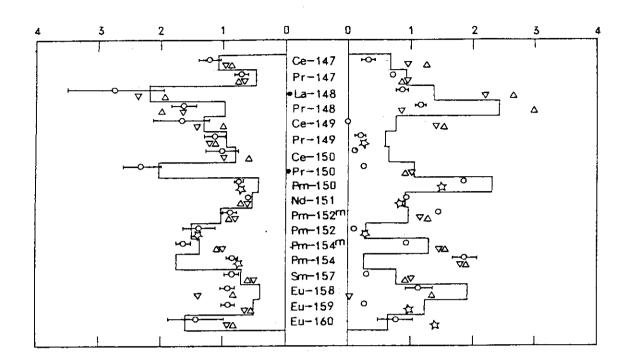
○: JNDC (1980)
 △: ENDF/B-IV
 ▽: Tasaka (1979)
 □: △ and ▽ overlapped

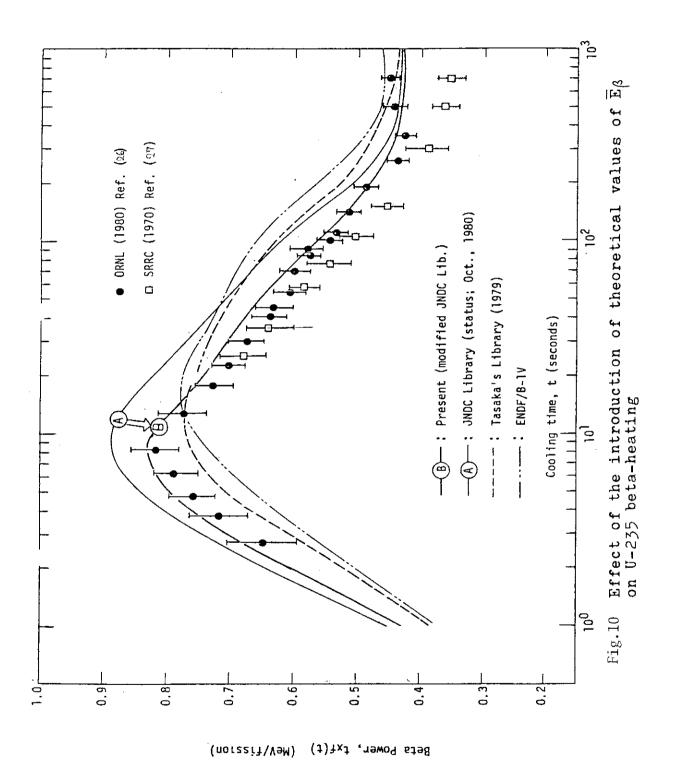




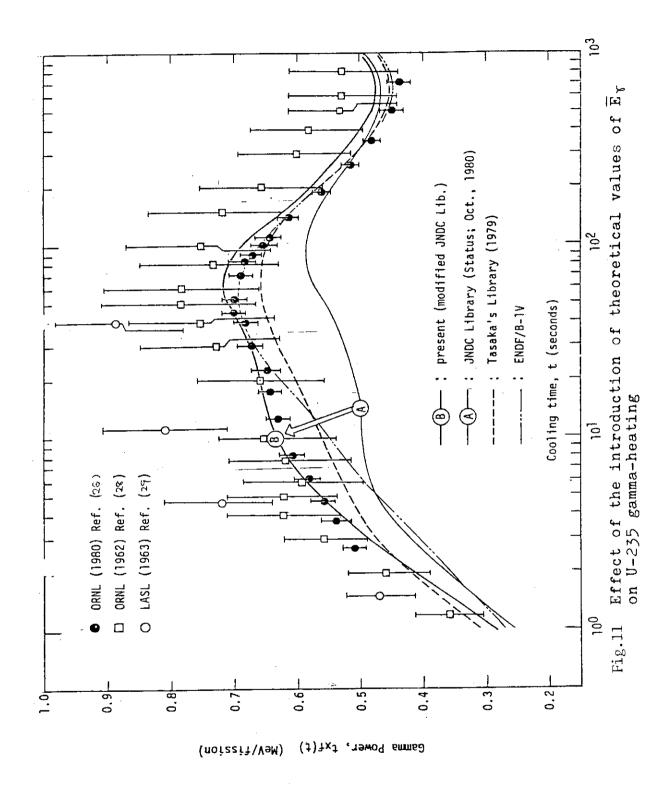








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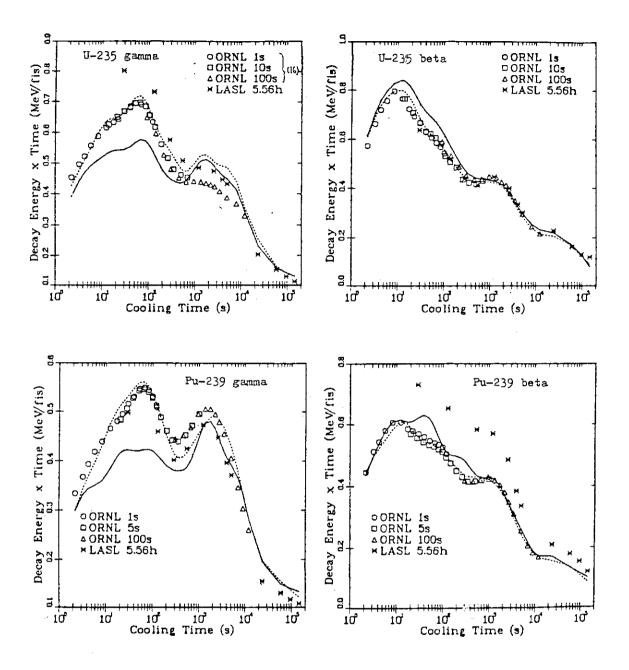
