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SUMMARY OF JENDL-2 GENERAL PURPOSE FILE

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Summary of JENDL-2 General Purpose File

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(Received May 12, 1984)

The general purpose file of the second version of Japanese Evaluated Nuclear Data Library (JENDL-2) was released in December 1982. Recently, descriptive data were added to JENDL-2 and at the same time the first revision of numerical data was performed. JENDL-2 (Rev1) consists of the data for 89 nuclides and about 211,000 records in the ENDF/B-IV format. In this report, full listings of presently added descriptive data are given to summarize the JENDL-2 general purpose file. The 2200-m/sec and 14-MeV cross sections, resonance integrals, Maxwellian and fission spectrum averaged cross sections are given in a table. Average cross sections were also calculated in suitable energy intervals.

Keywords :

JENDL-2, Evaluated Data File, Descriptive Data, Resonance Integral, 2200-m/sec Cross Section, 14-MeV Cross Section.

JENDL-2 General Purpose ファイルの概要

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(1984年5月12日受理)

日本の評価済みデータライブラリー第2版 (JENDL-2) の General Purpose ファイルは 1982年12月に公開された。最近, JENDL-2 にデータの様子を示すコメント情報を追加すると同時に第1回目の数値データの修正を行った。この JENDL-2 (Rev 1) は 89核種のデータを含み, ENDF/B-IV フォーマットで約 211,000 レコードから成っている。本報告では, JENDL-2 General Purpose ファイルの概要を示すために, 今回加えられたコメント情報が示される。2200 m/sec および 14 MeV 断面積, 共鳴積分値, マックスエルおよび核分裂スペクトルでの平均断面積が表に与えられる。さらに適当なエネルギー区間を用いた平均断面積も計算された。

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Preface

The general purpose file of the second version of Japanese Evaluated Nuclear Data Library (JENDL-2) was released in December 1982. However this library, called JENDL-2 (Rev0), does not contain descriptive data of evaluation. Recently the descriptive data were added and some errors already encountered in numerical data were corrected. This newly revised version of JENDL-2 is called as JENDL-2 (Rev1).

This report gives full listings of the descriptive data and some numerical data tables in order to summarize the JENDL-2 general purpose file. Details of correction of numerical data are described in Appendix 3, for the convenience of JENDL-2 users. Full documentation of JENDL-2 is now under preparation as a JAERI report.

Descriptive Data

In order to complete descriptive data part of JENDL-2 general purpose file, each evaluator of JENDL-2 data was asked to write a brief documentation, and to send it to the JAERI Nuclear Data Center. These descriptive data gathered were modified to correctly describe the present JENDL-2 (Rev1) and inserted into MF=1 of JENDL-2. All of them are listed in this report. In the descriptive data, 2200-m/sec cross sections and resonance integrals are given for the total, elastic, capture and fission cross sections, which were calculated with RESEND¹⁾ and INTERN²⁾. This calculation of resonance cross sections with RESEND¹⁾ was made by applying accuracy of 1.0 percent.

Data of JENDL-2 (Rev1)

JENDL-2 (Rev1) contains the data of 89 nuclides and consists of about 211,000 records in the ENDF/B-IV format³⁾. The data are stored in six files as shown in Table 1. Any processing codes for the ENDF/B-IV format can be used to handle JENDL-2 (Rev1). However, A special care is required in treating resonance parameters, because the parameters for the multilevel formula often contain resonances whose J value is unknown. Table 2 shows the resonance region and the applied formula of each nuclide. The nuclides having this problem are marked with asterisks. For these nuclides, RESEND should be used to calculate resonance cross sections. To avoid incorrect calculation and for the convenience of users, pointwise data were also prepared and stored in 14 files as listed in Table 3. The data in these pointwise files were calculated with RESEND applying accuracy of 1.0 percent. Energies of cross sections calculated from resonance parameters are written in the seven-digit format. The pointwise data files contain the whole data of JENDL-2 except resonance parameters.

The 2200-m/sec and 14-MeV cross sections, resonance integrals, and Maxwellian and fission spectrum average cross sections were obtained from the pointwise data with INTERN. The resonance integrals were calculated by assuming a cut-off energy of 0.5 eV. The Maxwellian spectrum average cross sections were calculated in the energy interval from 10^{-5} eV to 3.0 eV, and fission spectrum average cross sections from 10^{-5} eV to 20 MeV with the following Watt-type fission spectrum.

$$S(E) = \sqrt{4/(\pi a^3 b)} \times \exp(-ab/4 - E/a) \times \sinh(bE),$$

where a and b were assumed to be 0.988 MeV and $2.249 \times 10^{-6} \text{ eV}^{-1}$, respectively. The results are listed in Appendix 1.

The average cross sections were also calculated in 75 energy intervals by using CRECTJ5⁴⁾ as follows.

$$\bar{\sigma}_i = \int_{E_i}^{E_{i+1}} \sigma(E) dE / (E_{i+1} - E_i).$$

The average cross sections are given in Appendix 2.

Correction of Numerical Data

Numerical data of JENDL-2 (Rev0) were checked by using FIZCON⁵⁾ and PHYCHE⁶⁾ which are data checking codes for data in the ENDF/B format. Some characteristic data such as 2200-m/sec cross sections were calculated and compared with other evaluated data and recommended values in Refs. 7 and 8. Furthermore the data were carefully checked by eyes.

The errors found by above processes were corrected and some data were replaced with more reasonable data by mainly using CRECTJ5⁴⁾ which is a computer code for compilation of evaluated data in the ENDF/B format. Details of this revision work are described in Appendix 3 to let the JENDL-2 users know which parts of data have been revised.

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Table 1 JENDL-2 (Revision-1) Files

Tape No.	No.	Nuclide	MAT number	Records
201	1	1-H - 1	2011	249
	2	1-H - 2	2012	4623
	3	3-Li- 6	2031	698
	4	3-Li- 7	2032	610
	5	4-Be- 9	2041	545
	6	5-B - 10	2051	1857
	7	6-C - 12	2061	1175
	8	9-F - 19	2091	1148
	9	11-Na- 23	2111	1642
	10	13-Al- 27	2131	1043
	11	14-Si- 0	2140	2117
	12	20-Ca- 0	2200	2529
	13	20-Ca- 40	2201	1772
	14	20-Ca- 42	2202	875
	15	20-Ca- 43	2203	752
	16	20-Ca- 44	2204	733
	17	20-Ca- 46	2205	629
	18	20-Ca- 48	2206	729
	19	21-Sc- 45	2211	2057
	20	23-V - 51	2231	3745
			(Total	29528)
202	1	24-Cr- 0	2240	3510
	2	24-Cr- 50	2241	3314
	3	24-Cr- 52	2242	3770
	4	24-Cr- 53	2243	1457
	5	24-Cr- 54	2244	3417
	6	25-Mn- 55	2251	1986
	7	26-Fe- 0	2260	5242
	8	26-Fe- 54	2261	1156
	9	26-Fe- 56	2262	2044
	10	26-Fe- 57	2263	1099
	11	26-Fe- 58	2264	791
	12	27-Co- 59	2271	1126
	13	28-Ni- 0	2280	4291
	14	28-Ni- 58	2281	4284
	15	28-Ni- 60	2282	4197
	15	28-Ni- 61	2283	3761
	17	28-Ni- 62	2284	3769
	18	28-Ni- 64	2285	3533
			(Total	52747)
203	1	29-Cu- 0	2290	1157
	2	29-Cu- 63	2291	1379
	3	29-Cu- 65	2292	1688
	4	41-Nb- 93	2411	1997
	5	42-Mo- 0	2420	4826
	6	42-Mo- 92	2421	1106
	7	42-Mo- 94	2422	1526
	8	42-Mo- 95	2423	2645

Table 1 (continued)

Tape No.	No.	Nuclide	MAT number	Records
203	9	42-Mo- 96	2424	1862
	10	42-Mo- 97	2425	2782
	11	42-Mo- 98	2426	2387
	12	42-Mo-100	2427	2154
			(Total	25509)
204	1	72-Hf-174	2721	2621
	2	72-Hf-176	2722	3512
	3	72-Hf-177	2723	2878
	4	72-Hf-178	2724	2994
	5	72-Hf-179	2725	2363
	6	72-Hf-180	2726	2815
	7	73-Ta-181	2731	1311
	8	82-Pb- 0	2820	3005
	9	82-Pb-204	2821	3794
	10	82-Pb-206	2822	3634
	11	82-Pb-207	2823	3600
	12	82-Pb-208	2824	2787
		(Total	35314)	
205	1	90-Th-228	2901	1549
	2	90-Th-230	2902	1657
	3	90-Th-232	2903	4881
	4	90-Th-233	2904	1802
	5	90-Th-234	2905	1873
	6	91-Pa-233	2911	1316
	7	92-U -233	2921	3160
	8	92-U -234	2922	1184
	9	92-U -235	2923	6307
	10	92-U -236	2924	1882
	11	92-U -238	2925	3907
	12	93-Np-237	2931	3024
	13	93-Np-239	2932	898
		(Total	33440)	
206	1	94-Pu-236	2941	1012
	2	94-Pu-238	2942	1696
	3	94-Pu-239	2943	4862
	4	94-Pu-240	2944	2746
	5	94-Pu-241	2945	2683
	6	94-Pu-242	2946	1675
	7	95-Am-241	2951	4059
	8	95-Am-242	2952	1591
	9	95-Am-242m	2953	3039
	10	95-Am-243	2954	2541
	11	96-Cm-242	2961	902
	12	96-Cm-243	2962	4129
	13	96-Cm-244	2963	1279
	14	96-Cm-245	2964	2811
		(Total	35025)	

Table 2 Resonance Region and Formula

Nuclide	MAT	Spin	Resolved Res. (Formula)	Unresolved Res.
1-H - 1	2011	1/2+	no resonances	
1-H - 2	2012	1+	no resonances	
3-Li- 6	2031	1+	no resonances	
3-Li- 7	2032	3/2-	no resonances	
4-Be- 9	2041	3/2-	no resonances	
5-B - 10	2051	3+	no resonances	
6-C - 12	2061	0+	no resonances	
9-F - 19	2091	1/2+	10 ⁻⁵ eV - 100 keV (SL)	not given
11-Na- 23	2111	3/2+	500 eV - 150 keV (ML)	not given
13-Al- 27	2131	5/2+	3 keV - 140 keV (ML)	not given
14-Si- 0	2140		no resonances	
20-Ca- 0	2200		10 ⁻⁵ eV - 400 keV (ML)	not given
20-Ca- 40	2201	0+	10 ⁻⁵ eV - 400 keV (ML)	not given
20-Ca- 42	2202	0+	10 ⁻⁵ eV - 400 keV (ML)	not given
20-Ca- 43	2203	7/2-	10 ⁻⁵ eV - 30 keV (ML)	not given
20-Ca- 44	2204	0+	10 ⁻⁵ eV - 400 keV (ML)	not given
20-Ca- 46	2205	0+	no resonances	
20-Ca- 48	2206	0+	10 ⁻⁵ eV - 400 keV (ML)	not given
21-Sc- 45	2211	7/2-	10 ⁻⁵ eV - 90 keV (ML*)	not given
23-V - 51	2231	7/2-	10 ⁻⁵ eV - 100 keV (ML*)	not given
24-Cr- 0	2240		10 ⁻⁵ eV - 300 keV (ML)	not given
24-Cr- 50	2241	0+	10 ⁻⁵ eV - 300 keV (ML)	not given
24-Cr- 52	2242	0+	10 ⁻⁵ eV - 300 keV (ML)	not given
24-Cr- 53	2243	3/2-	10 ⁻⁵ eV - 120 keV (ML)	not given
24-Cr- 54	2244	0+	10 ⁻⁵ eV - 300 keV (ML)	not given
25-Mn- 55	2251	5/2-	10 ⁻⁵ eV - 100 keV (ML)	not given
26-Fe- 0	2260		10 ⁻⁵ eV - 250 keV (ML*)	not given
26-Fe- 54	2261	0+	10 ⁻⁵ eV - 250 keV (ML)	not given
26-Fe- 56	2262	0+	10 ⁻⁵ eV - 250 keV (ML)	not given
26-Fe- 57	2263	1/2-	10 ⁻⁵ eV - 200 keV (ML*)	not given
26-Fe- 58	2264	0+	10 ⁻⁵ eV - 100 keV (ML)	not given
27-Co- 59	2271	7/2-	10 ⁻⁵ eV - 100 keV (ML*)	not given
28-Ni- 0	2280		10 ⁻⁵ eV - 600 keV (ML*)	not given
28-Ni- 58	2281	0+	10 ⁻⁵ eV - 600 keV (ML)	not given
28-Ni- 60	2282	0+	10 ⁻⁵ eV - 600 keV (ML)	not given
28-Ni- 61	2283	3/2-	10 ⁻⁵ eV - 68.5158keV (ML*)	not given
28-Ni- 62	2284	0+	10 ⁻⁵ eV - 600 keV (ML)	not given
28-Ni- 64	2285	0+	10 ⁻⁵ eV - 600 keV (ML)	not given
29-Cu- 0	2290		10 ⁻⁵ eV - 35 keV (ML*)	not given
29-Cu- 63	2291	3/2-	10 ⁻⁵ eV - 35 keV (ML*)	not given
29-Cu- 65	2292	3/2-	10 ⁻⁵ eV - 35 keV (ML*)	not given
41-Nb- 93	2411	9/2+	10 ⁻⁵ eV - 7 keV (ML*)	50 keV
42-Mo- 0	2420		10 ⁻⁵ eV - 50 keV (ML*)	100 keV
42-Mo- 92	2421	0+	10 ⁻⁵ eV - 50 keV (ML)	100 keV
42-Mo- 94	2422	0+	10 ⁻⁵ eV - 20 keV (ML)	100 keV
42-Mo- 95	2423	5/2+	10 ⁻⁵ eV - 2 keV (ML*)	100 keV
42-Mo- 96	2424	0+	10 ⁻⁵ eV - 19 keV (ML)	100 keV
42-Mo- 97	2425	5/2+	10 ⁻⁵ eV - 1.8 keV (ML*)	100 keV
42-Mo- 98	2426	0+	10 ⁻⁵ eV - 32 keV (ML)	100 keV
42-Mo-100	2427	0+	10 ⁻⁵ eV - 26 keV (ML)	100 keV

Table 2 (continued.)

Nuclide	MAT	Spin	Resolved Res. (Formula)	Unresolved Res.
72-Hf-174	2721	0+	0.5 eV - 220 eV (ML)	50 keV
72-Hf-176	2722	0+	0.5 eV - 700 eV (ML)	50 keV
72-Hf-177	2723	7/2-	0.5 eV - 250 eV (ML*)	50 keV
72-Hf-178	2724	0+	0.5 eV - 1.5 keV (ML)	50 keV
72-Hf-179	2725	9/2+	0.5 eV - 250 eV (ML*)	50 keV
72-Hf-180	2726	0-	0.5 eV - 2.5 keV (ML)	50 keV
73-Ta-181	2731	7/2+	10 ⁻⁵ eV - 1 keV (ML*)	50 keV
82-Pb-0	2820		10 ⁻⁵ eV - 500 keV (ML)	not given
82-Pb-204	2821	0+	10 ⁻⁵ eV - 50 keV (ML)	not given
82-Pb-206	2822	0+	10 ⁻⁵ eV - 200 keV (ML)	not given
82-Pb-207	2823	1/2-	10 ⁻⁵ eV - 500 keV (ML)	not given
82-Pb-208	2824	0+	10 ⁻⁵ eV - 800 keV (ML)	not given
90-Th-228	2901	0+	10 ⁻⁵ eV - 7.798 eV (ML)	not given
90-Th-230	2902	0+	10 ⁻⁵ eV - 564.26 eV (ML)	not given
90-Th-232	2903	0+	10 ⁻⁵ eV - 3.5 keV (ML)	50 keV
90-Th-233	2904	1/2+	no resonances	
90-Th-234	2905	0+	no resonances	
91-Pa-233	2911	3/2-	2.38 eV - 17 eV (SL)	1 keV
92-U-233	2921	5/2+	1.0 eV - 100 eV (SL)	30 keV
92-U-234	2922	0+	10 ⁻⁵ eV - 215 eV (ML)	not given
92-U-235	2923	7/2-	1.0 eV - 100 eV (SL)	30 keV
92-U-236	2924	0+	10 ⁻⁵ eV - 1.5 keV (ML)	not given
92-U-238	2925	0+	10 ⁻⁵ eV - 4 keV (ML)	50 keV
93-Np-237	2931	5/2+	10 ⁻⁵ eV - 130 eV (SL)	30 keV
93-Np-239	2932	5/2+	no resonances	
94-Pu-236	2941	0+	10 ⁻⁵ eV - 6 eV (SL)	not given
94-Pu-238	2942	0+	10 ⁻⁵ eV - 500 eV (ML)	not given
94-Pu-239	2943	1/2+	1.0 eV - 598 eV (ML*)	30 keV
94-Pu-240	2944	0+	10 ⁻⁵ eV - 4 keV (ML)	40 keV
94-Pu-241	2945	5/2+	1.0 eV - 100 eV (SL)	30 keV
94-Pu-242	2946	0+	10 ⁻⁵ eV - 1.29 keV (ML)	not given
95-Am-241	2951	5/2-	10 ⁻⁵ eV - 150 eV (ML*)	30 keV
95-Am-242	2952	1-	no resonances	
95-Am-242m	2953	5-	10 ⁻⁵ eV - 3.5 eV (SL)	not given
95-Am-243	2954	5/2-	10 ⁻⁵ eV - 215 eV (ML*)	30 keV
96-Cm-242	2961	0+	10 ⁻⁵ eV - 275 eV (ML)	not given
96-Cm-243	2962	5/2+	10 ⁻⁵ eV - 27 eV (RM*)	not given
96-Cm-244	2963	0+	10 ⁻⁵ eV - 1 keV (ML)	not given
96-Cm-245	2964	7/2+	10 ⁻⁵ eV - 60 eV (SL)	not given

SL : Single-level Breit-Wigner formula.

ML : Multilevel Breit-Wigner formula.

RM : Reich-Moore multilevel formula.

* : There exist resonances of which J value is unknown. The resonance cross sections should be calculated with RESENDD.

Table 3 JENDL-2 (Revision-1) Pointwise Files

Tape No.	No.	Nuclide	MAT number	Records
251	1	1-H - 1	2011	249
	2	1-H - 2	2012	4623
	3	3-Li- 6	2031	698
	4	3-Li- 7	2032	610
	5	4-Be- 9	2041	545
	6	5-B - 10	2051	1856
	7	6-C - 12	2061	1178
	8	9-F - 19	2091	1514
	9	11-Na- 23	2111	2640
	10	13-Al- 27	2131	1328
	11	14-Si- 0	2140	2117
	12	20-Ca- 0	2200	11399
	13	20-Ca- 40	2201	6783
	14	20-Ca- 42	2202	5116
	15	20-Ca- 43	2203	2713
	16	20-Ca- 44	2204	3610
	17	20-Ca- 46	2205	629
	18	20-Ca- 48	2206	1053
			(Total	48661)
252	1	21-Sc- 45	2211	14497
	2	23-V - 51	2231	5796
	3	24-Cr- 0	2240	10630
	4	24-Cr- 50	2241	7283
	5	24-Cr- 52	2242	7520
	6	24-Cr- 53	2243	4052
	7	24-Cr- 54	2244	5438
			(Total	55216)
253	1	25-Mn- 55	2251	12420
	2	26-Fe- 0	2260	16075
	3	26-Fe- 54	2261	3923
	4	26-Fe- 56	2262	10162
	5	26-Fe- 57	2263	4921
	6	26-Fe- 58	2264	2470
	7	27-Co- 59	2271	15448
			(Total	65419)
254	1	28-Ni- 0	2280	23058
	2	28-Ni- 58	2281	15734
	3	28-Ni- 60	2282	12653
	4	28-Ni- 61	2283	8263
	5	28-Ni- 62	2284	9837
	6	28-Ni- 64	2285	7665
			(Total	77210)

Table 3 (continued)

Tape No.	No.	Nuclide	MAT number	Records
255	1	29-Cu- 0	2290	5528
	2	29-Cu- 63	2291	4901
	3	29-Cu- 65	2292	3879
	4	41-Nb- 93	2411	20915
	5	42-Mo- 0	2420	36674
			(Total	71897)
256	1	42-Mo- 92	2421	10865
	2	42-Mo- 94	2422	9020
	3	42-Mo- 95	2423	7899
	4	42-Mo- 96	2424	11714
	5	42-Mo- 97	2425	9044
	6	42-Mo- 98	2426	19043
	7	42-Mo-100	2427	18711
			(Total	86296)
257	1	72-Hf-174	2721	4172
	2	72-Hf-176	2722	6408
	3	72-Hf-177	2723	9617
	4	72-Hf-178	2724	6918
	5	72-Hf-179	2725	6637
	6	72-Hf-180	2726	5576
	7	73-Ta-181	2731	19543
			(Total	58871)
258	1	82-Pb- 0	2820	14750
	2	82-Pb-204	2821	6589
	3	82-Pb-206	2822	10144
	4	82-Pb-207	2823	9336
	5	82-Pb-208	2824	4426
			(Total	45245)
259	1	90-Th-228	2901	1917
	2	90-Th-230	2902	8156
	3	90-Th-232	2903	60674
	4	90-Th-233	2904	1802
	5	90-Th-234	2905	1873
	6	91-Pa-233	2911	2792
			(Total	77214)
260	1	92-U -233	2921	5934
	2	92-U -234	2922	5861
	3	92-U -235	2923	12839
	4	92-U -236	2924	22484
			(Total	47118)
261	1	92-U -238	2925	73607
	2	93-Np-237	2931	17079
	3	93-Np-239	2932	898
			(Total	91584)

Table 3 (continued)

Tape No.	No.	Nuclide	MAT number	Records
262	1	94-Pu-236	2941	1301
	2	94-Pu-238	2942	10455
	3	94-Pu-239	2943	23240
	4	94-Pu-240	2944	46408
				(Total
263	1	94-Pu-241	2945	5891
	2	94-Pu-242	2946	18636
	3	95-Am-241	2951	18743
	4	95-Am-242	2952	1591
	5	95-Am-242m	2953	3192
			(Total	48053)
264	1	95-Am-243	2954	21267
	2	96-Cm-242	2961	3664
	3	96-Cm-243	2962	5219
	4	96-Cm-244	2963	15295
	5	96-Cm-245	2964	4475
			(Total	49920)

Descriptive Data

Full listings of descriptive data of JENDL-2 (Rev1) are given. Characters of them were converted from capital letters to a normal style of mixture of capital and small letters. To output them, the ATF (Advanced Text Formatter for science) system of the FACOM-M 380 computer was used.

1-H - 1 MAT number = 2011

1-H - 1 Hitachi Eval-Apr76 M.Yamamoto
JAERI-1261 Dist-Mar83 Rev1-Nov83

History

83-03 Compiled by K.Shibata

Main part was carried over from JENDL-1 data evaluated by M.Yamamoto. Details are given in ref. /1/.

83-11 MF=2 was added. The transformation matrix given for MT=2 of MF=4.

MF=1 General Information

MT=451 Descriptive Data and Dictionary

MF=2 Resonance Parameters

MT=151 Scattering radius only

2200-m/s cross sections and calculated res. integrals.

	2200-m/s	res. integ.
elastic	20.44 b	-
capture	0.332 b	0.149 b
total	20.77 b	-

MF=3 Neutron Cross Sections

MT=1 Total Cross Section

Sum of elastic and capture cross sections

MT=2 Elastic Scattering Cross Section

Below 100 keV, calculated by using effective range and scattering length parameters of Lomon and Wilson/2/. Above 100 keV, the data of Hopkins and Breit/3/ were recommended.

MT=102 Capture Cross Section

The data of Horsley/4/ were recommended.

MT=251 Mu-bar

Calculated from the data in MF=4.

MF=4 Angular Distributions of Secondary Neutrons

MT=2

Below 100 keV, isotropic in the center of mass system was assumed. Above 100 keV, the data of hopkins and breit/3/ were recommended.

References

- 1) Igarasi S. et al.: JAERI-1261 (1979).
- 2) Lomon E. and Wilson R.: Phys. Rev. C9(1974) 1392.
- 3) Hopkins J.C. and Breit G.: Nucl. Data Table A9(1971) 137.
- 4) Horsley A.: Nucl. Data A2(1966) 243.

1-H - 2 MAT number = 2012

1-H - 2 JAERI Eval-Jul82 K.Shibata,T.Narita,S.Igarasi
 JAERI-M 83-006 Dist-Mar83 Rev1-Nov83

History

83-01 New evaluation for JENDL-2. Details are given in Ref. /1/.
 Data were compiled by the authors.
 83-11 MF=2 was added.

MF=1 General Information

MT=451 Descriptive data and dictionary

MF=2 Resonance Parameters

MT=151 Scattering radius only

2200-m/s cross sections and calculated res. integrals.

	2200-m/s		res. integ.
elastic	3.389	b	-
capture	0.00055	b	0.000286 b
total	3.390	b	-

MF=3 Neutron Cross Sections

MT=1 Total

Based on a least-squares fit to the experimental data of
 /2/-/8/.

MT=2 Elastic

Elastic = Total - (n,2n) - Capture.

MT=16 (n,2n)

Based on a least-squares fit.
 Data listed in /9/-/11/ were used.

MT=102 Capture

Below 1 keV, $1/v$ form normalized to the data of
 Ishikawa /12/.
 Above 1 keV, evaluated on the basis of the inverse
 reaction /13/.

MT=251 Mu-bar

Calculated from the data in MF=4.

MF=4 Angular Distributions of Secondary Neutrons

MT=2,16

Calculated from the three-body model based on
 the Faddeev equation /14/.

MF=5,6 Energy and Energy-Angular Distributions of Secondary
 Neutrons

MT=16 The three-body model calculation.

References

- 1) Shibata, K. et al.: JAERI-M 83-006 (1983).
- 2) Adair, R.K. et al.: Phys. Rev. 89 (1953) 1165.
- 3) Seagrave, J.D. and Henkel, R.L.: Phys. Rev. 98 (1955) 666.
- 4) Stoler, P. et al.: Phys. Rev. C8 (1973) 1539.
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- 6) Dilg, W. et al. : Phys. Lett. 36B (1971) 208.
- 7) Clement, J.M. et al. : Nucl. Phys. A183 (1972) 51.
- 8) Foster, Jr., D.G. and Glasgow, D.W. : Phys. Rev. C3(1971)576.
- 9) Holmberg, M. : Nucl. Phys. A129 (1969) 327.
- 10) Pauletta, G. and Brooks, F.D. : Nucl. Phys. A255 (1975) 267.
- 11) Catron, H.C. et al. : Phys. Rev. 123 (1961) 218.
- 12) Ishikawa, H. : Nucl. Instr. Meth. 109 (1973) 493.
- 13) Gunn, J.C. and Irving, J. : Phil. Mag. 42 (1951) 1353.
- 14) Ebenhoh, W. : Nucl. Phys. A191 (1972) 97.

3-Li- 6 MAT number = 2031

3-Li- 6 JAERI Eval-Jul77 S.Komoda,S.Igarasi
 JAERI-M-7148 Dist-Mar83 Rev1-Nov83

History

77-01 New evaluation for JENDL-1. Details given in Ref. /1/.
 81-12 Partly revised by S.Komoda /2/ for JENDL-2, and compiled
 by T.Nakagawa.
 83-11 Comment data were added.

MF=1 General Information

MT=451 Descriptive data and dictionary

MF=2 Resonance Parameters

MT=151 No resonance parameters given. Scattering radius only.

2200-m/s cross sections and calculated res. integrals

	2200-m/s	res.integ.
elastic	0.736 b	-
capture	0.028 b	0.0126 b
(n,alpha)	936.3 b	423. b
total	937.1 b	-

MF=3 Neutron Cross Sections

MT=1 Total

Sum of all the partial cross sections.

MT=2 Elastic

Calculated with the Kapur-Peierls theory. Details given
 in Ref. /1/. Between 2 and 6 MeV, based on the experi-
 mental data by Knitter et al. /5/ and Lane et al. /6/.

MT=4 Total inelastic

Sum of MT=52 and 91.

MT=52 Inelastic (discrete)

Based on the data of Presser et al. /3/.

MT=102 Capture

The thermal cross section of Bartholemew and Campion /4/
 was extrapolated as $1/v$ up to 20MeV.

MT=107 (n,alpha)

Calculated with the Kapur-Peierls theory. Details given
 in Ref. /1/.

MT=24,91,103 (n,2n alpha)p, inelastic(cont), (n,p)

The data of ENDF/B-IV are recommended.

MT=251 Mu-bar

Calculated from the data in MF=4.

MF=4 Angular Distributions of Secondary Neutrons

MT=2 Based on the experimental data /5/-/8/.

MT=24 Isotropic in the lab system.

MT=52 Isotropic in the center-of-mass system.

MT=91 ENDF/B-IV recommended.

MF=5 Energy Distributions of Secondary Neutrons

MT=24,91 Evaporation spectrum.

Values of nuclear temperature were taken from
ENDF/B-IV.

References

- 1) Komoda, S. and Igarasi, S.: JAERI-M 7148 (1977).
Komoda, S. and Igarasi, S.: J. Nucl. Sci. Technol. 15 (1978)
79.
- 2) Komoda, S.: private communication.
- 3) Presser, G. et al.: Nucl. Phys. A3 (1969) 679.
- 4) Bartholmew, G.A. and Campion, P.J.: Can. J. Phys. 35(1957)1347
- 5) Knitter, H.-H. et al.: EUR 5726E (1977).
- 6) Lane, R.O. et al.: Lowell Conf. (1976).
- 7) Cookson et al.: Nucl. Phys. A91 (1967) 273.
- 8) Hyakutake et al.: J. Nucl. Sci. Technol. 11 (1974) 407.

MT=51

Isotropic in the center-of-mass system.

MF=5 Energy Distributions of Secondary Neutrons

MT=16,24,91

Evaporation spectrum.

Values of nuclear temperature taken from ENDF/B-IV.

References

- 1) Hibdon, C.T. and Langsdorf, Jr., A. : ANL-5171, p.7 (1954).
- 2) Hibdon, C.T. and Mooring, F.P. : '68 Washington Conf.
- 3) Meadows, J.W. and Whalen, J.F. : Nucl. Sci. Eng. 41 (1970) 351.
- 4) Foster, Jr., D.G. and Glasgow, D.W. : Phys. Rev. C3 (1971) 576.
- 5) Goulding, C.A. et al. : private communication (1972).
- 6) Lamaze, G.P. et al. : Bull. Am. Phys. Soc. 24 (1979) 862.
- 7) Benveniste et al. : Nucl. Phys. 38 (1962) 300.
- 8) Presser, G. and Bass, R. : Nucl. Phys. A182 (1972) 321.
- 9) Wyman, M.E. and Thorpe, M.M. : LA-2235 (1958).
- 10) Brown, F. et al. : J. Nucl. Energy Parts A/B 17 (1963) 137.
- 11) Hopkins, J.C. et al. : Nucl. Phys. A107 (1968) 139.
- 12) Lisowski, P.W. et al. : LA-8342 (1980).
- 13) Smith, D.L. et al. : Nucl. Sci. Eng. 78 (1981) 359.
- 14) Liskien, H. and Paulsen, A. : INDC(EUR) 014/G, p.14 (1980).
- 15) Journey, E.T. : USNDC-9, p.109 (1973).
- 16) Lane, R.O. et al. : Ann. Phys. 12 (1961) 135.
- 17) Hogue, H.H. et al. : Nucl. Sci. Eng. 69 (1979) 22.
- 18) Knox, H.D. et al. : Nucl. Sci. Eng. 69 (1979) 223.
- 19) Watson, B.A. et al. : Phys. Rev. 182 (1969) 977.

4-Be- 9 MAT number = 2041

4-Be- 9 JAERI+ Eval-Sep82 K.Sibata,K.Ioki (MAPI)
 Dist-Mar83 Rev1-Nov83

History

82-09 New evaluation was made by K.Sibata (JAERI) and K.Ioki (MAPI)
 83-11 Comment was added.

MT=1 General Information

MT=451 Descriptive data

MT=2 Resonance Parameters

MT=151 Scattering radius only

2200-m/sec cross sections and resonance integrals.

	2200 m/sec	res. integ.
elastic	6.000 b	-
capture	0.0076 b	3.42 milli-b
total	6.0076 b	-

MT=3 Neutron Cross Sections

MT=1 Total

Below 1 keV, Total = 6.0 + Capture (b).
 Above 1 keV, data listed in /1/-/10/ were used.

MT=2 Elastic

Elastic = Total - Reaction.

MT=16 (n,2n)

Data listed in /11/-/15/ were used.

MT=102 Capture

1/v form normalized to the data of Jurney /16/.

MT=103 (n,p)

Evaluated on the basis of the data of Augustson and Menlove /17/ by taking account of the branching ratio of 35 percent for $Li9 \Rightarrow Be9^* \Rightarrow 2\alpha + n$.

MT=104 (n,d)

Based on the data of Scoebel /18/.

MT=105 (n,t)

Based on the data of Biro et al. /19/ and Qaim and Wolfle /20/.

MT=107 (n,alpha)

Data listed in /21/-/25/ were used.
 Only the transition to the ground state in He6 is given.

MT=251 Mu-bar

Calculated from the data in File4.

MT=4 Angular Distributions of Secondary Neutrons

MT=2

- 1.0E-5 eV to 40 keV : Isotropic in the center-of-mass sys.
 50 keV to 14 MeV : Data listed in /26/-/31/ used.
 15 MeV to 20 MeV : Optical model calculation with
 parameters of Ref./32/.

MT=16

Isotropic in the laboratory system.

MT=5 Energy Distributions of Secondary Neutrons

MT=16

Evaporation spectrum.

References

- 1) Adair, R.K. et al. : Phys. Rev. 75 (1949) 1124.
- 2) Bockelman, C.K. : Phys. Rev. 80 (1950) 1011.
- 3) Bockelman, C.K. et al. : Phys. Rev. 84 (1951) 69.
- 4) Hibdon, C.T. and Langsdorf, Jr., A. : Phys. Rev. 98 (1955) 223.
- 5) Fowler, J.L. and Cohn, H.O. : Bull. Am. Phys. Soc. 4(1959)385.
- 6) Bilpuch, E.G. et al. : private communication, 1962.
- 7) Schwartz, R.B. et al. : Bull. Am. Phys. Soc. 16 (1971) 495.
- 8) Foster, Jr., D.G. and Glasgow, D.W. : Phys. Rev. C3(1971)576.
- 9) Cabe, J. and Cance, M : CEA-R-4524, 1973.
- 10) Auchampaugh, G.F. et al. : Nucl. Sci. Eng. 69 (1979) 30.
- 11) Ashby, V.J. et al. : Phys. Rev. 111 (1958) 616.
- 12) Catron, H.C. et al. : Phys. Rev. 123 (1961) 218.
- 13) Holmberg, M. and Hansen, J. : Nucl. Phys. A129 (1969) 305.
- 14) Bloser, M. : Atomkernenergie 20 (1972) 309.
- 15) Drake, D.M. et al. : Nucl. Sci. Eng. 63 (1977) 401.
- 16) Journey, E.T. : USNDC-11, p.149, 1974.
- 17) Augustson, R.H. and Menlove, H.O : Nucl. Sci. Eng. 54(1974)190
- 18) Scoebel, W. : Z. Naturforsch. A24 (1969) 289.
- 19) Biro, T. et al. : J. Inorg. Nucl. Chem. 37 (1975) 1583.
- 20) Qaim, S.M. and Wolfle, R. : Nucl. Phys. A295 (1978) 150.
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- 23) Bass, R. et al. : Nucl. Phys. 23 (1961) 122.
- 24) Paic, G. et al. : Nucl. Phys. A96 (1967) 476.
- 25) Perroud, J.P. and Sellem, CH. : Nucl. Phys. A227 (1974) 330.
- 26) Lane, R.O. et al. : Phys. Rev. 133B (1964) 409.
- 27) Lane, R.O. et al. : Ann. Phys. 12 (1961) 135.
- 28) Levin, J.S. and Cranberg, L. : private communication, 1960.
- 29) Phillips, D.D. : private communication, 1961.
- 30) Marion, J.B. et al. : Phys. Rev. 114 (1959) 1584.
- 31) Hogue, H.H. et al. : Nucl. Sci. Eng. 68 (1978) 38.
- 32) Agee, F.P. and Rosen, L. : LA-3538-MS, 1966.

5-B - 10 MAT number = 2051

5-B - 10 Hitachi Eval-Apr76 M.Yamamoto
 JAERI-1261 Dist-Mar83 Rev1-Nov83

History

76-01 Evaluation was made for JENDL-1 by M.Yamamoto. Details are given in Ref. /1/.

83-03 JENDL-2 data were taken from JENDL-1.

83-11 Comment was added.

MF=1 General Information

MT=451 Comments and Dictionary

MF=2 Resonance Parameters

MT=151 Scattering radius only

2200-m/sec cross sections and resonance integrals

	2200 m/sec	res. integ.
elastic	2.173 b	-
capture	0.503 b	0.0643 b
(n,alpha)	3836. b	1720. b
(n,t 2alpha)	0.566 milli-b	0.234 b
total	3839. b	-

MF=3 Neutron Cross Sections

MT=1 Total

Sum of partial cross sections

MT=2 Elastic scattering

Below 580 keV, calculated from the resonance parameters in BNL-325, 3rd ed. /2/. Above 580 keV, ENDF/B-IV recommended.

MT=4 Total inelastic

Sum of MT=51 to 91.

MT=16 (n,2n)

A straight line passing through the data of Mather and Pain /3/ was assumed.

MT=51-61,91,103,104,113 inelastic, (n,p), (n,d) and (n,t2a)

ENDF/B-IV recommended.

MT=102 Capture

1/v curve normalized to the recommended value of Ref./2/.

MT=107,780,781 (n,a), (n,a0) and (n,a1)

Below 235 keV, based on the measured data of Sowerby et al. /4/. Above 235 keV, ENDF/B-IV recommended.

MT=113 (n,t 2a)

ENDF/B-IV recommended.

MT=251 Mu-bar

ENDF/B-IV recommended.

MF=4 Angular Distributions of Secondary Neutrons

MT=2.16,51-61,91

ENDF/B-IV recommended.

MF=5 Energy Distributions of Secondary Neutrons

MT=16,91

ENDF/B-IV recommended.

References

- 1) Igarasi S. et al.: JAERI-1261 (1979).
- 2) Mughabghab S.F. and Garber D.I.: BNL-325, 3rd Edition (1973).
- 3) Mather D.S. and Pain L.F.: AWRE 047/69 (1969).
- 4) Sowerby M.G. et al.: AWRE-6316 (1970).

6-C - 12 MAT number = 2061

6-C - 12 Hitachi Eval-Apr76 M.Yamamoto
JAERI-1261 Dist-Mar83

History

76-04 Recommendation was made by M.Yamamoto (Hitachi) for
JENDL-1. Details given in Ref./1/.

83-03 Main part of JENDL-2 data was carried over from JENDL-1.

83-11 Comment was added.

MF=1 General Information

MT=451 Comments and dictionary

MF=2 Resonance Parameters

MT=151 Scattering radius only

2200-m/sec cross sections and resonance integrals

	2200-m/sec	res. integ.
elastic	4.699 b	-
capture	0.0034 b	0.00153 b
total	4.702 b	-

MF=3 Neutron Cross Sections

MT=1 Total

Sum of partial cross sections.

MT=2 Elastic scattering

Below 2 MeV, based on the evaluated data of Nishimura et al.
/2/. Above 2 MeV, ENDF/B-IV recommended.

MT=4 Total inelastic

sum of MT=51 and 91.

MT=51,91,107 Inelastic scattering and (n,a)

ENDF/B-IV recommended.

MT=102 Capture

1/v curve normalized to the recommended value of BNL-325
3rd edition/3/.

MT=251 Mu-bar

ENDF/B-IV recommended.

MF=4 Angular Distributions of Secondary Neutrons

MT=2,51

ENDF/B-IV recommended.

MT=91

Isotropic distributions in the center-of-mass system were
assumed, and transformed into the laboratory system.

MF=5 Energy Distributions of Secondary Neutrons

MT=91

ENDF/B-IV recommended.

References

- 1) Igarasi S. et al.: JAERI-1261 (1979).
- 2) Nishimura K. et al.: JAERI-1218 (1971).
- 3) Mughabghab S.F. and Garber D.I.: BNL-325, 3rd Edition (1973).

9-F - 19 MAT number = 2091

9-F - 19 JAERI Eval-Apr77 T.Sugi and K.Nishimura
 JAERI-M 7253(1977) Dist-Mar83 Rev1-Nov83

History

77-04 Data above 100 keV were evaluated by T.Sugi and K.Nishimura (JAERI). Details are given in Ref. /1/.
 83-01 Resonance parameters were evaluated by T.Sugi.
 83-11 Modification of angular distributions was made. Comment data were added in MF=1.

MF=1 General Information

MT=451 Descriptive data and dictionary

MF=2 Resonance Parameters

MT=151 Resolved resonance parameters : 1.0E-5 eV - 100 keV
 The single-level Breit-Wigner formula was used.
 Res. energis and Gam-n : The first three levels were based on Johnson et al. /2/. The 4th level was based on Mughabghab and Garber /3/.
 Gam-g : The first three levels were based on Macklin and Winters /4/. The 4th level was taken from the mean value of Macklin and Winters /4/, and Gabbard et al. /5/.
 J : Based on Mughabghab and Garber /3/.

Calculated 2200-m/s cross sections and res. integrals.

	2200 m/s	res. integ.
elastic	3.641 b	-
capture	9.6 milli-b	19.6 milli-b
total	3.651 b	-

MF=3 Neutron Cross Sections

Below 100 keV

Background data are given.

Above 100 keV

MT=1 Total cross section

Between 100 keV and 5.0 keV, evaluated based on the following experimental data.

Energy range	Experiments
100keV - 300keV	Hibdon /7/
300keV - 500keV	Whalen et al. /8/
500keV - 1.15MeV	Cabe /9/
1.15MeV - 2.2MeV	Elwyn /10/
2.2MeV - 5.0 MeV	Foster and Glasgow /11/

5.0MeV - 8.5MeV : Determined from the least-squares fitting of the experimental data. See Ref. /1/.

8.5MeV - 20MeV : Calculated with the optical model by using the code ELIESE-3 /12/. The optical potential parameters were determined with the code TOTALCS /13/ so that the calculated cross section curve is fitted to the experimental data from 3.1 MeV to 20 MeV.

Optical potential parameters

$$V = 45.54 - 0.733 * E \quad (\text{MeV}),$$

$W_s = 15.53$ (der. Woods-Saxon) (MeV),
 $V_{so} = 10.0$ (MeV),
 $r_0 = r_s = r_{so} = 1.31$ (fm),
 $a = a_{so} = 0.66$ (fm),
 $b = 0.47$ (fm).

MT=2 Elastic scattering cross section

Derived by subtracting the nonelastic from the total cross section.

MT=3 Nonelastic (not given in file)

1.0E-5 - 6MeV : Sum of all cross sections other than elastic scattering.

6MeV - 20MeV : Calculated with the Hauser-Feshbach method (ELIESE-3 /12/).

MT=4 Total inelastic scattering cross section

Up to 1 MeV : Sum of the inelastic scattering cross sections for the lowest two levels of 110 keV and 197 keV.

1MeV - 5.5MeV : Calculated with the Hauser-Feshbach method (ELIESE-3 /12/). The optical potential parameters are

$V = 51.56 - 1.492E$ (MeV),

$W_s = 11.82$ (der. Woods-Saxon) (MeV).

The other parameters are the same as those for the total cross section. These parameters were determined so that the calculated total cross section curve is fitted to the experimental data from 0.61 MeV to 20 MeV.

5.5MeV - 20MeV : Derived by subtracting the (n,alpha), (n,p), (n,d), (n,t), (n,n'alpha), (n,alpha n'), (n,n'p), (n,p n'), (n,2n) and capture cross sections from the nonelastic.

MT=16 (n,2n) cross section

Calculated by fitting the Pearlstein's function /14/ to the experimental data.

MT=22 (n,n' alpha) and (n.alpha n') cross sections

Calculated with a statistical model by using Pearlstein's empirical formula.

MT=28 (n,n' p) and (n,p n') cross sections

Calculated with a statistical model by using Pearlstein's empirical formula.

MT=51-56 Inelastic for the lowest six excited states

Up to 1MeV : Based on the experimental data of Broder et al. /16/.

1MeV - 5.5MeV : Calculated with the Hauser-Feshbach method (ELIESE-3 /12/) taking into account (n,alpha) and (n,p) as competing processes. The level scheme of F-19, N-16 0-19 were taken from Ajzenberg-Selove /17/,/18/.

5.5MeV - 20MeV : Ratio of the inelastic scattering cross sections for the lowest six excited states and for the continuum to the total inelastic scattering cross section were calculated with the Hauser-Feshbach method (ELIESE-3 /12/). The level density parameter of 3.609 (1/MeV) /19/ and pairing energy of 2.52 MeV /20/ were used.