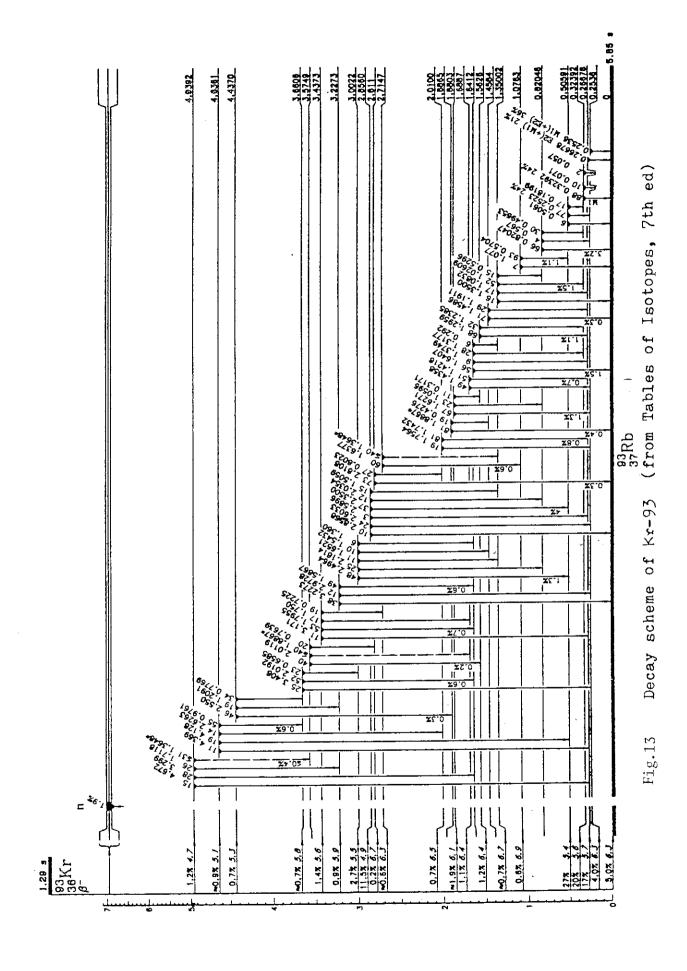


Fig. 12 Effect of the introduction of the theoretical values of Es and Es on beta and gamma-decay heats based on ENDF/B-V data library

(_____:original,----:after the introduction, calculated by T.R.England, Los Alamos Scientific Laboratory, et al.

(See also reference 30).)