MT=91 Inelastic to continuum

Calculated with the same method as MT=51-56, 5.5 MeV - 20 MeV.

MT=102 Capture cross section

100keV - 1.87MeV : Based on the experimental data of

Gabbard et al. /5/.

1.87MeV - 20MeV : Assumed to decrease with $1/v$ law.

MT=103 (n,p) cross section

Up to 9MeV : Based on the experimental data of Bass et al.

/21/.

9MeV - 20MeV : Calculated with the statistical model by using Pearlstein's empirical formula.

MT=104 (n,d) cross section

Calculated with the Pearlstein's empirical formula /15/.

The cross section was normalized to 39.5 milli-barns at 14.4 MeV.

MT=105 (n,t) cross section

Calculated with the Pearlstein's empirical formula /15/.

The cross section was normalized to 15.0 milli-barns at 14.4 MeV.

MT=107 (n,alpha) cross section

Below 9 MeV, Based on the following experimental data;

Up to 4MeV Davis et al. /22/.

4MeV - 5.5MeV Smith et al. /23/.

5.5MeV - 9MeV Bass et al. /21/.

Above 9 MeV, Calculated with the Pearlstein's formula.

MT=251 Average cosine in the laboratory system

Derived from the angular distributions.

MF=4 Angular Distributions of Secondary Neutrons

MT=2

Calculated with optical model (CASTHY /24/).

MT=16,22,28

Assumed to be isotropic in the laboratory system.

MT=51-56

Assumed to be isotropic in the center-of-mass system.

MT=91

Assumed to be isotropic in the center-of-mass system and transformed into the laboratory system.

MF=5 Energy Distributions of Secondary Neutrons

MT=16,22,28,91

Evaporation spectra were given.

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11-Na- 23 MAT number = 2111

11-Na-23 Hitachi Eval-Mar75 M.Yamamoto
JAERI 1261 Dist-Mar83 Rev1-Nov83

History

75-03 Evaluated by M.Yamamoto and compiled by C.G. for JENDL-1 with some modifications. Details are given in Ref. /1/.
83-03 JENDL-1 data were taken for JENDL-2, and MF=5 was modified.
83-11 Q values and MF=4 were corrected.

MF=1 General Information

MT=451 Descriptive data and dictionary

MF=2 Resonance Parameters

MT=151 Resolved resonance parameters

Evaluation was made on the basis of recommended values by Mughabghab and Garber /2/, Paik and Pitterle /3/, and the experimental data by Hockenbury et al. /4/. Resonance cross sections can be obtained with MLBW formula in the energy region from 500 eV to 150 keV.

2200-m/s cross sections and calculated res. integrals.

	2200-m/s	res. integ.
elastic	3.170 b	-
capture	0.530 b	0.329 b
total	3.700 b	-

MF=3 Neutron Cross Sections

Thermal energy region (from $1.0E-5$ eV to 500 eV)

The total and capture cross sections of 3.7 and 0.53 barns were taken from BNL-325 3rd ed. /2/, and the form of $1/v$ was assumed for the capture cross section.

Resonance energy region (from 500 eV to 150 keV)

Small background cross sections were given for the total and capture cross sections to connect smoothly resonance cross sections with those for below and above resonance region.

Above 150 keV

MT=1 Total

Based on the following experimental data.

150 keV - 550 keV : Stelson and Preston /5/

550 keV - 10 MeV : Cierjacks et al. /6/

Above 10 MeV : Glasgow and Foster /7/

MT=2 Elastic scattering

Obtained by subtracting partial cross sections from the total cross section.

MT=4 Total inelastic scattering

Below 4 MeV, summation of partial inelastic scattering cross sections (MT=51 - 57). Above 4 MeV, based on the evaluated data by Schmidt /8/ and the experimental data by Martin and

- Stewart /9/ and Sukhanov and Rakavishnikov /10/.
- MT=51 Inelastic scattering to the first level
Based on the experimental data by Towle and Gilboy /11/,
Chien and Smith /12/, Lind and Day /13/ and Shipley et al.
/14/.
- MT=52-57 Inelastic scattering to the second to 7th levels
Based on the data by Freeman and Montague /15/, Lind and Day
/13/, Towle and Owens /16/ and the evaluated data by Schmidt
/8/.
- MT=91 Inelastic scattering to continuum level
Determined from the total and partial inelastic scattering
cross sections.
- MT=16 (n,2n)
Based on the data by Menlove et al. /17/.
- MT=102 Capture
Based on the data by le Rigoleur et al. /18/.
- MT=103 (n,p)
Based on the data by Williamson /19/, Bass and Saleh /20/
and Picard and Williamson /21/.
- MT=107 (n,α)
Based on the data by Williamson /19/ and Woelfer and Bormann
/22/.
- MT=251 Mu-bar
Obtained from the angular distributions (MF=4,MT=2).
- MF=4 Angular Distributions of Secondary Neutrons
MT=2 Based on the compilation work by Garber et al. /23/,
and evaluation work by Moorhead /24/.
- MT=16 Isotropic in the lab system.
MT=51-57 Isotropic in the center-of-mass system.
MT=91 Isotropic distribution in the center-of-mass system
was transformed into the lab system.
- MF=5 Energy Distributions of Secondary Neutrons
MT=16,91 Evaporation spectrum

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13-A1- 27 MAT number = 2131

13-A1- 27 JAERI Eval-Mar75 JENDL C.G.
 JAERI 1261 Dist-Mar83 Rev1-Nov83

History

75-03 Evaluated for JENDL-1 by JENDL Compilation Group. Details are given in Ref. /1/.

83-03 JENDL-1 data were taken for JENDL-2.

83-11 Angular distributions were modified.

MF=1 General Information

MT=451 Descriptive data and dictionary

MF=2 Resonance Parameters

MT=151 Resolved resonance parameters for MLBW formula

The resonance parameters were taken from BNL-325 3rd edition /2/ and some modifications were made so that the calculated total cross section might satisfactorily reproduce the experimental data. A negative resonance was added.

2200-m/s cross sections and calculated res. integrals.

	2200-m/s	res. integ.
elastic	1.500 b	-
capture	0.230 b	0.147 b
total	1.730 b	-

MF=3 Neutron Cross Sections

Below 3 keV

The 2200-m/s cross sections recommended in Ref. /2/ were adopted. The capture cross section was assumed to have the form of $1/v$ below 500 eV and was estimated by an eye guide between 500 eV and 3 keV. The elastic scattering was assumed to be constant.

Resonance energy region (from 3 keV to 140 keV)

Background cross sections were given to reproduce the resonance structure around 10 keV.

Above 140 keV

MT=1 Total

Obtained with an eye-guide method.

MT=2 Elastic scattering

Obtained by subtracting partial cross sections from the total cross section.

MT=4,51-58,91 Inelastic scattering cross sections

Calculated with optical and statistical models by using the code CASTHY /3/. The following optical potential parameters were determined to reproduce well the total cross section. The capture, (n,p), (n, α) and (n,2n) reactions were taken into account as the competing processes.

Optical potential parameters

$$\begin{aligned}
 V &= 42.39 - 0.18 * E, & W_s &= 4.5, & V_{so} &= 5.8 & (\text{MeV}) \\
 r &= r_{so} = 1.235, & r_s &= 1.137 & & & (\text{fm}) \\
 a &= a_{so} = 0.65, & a_s &= 0.6 & & & (\text{fm})
 \end{aligned}$$

Level scheme

No.	Energy (MeV)	Spin-Parity
g.s.	0.0	5/2 +
1	0.842	1/2 +
2	1.013	3/2 +
3	1.65	5/2 +
4	1.83	5/2 +
5	2.21	7/2 +
6	2.73	5/2 +
7	2.98	3/2 +
8	3.00	9/2 +

Levels above 3.7 MeV were assumed to be overlapping.

MT=16 (n,2n)

Calculated with Pearlstein's method /4/.

MT=102 Capture

Obtained with an eye-guide method.

MT=103 (n,p)

Evaluated data by Asami /5/ were adopted.

MT=107 (n,alpha)

Evaluated data by Kanda and Nakasima /6/ were adopted.

MT=251 Mu-bar

Calculated with optical model.

MF=4 Angular Distributions of Secondary Neutrons

MT=2 Calculated with optical model.

MT=16 Isotropic in the lab system.

MT=51-58 Isotropic in the center-of-mass system.

MT=91 Isotropic distribution in the center-of-mass system was transformed into the lab system.

MF=5 Energy Distributions of Secondary Neutrons

MT=16,91 Evaporation spectrum

References

- 1) Igarasi S. et al.: JAERI 1261 (1979).
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14-Si- 0 MAT number = 2140

14-Si- 0 JAERI Eval-Mar76 T.Asami
JAERI 1261 Dist-Mar83 Rev1-Nov83

History

76-03 The evaluation was made by T.Asami (JAERI) for JENDL-1.

Details are given in Ref. /1/.

83-03 JENDL-1 data were adopted for JENDL-2 and extended to 20 MeV.

83-11 Small correction was made. Comment data were added.

MF=1 General Information

MT=451 Descriptive data and dictionary

MF=2 Resonance Parameters

MT=151 No resonance parameters are given.

2200-m/sec cross sections and calculated resonance integrals.

	2200 m/sec	Res. Integ.
elastic	2.200 b	-
capture	0.156 b	0.079 b
total	2.356 b	-

MF=3 Neutron Cross Sections

Energy region below 1 keV.

MT=1 Total

Sum of the elastic scattering and capture cross sections.

MT=2 Elastic scattering

The constant value of 2.2 barns was taken from Ref. /2/.

MT=102 Capture

The cross section of 0.156 barns at 0.0253 eV was obtained for natural silicon from the following experimental data.

For Si-28 and Si-29: Spitz and Boer /3/.

For Si-30 : Koehler and Knopf /4/, Ryves /5/.

The shape of cross section was assumed to be the form of $1/v$.

Energy region above 1 keV.

MT=1 Total

Obtained by averaging the following experimental data.

Below 200 keV: Fields and Walt /6/.

Above 200 keV: Cierjacks et al. /7/, Schwartz et al. /8/,

Perey et al. /9/, Cabe and Cance /10/.

MT=2 Elastic scattering

Obtained by subtracting partial cross sections from the total cross section.

MT=4,51-83,91 Inelastic scattering

Calculated with a statistical and optical model code CASTHY

/11/. The optical potential parameters of Bhat et al. /12/

was used. The level schemes are listed below. The capture,

(n,p), (n,alpha) and (n,2n) reactions were taken into account as the competing processes.

Level schemes for Si isotopes

No.	Si-28		Si-29		Si-30	
	Energy (MeV)		Energy (MeV)		Energy (MeV)	
g.s.	0.0	0+	0.0	1/2+	0.0	0+
1	1.799	2+	1.273	3/2+	2.235	2+
2	4.617	4+	2.028	5/2+	3.498	2+
3	4.975	0+	2.425	3/2+	3.770	1+
4	6.267	3+	3.067	5/2+	3.788	0+
5	6.691	0+	3.623	7/2-	4.809	2+
6	6.878	3-	4.080	7/2+	4.830	3+
7	6.889	4+	4.741	9/2+	5.230	3+
8	7.381	1+	4.839	1/2+	5.280	4+
9	7.416	2+	4.895	5/2+	5.372	0+
10	7.798	3+	4.933	3/2-	5.487	3-
11	7.935	2-			5.612	2+
12					5.951	4-

Overlapping levels were assumed above 8.25 MeV for Si-28, 5.2 MeV for Si-29 and 6.5 MeV for Si-30.

The Q values of inelastic levels of natural silicon were adjusted to keep the threshold energy of each level.

MT=16 (n,2n)

Constructed from the isotope data evaluated as follows. For Si-28, evaluation was based on the experimental data. For others, the cross section was calculated with Pearlstein's method /13/.

MT=102 Capture

For the energy region from 1 keV to 1.6 MeV, the cross section was calculated from the resonance parameters of Boldeman et al. /14/ and Kenney et al. /15/, and averaged. Then it was renormalized at 1 keV to the $1/v$ cross section mentioned above. Above 1.6 MeV, the cross section was estimated so as to increase and pass through the value of 0.56 milli-barns at 14.1 MeV which was obtained from the experimental data by Cvelber et al. /16/ and Rigaud et al. /17/.

MT=103 (n,p)

Constructed from the isotope data evaluated as follows. Si-28: From 5.0 to 7.8 MeV, the cross section was obtained by eye-guiding the experimental data of Marion et al. /18/ and Jeronymo et al. /19/. The shape of the data of Bass et al. /20/ was adopted, and renormalized by the factor of 1.4 in the energy range from 7.8 MeV to 9.0 MeV. Above 9.0 MeV, the curve was drawn by an eye guide.

Si-29: The shape of the Si-28(n,p) cross section was normalized to 0.120 barns at 14.5 MeV /21,22,23/.

Si-30: Ignored.

MT=107 (n,alpha)

Constructed from the isotope data evaluated as follows. Si-28: Based on the data of Birk et al. /24/, Mainsbridge et al. /25/ and Singh /23/. Si-29: Based on the data of Konijn and Lauber /26/, Birk et al. /24/ and Singh /23/. Si-30: The same shape as the Si-28(n,alpha) was adopted and normalized to 0.070 barns at 14.5 MeV /22,23/.

MT=251 Mu-bar
Calculated with CASTHY /11/.

MF=4 Angular Distributions of Secondary Neutrons

MT=2 Calculated with CASTHY /11/.
MT=16 Isotropic in the laboratory system.
MT=51-88 Isotropic in the center-of-mass system.
MT=91 Isotropic distribution in the center-of-mass system
was transformed into the laboratory system.

MF=5 Energy Distributions of Secondary Neutrons

MT=16,91 Evaporation spectra.

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20-Ca- 0 MAT number = 2200

20-Ca- 0 Mitsui E.S.Eval-Apr80 M.Hatchya
Dist-Mar83 Rev1-Feb84

History

80-04 New evaluation was made by M.Hatchya (Mitsui).
83-11 Ang. Dist. was modified, and comment data were added.
84-02 The total and elastic scattering cross sections were re-evaluated on the basis of experimental data.

MF=1 General Information

MT=451 Descriptive data and dictionary

MF=2 Resonance Parameters

MT=151 Resolved resonance parameters for MLBW formula
Parameters were evaluated on the basis of the following data.

Ca-40 : BNL 325 3rd ed. /1/, Musgrove et al. /2/,
Singh et al. /3/.

Ca-42,43,44 : Musgrove et al. /4/.

Ca-46 : no resonances were given.

Ca-48 : BNL 325 3rd ed. /1/.

Resonance energy region of each isotope is

Ca-40,42,44 : below 400 keV.

Ca-43 : below 30 keV.

Ca-48 : below 500 keV.

Calculated 2200-m/sec cross sections and resonance integrals.

	2200-m/sec	Res.Integ.
elastic	2.963 b	-
capture	0.4307 b	0.226 b
(n.alpha)	0.0024 b	0.349 b
total	3.396 b	-

MF=3 Neutron Cross Sections

Above resonance region.

MT=1 Total cross section

Between 400 keV and 5.0 MeV, the cross section was determined from the experimental data by Perey et al. /5/ and Cierjacks /6/. Above 5.0 MeV, the optical model calculation with CASTHY /7/ was adopted.

Optical potential parameters for Ca-40, 43, 44, 46 and 48 taken from Ref. /8/.

V = 46.72 (MeV),
Ws = 9.13 (MeV),
Vso = 5.37 (MeV),
r0 = rso = 1.26 (fm),
rs = 1.39 (fm),
a = aso = 0.76 (fm),
b = 0.40 (fm).

Optical potential parameters for Ca-42 obtained so as to

2 of Natural Calcium

reproduce the Ca-42 total cross section

$$V = 52.06 - 0.023 \cdot e \quad (\text{MeV}),$$

$$W_s = 5.57 \quad (\text{MeV}),$$

$$V_{so} = 5.37 \quad (\text{MeV}),$$

Others are the same as above parameters.

MT=2 Elastic scattering cross section

Derived by subtracting partial cross sections from the total cross section.

MT=4,51-88,91 Inelastic scattering cross sections

Calculated with optical and statistical model code CASTHY/7/

Level scheme

Level scheme for Ca-40 was taken from Ref./8/ and for other isotopes from Table of Isotopes /9/.
Q-values of natural calcium data were re-calculated from threshold energies.

MT	-Q(keV)	Ca-40	Ca-42	Ca-43	Ca-44	Ca-46	Ca-48
51	372.2	-	-	373 5/2-	-	-	-
52	592.4	-	-	593 3/2-	-	-	-
53	988.7	-	-	990 3/2+	-	-	-
54	1154.5	-	-	-	1157 2+	-	-
55	1342.8	-	-	-	-	1347 2+	-
56	1392.3	-	-	1395 5/2+	-	-	-
57	1522.9	-	1525 2+	-	-	-	-
58	1835.3	-	1837 0+	-	-	-	-
59	1879.4	-	-	-	1884 0+	-	-
60	2278.2	-	-	-	2283 4+	-	-
61	2420.9	-	2424 2+	-	-	-	-
62	2650.8	-	-	-	2657 2+	-	-
63	2749.3	-	2752 4+	-	-	-	-
64	3014.5	-	-	-	-	3024 2+	-
65	3185.8	-	3189 6+	-	-	-	-
66	3441.2	-	3445 3-	-	-	-	-
67	3601.7	-	-	-	-	3613 3-	-
68	3737.3	3737 3-	-	-	-	-	-
69	3816.3	-	-	-	-	-	3832 2+
70	3904.3	3904 2+	-	-	-	-	-
71	4484.9	-	-	-	-	-	4503 4+
72	4488.7	-	-	-	-	-	4507 3-
73	4492.3	4492 5-	-	-	-	-	-
74	4593.3	-	-	-	-	-	4612 3+
75	5249.4	5249 2+	-	-	-	-	-
76	5348.0	-	-	-	-	-	5370 3-
77	5627.4	5627 2+	-	-	-	-	-
78	6285.5	6285 3-	-	-	-	-	-
79	6585.5	6585 3-	-	-	-	-	-
80	6910.5	6910 2+	-	-	-	-	-
81	6932.5	6932 3-	-	-	-	-	-
82	7860.6	7860 2+	-	-	-	-	-
83	7930.6	7930 4+	-	-	-	-	-
84	8090.6	8090 2+	-	-	-	-	-
85	8280.6	8280 2+	-	-	-	-	-

3 of Natural Calcium

86	8371.6	8371	4+	-	-	-	-	-
87	8540.6	8540	2+	-	-	-	-	-
88	8553.6	8553	5-	-	-	-	-	-
91	1928.2	8900	c	3884	c	1931	c	3285
								4463
								6614

Level density parameters (Gilbert and Cameron /10/)

isotope	40	41	42	43	44	45
a (1/MeV)	5.43	6.00	6.58	7.00	7.10	7.12
S-C(1/SQRT(MeV))	2.42	2.59	2.75	2.88	2.95	3.00
Delta(MeV)	3.87	1.83	3.47	1.83	3.27	1.83
Ex (MeV)	10.12	7.99	9.54	7.82	9.18	7.66

isotope	46	47	48	49
a (1/MeV)	7.135	7.075	6.84	7.20
S-C(1/SQRT(MeV))	3.03	3.08	3.07	3.19
Delta(MeV)	3.37	1.83	3.13	1.83
Ex (MeV)	9.131	7.522	8.76	7.39

MT=16 (n,2n) cross section

Based on available data.

MT=22,28 (n,n'alpha) and (n,n'p) cross sections

Derived from the calculation by Fu /8/ and available data.

MT=102 Capture cross section

Calculated with CASTHY /7/.

MT=103,107 (n,p) and (n,alpha) cross sections

Statistical and pre-equilibrium model calculations using the optical potential parameters and the level density parameters given above. Fitted to available data.

MT=111 (n,2p) cross section

This cross section was given only for Ca-40 by adopting the calculated values by Fu /8/.

MT=251 Mu-bar

Calculated with optical model.

MF=4 Angular Distributions of Secondary Neutrons

MT=2

Optical model calculation

MT=51-88

Isotropic in the center-of-mass system.

MT=16,22,28

Isotropic in the laboratory system.

MT=91

Isotropic distribution in the center-of-mass system was transformed into the laboratory system.

MF=5 Energy Distributions of Secondary Neutrons

MT=16,22,28,91

Evaporation spectra.

References

- 1) Mughabghab S.F. and Garber D.I.: BNL-325, 3rd Edition, Vol.1 (1973).
- 2) Musgrove A.R.de L. et al.: Nucl. Phys. A259, 365 (1976).
- 3) Singh U.N. et al.: Phys. Rev. C10, 2143 (1974)
- 4) Musgrove A.R.de L. et al.: Nucl. Phys. A279, 317 (1977).
- 5) Cierjacks S.: KfK-1000 (1968).
- 6) Perey F.G. et al.: ORNL-4823 (1972).
- 7) Igarasi S.: J. Nucl. Sci. Technol., 12, 67 (1975).
- 8) Fu C.Y.: Atomic Data and Nuclear Data Table 17, 127 (1976).
- 9) Lederer C.M. and Shirley V.S.: Table of Isotopes, 7th Ed., Wiley-Interscience (1978).
- 10) Gilbert A. and Cameron A.G.W.: Can. J. Phys. 43, 1446 (1965).

20-Ca- 40 MAT number = 2201

20-Ca- 40 Mitsui E.S. Eval-Apr80 M.Hatchya
Dist-Mar83 Rev1-Feb84

History

80-04 New evaluation was made by M.Hatchya (Mitsui).
83-11 Ang. dist. was modified.
84-02 Comment was added.

MF=1 General Information

MT=451 Descriptive data and dictionary

MF=2 Resonance Parameters

MT=151 Resolved resonance parameters for MLBW formula
Resonance energy region = $1.0E-5$ eV to 400 keV.
Parameters were evaluated on the basis of the following
data.

BNL 325 3rd ed. /1/, Musgrove et al. /2/,
Singh et al. /3/.

Calculated 2200-m/sec cross sections and resonance integrals

	2200-m/sec	Res.Integ.
elastic	3.010 b	-
capture	0.410 b	0.216 b
(n,alpha)	0.0025 b	0.355 b
total	3.423 b	-

MF=3 Neutron Cross Sections

Above resonance region.

MT=1 Total cross section

The optical model calculation with CASTHY /4/ was adopted.

Optical potential parameters taken from Ref. /5/.

V = 46.72 (MeV),
W_s = 9.13 (MeV),
V_{so} = 5.37 (MeV),
r₀ = r_{so} = 1.26 (fm),
r_s = 1.39 (fm),
a = a_{so} = 0.76 (fm),
b = 0.40 (fm).

MT=2 Elastic scattering cross section

Derived by subtracting partial cross sections from the total
cross section.

MT=4,51-66,91 Inelastic scattering cross sections

Calculated with optical and statistical model code CASTHY
/4/.

Level scheme

Taken from Ref. /6/

No. Energy (MeV) Spin-Parity

g. s.	0.0	0 +
1	3.737	3 -
2	3.904	2 +
3	4.492	5 -
4	5.249	2 +
5	5.627	2 +
6	6.285	3 -
7	6.585	3 -
8	6.910	2 +
9	6.932	3 -
10	7.860	2 +
11	7.930	4 +
12	8.090	2 +
13	8.280	2 +
14	8.371	4 +
15	8.540	2 +
16	8.553	5 -

Continuum levels were assumed above 8.99 MeV.

Level density parameters (Gilbert and Cameron /7/)

isotope	40	41
a (1/MeV)	5.43	6.00
S-C(1/SQRT(MeV))	2.42	2.59
Delta(MeV)	3.87	1.83
Ex (MeV)	10.12	7.99

MT=16 (n,2n) cross section

Based on available data.

MT=22,28 (n,n'alpha) and (n,n'p) cross sections

Derived from the calculation by Fu /5/.

MT=102 Capture cross section

Calculated with CASTHY /4/.

MT=103,107 (n,p) and (n,alpha) cross sections

Statistical and pre-equilibrium model calculations using the optical potential parameters and the level density parameters given above. Fitted to available data.

MT=111 (n,2p) cross section

The calculated values by Fu /5/ were adopted.

MT=251 Mu-bar

Calculated with optical model.

MF=4 Angular Distributions of Secondary Neutrons

MT=2,51-66,91

Optical model calculation

MT=16,22,28

Isotropic in the laboratory system.

MF=5 Energy Distributions of Secondary Neutrons

MT=16,22,28,91

Evaporation spectra.

References

1) Mughabghab S.F. and Garber D.I.: BNL-325, 3rd Edition, Vol.1

- (1973).
- 2) Musgrove A.R.de L. et al.: Nucl. Phys. A259, 365 (1976).
 - 3) Singh U.N. et al.: Phys. Rev. C10, 2143 (1974)
 - 4) Igarasi S.: J. Nucl. Sci. Technol., 12, 67 (1975).
 - 5) Fu C.Y.: Atomic Data and Nuclear Data Table 17, 127 (1976).
 - 6) Lederer C.M. and Shirley V.S.: Table of Isotopes, 7th Ed., Wiley-Interscience (1978).
 - 7) Gilbert A. and Cameron A.G.W.: Can. J. Phys. 43, 1446 (1965).

20-Ca- 42 MAT number = 2202

20-Ca- 42 Mitsui E.S.Eval-Apr80 M.Hatchya
Dist-Mar83 Rev1-Feb84

History

80-04 New evaluation was made by M.Hatchya (Mitsui).

83-11 Ang. dist. was modified.

84-02 Comment was added.

MF=1 General Information

MT=45! Descriptive data and dictionary

MF=2 Resonance Parameters

MT=15! Resolved resonance parameters for MLBW formula

Resonance energy region = $1.0E-5$ eV to 400 keV.

Parameters were evaluated on the basis of the experimental data by Musgrove et al. /1/.

Calculated 2200-m/sec cross sections and resonance integrals

	2200-m/sec	Res.Integ.
elastic	1.230 b	-
capture	0.680 b	0.384 b
total	1.910 b	-

MF=3 Neutron Cross Sections

Above resonance region.

MT=1 Total cross section

The optical model calculation with CASTHY /2/ was adopted.

Optical potential parameters were taken from Ref. /3/, and modified so as to reproduce the Ca-42 total cross section

$$\begin{aligned} V &= 52.06 - 0.023E \quad (\text{MeV}), \\ W_s &= 5.57 \quad (\text{MeV}), \\ V_{so} &= 5.37 \quad (\text{MeV}), \\ r_0 &= r_{so} = 1.26 \quad (\text{fm}), \\ r_s &= 1.39 \quad (\text{fm}), \\ a &= a_{so} = 0.76 \quad (\text{fm}), \\ b &= 0.40 \quad (\text{fm}). \end{aligned}$$

MT=2 Elastic scattering cross section

Derived by subtracting partial cross sections from the total cross section.

MT=4,51-56,91 Inelastic scattering cross sections

Calculated with optical and statistical model code CASTHY /2/.

Level scheme

Taken from Table of Isotopes /4/.

No. Energy (MeV) Spin-Parity

g.s.	0.0	0 +
1	1.5246	2 +
2	1.8373	0 +
3	2.4236	2 +
4	2.7523	4 +
5	3.1893	6 +
6	3.445	3 -

Levels above 3.884 MeV were assumed to be overlapping.

Level density parameters (Gilbert and Cameron /5/)

isotope	42	43
a (1/MeV)	6.58	7.00
S-C(1/SQRT(MeV))	2.75	2.88
Delta (MeV)	3.47	1.83
Ex (MeV)	9.54	7.82

MT=16 (n,2n) cross section

Based on available data.

MT=102 Capture cross section

Calculated with CASTHY /2/.

MT=107 (n,alpha) cross section

Statistical and pre-equilibrium model calculations using the optical potential parameters and the level density parameters given above. Fitted to available data.

MT=251 Mu-bar

Calculated with optical model.

MF=4 Angular Distributions of Secondary Neutrons

MT=2,51-56,91

Optical model calculation

MT=16

Isotropic in the laboratory system.

MF=5 Energy Distributions of Secondary Neutrons

MT=16,91

Evaporation spectra.

References

- 1) Musgrove A.R.de L. et al.: Nucl. Phys. A279, 317 (1977).
- 2) Igarasi S.: J. Nucl. Sci. Technol., 12, 67 (1975).
- 3) Fu C.Y.: Atomic Data and Nuclear Data Table 17, 127 (1976).
- 4) Lederer C.M. and Shirley V.S.: Table of Isotopes, 7th Ed., Wiley-Interscience (1978).
- 5) Gilbert A. and Cameron A.G.W.: Can. J. Phys. 43, 1446 (1965).

20-Ca- 43 MAT number = 2203

20-Ca- 43 Mitsui E.S.Eval-Apr80 M.Hatchya
Dist-Mar83 Rev1-Feb84

History

80-04 New evaluation was made by M.Hatchya (Mitsui).
83-11 Ang. dist. was modified.
84-02 Comment was added.

MF=1 General Information

MT=451 Descriptive data and dictionary

MF=2 Resonance Parameters

MT=151 Resolved resonance parameters for MLBW formula
Resonance energy region = $1.0E-5$ eV to 30 keV.
Parameters were evaluated on the basis of the data of
Musgrove et al. /1/.

Calculated 2200-m/sec cross sections and resonance integrals

	2200-m/sec	Res.Integ.
elastic	2.997 b	-
capture	6.200 b	3.20 b
total	9.197 b	-

MF=3 Neutron Cross Sections

Below 30 keV, background cross sections were given to reproduce
the thermal capture cross section of 6.2 barns /2/ and
reasonable elastic scattering cross section. Above resonance
region, data were evaluated as follows.

MT=1 Total cross section

The optical model calculation with CASTHY /3/ was adopted.

Optical potential parameters were taken from Ref. /4/.

V = 46.72 (MeV),
W_s = 9.13 (MeV),
V_{so} = 5.37 (MeV),
r₀ = r_{so} = 1.26 (fm),
r_s = 1.39 (fm),
a = a_{so} = 0.76 (fm),
b = 0.40 (fm).

MT=2 Elastic scattering cross section

Derived by subtracting partial cross sections from the total
cross section.

MT=4,51-54,91 Inelastic scattering cross sections

Calculated with optical and statistical model code CASTHY
/3/.

Level scheme

Level scheme was taken from Table of Isotopes /5/.

No.	Energy (MeV)	Spin-Parity
g.s.	0.0	7/2 -
1	0.3728	5/2 -
2	0.5934	3/2 -
3	0.9903	3/2 +
4	1.3946	5/2 +

Levels above 1.9314 MeV were assumed to be overlapping.

Level density parameters (Gilbert and Cameron /6/)

isotope	43	44
a (1/MeV)	7.00	7.10
S-C (1/SQRT (MeV))	2.88	2.95
Delta (MeV)	1.83	3.27
Ex (MeV)	7.82	9.18

MT=16 (n,2n) cross section

Based on available data.

MT=102 Capture cross section

Calculated with CASTHY /3/.

MT=103,107 (n,p) and (n,alpha) cross sections

Statistical and pre-equilibrium model calculations using the optical potential parameters and the level density parameters given above. Fitted to available data.

MT=251 Mu-bar

Calculated with optical model.

MF=4 Angular Distributions of Secondary Neutrons

MT=2,51-54,91

Optical model calculation

MT=16

Isotropic in the laboratory system.

MF=5 Energy Distributions of Secondary Neutrons

MT=16,91

Evaporation spectra.

References

- 1) Musgrove A.R.de L. et al.: Nucl. Phys. A279, 317 (1977).
- 2) Mughabghab S.F. and Garber D.I.: BNL-325, 3rd Edition, Vol.1 (1973).
- 3) Igarasi S.: J. Nucl. Sci. Technol., 12, 67 (1975).
- 4) Fu C.Y.: Atomic Data and Nuclear Data Table 17, 127 (1976).
- 5) Lederer C.M. and Shirley V.S.: Table of Isotopes, 7th Ed., Wiley-Interscience (1978).
- 6) Gilbert A. and Cameron A.G.W.: Can. J. Phys. 43, 1446 (1965).

20-Ca- 44 MAT number = 2204

20-Ca- 44 Mitsui E.S. Eval-Apr80 M.Hatchya
Dist-Mar83 Rev1-Feb84

History

80-04 New evaluation was made by M.Hatchya (Mitsui).
83-11 Ang. dist. was modified.
84-02 Comment was added.

MF=1 General Information

MT=451 Descriptive data and dictionary

MF=2 Resonance Parameters

MT=151 Resolved resonance parameters for MLBW formula
Resonance energy region = $1.0E-5$ eV to 400 keV.
Parameters were evaluated on the basis of the data of
Musgrove et al. /1/.

Calculated 2200-m/sec cross sections and resonance integrals

	2200-m/sec	Res.Integ.
elastic	1.323 b	-
capture	0.8799 b	0.429 b
total	2.203 b	-

MF=3 Neutron Cross Sections

Below 400 keV, background cross sections were given to reproduce
the thermal capture cross section of 0.88 barns /2/. Above
resonance region, data were evaluated as follows.

MT=1 Total cross section

The optical model calculation with CASTHY /3/ was adopted.

Optical potential parameters were taken from Ref. /4/.

V = 46.72 (MeV),
Ws = 9.13 (MeV),
Vso = 5.37 (MeV),
r0 = rso = 1.26 (fm),
rs = 1.39 (fm),
a = aso = 0.76 (fm),
b = 0.40 (fm).

MT=2 Elastic scattering cross section

Derived by subtracting partial cross sections from the total
cross section.

MT=4,51-54,91 Inelastic scattering cross sections

Calculated with optical and statistical model code CASTHY
/3/.

Level scheme

Level scheme was taken from Table of Isotopes /5/.

No. Energy (MeV) Spin-Parity

g.s.	0.0	0 +
1	1.157	2 +
2	1.8835	0 +
3	2.2831	4 +
4	2.6565	2 +

Levels above 3.2849 MeV were assumed to be overlapping.

Level density parameters (Gilbert and Cameron /6/)

isotope	44	45
a (1/MeV)	7.10	7.12
S-C (1/SQRT (MeV))	2.95	3.00
Delta (MeV)	3.27	1.83
Ex (MeV)	9.18	7.66

MT=16 (n,2n) cross section

Based on available data.

MT=102 Capture cross section

Calculated with CASTHY /3/.

MT=103,107 (n,p) and (n,alpha) cross sections

Statistical and pre-equilibrium model calculations using the optical potential parameters and the level density parameters given above. Fitted to available data.

MT=251 Mu-bar

Calculated with optical model.

MF=4 Angular Distributions of Secondary Neutrons

MT=2,51-54,91

Optical model calculation

MT=16

Isotropic in the laboratory system.

MF=5 Energy Distributions of Secondary Neutrons

MT=16,91

Evaporation spectra.

References

- 1) Musgrove A.R.de L. et al.: Nucl. Phys. A279, 317 (1977).
- 2) Mughabghab S.F. and Garber D.I.: BNL-325, 3rd Edition, Vol.1 (1973).
- 3) Igarasi S.: J. Nucl. Sci. Technol., 12, 67 (1975).
- 4) Fu C.Y.: Atomic Data and Nuclear Data Table 17, 127 (1976).
- 5) Lederer C.M. and Shirley V.S.: Table of Isotopes, 7th Ed., Wiley-Interscience (1978).
- 6) Gilbert A. and Cameron A.G.W.: Can. J. Phys. 43, 1446 (1965).

20-Ca- 46 MAT number = 2205

20-Ca- 46 Mitsui E.S.Eval-Apr80 M.Hatchya
Dist-Mar83 Rev1-Feb84

History

80-04 New evaluation was made by M.Hatchya (Mitsui).
83-11 Ang. dist. was modified.
84-02 Comment was added.

MF=1 General Information

MT=451 Descriptive data and dictionary

MF=2 Resonance Parameters

MT=151 No resonance parameters

2200-m/sec cross sections and calculated resonance integrals

	2200-m/sec	Res.Integ.
elastic	2.900 b	-
capture	0.7400 b	0.339 b
total	3.640 b	-

MF=3 Neutron Cross Sections

Thermal region was assumed to be below 1.0 keV. The capture and elastic scattering cross sections were assumed to be 0.74 barns /1/ and 2.9 barns at 0.0253 eV, respectively. The total cross section was calculated as a sum of these two. Above 1.0 keV, data were evaluated as follows.

MT=1 Total cross section

The optical model calculation with CASTHY /2/ was adopted.

Optical potential parameters were taken from Ref. /3/.

V =	46.72	(MeV),
Ws =	9.13	(MeV),
Vso =	5.37	(MeV),
r0 = rso =	1.26	(fm),
rs =	1.39	(fm),
a = aso =	0.76	(fm),
b =	0.40	(fm).

MT=2 Elastic scattering cross section

Derived by subtracting partial cross sections from the total cross section.

MT=4,51-53,91 Inelastic scattering cross sections

Calculated with optical and statistical model code CASTHY /2/.

Level scheme

Level scheme was taken from Table of Isotopes /4/.

No.	Energy (MeV)	Spin-Parity
g.s.	0.0	0 +

1	1.347	2 +
2	3.024	2 +
3	3.613	3 -

Levels above 4.463 MeV were assumed to be overlapping.

Level density parameters (Gilbert and Cameron /5/)

isotope	46	47
a (1/MeV)	7.135	7.075
S-C (1/SQRT (MeV))	3.03	3.08
Delta (MeV)	3.37	1.83
Ex (MeV)	9.131	7.522

MT=16 (n,2n) cross section

Based on available data.

MT=102 Capture cross section

Calculated with CASTHY /2/.

MT=103,107 (n,p) and (n,alpha) cross sections

Statistical and pre-equilibrium model calculations using the optical potential parameters and the level density parameters given above. Fitted to available data.

MT=251 mu-bar

Calculated with optical model.

MF=4 Angular Distributions of Secondary Neutrons

MT=2,51-53,91

Optical model calculation.

MT=16

Isotropic in the laboratory system.

MF=5 Energy Distributions of Secondary Neutrons

MT=16,91

Evaporation spectra.

References

- 1) Mughabghab S.F. et al.: Neutron Cross Sections, Vol. 1, Part A (1981).
- 2) Igarasi S.: J. Nucl. Sci. Technol., 12, 67 (1975).
- 3) Fu C.Y.: Atomic Data and Nuclear Data Table 17, 127 (1976).
- 4) Lederer C.M. and Shirley V.S.: Table of Isotopes, 7th Ed., Wiley-Interscience (1978).
- 5) Gilbert A. and Cameron A.G.W.: Can. J. Phys. 43, 1446 (1965).

20-Ca- 48 MAT number = 2206

20-Ca- 48 Mitsui E.S.Eval-Apr80 M.Hatchya
Dist-Mar83 Rev1-Feb84

History

80-04 New evaluation was made by M.Hatchya (Mitsui).
83-11 Ang. dist. was modified.
84-02 Comment was added.

MF=1 General Information

MT=451 Descriptive data and dictionary

MF=2 Resonance Parameters

MT=151 Resolved resonance parameters for MLBW formula
Resonance energy region = 1.0E-5 eV to 400 keV.
No s-wave resonances were given. P-wave resonance parameters were evaluated on the basis of BNL 325 3rd ed. /1/.

Calculated 2200-m/sec cross sections and resonance integrals

	2200-m/sec	Res.Integ.
elastic	2.900 b	-
capture	1.090 b	0.492 b
total	3.990 b	-

MF=3 Neutron Cross Sections

Below 400 keV, background cross sections were given.
Above resonance region, data were evaluated as follows.

MT=1 Total cross section

The optical model calculation with CASTHY /2/ was adopted.

Optical potential parameters were taken from Ref. /3/.

V = 46.72 (MeV),
Ws = 9.13 (MeV),
Vso = 5.37 (MeV),
r0 = rso = 1.26 (fm),
rs = 1.39 (fm),
a = aso = 0.76 (fm),
b = 0.40 (fm).

MT=2 Elastic scattering cross section

Derived by subtracting partial cross sections from the total cross section.

MT=4,51-55,91 Inelastic scattering cross sections

Calculated with optical and statistical model code CASTHY /2/.

Level scheme

Level scheme was taken from Table of Isotopes /4/.

No.	Energy (MeV)	Spin-Parity
g.s.	0.0	0 +

1	3.8317	2 +
2	4.503	4 +
3	4.5069	3 -
4	4.6119	3 +
5	5.3696	3 -

Levels above 6.6137 MeV were assumed to be overlapping.

Level density parameters (Gilbert and Cameron /5/)

isotope	48	49
a (1/MeV)	6.84	7.20
S-C(1/SQRT(MeV))	3.07	3.19
Delta(MeV)	3.13	1.83
Ex (MeV)	8.76	7.39

MT=16 (n,2n) cross section

Based on available data.

MT=102 Capture cross section

Calculated with CASTHY /2/.

MT=103 (n,p) cross sections

Statistical and pre-equilibrium model calculations using the optical potential parameters and the level density parameters given above. Fitted to available data.

MT=251 Mu-bar

Calculated with optical model.

MF=4 Angular Distributions of Secondary Neutrons

MT=2,51-55,91

Optical model calculation

MT=16

Isotropic in the laboratory system.

MF=5 Energy Distributions of Secondary Neutrons

MT=16,91

Evaporation spectra.

References

- 1) Mughabghab S.F. and Garber D.I.: BNL-325, 3rd Edition, Vol.1 (1973).
- 2) Igarasi S.: J. Nucl. Sci. Technol., 12, 67 (1975).
- 3) Fu C.Y.: Atomic Data and Nuclear Data Table 17, 127 (1976).
- 4) Lederer C.M. and Shirley V.S.: Table of Isotopes, 7th Ed., Wiley-Interscience (1978).
- 5) Gilbert A. and Cameron A.G.W.: Can. J. Phys. 43, 1446 (1965).

21-Sc- 45 MAT number = 2211

21-Sc- 45 UTOK, JAERI Eval-Feb82 Y.Oka, T.Nakagawa, Y.Kikuchi
 JAERI-M 9981 Dist-Mar83 Rev1-Nov83

History

82-02 Evaluation was made by Y.Oka (Tokyo University),
 T.Nakagawa and Y.Kikuchi (JAERI). Details are given in
 Ref. /1/.

83-11 Angular dist. was modified and comment was added.

MF=2, MT=151 Resonance parameters for MLBW formula

Resolved resonance region : 1.0E-5 eV - 90 keV

On the basis of the data of Liou+ /2/ and Kenny+ /3/.

Adjusted to reproduce

- 1) total cross section minimum at 2 keV : 0.23 b /4/.
- 2) thermal cross sections of BNL-325, 3rd ed.

Calculated thermal cross sections and resonance integrals:

	2200 m/s value	res.int.
total	51.05 b	-
elastic	25.03 b	-
capture	26.02 b	11.3 b

MF=3 Cross Sections

MT=1,2,4,51-61,91,102 Sig-t, Sig-el, Sig-in, Sig-c

Calculated with optical and statistical models.

Optical potential parameters were obtained by fitting the
 data of Foster+ /5/ and Barnard+ /6/ :

$$\begin{aligned}
 V &= 56.15 - 0.2189 \cdot E_n & , W_s &= 8.698 & , V_{so} &= 6.874 \text{ (MeV)} \\
 r &= 1.16 & , r_s &= 1.288 & , r_{so} &= 1.185 \text{ (fm)} \\
 a &= 0.677 & , b &= 0.310 & , a_{so} &= 0.76 \text{ (fm)}
 \end{aligned}$$

Statistical model calculation with CASTHY code /7/.

Competing processes : (n,p); (n,alpha); (n,2n).

Level fluctuation considered.

The level scheme taken from Ref. /8/:

No	Energy (MeV)	Spin-Parity
g.s.	0	7/2 -
1	0.0124	3/2 +
2	0.3764	3/2 -
3	0.5429	5/2 +
4	0.7202	5/2 +
5	0.9391	1/2 +
6	0.9745	7/2 +
7	1.2364	11/2 -
8	1.3032	3/2 +
9	1.4334	9/2 +
10	1.6615	9/2 -
11	1.8006	5/2 +

Continuum levels assumed above 1.9 MeV.

The level density parameters : Gilbert and Cameron /9/.

The gamma-ray strength function was determined so that
 Sig-c = 32 mb at 100 keV /3/.

MT=16 (n,2n)
Evaluated on the basis of the data of Holub+ /10/.

MT=103,107 (n,p), (n,alpha)
Taken from compilation by Alley and Lessler /11/.

MT=251 Mu-bar
Calculated with optical model.

MF=4 Angular Distributions of Secondary Neutrons
MT=2 Calculated with optical model.
MT=16 Isotropic in laboratory system.
MT=51-61 90 deg. symmetry in center of mass system.
MT=91 90 deg. symmetry in laboratory system.

MF=5 Energy Distributions of Secondary Neutrons
MT=16,91 Evaporation spectrum.

References

- 1) Oka Y., Nakagawa T., Kikuchi Y. : JAERI-M9981 (1982).
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- 6) Barnard E. et al. : Z. Phys., 245, 36 (1971).
- 7) Igarasi S. : J. Nucl. Sci. Technol., 12, 67 (1975).
- 8) Lederer C.M., Shirley V.S. : Table of Isotopes, 7th Ed. (1978).
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- 10) Holub E., Cindro N. : Z. Phys., A289, 421 (1979).
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23-V - 51 MAT number = 2231

23-V - 51 JAERI Eval-Oct82 S.Tanaka
 JAERI-M 82-151 Dist-Mar83 Rev1-Feb84

History

- 82-10 Evaluation was made by S. Tanaka (JAERI). Details are given in Ref. /1/.
- 83-11 Q value and threshold energy of 2nd level was corrected. Comment data were added.
- 84-02 Background cross sections were replaced with correct data.

MF=1 General Information

MT=451 Descriptive data and dictionary

MF=2, MT=151 Resonance parameters

Resolved resonances for MLBW formula : $1.0E-5$ eV - 100 keV
 Parameters were taken from BNL 325 3rd edition /2/, and modified to reproduce experimental total cross section. Cross sections calculated with these parameters are to be corrected by adding MF=3, MT=1, 2 and 102 data.

Calculated 2200-m/sec cross sections and resonance integrals

	2200 m/sec	Res. Integ.
elastic	4.805 b	-
capture	4.900 b	2.53 b
total	9.705 b	-

MF=3 Neutron Cross Sections

Below 100 keV.

Background cross sections are given.

100 - 500 keV.

MT=1 Total

Based on the following experimental data.

100 - 220 keV, data of Rohr and Friedland /3/.

220 - 360 keV, data of Smith et al. /4/ with energy shift.

360 - 500 keV, data of Cierjacks et al. /5/.

MT=2 Elastic scattering

Obtained by subtracting the sum of MT=102 and 51 from MT=1.

MT=51 Inelastic scattering to the 1st level

Hauser-Feshbach calculation mentioned below.

MT=102 capture

Based on the following experimental data.

100 - 210 keV, data of Winter et al. /6/.

210 - 500 keV, data of Dudgey et al. /7/.

Above 0.5 MeV.

MT=1, 2, 4, 51, 76, 91, 102 Total, Elastic, Inelastic and Capture

Calculated with optical and statistical models except for MT=51 and 52 data in 4.5 - 20 MeV, which follow the data of Perey and Kinney /8/ and extrapolation of their data above 8.5 MeV. The effect of this exception and threshold reactions are reflected in MT=2 data.

The spherical optical potential parameters:

$$V = 49.50 - 0.33 \cdot E_n \quad , \quad V_{so} = 7.0 \quad (\text{MeV})$$

$$W_s = 4.6 + 0.34 \cdot E_n \quad , \quad W_v = 0 \quad (\text{MeV})$$

$$r = r_s = r_{so} = 1.23 \quad (\text{fm})$$

$$a = a_{so} = 0.65 \quad , \quad b = 0.48 \quad (\text{fm}).$$

Statistical model calculation with CASTHY code /9/ was performed. MT=102 data were normalized to the experimental data of Dudev et al. /7/ at 0.5 MeV.

The level scheme taken from Ref. /10/:

No	Energy (MeV)	Spin-Parity
g.s.	0	7/2 -
1	0.320	5/2 -
2	0.929	3/2 -
3	1.609	11/2 -
4	1.813	9/2 -
5	2.409	3/2 -
6	2.545	1/2 +
7	2.675	3/2 +
8	2.699	15/2 -
9	2.790	(9/2 -)
10	3.084	5/2 -
11	3.195	(5/2 -)
12	3.215	3/2 -
13	3.262	5/2 -
14	3.280	5/2 (+)
15	3.381	3/2 -
16	3.383	9/2 -
17	3.386	13/2 -
18	3.396	13/2 -
19	3.412	(9/2 -)
20	3.452	9/2 -
21	3.515	(13/2 -)
22	3.569	(13/2 -)
23	3.576	(3/2 -)
24	3.614	11/2 -
25	3.631	(1/2 -)
26	3.674	3/2 -

() : arbitrarily assigned.

Continuum levels assumed above 3.68 MeV. The level density parameters of Dilg et al. /11/ were used.

MF=16 (n,2n)

Guided by experimental data of Frehaut et al. /12/.

MT=22 (n,n'alpha)

Based on the assertion of Hillman /13/.

MT=28 (n,n')

Given by subtracting the (n,p) cross section (MT=103) from the (n,xp) cross section calculated by Kitazawa and Isogai /14/.

MT=103 (n,p)

Kitazawa and Isogai's calculation /14/ normalized to Bormann's experimental data /15/ at 13.2 MeV.

MT=104 (n,d)

Calculation of Guerther et al. /16/.

MT=105 (n,t)

Roughly the same shape as the (n,d) cross section was adopted by normalizing to 0.001 barns at 14 MeV.

MT=107 (n, alpha)

Follows experimental data of Paulsen et al. /17/.

MT=251 Mu-ber

Calculated with optical model.

MF=4 Angular Distributions of Secondary Neutrons

MT=2 Calculated with optical model.

MT=51-76,91 Calculated with Hauser-Feshbach formula.

MT=16,22,28 Isotropic in the laboratory system.

MF=5 Energy Distributions of Secondary Neutrons

MT=16,22,28,91 Evaporation spectra.

References

- 1) Tanaka, S.: JAERI-M 82-151 (1982).
- 2) Maghabghab, S.F. and Garber, D.I.: BNL 325, 3rd Ed., Vol. 1 (1973).
- 3) Rohr, G. and Friedland, E.: Nucl. Phys. A104, 1 (1967).
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- 5) Cierjacks, S. et al.: KfK 1000 (1968).
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- 8) Perey, F. and Kinney, W.: ORNL-4551 (1970).
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24-Cr- 0 MAT number = 2240

24-Cr- 0 JAERI Eval-Aug82 T.Asami
Dist-Mar83 Rev1-Nov83

History

82-08 New evaluation was made by T. Asami (JAERI) for JENDL-2.
83-11 Modification for MF=4.

MF=1 General Information

MT=451 Descriptive data and dictionary

MF=2 Resonance Parameters

MT=151 Resolved resonance parameters for MLBW formula

Resolved resonance region :

1.0E-5 eV to 300 keV for Cr-50, Cr-52 and Cr-54.

1.0E-5 eV to 120 keV for Cr-53.

Resonance parameters were evaluated from the following data:

Cr-50 : Stieglitz+71 /1/, Beer+74 /2/, Allen+77 /3/ and
Kenny+77 /4/.

Cr-52 : same as above.

Cr-53 : same as above and Mueller+71 /5/.

Cr-54 : Stieglitz+71 /1/, BNL-325 /6/, Allen+77 /3/ and
Kenny+77 /4/.

For unknown radiative widths, assumed were average values of known widths. Effective scattering radii of Cr-50, Cr-53 and Cr-54 were taken from BNL-325 /6/ and radius of Cr-52 was determined to get a good fit to the experimental total cross sections.

calculated 2200-m/s cross sections and res. integrals.

	2200-m/s	res. integ.
elastic	3.830 b	-
capture	3.070 b	1.60 b
total	6.900 b	-

MF=3 Neutron Cross Sections

Below 300 keV.

Background cross sections were applied to reproduce the 2200-m/s capture cross section of 3.07 barns and elastic scattering of 3.8 barns. Contribution from Cr-53 in the energy range from 120 to 300 keV were also considered as background cross sections.

Above 300 keV.

MT=1 Total

Cross sections in the energy range of 300 keV to 7 MeV were estimated from the experimental data of Cierjacks+68 /7/. the data above 7 MeV were calculated by using optical model code CASTHY /8/. Potential parameters /9/ were obtained by fitting average total cross section of natural chromium.

$V = 50.05 - 0.262 \cdot E$, $W_s = 4.87 + 0.352 \cdot E$, $V_{so} = 7.0$ (MeV)
 $r_0 = 1.24$, $r_s = 1.4$, $r_{so} = 1.24$ (fm)

$$a_0 = 0.48 \quad , \quad b = 0.4 \quad , \quad a_{s0} = 0.48(\text{fm})$$

MT=2 Elastic scattering

(Total) - (All other partial cross sections)

MT=4,51-90,91 Inelastic scattering

Calculated with statistical and optical model code CASTHY/9/ for four stable isotopes, and constructed taking into account of their isotope abundances. In the calculation, optical potential parameters given above and level density parameters by Yoshida /10/ were used. Level schemes were taken from Ref. /11/. Level energies and corresponding isotopes are as follows:

MT	Energy (MeV)	Isotope	MT	Energy (MeV)	Isotope
51	0.5638	53	71	2.7071	53
52	0.7839	50	72	2.7678	52
53	0.8343	54	73	2.7711	53
54	1.0060	53	74	2.8256	53
55	1.2891	53	75	2.8275	54
56	1.4341	52	76	2.9268	50
57	1.5361	53	77	2.9649	52
58	1.8225	54	78	2.9920	53
59	1.8829	50	79	3.0718	54
60	1.9729	53	80	3.0831	53
61	2.1717	53	81	3.0920	53
62	2.2332	53	82	3.1139	52
63	2.3200	53	83	3.1369	53
64	2.3697	52	84	3.1578	54
65	2.4523	53	85	3.1618	52
66	2.6177	54	86	3.1636	50
67	2.6471	52	87	3.1666	50
68	2.6561	53	88	3.1782	53
69	2.6686	53	89	3.2203	54
70	2.7056	53	90	3.2428	53

Contributions from the levels above 3.260 MeV were put together into continuum (MT=91).

MT=16 (n,2n)

Constructed from the evaluated (n,2n) data for Cr-50, 52, 53 and 54. Data for Cr-50 and Cr-52 were estimated from the experimental data. Data for Cr-53 and 54 were obtained from calculations with evaporation-model code GROGI /12/, and adjusted to the experimental data of Frehaut+80 /13/ for natural chromium in the energy range below 15 MeV.

MT=28 (n,n'p)

Constructed from the evaluated (n,n'p) data for Cr-50, 52, 53 and 54 which were calculated with evaporation-model code GROGI /12/, and normalized to the experimental data.

MT=102 Capture

Calculated with statistical and optical model code CASTHY/8/, and normalized to reproduce 10 milli-barns at 50 keV.

MT=103 (n,p)

Constructed from the evaluated (n,p) data for Cr-50, 52, 53 and 54 which were calculated with evaporation-model code GROGI /12/, and normalized to the experimental data.

MT=107 (n,alpha)

Constructed from the evaluated (n,alpha) data for Cr-50, 52, 53 and 54 which were calculated with evaporation-model code

3 of Natural Chromium

GROGI /12/, and normalized to the experimental data. Data for Cr-52 were modified in the energies below 10 MeV to reproduce the experimental data of Paulsen+80 /4/ for natural chromium.

MT=251 Mu-bar
Calculated with optical model.

MF=4 Angular Distributions of Secondary Neutrons
MT=2 Calculated with optical model.
MT=51-90 Isotropic in the center-of-mass system.
MT=16,28,91 Isotropic in the laboratory system.

MF=5 Energy Distributions of Secondary Neutrons
MT=16,28,91 Evaporation spectra were given.

References

- 1) Stieglitz R.G. et al.: Nucl. Phys. A163, 592 (1971).
- 2) Beer H. and Spencer R.P.: KfK-2063 (1974), also Nucl. Phys. A240, 29 (1975).
- 3) Allen B.J. and Musgrove A.R.de L.: Neutron Data of Structural Materials for FBR, 1977 geel Geeting, p.447, Pergamon Prees (1979).
- 4) Kenny M.J. et al.: AAEC/E-400 (1977).
- 5) Mueller K.N. et al.: Nucl. Phys., A164, 97 (1971).
- 6) Mughabghab S.F. and Garber D.L.: BNL-325 3rd Ed., Vol.1 (1973)
- 7) Cierjacks S. et al.: KfK-1000 (1968).
- 8) Igarasi S.: J. Nucl. Sci. Technol., 12, 67 (1975).
- 9) Kawai M.: unpublished.
- 10) Yoshida T.: unpublished.
- 11) Lederer C.M. and Shirley V.S.: Table of Isotopes, 7th Ed., (1978).
- 12) Gilat J.: BNL-50246(T-580) (1970).
- 13) Frehaut J. et al.: Proc. Symp. on Neutron Cross Sections from 10 to 50 MeV, BNL 1980, BNL-NCS-51245, p. 399 (1980).
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24-Cr- 50 MAT number = 2241

24-Cr- 50 JAERI Eval-Aug82 T.Asami
Dist-Mar83 Rev1-Nov83

History

82-08 New evaluation was made by T. Asami (JAERI) for JENDL-2.
83-11 Modification for MF=4.

MF=1 General Information

MT=451 Descriptive Data and Dictionary

MF=2 Resonance Parameters

MT=151 Resolved resonance parameters for MLBW

Resolved resonance region : 1.0E-5 eV - 300 keV

Evaluation based on the experimental data by Stieglitz+71
/1/, Beer+74 /2/, Allen+77 /3/ and Kenny+77 /4/.assumed gamma width = 1.81 eV for s-wave and 0.92 eV for
p-wave resonances.

Effective scattering radius = 5.4 fm /5/.

Calculated 2200-m/s cross sections and res. integrals.

	2200-m/s	res. integ.
elastic	8.581 b	-
capture	15.90 b	7.77 b
total	24.48 b	-

MF=3 Neutron Cross Sections

Resonance region (from 1.0E-5 eV to 300 keV)

Background cross sections were applied to reproduce the
2200-m/s capture cross section of 15.9 +/- 0.2 barns /5/,
and to modify the elastic scattering cross section in the
lower energy region.

Above 300 keV

MT=1 Total

Calculated with optical model. Potential parameters /6/
were obtained by fitting Cr-natural average total cross
section.

$$V = 50.05 - 0.262E, \quad W_s = 4.87 + 0.352E, \quad V_{so} = 7.0 \text{ (MeV)}$$

$$r_0 = 1.24, \quad , \quad r_s = 1.4, \quad , \quad r_{so} = 1.24 \text{ (fm)}$$

$$a_0 = 0.48, \quad , \quad b = 0.4, \quad , \quad a_{so} = 0.48 \text{ (fm)}$$

MT=2 Elastic scattering

(Total) - (All other partial cross sections)

MT=4,51-70,91 Inelastic scattering

Calculated with statistical and optical model code CASTHY/7/.

Level scheme taken from Ref. /8/.

No.	Energy (MeV)	Spin-Parity
g.s.	0.0	0 +
1	0.7833	2 +
2	1.8814	4 +

3	2.9245	2 +
4	3.1611	2 +
5	3.1641	6 +
6	3.3247	4 +
7	3.5946	4 +
8	3.6101	4 +
9	3.6295	1 +
10	3.6940	0 +
11	3.6978	2 +
12	3.7924	5 +
13	3.8261	6 +
14	3.8443	3 +
15	3.8500	0 +
16	3.8752	6 +
17	3.8953	2 +
18	3.8983	4 +
19	3.9377	3 +
20	4.0517	0 +

Continuum levels assumed above 4.066 MeV.

Level density parameters of Yoshida /9/ were used.

MT=16 (n,2n)

Evaluated mainly on the basis of the experimental data of Bormann65 /10/.

MT=28 (n,n'p)

Calculated with evaporation-model code GROGI /11/, and normalized to 0.393 barns at 14.7 MeV which was estimated from the experimental data of Qaim+82 /12/ and Grimes+79/13/.

MT=102 Capture

Calculated with statistical and optical model code CASTHY/7/.

MT=103 (n,p)

Calculated with evaporation-model code GROGI /11/, and normalized to 0.437 barns at 14.7 MeV which was estimated based on the experimental data of Grimes+79 /13/.

MT=107 (n.alpha)

Calculated with evaporation-model code GROGI /11/, and normalized to 0.108 barns at 14.8 MeV which is an average value of the experimental data of Grimes+79 /13/ and Dolja+73 /14/.

MT=251 Mu-bar

Calculated with optical model.

MF=4 Angular Distributions of Secondary Neutrons

MT=2,51-70 Calculated with CASTHY /7/.

MT=91 Calculated with CASTHY, and the same distribution was assumed in the lab system.

MT=16,28 Assumed to be isotropic in the lab system.

MF=5 Energy Distributions of Secondary Neutrons

MT=16,28,91 Evaporation spectra were given.

References

- 1) Stieglitz R.G. et al.: Nucl. Phys. A163, 592 (1971).
- 2) Beer H. and Spencer R.P.: KfK-2063 (1974), also Nucl. Phys. A240, 29 (1975).
- 3) Allen B.J. and Musgrove A.R.De L.: Neutron Data of Structural Materials for FBR, 1977 Geel Meeting, p.447, Pergamon Press

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 - 5) Mughabghab S.F. and Garber D.L.: BNL-325 3rd Ed., Vol.1 (1973)
 - 6) Kawai M.: unpublished.
 - 7) Igarasi S.: J. Nucl. Sci. Technol., 12, 67 (1975).
 - 8) Lederer C.M. and Shirley V.S.: Table of Isotopes, 7th Ed., (1978).
 - 9) Yoshida T.: unpublished.
 - 10) Bormann M.: data in EXFOR file (1965).
 - 11) Gilat J.: BNL-50246(T-580) (1970).
 - 12) Qaim S.M. et al.: Nucl. Phys., A382, 255 (1982).
 - 13) Grimes S.M. et al.: Phys. Rev., C19, 2127 (1979).
 - 14) Dolja G.P. et al.: 1973 Kiev Conf., Vol.3, 131 (1973).

g.s.	0.0	0 +
1	1.4341	2 +
2	2.3696	4 +
3	2.6470	0 +
4	2.7677	4 +
5	2.9648	2 +
6	3.1138	6 +
7	3.1617	2 +
8	3.4152	4 +
9	3.4722	3 +
10	3.6158	5 +
11	3.7000	2 +
12	3.7717	2 +
13	3.9460	4 +
14	3.9512	1 +
15	4.0154	5 +
16	4.0380	4 +
17	4.5630	3 +
18	4.6270	5 +
19	4.7060	2 +
20	4.7410	2 +
21	4.7507	8 +
22	4.7940	0 +
23	4.8045	6 +

Continuum levels assumed above 4.816 MeV.

Level density parameters of Yoshida /9/ were used.

MT=16 (n,2n)

Evaluated mainly on the basis of the experimental data of Wenusch+62 /10/, Bormann+68 /11/, Maslov+72 /12/, Qaim72/13/, Sailer+77 /14/ and Molla81 /15/.

MT=28 (n,n'p)

Calculated with evaporation-model code GROGI /16/, and normalized to 0.085 barns at 14.8 MeV which was estimated from the experimental data of Grimes+79/17/.

MT=102 Capture

Calculated with statistical and optical model code CASTHY/7/, and normalized to reproduce 10 milli-barns at 50 keV for Cr-natural.

MT=103 (n,p)

Calculated with evaporation-model code GROGI /16/, and normalized to 0.095 barns at 14.7 MeV which is an average value of the experimental data. Calculated data below 9 MeV were modified using the experimental data of Smith+79 /18/.

MT=107 (n,alpha)

Calculated with evaporation-model code GROGI /16/. Calculated values were normalized to 0.038 barns at 14.8 MeV which is an average value of the experimental data of Grimes+79 /17/ and Dolja+73 /19/, and modified to reproduce the experimental values of Cr-natural (n,a) by Paulsen+80/20/ in the energy region below 10 MeV.

MT=251 Mu-bar

Calculated with optical model.

MF=4 Angular Distributions of Secondary Neutrons

MT=2,51-70 Calculated with CASTHY /7/.

MT=91 Calculated with CASTHY, and the same distribution

was assumed in the lab system.
 MT=16,28 Assumed to be isotropic in the lab system.

MF=5 Energy Distributions of Secondary Neutrons
 MT=16,28,91 evaporation spectra were given.

References

- 1) Stieglitz R.G. et al.: Nucl. Phys. A163, 592 (1971).
- 2) Beer H. and Spencer R.P.: KfK-2063 (1974), also Nucl. Phys. A240, 29 (1975).
- 3) Allen B.J. and Musgrove A.R.De L.: Neutron Data of Structural Materials for FBR, 1977 Geel Meeting, p.447, Pergamon Press (1979).
- 4) Kenny M.J. et al.: AAEC/E-400 (1977).
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- 18) Smith D.L. et al.: Nucl. Sci. Eng., 76, 43 (1979).
- 19) Dolja G.P. et al.: 1973 Kiev Conf., Vol.3, 131 (1973).
- 20) Paulsen A. et al.: data in EXFOR file (1980).
- 21) Kinney W.E. et al.: ORNL-4806 (1974).

24-Cr- 53 MAT number = 2243

24-Cr- 53 JAREI Eval-Aug82 T.Asami
Dist-Mar83 Rev1-Nov83

History

82-08 New evaluation was made by T. Asami (JAERI) for JENDL-2.
83-11 Modification for MF=4.

MF=1 General Information

MT=451 Descriptive data and dictionary

MF=2 Resonance Parameters

MT=151 Resolved resonance parameters for MLBW formula
Resolved resonance region : 1.0E-5 eV - 120 keV
Evaluation mainly based on the experimental data by Stieglitz
+71 /1/, Beer+74 /2/, Allen+77 /3/, Kenny+77 /4/ and
Mueller+71/5/.
Assumed gamma width = 2.21 eV for s-wave and 0.61 eV for
p-wave resonances.
Effective scattering radius = 6.9 fm /6/.

Calculated 2200-m/s cross sections and res. integrals.

	2200-m/s	res. integ.
elastic	16.31 b	-
capture	18.20 b	8.86 b
total	34.51 b	-

MF=3 Neutron Cross Sections

Resonance region (from 1.0E-5 eV to 120 keV)

Background cross sections were applied to reproduce the
2200-m/s capture cross section of 18.2 -- 1.5 barns /6/.
and to modify the elastic scattering cross section in the
lower energy region.

Above 120 keV

MT=1 Total

Calculated with optical model. Potential parameters /7/
were obtained by fitting Cr-natural average total cross
section.

$$V = 50.05 - 0.262 * E, \quad W_s = 4.87 + 0.352 * E, \quad V_{so} = 7.0 \text{ (MeV)}$$

$$r_0 = 1.24, \quad , \quad r_s = 1.4, \quad , \quad r_{so} = 1.24 \text{ (fm)}$$

$$a_0 = 0.48, \quad , \quad b = 0.4, \quad , \quad a_{so} = 0.48 \text{ (fm)}$$

MT=2 Elastic scattering

(Total) - (All other partial cross sections)

MT=4.51-72,91 Inelastic scattering

Calculated with statistical and optical model code CASTHY/8/.

Level scheme taken from Ref. /9/.

No.	Energy (MeV)	Spin-Parity
g.s.	0.0	3/2 -
1	0.5640	1/2 -

2	1.0063	5/2 -
3	1.2895	7/2 -
4	1.5366	7/2 -
5	1.9736	5/2 -
6	2.1724	11/2 -
7	2.2330	9/2 -
8	2.3208	3/2 -
9	2.4531	3/2 -
10	2.6570	5/2 -
11	2.6695	1/2 -
12	2.7065	13/2 -
13	2.7080	3/2 -
14	2.7720	5/2 -
15	2.8266	11/2 -
16	2.9930	7/2 -
17	3.0841	15/2 -
18	3.0930	5/2 -
19	3.1380	5/2 -
20	3.1793	3/2 -
21	3.2439	11/2 -
22	3.2610	5/2 -

Continuum levels assumed above 3.435 MeV.

Level density parameters of Yoshida /10/ were used.

MT=16 (n,2n)

Calculated with evaporation-model code GROGI /11/, and normalized to the evaluated value of Boedy+73 /18/ (0.89 b at 14.8 MeV) and modified to reproduce the experimental values of Cr-natural (n,2n) by Frehau+80 /19/ in the range of 9.0 to 15 MeV.

MT=28 (n,n'p)

Calculated with evaporation-model code GROGI /11/, and normalized to 7.2 milli-barns at 14.8 MeV which is an average value of the experimental data by Husain+67 /12/ and Webber+68 /13/.

MT=102 Capture

Calculated with statistical and optical model code CASTHY/8/, and normalized to reproduce 10 milli-barns at 50 keV for Cr-natural.

MT=103 (n,p)

Calculated with evaporation-model code GROGI /11/, and normalized to 0.0416 barns at 14.8 MeV (average value of the experimental data by Husain+67 /12/, Prasad+71 /14/, Valkonen76 /15/ and Qaim+77 /16/).

MT=107 (n,alpha)

Calculated with evaporation-model code GROGI /11/, and normalized to 0.0451 barns at 14.7 MeV by Dolja+73 /14/.

MT=251 Mu-bar

Calculated with optical model.

MF=4 Angular Distributions of Secondary Neutrons

MT=2 Calculated with CASTHY /7/.

MT=16,28 Assumed to be isotropic in the lab system.

MT=51-72 Assumed to be isotropic in the center-of-mass system.

MT=91 Calculated with CASTHY, and the same distribution was assumed in the lab system.

MF=5 Energy Distributions of Secondary Neutrons
MT=16,28,91 Evaporation spectra were given.

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2	1.8237	4 +
3	2.6195	2 +
4	2.8294	0 +
5	3.0739	2 +
6	3.1600	2 +
7	3.2225	6 +
8	3.3920	1 +
9	3.4366	2 +
10	3.4680	1 +
11	3.5140	2 +
12	3.6552	4 +
13	3.7198	2 +
14	3.7858	4 +
15	3.7989	4 +
16	3.8640	2 +
17	3.9340	1 +
18	3.9900	3 +
19	4.0160	0 -
20	4.0450	6 -
21	4.0832	4 +

Continuum levels assumed above 4.088 MeV.

Level density parameters of Yoshida /8/ were used.

MT=16 (n,2n)

Calculated with evaporation-model code GROGI /9/, and normalized to 1.12 barns at 14.8 MeV which was evaluated by Boedy+73 /15/.

MT=102 Capture

Calculated with statistical and optical model code CASTHY/6/, and normalized to reproduce 10 milli-barns at 50 keV for Cr-natural.

MT=103 (n,p)

Calculated with evaporation-model code GROGI /9/, and normalized to 0.016 barns at 14.7 MeV (average value of the experimental data by Husain-67 /10/, Valkonen76 /11/ and Qaim+77 /12/).

MT=107 (n.alpha)

Calculated with evaporation-model code GROGI /9/, and normalized to 0.014 barns at 14.7 MeV which is an average value of the experimental data by Husain+67 /10/, Qaim74 /13/ and Sailer+77 /14/.

MT=251 Mu-bar

Calculated with optical model.

MF=4 Angular Distributions of Secondary Neutrons

MT=2,51-70 Calculated with CASTHY /6/.

MT=91 Calculated with CASTHY, and the same distribution was assumed in the lab system.

MT=16 Assumed to be isotropic in the lab system.

MF=5 Energy Distributions of Secondary Neutrons

MT=16,91 Evaporation spectra were given.

References

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25-Mn- 55 MAT number = 2251

25-Mn- 55 FBEC Eval-Dec82 T.Hojuyama
Dist-Mar83 Rev1-Nov83

History

82-12 Data were evaluated by T. Hojuyama (FBEC) for JENDL-2.
83-11 Comment was added.

MF=1 General Information

MT=451 Descriptive data and dictionary

MF=2 Resonance Parameters

MT=151 Resolved resonance parameters for MLBW formula

Energy range from 1.0E-5 to 1.0E+5 eV. Resonance parameters
were taken from BNL-325 4th ed. (Ref.1). Effective scatter-
ing radius was determined to 5.3 fermi.Calculated 2200-m/s cross sections and resonance integrals 2200
m/sec res. integ.

elastic	2.184 b	-
capture	13.32 b	14.6 b
total	15.50 b	-

MF=3 Neutron Cross Sections

MT= 1 Total cross section

Obtained with optical model calculation. Optical potential
parameters were taken from Kawai's evaluation (Ref.2).

—Optical potential parameters—

V = 47.856 - 0.032 * En (MeV)

Ws = 5.288 + 0.342 * En (MeV)

Vso = 6.90 (MeV)

r0 = rso = 1.24 , rs = 1.41 (fm)

aso = a = 0.522 , b = 0.392 (fm)

MT= 2 Elastic scattering cross section

Obtained by statistical model calculations.

MT=4 & from 51 to 91 Inelastic scattering cross sections

Obtained by statistical and optical model calculations.

Level scheme taken from N.D.S. (Ref.3)

No.	Energy (MeV)	Spin-Parity
g.s.	0.0	5/2 -
1	0.1260	7/2 -
2	0.9843	9/2 -
3	1.2900	1/2 -
4	1.2922	11/2 -
5	1.5289	3/2 -
6	1.8853	7/2 -
7	2.1985	7/2 -
8	2.2153	5/2 -
9	2.2533	3/2 -
10	2.2694	1/2 +
11	2.3118	13/2 -
12	2.3666	5/2 -
13	2.3990	5/2 -

14	2.4286	1/2 +
15	2.5648	3/2 -

Continuum levels assumed above 2.58 MeV.

MT= 16 (n,2n) cross section

Based on the following exp. data ;

Paulsen(Ref.4) : Thr. - 14.7 MeV

Auchampaugh(Ref.5) : 14.7 - 20.0 MeV

Normalization ;

Energy : 14.7 MeV

Cross section : 787 mb

Data-base : Barrall(Ref.6) & Auchampaugh(Ref.5)

MT=22 & 28 (n,n'a) & (n,n'p) cross sections

Determined by statistical model calculation with preequilibrium effect corrections(Ref.7).

Normalization ;

Method : Cross-section systematics

Energy : 14.7 MeV

Cross-section : 5 mb(n,n'a) & 11 mb(n,n'p)

MT=102 Capture cross section

Based on following exp. data ;

Garg(Ref.8) : < 0.7MeV Dovbenko(Ref.9) : < 1.0MeV

Dovbenko & Menlove(Ref.10) : < 3.5MeV

Menlove : < 10 MeV Schwerer(Ref.11)&Budnar(Ref.12) : > 10 MeV

MT=103 (n,p) cross section

Determined by statistical model calculation(Ref.7)

Normalization ;

Energy : 14.7 MeV

Cross-section : 44.7 mb

Data-base : Prasad(Ref.13) & Allan(Ref.14)

MT=107 (n,a) cross section

Based on the statistical model calculation(Ref.7) <13MeV, and exp. data(Zupranska(Ref.15)) >13MeV.

Normalization ;

Energy : 14.7 MeV

Cross-section : 28.5 mb

Data-base : Dresler(Ref.16) & Zupranska

MT=251 Mu-bar

Calculated with optical model.

MF=4 Angular Distributions of Secondary Neutrons

MT= 2 Elastic scattering based on statistical & optical model calculation.

MT= 16,22,28 & 91 The angular distributions of the secondary neutrons from (n,2n), (n,n'a), (n,n'p) & inelastic processes to the continuum levels assumed to be isotropic in the laboratory system.

MT= from 51 to 65 The angular distributions of the secondary neutrons from inelastic processes assumed to be isotropic in the c.o.m. system.

MF=5 Energy Distributions of Secondary Neutrons

MT= 16,22,28 and 91 The evaporation spectrum assumed for the secondary neutrons from (n,2n), (n,n'a), (n,n'p) & in- elastic processes.

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26-Fe- 0 MAT number = 2260

26-Fe- 0 JNDC Eval-Oct78 S.Iijima,H.Yamakoshi
Dist-Mar83 Rev1-Nov83

History

- 78-10 New evaluation for JENDL-2. Details given in Ref. /1/.
 83-03 Resonance region was revised by T.Asami and T.Narita.
 The file structure was modified and background data were
 evaluated to reproduce the same cross sections as before.
 83-11 The Q values were adjusted to threshold energies. Other
 small corrections were made.

Natural iron data constructed from Fe-isotopes. Fe-58 was ignored
 because of small abundance.

MF=1 General Information

MT=451 Descriptive data and dictionary

MF=2 Resonance Parameters

MT=151 Resolved resonances

Resonance region = 1.0E-5 eV to 250.0 keV

The multilevel Breit-Wigner formula was used. Parameters
 were adopted from the following sources.

Fe-54 : Pandey+/2/ for 0 - 680 keV. R=5.6 fm from Ref.1

Fe-56 : Perey+/3/ for -2.0 - 400 keV. R=5.4 fm from fit-
 ting to total cross section below 60 keV.

Fe-57 : Allen+/4/ for s-wave resonances, and Beer+/5/
 for p-wave resonances in 0 - 185 keV.

For Fe-56, a negative level was added at -3.75 keV with
 neutron width of 100 eV and gamma width of 1.0 eV. Neutron
 width of 27.67-keV resonance was taken as 1420 eV.

Calculated 2200 m/s cross sections and res. integrals.

	2200-m/s	res. integ.
elastic	12.44 b	-
capture	2.514 b	1.349 b
total	14.95 b	-

MF=3 Neutron Cross Sections

Below 250 keV, background cross sections were given.

MT=1 Total

For energies 250 keV - 20 meV, fine resolution data were
 taken by eye-guide using interactive display of NDES (
 Neutron Data Evaluation System) developed by T.Nakagawa at
 the Nuclear Data Center, JAERI. Below 4 MeV, data of
 Carlson+/6/ were adopted. Above 4 MeV, data of Cierjacks+
 /7/ were adopted. Spherical optical model calculation was
 also made (but not adopted as the total cross section for
 JENDL-2). Parameters are as follows.

For Fe-56

$$V = 52.644 - 0.002 * E - 0.006 * E^{*2}, \quad r_0 = 1.166, \quad a_0 = 0.371$$

$$W_s = 2.869 + 0.289 * E, \quad r_s = 1.450, \quad a_s = 0.480$$

$V_{so} = 6.138$, $r_{so} = 1.166, a_{so} = 0.371$
 For Fe-54 and -57
 $V = 50.136 - 0.150 * E$, $r_0 = 1.240, a_0 = 0.500$
 $W_s = 4.600 + 0.340 * E$, $r_s = 1.400, a_s = 0.400$
 $V_{so} = 7.00$, $r_{so} = 1.240, a_{so} = 0.500$

Energies in MeV unit, lengths in fm unit.

MT=2 Elastic scattering

Given as total minus other cross sections

MT=16 (n,2n)

Calculated using essentially the method of Pearlstein.

Normalized to experimental data at 14 MeV.

MT=4,51-91 Inelastic scattering

Level excitation cross sections were calculated for each isotope with the optical and statistical model code CASTHY /8/, and the results were modified to obtain a better fit to experimental data. The modifications are :

Fe-54 : Calculation was multiplied by a factor of 1.5.

Fe-56 : Calculation was multiplied by a factor of 1.17.

The 1st level excitation below 2.12 MeV was replaced with fine resolution data of Kinney+ /9/.

Fe-57 : CASTHY calculation for 1st level (14.4 keV)

Excitation was replaced in the energy from 14.65 keV to 200 keV by calculated cross sections from resonance parameters.

For natural iron, isotopic level excitation cross sections with about equal threshold energies were condensed together. Isotopic level schemes recommended by R.Nakasima and condensed level scheme are tabulated below. Q-values of natural iron levels were calculated from their threshold energies.

No.	-(Q-val (MeV))	Fe-54		Fe-56		Fe-57	
		E (MeV)	J-P	E (MeV)	J-P	E (MeV)	J-P
1	0.0144	-	-	-	-	0.0144	3/2-
2	0.1366	-	-	-	-	0.1366	5/2-
3	0.3666	-	-	-	-	0.3667	3/2-
4	0.7064	-	-	-	-	0.7067	5/2-
5	0.8468	-	-	0.8468	2+	-	-
6	1.0076	-	-	-	-	1.008	7/2-
7	1.1976	-	-	-	-	1.198	9/2-
8	1.2647	-	-	-	-	1.2651	1/2-
9	1.3563	-	-	-	-	1.3568	(1/2-)
10	1.4091	1.4082	2+	-	-	-	-
11	1.6271	-	-	-	-	1.6277	3/2-
12	1.7251	-	-	-	-	1.7257	3/2-
13	1.9743	-	-	-	-	1.975	(1/2-)
						1.9894	9/2-
14	2.0850	-	-	2.0851	4+	-	-
15	2.1162	-	-	-	-	2.117	5/2-
16	2.5397	2.5382	4+	-	-	-	-
17	2.5629	2.5613	0+	-	-	-	-
18	2.6574	-	-	2.6576	2+	-	-
19	2.9416	2.9499	6+	2.9417	0+	-	-
		2.9590	2+	2.9600	2+	-	-
20	3.1199	-	-	3.1200	(1+)	-	-
				3.1229	4+	-	-

3 of Natural Iron

21	3.1680	3.1661	2+	-	-
22	3.2972	3.2952	4+	-	-
23	3.3470	3.3450	3-	3.3702 2+	-
				3.3884 6+	
24	3.4451	-		3.4454 3+	-
				3.4493 1+	
25	3.6007	-		3.6009 2+	-
				3.6019 2+	
				3.6070 0+	
26	3.7478	-		3.7480 2+	-
				3.7558 6+	
27	3.8318	3.8338	4+	3.832 2+	-
				3.8565 3+	
28	4.0354	4.033	4+	4.0940 (3+)	-
		4.047	4+		
		4.072	3+		
29	4.1001	-		4.1003 (3+)	-
				4.1200 (4+)	
30	4.2656	4.263	4+	4.2982 4+	-
		4.292	0+	4.302 (0+)	
31	4.3948	-		4.3950 3+	-
				4.401 (2+)	
32	4.4582	-		4.4584 3+	-
33	4.5098	-		4.5100 3-	-

Continuum level excitation including each isotopic continuum level and 15, 16, 17, 18, 19, 20th levels of Fe-54.

Level density parameters for modified Gilbert-Cameron formula (as proposed in FPND Conf., Petten (1977) /10,11/) are as follows. For notation, see Ref. /11/.

Isotope	a (1/MeV)	T (MeV)	C (1/MeV)	EX (MeV)
Fe-54	6.19	1.45	0.532	12.0
Fe-55	6.90	1.30	1.274	9.0
Fe-56	7.58	1.27	0.746	10.0
Fe-57	8.27	1.14	1.694	7.70
Fe-58	8.45	1.18	0.742	10.0

MT=102 Capture

Background cross section was given below 3 keV. Between 3 and 800 keV, recommended cross section by Ribon /12/ was adopted. Above 800 keV, CASTHY calculation was used adjusting S-gamma to the experimental cross sections of 10 mb at 200 keV for Fe-54 and 5.5 mb at 200 keV for Fe-56. obtained effective S-gamma values are 0.34E-4 for Fe-54 and 0.18E-4 for Fe-56. The S-gamma of 3.53E-4 was used for Fe-57 without adjustment. Giant dipole resonance parameters were taken from systematics of compilation by Berman /13/.

MT=103,107 (n,p) and (n,alpha)

Adopted from experimental data. For Fe-56 (n,alpha), the same cross section as Fe-54 was adopted.

MT=251 Mu-bar

Calculated with CASTHY /8/.

MF=4 Angular Distributions of Secondary Neutrons

MT=2 : CASTHY-code calculation

MT=51-88 : Isotropic in the center-of-mass system

MT=16,91 : Isotropic in the laboratory system

MF=5 Energy Distributions of Secondary Neutrons

MT=16,91 : Evaporation spectrum

References

- 1) Iijima S. et al.: Proc. NEANDC Topical Discussions in 1979.
Kawai M.: *ibid.*
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26-Fe-54 MAT number = 2261

26-Fe-54 JNDC Eval-Oct78 S.Iijima,H.Yamakoshi
Dist-Mar83 Rev1-Feb84

History

78-10 New evaluation for JENDL-2. Details given in Ref. /1/.
83-11 Small corrections were made.
84-02 Effective scattering radius was corrected. Comment was added.

MF=1 General Information

MT=451 Descriptive data and dictionary

MF=2 Resonance Parameters

MT=151 Resolved resonances

Resonance region - $1.0E-5$ eV to 250.0 keV

The multilevel Breit-Wigner formula was used. Parameters were adopted mainly from Pandey+/2/ by assuming the average radiative width to be 2.5 eV /3/. $R=5.6$ fm was taken from Ref. /4/.

Calculated 2200-m/s cross sections and res. integrals.

	2200-m/s	Res. Integ.
elastic	0.4929 b	-
capture	2.156 b	1.33 b
total	2.649 b	-

MF=3 Neutron Cross Sections

Below 250 keV, background cross sections were given for the total and elastic scattering cross sections on the upper side of the first resonance. Above 250 keV, the cross sections were evaluated as follows.

MT=1 Total

Spherical optical model calculation was made by using code CASTHY /5/. Optical potential parameters/1/ are as follows,

$$\begin{aligned} V &= 50.136 - 0.150 * E & , r_0 &= 1.240, a_0 = 0.500 \\ W_s &= 4.600 + 0.340 * E & , r_s &= 1.400, a_s = 0.400 \\ V_{so} &= 7.00 & , r_{so} &= 1.240, a_{so} = 0.500 \end{aligned}$$

(energies in MeV, lengths in fm)

MT=2 Elastic scattering

Given as total minus other cross sections

MT=16 (n,2n)

Calculated using essentially the method of Pearlstein /6/ and normalized to experimental data at 14 MeV.

MT=4,51-91 Inelastic scattering

Level excitation cross sections were calculated with the optical and statistical model code CASTHY /5/, and the results were multiplied by a factor of 1.5 to obtain a better fit to experimental data. Level scheme was recommended by R.Nakasima /7/ as follows.

No.	Energy (MeV)	Spin-Parity
g.s.	0.0	0 +

1	1.4082	2 +
2	2.5382	4 +
3	2.5613	0 +
4	2.9499	6 +
5	2.9590	2 +
6	3.1661	2 +
7	3.2952	4 +
8	3.3450	3 -
9	3.8338	4 +
10	4.033	4 +
11	4.047	4 +
12	4.072	3 +
13	4.263	4 +
14	4.2916	0 +
15	4.578	2 +
16	4.655	2 +
17	4.696	4 +
18	4.700	3 -
19	4.780	3 -
20	4.949	4 +

Continuum levels were assumed above 5.0 MeV.

Level density parameters for modified Gilbert-Cameron formula (as proposed in FPND Conf., Petten (1977) /8.9/) are as follows. For notation, see Ref. /9/.

isotope	a(1/MeV)	T(MeV)	C(1/MeV)	Ex(MeV)
Fe-54	6.19	1.45	0.532	12.0
Fe-55	6.90	1.30	1.274	9.0

MT=102 Capture

CASTHY calculation was used adjusting S-gamma to the experimental cross sections of 10 mb at 200 keV. Obtained effective S-gamma value is $0.34E-4$. Giant dipole resonance parameters were taken from systematics of compilation by Berman /10/.

MT=103,107 (n,p) and (n,alpha)

Adopted from experimental data.

MT=251 Mu-bar

Calculated with CASTHY /5/.

MF=4 Angular Distributions of Secondary Neutrons

- MT=2 : CASTHY-code calculation
- MT=51-70 : Isotropic in the center-of-mass system
- MT=16,91 : Isotropic in the laboratory system

MF=5 Energy Distributions of Secondary Neutrons

- MT=16,91 : Evaporation spectrum

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- 1) Iijima S. et al.: Proc. NEANDC Topical Discussions in 1979.
Kawai M.: ibid.
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Yamakoshi H. et al.: J. Nucl. Sci. Technol., 17, 477 (1980).
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- 10) Berman B.L.: Atom. Data and Nucl. Data Tables, 15, No.4 (1975)

26-Fe-56 MAT number = 2262

26-Fe-56 JNDC Eval-Oct78 S.Iijima,H.Yamakoshi
Dist-Mar83 Rev1-Feb84

History

78-10 New evaluation for JENDL-2. Details given in Ref. /1/.
83-11 Small corrections were made.
84-02 Background data were modified. Comment data were added.

MF=1 General Information

MT=451 Descriptive data and dictionary

MF=2 Resonance Parameters

MT=151 Resolved resonances

Resonance region = 1.0E-5 eV to 250.0 keV

The multilevel Breit-Wigner formula was used. Parameters were adopted from the experimental data by Perey+ /2/.

R=6.5 fm was selected to reproduce the 24-keV window cross section. Neutron width of 27.67-keV resonance was taken as 1420 eV.

Calculated 2200-m/s cross sections and res. integrals.

	2200-m/s	Res. Integ.
elastic	12.46 b	-
capture	2.813 b	1.44 b
total	15.18 b	-

MF=3 Neutron Cross Sections

Below 250 keV, background cross sections were given to reproduce the thermal elastic scattering cross section of 12.46 barns /3/. Above 250 keV, cross sections were evaluated as follows.

MT=1 Total

Spherical optical model calculation was made by using CASTHY code /4/. Parameters /1/ are as follows,

$$V = 52.644 - 0.002 * E - 0.006 * E ** 2, \quad r_0 = 1.166, \quad a_0 = 0.371$$

$$W_s = 2.869 + 0.289 * E, \quad , \quad r_s = 1.450, \quad a_s = 0.480$$

$$V_{so} = 6.138, \quad , \quad r_{so} = 1.166, \quad a_{so} = 0.371$$

(energies in MeV, lengths in fm).

MT=2 Elastic scattering

Given as total minus other cross sections. Fine structure in the MeV region is due to the inelastic scattering cross section.

MT=16 (n,2n)

Calculated using essentially the method of Pearlstein /5/. Normalized to experimental data at 14 MeV.

MT=4,51-77,91 Inelastic scattering

Level excitation cross sections were calculated with the optical and statistical model code CASTHY /4/. The result was multiplied by a factor of 1.17. The 1st level excitation below 2.12 MeV was replaced with fine resolution data of Kinney+ /6/. Level scheme was recommended by R.Nakasima /7/.