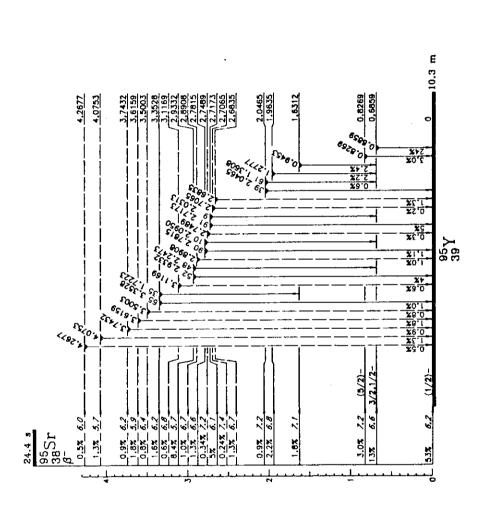


Fig. 14 Decay scheme of 95Sr (from Tables of Isotopes, 7th ed.)

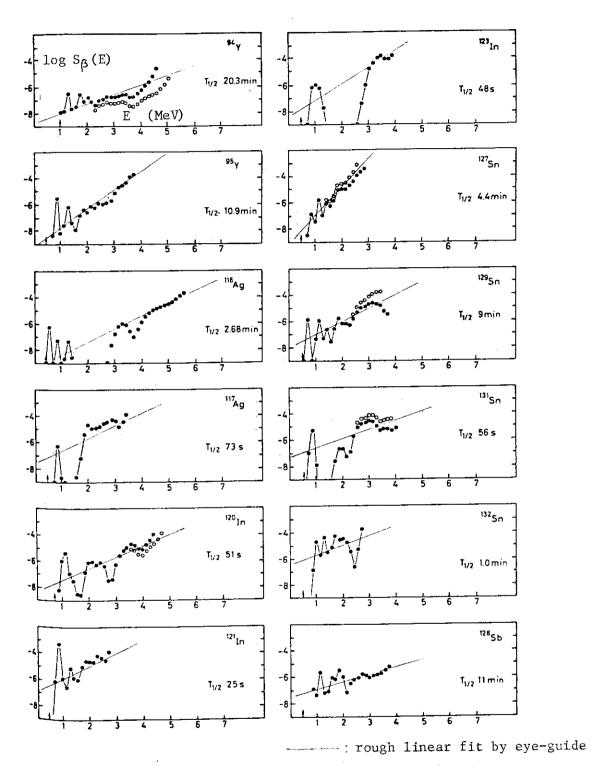


Fig.15 Examples of measured beta-strength functions (from K.H.Johansen, K.B.Nielsen, G.Rudstam, Nucl.Phys., A203, 481(1973))

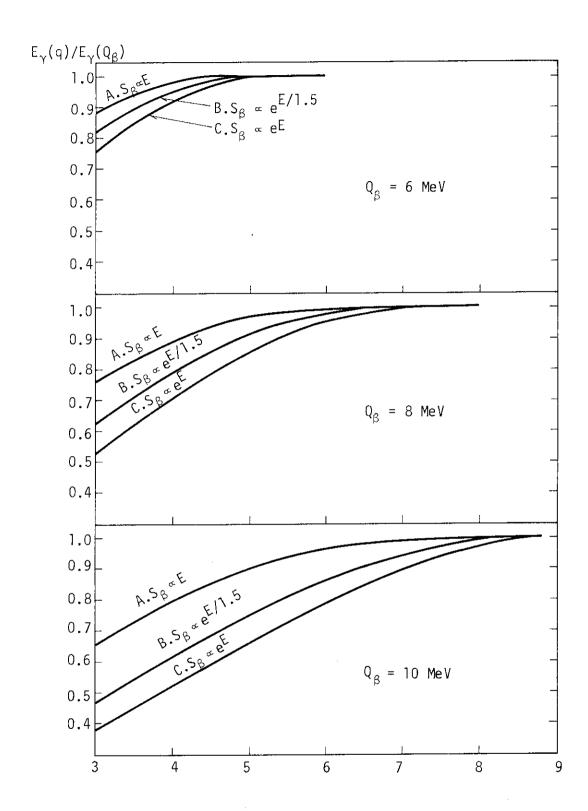


Fig. 16 Decrease of E $\,$ due to possible missing of beta strengths at high excitation