No.	Energy (MeV)	Spin-Parity
g.s	0.0	0 +
1	0.8468	2 +
2	2.0851	4 +
3	2.6576	2 +
4	2.9417	0 +
5	2.9600	2 +
6	3.1200	(1 +)
7	3.1229	4 +
8	3.3702	2 +
9	3.3884	6 +
10	3.4454	3 +
11	3.4493	1 +
12	3.6009	2 +
13	3.6019	2 -
14	3.6070	0 +
15	3.7480	2 +
16	3.7558	6 +
17	3.832	2 +
18	3.8565	3 +
19	4.0940	(3 +)
20	4.1003	(3 +)
21	4.1200	(4 +)
22	4.2982	4 +
23	4.302	(0 +)
24	4.3950	3 +
25	4.401	(2 +)
26	4.4584	3 +
27	4.5100	3 -

Continuum levels were assumed above 4.6 MeV.

Level density parameters for modified Gilbert-Cameron formula (as proposed in FPND conf., Petten (1977) /8,9/) are as follows. For notation, see Ref. /9/.

isotope	a(1/MeV)	T(MeV)	C(1/MeV)	Ex(MeV)
Fe-56	7.58	1.27	0.746	10.0
Fe-57	8.27	1.14	1.694	7.70

MT=102 Capture

CASTHY calculation was used adjusting S-gamma to the experimental cross sections of 5.5 mb at 200 keV. Obtained effective S-gamma value is 0.18E-4. Giant dipole resonance parameters were taken from systematics of compilation by Berman /10/.

MT=103,107 (n,p) and (n,alpha)

Adopted were the same cross section as Fe-54 which was evaluated from experimental data.

MT=251 Mu-bar

Calculated with CASTHY /4/.

MF=4 Angular Distributions of Secondary Neutrons

MT=2 : CASTHY-code calculation

MT=51-77 : Isotropic in the center-of-mass system

MT=16,91 : Isotropic in the laboratory system

MF=5 Energy Distributions of Secondary Neutrons
MT=16,91 : Evaporation spectrum

References

- 1) Iijima S. et al.: Proc. NEANDC Topical Discussions in 1979.
Kawai M.: *ibid.*
Yoshida T.: *ibid.*
Yamakoshi H. et al.: J. Nucl. Sci. Technol., 17, 477 (1980).
Iijima S. et al.: to be published as JAERI-M report.
- 2) Perey F.G. et al.: Proc. Specialist Meeting on Neutron Data of Structural Materials for Fast Reactors, Geel, (1977), p.530.
- 3) Mughabghab S.F. et al.: Neutron Cross Sections, Vol. 1, Part A (1981).
- 4) Igarasi S. : J. Nucl. Sci. Technol., 12, 67 (1975).
- 5) Pearlstein S.: Nucl. Sci. Eng., 23, 238 (1965).
- 6) Kinney W.E. and Perey F.G.: Nucl. Sci. Eng., 63, 418 (1977).
- 7) Nakasima R.: private communication.
- 8) Gruppelaar H.: ECN-13 (1977).
- 9) Iijima S.: IAEA-213, Proc. IAEA Second Advisory Group Meeting on Fission Product Nuclear Data, Petten, (1977), p.279.
- 10) Berman B.L.: Atom. Data and Nucl. Data Tables, 15, No.4 (1975)

26-Fe- 57 MAT number = 2263

26-Fe- 57 JNDC Eval-Oct78 S.Iijima,H.Yamakoshi
Dist-Mar83 Rev1-Feb84

History

78-10 New evaluation for JENDL-2. Details given in Ref. /1/.
83-11 Small corrections were made.
84-02 Comment was added.

MF=1 General Information

MT=451 Descriptive data and dictionary

MF=2 Resonance Parameters

MT=151 Resolved resonances

Resonance region = $1.0E-5$ eV to 200.0 keV

The multilevel Breit-Wigner formula was used. Parameters were adopted from Allen+/2/ for s-wave resonances, and Beer+/3/ for p-wave resonances in 0 - 185 keV.

Calculated 2200-m/s cross sections and res. integrals.

	2200-m/s	Res. Integ.
elastic	0.2021 b	-
capture	2.462 b	1.45 b
total	2.664 b	-

MF=3 Neutron Cross Sections

Below 200 keV, background cross section was given for the capture cross section to reproduce the value of (2.48 ± 0.3) barns /4/ at 0.0253 eV. The background data for the total cross section contain also contributions from the inelastic scattering cross section. Above 200 keV, the data were evaluated as follows.

MT=1 Total

Spherical optical model calculation was made with CASTHY code /5/. Parameters /1/ are as follows,

$$\begin{aligned} V &= 50.136 - 0.150 * E & , r_0 &= 1.240, a_0 = 0.500 \\ W_s &= 4.600 + 0.340 * E & , r_s &= 1.400, a_s = 0.400 \\ V_{so} &= 7.00 & , r_{so} &= 1.240, a_{so} = 0.500 \end{aligned}$$

(energies in MeV unit, lengths in fm unit)

MT=2 Elastic scattering

Given as total minus other cross sections

MT=16 (n,2n)

Calculated using essentially the method of Pearlstein /6/, and normalized to experimental data at 14 MeV.

MT=4,51-64,91 Inelastic scattering

Level excitation cross sections were calculated with the optical and statistical model code CASTHY /5/. The calculation for 1st level (14.4 keV) excitation was replaced in the energy from 14.65 keV to 200 keV by calculated cross sections from resonance parameters.

Level scheme was recommended by R.Nakasima /7/.

No.	Energy (MeV)	Spin-Parity
g.s.	0.0	1/2 -
1	0.0144	3/2 -
2	0.1366	5/2 -
3	0.3667	3/2 -
4	0.7067	5/2 -
5	1.008	7/2 -
6	1.198	9/2 -
7	1.2651	1/2 -
8	1.3568	(1/2 -)
9	1.6277	3/2 -
10	1.7257	3/2 -
11	1.975	(1/2 -)
12	1.9894	9/2 -
13	2.117	5/2 -
14	2.207	5/2 -

Continuum levels were assumed above 2.3 MeV.

Level density parameters for modified Gilbert-Cameron formula (as proposed in FPND conf., Petten (1977) /8,9/) are as follows. For notation, see Ref. /9/.

isotope	a(1/MeV)	T(MeV)	C(1/MeV)	Ex(MeV)
Fe-57	8.27	1.14	1.694	7.70
Fe-58	8.45	1.16	0.742	10.0

MT=102 Capture

Calculated with CASTHY adopting the S-gamma of 3.53E-4.

Giant dipole resonance parameters were taken from systematics of compilation by Berman /10/.

MT=251 Mu-bar

Calculated with CASTHY /5/.

MF=4 Angular Distributions of Secondary Neutrons

MT=2 : CASTHY-code calculation

MT=51-64 : Isotropic in the center-of-mass system

MT=16.91 : Isotropic in the laboratory system

MF=5 Energy Distributions of Secondary Neutrons

MT=16.91 : Evaporation spectrum

References

- 1) Iijima S. et al.: Proc. NEANDC Topical Discussions in 1979.
Kawai M.: *ibid.*
Yoshida T.: *ibid.*
Yamakoshi H. et al.: J. Nucl. Sci. Technol., 17, 477 (1980).
Iijima S. et al.: to be published as JAERI-M report.
- 2) Allen B.J. et al.: *ibid.* (loc.cit.), p.476.
- 3) Beer H. and Spencer R.R.: KfK-2063 (1974).
- 4) Mughabghab S.F. et al.: Neutron Cross Sections, Vol. 1, Part A (1981).
- 5) Igarasi S. : J. Nucl. Sci. Technol., 12, 67 (1975).
- 6) Pearlstein S.: Nucl. Sci. Eng., 23, 238 (1965).
- 7) Nakasima R.: private communication.
- 8) Gruppelaar H.: ECN-13 (1977).
- 9) Iijima S.: IAEA-213, Proc. IAEA Second Advisory Group Meeting on Fission Product Nuclear Data, Petten, (1977), p.279.
- 10) Berman B.L.: Atom. Data and Nucl. Data Tables, 15, No.4 (1975)

26-Fe-58 MAT number = 2264

26-Fe-58 JAERI Eval-Mar76 JENDL-CG
Dist-Mar83 Rev1-Jan84

History

76-03 Evaluation for JENDL-1 /1/ was made by JENDL-1 Compilation Group.

83-03 Resonance region was revised by T.Asami (JAERI). MF=5 was also revised.

84-01 Comment was added.

MF=1 General Information

MT=451 Descriptive data and dictionary

MF=2 Resonance Parameters

MT=151 Resolved resonances

Resonance region = 1.0E-5 eV to 100.0 keV

The multilevel Breit-Wigner formula was used. Parameters were adopted from the recommended values by Mughabghab et al. /2/.

Calculated 2200-m/s cross sections and res. integrals.

	2200-m/s	res. integ.
elastic	2.821 b	-
capture	1.280 b	1.83 b
total	4.101 b	-

MF=3 Neutron Cross Sections

Below 100 keV, background cross sections were given to reproduce the thermal cross section recommended in Ref. /2/. Above 100 keV, the data were evaluated as follows.

MT=1,2,4,51-58,91,102 Total, Elastic, Inelastic and Capture

Calculated with optical and statistical model code CASTHY

/3/. Optical potential parameters were determined by

Yamakoshi /1/ to reproduce the smoothed total cross section.

$V = 46.0 - 0.25 * E_n$ (MeV), $W_i = 0.125 * E_n - 0.0004 * E_n^2$ (MeV)

$W_s = 14.0 - 0.2 * E_n$ (MeV), $V_{so} = 6.0$ (MeV)

(Gaussian form)

$R = 1.16 * a^{1/3} + 0.4821$ (fm), $a_0 = 0.62$ (fm)

$R_i = 1.16 * a^{1/3} + 0.8799$ (fm), $a_i = 0.62$ (fm)

$R_s = 1.16 * a^{1/3} + 0.8799$ (fm), $a_s = 0.7$ (fm)

$R_{so} = 1.16 * a^{1/3} - 0.3443$ (fm), $a_{so} = 0.62$ (fm)

The level scheme was taken from Refs. /4,5/ as follows.

No.	Energy (MeV)	Spin-Parity
g.s.	0.0	0 +
1	0.8106	2 +
2	1.6745	2 +
3	2.133	3 +
4	2.257	0 +
5	2.596	4 +
6	2.782	1 +
7	2.876	2 +

8 3.084 2 +

Levels above 3.15 MeV were assumed to be overlapping. The (n,2n), (n,p) and (n,alpha) reactions were considered as competing processes.

MT=16 (n,2n)

Calculated with Pearlstein's method /6/, and normalized to 1.06 barns /7/ at 14.5 MeV.

MT=103 (n,p)

Adopted from the evaluated data of Alley and Lessler /8/.

MT=107 (n,alpha)

The shape of cross section was taken from Schmit's evaluation /9/ and normalized to the data of Gardner and Yu-Wen /10/.

MT=251 Mu-bar

Calculated with CASTHY /3/.

MF=4 Angular Distributions of Secondary Neutrons

MT=2 : CASTHY-code calculation

MT=51-58 : Isotropic in the center-of-mass system

MT=16,91 : Isotropic in the laboratory system

MF=5 Energy Distributions of Secondary Neutrons

MT=16,91 : Evaporation spectrum

References

- 1) Igarasi S. et al.: JAERI 1261 (1979).
- 2) Mughabghab S.F. et al.: "Neutron Cross Sections, Vol. 1, Part A", Academic Press (1981).
- 3) Igarasi S. : J. Nucl. Sci. Technol., 12, 67 (1975).
- 4) Lederer C.M. et al.: "Table of Isotopes, Sixth Edition", John Wiley and Sons Inc. (1967).
- 5) Raman S.: Nucl. Data Sheets, 3, 145 (1970).
- 6) Pearlstein S.: Nucl. Sci. Eng., 23, 238 (1965).
- 7) Boedy Z.T.: INDC(HUN)-10 (1973).
- 8) Alley W.E. and Lessler R.M.: Nucl. Data Tables, 11, 622 (1973).
- 9) Schmit J.J: KfK-120 (1966).
- 10) Gardner L. and Yu-Wen Yu.: Nucl. Phys., 60, 49 (1964).

27-Co-59 MAT number = 2271

27-Co-59 FUJI+ Eval-Nov82 T.Aoki,T.Asami
Dist-Mar83 Rev1-Jan84

History

82-11 Evaluation was completed by T.Aoki (FUJI) and T.Asami (JAERI).
84-01 Resonance parameters were revised and comment was added.

MF=1 General Information

MT=451 Descriptive data and dictionary

MF=2 Resonance Parameters

MT=151 Resolved resonance parameters for MLBW formula

Energy range : from 1.0E-5 eV to 100 keV.

Resonance energies, neutron and radiative widths were taken from recommended values of Mughabghab et al. /1/. Radiative widths assumed for resonances whose widths were not recommended were 0.56 eV and 0.7 eV for s-wave and p-wave resonances, respectively. Two negative resonances were adopted also from Ref. /1/. The effective scattering radius and parameters of the -500-keV resonance were adjusted to reproduce the thermal cross sections recommended in Ref. /1/.

Calculated 2200-m/sec cross sections and resonance integrals.

	2200-m/sec	res. integ.
elastic	6.001 b	-
capture	37.18 b	75.6 b
total	43.18 b	-

MF=3 Neutron Cross Sections

Below 100 keV: Resonance region. Background cross sections are zero.

Above 100 keV: Data were evaluated for the following MT's.

MT= 1 total cross section
 MT= 2 elastic scattering cross section
 MT= 4 total inelastic scattering cross section
 MT= 16 (n,2n) cross section
 MT=51-57 inelastic scattering cross sections to discrete levels
 MT= 91 inelastic scattering cross section to continuum levels
 MT=102 capture cross section
 MT=103 (n,p) cross section
 MT=107 (n,alpha) cross section
 MT=251 mu-bar

Cross sections were calculated with optical and statistical model code CASTHY /2/. The optical potential parameters were selected by Kawai /3/ to reproduce average total cross section in the high energy region.

$V = 49.69 - 0.135 \cdot E_n$, $W_s = 4.931 - 0.198 \cdot E_n$, $V_{so} = 7.00$ (MeV)
 $r = 1.240$, $r_s = 1.400$, $r_{so} = 1.240$ (fm)
 $a = 0.541$, $b = 0.400$, $a_{so} = 0.541$ (fm)

The inelastic scattering cross sections were given for seven

discrete levels of which level scheme was taken from Ref. /4/.

No.	Energy (MeV)	Spin-Parity
g.s.	0.0	7/2 -
1	1.099	3/2 -
2	1.292	3/2 -
3	1.434	1/2 -
4	1.482	5/2 +
5	1.745	7/2 -
6	2.063	7/2 -
7	2.088	9/2 -

Levels above 2.154 MeV were assumed to be continuum. The level density parameters of Gilbert and Cameron /5/ were used. The (n,2n), (n,p) and (n, α) cross sections were taken into account as competing processes. The evaluation of these cross sections were made as follows.

(n,2n) based on the experimental data of Paulsen and Liskien /6/.

(n,p) calculated with GNASH /7/, and normalized to the experimental data of Smith and Meadows /8,9/ at 5 MeV.

(n, α) evaluated from the experimental data of Santry and Butler /10/.

The μ -bar was also calculated with CASTHY /2/.

MF=4 Angular Distributions of Secondary Neutrons

MT=2,51-57 : Calculated with CASTHY /2/.

MT=16 : Assumed to be isotropic in the laboratory system.

MT=91 : Calculated with CASTHY /2/.

MF=5 Energy Distributions of Secondary Neutrons

MT=16,91 : Evaporation spectra.

References

- 1) Mughabghab S.F. et al.: "Neutron Cross Sections, Vol. 1, Part A.", Academic Press, (1981).
- 2) Igarasi S.: J. Nucl. Sci. Technol., 61, 477 (1976).
- 3) Kawai M.: Contribution to 1979 NEANDCc Topical Discussions.
- 4) Lederer C.M. and Shirley V.S. (Ed.): "Table of Isotopes 7th Ed.", Wiley-Interscience (1978).
- 5) Gilbert A. and Cameron A.G.W.: Can. J. Phys., 43, 1446 (1965).
- 6) Paulsen A. and Liskien H.: J. Nucl. Energy, AB19, 907 (1965).
- 7) Young P.G. and Arthur E.D.: LA-6947 (1977).
- 8) Smith D.L. and Meadows J.W.: ANL/NDM-10 (1975).
- 9) Smith D.L. and Meadows J.W.: Nucl. Sci. Eng., 60, 187 (1976).
- 10) Santry D.C. and Butler J.P.: Can. J. Phys., 42, 1030 (1964).

28-Ni- 0 MAT number = 2280

28-Ni- 0 JAERI Eval-Nov79 Y.Kikuchi and N.Sekine
Dist-Dec79 Rev1-Nov83

History

79-11 New evaluation for JENDL-2. MF's 2, 3 and 4 were relieved
as JENDL-2B /1/.
83-03 MF 5 was added as final JENDL-2 data.
83-11 Comment was added.

MF=1, MT=451 Comments and dictionary

MF=2, MT=151 Resolved resonance parameters : 1.0E-5 eV - 600 keV
Evaluation based on the following data.

Ni-58 : Trans. : Perey+/2/ , Syme+/3/ , Farrel+/5/
Capt. : Perey+/2/ , Froehner/4/ , Hockenbury+/6/
Ni-60 : Trans. : Syme+/3/ , Stieglitz+/7/ , Farrel+/5/
Capt. : Froehner/4/ , Stieglitz+/7/ , Hockenbury+/6/
Ni-61 : Trans. : Cho+/8/
Capt. : Froehner/4/ , Hockenbury+/5/
Ni-62 : Trans. : Beer+/9/ , Farrel+/5/
Capt. : Beer+/9/
Ni-64 : Trans. : Beer+/9/ , Farrel+/5/
Capt. : Beer+/9/

A negative resonance added for Ni-58.

Assumed Gam-g : 2 eV for s-wave res. and 1 eV for p-wave.

Calculated 2200 m/s values and resonance integrals (barn):

	2200 m/s value	res.int.
total	21.20	-
elastic	16.77	-
capture	4.429	2.22

MF=3 Neutron Cross Sections

Background cross sections (BGCS) applied to resonance region.

MT=1,2 : Positive or negative BGCS to compensate errors
due to constant R and resonance truncation /10/.

MT=102 : Smooth positive BGCS above 10 keV.

Cross sections above resonance region evaluated as follows :

MT=1 : Total cross section

Calculated with optical model.

Potential parameters obtained by fitting nat-Ni data /11/:

$V = 51.33 - 0.331 * E_n$, $W_s = 8.068 + 0.112 * E_n$, $V_{so} = 7.0$ (MeV)
 $r_0 = r_{so} = 1.24$, $r_s = 1.40$ (fm)
 $a_0 = a_{so} = 0.541$, $b = 0.4$ (fm)

MT=2 : Elastic scattering

(Total) - (All the other partial cross sections).

MT=16 : (n,2n)

Ni-58

2 of Natural Nickel

Data of JENDL-1, evaluated on the basis of plenty experimental data, extended up to 20 MeV.

Ni-60, -61, -62, -64

Calculated with evaporation model.

MT=17 : (n,3n) given only for Ni-64.

Calculated with evaporation model.

MT=22 : (n,na) given only for Ni-58.

Evaluated on the analogy of Cu-65 (n,na) cross section.

MT=28 : (n,np)

Calculated with evaporation model.

MT=51-90,91 : Inelastic scattering

Calculated with the statistical model code CASTHY /12/.

Competing processes : (n,2n), (n,3n), (n,np), (n,na),
(n,p), (n,a).

Level fluctuation considered.

Inelastic scattering to the 1st level for even-A isotopes evaluated on the basis of experimental data up to 7 MeV.

Direct reaction calculated with DWBA and added above 7 MeV

The level scheme for each isotope taken from Ref./13/.

Ni-58	No	Energy (MeV)	Spin-Parity	No	Energy (MeV)	Spin-Parity
g.s.	0		0 +	12	3.6206	4 +
1	1.4545		2 +	13	3.7757	4 +
2	2.4595		4 +	14	3.8989	2 +
3	2.7757		2 +	15	4.1080	2 +
4	2.9026		1 +	16	4.2900	3 +
5	2.9428		0 +	17	4.3430	6 +
6	3.0383		2 +	18	4.3490	4 +
7	3.2645		2 +	19	4.3800	5 -
8	3.4208		3 +	20	4.4010	4 +
9	3.5240		4 +	21	4.4498	0 +
10	3.5313		0 +	22	4.4720	3 -
11	3.5942		1 +			

continuum levels assumed above 4.517 MeV.

Ni-60	No	Energy (MeV)	Spin-Parity	No	Energy (MeV)	Spin-Parity
g.s.	0		0 +	12	3.3183	0 +
1	1.3325		2 +	13	3.3810	4 +
2	2.1589		2 +	14	3.3936	2 +
3	2.2848		0 +	15	3.5300	0 +
4	2.5058		4 +	16	3.5890	3 +
5	2.6262		3 +	17	3.6197	3 +
6	3.1190		4 +	18	3.6710	4 +
7	3.1241		2 -	19	3.7290	3 +
8	3.1300		4 +	20	3.7355	1 +
9	3.1864		3 +	21	3.7410	0 +
10	3.1941		1 +	22	3.8714	2 +
11	3.2694		2 +			

Continuum levels assumed above 3.895 MeV.

Ni-61	No	Energy (MeV)	Spin-Parity	No	Energy (MeV)	Spin-Parity
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3 of Natural Nickel

g.s.	0	3/2 -	11	1.7298	3/2 -
1	0.0674	5/2 -	12	1.8080	7/2 -
2	0.2830	1/2 -	13	1.9780	9/2 +
3	0.6560	3/2 -	14	1.9970	3/2 -
4	0.9088	5/2 -	15	2.0030	7/2 -
5	1.0150	7/2 -	16	2.0190	7/2 -
6	1.1000	3/2 -	17	2.1140	9/2 +
7	1.1323	5/2 -	18	2.1230	1/2 -
8	1.1857	3/2 -	19	2.4100	5/2 -
9	1.4580	7/2 -	20	2.4660	7/2 -
10	1.6100	5/2 -			

Continuum levels assumed above 2.528 MeV.

Ni-62			Ni-62		
No	Energy (MeV)	Spin-Parity	No	Energy (MeV)	Spin-Parity
g.s.	0	0 +	11	3.2699	2 +
1	1.1729	2 +	12	3.2774	4 +
2	2.0486	0 +	13	3.3703	1 +
3	2.3018	2 +	14	3.4620	4 -
4	2.3364	4 +	15	3.4860	0 +
5	2.8912	0 +	16	3.5185	2 +
6	3.0582	2 +	17	3.5229	3 +
7	3.1580	2 +	18	3.7570	3 -
8	3.1765	4 +	19	3.8493	1 +
9	3.2577	2 +	20	3.8530	2 +
10	3.2620	4 +	21	3.8600	2 +

Continuum levels assumed above 3.967 MeV.

Ni-64			Ni-64		
No	Energy (MeV)	Spin-Parity	No	Energy (MeV)	Spin-Parity
g.s.	0	0 +	11	3.393	3 +
1	1.3459	2 +	12	3.459	1 +
2	2.2750	0 +	13	3.483	4 +
3	2.6080	4 +	14	3.560	3 -
4	2.7500	2 +	15	3.647	2 +
5	2.8650	0 +	16	3.748	4 +
6	2.8850	2 +	17	3.795	1 +
7	2.9710	2 +	18	3.808	3 +
8	3.0280	0 +	19	3.848	5 -
9	3.1650	4 +	20	3.965	4 +
10	3.2730	2 +			

Continuum levels assumed above 4.084 MeV.

The inelastic levels of each isotope are grouped in natural Nickel file as follows :

MT	-Q (MeV)	Ni-58	Ni-60	Ni-61	Ni-62	Ni-64
51	0.0674	-	-	51	-	-
52	0.2828	-	-	52	-	-
53	0.6556	-	-	53	-	-
54	0.9082	-	-	54	-	-
55	1.0144	-	-	55	-	-
56	1.0993	-	-	56,57	-	-
57	1.1719	-	-	58	51	-
58	1.3320	-	51	-	-	51
59	1.4549	51	-	59,60	-	-
				61,62	-	-
60	1.9768	-	-	63,64	52	-
				65,66		

4 of Natural Nickel

		67,68				
61	2.1582	-	52	-	-	52
62	2.2840	-	53	69	53,54	-
63	2.4601	52	-	70	-	-
64	2.5049	-	54	-	-	53
65	2.6253	-	55	-	-	54
66	2.7763	53	-	-	55	55,56
67	2.9033	54	-	-	-	-
68	2.9435	55	-	-	-	57,58
69	3.0390	56	-	-	56	-
70	3.1179	-	56,57	-	57,58	59
			58			
71	3.1853	-	59,60	-	59,60	-
72	3.2652	57	61	-	61,62	60
73	3.3172	-	62	-	63	-
74	3.3798	-	63,64	-	-	61
75	3.4216	58	-	-	64,65	62,63
					66,67	
76	3.5248	59,60	65	-	-	64
77	3.5878	61	66	-	-	65
78	3.6185	62	67	-	-	-
79	3.6697	-	68	-	-	-
80	3.7277	-	69,70	-	68	66
			71			
81	3.7761	63	-	-	69,70	67,68
					71	69
82	3.8701	-	72	-	-	-
83	3.8998	64	-	-	-	70
84	4.1089	65	-	-	-	-
85	4.2910	67	-	-	-	-
86	4.3440	68,69	-	-	-	-
87	4.3810	70	-	-	-	-
88	4.4020	71	-	-	-	-
89	4.4508	72	-	-	-	-
90	4.4730	73	-	-	-	-
91	2.5264	91	91	91	91	91

The level density parameters evaluated by Yoshida /14/.

Ni-isotope	57	58	59	60	61
a (1/MeV)	5.00	6.45	6.97	7.55	8.14
Delta (MeV)	1.20	2.47	1.20	2.47	1.20
Ex (MeV)	6.33	7.30	8.00	10.00	7.00
Tc (MeV)	1.44	1.49	1.35	1.26	1.17
Ni-isotope	62	63	64	65	
a (1/MeV)	8.77	9.37	9.98	10.57	
Delta (MeV)	2.60	1.20	2.70	1.20	
Ex (MeV)	9.00	3.00	4.32	4.00	
Tc (MeV)	1.08	1.36	1.15	0.947	

MT=102 : Capture

Calculated with the statistical model code CASTHY /12/.

Competing processes : (n,2n), (n,3n), (n,np), (n,na),
(n,p), (n,a).

Level fluctuation considered.

5 of Natural Nickel

The gamma-ray strength function obtained from the capture cross section of natural-Ni ; 9.6 mb at 450 keV.

Ni-58 : 4.62E-5 , Ni-60 : 2.77E-5
 Ni-61 : 1.94E-4 , Ni-62 : 9.52E-6
 Ni-64 : 5.87E-6

MT=103 : (n,p)
 Ni-58, Ni-60

Data of JENDL-1, evaluated on the basis of plenty experimental data, extended up to 20 MeV.

Ni-61, -62, -64

Evaluated on the analogy of Ni-60 (n,p) cross section.

MT=107 : (n,a)

Evaluated on the analogy of Co-59 (n,a) cross section.

MT=251 : Mu-bar

Calculated with CASTHY /12/.

MF=4 Angular Distributions of Secondary Neutrons

MT=2 : Calculated with optical model.

MT=16,17,22,28,91 : Isotropic in laboratory system.

MT=51-90 : Isotropic in center of mass system.

MF=5 Energy Distributions of Secondary Neutrons

MT=16,17,22,28,91 : Evaporation spectrum.

References

- 1) Kikuchi Y. et al.: J.Nucl.Sci.Technol.,17,567(1980).
- 2) Perey F.G et al.: Neutron Data of Structural Materials for FBR, 1977 Geel Meet., p.503, Pergamon Press(1979).
- 3) Syme D.B. et al.: ibid,p.703.
- 4) Froehner F. : ibid,p.138.
- 5) Farrell J.A. et al.: Ann.Phys.,37,367 (1966).
- 6) Hockenbury R.W. et al.: Phys.Rev.,178,1746 (1969).
- 7) Stieglitz R.G. et al.: Nucl.Phys.,A163,592 (1971).
- 8) Cho et al.: Nuclear Data for Reactors, Proc. 1970 Helsinki Conf., p.619, IAEA(1970).
- 9) Beer H. and Spencer R.R.: Nucl.Phys.,A240,29 (1975).
- 10) Kikuchi Y. and Sekine N. : to be published as JAERI-M report.
- 11) Kawai M. : unpublished.
- 12) Igarasi S.: J.Nucl.Sci.Technol.,12,67 (1975).
- 13) Lederer C.M. and Shirley V.S.: Table of Isotopes,7th Edition, Wiley-Interscience (1978).
- 14) Yoshida T. : unpublished.

28-Ni- 58 MAT number = 2281

28-Ni- 58 JAERI Eval-Aug82 Y.Kikuchi and N.Sekine
Dist-Mar83 Rev1-Nov83

History

82-08 New evaluation for JENDL-2 was made by Y.Kikuchi (JAERI) and
N.Sekine (HEC)
83-11 Comment was added.

MF=1,MT=451 Comments and dictionary

MF=2,MT=151 Resolved resonance parameters : 1.0E-5 eV - 600 keV
Evaluation based on the following data.
Transmission : Perey+/1/ , Syme+/2/ ,Farrel+/4/ ,
Capture : Perey+/1/ , Froehner/3/ ,Hockenbury+/5/ .
Two negative resonances added.
Assumed Gam-g : 2 eV for s-wave res. and 1 eV for p-wave.

Calculated 2200 m/s values and resonance integrals (barn):

	2200 m/s value	res. int.
total	30.62	-
elastic	26.02	-
capture	4.605	2.21

MF=3 Neutron Cross Sections

Background cross sections (BGCS) applied to resonance region.

MT=1,2 : Many point BGCS to compensate errors due to constant
R and resonance truncation /6/.

MT=102 : Smooth BGCS to correct p-wave level missing above
200 keV.

Cross sections above 600 keV evaluated as follows :

MT=1 : Total cross section

Calculated with optical model.

Potential parameters obtained by fitting nat-Ni data /7/:

$V = 51.33 - 0.331 * E_n$, $W_s = 8.068 + 0.112 * E_n$, $V_{so} = 7.0$ (MeV)
 $r_0 = r_{so} = 1.24$, $r_s = 1.40$ (fm)
 $a_0 = a_{so} = 0.541$, $b = 0.4$ (fm)

MT=2 : Elastic scattering

(Total) - (All the other partial cross sections).

MT=16,103 : (n,2n), (n,p)

Data of JENDL-1, evaluated on the basis of plenty experimen
tal data, extended up to 20 MeV.

MT=22 : (n,n'a)

Evaluated on the analogy of Cu-65(n,na) cross section.

MT=28 : (n,n'p)

Calculated with evaporation model.

MT=51 : Inelastic scattering to the 1st level
 Evaluated on the basis of experimental data up to 7 MeV.
 Direct reaction calculated with DWBA and added above 7 MeV

MT=52-72,91,102 : Inelastic scattering and capture
 Calculated with the statistical model code CASTHY /8/.
 Competing processes : (n,2n), (n,p), (n,a), (n,np), (n,na).
 Level fluctuation considered.
 The level scheme taken from Ref./9/.

No	Energy (MeV)	Spin-Parity
g.s.	0.0	0 +
1	1.4545	2 +
2	2.4595	4 +
3	2.7757	2 +
4	2.9026	1 +
5	2.9428	0 +
6	3.0383	2 +
7	3.2645	2 +
8	3.4203	3 +
9	3.5240	4 +
10	3.5313	0 +
11	3.5942	1 +
12	3.6206	4 +
13	3.7757	4 +
14	3.8989	2 +
15	4.1080	2 +
16	4.2900	3 +
17	4.3430	6 +
18	4.3490	4 +
19	4.3800	5 -
20	4.4010	4 +
21	4.4498	0 +
22	4.4720	3 -

Continuum levels assumed above 4.517 MeV.
 The level density parameters evaluated by Yoshida /10/.

Ni-isotope	57	58	59
a (1/MeV)	5.00	6.45	6.97
Delta (MeV)	1.20	2.47	1.20
Ex (MeV)	6.33	7.30	8.00
Tc (MeV)	1.44	1.49	1.35

The gamma-ray strength function of $4.62E-5$ obtained from the capture cross section of natural-Ni.

MT=107 : (n,a)
 Evaluated on the analogy of Co-59(n,a) cross section.

MT=251 : Mu-bar
 Calculated with optical model.

MF=4 Angular Distributions of Secondary Neutrons
 MT=2 : Calculated with optical model.
 MT=16,22,28 : Isotropic in the laboratory system.
 MT=51-72 : 90 degree symmetric in the center-of-mass system, calculated with CASTHY.
 MT=91 : 90 degree symmetric in the laboratory system, calculated with CASTHY.

MF=5 Energy Distributions of Secondary Neutrons
MT=16,22,28,91 : Evaporation spectrum.

References

- 1) Perey F.G. et al.: Neutron Data of Structural Materials for FBR, 1977 Geel Meet., p.503, Pergamon Press (1979).
- 2) Syme D.B. et al.: *ibid*, p.703.
- 3) Froehner F. : *ibid*, p.138.
- 4) Farrell J.A. et al.: *Ann.Phys.*, **37**, 367 (1966).
- 5) Hockenbury R.W. et al.: *Phys.Rev.*, **178**, 1746 (1969).
- 6) Kikuchi Y. and Sekine N. : to be published as JAERI-M report.
- 7) Kawai M. : unpublished.
- 8) Igarasi S.: *J.Nucl.Sci.Technol.*, **12**, 67 (1975).
- 9) Lederer C.M. and Shirley V.S.: *Table of Isotopes*, 7th Edition, Wiley-Interscience (1978).
- 10) Yoshida T. : unpublished.

28-Ni-60 MAT number = 2282

28-Ni-60 JAERI Eval-Aug82 Y.Kikuchi and N.Sekine
Dist-Mar83 Rev1-Nov83

History

82-08 New evaluation for JENDL-2 was made by Y.Kikuchi (JAERI) and N.Sekine (HEC).

83-11 Comment was added.

MF=1,MT=451 Comments and dictionary

MF=2,MT=151 Resolved resonance parameters : 1.0E-5 eV - 600 keV
Evaluation based on the following data.

Transmission : Syme+/1/, Stieglitz+/3/, Farrel+/4/,

Capture : Froehner/2/, Stieglitz-/3/, Hockenbury-/5/

A negative resonance added.

Assumed Gam-g : 2 eV for s-wave res. and 1 eV for p-wave.

Calculated 2200 m/s values and resonance integrals (barn):

	2200 m/s value	res. int.
total	3.813	-
elastic	1.013	-
capture	2.801	1.50

MF=3 Neutron Cross Sections

Background cross sections (BGCS) applied to resonance region.

MT=1,2 : Many point BGCS to compensate errors due to constant R and resonance truncation /6/.

MT=102 : Smooth BGCS near 12.5 keV and above 150 keV.

Cross sections above 600 keV evaluated as follows :

MT=1 : Total cross section

Calculated with optical model.

Potential parameters obtained by fitting nat-Ni data /7/:

$V = 51.33 - 0.331 * E_n$, $W_s = 8.068 + 0.112 * E_n$, $V_{so} = 7.0$ (MeV)

$r_0 = r_{so} = 1.24$, $r_s = 1.40$ (fm)

$a_0 = a_{so} = 0.541$, $b = 0.4$ (fm)

MT=2 : Elastic scattering

(Total) - (All the other partial cross sections).

MT=16,28 : (n,2n) and (n,np)

Calculated with evaporation model.

MT=51 : Inelastic scattering to the 1st level

Evaluated on the basis of experimental data up to 7 MeV.

Direct reaction calculated with dwba and added above 7 MeV

MT=52-72,91,102 : Inelastic scattering and capture

Calculated with the statistical model code CASTHY /8/.

Competing processes : (n,2n), (n,p), (n, α), (n,np).

Level fluctuation considered.

The level scheme taken from Ref./9/.

No	Energy (MeV)	Spin-Parity
g.s.	0	0 +
1	1.3325	2 +
2	2.1589	2 +
3	2.2848	0 +
4	2.5058	4 +
5	2.6262	3 +
6	3.1190	4 +
7	3.1241	2 +
8	3.1300	4 +
9	3.1864	3 +
10	3.1941	1 +
11	3.2694	2 +
12	3.3183	0 +
13	3.3810	4 +
14	3.3936	2 +
15	3.5300	0 +
16	3.5890	3 +
17	3.6197	3 +
18	3.6710	4 +
19	3.7290	3 +
20	3.7355	1 +
21	3.7410	0 +
22	3.8714	2 +

Continuum levels assumed above 3.895 MeV.

The level density parameters evaluated by Yoshida /10/.

Ni-isotope	59	60	61
a (1/MeV)	6.97	7.55	8.14
Delta (MeV)	1.20	2.47	1.20
Ex (MeV)	8.00	10.00	7.00
Tc (MeV)	1.35	1.26	1.17

The gamma-ray strength function of $2.31E-5$ obtained from the capture cross section data of Ernst+/11/.

MT=103 : (n,p)

Data of JENDL-1, evaluated on the basis of plenty experimental data, extended up to 20 MeV.

MT=107 : (n,a)

Evaluated on the analogy of Co-59(n,a) cross section.

MT=251 : Mu-bar

Calculated with optical model.

MF=4 Angular Distributions of Secondary Neutrons

MT=2 : Calculated with optical model.

MT=16,28 : Isotropic in the laboratory system.

MT=51-72 : 90 degree symmetric in the center-of-mass system, calculated with CASTHY.

MT=91 : 90 degree symmetric in the laboratory system, calculated with CASTHY.

MF=5 Energy Distributions of Secondary Neutrons

MT=16,28,91 : Evaporation spectrum.

References

- 1) Syme D.B. et al.: Neutron Data of Structural Materials for FBR, 1977 Geel Meet., p.703, Pergamon Press (1979).
- 2) Froehner F. : *ibid*, p.138.
- 3) Stieglitz R.G. et al.: Nucl.Phys., A163, 592 (1971).
- 4) Farrell J.A. et al.: Ann.Phys., 37, 367 (1966).
- 5) Hockenbury R.W. et al.: Phys.Rev., 178, 1746 (1969).
- 6) Kikuchi Y. and Sekine N. : to be published as JAERI-M report.
- 7) Kawai M. : unpublished.
- 8) Igarasi S.: J.Nucl.Sci.Technol., 12, 67 (1975).
- 9) Lederer C.M. and Shirley V.S.: Table of Isotopes, 7th Edition, Wiley-Interscience (1978).
- 10) Yoshida T. : unpublished.
- 11) Ernst A. et al.: Nuclear Data for Reactors, Proc. 1970 Helsinki Conf, p.633, IAEA (1970)

2	0.2830	1/2 -
3	0.6560	3/2 -
4	0.9088	5/2 -
5	1.0150	7/2 -
6	1.1000	3/2 -
7	1.1323	5/2 -
8	1.1857	3/2 -
9	1.4580	7/2 -
10	1.6100	5/2 -
11	1.7298	3/2 -
12	1.8080	7/2 -
13	1.9780	9/2 +
14	1.9970	3/2 -
15	2.0030	7/2 -
16	2.0190	7/2 -
17	2.1140	9/2 +
18	2.1230	1/2 -
19	2.4100	5/2 -
20	2.4660	7/2 -

Continuum levels assumed above 2.528 MeV.

The level density parameters evaluated by Yoshida /8/

Ni-isotope	60	61	62
a (1/MeV)	7.55	8.14	8.77
Delta (MeV)	2.47	1.20	2.60
Ex (MeV)	10.00	7.00	9.00
Tc (MeV)	1.26	1.17	1.08

The gamma-ray strength function of $4.65E-4$ obtained from the capture cross section data of Ernst+ /10/

MT=103 : (n,p)

Evaluated on the analogy of Ni-60(n,p) cross section.

MT=107 : (n,a)

Evaluated on the analogy of Co-59(n,a) cross section.

MT=251 : Mu-bar

Calculated with optical model.

MF=4 Angular Distributions of Secondary Neutrons

MT=2 : Calculated with optical model.

MT=16,28 : Isotropic in the laboratory system.

MT=51-70 : 90 degree symmetric in the center-of-mass system, calculated with CASTHY.

MT=91 : 90 degree symmetric in the laboratory system, calculated with CASTHY.

MF=5 Energy Distributions of Secondary Neutrons

MT=16,28,91 : Evaporation spectrum.

References

- 1) Cho et al.: Nuclear Data for Reactors, Proc. 1970 Helsinki Conf., p.619, IAEA(1970).
- 2) Froehner F. : Neutron Data of Structural Materials for FBR, 1977 Geel Meet., p.138, Pergamon Press(1979).
- 3) Hockenbury R.W. et al.: Phys.Rev.,178,1746 (1969).
- 4) Kikuchi Y. and Sekine N. : to be published as JAERI-M report.

- 5) Kawai M. : unpublished.
- 6) Igarasi S. : J.Nucl.Sci.Technol.,12,67 (1975).
- 7) Lederer C.M. and Shirley V.S. : Table of Isotopes, 7th Edition, Wiley-Interscience (1978).
- 8) Yoshida T. : unpublished.
- 9) Ernst A. et al. : Nuclear Data for Reactors, Proc. 1970 Helsinki Conf., p.633, IAEA (1970).

28-Ni-62 MAT number = 2284

28-Ni-62 JAERI Eval-Aug82 Y.Kikuchi and N.Sekine
Dist-Mar83 Rev1-Nov83

History

82-08 New evaluation for JENDL-2 was made by Y.Kikuchi (JAERI) and N.Sekine (hec).

83-11 Comment was added.

MF=1,MT=451 Comments and dictionary

MF=2,MT=151 Resolved resonance parameters : 1.0E-5 eV - 600 keV

Evaluation based on the following data.

Transmission : Beer+/1/ ,Farrel+/2/,

Capture : Beer+/1/

Assumed Gam-g : 2 eV for s-wave res. and 1 eV for p-wave.

Calculated 2200 m/s values and resonance integrals (barn):

	2200 m/s value	Res.Int
total	23.70	-
elastic	9.505	-
capture	14.20	6.91

MF=3 Neutron Cross Sections

Background cross sections (BGCS) applied to resonance region.

MT=1,2 : Many point BGCS to compensate errors due to constant R and resonance truncation /3/.

MT=102 : Smooth BGCS above 150 keV.

Cross sections above 600 keV evaluated as follows :

MT=1 : Total cross section

Calculated with optical model.

Potential parameters obtained by fitting nat-Ni data /4/:

$V = 51.33 - 0.331 * E_n$, $W_s = 8.068 + 0.112 * E_n$, $V_{so} = 7.0$ (MeV)

$r_0 = r_{so} = 1.24$, $r_s = 1.40$ (fm)

$a_0 = a_{so} = 0.541$, $b = 0.4$ (fm)

MT=2 : Elastic scattering

(Total) - (All the other partial cross sections).

MT=16,28 : (n,2n) and (n,np)

Calculated with evaporation model.

MT=51 : Inelastic scattering to the 1st level

Evaluated on the basis of experimental data up to 7 MeV.

Direct reaction calculated with DWBA and added above 7 MeV.

MT=52,71,91,102 : Inelastic scattering and capture

Calculated with the statistical model code CASTHY /5/.

Competing processes : (n,2n), (n,p), (n,a), (n,np).

Level fluctuation considered.

The level scheme taken from Ref./6/.

No	Energy (MeV)	Spin-Parity
g.s.	0	0 +
1	1.1729	2 +
2	2.0486	0 +
3	2.3018	2 +
4	2.3364	4 +
5	2.8912	0 +
6	3.0582	2 +
7	3.1580	2 +
8	3.1765	4 +
9	3.2577	2 +
10	3.2620	4 +
11	3.2699	2 +
12	3.2774	4 +
13	3.3703	1 +
14	3.4620	4 +
15	3.4860	0 +
16	3.5185	2 +
17	3.5229	3 +
18	3.7570	3 -
19	3.8493	1 +
20	3.8530	2 +
21	3.8600	2 +

Continuum levels assumed above 3.967 MeV.

The level density parameters evaluated by Yoshida /7/.

Ni-isotope	61	62	63
a (1/MeV)	8.14	8.77	9.37
Delta (MeV)	1.20	2.60	1.20
Ex (MeV)	7.00	9.00	3.00
Tc (MeV)	1.17	1.08	1.36

The gamma-ray strength function of $1.38E-5$ obtained from the capture cross section data of Beer+/1/.

MT=103 : (n,p)

Evaluated on the analogy of Ni-60(n,p) cross section.

MT=107 : (n,a)

Evaluated on the analogy of Co-59(n,a) cross section.

MT=251 : Mu-bar

Calculated with optical model.

MF=4 Angular Distributions of Secondary Neutrons

MT=2 : Calculated with optical model.

MT=16,28 : Isotropic in the laboratory system.

MT=51-71 : 90 degree symmetric in the center-of-mass system, calculated with CASTHY.

MT=91 : 90 degree symmetric in the laboratory system, calculated with CASTHY.

MF=5 Energy Distributions of Secondary Neutrons

MT=16,28,91 : Evaporation spectrum.

References

- 1) Beer H. and Spencer R.R.: Nucl.Phys., A240, 29 (1975).
- 2) Farrell J.A. et al.: Ann.Phys., 37, 367 (1966).

- 3) Kikuchi Y. and Sekine N. : to be published as JAERI-M report.
- 4) Kawai M. : unpublished.
- 5) Igarasi S. : J.Nucl.Sci.Technol.,12,67 (1975).
- 6) Lederer C.M. and Shirley V.S. : Table of Isotopes,7th Edition,
Wiley-Interscience (1978).
- 7) Yoshida T. : unpublished.

28-Ni- 64 MAT number = 2285

28-Ni- 64 JAERI Eval-Aug82 Y.Kikuchi and N.Sekine
Dist-Mar83 Rev1-Nov83

History

82-08 New evaluation for JENDL-2 was made by Y.Kikuchi (JAERI) and N. Sekine (HEC).

83-11 Comment was added.

MF=1,MT=451 Comments and dictionary

MF=2,MT=151 Resolved resonance parameters : 1.0E-5 eV - 600 keV
Evaluation based on the following data.

Transmission : Beer+/1/ ,Farrel+/2/,

Capture : Beer+/1/

Assumed Γ_{avg} : 2 eV for s-wave res. and 1 eV for p-wave.

Calculated 2200 m/s values and resonance integrals (barn):

	2200 m/s value	Res.Int
total	1.515	-
elastic	0.003464	-
capture	1.480	0.819

MF=3 Neutron Cross Sections

Background cross sections (BGCS) applied to resonance region.

MT=1,2 : Many point bgcs to compensate errors due to constant R and resonance truncation /3/.

MT=102 : Smooth bgcs above 370 keV.

Cross sections above 600 keV evaluated as follows :

MT=1 : Total cross section

Calculated with optical model.

Potential parameters obtained by fitting nat-Ni data /4/:

$V = 51.33 - 0.331 * E_n$, $W_s = 8.068 + 0.112 * E_n$, $V_{so} = 7.0$ (MeV)

$r_0 = r_{so} = 1.24$, $r_s = 1.40$ (fm)

$a_0 = a_{so} = 0.541$, $b = 0.4$ (fm)

MT=2 : Elastic scattering

(Total) - (All the other partial cross sections).

MT=16,17 : (n,2n) and (n,3n)

Calculated with evaporation model.

MT=51 : Inelastic scattering to the 1st level

Direct reaction calculated with DWBA, added above 7 MeV

MT=52-70,91,102 : Inelastic scattering and capture

Calculated with the statistical model code CASTHY /5/.

Competing processes : (n,2n), (n,3n), (n,p), (n,a).

Level fluctuation considered.

The level scheme taken from Ref./6/.

No	Energy (MeV)	Spin-Parity
----	--------------	-------------

g.s.	0	0 +
1	1.3459	2 +
2	2.2750	0 +
3	2.6080	4 +
4	2.7500	2 +
5	2.8650	0 +
6	2.8850	2 +
7	2.9710	2 +
8	3.0280	0 +
9	3.1650	4 +
10	3.2730	2 +
11	3.393	3 +
12	3.459	1 +
13	3.483	4 +
14	3.560	3 -
15	3.647	2 +
16	3.748	4 +
17	3.795	1 +
18	3.808	3 +
19	3.848	5 -
20	3.965	4 +

Continuum levels assumed above 4.084 MeV.

The level density parameters evaluated by Yoshida /7/.

Ni-isotope	62	63	64	65
a (1/MeV)	8.77	9.37	9.98	10.57
Delta (MeV)	2.60	1.20	2.70	1.20
Ex (MeV)	9.00	3.00	4.32	4.00
Tc (MeV)	1.08	1.36	1.15	0.947

The gamma-ray strength function of $7.67E-6$ obtained from the capture cross section data of Beer+/1/.

MT=103 : (n,p)

Evaluated on the analogy of Ni-60(n,p) cross section.

MT=107 : (n,a)

Evaluated on the analogy of Co-59(n,a) cross section.

MT=251 : Mu-bar

Calculated with optical model.

MF=4 Angular Distributions of Secondary Neutrons

MT=2 : Calculated with optical model.

MT=16,17 : Isotropic in the laboratory system.

MT=51-70 : 90 degree symmetric in the center-of-mass system, calculated with CASTHY.

MT=91 : 90 degree symmetric in the laboratory system, calculated with CASTHY.

MF=5 Energy Distributions of Secondary Neutrons

MT=16,17,91 : Evaporation spectrum.

References

- 1) Beer H. and Spencer R.R.: Nucl. Phys., A240, 29 (1975).
- 2) Farrell J.A. et al.: Ann. Phys., 37, 367 (1966).
- 3) Kikuchi Y. and Sekine N.: to be published as JAERI-M report.
- 4) Kawai M.: unpublished.

- 5) Igarasi S.: J.Nucl.Sci.Technol.,12,67 (1975).
- 6) Lederer C.M. and Shirley V.S.: Table of Isotopes,7th Edition,
Wiley-Interscience (1978).
- 7) Yoshida T. : unpublished.

29-Cu- 0 MAT number = 2290

29-Cu- 0 JAERI, MAPI Eval-Mar82 S. Igarasi, M. Sasaki
Dist-Mar83 Rev1-Jan84

History

- 75-03 Evaluation was made for JENDL-1 by M. Sakaki (MAPI).
 83-03 Data in the energy region above 35 keV were re-evaluated for JENDL-2 by S. Igarasi (JAERI), and the background data in the resonance region were modified.
 84-01 Comment was added.

MF=1 General Information

MT=451 Descriptive data and dictionary

MF=2 Resonance Parameters

MT=151 Resolved resonance parameters for MLBW formula
 Resonance region = $1.0E-5$ eV to 35 keV.
 Parameters of each isotope were mainly taken from BNL-325 3rd edition /1/. A bound level was added to reproduce the 2200 m/sec capture cross section of each isotope. The effective scattering radius of 6.70 fm was taken from Ref. /2/ for Cu-63 and 6.56 fm /1/ for Cu-65.

Calculated 2200-m/s cross sections and res. integrals.

	2200 m/s	res. integ.
elastic	7.859 b	-
capture	3.775 b	3.40 b
total	11.63 b	-

MF=3 Neutron Cross Sections

Below 35 keV, all background cross sections are zero.
 Above 35 keV, data were constructed from isotope data which were evaluated as follows.

MT=1 Total

Optical and statistical model calculation was made with code CASTHY /3/. The optical potential parameters used for both isotopes are as follows (in the units of MeV and fermi),

$$\begin{aligned}
 V &= 46.0 - 0.250 * E & , & \quad R_0 = 1.16 * A^{1/3} + 0.6, \quad a_0 = 0.62 \\
 W_i &= 0.125 * E - 0.0004 * E^{*2}, & \quad R_i &= 1.16 * A^{1/3} + 0.6, \quad a_i = 0.62 \\
 W_s &= 7.0 & , & \quad R_s = 1.16 * A^{1/3} + 1.1, \quad a_s = 0.35 \\
 W_{s0} &= 7.0 & , & \quad R_{s0} = 1.16 * A^{1/3} + 0.6, \quad a_{s0} = 0.60
 \end{aligned}$$

MT=2 Elastic scattering

(Total) - (All other partial cross sections)

MT=4,51-67,91 Inelastic scattering

Optical and statistical model calculation was made by taking into account of competing processes of (n,2n), (n,n'a) and (n,a) reactions for Cu-63, and (n,2n), (n,n'a) and (n,p) for Cu-65. The level schemes were taken from Ref. /4/.

	Cu-nat	Cu-63		Cu-65	
MT	Energy (MeV)	Energy (MeV)	J-p	Energy (MeV)	J-p
51	0.6698	0.66962	1/2 -	-	-
52	0.7704	-	-	0.7706	1/2 -
53	0.9623	0.96206	5/2 -	-	-

2 of Natural Copper

54	1.1153	-		1.11554	5/2 -
55	1.3274	1.32703	7/2 -	-	
56	1.4124	1.41203	5/2 -	-	
57	1.4815	-		1.48183	7/2 -
58	1.5475	1.54702	3/2 -	-	
59	1.6231	-		1.62344	5/2 -
60	1.7246	-		1.72494	3/2 -
61	1.8618	1.8613	5/2 -	-	
62	2.0117	2.0111	3/2 -	-	
63	2.0926	-		2.093	5/2 -
64	2.2118	-		2.2123	3/2 -
65	2.2795	-		2.280	5/2 -
66	2.3277	-		2.3282	3/2 -
67	2.5305	-		2.531	9/2 +
91	2.0506	above 2.05		above 2.54	

MT=16,22,103,107 (n,2n), (n,n'a), (n,p) and (n,a)

Recommended by Kobayashi /5/.

MT=102 Capture

Calculated with CASTHY /3/ and normalized to the value of 23.7 milli-barns for Cu-63 and 11.9 milli-barns for Cu-65 at 230 keV which were measured by Zaikin /6/.

MT=251 Mu-bar

Calculated with CASTHY /3/.

MF=4 Angular Distributions of Secondary Neutrons

MT=2 : Calculated with CASTHY /3/.

MT=16,22,91 : Assumed to be isotropic in the lab system.

MT=51,67 : Assumed to be isotropic in the center-of-mass system.

MF=5 Energy Distributions of Secondary Neutrons

MT=16,22,91 : Evaporation spectra.

References

- 1) Mughabghab S.F. and Garber D.I.: BNL 325, 3rd Ed., vol. 1 (1973).
- 2) Mughabghab S.F. et al.: "Neutron Cross Sections, Vol. 1, Part A", Academic Press (1981).
- 3) Igarasi S.: J. Nucl. Sci. Technol., 12, 67 (1975).
- 4) Auble R.L.: Nuclear Data Sheets, 14, 119 (1975).
- 5) Kobayashi K.: private communication.
- 6) Zaikin G.G. et al.: Atomnaya Energiya, 25, 526 (1968).

29-Cu- 63 MAT number = 2291

29-Cu- 63 JAERI, MAPI Eval-Mar82 S. Igarasi, M. Sasaki
Dist-Mar83 Rev1-Jan84

History

- 75-03 Evaluation was made for JENDL-1 by M. Sakaki (MAPI).
83-03 Data in the energy region above 35 keV were re-evaluated
for JENDL-2 by S. Igarasi (JAERI), and the background data
in the resonance region were modified.
84-01 Comment was added.

MF=1 General Information

MT=451 Descriptive data and dictionary

MF=2 Resonance Parameters

MT=151 Resolved resonance parameters for MLBW formula

Resonance region = 1.0E-5 eV to 35 keV.

Parameters were mainly taken from BNL-325 3rd edition /1/.

A bound level was added to reproduce the 2200-m/sec capture
cross section of 4.5 +- 0.1 barns /1/. The effective scat-
tering radius of 0.67 fm was taken from Ref. /2/.

Calculated 2200-m/s cross sections and res. integrals.

	2200 m/s	res. integ.
elastic	4.979 b	-
capture	4.492 b	5.41 b
total	9.471 b	-

MF=3 Neutron Cross Sections

Below 35 keV, all background cross sections are zero.

Above 35 keV, data were evaluated as follows.

MT=1 Total

Optical and statistical model calculation was made with
code CASTHY /3/. The optical potential parameters used are
as follows (in the units of MeV and fermi),

$$V = 46.0 - 0.250 * E, \quad R_0 = 1.16 * A^{1/3} + 0.6, \quad a_0 = 0.62$$

$$W_i = 0.125 * E - 0.0004 * E^{**2}, \quad R_i = 1.16 * A^{1/3} + 0.6, \quad a_i = 0.62$$

$$W_s = 7.0, \quad R_s = 1.16 * A^{1/3} + 1.1, \quad a_s = 0.35$$

$$W_{so} = 7.0, \quad R_{so} = 1.16 * A^{1/3} + 0.6, \quad a_{so} = 0.60$$

MT=2 Elastic scattering

(Total) - (All other partial cross sections)

MT=4,51-57,91 Inelastic scattering

Optical and statistical model calculation was made by taking
into account of (n,2n), (n,n'a) and (n,a) reactions as com-
peting processes. The level scheme was taken from Ref. /4/.

No.	Energy (MeV)	Spin-Parity
g.s.	0.0	3/2 -
1	0.66962	1/2 -
2	0.96206	5/2 -
3	1.32703	7/2 -
4	1.41203	5/2 -
5	1.54702	3/2 -
6	1.8613	5/2 -

7 2.0111 3/2 -

Levels above 2.05 MeV were assumed to be overlapping.

MT=16,22,107 : (n,2n), (n,n'a) and (n,a)

Recommended by Kobayashi /5/.

MT=102 Capture

Calculated with CASTHY /3/ and normalized to the value of
23.7 milli-barns at 230 keV which was measured by Zaikin /6/.

MT=251 Mu-bar

Calculated with CASTHY /3/.

MF=4 Angular Distributions of Secondary Neutrons

MT=2,51-57 : Calculated with CASTHY /3/.

MT=16,22 : Assumed to be isotropic in the lab system.

MT=91 : Calculated with CASTHY in the center-of-mass
system, and assumed to be the same in the
laboratory system.

MF=5 Energy Distributions of Secondary Neutrons

MT=16,22,91 : Evaporation spectra.

References

- 1) Mughabghab S.F. and Garber D.I.: BNL 325, 3rd Ed., vol. 1 (1973).
- 2) Mughabghab S.F. et al.: "Neutron Cross Sections, Vol. 1, Part A", Academic Press (1981).
- 3) Igarasi S.: J. Nucl. Sci. Technol., 12, 67 (1975).
- 4) Auble R.L.: Nuclear Data Sheets, 14, 119 (1975).
- 5) Kobayashi K.: private communication.
- 6) Zaikin G.G. et al.: Atomnaya Energiya, 25, 526 (1968).

29-Cu- 65 MAT number = 2292

29-Cu- 65 JAERI, MAPI Eval-Mar82 S. Igarasi, M. Sasaki
Dist-Mar83 Rev1-Jan84

History

- 75-03 Evaluation was made for JENDL-1 by M. Sakaki (MAPI).
83-03 Data in the energy region above 35 keV were re-evaluated for JENDL-2 by S. Igarasi (JAERI), and the background data in the resonance region were modified.
84-01 Comment was added.

MF=1 General Information

MT=451 Descriptive data and dictionary

MF=2 Resonance Parameters

MT=151 Resolved resonance parameters for MLBW formula

Resonance region = 1.0E-5 eV to 35 keV.

Parameters were mainly taken from BNL 325 3rd edition /1/. A bound level was added to reproduce the 2200-m/sec capture cross section of 2.17 ± 0.03 barns /1/. The effective scattering radius of 6.56 fm was taken from Ref. /1/.

Calculated 2200-m/s cross sections and res. integrals.

	2200 m/s	res. integ.
elastic	14.30 b	-
capture	2.170 b	2.13 b
total	16.47 b	-

MF=3 Neutron Cross Sections

Below 35 keV, all background cross sections are zero.

Above 35 keV, data were evaluated as follows,

MT=1 Total

Optical and statistical model calculation was made with code CASTHY /2/. The optical potential parameters used are as follows (in the units of MeV and fermi),

$$V = 46.0 - 0.250 \cdot E, \quad R_0 = 1.16 \cdot A^{1/3} + 0.6, \quad a_0 = 0.62$$

$$W_i = 0.125 \cdot E - 0.0004 \cdot E^2, \quad R_i = 1.16 \cdot A^{1/3} + 0.6, \quad a_i = 0.62$$

$$W_s = 7.0, \quad R_s = 1.16 \cdot A^{1/3} + 1.1, \quad a_s = 0.35$$

$$W_{so} = 7.0, \quad R_{so} = 1.16 \cdot A^{1/3} + 0.6, \quad a_{so} = 0.60$$

MT=2 Elastic scattering

(Total) - (All other partial cross sections)

MT=4,51-60,91 Inelastic scattering

Optical and statistical model calculation was made by taking into account of (n,2n), (n,n'a) and (n,p) reactions as competing processes. The level scheme was taken from Ref. /3/.

No.	Energy (MeV)	Spin-Parity
g.s.	0.0	3/2 -
1	0.7706	1/2 -
2	1.11554	5/2 -
3	1.48183	7/2 -
4	1.62344	5/2 -
5	1.72494	3/2 -
6	2.093	5/2 -

7	2.2123	3/2 -
8	2.280	5/2 -
9	2.3282	3/2 -
10	2.531	9/2 +

Levels above 2.54 MeV were assumed to be overlapping.

MT=16,22,103 (n,2n), (n,n'a) and (n,p)

Recommended by Kobayashi /4/.

MT=102 Capture

Calculated with CASTHY /2/ and normalized to the value of 11.9 milli-barns at 230 keV which was measured by Zaikin /5/.

MT=251 Mu-bar

Calculated with CASTHY /2/.

MF=4 Angular Distributions of Secondary Neutrons

MT=2.51-60 : Calculated with CASTHY /2/.

MT=16,22 : Assumed to be isotropic in the lab system.

MT=91 : Calculated with CASTHY in the center-of-mass system, and assumed to be the same in the laboratory system.

MF=5 Energy Distributions of Secondary Neutrons

MT=16,22,91 : Evaporation spectra.

References

- 1) Mughabghab S.F. and Garber D.I.: BNL 325, 3rd ed., vol. 1 (1973).
- 2) Igarasi S.: J. Nucl. Sci. Technol., 12, 67 (1975).
- 3) Auble R.L.: Nuclear Data Sheets, 14, 119 (1975).
- 4) Kobayashi K.: private communication.
- 5) Zaikin G.G. et al.: Atomnaya Energiya, 25, 526 (1968).

41-Nb- 93 MAT number = 2411

41-Nb- 93 JNDC Eval-Oct82 JNDC FPND W.G.
Dist-Mar83 Rev1-Nov83

History

- 82-10 New evaluation for JENDL-2 was made by W.G. on FP nuclear data of JNDC.
83-11 Small modification was made and comment was added.

MF=1 General Information

MT=451 Comments and dictionary

MF=2,MT=151 Resonance Parameters

Resolved resonances : 1.0E-5 eV - 7 keV

Evaluated by M.Kawai on the basis of the following data.

Transmission : Garg+ /1/, Poittevin+ /2/, Iliescu+ /6/

Scattering : Iliescu+ /6/

Capture : Macklin /3/, Lopez+ /4/, Iliescu+ /6/

Gamma spectrum: Haste+ /5/

Assumed Gam-g : 172 milli-eV

212 milli-eV for doublet

Unresolved resonances : 7 keV - 50 keV

Energy independent parameters are given:

S0 = 0.37E-4 , S1 = 5.48E-4 , S2 = 3.65E-4,

Dobs= 80.5 eV , Gam-g= 0.160 eV, R = 6.70 fm.

Calculated 2200 m/s values and resonance integrals (barns) :

	2200 m/s value	res.int.
total	7.477	-
elastic	6.326	-
capture	1.152	9.59

MF=3 Neutron Cross Sections

Slight background correction for Sig-t and Sig-c between 30 and 50 keV. Cross sections above 50 keV evaluated as follows;

MT=1 : Total

Calculated with optical model.

Potential parameters obtained by systematic fitting to Sig-t by Iijima+/7/ :

V = 46.0 - 0.25*En , Ws=7.0 , Vso=7.0 (MeV)

R0=Rso=5.89 , Rs=6.39 (fm)

a0=aso=0.62 , b =0.35 (fm)

MT=2 : Elastic scattering

(Total) - (All other partial cross sections).

MT=16,103,107 : (n,2n), (n,p), (n,a)

Calculated by Y.Kanda with GNASH code /8/ considering pre-equilibrium process.

MT=51-57,91,102 : Inelastic scattering and capture

Calculated with the statistical model code CASTHY /9/.

Competing processes : (n,2n), (n,p), (n,a)

Level fluctuation considered.

The level scheme taken from Ref./10/.

No	Energy (MeV)	Spin-Parity
g.s.	0.0	9/2 +
1	0.0304	1/2 -
2	0.6860	3/2 -
3	0.7440	7/2 +
4	0.8087	5/2 +
5	0.8101	5/2 -
6	0.9499	13/2 +
7	0.9791	11/2 +
8	1.0826	9/2 +
9	1.2800	3/2 -
10	1.2974	9/2 +
11	1.3156	5/2 -
12	1.3351	17/2 +
13	1.3640	7/2 -

Continuum levels assumed above 1.39 MeV.

The level density parameters evaluated by Iijima+ /11/.

Nb-isotope	91	92	93	94
a (1/MeV)	9.97	10.38	12.5	12.81
Delta (MeV)	0.93	0.0	0.72	0.0
Ex (MeV)	5.045	4.115	4.629	4.250
Tc (MeV)	0.655	0.641	0.712	0.723

The gamma-ray strength function of $19.7E-4$ obtained so as to reproduce the ORELA capture data /3/.

Mt=251 Mu-bar

Calculated with opticalmodel.

MF-4 Angular Distributions of Secondary Neutrons

MT=2 : Calculated with optical model.

MT=16 : Isotropic in the laboratory system.

MT=51-57 : 90 degree symmetric in the center-of-mass system.

MT=91 : 90 degree symmetric in the laboratory system.

MF-5 Energy Distributions of Secondary Neutrons

MT=16,91 : Evaporation spectrum.

References

- 1) Garg J.B. et al.: Phys. Rev., B137, 547 (1965).
- 2) Poittevin G.le. et al.: Nucl. Phys., 70, 497 (1965).
- 3) Macklin R.L.: Nucl. Sci. Eng., 59, 12 (1976).
- 4) Lopez W.M. et al.: Nucl. Phys., A93, 340 (1967).
- 5) Haste T.J. and Thomas B.W.: J. Physics, G1, 967 (1975).
- 6) Iijima S. and Kawai M.: J. Nucl. Sci. Technol., 20, 77 (1983).
- 7) Young P.G. and Arthur E.D.: LA-6947 (1977).
- 8) Igarasi S.: J. Nucl. Sci. Technol., 12, 67 (1975).
- 9) Lederer C.M. and Shirley V.S.: Table of Isotopes, 7th Edition, Wiley-Interscience (1978).
- 10) Iijima S. et al.: to be published in J. Nucl. Sci. Technol.

42-Mo- 0 MAT number = 2420

42-Mo- 0 JNDC Eval-Aug82 Y.Kikuchi et al.
Dist-Mar83 Rev1-Nov83

History

82-08 New evaluation was made by W.G. on FP nuclear data of JNDC.
Natural-Mo data constructed with data of Mo-isotopes.
83-11 Comment was added.

MF=1,MT=451 Comments and dictionary

MF=2,MT=151 Resonance parameters : 1.0E-5 eV - 100 keV
Resolved resonances for MLBW formula.

Evaluation based on the following data.

Mo-92	Transmiss.	: Wasson+/1/
	Capture	: Wasson+/1/,Weigmann+/2/,Musgrove+/3/
Mo-94	Capture	: Weigmann+/2/,Musgrove+/3/
Mo-95	Transmiss.	: Shwe+/4/
	Capture	: Weigmann+/2/
Mo-96	Capture	: Weigmann+/2/,Musgrove+/3/
Mo-97	Transmiss.	: Shwe+/4/
	Capture	: Weigmann+/2/
Mo-98	Transmiss.	: Chrien+/5/
	Capture	: Weigmann+/2/,Musgrove+/3/
Mo-100	Transmiss.	: Weigmann+/6/
	Capture	: Weigmann+/2/,Musgrove+/3/

A negative resonance added for Mo-95,-97,-98 and -100.

Connecting energy between resolved and unresolved resonances

Mo-92	: 50 keV	, Mo-94	: 20 keV	, Mo-95	: 2 keV
Mo-96	: 19 keV	, Mo-97	: 1.8 keV	, Mo-98	: 32 keV
Mo-100	: 26 keV				

Unresolved resonances up to 100 keV

Energy independent parameters calculated with optical and
statistical models are given.

S0 = 0.37E-4 , S1 = 5.48E-4 , S2 = 3.65E-4.

Calculated 2200 m/s values and resonance integrals (barn) :

	2200 m/s value	Res.Int.
total	8.037	-
elastic	5.486	-
capture	2.551	25.4

MF=3 Neutron Cross Sections

Slight background correction are applied for Sig-t and Sig-c in
the unresolved resonance region.

Cross sections above 100 keV evaluated as follows

MT=1 : Total

Calculated with optical model.

Potential parameters obtained by systematic fitting of Sig-t

2 of Natural Molybdenum

by Iijima+/7/ :

$$\begin{aligned}
 V &= 46.0 - 0.25 \cdot E_n & , W_s &= 7.0 & , V_{so} &= 7.0 & \text{(MeV)} \\
 R_0 &= R_{so} = 5.89 & , R_s &= 6.39 & & & \text{(fm)} \\
 a_0 &= a_{so} = 0.62 & , b &= 0.35 & & & \text{(fm)}
 \end{aligned}$$

MT=2 : Elastic scattering
(Total) - (All other partial cross sections).

MT=16,17,103,107 : (n,2n), (n,3n), (n,p), (n,a)
Calculated with GNASH code /8/ considering pre-equilibrium process.

MT=51-91 : Inelastic scattering
Calculated with the statistical model code CASTHY /9/.
Competing processes : (n,2n), (n,3n), (n,p), (n,a)
Level fluctuation considered.

The level scheme taken from Ref. /10/ for Mo-92 and -94, and from evaluation by Matumoto+/11/ for the other isotopes.

Mo-92	No	Energy (MeV)	Spin-Parity	No	Energy (MeV)	Spin-Parity
g.s.	0		0 +	4	2.5270	5 -
1	1.5095		2 +	5	2.6130	6 +
2	2.2826		4 +	6	2.7600	8 +
3	2.5197		0 +	7	2.8497	3 -

Continuum levels assumed above 3 MeV.

Mo-94	No	Energy (MeV)	Spin-Parity	No	Energy (MeV)	Spin-Parity
g.s.	0		0 +	6	2.2940	4 +
1	0.8710		2 +	7	2.3930	2 +
2	1.5737		4 +	8	2.4230	6 +
3	1.7420		0 +	9	2.5337	3 -
4	1.8642		2 +	10	2.5870	4 +
5	2.0674		2 +	11	2.6100	5 -

Continuum levels assumed above 2.74 MeV.

Mo-95	No	Energy (MeV)	Spin-Parity	No	Energy (MeV)	Spin-Parity
g.s.	0		5/2 +	10	1.3100	1/2 +
1	0.2039		3/2 +	11	1.3760	3/2 +
2	0.7658		7/2 +	12	1.4350	5/2 +
3	0.7862		1/2 +	13	1.5410	11/2 +
4	0.8206		3/2 +	14	1.5528	9/2 +
5	0.9478		9/2 +	15	1.6202	3/2 +
6	1.0391		1/2 +	16	1.6700	5/2 +
7	1.0590		5/2 +	17	1.6830	9/2 +
8	1.0741		7/2 +	18	1.7070	1/2 +
9	1.2225		5/2 +	19	1.9380	11/2 -

Continuum levels assumed above 2 MeV.

Mo-96	No	Energy (MeV)	Spin-Parity	No	Energy (MeV)	Spin-Parity
g.s.	0		0 +	8	2.0956	2 +
1	0.7783		2 +	9	2.2193	4 +
2	1.1479		0 +	10	2.2345	3 -
3	1.4978		2 +	11	2.4262	3 +
4	1.6260		2 +	12	2.4384	5 +
5	1.6280		4 +	13	2.4406	6 +

3 of Natural Molybdenum

6	1.8695	4 +	14	2.4807	4 +
7	1.9783	3 +			

Continuum levels assumed above 2.5 MeV.

Mo-97	No	Energy (MeV)	Spin-Parity	No	Energy (MeV)	Spin-Parity
	g.s.	0	5/2 +	11	1.2686	7/2 +
	1	0.4809	3/2 +	12	1.2730	3/2 +
	2	0.6579	7/2 +	13	1.2840	13/2 +
	3	0.6796	1/2 +	14	1.2846	3/2 +
	4	0.7195	5/2 +	15	1.4095	11/2 +
	5	0.7211	3/2 +	16	1.4373	11/2 -
	6	0.8882	1/2 +	17	1.4470	3/2 +
	7	1.0245	7/2 +	18	1.5156	9/2 +
	8	1.0926	3/2 +	19	1.5452	5/2 -
	9	1.1167	9/2 +	20	1.5651	3/2 -
	10	1.1486	7/2 -			

Continuum levels assumed above 1.58 MeV.

Mo-98	No	Energy (MeV)	Spin-Parity	No	Energy (MeV)	Spin-Parity
	g.s.	0	0 +	10	2.1049	2 +
	1	0.7349	0 +	11	2.2069	2 +
	2	0.7874	2 +	12	2.2240	2 +
	3	1.4323	2 +	13	2.3334	2 +
	4	1.5101	4 +	14	2.3437	6 +
	5	1.7585	2 +	15	2.4198	3 -
	6	1.8809	3 +	16	2.4500	4 +
	7	1.9650	0 +	17	2.4854	3 +
	8	1.9855	1 +	18	2.5063	3 -
	9	2.0176	3 -			

Continuum levels assumed above 2.53 MeV.

Mo-100	No	Energy (MeV)	Spin-Parity	No	Energy (MeV)	Spin-Parity
	g.s.	0	0 +	9	2.0330	0 +
	1	0.5356	2 +	10	2.0400	2 +
	2	0.6944	0 +	11	2.1014	4 +
	3	1.0637	2 +	12	2.3400	2 +
	4	1.1361	4 +	13	2.4156	3 -
	5	1.4633	2 +	14	2.4700	4 +
	6	1.7657	1 +	15	2.5632	3 +
	7	1.7704	3 +	16	2.5900	4 +
	8	1.9081	3 -			

Continuum levels assumed above 2.62 MeV.

The inelastic levels of each isotope are grouped in natural molybdenum file as follows:

MT	-Q (MeV)	Mo-92	Mo-94	Mo-95	Mo-96	Mo-97	Mo-98	Mo-100
51	0.2039	-	-	51	-	-	-	-
52	0.4808	-	-	-	-	51	-	-
53	0.5354	-	-	-	-	-	-	51
54	0.6578	-	-	-	-	52, 53	-	-
55	0.6941	-	-	-	-	-	-	52
56	0.7194	-	-	-	-	54, 55	-	-
57	0.7347	-	-	-	-	-	51	-
58	0.7659	-	-	52	51	-	-	-
59	0.7863	-	-	53	-	-	52	-
60	0.8207	-	-	54	-	-	-	-

4 of Natural Molybdenum

61	0.8712	-	51	-	-	56	-	-
62	0.9479	-	-	55	-	-	-	-
63	1.0244	-	-	56	-	57	-	-
64	1.0591	-	-	57,58	-	-	-	53
65	1.0925	-	-	-	-	58,59	-	-
66	1.1356	-	-	-	52	60	-	54
67	1.2226	-	-	59	-	-	-	-
68	1.2685	-	-	-	-	61,62 63,64	-	-
69	1.3101	-	-	60	-	-	-	-
70	1.3761	-	-	61	-	65	-	-
71	1.4320	-	-	62	-	66	53	-
72	1.4468	-	-	-	-	67	-	55
73	1.4978	51	-	-	53	68	54	-
74	1.5412	-	52	63,64	-	69,70	-	-
75	1.6204	-	-	65	54,55	-	-	-
76	1.6702	-	-	66,67 68	-	-	-	-
77	1.7424	-	53	-	-	-	55	56,57
78	1.8646	-	54	-	56	-	56	-
79	1.9073	-	-	69	-	-	-	58
80	1.9646	-	-	-	57	-	57,58	-
81	2.0172	-	55	-	-	-	59	59,60
82	2.0956	-	-	-	58	-	60	61
83	2.2064	-	-	-	59,60	-	61,62	-
84	2.2836	52	56	-	-	-	-	-
85	2.3329	-	-	-	-	-	63,64	62
86	2.3935	-	57,58	-	61	-	65	63
87	2.4384	-	-	-	62,63	-	66	64
88	2.4807	-	-	-	64	-	67,68	-
89	2.5208	53,54	59	-	-	-	-	65
90	2.5676	55	60,61	-	-	-	-	66
91	1.5798	56,57 91	91	91	91	91	91	91

The level density parameters evaluated by Iijima+/12/.

Mo-isotope	91	92	93	94	95	96
a (1/MeV)	10.87	10.20	11.25	11.80	13.60	14.03
Delta (MeV)	1.28	2.21	1.28	2.00	1.28	2.40
Ex (MeV)	5.428	6.665	3.14	6.228	5.835	7.645
Tc (MeV)	0.627	0.85	0.605	0.760	0.715	0.741

Mo-isotope	97	98	99	100	101
a (1/MeV)	15.17	15.97	17.74	19.35	20.85
Delta (MeV)	1.28	2.57	1.28	2.22	1.28
Ex (MeV)	4.988	7.53	5.775	6.795	5.766
Tc (MeV)	0.618	0.671	0.605	0.600	0.549

MT=102 : Capture

Calculated with the statistical model code CASTHY /9/.

Competing processes : (n,2n), (n,3n), (n,p), (n,a)

Level fluctuation considered.

The gamma-ray strength function of each isotope was obtained so as to reproduce the ORELA capture data /3/:

Mo-92 : $9.4E-5$, Mo-94 : $2.0E-4$, Mo-95 : $2.9E-3$,
 Mo-96 : $1.7E-4$, Mo-97 : $2.9E-3$, Mo-98 : $1.4E-4$,

Mo-100: 1.4E-4

MF=4 Angular Distributions of Secondary Neutrons

MT=2 : Calculated with optical model.

MT=51,52,53,55,57,60,62,67,69

: 90 degree symmetric in the center-of-mass system.

MT=54-90 (other than above)

: Isotropic in the center-of-mass system.

MT=16,17,91 : Isotropic in the laboratory system.

MF=5 Energy Distributions of Secondary Neutrons

MT=16,17,91 : Evaporation spectrum.

References

- 1) Wasson O.A. et al.: Phys.Rev.,C7,1532 (1973).
- 2) Weigmann H. et al.: 1971 Knoxville Conf.,CONF-710301,p.749.
- 3) Musgrove A.R.de.L. et al.: Nucl.Phys.,A270,108 (1976).
- 4) Shve H. and Cote R.E.: Phys.Rev.179,1148 (1969).
- 5) Chrien R.E. et al.: Phys.Rev.,C13,578(1976).
- 6) Weigmann H. et al.: Phys.Rev.,C20,115 (1969).
- 7) Iijima S. and Kawai M.: J.Nucl.Sci.Technol.,20,77 (1983).
- 8) Young P.G. and Arthur E.D.: LA-6947 (1977).
- 9) Igarasi S.: J.Nucl.Sci.Technol.,12,67 (1975).
- 10) Lederer C.M. and Shirley V.S.: Table of Isotopes,7th Edition, Wiley-Interscience (1978).
- 11) Matumoto Z. et al.:JAERI-M 7734(1978).
- 12) Iijima S. et al.: to be published in J.Nucl.Sci.Technol.

42-Mo- 92 MAT number = 2421

42-Mo- 92 JNDC Eval-Aug82 Y.Kikuchi et al.
Dist-Mar83 Rev1-Nov83

History

82-08 New evaluation for JENDL-2 by W.G. on FP nuclear data of JNDC.

83-11 Comment was added.

MF=1,MT=451 Comments and dictionary

MF=2,MT=151 Resonance parameters

Resolved resonances for MLBW formula : 1.0E-5 eV - 50 keV

Evaluation based on the following data.

Transmission : Wasson-/1/.

Capture : Wasson-/1/.,Weigmann-/2/.,Musgrove+/3/.

Assumed Gam-g : 200 milli-eV for s-wave and
425 milli-eV for p-wave

Unresolved resonances : 50 keV - 100 keV

Energy independent parameters are given:

S0 = 0.37E-4 ,S1 = 5.48E-4 ,S2 = 3.65E-4,

Dobs= 2400 eV ,Gam-g= 0.226 eV,R = 6.72 fm.

Calculated 2200 m/s values and resonance integrals (barn) :

	2200 m/s value	Res.Int.
total	5.566	-
elastic	5.545	-
capture	0.02075	0.981

MF=3 Neutron Cross Sections

Slight background correction for Sig-t and Sig-c between 50 and 100 keV.

Cross sections above 100 keV evaluated as follows.

MT=1 : Total

Calculated with optical model.

Potential parameters obtained by systematic fitting to Sig-t
by Iijima+/4/ :

V =46.0 - 0.25*En ,Ws=7.0 ,Vso=7.0 (MeV)

R0=Rso=5.89 ,Rs=6.39 (fm)

a0=aso=0.62 ,b =0.35 (fm)

MT=2 : Elastic scattering

(Total) - (All other partial cross sections).

MT=16,103,107 : (n,2n), (n,p), (n,a)

Calculated with GNASH code /5/ considering pre-equilibrium
process.

MT=51-57,91,102 : Inelastic scattering and capture

Calculated with the statistical model code CASTHY /6/.

Competing processes : (n,2n), (n,p), (n,a)

Level fluctuation considered.

The level scheme taken from Ref./7/.

No	Energy (MeV)	Spin-Parity
g.s.	0	0 +
1	1.5095	2 +
2	2.2826	4 +
3	2.5197	0 +
4	2.5270	5 -
5	2.6130	6 +
6	2.7600	8 +
7	2.8497	3 -

Continuum levels assumed above 3 MeV.

The level density parameters evaluated by Iijima+/8/.

Mo-isotope	91	92	93
a (1/MeV)	10.87	10.2	11.25
Delta (MeV)	1.28	2.21	1.28
Ex (MeV)	5.428	6.665	3.14
Tc (MeV)	0.627	0.85	0.605

The gamma-ray strength function of $0.94E-4$ obtained so as to reproduce the ORELA capture data /3/.

MT=251 : Mu-bar

Calculated with optical model.

MF=4 Angular Distributions of Secondary Neutrons

MT=2 : Calculated with optical model.

MT=16 : Isotropic in the laboratory system.

MT=51-57 : 90 degree symmetric in the center-of-mass system.

MT=91 : 90 degree symmetric in the laboratory system.

MF=5 Energy Distributions of Secondary Neutrons

MT=16,91 : Evaporation spectrum.

References

- 1) Wasson O.A. et al.: Phys.Rev., C7,1532 (1973).
- 2) Weigmann H. et al.: 1971 Knoxville Conf., CONF-710301, p.749.
- 3) Musgrove A.R.de.L. et al.: Nucl.Phys., A270,108 (1976).
- 4) Iijima S. and Kawai M.: J.Nucl.Sci.Technol., 20,77 (1983)
- 5) Young P.G. and Arthur E.D.: LA-6947 (1977).
- 6) Igarasi S.: J.Nucl.Sci.Technol., 12,67 (1975).
- 7) Lederer C.M. and Shirley V.S.: Table of Isotopes, 7th Edition, Wiley-Interscience (1978).
- 8) Iijima S. et al.: to be published in J.Nucl.Sci.Technol.

42-Mo- 94 MAT number = 2422

42-Mo- 94 JNDC Eval-Aug82 Y.Kikuchi et al.
Dist-Mar83 Rev1-Nov83

History

82-08 New evaluation for JENDL-2 by W.G. on FP nuclear data of JNDC.

83-11 Comment was added.

MF=1,MT=451 Comments and dictionary

MF=2,MT=151 Resonance parameters

Resolved resonances for MLBW formula : $1.0E-5$ eV - 20 keV

Evaluation based on the following data.

Capture : Weigmann-1/Musgrove-2/.

Assumed Gam-g : 135 milli-eV for s-wave and
175 milli-eV for p-wave.

Unresolved resonances : 20 keV - 100 keV

Energy independent parameters are given:

S0 = $0.37E-4$, S1 = $5.48E-4$, S2 = $3.65E-4$,

Dobs = 1150 eV , Gam-g = 0.230 eV, R = 6.68 fm.

Calculated 2200 m/s values and resonance integrals (barn) :

	2200 m/s value	Res.Int.
total	6.011	-
elastic	5.998	-
capture	0.01311	1.43

MF=3 Neutron Cross Sections

Slight background correction for Sig t and Sig-c between 30 keV and 100 keV.

Cross sections above 100 keV evaluated as follows.

MT=1 : Total

Calculated with optical model.

Potential parameters obtained by systematic fitting to Sig-t by Iijima-3/ :

V = $46.0 - 0.25 \times E_n$, Ws = 7.0 , Vso = 7.0 (MeV)

R0 = Rso = 5.89 , Rs = 6.39 (fm)

a0 = aso = 0.62 , b = 0.35 (fm)

MT=2 : Elastic scattering

(Total) - (All other partial cross sections).

MT=16,17,103,107 : (n,2n), (n,3n), (n,p), (n,a)

Calculated with GNASH code /4/ considering pre-equilibrium process.

MT=51-61,91,102 : Inelastic scattering and capture

Calculated with the statistical model code CASTHY /5/.

Competing processes : (n,2n), (n,3n), (n,p), (n,a)

Level fluctuation considered.

The level scheme taken from Ref. /6/.

No	Energy (MeV)	Spin-Parity
g.s.	0	0 +
1	0.8710	2 +
2	1.5737	4 +
3	1.7420	0 +
4	1.8642	2 +
5	2.0674	2 +
6	2.2940	4 +
7	2.3930	2 +
8	2.4230	6 +
9	2.5337	3 -
10	2.5670	4 +
11	2.6100	5 -

Continuum levels assumed above 2.74 MeV.

The level density parameters evaluated by Iijima-/7/.

Mo-isotope	93	94	95
a (1/MeV)	11.25	11.80	13.60
Delta (MeV)	1.28	2.0	1.28
Ex (MeV)	3.14	6.228	5.835
Tc (MeV)	0.605	0.76	0.715

The gamma-ray strength function of $2.0E-4$ obtained so as to reproduce the ORELA capture data /2/.

MT=251 : Mu-bar

Calculated with optical model.

MF=4 Angular Distributions of Secondary Neutrons

MT=2 : Calculated with optical model.

MT=16,17 : Isotropic in the laboratory system.

MT=51-61 : 90 degree symmetric in the center-of-mass system.

MT=91 : 90 degree symmetric in the laboratory system.

MF=5 Energy Distributions of Secondary Neutrons

MT=16,17,91 : Evaporation spectrum.

References

- 1) Weigmann H. et al.: 1971 Knoxville Conf., CONF-710301, p.749.
- 2) Musgrove A.R.de.L. et.al.: Nucl.Phys., A270,108 (1976).
- 3) Iijima S. and Kawai M.: J.Nucl.Sci.Technol., 20,77 (1983).
- 4) Young P.G. and Arthur E.D.: LA-6947 (1977).
- 5) Igarasi S.: J.Nucl.Sci.Technol., 12,67 (1975).
- 6) Lederer C.M. and Shirley V.S.: Table of Isotopes, 7th Edition, Wiley-Interscience (1978).
- 7) Iijima S. et al.: to be published in J.Nucl.Sci.Technol.

42-Mo-95 MAT number = 2423

42-Mo-95 JNDC Eval-Aug82 Y.Kikuchi et al.
Dist-Mar83 Rev1-Nov83

History

82-08 New evaluation for JENDL-2 by W.G. on FP nuclear data of JNDC.

83-11 Comment was added.

MF=1, MT=451 Comments and dictionary

MF=2, MT=151 Resonance parameters

Resolved resonances for MLBW formula : $1.0E-5$ eV - 2 keV

Evaluation based on the following data.

Transmission : Shwe-/1/

Capture : Weigmann-/2/

Assumed Gam-g : 150 milli-eV for s-wave and
180 milli-eV for p-wave.

A negative resonance added at - 20 eV.

Unresolved resonances : 2 keV - 100 keV

Energy independent parameters are given:

$S_0 = 0.37E-4$, $S_1 = 5.48E-4$, $S_2 = 3.65E-4$,

Dobs = 80 eV, Gam-g = 0.232 eV, R = 6.70 fm.

Calculated 2200 m/s values and resonance integrals (barn) :

	2200 m/s value	Res.Int.
total	19.58	-
elastic	5.586	-
capture	13.99	119

MF=3 Neutron Cross Sections

Slight background correction for Sig-t and Sig-c between 40 and 100 keV.

Cross sections above 100 keV were evaluated as follows.

MT=1 : Total

Calculated with optical model.

Potential parameters obtained by systematic fitting of Sig-t by Iijima+/3/ :

$V = 46.0 - 0.25 * E_n$, $W_s = 7.0$, $V_{so} = 7.0$ (MeV)

$R_0 = R_{so} = 5.89$, $R_s = 6.39$ (fm)

$a_0 = a_{so} = 0.62$, $b = 0.35$ (fm)

MT=2 : Elastic scattering

(Total) - (All other partial cross sections).

MT=16, 17, 103, 107 : (n,2n), (n,3n), (n,p), (n,a)

Calculated with GNASH code /4/ considering pre-equilibrium process.

MT=51-69, 91, 102 : Inelastic scattering and capture

Calculated with the statistical model code CASTHY /5/.

Competing processes : (n,2n), (n,3n), (n,p), (n,a)

Level fluctuation considered.

The level scheme taken from evaluation by Matumoto+/6/.

No	Energy (MeV)	Spin-Parity
g.s.	0	5/2 +
1	0.2039	3/2 +
2	0.7658	7/2 +
3	0.7862	1/2 +
4	0.8206	3/2 +
5	0.9478	9/2 +
6	1.0391	1/2 +
7	1.0590	5/2 +
8	1.0741	7/2 +
9	1.2225	5/2 +
10	1.3100	1/2 +
11	1.3760	3/2 +
12	1.4350	5/2 +
13	1.5410	11/2 +
14	1.5528	9/2 +
15	1.6202	3/2 +
16	1.6700	5/2 +
17	1.6830	9/2 +
18	1.7070	1/2 +
19	1.9380	11/2 -

Continuum levels assumed above 2 MeV.

The level density parameters evaluated by Iijima+/7/.

Mo-isotope	93	94	95	96
a (1/MeV)	11.25	11.80	13.60	14.03
Delta (MeV)	1.28	2.0	1.28	2.40
Ex (MeV)	3.14	6.228	5.835	7.645
Tc (MeV)	0.605	0.76	0.715	0.741

The gamma-ray strength function of $2.9E-3$ obtained so as to reproduce the ORELA capture data /8/.

MT-251 : Mu bar

Calculated with optical model.

MF=4 Angular Distributions of Secondary Neutrons

MT=2 : Calculated with optical model.

MT=16,17 : Isotropic in the laboratory system.

MT=51-69 : 90 degree symmetric in the center-of-mass system.

MT=91 : 90 degree symmetric in the laboratory system.

MF=5 Energy Distributions of Secondary Neutrons

MT=16,17,91 : Evaporation spectrum.

References

- 1) Shwe H. and Cote R.E.: Phys.Rev.179,1148 (1969)
- 2) Weigmann H. et al.: 1971 Knoxville Conf.,CONF-710301,p.749.
- 3) Iijima S. and Kawai M.: J.Nucl.Sci.Technol.,20,77 (1983).
- 4) Young P.G. and Arthur E.D.: LA-6947 (1977).
- 5) Igarasi S.: J.Nucl.Sci.Technol.,12,67 (1975).
- 6) Matumoto Z. et al.:JAERI-M 7734(1978).
- 7) Iijima S. et al.: to be published in J.Nucl.Sci.Technol.
- 8) Musgrove A.R.de.L. et al.: Nucl.Phys.,A270,108 (1976).

42-Mo-96 MAT number = 2424

42-Mo-96 JNDC Eval-Aug82 Y.Kikuchi et al.
Dist-Mar83 Rev1-Nov83

History

82-08 New evaluation for JENDL-2 by W.G. on FP nuclear data of JNDC.

83-11 Comment was added.

MF=1,MT=451 Comments and dictionary

MF=2,MT=151 Resonance parameters

Resolved resonances for MLBW formula : $1.0E-5$ eV - 19 keV

Evaluation based on the following data.

Capture : Weigmann-1/, Musgrove-2/

Assumed Gam-g : 114 milli-eV for s-wave and
136 milli-eV for p-wave.

Unresolved resonances : 19 keV - 100 keV

Energy independent parameters are given:

$S_0 = 0.37E-4$, $S_1 = 5.48E-4$, $S_2 = 3.65E-4$,

Dobs = 950 eV, Gam-g = 162 MeV, R = 6.68 fm.

Calculated 2200 m/s values and resonance integrals (barn) :

	2200 m/s value	Res.Int.
total	5.322	-
elastic	4.727	-
capture	0.5954	17.6

MF=3 Neutron Cross Sections

Slight background correction for Sig-t and Sig-c between 30 and 100 keV.

Cross sections above 100 keV were evaluated as follows.

MT=1 : Total

Calculated with optical model.

Potential parameters obtained by systematic fitting of Sig-t by Iijima-3/ :

$V = 46.0 - 0.25 * E_n$, $W_s = 7.0$, $V_{so} = 7.0$ (MeV)

$R_0 = R_{so} = 5.89$, $R_s = 6.39$ (fm)

$a_0 = a_{so} = 0.62$, $b = 0.35$ (fm)

MT=2 : Elastic scattering

(Total) - (All other partial cross sections).

MT=16,17,103,107 : (n,2n), (n,3n), (n,p), (n,a)

Calculated with GNASH code-4/ considering pre-equilibrium process.

MT=51-64,91,102 : Inelastic scattering and capture

Calculated with the statistical model code CASTHY-5/.

Competing processes : (n,2n), (n,3n), (n,p), (n,a)

Level fluctuation considered.

The level scheme taken from evaluation by Matumoto-6/.

No	Energy (MeV)	Spin-Parity
g.s.	0	0 +
1	0.7783	2 +
2	1.1479	0 +
3	1.4978	2 +
4	1.6260	2 +
5	1.6280	4 +
6	1.8695	4 +
7	1.9783	3 +
8	2.0956	2 +
9	2.2193	4 +
10	2.2345	3 -
11	2.4262	3 +
12	2.4384	5 +
13	2.4406	6 +
14	2.4807	4 +

Continuum levels assumed above 2.5 MeV.

The level density parameters evaluated by Iijima+/7/.

Mo-isotope	94	95	96	97
a (1/MeV)	11.80	13.60	14.03	15.17
Delta (MeV)	2.0	1.28	2.40	1.28
Ex (MeV)	6.228	5.835	7.645	4.988
Tc (MeV)	0.76	0.715	0.741	0.618

The gamma-ray strength function of $1.7E-4$ obtained so as to reproduce the ORELA capture data /2/.

MT=251 : Mu-bar
Calculated with optical model.

MF=4 Angular Distributions of Secondary Neutrons
 MT=2 : Calculated with optical model.
 MT=16,17 : Isotropic in the laboratory system.
 MT=51-64 : 90 degree symmetric in the center-of-mass system.
 MT=91 : 90 degree symmetric in the laboratory system.

MF=5 Energy Distributions of Secondary Neutrons
 MT=16,17,91 : Evaporation spectrum.

References

- 1) Weigmann H. et al.: 1971 Knoxville Conf., CONF-710301, p.749.
- 2) Musgrove A.R.de.L. et al.: Nucl.Phys., A270,108 (1976).
- 3) Iijima S. and Kawai M.: J.Nucl.Sci.Technol., 20,77 (1983).
- 4) Young P.G. and Arthur E.D.: LA-6947 (1977).
- 5) Igarasi S.: J.Nucl.Sci.Technol., 12,67 (1975).
- 6) Matumoto Z. et al.: JAERI-M 7734 (1978).
- 7) Iijima S. et al.: to be published in J.Nucl.Sci.Technol.

Level fluctuation considered.

The level scheme taken from evaluation by Matumoto+/6/.

No	Energy (MeV)	Spin-Parity
g.s.	0	5/2 +
1	0.4809	3/2 +
2	0.6579	7/2 +
3	0.6796	1/2 +
4	0.7195	5/2 +
5	0.7211	3/2 +
6	0.8882	1/2 +
7	1.0245	7/2 +
8	1.0926	3/2 +
9	1.1167	9/2 +
10	1.1486	7/2 -
11	1.2686	7/2 +
12	1.2730	3/2 +
13	1.2840	13/2 +
14	1.2846	3/2 +
15	1.4095	11/2 +
16	1.4373	11/2 -
17	1.4470	3/2 +
18	1.5156	9/2 +
19	1.5452	5/2 -
20	1.5651	3/2 -

Continuum levels assumed above 1.58 MeV.

The level density parameters evaluated by Iijima+/7/.

Mo-isotope	95	96	97	98
a (1/MeV)	13.60	14.03	15.17	15.94
Delta (MeV)	1.28	2.40	1.28	2.57
Ex (MeV)	5.835	7.645	4.988	7.53
Tc (MeV)	0.715	0.741	0.618	0.671

The gamma-ray strength function of $2.9E-3$ obtained so as to reproduce the ORELA capture data /8/.

MT=251 : Mu-bar

Calculated with optical model.

MF=4 Angular Distributions of Secondary Neutrons

MT=2 : Calculated with optical model.

MT=16,17 : Isotropic in the laboratory system.

MT=51-70 : 90 degree symmetric in the center-of-mass system.

MT=91 : 90 degree symmetric in the laboratory system.

MF=5 Energy Distributions of Secondary Neutrons

MT=16,17,91 : Evaporation spectrum.

References

- 1) Shwe H. and Cote R.E.: Phys.Rev.179,1148 (1969).
- 2) Weigmann H. et al.: 1971 Knoxville Conf.,CONF-710301,p.749.
- 3) Iijima S. and Kawai M.: J.Nucl.Sci.Technol.,20,77 (1983).
- 4) Young P.G. and Arthur E.D.: LA-6947 (1977).
- 5) Igarasi S.: J.Nucl.Sci.Technol.,12,67 (1975).
- 6) Matumoto Z. et al.:JAERI-M 7734(1978).
- 7) Iijima S. et al.: to be published in J.Nucl.Sci.Technol.
- 8) Musgrove A.R.de.L. et al.: Nucl.Phys.,A270,108 (1976).

42-Mo-98 MAT number = 2426

42-Mo-98 JNDC Eval-Aug82 Y.Kikuchi et al.
Dist-Mar83 Rev1-Nov83

History

82-08 New evaluation for JENDL-2 by W.G. on FP nuclear data of JNDC.

83-11 Comment was added.

MF=1, MT=451 Comments and dictionary

MF=2, MT=151 Resonance parameters

Resolved resonances for MLBW formula : $1.0E-5$ eV - 32 keV

Evaluation based on the following data.

Transmission : Chrien+/1/

Capture : Weigmann+/2/, Musgrove+/3/

Assumed Gam-g : 85 milli-eV for s-wave and
120 milli-eV for p-wave.

A negative resonance added at - 980eV.

Unresolved resonances : 32 keV - 100 keV

Energy independent parameters are given:

S0 = $0.37E-4$, S1 = $5.48E-4$, S2 = $3.65E-4$,

Dobs = 950 eV, Gam-g = 0.133 eV, R = 6.66 fm.

Calculated 2200 m/s values and resonance integrals (barn) :

	2200 m/s value	Res.Int.
total	5.772	-
elastic	5.642	-
capture	0.1300	6.56

MF=3 Neutron Cross Sections

Slight background correction for Sig-t and Sig-c between 32 and 100 keV.

Cross sections above 100 keV were evaluated as follows.

MT=1 : Total

Calculated with optical model.

Potential parameters obtained by systematic fitting of Sig-t by Iijima+/4/ :

V = $46.0 - 0.25 * E_n$, Ws = 7.0, Vso = 7.0 (MeV)
 R0 = Rso = 5.89, Rs = 6.39 (fm)
 a0 = aso = 0.62, b = 0.35 (fm)

MT=2 : Elastic scattering

(Total) - (All other partial cross sections).

MT=16, 17, 103, 107 : (n,2n), (n,3n), (n,p), (n,a)

Calculated with GNASH code /5/ considering pre-equilibrium process.

MT=51-68, 91, 102 : Inelastic scattering and capture

Calculated with the statistical model code CASTHY /6/.

Competing processes : (n,2n), (n,3n), (n,p), (n,a)

Level fluctuation considered.

The level scheme taken from evaluation by Matumoto+/7/.

No	Energy (MeV)	Spin-Parity
g.s.	0	0 +
1	0.7349	0 +
2	0.7874	2 +
3	1.4323	2 +
4	1.5101	4 +
5	1.7585	2 +
6	1.8809	3 +
7	1.9650	0 +
8	1.9855	1 +
9	2.0176	3 -
10	2.1049	2 +
11	2.2069	2 +
12	2.2240	2 +
13	2.3334	2 +
14	2.3437	6 +
15	2.4198	3 -
16	2.4500	4 +
17	2.4854	3 +
18	2.5063	3 -

Continuum levels assumed above 2.53 MeV.

The level density parameters evaluated by Iijima+/8/.

Mo-isotope	96	97	98	99
a (1/MeV)	14.03	15.17	15.94	17.74
Delta (MeV)	2.40	1.28	2.57	1.28
Ex (MeV)	7.645	4.988	7.53	5.775
Tc (MeV)	0.741	0.618	0.671	0.605

The gamma-ray strength function of $1.4E-4$ obtained so as to reproduce the ORELA capture data /3/.

MT=251 : Mu-bar

Calculated with optical model.

MF=4 Angular Distributions of Secondary Neutrons

MT=2 : Calculated with optical model.

MT=16,17 : Isotropic in the laboratory system.

MT=51-68 : 90 degree symmetric in the center-of-mass system.

MT=91 : 90 degree symmetric in the laboratory system.

MF=5 Energy Distributions of Secondary Neutrons

MT=16,17,91 : Evaporation spectrum.

References

- 1) Chrien R.E. et al.: Phys.Rev., C13,578(1976).
- 2) Weigmann H. et al.: 1971 Knoxville Conf., CONF-710301, p.749.
- 3) Musgrove A.R.de.L. et al.: Nucl.Phys., A270,108 (1976).
- 4) Iijima S. and Kawai M.: J.Nucl.Sci.Technol., 20,77 (1983).
- 5) Young P.G. and Arthur E.D.: LA-6947 (1977).
- 6) Igarasi S.: J.Nucl.Sci.Technol., 12,67 (1975).
- 7) Matumoto Z. et al.: JAERI-M 7734(1978).
- 8) Iijima S. et al.: to be published in J.Nucl.Sci.Technol.

42-Mo-100 MAT number = 2427

42-Mo-100 JNDC Eval-Aug82 Y.Kikuchi et al.
Dist-Mar83 Rev1-Nov83

History

82-08 New evaluation for JENDL-2 by W.G. on FP nuclear data of JNDC.

83-11 Comment was added.

MF=1, MT=451 Comments and dictionary

MF=2, MT=151 Resonance parameters

Resolved resonances for MLBW formula : $1.0E 5$ eV - 26 keV

Evaluation based on the following data.

Transmission : Weigmann-1/

Capture : Weigmann-2/ Musgrove-3/

Assumed Gam-g : 65 milli-eV for s-wave and
80 milli-eV for p-wave.

A negative resonance added at - 172 eV.

Unresolved resonances : 26 keV - 100 keV

Energy independent parameters are given:

S0 = $0.37E-4$, S1 = $5.48E-4$, S2 = $3.65E-4$,

Dobs = 620 eV , Gam-g = 0.85 eV , R = 6.64 fm.

Calculated 2200 m/s values and resonance integrals (barn) :

	2200 m/s value	Res.Int.
total	5.499	-
elastic	5.300	-
capture	0.1990	3.92

MF=3 Neutron Cross Sections

Slight background correction for Sig t and Sig-c between 26 and 100 keV.

Cross sections above 100 keV were evaluated as follows.

MT=1 : Total

Calculated with optical model.

Potential parameters obtained by systematic fitting of Sig-t by Iijima+4/ :

V = $46.0 - 0.25 * E_n$, $W_s = 7.0$, $V_{so} = 7.0$ (MeV)R0 = $R_{so} = 5.89$, $R_s = 6.39$ (fm)a0 = $a_{so} = 0.62$, $b = 0.35$ (fm)

MT=2 : Elastic scattering

(Total) - (All other partial cross sections).

MT=16, 17, 103, 107 : (n,2n), (n,3n), (n,p), (n,a)

Calculated with GNASH code /5/ considering pre-equilibrium process.

MT=51-66, 91, 102 : Inelastic scattering and capture

Calculated with the statistical model code CASTHY /6/.

Competing processes : (n,2n), (n,3n), (n,p), (n,a)

Level fluctuation considered.

The level scheme taken from evaluation by Matumoto+/7/.

No	Energy (MeV)	Spin-Parity
g.s.	0	0 +
1	0.5356	2 +
2	0.6944	0 +
3	1.0637	2 +
4	1.1361	4 +
5	1.4633	2 +
6	1.7657	1 +
7	1.7704	3 +
8	1.9081	3 -
9	2.0330	0 +
10	2.0400	2 +
11	2.1014	4 +
12	2.3400	2 +
13	2.4156	3 -
14	2.4700	4 +
15	2.5632	3 -
16	2.5900	4 +

Continuum levels assumed above 2.62 MeV.

The level density parameters evaluated by Iijima+/8/.

Mo-isotope	98	99	100	101
a (1/MeV)	15.97	17.74	19.35	20.85
Delta (MeV)	2.57	1.28	2.22	1.28
Ex (MeV)	7.53	5.775	6.795	5.766
Tc (MeV)	0.671	0.605	0.600	0.549

The gamma-ray strength function of $1.4E-4$ obtained so as to reproduce the ORELA capture data /3/.

MT=251 : Mu-bar

Calculated with optical model.

MF=4 Angular Distributions of Secondary Neutrons

MT=2 : Calculated with optical model.

MT=16,17 : Isotropic in the laboratory system.

MT=51-66 : 90 degree symmetric in the center-of-mass system.

MT=91 : 90 degree symmetric in the laboratory system.

MF=5 Energy Distributions of Secondary Neutrons

MT=16,17,91 : Evaporation spectrum.

References

- 1) Weigmann H. et al.: Phys.Rev.,C20,115 (1969).
- 2) Weigmann H. et al.: 1971 Knoxville Conf.,CONF-710301,p.749.
- 3) Musgrove A.R.de.L. et al.: Nucl.Phys.,A270,108 (1976).
- 4) Iijima S. and Kawai M.: J.Nucl.Sci.Technol.,20,77 (1983).
- 5) Young P.G. and Arthur E.D.: LA-6947 (1977).
- 6) Igarasi S.: J.Nucl.Sci.Technol.,12,67 (1975).
- 7) Matumoto Z. et al.:JAERI-M 7734 (1978).
- 8) Iijima S. et al.: to be published in J.Nucl.Sci.Technol.

72-Hf-174 MAT number = 2721

72-Hf-174 NAIG+ Eval-Dec82 Hida, Yoshida, Iijima, Takano (JAERI)
Dist-Mar83 Rev1-Dec83

History

82-12 New evaluation for JENDL-2 was made by K.Hida, T.Yoshida,
S.Iijima (NAIG) and H.Takano (JAERI).

83-12 Angular distributions were modified and comment was added.

MF=1 General Information

MT=451 Descriptive data and dictionary

MF=2 Resonance Parameters

MT=151 Resolved and unresolved resonance parameters

Resolved resonances for MLBW formula

Energy range : 0.5 eV to 220 eV.

Res. energies and Gam-n : BNL-325 /1/ and Drake et al. /2/.

Gam-gamma : 0.060 eV assumed if unknown.

Background cross sections introduced.

Unresolved resonances

Energy range : 220 eV to 50 keV.

S0 : BNL-325 /1/.

S1,R and Gam-gamma : Adjusted so that the total cross
section of 9.49 b and capture
cross section of 0.752 b at 50 keV
were reproduced well.Parameters are D-obs = 16.0 eV, S0 = 2.80E-4, S1 = 1.06E-4,
R = 6.01 fm and Gam-gamma = 0.0844 eV.

2200 m/sec cross sections and calculated res. integrals.

	2200 m/sec	res. integ.
total	398.0 b /3/	-
elastic	8.0 b	-
capture	390.0 b /4/	492 b

MF=3 Neutron Cross Sections

Below 0.5 eV:

MF=1 Total

Sum of the elastic scattering and capture cross sections.

MF=2 Elastic scattering

The constant cross section of 8.0 barns was assumed.

MF=102 Capture

The curve in the form of $1/v$ was adjusted to 390 barns /4/ at
0.0253 eV.

From 0.5 eV to 50 keV:

Background cross sections are given.

Above 50 keV:

MF=1,2,4,51-68,91,102 Total, elastic, inelastic and capture
Calculated with optical and statistical models. Optical
potential parameters were fitted to the total cross section
of natural hafnium.

V0 = 38.0, Ws = 8.0 + 0.5 * SQRT(En), Vso = 7.0 (MeV),

a0 = 0.47, as = 0.52, aso = 0.47 (fm),

$r_0 = 1.32$, $r_s = 1.32$, $r_{so} = 1.32$ (fm).

Statistical model calculation was made with CASTHY code /5/.

Competing processes ; (n,2n), (n,3n), (n,p), (n,alpha),
and level fluctuation were considered.

Level schem taken from Table of Isotopes /6/

No.	Energy (MeV)	Spin-Parity
g.s.	0.0	0 +
1	0.0910	2 +
2	0.2975	4 +
3	0.6084	6 +
4	0.8282	0 +
5	0.9002	2 +
6	1.0622	4 +
7	1.2268	2 +
8	1.3034	3 +
9	1.3087	2 -
10	1.3194	2 +
11	1.3365	3 +
12	1.3947	4 +
13	1.4253	4 -
14	1.4429	5 -
15	1.4489	4 +
16	1.4964	2 +
17	1.5034	3 +
18	1.6261	4 +

Continuum levels assumed above 1.649 MeV.

Level density paramters were newly evaluated for Gilbert
and Cameron's formula /7/.

	a(1/MeV)	C(1/MeV)	T(MeV)	Ex(MeV)
Hf-174	23.09	2.31	0.477	5.01
Hf-175	22.93	10.0	0.484	4.42

MT=16,17,103,107 (n,2n), (n,3n), (n,p) and (n,alpha)

Calculated with multi-step Hauser-Feshbach model using
GNASH code /8/.

MT=251 Mu bar

Calculated with CASTHY code /5/.

MF=4 Angular Distributions of Secondary Neutrons

MT=2,51-68 : Calculated with CASTHY code /5/.

MT=16,17 : Isotropic in the laboratory system.

MT=91 : Calculated with CASTHY code /5/.

MF=5 Energy Distributions of Secondary Neutrons

MT=16,17,91 : Evaporation spectra.

References

- 1) Mughabghab S.F. and Garber D.I.: BNL 325 3rd Edition (1973).
- 2) Drake M.K., Sargis D.A. and Maung T.: EPRI NP-250 (1976).
- 3) Conrad C.A. et al.: Bull. Am. Phys. Soc., 14, 496 (1969).
- 4) Esch L.J. and Moore W.E.: Bull. Am. Phys. Soc., 6, 70 (1961).
- 5) Igarasi S.: J. Nucl. Sci. Technol., 12, 67 (1975).
- 6) Lederer C.M. and Shirley V.S.: Table of Isotopes 7th Edition (1979).
- 7) Gilbert A. and Cameron A.G.W.: Can. J. Phys., 43, 1446 (1965).
- 8) Young P.G. and Arthur E.D.: LA-6947 (1977).

72-Hf-176 MAT number = 2722

72-Hf-176 NAIG+ Eval-Dec82 Hida, Yoshida, Iijima, Takano (JAERI)
 Dist-Mar83 Rev1-Dec83

History

82-12 New evaluation for JENDL-2 was made by K.Hida, T.Yoshida,
 S.Iijima (NAIG) and H.Takano (JAERI).

83-12 Angular distributions were modified and comment was added.

MF=1 General Information

MT=451 Descriptive data and dictionary

MF=2 Resonance Parameters

MT=151 Resolved and unresolved resonance parameters

Resolved resonances for MLBW formula

Energy range : 0.5 eV to 700 eV.

Res. energies and Gam-n : BNL-325 /1/ and Drake et al. /2/.

Gam-gamma : 0.060 eV assumed, if unknown.

Background cross sections introduced.

Unresolved resonances

Energy range : 700 eV to 50 keV.

S0 : Calculated with optical model.

S1,R and Gam-gamma : Fitted to the capture cross section of Kapchigashev /3/ at 30 keV.

Parameters are D-obs = 32.0 eV, S0 = 1.92E-4, S1 = 1.11E-4,

R = 7.14 fm and Gam-gamma = 0.120 eV.

2200 m/sec cross sections and calculated res. integrals.

	2200 m/sec	res. integ.
total	46.00 b /4/	-
elastic	8.00 b	-
capture	38.00 b /5/	360 b

MF=3 Neutron Cross Sections

Below 0.5 eV:

MT=1 Total

Sum of the elastic scattering and capture cross sections.

MT=2 Elastic scattering

The constant cross section of 8.0 barns was assumed.

MT=102 capture

The curve in the form of 1/v was adjusted to 38 barns /4/ at 0.0253 eV.

From 0.5 eV to 50 keV:

Background cross sections are given.

Above 50 keV:

MT=1,2,4,51-73,91,102 Total, elastic, inelastic and capture

Calculated with optical and statistical models. Optical potential parameters were fitted to the total cross section of natural hafnium.

$V_0 = 38.0$, $W_s = 8.0 + 0.5 \cdot \text{SQRT}(E_n)$, $V_{s0} = 7.0$ (MeV),

$a_0 = 0.47$, $a_s = 0.52$, $a_{s0} = 0.47$ (fm),

$r_0 = 1.32$, $r_s = 1.32$, $r_{s0} = 1.32$ (fm).

Statistical model calculation was made with CASTHY code /6/.

Competing processes ; (n,2n), (n,3n), (n,p), (n,alpha),
and level fluctuation were considered.

Level schem taken from Table of Isotopes /7/

No.	Energy(MeV)	Spin-Parity
g.s.	0.0	0 +
1	0.0883	2 +
2	0.2902	4 +
3	0.5970	6 +
4	0.9980	8 +
5	1.1499	0 +
6	1.2266	2 +
7	1.2477	2 -
8	1.2932	0 +
9	1.3133	3 -
10	1.3413	2 +
11	1.3794	2 +
12	1.4046	4 -
13	1.4458	3 +
14	1.5777	3 +
15	1.6434	1 -
16	1.6723	1 +
17	1.7046	2 +
18	1.7102	3 -
19	1.7221	1 -
20	1.7675	2 -
21	1.7861	3 +
22	1.7937	3 -
23	1.8190	0 -

Continuum levels assumed above 1.840 MeV.

Level density paramters were newly evaluated for Gilbert
and Cameron's formula /8/.

	a(1/MeV)	C(1/MeV)	T(MeV)	Ex(MeV)
Hf-176	22.77	1.74	0.454	4.38
Hf-177	22.61	9.06	0.486	4.38

MT=16,17,103,107 (n,2n), (n,3n), (n,p) and (n.alpha)

Calculated with multi-step Hauser-Feshbach model using
GNASH code /9/.

MT=251 Mu-bar

Calculated with CASTHY code /6/.

MF=4 Angular Distributions of Secondary Neutrons

MT=2,51-68 : Calculated with CASTHY code /6/.

MT=16,17 : Isotropic in the laboratory system.

MT=91 : Calculated with CASTHY code /6/.

MF=5 Energy Distributions of Secondary Neutrons

MT=16,17,91 : Evaporation spectra.

References

- 1) Mughabghab S.F. and Garber D.I.: BNL 325 3rd Edition (1973).
- 2) Drake M.K., Sargis D.A. and Maung T.: EPRI NP-250 (1976).
- 3) Kapchigashev A.P.: Atomizdat, Moscow (1970).
- 4) Conrad C.A. et al.: Bull. Am. Phys. Soc., 14, 496 (1969).
- 5) Esch L.J. and Moore W.E.: Bull. Am. Phys. Soc., 6, 70 (1961).
- 6) Igarasi S.: J. Nucl. Sci. Technol., 12, 67 (1975).
- 7) Lederer C.M. and Shirley V.S.: Table of Isotopes 7 th Ed.

- (1979).
- 8) Gilbert A. and Cameron A.G.W.: Can. J. Phys., 43, 1446 (1965).
 - 9) Young P.G. and Arthur E.D.: LA-6947 (1977).

72-Hf-177 MAT number = 2723

72-Hf-177 NAIG+ Eval-Dec82 Hida, Yoshida, Iijima, Takano (JAERI)
Dist-Mar83 Rev1-Dec83

History

82-12 New evaluation for JENDL-2 was made by K.Hida, T.Yoshida,
S.Iijima (NAIG) and H.Takano (JAERI).
83-12 Angular distributions were modified and comment was added.

MF=1 General Information

MT=451 Descriptive data and dictionary

MF=2 Resonance Parameters

MT=151 Resolved and unresolved resonance parameters

Resolved resonances for MLBW formula

Energy range : 0.5 eV to 250 eV.
Res. energies and Gam-n : BNL 325 /1/ and Drake et al. /2/.
Gam-gamma : 0.066 eV assumed, if unknown.

Unresolved resonances

Energy range : 250 eV to 50 keV.
S0 : calculated with optical model.
S1,R and Gam-gamma : fitted to the 15 percent greater
value than capture cross section
of Kapchigashev /3/ at 30 keV.Parameters are D-obs = 2.40 eV, S0 = 1.92E-4, S1 = 1.12E-4,
R = 6.86 fm and Gam-gamma = 0.125 eV.

2200 m/s cross sections and calculated res. integrals.

	2200 m/s	Res. Integ.
total	359.0 b /4/	
elastic	7.0 b	
capture	352.0 b /5/	6950 b

MF=3 Neutron Cross Sections

Below 0.5 eV:

MT=1 Total

Sum of the elastic scattering and capture cross sections.

MT=2 Elastic scattering

The constant value of 7.0 barns was assumed at low energies.

MT=102 Capture

The curve in the form of $1/v$ was adjusted to 352 barns /5/ at
0.0253 eV.

From 0.5 eV to 50 keV:

Background cross sections are zero.

Above 50 keV.

MT=1,2,4,51-66,91,102 Total, elastic, inelastic and capture
Calculated with optical and statistical models. Optical
potential parameters were fitted to the total cross section
of natural hafnium.V0 = 38.0, Ws = 8.0(0.5+SQRT(En)), Vso = 7.0 (MeV),
a0 = 0.47, as = 0.52, aso = 0.47 (fm),
r0 = 1.32, rs = 1.32, rso = 1.32 (fm).

Statistical model calculation was made with CASTHY code /6/.

Competing processes ; (n,2n), (n,3n), (n,p), (n.alpha),
and level fluctuation were considered.

Level scheme taken from Table of Isotopes /7/

No.	Energy (MeV)	Spin-Parity
g.s.	0.0	7/2 -
1	0.1130	9/2 -
2	0.2497	11/2 -
3	0.3213	9/2 +
4	0.4095	13/2 -
5	0.4267	11/2 +
6	0.5081	5/2 -
7	0.5552	13/2 +
8	0.5913	15/2 -
9	0.6044	7/2 -
10	0.7085	15/2 +
11	0.7459	7/2 +
12	0.7945	17/2 -
13	0.8057	3/2 -
14	0.8474	9/2 +
15	0.8730	5/2 -
16	0.8828	17/2 +

Continuum levels assumed above 0.948 MeV.

Level density paramters were newly evaluated for Gilbert
and Cameron's formula /8/.

	a (1/MeV)	C (1/MeV)	T (MeV)	Ex (MeV)
Hf-177	22.61	9.06	0.486	4.38
Hf-178	22.36	2.22	0.451	4.08

MT=16,17,103,107 (n,2n), (n,3n), (n,p) and (n,alpha)

Calculated with multi-step Hauser-Feshbach model using
GNASH code /9/.

MT=251 Mu-bar

Calculated with CASTHY code /6/.

MF=4 Angular Distributions of Secondary Neutrons

MT=2.51-66 : Calculated with CASTHY code /6/.

MT=16,17 : Isotropic in the laboratory system.

MT=91 : Assumed the same distributions in the laboratory
system as those calculated with CASTHY code in
the center-of-mass system.

MF=5 Energy Distributions of Secondary Neutrons

MT=16,17,91 : Evaporation spectra.

References

- 1) Mughabghab S.F. and Garber D.I.: BNL 325 3rd Edition (1973).
- 2) Drake M.K., Sargis D.A. and Maung T.: EPRI NP-250 (1976).
- 3) Kapchigashev S.P.: Atomizdat, Moscow (1970).
- 4) Conrad C.A. et al.: Bull. Am. Phys. Soc., 14, 496 (1969).
- 5) Pavlenko et al.: 1975 Kiev Conf., Vol. 3, 171 (1975).
- 6) Igarasi S.: J. Nucl. Sci. Technol., 12, 67 (1975).
- 7) Lederer C.M. and Shirley V.S.: Table of Isotopes, 7th Ed.
(1979).
- 8) Gilbert A. and Cameron A.G.W.: Can. J. Phys., 43, 1446 (1965).
- 9) Young P.G. and Arthur E.D.: LA-6947 (1977).

72-Hf-178 MAT number = 2724

72-Hf-178 NAIG+ Eval-Dec82 Hida, Yoshida, Iijima, Takano (JAERI)
Dist-Mar83 Rev1-Jan84

History

82-12 New evaluation for JENDL-2 was made by K.Hida, T.Yoshida,
S.Iijima (NAIG) and H.Takano (JAERI).
83-12 Angular distributions were modified and comment was added.
84-01 Point-wise cross sections below 0.5 eV and background cross
sections were modified.

MF=1 General Information

MT=451 Descriptive data and dictionary

MF=2 Resonance Parameters

MT=151 Resolved and unresolved resonance parameters

Resolved resonances for MLBW formula

Energy range : 0.5 eV to 1.5 keV.
Res. energies and Gam-n : BNL-325 /1/ and Drake et al. /2/.
Gam-gamma : 0.060 eV assumed.
Background cross sections introduced.

Unresolved resonances

Energy region : 1.5 keV to 50 keV.
S0 : calculated with optical model.
S1,R and Gam-gamma : fitted to the capture cross sec-
tion of Beer and Macklin /3/.

Parameters are D-obs = 52.5 eV, S0 = 1.92E-4, S1 = 0.435E-4,
R = 7.17 fm and Gam-gamma = 0.060 eV.

2200 m/s cross sections and calculated res. integrals.

	2200 m/s	Res. Integ.
total	91.00 b /4/	-
elastic	5.00 b	-
capture	86.00 b /5/	1920 b

MF=3 Neutron Cross Sections

Below 0.5 eV:

MT=1 Total

Sum of the elastic scattering and capture cross sections.

MT=2 Elastic scattering

The cross section of 5.0 barns was assumed below 0.1 eV.
Above 0.1 eV, the cross section was connected smoothly to the
cross sections calculated from resonance parameters.

MT=102 Capture

The curve in the form of $1/v$ was normalized to 86 barns /5/
at 0.0253 eV.

From 0.5 eV to 50 keV:

Background cross section was given for the elastic scattering
cross section below 3.0 eV.

Above 50 keV:

MT=1,2,4,51,71,91,102 Total, elastic, inelastic and capture
Calculated with optical and statistical models. Optical
potential parameters were fitted to the total cross section

of natural hafnium.

$$V_0 = 38.0, W_s = 8.0 + 0.5 \cdot \text{SQRT}(E_n), V_{s0} = 7.0 \text{ (MeV)},$$

$$a_0 = 0.47, a_s = 0.52, a_{s0} = 0.47 \text{ (fm)},$$

$$r_0 = 1.32, r_s = 1.32, r_{s0} = 1.32 \text{ (fm)}.$$

Statistical model calculation was made with CASTHY code /6/.

Competing processes ; (n,2n), (n,3n), (n,p), (n,alpha),
and level fluctuation were considered.

Level scheme taken from Table of Isotopes /7/

No.	Energy (MeV)	Spin-Parity
g.s.	0.0	0 +
1	0.0932	2 +
2	0.3066	4 +
3	0.6322	6 +
4	1.0585	8 +
5	1.1474	8 -
6	1.1746	2 +
7	1.1993	0 +
8	1.2602	2 -
9	1.2766	2 -
10	1.3099	1 -
11	1.3224	3 -
12	1.3624	2 -
13	1.3641	9 -
14	1.4340	0 +
15	1.4438	0 +
16	1.4790	8 -
17	1.4961	2 +
18	1.5136	1 -
19	1.5613	2 +
20	1.5665	1 -
21	1.6015	10 -

Continuum levels assumed above 1.640 MeV.

Level density paramters were newly evaluated for Gilbert
and Cameron's formula /8/.

	a (1 MeV)	C (1 MeV)	T (MeV)	Ex (MeV)
Hf-178	22.36	2.22	0.451	4.08
Hf-179	22.57	6.88	0.465	3.98

MT=16,17,103,107 (n,2n), (n,3n), (n,p) and (n,alpha)

Calculated with multi-step Hauser-Feshbach model using
GNASH code /9/.

MT=251 Mu-bar

Calculated with CASTHY code /6/.

MF=4 Angular Distributions of Secondary Neutrons

MT=2,51-71 : Calculated with CASTHY code /6/.

MT=16,17 : Isotropic in the laboratory system.

MT=91 : Assumed the same distributions in the laboratory
system as those calculated with CASTHY code in
the center-of-mass system.

MF=5 Energy Distributions of Secondary Neutrons

MT=16,17,91 : Evaporation spectra.

References

- 1) Mughabghab S.F. and Garber D.I.: BNL 325 3rd Edition (1973).
- 2) Drake M.K., Sargis D.A. and Maung T.: EPRI NP-250 (1976).

- 3) Beer H. and Macklin R.L.: Phys. Rev., C26, 1404 (1982).
- 4) Conrad C.A. et al.: Bull. Am. Phys. Soc., 14, 496 (1969).
- 5) Pavlenko et al.: 1975 Kiev Conf., Vol. 3, 171 (1975).
- 6) Igarasi S.: J. Nucl. Sci. Technol., 12, 67 (1975).
- 7) Lederer C.M. and Shirley V.S.: Table of Isotopes, 7th Ed. (1979).
- 8) Gilbert A. and Cameron A.G.W.: Can. J. Phys., 43, 1446 (1965).
- 9) Young P.G. and Arthur E.D.: LA-6947 (1977).

72-Hf-179 MAT number = 2725

72-Hf-179 NAIG+ Eval-Dec82 Hida, Yoshida, Iijima, Takano (JAERI)
Dist-Mar83 Rev1-Dec83

History

82-12 New evaluation for JENDL-2 was made by K.Hida, T.Yoshida,
S.Iijima (NAIG) and H.Takano (JAERI).
83-12 Angular distributions were modified and comment was added.

MF=1 General Information

MT=451 Descriptive data and dictionary

MF=2 Resonance Parameters

MT=151 Resolved and unresolved resonance parameters

Resolved resonances for MLBW formula

Energy range : 0.5 eV to 250 eV.
Res. energies and Gam-n : BNL-325 /1/ and Drake et al. /2/.
Gam-gamma : 0.066 eV assumed.
Background cross sections introduced.

Unresolved resonances

Energy range : 250 eV to 50 keV.
S0 : calculated with optical model.
S1,R and Gam-gamma : fitted to the capture cross section of Beer and Macklin /3/.

Parameters are D-obs = 4.73 eV, S0 = 1.92E-4, S1 = 1.14E-4,
R = 7.12 fm and Gam-gamma = 0.063 eV.

2200 m/s cross sections and calculated res. integrals.

	2200 m/s	Res. Integ.
total	51.0 b /4/	-
elastic	6.0 b	
capture	45.0 b /1/	517 b

MF=3 Neutron Cross Sections

Below 0.5 eV:

MT=1 Total

Sum of the elastic scattering and capture cross sections.

MT=2 Elastic scattering

The constant cross section of 6.0 barns was assumed.

MT=102 Capture

The curve in the form of $1/v$ was normalized to 45 barns /1/
at 0.0253 eV.

From 0.5 eV to 50 keV:

Background cross section was given.

Above 50 keV:

MT=1,2,4,51-62,91,102 Total, elastic, inelastic and capture
Calculated with optical and statistical models. Optical
potential parameters were fitted to the total cross section
of natural hafnium.

$V_0 = 38.0$, $W_s = 8.0 + 0.5 \cdot \text{SQRT}(E_n)$, $V_{s0} = 7.0$ (MeV),
 $a_0 = 0.47$, $a_s = 0.52$, $a_{s0} = 0.47$ (fm),
 $r_0 = 1.32$, $r_s = 1.32$, $r_{s0} = 1.32$ (fm).

Statistical model calculation was made with CASTHY code /5/.

Competing processes ; (n,2n), (n,3n), (n,p), (n,alpha), and level fluctuation were considered.

Level scheme taken from Table of Isotopes /6/

No.	Energy (MeV)	Spin-Parity
g.s.	0.0	9/2 +
1	0.1227	11/2 +
2	0.2143	7/2 -
3	0.2688	13/2 +
4	0.3377	9/2 -
5	0.3750	1/2 -
6	0.4386	15/2 +
7	0.5184	5/2 -
8	0.6169	7/2 -
9	0.6312	17/2 +
10	0.8483	19/2 +
11	0.8702	7/2 -
12	1.0034	5/2 +

Continuum levels assumed above 1.070 MeV.

Level density paramters were newly evaluated for Gilbert and Cameron's formula /7/.

	a(1/MeV)	C(1/MeV)	T(MeV)	ex(MeV)
Hf-179	22.57	6.88	0.465	3.98
Hf-180	21.37	2.35	0.519	5.42

MT=16,17,103,107 (n,2n), (n,3n), (n,p) and (n,alpha)

Calculated with multi-step Hauser-Feshbach model using GNASH code /8/.

MF=4 Angular Distributions of Secondary Neutrons

MT=2,51-62 : Calculated with CASTHY code /6/.

MT=16,17 : Isotropic in the laboratory system.

MT=91 : Assumed the same distributions in the laboratory system as those calculated with CASTHY code in the center-of-mass system.

MF=5 Energy Distributions of Secondary Neutrons

MT=16,17,91 : Evaporation spectra.

References

- 1) Mughabghab S.F. and Garber D.I.: BNL 325 3rd Edition (1973).
- 2) Drake M.K., Sargis D.A. and Maung T.: EPRI NP-250 (1976).
- 3) Beer H. and Macklin R.L.: Phys. Rev., C26, 1404 (1982).
- 4) Conrad C.A. et al.: Bull. Am. Phys. Soc., 14, 496 (1969).
- 5) Igarasi S.: J. Nucl. Sci. Technol., 12, 67 (1975).
- 6) Lederer C.M. and Shirley V.S.: Table of Isotopes, 7th Ed. (1979).
- 7) Gilbert A. and Cameron A.G.W.: Can. J. Phys., 43, 1446 (1965).
- 8) Young P.G. and Arthur E.D.: LA-6947 (1977).

72-Hf-180 MAT number = 2726

72-Hf-180 NAIG+ Eval-Dec82 Hida, Yoshida, Iijima, Takano (JAERI)
Dist-Mar83 Rev1-Dec83

History

82-12 New evaluation for JENDL-2 was made by K.Hida, T.Yoshida,
S.Iijima (NAIG) and H.Takano (JAERI).
83-12 Angular distributions were modified and comment was added.

MF=1 General Information

MT=451 Descriptive data and dictionary

MF=2 Resonance Parameters

MT=151 Resolved and unresolved resonance parameters

Resolved resonances for MLBW formula

Energy range : 0.5 eV to 2.5 keV.
Res. energies and Gam-n : BNL-325 /1/ and Drake et al. /2/.
Gam-gamma : 0.060 eV assumed, if unknown.

Unresolved resonances

Energy region : 2.5 keV to 50 keV.
S0 : calculated with optical model.
S1,R and Gam-gamma : fitted to the capture cross section
of Beer and Macklin /3/.

Parameters are D-obs = 140 eV, S0 = 1.92E-4, S1 = 0.496E-4,
R = 7.14 fm and Gam-gamma = 0.060 eV.

2200 m/s cross sections and calculated res. integrals.

	2200 m/s	Res. Integ.
total	32.00 b /4/	-
elastic	19.40 b	-
capture	12.60 b /5/	34.6 b

MF=3 Neutron Cross Sections

Below 0.5 eV:

Point-wise cross sections were given.

From 0.5 eV to 50 keV:

Background cross section of zero was given.

Above 50 keV:

MT=1,2,4,51-58,91,102 Total, elastic, inelastic and capture
Calculated with optical and statistical models. Optical
potential parameters were fitted to the total cross section
of natural hafnium.

$V_0 = 38.0$, $W_s = 8.0 + 0.5 \cdot \text{SQRT}(E_n)$, $V_{so} = 7.0$ (MeV),
 $a_0 = 0.47$, $a_s = 0.52$, $a_{so} = 0.47$ (fm),
 $r_0 = 1.32$, $r_s = 1.32$, $r_{so} = 1.32$ (fm).

Statistical model calculation was made with CASTHY code /6/.

Competing processes ; (n,2n), (n,3n), (n,p), (n,alpha),
and level fluctuation were considered.

Level scheme taken from Table of Isotopes /7/

No.	Energy (MeV)	Spin-Parity
g.s.	0.0	0 -
1	0.0458	1 -
2	0.0680	4 +

3	0.0986	2 -
4	0.1700	5 +
5	0.2070	3 -
6	0.2570	1 -
7	0.2980	6 +
8	0.3320	2 -

Continuum levels assumed above 0.445 MeV.

Level density parameters were newly evaluated for Gilbert and Cameron's formula /8/.

	a(1/MeV)	C(1/MeV)	T(MeV)	Ex(MeV)
Hf-180	21.37	2.35	0.519	5.42
Hf-181	21.91	6.47	0.479	4.08

MT=16,17,103,107 (n,2n); (n,3n), (n,p) and (n,alpha)

Calculated with multi-step Hauser-Feshbach model using GNASH code /9/.

MT=251 Mu-bar

Calculated with CASTHY code /6/.

MF=4 Angular Distributions of Secondary Neutrons

MT=2,51-58 : Calculated with CASTHY code /6/.

MT=16,17 : Isotropic in the laboratory system.

MT=91 : Assumed the same distributions in the laboratory system as those calculated with CASTHY code in the center-of-mass system.

MF=5 Energy Distributions of Secondary Neutrons

MT=16,17,91 : Evaporation spectra.

References

- 1) Mughabghab S.F. and Garber D.I.: BNL 325 3rd Edition (1973).
- 2) Drake M.K., Sargis D.A. and Maung T.: EPRI NP-250 (1976).
- 3) Beer H. and Macklin R.L.: Phys. Rev., C26, 1404 (1982).
- 4) Conrad C.A. et al.: Bull. Am. Phys. Soc., 14, 496 (1969).
- 5) Scharff Goldhaber G. and McKeown M.: Phys. Rev., 158, 1105 (1967).
- 6) Igarasi S.: J. Nucl. Sci. Technol., 12, 67 (1975).
- 7) Lederer C.M. and Shirley V.S.: Table of Isotopes, 7th Ed. (1979).
- 8) Gilbert A. and Cameron A.G.W.: Can. J. Phys., 43, 1446 (1965).
- 9) Young P.G. and Arthur E.D.: LA-6947 (1977).

73-Ta-181 MAT number = 2731

73-Ta-181 SRI + Eval-Mar76 H.Yamakoshi, JENDL-CG, Y.Kikuchi
Dist-Mar83 Rev1-Nov83

History

76-03 The evaluation for JENDL-1 /1/ was made by H.Yamakoshi (Ship Research Institute) and JENDL-1 Compilation Group.
83-03 JENDL-1 data were adopted for JENDL-2 and extended to 20 MeV. MF=5 was revised, and unresolved resonance parameters were added by Y. Kikuchi (JAERI).
83-11 Comment data were added.

MF=1 General Information

MT=451 Descriptive data and dictionary

MF=2 Resonance Parameters

MT=151 Resolved and unresolved resonance parameters

Resolved parameters for MLBW formula

The energy region is from $1.0E-5$ eV to 1.0 keV. Parameters were taken from Ref. /2/ for positive resonances, and from ENDF/B-IV for a negative resonance. The radiative width of 0.0559 eV was assumed for the resonances whose radiative width was unknown.

Unresolved parameters

In the energy range from 1 to 50 keV, parameters were determined to reproduce the capture cross section evaluated for JENDL-1. The calculated total and elastic scattering cross sections were corrected by background cross sections. The parameters are as follows,

$R = 4.435$ fm, $D_{\text{obs}} = 4.39$ eV, radiative width = 0.0598 eV,
 $S_0 = 3.466E-4$, $S_1 = 0.45E-4$, $S_2 = 3.2E-4$.

Calculated 2200 m/sec cross sections and resonance integrals.

	2200-m/sec	res. integ.
elastic	6.110 b	-
capture	21.21 b	744. b
total	27.32 b	-

MF=3 Neutron Cross Sections

Below 50 keV.

Background cross sections were given for the unresolved resonance parameters.

Above 50 keV.

MT=1 Total

Evaluated from experimental data.

MT=2 Elastic scattering

Obtained by subtracting partial cross sections from the total cross section.

MT=4,51-61,91 Inelastic scattering

Calculated with statistical and optical model code CASTHY /3/. Optical potential parameters were determined so as to reproduce the average total cross section in the high energy region.

$V = 46.0 - 0.25 * E$ (MeV), $r = 1.268$, $a_0 = 0.62$ (fm)
 $W_i = 0.125 * E - 0.0004 * E ** 2$ (MeV), $r_i = 1.268$, $a_i = 0.62$ (fm)
 $W_s = 14.0 - 0.2 * E$ (MeV), $r_s = 1.316$, $a_s = 0.7$ (fm)
 $V_{so} = 6.0$ (MeV), $r_{so} = 1.099$, $a_{so} = 0.62$ (fm)

The level scheme was adopted from Ref. /4/.

No.	Energy (MeV)	Spin-Parity
g.s.	0.0	7/2 +
1	0.00621	9/2 -
2	0.13625	9/2 +
3	0.1587	11/2 -
4	0.3014	11/2 +
5	0.3390	13/2 -
6	0.4821	5/2 +
7	0.4951	13/2 +
8	0.5480	15/2 -
9	0.6151	1/2 +
10	0.6190	3/2 +
11	0.7166	15/2 +

Levels above 780 keV were assumed to overlapping.

MT=16 (n,2n)

Calculated with Pearlstein's method /5/.

MT=102 Capture

Calculated withn CASTHY /3/ by using D-obs = 4.4 eV and the average radiative width of 0.0598 eV.

MT=103 (n,p)

Calculated with Pearlstein's method /5/.

MT=251 Mu-bar

Calculated with CASTHY /3/.

MF=4 Angular Distributions of Secondary Neutrons

MT=2 Calculated with CASTHY code /3/.

MT=51.61 Isotropic in the center-of-mass system.

MT=16.91 Isotropic in the laboratory system.

MF=5 Energy Distributions of Secondary Neutrons

MT=16.91 Evaporation spectrum.

References

- 1) Igarasi S. et al.: JAERI 1261 (1979).
- 2) Mughabghab S.F. and Garber D.I.: BNL 325, 3rd Ed. (1973).
- 3) Igarasi S.: J. Nucl. Sci. Technol., 12, 67 (1975).
- 4) Ellis Y.A.: Nucl. Data Sheets, 9, 319 (1973).
- 5) Pearlstein S.: Nucl. Sci. Eng., 23, 238 (1965).

82-Pb- 0 MAT number = 2820

82-Pb- 0 JAERI Eval-Mar81 T.Asami
Dist-Mar83 Rev1-Jan84

History

81-03 Newly evaluated for JENDL-2 by T.Asami (JAERI).

84-01 Interpolation laws of cross sections and angular distributions were corrected. The total cross section was replaced with the data evaluated on the basis of experimental data. Comment was added.

MF=1 General Information

MT=451 Descriptive data and dictionary

MF=2 Resonance Parameters

MT=151 Resolved resonance parameters for MLBW formula

Resonance ranges

Pb-204: 1.0E-5 eV - 50 keV, Pb-206: 1.0E-5 eV - 200 keV

Pb-207: 1.0e-5 eV - 500 keV, pb-208: 1.0E-5 eV - 500 keV

Parameters were evaluated from the following exp. data.

Pb-204: Block+63 /1/, Gibbons+67 /2/, Allen+73 /3/.

Pb-206: Allen+73 /3/, Horen+79 /4/, Mizumoto+79 /5/.

Pb-207: Allen+73 /3/, Raman+77 /6/, Horen+79 /4/.

Pb-208: Allen+73 /3/, Wilenzick+61 /7/, Macklin+77 /8/,
Fowler66 /9/.

For unknown radiative widths, average values of known radiative widths were used.

Calculated 2200-m/s cross sections and res. integrals.

	2200 m/s	res. integ.
elastic	11.42 b	-
capture	0.1716b	0.148 b
total	11.59 b	-

MF=3 Neutron Cross Sections

Below 500 keV.

Background cross sections are given to take account of contribution from bound levels and to reproduce the thermal capture cross section of 0.171 barns which was evaluated from the experimental data /10-12/. Contributions from Pb-204 and Pb-206 were added in the background cross section below 500 keV.

Above 500 keV.

MT=1 Total

Cross sections in the energies from 500 keV to 15 MeV were obtained based on the experimental data of Schwartz+77 /13/. Above 15 MeV, cross sections were calculated with optical and statistical model code CASTHY /14/ by using optical potential parameters given below.

MT=2 Elastic scattering

(Total)-(All other partial cross sections)

MT=4,51-90,91 Inelastic scattering

Calculated with CASTHY /14/ for each isotope and constructed taking account of their isotope abundances. Contributions from some levels of Pb-204 and 206 were lumped and contributions from levels above 2.9454 MeV were put together into continuum (MT=91). The optical potential parameters used in the calculation were obtained by fitting average total cross section of natural lead as follows,

$$V = 47.0 - 0.250 * E, \quad W_s = 2.30 + 0.41 * E, \quad V_{so} = 6.0 \text{ (MeV)},$$

$$r_0 = 1.25, \quad r_s = 1.30, \quad r_{so} = 1.30 \text{ (fm)},$$

$$a_0 = 0.65, \quad b = 0.48, \quad a_{so} = 0.689 \text{ (fm)}.$$

Level density parameters for back-shifted fermi gas model were determined using low-lying level data and observed neutron resonance spacing. Some data for level density parameters were taken from Ref. /15/. Level scheme was taken from Ref. /16/. Level energies and corresponding isotopes are as follows:

MT	Energy (MeV)	Isotope	MT	Energy (MeV)	Isotope
51	0.5697	207	71	2.7260	207
52	0.8031	206	72	3.0165	206
53	0.8977	207	73	3.1800	207
54	0.8991	204	74	3.1977	208
55	1.1650	206	75	3.2000	207
56	1.2738	204	76	3.2230	207
57	1.3406	206	77	3.2793	206
58	1.4670	206	78	3.3000	207
59	1.5629	204	79	3.3840	207
60	1.6333	207	80	3.4130	207
61	1.6841	206	81	3.4750	208
62	1.9977	206	82	3.5090	207
63	2.0650	204	83	3.5830	207
64	2.2641	204	84	3.7085	208
65	2.3399	207	85	3.7440	206
66	2.3843	206	86	3.9199	208
67	2.6146	208	87	3.9464	208
68	2.6244	207	88	3.9609	208
69	2.6479	206	89	3.9957	208
70	2.6624	207	90	4.1252	208

MT=16,17,22,28,103,107 (n,2n), (n,3n), (n,n'p), (n,n'a), (n,p) and (n,a)

Calculated with evaporation model code GROGI /17/ for each isotope and constructed considering isotope abundances.

MT=102 Capture

Calculated with CASTHY /14/ for Pb-204, 206 and 207. For Pb-208, estimated from the experimental data of Pb-208 and natural lead. The capture cross section of natural lead were constructed from these isotopic data.

MT=251 Mu-bar

Calculated with CASTHY /14/.

MF=4 Angular Distributions of Secondary Neutrons

MT=2 : Calculated with CASTHY /14/.

MT=16,17,22,28 : Assumed to be isotropic in the lab system.

MT=51- 90 : Assumed to be isotropic in the center-of-mass system.

MT=91 : Assumed to be isotropic in the lab system.

MF=5 Energy Distributions of Secondary Neutrons
MT=16,17,22,28,91 : Evaporation spectra.

References

- 1) Block R.C. and Moxon M.C.: BAPS 8, 513 (1963).
- 2) Gibbons J.H. and Macklin R.L.: Phys. Rev., 153, 1356 (1967).
- 3) Allen B.J. et al.: Phys. Rev., C8, 1504 (1973).
- 4) Horen D.J. et al.: Phys. Rev., C20, 478 (1979).
- 5) Mizumoto M. et al.: Phys. Rev., C19, 335 (1979).
- 6) Raman S. et al.: Phys. Rev. Lett., 39, 598 (1977).
- 7) Wilenzick R.M. et al.: Phys. Rev., 121, 1150 (1961).
- 8) Macklin R.L. et al.: Astrophys. J., 217, 222 (1977).
- 9) Fowler J.L.: Phys. Rev., 147, 870 (1966).
- 10) Cranton et al.: Nucl. Phys., A169, 95 (1971).
- 11) Tattersall R.B. et al.: J. Nucl. Ener., A12, 32 (1960).
- 12) Stefanescu Al. et al.: International Conf. on Phys. and Technol. of Research Reactors. Bucurest. p.553 (1961).
- 13) Schwartz R.B. et al.: NBS mono 138 (1974), data in EXFOR (1971).
- 14) Igarasi S.: J. Nucl. Sci. Technol., 12, 67 (1975).
- 15) Dilg W. et al.: Nucl. Phys., A217, 269 (1973).
- 16) Lederer C.M. and Shirley V.S.: Table of Isotopes, 7th Edition (1978).
- 17) Gilat J.: BNL-50246(T-580) (1970).

82-Pb-204 MAT number = 2821

82-Pb-204 JAERI Eval-Mar81 T.Asami
Dist-Mar83 Rev1-Nov83

History

81-03 Newly evaluated for JENDL-2 by T.Asami (JAERI).
83-11 Interpolation laws of cross sections and angular distributions were corrected. Comment data were added.

MF=1 General Information

MT=451 Descriptive Data and Dictionary

MF=2 Resonance Parameters

MT=151 Resolved Resonance Parameters for MLBW Formula

Resonance range : 10^{-5} eV to 50 keV.

Parameters were evaluated from the data of Block+63 /1/, Gibbons+67 /2/ and Allen+73 /3/. Effective scattering radius of 8.5 fm was taken from Ref. /4/. For unknown radiative widths, assumed average values of 1.2 eV for s-wave and 0.6 eV for p-wave resonances.

Calculated 2200-m/s cross sections and res. integrals.

	2200 m/s	res. integ.
elastic	11.34 b	-
capture	0.661 b	2.69 b
total	12.00 b	-

MF=3 Neutron Cross Sections

Below 50 keV.

Background cross sections are given to take account of contribution from bound levels and to reproduce the thermal capture cross section of 0.661-barns /5/.

Above 50 keV.

Cross sections were obtained from optical and statistical model calculations. The optical potential parameters were obtained by fitting average total cross section of natural lead as follows,

$$V = 47.0 - 0.250 * E, \quad W_s = 2.30 + 0.41 * E, \quad V_{so} = 6.0 \text{ (MeV)},$$

$$r_0 = 1.25, \quad r_s = 1.30, \quad r_{so} = 1.30 \text{ (fm)},$$

$$a_0 = 0.65, \quad b = 0.48, \quad a_{so} = 0.689 \text{ (fm)}.$$

Level density parameters were determined using low-lying level data and observed neutron resonance spacing. Some data for level density parameters were taken from Ref. /6/.

MT=1 Total

Calculated with optical and statistical model code CASTHY /7/.

MT=2 Elastic Scattering

(Total) - (All other partial cross sections)

MT=4,51-68,91 Inelastic Scattering

Calculated with CASTHY /7/.

Level scheme taken from Ref. /8/.

No.	Energy (MeV)	Spin-Parity
g.s.	0.0	0 +

1	0.8991	2 +
2	1.2738	4 +
3	1.3538	2 +
4	1.5629	4 +
5	1.6047	3 +
6	1.8173	4 +
7	2.0650	5 +
8	2.1855	9 -
9	2.2578	5 -
10	2.2641	7 -
11	2.3381	5 -
12	2.3858	5 -
13	2.4050	7 -
14	2.4339	6 -
15	2.4801	6 -
16	2.5069	5 -
17	2.6271	3 -
18	2.6963	7 -

Levels above 2.945 MeV were assumed to be continuum.

MT=16,17,22,28,103,107 (n,2n), (n,3n), (n,n'p), (n,n'a), (n,p) and (n,a)

Calculated with evaporation model code GROGI /9/.

MT=102 Capture

Calculated with CASTHY /7/ and normalized to 30 milli-barns at 100 keV.

MT=251 Mu-bar

Calculated with CASTHY /7/.

MF=4 Angular Distributions of Secondary Neutrons

MT=2,51-68 : Calculated with CASTHY/7/.

MT=16,17,22,28 : Assumed to be isotropic in the lab system.

MT=91 : Assumed the same distributions in the lab system as those calculated with CASTHY in the center-of-mass system.

MF=5 Energy Distributions of Secondary Neutrons

MT=16,17,22,28,91 : Evaporation spectra.

References

- 1) Block R.C. and Moxon M.C.: BAPS 8, 513 (1963).
- 2) Gibbons J.H. and Macklin R.L.: Phys. Rev., 153, 1356 (1967).
- 3) Allen B.J. et al.: Phys. Rev., C8, 1504 (1973).
- 4) Macklin R.L. et al.: Phys. Rev., 136, B695 (1964).
- 5) Journey E. et al.: ANL-6797, 236 (1963).
- 6) Dilg W. et al.: Nucl. Phys., A217, 269 (1973).
- 7) Igarasi S.: J. Nucl. Sci. Technol., 12, 67 (1975).
- 8) Lederer C.M. and Shirley V.S.: Table of Isotopes, 7th Edition (1978).
- 9) Gilat J.: BNL-50246(T-580) (1970).

82-Pb-206 MAT number = 2822

82-Pb-206 JAERI Eval-Mar81 T.Asami
Dist-Mar83 Rev1-Nov83

History

81-03 Newly evaluated for JENDL-2 by T.Asami (JAERI).
83-11 Angular distributions were corrected. Comment data were added.

MF=1 General Information

MT=451 Descriptive Data and Dictionary

MF=2 Resonance Parameters

MT=151 Resolved Resonance Parameters for MLBW Formula

Resonance range : 10^{-5} eV to 200 keV.

Parameters were evaluated from the data of Allen+73 /1/, Horen+79 /2/ and Mizumoto+79 /3/. Effective scattering radius of 8.5 fm was taken from Ref. /4/. For unknown radiative widths, assumed average values of 0.8 eV for s-wave, 0.25 eV for p-wave and 0.08 eV for d-wave resonances.

Calculated 2200-m/s cross sections and res. integrals.

	2200 m/s	res. integ.
elastic	11.34 b	-
capture	0.028 b	0.0962 b
total	11.37 b	-

MF=3 Neutron Cross Sections

Below 200 keV.

Background cross sections are given to take account of contribution from bound levels and to reproduce the thermal capture cross section of 0.028 barns which was evaluated from experimental data to reproduce the thermal capture cross section of natural lead (0.171 barns).

Above 200 keV.

Cross sections were obtained from optical and statistical model calculations. The optical potential parameters were obtained by fitting average total cross section of natural lead as follows,

$$V = 47.0 - 0.250 * E, \quad W_s = 2.30 + 0.41 * e, \quad V_{so} = 6.0 \text{ (MeV)},$$

$$r_0 = 1.25, \quad r_s = 1.30, \quad r_{so} = 1.30 \text{ (fm)},$$

$$a_0 = 0.65, \quad b = 0.48, \quad a_{so} = 0.689 \text{ (fm)}.$$

Level density parameters were determined using low-lying level data and observed neutron resonance spacing. Some data for level density parameters were taken from Ref. /5/.

MT=1 Total

Calculated with optical and statistical model code CASTHY/6/.

MT=2 Elastic Scattering

(Total) - (All other partial cross sections)

MT=4,51-67,91 Inelastic Scattering

Calculated with CASTHY /6/.

Level scheme taken from Ref. /7/.

No.	Energy (MeV)	Spin-Parity
g.s.	0.0	0 +
1	0.8031	2 -
2	1.1650	0 +
3	1.3406	3 +
4	1.4670	2 +
5	1.6841	4 +
6	1.7030	1 +
7	1.7840	2 +
8	1.9977	4 +
9	2.1490	2 +
10	2.2002	7 -
11	2.3843	6 -
12	2.4240	2 +
13	2.6479	3 -
14	3.0165	5 -
15	3.1220	3 +
16	3.2793	5 -
17	3.744	1 +

Levels above 4.027 MeV were assumed to be continuum.

MT=16,17,22,28,103,107 (n,2n), (n,3n), (n,n'p), (n,n'a), (n,p) and (n,a)

Calculated with evaporation model code GROGI /8/.

MT=102 Capture

Calculated with CASTHY /6/ and normalized to 4 milli-barns at 50 keV.

MT=251 Mu-bar

Calculated with CASTHY /6/.

MF=4 Angular Distributions of Secondary Neutrons

MT=2,51-67 : Calculated with CASTHY/6/.

MT=16,17,22,28 : Assumed to be isotropic in the lab system.

MT=91 : Assumed the same distributions in the lab system as those calculated with CASTHY in the center-of-mass system.

MF=5 Energy Distributions of Secondary Neutrons

MT=16,17,22,28,91 : Evaporation spectra.

References

- 1) Allen J.B. et al.: Phys. Rev., C8, 1504 (1973).
- 2) Horen D.J. et al.: Phys. Rev., C20, 478 (1979).
- 3) Mizumoto M. et al.: Phys. Rev., C19, 335 (1979).
- 4) Macklin R.L. et al.: Phys. Rev., 136, B695 (1964).
- 5) Dilg W. et al.: Nucl. Phys., A217, 269 (1973).
- 6) Igarasi S.: J. Nucl. Sci. Technol., 12, 67 (1975).
- 7) Lederer C.M. and Shirley V.S.: Table of Isotopes, 7th Edition (1978).
- 8) Gilat J.: BNL-50246(T-580) (1970).

82-Pb-207 MAT number = 2823

82-Pb-207 JAERI Eval-Mar81 T.Asami
Dist-Mar83 Rev1-Nov83

History

81-03 Newly evaluated for JENDL-2 by T.Asami (JAERI).
83-11 Angular distributions were corrected. Comment data were added.

MF=1 General Information

MT=451 Descriptive Data and Dictionary

MF=2 Resonance Parameters

MT=151 Resolved Resonance Parameters for MLBW Formula

Resonance range : 1.0E-5 eV to 500 keV.

Parameters were evaluated from the data of Allen+73 /1/,
Raman+77 /2/ and Horen+78 /3/. Effective scattering
radius of 8.04 fm was taken from Ref. /3/. For unknown
radiative widths, assumed average value of 9.1 eV for s-
wave resonances.

Calculated 2200-m/s cross sections and res. integrals.

	2200 m/s	res. integ.
elastic	11.34 b	-
capture	0.703 b	0.375 b
total	12.04 b	-

MF=3 Neutron Cross Sections

Below 500 keV.

Background cross sections are given to take account of cont-
tribution from bound levels and to reproduce the thermal cap-
ture cross section of 0.703 barns which was evaluated from
experimental data to reproduce the thermal capture cross
section of natural lead (0.171 barns).

Above 500 keV.

Cross sections were obtained from optical and statistical
model calculations. The optical potential parameters were
obtained by fitting average total cross section of natural
lead as follows,

$$\begin{aligned}
 V &= 47.0 - 0.250 * E, & W_s &= 2.30 + 0.41 * E, & V_{so} &= 6.0 \text{ (MeV)}, \\
 r_0 &= 1.25, & r_s &= 1.30, & r_{so} &= 1.30 \text{ (fm)}, \\
 a_0 &= 0.65, & b &= 0.48, & a_{so} &= 0.689 \text{ (fm)}.
 \end{aligned}$$

Level density parameters were determined using low-lying
level data and observed neutron resonance spacing. Some data
for level density parameters were taken from Ref. /4/.

MT=1 Total

Calculated with optical and statistical model code CASTHY /5/.

MT=2 Elastic Scattering

(Total) - (All other partial cross sections)

MT=4,51 67.91 Inelastic Scattering

Calculated with CASTHY /5/.

Level scheme taken from Ref. /6/.

No.	Energy (MeV)	Spin-Parity
g.s.	0.0	1/2 -
1	0.5697	5/2 -
2	0.8977	3/2 -
3	1.6333	13/2 -
4	2.3399	7/2 -
5	2.6244	5/2 +
6	2.6624	7/2 +
7	2.7260	9/2 +
8	3.18	11/2 +
9	3.2	5/2 +
10	3.223	11/2 +
11	3.3	1/2 +
12	3.384	9/2 +
13	3.413	9/2 -
14	3.509	11/2 +
15	3.583	9/2 +
16	3.620	9/2 +
17	3.634	5/2 -

Levels above 4.100 MeV were assumed to be continuum.

MT=16,17,22,28,103,107 (n,2n), (n,3n), (n,n'p), (n,n'a), (n,p) and (n,a)

Calculated with evaporation model code GROGI /7/.

The calculated (n,p) cross section was normalized to 1.6 milli-barns at 14.5 MeV (Belovitchij+76 /8/). The (n,2n) cross section was normalized to 1.89 barns at 15.5 MeV. other cross sections were also normalized by the same factor as for the (n,p) cross section.

MT=102 Capture

Calculated with CASTHY /5/ and normalized to 2 milli-barns at 50 keV.

MT=251 Mu-bar

Calculated with CASTHY /5/.

MF=4 Angular Distributions of Secondary Neutrons

MT=2,51-67 : Calculated with CASTHY /5/.

MT=16,17,22,28 : Assumed to be isotropic in the lab system.

MT=91 : Assumed the same distributions in the lab system as those calculated with CASTHY in the center-of-mass system.

MF=5 Energy Distributions of Secondary Neutrons

MT=16,17,22,28,91 : Evaporation spectra.

References

- 1) Allen J.B. et al.: Phys. Rev., C8, 1504 (1973).
- 2) Raman S. et al.: Phys. Rev. Lett., 39, 598 (1977).
- 3) Horen D.J. et al.: Phys. Rev., C20, 478 (1979).
- 4) Dilg W. et al.: Nucl. Phys., A217, 269 (1973).
- 5) Igarasi S.: J. Nucl. Sci. Technol., 12, 67 (1975).
- 6) Lederer C.M. and Shirley V.S.: Table of Isotopes, 7th Edition (1978).
- 7) Gilat j.: BNL 50246(T-580) (1970).
- 8) Belovitchij G.E.: 1975 Kiev Conf., Vol.4, 209 (1976).

82-Pb-208 MAT number = 2824

82-Pb-208 JAERE Eval-Mar81 T.Asami
Dist-Mar83 Rev1-Nov83

History

81-03 Newly evaluated for JENDL-2 by T.Asami (JAERI).

83-11 Angular distributions were corrected. Comment data were added.

MF=1 General Information

MT=451 Descriptive Data and Dictionary

MF=2 Resonance Parameters

MT=151 Resolved Resonance Parameters for MLBW Formula

Resonance range : 1.0E-5 eV to 800 keV.

Parameters were evaluated from the data of Allen+73 /1/, Wilenzick+61 /2/, Macklin+77 /3/ and Fowler66 /4/. Effective scattering radius of 6.5 fm was selected. Neutron width of 515-keV s-wave resonance was estimated to reproduce the 2200-m/sec capture cross section of 0.48 milli-barns /5/.

Calculated 2200-m/s cross sections and res. integrals.

	2200 m/s	res. integ.
elastic	11.49 b	-
capture	0.4799 milli-b	7.83 milli-b
total	11.49 b	-

MF=3 Neutron Cross Sections

Below 800 keV.

Background cross sections are given for the elastic scattering cross section.

Above 800 keV.

Cross sections were obtained from optical and statistical model calculations. The optical potential parameters were obtained by fitting average total cross section of natural lead as follows,

$$V = 47.0 - 0.250 * E, \quad W_s = 2.30 + 0.41 * E, \quad V_{so} = 6.0 \text{ (MeV)},$$

$$r_0 = 1.25, \quad r_s = 1.30, \quad r_{so} = 1.30 \text{ (fm)},$$

$$a_0 = -0.65, \quad b = 0.48, \quad a_{so} = 0.689 \text{ (fm)}.$$

Level density parameters were determined using low-lying level data and observed neutron resonance spacing. Some data for level density parameters were taken from Ref. /6/.

MT=1 Total

Calculated with optical and statistical model code CASTHY /7/.

MT=2 Elastic Scattering

(Total) - (All other partial cross sections)

MT=4,51-64,91 Inelastic Scattering

Calculated with CASTHY /7/.

Level scheme taken from Ref. /8/.

No.	Energy (MeV)	Spin-Parity
g.s.	0.0	0 +
1	2.6146	3 -

2	3.1977	5 -
3	3.4750	4 -
4	3.7085	5 -
5	3.9199	6 -
6	3.9464	5 -
7	3.9609	4 -
8	3.9957	6 -
9	4.1252	4 -
10	4.1803	5 -
11	4.2962	5 -
12	4.3584	4 -
13	4.3829	6 -
14	4.4805	6 -

Levels above 4.577 MeV were assumed to be continuum.

MT=16,17 (n,2n) and (n,3n)

Calculated with evaporation model code GROGI /9/. The (n,2n) cross section was normalized to 2.01 barns at 15.5 MeV.

MT=22 (n,n'alpha)

calculated with code GROGI /9/ and normalized by the same factor as for (n,a) cross section.

MT=28 (n,n'p)

Calculated with code GROGI /9/ and normalized by the same factor as for (n,p) cross section.

MT=102 Capture

Estimated from the following experimental data:

Leipunskii+58 /10/, Csikai+67 /11/, Drake+71 /12/.

Bergqvist+72 /13/ and Diven+60 /14/.

MT=103 (n,p)

Calculated with code GROGI /9/ and normalized to an average value of experimental data by Hankla+72 /15/ and Belovitchkij+76 /16/ (0.48 milli-barns at 14.5 MeV).

MT=107 (n,a)

Calculated with code GROGI /9/ and normalized to 1.5 milli-barns at 14.5 MeV by Coleman-59 /17/.

MT=251 Mu-bar

Calculated with CASTHY /7/.

MF=4 Angular Distributions of Secondary Neutrons

MT=2,51-64 : Calculated with CASTHY/7/.

MT=16,17,22,28 : Assumed to be isotropic in the lab system.

MT=91 : Assumed the same distributions in the lab system as those calculated with CASTHY in the center-of-mass system.

MF=5 Energy Distributions of Secondary Neutrons

MT=16,17,22,28,91 : Evaporation spectra.

References

- 1) Allen J.B. et al.: Phys. Rev., C8, 1504 (1973).
- 2) Wilenzick R.M. et al.: Phys. Rev., 121, 1150 (1961).
- 3) Macklin R.L. et al.: Astrophys. J., 217, 222 (1977).
- 4) Fowler J.L.: Phys. Rev., 147, 870 (1966).
- 5) Emery J.F.: ORNL-4343, 71 (1968).
- 6) Dilg W. et al.: Nucl. Phys., A217, 269 (1973).
- 7) Igarasi S.: J. Nucl. Sci. Technol., 12, 67 (1975).
- 8) Lederer C.M. and Shirley V.S.: Table of Isotopes, 7th Edition

- (1978).
- 9) Gilat J.: BNL-50246(T-580) (1970).
 - 10) Leipunskii et al.: 2nd Geneva Conf., 15, 50 (1958).
 - 11) Csikai J. et al.: Nucl. Phys., A95, 229 (1967).
 - 12) Drake D. et al.: Phys., Letters, B36, 557 (1971).
 - 13) Bergqvist I. et al.: Nucl. Phys., A191, 641 (1972).
 - 14) Diven B.C. et al.: Phys. Rev., 120, 556 (1960).
 - 15) Hankla A.K. et al.: Nucl. Phys., A180, 157 (1972).
 - 16) Belovitchkij G.E.: 1975 Kiev Conf., Vol.4, 209 (1976).
 - 17) Coleman R.F. et al.: Proc. Roy. Soc. (London), 73, 215 (1959).

90-Th-228 MAT number = 2901

90-Th-228 Kyushu U. Eval-Apr81 T.Ohsawa and M.Ohta
Dist-Mar83 Rev1-Nov83

History

- 81-04 New evaluation was made by T. Osawa and M. Ohta (Kyushu University). Details of the evaluation are described in Ref. /1/.
- 83-11 Fission spectrum was added. Resonance formula was changed to MLBW formula. The total, (n,2n) and (n,3n) cross sections were modified. Comment was added.

MF=1 General Information

- MT=451 Comments and dictionary
- MT=452 Total number of neutrons emitted per fission
Calculated with the semi-empirical formula of Howerton /2/.

MF=2 Resonance Parameters

- MT=151 Resolved resonances
Resonance region is below 7.798 eV. Parameters were given for the MLBW formula. Only two resonances were observed by Simpson et al. /3/. An additional term with $1/v$ dependence was assumed to reproduce the thermal capture cross section. Fission cross section was also assumed to have $1/v$ behavior.

Calculated 2200-m/s cross sections and res. integ. (barns)

	2200-m/s	Res. Integ.
elastic	12.81	-
capture	119.9	1170
fission	0.300	1.02
total	133.0	-

MF=3 Neutron Cross Sections

Below 7.798 eV is the resonance region. Background data were given. The cross sections were evaluated above 7.798 eV as follows.

MT=1 Total cross section

Optical model calculation with the following parameters:

- $V = 41.0 - 0.05 \cdot E$ (MeV),
 $W_s = 6.4 + 0.15 \cdot \text{SQRT}(E)$ (MeV), — der. Woods-Saxon —
 $V_{so} = 7.0$ (MeV),
 $r_0 = r_{so} = 1.31$ (fm),
 $r_s = 1.38$ (fm),
 $a = b = a_{so} = 0.47$ (fm).

These parameters were taken from those for Th-232 /4/.

MT=2 Elastic scattering cross section

Statistical and optical model calculations using the code CASTHY /5/.

MT=4,51-62,91 Inelastic scattering cross section

Statistical and optical model calculations.

Level scheme of Th-228 /6/.

No. Energy (MeV) Spin-Parity

g.s.	0.0	0 +
1	0.0576	2 +
2	0.1869	4 +
3	0.328	1 -
4	0.3961	3 -
5	0.5193	5 -
6	0.8317	0 -
7	0.8746	2 +
8	0.9441	2 +
9	0.952	1 -
10	0.9688	2 +
11	1.016	3 -
12	1.0224	3 +

Levels above 1.025 MeV were assumed to be overlapping.

MT=16,17 (n,2n) and (n,3n) cross sections

Calculated by means of the evaporation model of Segev and Caner /7/.

MT=18 Fission cross section

The data of Vorotnikov et al. /8/ were adopted up to 5 MeV. The fission cross section of the neighboring even-even isotope Th-230 normalized to join smoothly to the data of Vorotnikov et al. was adopted above 5 MeV.

MT=102 Capture cross section

Statistical and optical model calculations with gamma-ray strength function of 0.00791.

MT=251 Mu-bar

Calculated with optical model.

MF=4 Angular Distributions of Secondary Neutrons

MT=2,51-62,91

Statistical and optical model calculations.

MT=16,17,18

Assumed to be isotropic in the laboratory system.

MF=5 Energy Distributions of Secondary Neutrons

MT=16,17,91

Evaporation spectra

MT=18

Fission spectrum estimated from $Z^{2/A}$ systematics by Smith et al. /9/.

References

- 1) Ohsawa T. and Ohta M.: Memoirs Faculty of Engineering, Kyushu Univ. 40, 149 (1980).
- 2) Howerton R.J.: Nucl. Sci. Eng. 62, 438 (1977).
- 3) Simpson O.D. et al.: ibid. 29, 423 (1967).
- 4) Ohsawa T. and Ohta M.: J. Nucl. Sci. Technol. 18, 408 (1981).
- 5) Igarasi S.: ibid. 12, 67 (1975).
- 6) Lederer C.M. and Shirley V.S. (Ed.): Table of Isotopes, 7th Edition (1978).
- 7) Segev M. and Caner M.: Ann. Nucl. Energy 5, 239 (1978).
- 8) Vorotnikov et al.: Sov. J. Nucl. Phys. 16, 505 (1973).
- 9) Smith A.B. et al.: ANL/NDM-50 (1979).

90-Th-230 MAT number = 2902

90-Th-230 Kyushu U. Eval-Apr81 T.Ohsawa and M.Ohta
Dist-Mar83 Rev1-Nov83

History

81-04 New evaluation was made by T. Ohsawa and M. Ohta (Kyushu University). Details of evaluation are described in Ref. /1/.

83-11 Fission spectrum was added. Resonance parameters, and total, (n,2n) and (n,3n) cross sections were modified. Comment data were added.

MF=1 General Information

MT=451 Comments and Dictionary

MT=452 Total number of neutrons emitted per fission
Calculated with the semi empirical formula of Howerton /2/.

MF=2 Resonance Parameters

MT=151 Resolved resonances

Resonance region is below 564.26 eV. The MLBW formula was selected to reproduce resonance cross sections. A total number of 28 resonances up to 563 eV measured by Kalebin et al. /3/ were adopted in the present evaluation. A background term with $1/v$ dependence was added in order to reproduce the thermal capture cross section.

Calculated 2200-m/s cross sections and res. integ. (barns)

	2200-m/s	Res. Integ.
elastic	9.774	-
capture	22.55	1040
fission	0.0	1.12
total	32.32	-

MF=3 Neutron Cross Sections

Below 564.26 eV is the resonance region where the background cross sections are given. Above 564.26 eV, the cross sections were evaluated as follows.

MT=1 Total cross section

Optical model calculation with the following parameters:

$V = 41.0 - 0.05 * E$ (MeV),
 $W_s = 6.4 + 0.15 * \text{SQRT}(E)$ (MeV), — der. Woods-Saxon —
 $V_{so} = 7.0$ (MeV),
 $r_0 = r_{so} = 1.31$ (fm),
 $r_s = 1.38$ (fm),
 $a = b = a_{so} = 0.47$ (fm).

These parameters were taken from those for Th-232 /4/.

MT=2 Elastic scattering cross section

Statistical and optical model calculations using the code CASTHY /5/.

MT=4.51 63.91 Inelastic scattering cross section

Statistical and optical model calculations.

Level scheme of Th-230 /6/.

No.	Energy (MeV)	Spin-Parity
g.s.	0.0	0 +
1	0.0534	2 +
2	0.173	4 +
3	0.357	6 +
4	0.506	1 -
5	0.571	3 -
6	0.635	0 +
7	0.678	2 +
8	0.682	5 -
9	0.781	2 +
10	0.881	4 +
11	0.951	1 -
12	1.009	2 +
13	1.012	3 -

Levels above 1.02 MeV were assumed to be overlapping.

MT=16,17 (n,2n) and (n,3n) cross sections

Calculated by means of the evaporation model of Segev and Caner /7/.

MT=18 Fission cross section

Evaluation was made on the basis of the data of Muir et al. /8/ up to 2 MeV. Above 2 MeV, the fission probability data of Back et al. /9/ were used to calculate the fission cross section.

MT=102 Capture cross section

Statistical and optical model calculations with gamma-ray strength function of 0.00791.

MT=251 Mu-bar

Calculated with CASTHY.

MF=4 Angular Distributions of Secondary Neutrons

MT=2,51-63,91

Statistical and optical model calculations.

MT=16,17,18

Assumed to be isotropic in the laboratory system.

MF=5 Energy Distributions of Secondary Neutrons

MT=16,17,91

Evaporation spectra.

MT=18

Fission spectrum estimated from Z^{*2}/A systematics by Smith et al. /10/.

References

- 1) Ohsawa T. and Ohta M.: Memoirs Faculty of Engineering, Kyushu Univ. 40, 149 (1980).
- 2) Howerton R.J.: Nucl. Sci. Eng. 62, 438 (1977).
- 3) Kalebin S.M. et al.: Sov. J. Atom. Energy 26, 588 (1969).
- 4) Ohsawa T. and Ohta M.: J. Nucl. Sci. Technol. 18, 408 (1981).
- 5) Igarasi S.: ibid. 12, 67 (1975).
- 6) Lederer C.M. and Shirley V.S. (Ed.): Table of Isotopes, 7th Edition (1978).
- 7) Segev M. and Caner M.: Ann. Nucl. Energy 5, 239 (1978).
- 8) Muir D.W. et al.: Proc. 3rd Conf. on Neutron Cross Sections and Technology, Knoxville (1971), p.292.

- 9) Back B.B. et al.: Phys. Rev. C13, 2374 (1974).
- 10) Smith A.B. et al.: ANL/NDM-50 (1979).

90-Th-232 MAT number = 2903

90-Th-232 Kyushu U. Eval-Mar80 T.Ohsawa and M.Ohta
 NST 18,408 (1981) Dist-Mar83 Rev1-Nov83

History

80-03 New evaluation for JENDL-2 was made by T. Ohsawa and M. Ohta
 (Kyushu University). Details given in Ref. /1/.

83-11 Comment was added.

MF=1 General Information

MT=451 Comments and dictionary

MT=452 Number of neutrons per fission

Sum of MT=455 and MT=456.

MT=454 Fission product yield data

Taken from ENDF B-IV.

MT=455 Delayed neutron data

MT=456 Number of prompt neutrons per fission

A single linear fit by Conde and Holmberg /2/ was adopted.

MF=2 Resonance Parameters

MT=151

Resolved resonances for MLBW formula : 1.0E-5 eV - 3.5 keV

Resonance parameters taken from Rahn et al. /3/ and BNL-
 325, 3rd Edition. 14 negative resonances were added.

Unresolved resonances: 3.5 keV - 50 keV

Parameters determined so as to reproduce the evaluated
 smooth cross sections. Strength functions have slight
 energy dependence.

$D(J=1/2) = 18.64 \text{ eV}$, $\text{Gam-g} = 21.2 \text{ milli-eV}$,

Average $S0 = 0.94E-4$, Average $S1 = 2.00E-4$.

Calculated 2200-m/s cross sections and res. integrals (barns)

	2200 m. s	Res. Integ.
elastic	12.16	-
fission	0.0	0.636
capture	7.258	79.9
total	19.42	-

MF=3 Neutron Cross Sections

Below 50 keV, background cross sections for unresolved resonance
 parameters were given. The cross sections represented with the
 unresolved resonance parameters and those above 50 keV were
 evaluated as follows.

MT=1,2,4,51-70,91,251 Total, elastic, inelastic, and mu-bar

Experimental data of Foster et al. /4/, Fasoli et al. /5/.

Kobayashi et al. /6/ and Uttley /7/ were adopted for total

cross section. The spherical optical potential parameters

were obtained from fitting to the above data:

$V = 41.0 - 0.05E$ (MeV),

$W_s = 6.4 - 0.15 \cdot \text{SQRT}(E)$ (MeV),

$V_{so} = 7.0$ (MeV),

$r_0 = r_{so} = 1.31$ (fm),

$r_s = 1.38$ (fm),
 $a = b = a_{so} = 0.47$ (fm).
 Derivative Woods-Saxon form assumed for surface
 imaginary part.

Statistical model calculation with CASTHY code /8/.
 Competing processes : fission, (n,2n) and (n,3n)
 Level width fluctuation considered.

The level scheme taken from Refs./9/ and /10/.

No.	Energy(keV)	Spin-Parity
g.s.	0.0	0 +
1	49.5	2 +
2	162.5	4 +
3	333.0	6 +
4	555.0	8 +
5	714.3	1 -
6	730.4	0 +
7	774.1	2 +
8	774.3	3 -
9	786.3	2 +
10	829.7	3 +
11	873.1	4 +
12	883.3	5 -
13	890.4	4 +
14	960.3	5 +
15	1053.9	2 -
16	1073.3	2 +
17	1077.7	1 -
18	1078.8	0 +
19	1095.0	3 +
20	1106.0	3 -

Continuum levels assumed above 1.11 MeV.

The level density parameters of Gilbert and Cameron /11/
 was used.

MT=16,17 (n,2n) and (n,3n)

Calculated by means of the evaporation model of Segev et al.
 /12/.

MT=18 Fission

Evaluated on the basis of the data of Behrens et al. /13/.
 using the U-235 fission cross section data of Matsunobu
 /14/.

MT=102 Capture

Evaluated on the basis of the measured data of Kobayashi
 et al. /15/ and Lindner et al. /16/.

MF=4 Angular Distributions of Secondary Neutrons

MT=2,51-70,91 Statistical model calculation with CASTHY /8/.

MT=16,17,18 Isotropic in the laboratory system.

MF=5 Energy Distributions of Secondary Neutrons

MT=16,17 Evaporation spectrum.

MT=18 Fission spectrum (Watt).

MT=455 Taken from ENDF/B-IV.

References

- 1) Ohsawa T. and Ohta M.: J. Nucl. Sci. Technol. 18, 408 (1981).
- 2) Conde H. and Holmberg M.: Proc. Symp. Phys. and Chem. of Fission, 2, 57 (1965).
- 3) Rahn F. et al.: Phys. Rev. C6, 1854 (1972).
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- 15) Kobayashi K. et al.: J. Nucl. Sci. Technol. 18, 823 (1981).
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90-Th-233 MAT number = 2904

90-Th-233 Kyushu U. Eval-Apr81 T.Ohsawa and M.Ohta
Dist-Mar83 Rev1-Nov83

History

- 81-04 Evaluation was made by T. Ohsawa and M. Ohta (Kyushu University). Details of the evaluation are described in Ref. /1/.
- 83-11 Fission spectrum was added. The total, (n,2n) and (n,3n) cross sections were modified. Comment was added.

MF=1 General Information

- MT=451 Comments and dictionary
- MT=452 Total number of neutrons emitted per fission
Calculated with the semi-empirical formula of Howerton /2/.

MF=2 Resonance Parameters

- MT=151 Resolved resonances
- No resolved resonances were adopted, since there were no measurements made. Capture and fission cross sections at 0.0253 eV were extrapolated up to 200 eV by assuming the form of $1/v$ for the former, and up to 20 keV by assuming the form of $1/v$ plus the constant value of 0.3 barns for the latter.

Calculated 2200-m/s cross sections and res. integ. (barns)

	2200-m/s	Res. Integ.
elastic	13.0	-
capture	1450.0	643
fission	15.0	11.1
total	1478.0	-

MF=3 Neutron Cross Sections

- MT=1 Total cross section
- Optical model calculation with the following parameters:
- $V = 41.0 - 0.05 \cdot E$ (MeV),
- $W_s = 6.4 + 0.15 \cdot \text{SQRT}(E)$ (MeV), -- der. Woods-Saxon --
- $V_{so} = 7.0$ (MeV),
- $r_0 = r_{so} = 1.31$ (fm),
- $r_s = 1.38$ (fm),
- $a = b = a_{so} = 0.47$ (fm).

These parameters were taken from those for Th-232 /3/.

- MT=2 Elastic scattering cross section
- Statistical and optical model calculations using the code CASTHY /4/.

- MT=4,51-65,91 Inelastic scattering cross section
- Statistical and optical model calculations.

Level scheme of Th-233 /5/.

No.	Energy (MeV)	Spin-Parity
g.s.	0.0	1/2 +
1	0.01687	3/2 +
2	0.05456	5/2 +

3	0.09363	7/2 +
4	0.37121	5/2 +
5	0.53958	1/2 -
6	0.58393	1/2 +
7	0.6115	3/2 +
8	0.62902	5/2 +
9	0.6822	3/2 -
10	0.7135	1/2 +
11	0.7218	3/2 +
12	0.7695	5/2 +
13	0.8145	3/2 +
14	0.8914	3/2 +
15	0.9476	3/2 -

Levels above 0.95 MeV were assumed to be overlapping.

MT=16,17 (n,2n) and (n,3n) cross sections

Calculated by means of the evaporation model of Segev and Caner /6/.

MT=18 Fission cross section

Fission probability deduced from direct reaction /7, 8/ was used to calculate the fission cross section.

MT=102 Capture cross section

Statistical and optical model calculations with gamma-ray strength function of 0.00352.

MT=251 Mu-bar

Calculated with optical model.

MF=4 Angular Distributions of Secondary Neutrons

MT=2,51-65,91

Statistical and optical model calculations.

MT=16,17,18

Assumed to be isotropic in the laboratory system.

MF=5 Energy Distributions of Secondary Neutrons

MT=16,17,91

Evaporation spectra.

MT=18

Fission spectrum estimated from $Z+2/A$ systematics of Smith et al. /9/.

References

- 1) Ohsawa T. and Ohta M.: Memoirs Faculty of Engineering, Kyushu Univ. 40, 149 (1980).
- 2) Howerton R.J.: Nucl. Sci. Eng. 62, 438 (1977).
- 3) Ohsawa T. and Ohta M.: J. Nucl. Sci. Technol. 18, 408 (1981).
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- 6) Segev M. and Caner M.: Ann. Nucl. Energy 5, 239(1978).
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90-Th-234 MAT number = 2905

90-Th-234 Kyushu U. Eval-Apr81 T.Ohsawa and M.Ohta
Dist-Mar83 Rev1-Nov83

History

81-04 Evaluation was made by T. Ohsawa and M. Ohta (Kyushu University). Details of the evaluation are described in Ref. /1/.

83-11 Fission spectrum was given. The total, (n,2n) and (n,3n) cross sections were modified. Comment was added.

MF=1 General Information

MT=451 Comments and dictionary

MT=452 Total number of neutrons emitted per fission
Calculated with the semi-empirical formula of Howerton /2/.

MF=2 Resonance Parameters

MT=151 Resolved resonances

No resolved resonances were adopted, since there were no measurements made. Capture and fission cross sections at 0.0253 eV were extrapolated on an $1/v$ basis up to an energy of 15 eV.

Calculated 2200-m/s cross sections and res. integ. (barns)

	2200-m/s	Res. Integ.
elastic	13.0	-
capture	1.75	93.7
fission	0.0	0.26
total	14.75	-

MF=3 Neutron Cross Sections

MT=1 Total cross section

Optical model calculation with the following parameters:

$V = 41.0 - 0.05E$ (MeV),
 $W_s = 6.4 + 0.15 \cdot \text{SQRT}(E)$ (MeV), — der. Woods-Saxon —
 $V_{so} = 7.0$ (MeV),
 $r_0 = r_{so} = 1.31$ (fm),
 $r_s = 1.38$ (fm),
 $a = b = a_{so} = 0.47$ (fm).

These parameters were taken from those for Th-232 /3/.

MT=2 Elastic scattering cross section

Statistical and optical model calculations using the code CASTHY /4/.

MT=4,51-67,91 Inelastic scattering cross section

Statistical and optical model calculations:

Level scheme of Th-234 (estimated from systematics)

No.	Energy (MeV)	Spin-Parity
g.s.	0.0	0 +
1	0.048	2 +
2	0.160	4 +
3	0.336	6 +
4	0.576	8 +

5	0.730	0 +
6	0.767	2 +
7	0.785	2 +
8	0.853	4 +
9	0.882	1 -
10	0.889	4 +
11	0.942	3 -
12	0.987	6 +
13	1.050	5 -
14	1.053	6 +
15	1.073	8 +
16	1.206	7 +
17	1.277	8 +

Levels above 1.06 MeV were assumed to be overlapping.

MT=16,17 (n,2n) and (n,3n) cross sections

Calculated by means of the evaporation model of Segev and Caner /5/.

MT=18 Fission cross section

Fission probability deduced from direct reaction /6/ and systematics of Behrens /7/ were used to obtain fission cross section.

MT=102 Capture cross section

Statistical and optical model calculations with gamma-ray strength function of 0.00791.

MT=251 Mu-bar

Calculated with optical model.

MF=4 Angular Distributions of Secondary Neutrons

MT=2,51-67,91

Statistical and optical model calculations.

MT=16,17,18

Assumed to be isotropic in the laboratory system.

MF=5 Energy Distributions of Secondary Neutrons

MT=16,17,91

Evaporation spectra were given.

MT=18

Fission spectrum was estimated from $Z^{2/A}$ systematics of Smith et al. /8/.

References

- 1) Ohsawa T. and Ohta M.: Memoirs Faculty of Engineering, Kyushu Univ. 40, 149 (1980).
- 2) Howerton R.J.: Nucl. Sci. Eng. 62, 438 (1977).
- 3) Ohsawa T. and Ohta M.: J. Nucl. Sci. Technol. 18, 408 (1981).
- 4) Igarasi S.: ibid. 12, 67 (1975).
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- 8) Smith A.B. et al.: ANL-NDM 50 (1979).

91-Pa-233 MAT number = 2911

91-Pa-233 Kyushu u. Eval-Mar76 Y.Kanda, JENDL-CG
Dist-Mar83 Rev1-Jan84

History

- 76-03 The evaluation of Drake and Nichols /1/ was recommended by Kanda (Kyushu univ.) for JENDL-1. JENDL-1 compilation group made partly recalculation with optical and statis-model.
- 83-03 JENDL-1 data were adopted for JENDL-2 and extended to 20 MeV. MF=5 was revised.
- 84-01 Small modification. Comment data were added.

MF=1 General Information

- MT=451 Descriptive data and dictionary
MT=452 Number of neutrons per fission
Taken from Drake and Nichols /1/, and extended to 20 MeV.

MF=2 Resonance Parameters

- MT=151 Resolved and unresolved resonance parameters
Resolved resonances for SLBW formula : from 2.38 to 17 eV.
Taken from the evaluation of Drake and Nichols based on the data by Simpson and Coddig /2/.
- Unresolved resonances : from 17 eV to 1 keV.
Taken from the evaluation of Drake and Nichols.

2200-m/sec cross sections and calculated resonance integrals.

	2200 m/sec	res. integ.
elastic	11.02 b	-
capture	42.80 b	779. b
fission	0.0 b	4.68 b
total	53.82 b	-

MF=3 Neutron Cross Sections

Below 2.38 eV.

The evaluation of Drake and Nichols was adopted. The cross sections are calculated values from resonance parameters in MF=2.

Between 2.38 eV to 1 keV.

Background cross sections of zero were given.

Above 1 keV.

MT=1 Total

The sum of partial cross sections

MT=2 Elastic scattering

Taken from Drake and Nichols' evaluation.

MT=4.51-66,91 Inelastic scattering

Calculated with CASTHY /3/. The fission, (n,2n), and (n,3n) were considered as competing processes. The optical potential parameters determined by Igarasi /4/ were adopted.

$$V_0 = 40.5 + 0.5 \cdot E_n \quad (\text{MeV})$$

$$W_s = 8.2 + 0.5 \cdot \text{SQRT}(E_n) \quad (\text{MeV})$$

$$W_{so} = 7.0 \quad (\text{MeV})$$

$$r_0 = r_s = r_{so} = 1.32 \quad (\text{fm})$$

$$a_0 = a_s = a_{s0} = 0.47 \quad (\text{fm})$$

The level scheme used in the calculation is as follows.

No.	Energy (MeV)	Spin-Parity
g.s.	0.0	3/2 -
1	0.0067	1/2 -
2	0.0571	7/2 -
3	0.0710	5/2 -
4	0.0865	5/2 +
5	0.0947	3/2 +
6	0.1037	7/2 +
7	0.1090	9/2 +
8	0.1633	11/2 -
9	0.1692	1/2 +
10	0.1800	9/2 -
11	0.2017	3/2 +
12	0.2123	5/2 +
13	0.2379	5/2 +
14	0.2796	7/2 +
15	0.3004	7/2 +
16	0.3662	9/2 +

Continuum levels were assumed above 400 keV.

MT=16,17 (n,2n) and (n,3n)

Calculated with Pearlstein's method /5/.

MT=18 Fission

Taken from Drake and Nichols. The cross section was obtained by drawing a smooth curve through the experimental data /6,7/ for the range from 0.1 to 3 MeV. Above 3 MeV, it was assumed to have the same shape as similar nuclei.

MT=102 Capture

Taken from Drake and Nichols. They calculated the capture cross section from the unresolved resonance parameters.

MT=251 Mu-bar

Calculated with CASTHY /3/.

MF=4 Angular Distributions of Secondary Neutrons

MT=2 Calculated with CASTHY code /3/.

MT=51-66 Isotropic in the center-of-mass system.

MT=16,17,18,91 Isotropic in the laboratory system.

MF=5 Energy Distributions of Secondary Neutrons

MT=16,17,91 Evaporation spectrum.

MT=18 Maxwellian fission spectrum estimated from Z^2/A systematics /8/.

References

- 1) Drake N.K. and Nichols P.F.: GA-7462 (1967).
- 2) Simpson F.B. and Coddling J.W.Jr: Nucl. Sci. Eng., 28, 133 (1967).
- 3) Igarasi S.: J. Nucl. Sci. Technol., 12, 67 (1975).
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- 8) Smith A.B. et al.: ANL/NDM-50 (1979).

92-U -233 MAT number = 2921

92-U -233 SAEI+ Eval-Jun82 N.Asano,H.Matsunobu,Y.Kikuchi
 NST 19 1037 Dist-Mar83 Rev1-Nov83
 82-06 New evaluation for JENDL-2 by N.Asano, H.Matsunobu (SAEI)
 and Y.Kikuchi (JAERI).
 83-11 Comment was added.

MF=1 General Information

MT=451 Comments and dictionary

MT=452 Nu-total

Sum of Nu-d and Nu-p

MT=454 Fission yield data

Taken from ENDF/B-IV.

MT=455 Nu-d

Below 4 MeV

$$\text{Nu-d} = 0.007549 + 4.627\text{E-5} \cdot \ln(\text{E}(\text{MeV}))$$

Between 4 and 20 MeV

Based on the data of Masters et al. /1/ and Evans et al.

/2/.

MT=456 Nu-p

Renormalization was made to 3.756 of Cf-242.

Below 1 MeV

$$\text{Nu-p} = 2.486 + 0.121 \cdot (\text{E-DE}),$$

where DE is difference of average fragment kinetic energy
 between incident and thermal neutron energies. It was
 taken from data of Boldeman et al. /3/.

Between 1 and 2.73 MeV

$$\text{Nu-p} = 2.436 + 0.1279 \cdot \text{E}$$

Between 2.73 and 7.47 MeV

$$\text{Nu-p} = 2.327 + 0.1678 \cdot \text{E}$$

Above 7.47 MeV

$$\text{Nu-p} = 2.857 + 0.09689 \cdot \text{E}$$

MF=2 Resonance Parameters

MT=151

a) Resolved resonance region (1 eV to 100 eV)

Resolved resonance parameters for the single-level Breit-

Wigner formula based on the data of Nizamuddin and Blons

/4/.

b) Unresolved resonance region (0.1 keV to 30 keV)

Resonance parameters were deduced with ASREP code /5/ so as
 to reproduce the evaluated cross sections in this energy
 region.

MF=3 Neutron Cross Sections

a) Thermal energy region (below 1.0 eV)

MT=1 Total

Sum of partial cross sections

MT=2 Elastic scattering

Calculated from resolved resonance parameters by using the
 effective scattering radius of 9.93 fm.

MT=18 Fission

Based on data of Weston et al. /6/, Cao et al. /7/,
Deruytter and Wagemans /8/ and Pshenichny et al. /9/.
MT=102 Capture
Based on the data of Weston et al. /6/.

	2200 m/s	Res. Integ.
elastic	12.70 b	-
capture	45.30 b	139 b
fission	529.9 b	772 b
total	587.9 b	-

b) Resonance Region (from 1 eV to 30 keV)
Represented with resolved and unresolved resonance parameters. Background cross section was given for the total and fission cross sections in the resolved resonance region.

c) Smooth part (above 30 keV)

MT=1 Total

Based on the data of Poenitz /10/, Green and Mitchell /11/, Foster and Glasgow /12/. Between 10 and 50 keV, and above 15 MeV, optical model calculation was applied by using the following optical potential parameters.

$$V = 41.8 - 0.20 \cdot E + 0.008 \cdot E^2, \quad W_s = 6.50 - 0.15 \cdot E, \quad V_{so} = 6.0 \text{ (MeV)}$$

$$r_0 = 1.31, \quad rs = 1.36, \quad r_{so} = 1.32 \text{ (fm)}$$

$$a_0 = 0.57, \quad b = 0.44, \quad a_{so} = 0.50 \text{ (fm)}$$

MT=2 Elastic

Obtained by subtracting non-elastic scattering cross section from the total cross section.

MT=4 and 51-64,91 Inelastic scattering

Based on optical and statistical model calculation.
Level scheme taken from Ref. /13/ was as follows,

No.	Energy (MeV)	Spin-Parity
g.s.	0.0	5/2 +
1	0.04035	7/2 +
2	0.0922	9/2 +
3	0.1551	11/2 +
4	0.29882	5/2 -
5	0.31191	3/2 +
6	0.3208	7/2 -
7	0.34047	5/2 +
8	0.3537	9/2 -
9	0.397	11/2 -
10	0.39849	1/2 +
11	0.41576	3/2 +
12	0.5039	7/2 -
13	0.5467	5/2 +
14	0.5971	7/2 +

Above 0.6 MeV, assumed to be overlapped.

MT=16,17 (n,2n) and (n,3n)

Calculated by Pearlstein's method /14/ and normalized to fission-spectrum-averaged value by Kobayashi /15/.

MT=18 Fission

Based on data of Blons /16/, Gwin et al. /17/, Poenitz /18/ and Alkhazov et al. /19/. For cross section shape, based on ratio data of Carlson and Behrens /20/ and Shpak and

Smirenkin /21/.

MT=102 Capture

Based on statistical and optical model calculations, and normalized to the data of Hopkins and Diven /22/.

MT=251 Mu-bar

Based on optical model calculation.

MF=4 Angular Distributions of Secondary Neutrons

MT=2

Based on optical model calculation.

MT=51-64

Assumed to be isotropic in the center-of-mass system.

MT=16,17,18 and 91

Assumed to be isotropic in the lab system.

MF=5 Energy Distributions of Secondary Neutrons

MT=16,17,91 Evaporation spectrum.

MT=18 Maxwellian at temp. of 1.338 MeV estimated from

Z=2 A systematics of Smith et al. /23/.

MT=455 Taken from ENDF/B-IV.

References

- 1) Master C.F. et al.: Nucl. Sci. Eng., 36, 202 (1969).
- 2) Evans A.E. et al.: Nucl. Sci. Eng., 50, 80 (1973).
- 3) Boldeman J.W. et al.: Nucl. Phys., A265, 337 (1976).
- 4) Nizamuddin S. and Blons J.: Nucl. Sci. Eng., 54, 116 (1974).
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- 11) Green L. and Mitchell J.A.: WAPD-TM-1073 (1973).
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- 17) Gwin R. et al.: Nucl. Sci. Eng., 59, 79 (1976).
- 18) Poenitz W.P.: ANL/NDM-36 (1978).
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- 21) Shpak D.L. and Smirenkin G.N.: Sov. J. Nucl. Phys., 21, 363 (1975).
- 22) Hopkins J.C. and Diven B.C.: Nucl. Sci. Eng., 12, 169 (1962).
- 23) Smith A.B. et al.: ANL/NDM-50 (1979).

92-U -234 MAT number = 2922

92-U -234 JAERI Eval-Mar76 T.Asami
Dist-Mar83 Rev1-Jan84

History

76-03 The evaluation was made by T.Asami (JAERI) for JENDL-1 /1/.
83-03 JENDL-1 data were adopted for JENDL-2 and extended to 20 MeV.
84-01 Resonance formula was changed. MT=5 and comment data were added.

MF=1 General Information

MT=451 Descriptive data and dictionary
MT=452 Number of neutrons per fission
Taken from ENDF/B-IV evaluation.

MF=2 Resonance Parameters

MT=151 Resolved resonance parameters for MLBW formula
Energy range : 1.0E-5 eV to 215.0 eV.
Parameters were adopted from James and Slaughter /2/. A bound level at -1.6777 eV was taken from Drake and Nichols /3/ to reproduce the thermal cross section.

Calculated 2200-m/sec cross sections and resonance integrals.

	2200 m/sec	res. integ.
elastic	14.72 b	-
capture	95.44 b	609. b
fission	0.006367 b	6.44 b
total	110.2 b	-

MF=3 Neutron Cross Sections

Below 215 eV: Background cross sections of zero.
Above 215 eV:

MT=1,2,4,51-63,91,102 Total, Elastic, Inelastic and Capture
Calculated with statistical and optical model code CASTHY /4/. Potential parameters were taken from Agee and Rosen /5/.

$V = 40.5 + 0.5 \cdot E_n$, $W_s = 8.2$, $V_{so} = 7.0$ (MeV)
 $r = 1.32$, $r_s = 1.32$, $r_{so} = 1.32$ (fm)
 $a_0 = 0.47$, $a_s = 0.47$, $a_{so} = 0.47$ (fm)

The level scheme used was as follows.

No.	Energy (MeV)	Spin-Parity
g.s.	0.0	0 +
1	0.044	2 +
2	0.144	4 +
3	0.297	6 +
4	0.499	8 +
5	0.790	1 -
6	0.811	0 +
7	0.8496	3 -
8	0.8516	2 +
9	0.9269	2 +
10	0.948	4 +

11	0.965	3 +
12	1.023	3 -
13	1.046	0 +

Levels above 1.06 MeV were assumed to be overlapping. The fission, (n,2n) and (n,3n) cross sections were used as the cross sections of competing processes. The parameters D-obs of 12.3 eV and average radiative width of 0.025 eV were adopted to normalize the gamma-ray transmission coefficients.

MT=16,17 (n,2n) and (n,3n)

Calculated with Pearlstein's method /6/.

MT=18,19,20,21 Fission

The evaluated data by Drake and Nichols /3/ were adopted from 215 eV to 2 MeV. Above 2 MeV, the cross section calculated by Jary /7/ was adopted.

MT=251 Mu-bar

Calculated with CASTHY /4/.

MF=4 Angular Distributions of Secondary Neutrons

MT=2 Calculated with CASTHY code /4/.

MT=51-63 Isotropic in the center-of-mass system.

MT=16,17,18,19,20,21,91 Isotropic in the laboratory system.

MF=5 Energy Distributions of Secondary Neutrons

MT=16,17,91 Evaporation spectrum.

MT=18,19,20,21 Maxwellian fission spectrum taken from ENDF/B-IV.

References

- 1) Igarasi S. et al.: JAERI 1261 (1979).
- 2) James G.D. and Slaughter G.G.: Nucl. Phys., A139, 471 (1969).
- 3) Drake N.K. and Nichols P.F.: GA-8135 (1967).
- 4) Igarasi S.: J. Nucl. Sci. Technol., 12, 67 (1975).
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92-U -235 MAT number = 2923

92-U -235 SAEI+ Eval-Sep79 H.Matsunobu,A.Asami,Y.Kikuchi
 79Knoxville,715 Dist-Mar83 Rev1-Nov83

History

79-09 Newly evaluated for JENDL-2 by the following evaluaters.
 A.Asami (High Energy R.I.) Resolved resonance parameters
 Y.Kikuchi (JAERI) Unresolved resonance parameters
 H.Matsunobu (SAEI) other quantities
 83-11 Comment was added.

MF=1 General Information

MT=451 Comments and dictionary
 MT=452 Total number of neutrons per fission
 Sum of nu-p (MT=453) and nu-d (MT=455).
 MT=454 Fission product yield data
 taken from ENDF/B-IV.
 MT=455 Delayed neutron data
 Adopted the evaluated data by Schatz /2/.
 MT=456 Number of prompt neutrons
 Evaluated on the basis of the experimental data by Boldeman
 and Walsh /3/, Soleilhac et al. /4/, Frehaut et al. /5,6/,
 Meadows and Whalen /7/, Prokhorova et al. /8,9/ and Savin
 et al. /10/.

MF=2 Resonance Parameters

MT=151

- 1) Resolved resonances : 1.0 - 100 eV
 $2g+\text{Gamma-n}$: Simple average of experimental data.
 Gamma-g : Weighted average of experimental data.
 Gamma-f : Calculated from the averaged fission area.
 Details of the evaluation given in Ref. /11/.
- 2) Unresolved resonance parameters : 100 eV - 30 keV
 The evaluated total, capture and fission cross sections
 were fitted by adjusting S0, S1 and Gamma-f .
 Fixed parameters : R= 9.9 fm, Gamma-g = 45 milli-eV,
 Dobs= 0.567 eV.

2200-m/s cross sections and calculated res. integrals.

	2200 m/s	res. integ.
elastic	17.0 b	-
fission	584.0 b	279 b
capture	96.0 b	153 b
total	697.0 b	-

MF=3 Neutron Cross Sections

Below 1.0 eV: Based on the experimental data.

Between 1.0 and 100 eV: Background data for resonance parameters are given to well reproduce the experimental data.

Above 100 eV: Data were evaluated as follows. Between 100 eV and 30 keV, the unresolved resonance parameters and the background data were given to reproduce

these cross sections.

MT=1 Total

Evaluated on the basis of the experimental data by Uttley et al. /12/, Boeckhoff et al. /13/, Schwartz et al. /14/, Green et al. /15/ and Foster and Glasgow /16/.

MT=2 Elastic scattering

Evaluated on the basis of the experimental data by Smith /17/, Smith and Whalen /18/ and Knitter et al. /19/ in the energy range from 0.3 to 2.3 MeV. In the remaining energy range it was derived by subtracting sum of partial cross sections from total cross section.

MT=4,51-79,91,251 Inelastic scattering cross section and mu-bar

Evaluated on the basis of experimental data and calculation with optical and statistical models.

The optical potential parameters were obtained by fitting the experimental data of the total cross section.

$$\begin{aligned} V &= 40.90 - 0.04 \cdot E_n \quad (\text{MeV}) \\ W_s &= 6.50 + 0.25 \cdot E_n \quad (\text{MeV}) \\ v_{so} &= 7.0 \quad (\text{meV}) \\ r_0 &= 1.312, \quad r_s = 1.375, \quad r_o = 1.320 \quad (\text{fm}) \\ a &= 0.490, \quad b = 0.454, \quad a_o = 0.470 \quad (\text{fm}) \end{aligned}$$

Statistical model calculation with CASTHY code /20/.

Competing processes : fission (n,2n), (n,3n), (n,4n).
Level fluctuation was considered.

The level scheme taken from Ref. /21/.

No.	Energy (keV)	Spin-Parity
g.s.	0.0	7/2 -
1	0.075	1/2 +
2	13.038	3/2 +
3	46.347	9/2 -
4	51.697	5/2 +
5	81.732	7/2 +
6	103.1	11/2 -
7	129.292	5/2 +
8	150.6	9/2 +
9	170.7	13/2 -
10	171.378	7/2 +
11	197.1	11/2 +
12	225.40	9/2 +
13	249.1	15/2 -
14	291.1	11/2 +
15	294.7	13/2 +
16	332.818	5/2 +
17	338.8	17/2 -
18	357.2	15/2 +
19	367.05	7/2 +
20	368.8	13/2 +
21	393.184	3/2 +
22	412.3	9/2 +
23	426.71	5/2 +
24	438.5	19/2 -
25	445.72	7/2 +
26	474.27	7/2 +

27	510.0	9/2 +
28	532.0	9/2 +
29	550.4	21/2 -

Continuum levels assumed above 580 keV.

The level density parameters : Gilbert and Cameron /22/.

MT=16,17,37 (n,2n), (n,3n), (n,4n)

Evaluated on the basis of the following experimental data and calculation with evaporation model.

(n,2n) : Mather et al. /23/

(n,3n) and (n,4n) : Veesser and Arthur /24/

MT=18 Fission

Evaluated on the basis of the following experimental data:

100 eV - 10 keV : Perez et al. /25,26/

10 keV - 1 MeV : Szabo and Marquette /27/, Poenitz /28,29/, White /30/

1 MeV - 20 MeV : Szabo and Marquette /27/, Barton et al. /31/, Poenitz /29/, Czirr and Sidhu /32,33/, Cance and Grenier /34/

A special care was paid for evaluating the fission cross section of U-235 so that the consistency could be kept between the relative and absolute measurements for the other heavy nuclides.

MT=102 Capture

Derived from the evaluated alpha value and fission cross section below 1 MeV. Calculated with the statistical model above 1 MeV.

Alpha value was evaluated on the basis of the experimental data by Kononov et al. /35/, Dvukhshestnov et al. /36/, Gwin et al. /37/, Bluhm and Yen /38/ and Hopkins and Diven /39/.

MF=4 Angular Distributions of Secondary Neutrons

MT=2 Calculated with optical model.

MT=51-79 Isotropic in the center-of-mass system.

MT=16,17,18,37,91 Isotropic in the lab system.

MF=5 Energy Distributions of Secondary Neutrons

MT=16,17,37,91 Evaporation spectrum

MT=18,455 Taken from ENDF/B-IV.

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92-U -236 MAT number = 2924

92-U -236 NAIG Eval-Mar79 T.Yoshida
Dist-Mar83 Rev1-Dec83

History

79-03 New evaluation for JENDL-2 was made by T.Yoshida (NAIG).
83-03 MF=1 and MF=5 were added by Y.Kikuchi (JAERI).
83-12 MF=1, MT=451 was added.

MF=1 General Information

MT=451 Descriptive data and dictionary
MT=452 Number of neutrons per fission
Taken from ENDF/B-IV.

MF=2 MT=151 Resonance parameters

Resolved resonances for MLBW formula : $1.0E-5$ eV to 1.5 keV
Res. energies and Γ_n (for Γ_n greater than $0.1 \times \Gamma_g$)
: Carraro /1/
 Γ_n (for Γ_n smaller than $0.1 \times \Gamma_g$) : Mewissen /2/
 Γ_g : Mewissen /2/, when not given average value was taken.
 Γ_f : Theobald /3/.

Average Γ_g = 23.0 milli-eVAverage Γ_f = 0.354 milli-eV

A negative resonance was introduced to reproduce the 2200-m/s capture cross section of (5.2 ± 0.3) barns recommended in BNL-325 3rd edition.

Calculated 2200-m/s cross sections and res. integrals

	2200-m/sec	Res. Integ.
elastic	8.337 b	-
fission	0.043 b	7.61 b
capture	5.295 b	347. b
total	13.67 b	-

MF=3 Neutron Cross Sections

Below 1.5 keV, all background cross sections are zero.
Above 1.5 keV, data were evaluated as follows.

MT=1,2,4,51-79,91,102,251 Sig-t, Sig-el, Sig-in, Sig-c, Mu-bar
Calculated with optical and statistical models.

The spherical optical potential parameters /4/ :

 $V=40.8 - 0.05 \times E_n$, $W_s=0.5 + 0.15 \times E_n$, $V_{so}=7.0$ (MeV), $r=1.32$, $r_s=1.38$, $r_{so}=1.32$ (fm), $a=as=aso=0.47$ (fm).

Optical and statistical model calculation was made with
CASTHY code /5/.

Competing processes : fission, $(n,2n)$ and $(n,3n)$

Level fluctuation was considered. The gamma-ray strength
function was determined so that the calculated capture
cross section reproduced the measured value of 1.05 barns
/6/ around 10 keV.

The level scheme taken from Ref. /7/.

No.	Energy (MeV)	J-Parity	No.	Energy (MeV)	J-Parity

2 of Uranium-236

gs	0.0	0 +	1	0.04524	2 +
2	0.14948	4 +	3	0.30979	6 +
4	0.52225	8 +	5	0.68757	1 -
6	0.7442	3 -	7	0.7828	10 +
8	0.8476	5 -	9	0.91916	0 +
10	0.9581	2 +	11	0.9604	2 +
12	0.9670	1 -	13	0.9880	2 -
14	1.0014	3 +	15	1.0020	7 -
16	1.0356	3 -	17	1.0512	4 +
18	1.0529	4 -	19	1.0587	4 +
20	1.0661	3 +	21	1.0700	4 -
22	1.0862	12 +	23	1.0938	2 +
24	1.1044	5 -	25	1.1110	2 -
26	1.1267	5 +	27	1.1470	3 +
28	1.1494	3 -	29	1.1640	6 -

Continuum levels assumed above 1.17 MeV.

MF=16,17 (n,2n) and (n,3n)

Calculated with the Pearlstein's method /8/.

MT=18 Fission

Evaluated on the basis of measured data of U-236/U-235 /9,10/. To get absolute value Matsunobu's evaluation /11/ for U-235(n,f) was employed.

MF=4 Angular Distributions of Secondary Neutrons

MT=2 Calculated with optical model.

MT=51-79 Isotropic in the center-of-mass system.

MT=16-18,91 Isotropic in the laboratory system.

MF=5 Energy Distributions of Secondary Neutrons

MT=16,17,91 Evaporation spectrum.

MT=18 Maxwellian fission spectrum. Temperature was estimated from $Z+2/A$ values /12/.

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92-U -238 MAT number = 2925

92-U -238 Kyushu U.+ Eval-Aug79 Y.Kanda,T.Nakagawa,Y.Kikuchi
Dist-Mar83 Rev1-Jan84

History

79-08 Evaluation was made by
T.Nakagawa (JAERI) for resonance parameters and background
cross sections,
Y.Kikuchi (JAERI) for unresolved resonance parameters,
Y.Kanda (Kyushu Univ.) for cross sections above resonance
region and other quantities.
83-03 MF=5 was revised.
84-01 Comment data were added.

MF=1 General Information

MT=451 Descriptive data and dictionary

The following four MTs' data were entirely taken from ENDF/B-IV
evaluation.

MT=452 Number of neutrons per fission
MT=454 Fission product yields
MT=455 Delayed neutron data
MT=456 Number of prompt neutrons per fission

MF=2 Resonance parameters

MT=151 Resolved and unresolved resonance parameters
Resolved resonances for MLBW formula : from $1.0E-5$ eV to 4 keV.
Reference /1/ gives an outline of the present evaluation.
Resonance energies : Evaluated on the basis of the experimen-
tal data by Poortmans et al. /2/, Olsen et al. /3,4/ and
Nakajima /5/. Four negative resonances were added to
consider interference effects in the low energy region.
Neutron and capture widths : Obtained from resonance areas
calculated from various measurements by giving relatively
high weight to the recent data /2-8/.
Sub-threshold fission widths : Determined from the fission
resonance areas measured by Diffilippo et al. /9/ for 28
s-wave resonances.
Effective scattering radius : 9.48 fm obtained by averaging
the values of Olsen et al. below 2.2 keV.
Unresolved resonances : from 4 keV to 50 keV.
The energy dependent parameters were determined to reproduce
cross sections evaluated by Kanda (see the description of
MF=3).

2200-m/sec cross sections and calculated resonance integrals.

	2200 m/sec	res. integ.
elastic	8.873 b	-
capture	2.700 b	279. b
fission	$3.22E-6$ b	2.05 b
total	11.57 b	-

MF=3 Neutron Cross Sections

Below 4.0 keV: Background data for resolved resonances.

The background cross sections were obtained with the picket-fence model. The contributions from missed p-wave resonances were also taken into account for the capture cross section in the energy region above 1.5 keV.

Above 4 keV.

Evaluated cross sections were replaced with unresolved resonance parameters and background cross sections in the energy region between 4 keV and 50 keV.

MT=1 Total

Evaluated from the following experimental data.

Below 500 keV: Uttley et al. /10/, Whalen et al. /11/.

0.5 - 4.5 MeV: Kopsch et al. /12/.

4.5 - 15 MeV: Foster and Glasgow /13/.

15 - 20 MeV: Bratenahl et al. /14/, Peterson et al. /15/.

MT=2 Elastic scattering

Calculated as (total) - (partial cross sections).

MT=4 Total inelastic

Evaluated by Kanda.

MT=51-75,91 Inelastic scattering

Calculated as follows by using the presently evaluated total inelastic and partial inelastic scattering cross sections of JENDL-1.

$\text{Sig}(i\text{-th level}) = \text{Sig}(\text{inel.}) * (\text{branching ratio to } i\text{-th level})$
where the branching ratio to the i -th level was calculated from JENDL-1 data /16/.

The level scheme.

No.	Energy (MeV)	Spin-Parity
g.s.	0.0	0 +
1	0.0447	2 +
2	0.148	4 +
3	0.301	6 +
4	0.520	8 +
5	0.680	1 -
6	0.732	3 -
7	0.790	10 +
8	0.838	5 -
9	0.939	2 +
10	0.968	2 +
11	1.006	0 +
12	1.047	2 +
13	1.076	2 +
14	1.100	12 +
15	1.123	1 -
16	1.150	2 -
17	1.190	3 -
18	1.210	2 +
19	1.246	4 -
20	1.272	5 -
21	1.313	2 +
22	1.361	2 +
23	1.401	2 +
24	1.437	14 +
25	1.470	1 -

Continuum levels were assumed above 1.5 MeV.

MT=16,17 (n,2n) and (n,3n)

Calculated with the evaporation model of Segev and Caner /17/, and normalized to the data by Frehaut and Mosinski /18/.

MT=18 Fission

Evaluated on the basis of the data of Diffilippo et al. /19/, Behrens and Carlson /20/, Nordborg et al. /21/ and Meadows /22,23/. They were renormalized with the U-235 fission cross section evaluated by Matsunobu /24/.

MT=102 Capture

Determined mainly from the measurements by Poenitz /25/, Panitkin and Sherman /26/, Moxon /27/, Fricke et al. /28/ and Menlove and Poenitz /29/.

MT=251 Mu-bar

Taken from JENDL-1 /16/.

MF=4 Angular Distributions of Secondary Neutrons

MT=2 Taken from JENDL-1 /16/.

MT=51,52 Taken from JENDL-1 /16/.

MT=53-75 Isotropic in the center-of-mass system.

MT=16,17,18,91 Isotropic in the laboratory system.

MF=5 Energy Distributions of Secondary Neutrons

MT=16,17,91 Evaporation spectrum.

MT=18 Maxwellian fission spectrum estimated from $Z^{2/3}/A$ systematics /30/.

MT=455 Taken from ENDF/B-IV.

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93-Np-237 MAT number = 2931

93-Np-237 Kyushu U. + Eval-Mar79 N.Wachi, Y.Kanda, Y.Kikuchi
Dist-Mar83 Rev1-Nov83

History

79-03 New evaluation was made by N.Wachi and Y.Kanda (Kyushu University), and Y.Kikuchi (JAERI).

83-11 Comment was added.

MF=1 General Information

MT=451 Comments and dictionary
MT=452 Number of neutrons per fission
Experimental data of Frehaut + /1/.
MT=455 Delayed neutron data
Experimental data of Benedetti - /2/ and systematics
by Tuttle /3/.

MF=2, MT=151 Resonance parameters

Resolved resonances for SLBW formula : $1.0E-5 - 130$ eV

Res. energy, Γ_n , Γ_g : Weston and Todd /4/.

Γ_f : Plattard + /5/.

Average $\Gamma_g = 40$ milli-eV.

A negative resonance added.

Unresolved resonances : 130 eV - 30 keV

Parameters by Weston and Todd /4/ with slight modification

Adopted parameters :

$S_0 = 1.02E-4$, $S_1 = 1.888E-4$, $D_{\text{obs}} = 0.45$ eV

$\Gamma_g = 40$ milli-eV.

Γ_f values determined so that $\text{Sig-f} = 0.009$ b.

Calculated 2200 m/s cross sections and resonance integrals:

	2200 m/s value	Res.Int.
total :	208.5 b	-
elastic :	27.52 b	-
fission :	0.01921 b	6.26 b
capture :	181.0 b	663 b

MF=3 Neutron Cross Sections

MT=1,2,4,51-64,91,102,251 Sig-t, Sig-el, Sig-in, Sig-c, Mu-bar

Calculated with optical and statistical models.

The spherical optical potential parameters :

$V = 43.55$, $W_s = 11.0$, $V_{s0} = 7.0$ (MeV)

$r = r_s = 1.32$, $r_{s0} = 1.3$ (fm)

$a = b = 0.47$, $a_{s0} = 0.4$ (fm).

Statistical model calculation with CASTHY code /6/.

Competing processes : fission, (n,2n) and (n,3n).

Level fluctuation considered.

The gamma-ray strength function determined so that

$\text{Sig-c} = 0.742$ b at 200 keV.

The level scheme taken from compilation by Ellis /7/.

No	Energy (MeV)	Spin-Parity
g.s.	0.0	5/2+
1	0.03320	7/2+

2 of Neptunium-237

2	0.05954	5/2-
3	0.07580	9/2+
4	0.10296	7/2-
5	0.13000	11/2+
6	0.15852	9/2-
7	0.2260	11/2-
8	0.26754	3/2-
9	0.281	1/2-
10	0.305	13/2-
11	0.327	7/2-
12	0.332	1/2+
13	0.357	5/2-
14	0.369	5/2+

Continuum levels assumed above 0.370 MeV.

The level density parameters of Gilbert and Cameron /8/.

MT=16,17 (n,2n), (n,3n)

Calculated with the evaporation model by Segev + /9/.

MT=18 fission

Evaluated from measured data.

Verified by calculating spectrum-averaged cross section.

MF=4 Angular Distributions of Secondary Neutrons

MT=2,51-64,91 Calculated with the optical model.

MT=16,17,18 Isotropic in the laboratory system.

MF=5 Energy Distributions of Secondary Neutrons

MT=16,17,91 Evaporation spectrum.

MT=18 Estimated from Z^{*2}/A systematics by Smith +/10/
by assuming $E(\text{Cf-252}) = 2.13$ MeV.

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93-Np-239 MAT number = 2932

93-Np-239 Kyushu U.+ Eval-Mar76 Y.Kanda, JENDL-CG
Dist-Mar83 Rev1-Jan84

History

76-03 The evaluation for JENDL-1 was performed by Kanda (Kyushu Univ.) and JENDL-1 Compilation Group. Details are given in Ref. /1/.

83-03 JENDL-1 data were adopted for JENDL-2 and extended to 20 MeV. MF=5 was revised.

84-01 Comment data were added.

MF=1 General Information

MT=451 Descriptive data and dictionary

MT=452 Number of neutrons per fission

Taken from the Np-237 data of ENDF/B-IV.

MF=2 Resonance Parameters

MT=151 No resonance parameters were given.

2200-m/sec cross sections and calculated resonance integrals.

	2200 m/sec	res. integ.
elastic	10.50 b	-
capture	37.00 b	445. b
fission	0.0 b	7.06 b
total	47.50 b	-

MF=3 Neutron Cross Sections

Below 4.0 eV.

MT=1 Total

Sum of partial cross sections.

MT=2 Elastic scattering

The constant cross section of 10.5 barns was assumed from
 $\text{Sig} = 4 * 3.14 * (0.147 * A^{1/3})^{*2}$.

MT=18 Fission

Assumed to be zero barns.

MT=102 Capture

The form of $1/v$ was assumed. The 2200-m/sec cross section was adopted from the experimental data by Stoughton and Halperin /2/.

Above 4.0 eV.

MT=1 Total

Calculated with optical and statistical model code CASTHY /3/. Optical potential parameters were obtained by Ohta and Miyamoto /4/ by using the total cross section of Pu-239.

$V = 45.87 - 0.2 * \ln W$, $W_i = 0.06$, $W_s = 14.1$, $V_{so} = 7.3$ (MeV)

$r = 1.27$, $r_i = 1.27$, $r_s = 1.302$, $r_{so} = 1.27$ (fm)

$a_0 = 0.652$, $a_i = 0.315$, $a_s = 0.98$, $a_{so} = 0.652$ (fm)

MT=2 Elastic scattering

Calculated with CASTHY /3/.

MT=4.51 58.91 Inelastic scattering

Calculated with CASTHY /3/. The level scheme was adopted from Nucl. Data Sheets Vol.6.

No.	Energy (MeV)	Spin-Parity
g.s.	0.0	5/2 +
1	0.03114	7/2 +
2	0.07112	9/2 +
3	0.07467	5/2 -
4	0.11766	11/2 +
5	0.1230	7/2 -
6	0.17305	9/2 -
7	0.2414	11/2 -
8	0.320	13/2 -

Levels above 430 keV were assumed to overlapping. In the calculation the capture, fission, (n,2n) and (n,3n) cross sections were considered as competing processes.

MT=16,17 (n,2n) and (n,3n)

Calculated with Pearlstein's method /5/.

MT=18 Fission

Estimated from the Np-237 fission cross section by normalizing with neutron separation energies.

MT=102 Capture

Below 100 keV, the cross section was calculated from

$\text{Sig} = 435 / \text{SQRT}(E_n)$ barns.

Above 100 keV, the shape of the experimental data for Np-237 by Nagle et al. /6/ was adopted and normalized to 1.4 barns at 100 keV.

MT=251 Mu-bar

Calculated with CASTHY /3/.

MF=4 Angular Distributions of Secondary Neutrons

MT=2 Calculated with CASTHY code /3/.

MT=51-58 Isotropic in the center-of-mass system.

MT=16,17,18,91 Isotropic in the laboratory system.

MF=5 Energy Distributions of Secondary Neutrons

MT=16,17,91 Evaporation spectrum.

MT=18 Maxwellian fission spectrum estimated from Z^2/A systematics /7/.

References

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94-Pu-236 MAT number = 2941

94-Pu-236 FBEC Eval-Apr79 T.Hojuyama
Dist-Mar83 Rev1-Nov83

History

79-04 New evaluation was made by T. Hojuyama (FBEC) /1/ in the energy range from 1.0E-5 eV to 20 MeV.
83-11 Comment was added.

MF=1 General Information

MT=451 Comment and dictionary

MT=452 Number of neutrons per fission

Nu-p and Nu-d for thermal neutron based on Manero's semi-empirical formula /2/. Neutron-energy dependence of Nu based on Howerton's evaluation /3/.

MF=2 Resonance Parameters

MT=151 Resolved resonance (one resonance)

Energy range from 1.0E-5 to 6 eV. Gam-f was so determined that Sig-f calculated from the unresolved resonance formula with the Gam-f may smoothly connect at 10 keV to Sig-f in the high energy region. Gam-g, S0, S1, <D> and R were estimated from systematics. E0 was so determined that the fission rate calculated with the resonance parameters in a thermal reactor may agree with exp. data /6/.

---Resonance Parameters---

E0	:	0.445 eV	/6/
Gam-n	:	0.526 milli-eV	(from S0 and <D>)
Gam-f	:	3.55 milli-eV	see above
Gam-g	:	41.5 milli-eV	/4/
R	:	9.46 fm	see above
<D>	:	6.3 eV	/4/
S0	:	1.25E-4	/4.5/
S1	:	2.22E-4	/5/

Calculated 2200-m/s cross sections and resonance integrals.

	2200 m/sec	Res. Integ.
elastic	3.376 b	-
fission	65.41 b	101 b
capture	764.6 b	1067 b
total	833.4 b	-

MF=3 Neutron Cross Sections

MT= 1 Total cross section

Obtained by optical model calculation. Optical potential parameters taken from Murata's evaluation /7/ except real potential.

---Optical Potential Parameters---

V	=	39.5-0.05*En	(MeV)
Ws	=	6.5+0.15*En	(MeV)
Vso	=	7.0	(MeV)
r0	=	rso= 1.32 , rs = 1.38	(fm)
a	=	aso= 0.47 , b = 0.47	(fm)

MT= 2 Elastic scattering cross section
Obtained by optical and statistical model calculations.

MT=4,51-54,91 Inelastic scattering cross sections
Obtained by optical and statistical model calculations.
Level scheme taken from N.D.S. /8/ except 4th level of
which energy based on Lynn /9/.

No.	En (keV)	Spin-Parity
g.s.	0.0	0 +
1	44.6	2 +
2	145	4 +
3	305	6 +
4	523	8 +

Continuum levels assumed above 661 keV.

MT=16,17 (n,2n) and (n,3n) cross sections
Calculated with statistical model based on Pearlstein /10/.

MT=18,19,20,21 Fission cross sections

Below 10 keV:

Calculated from the unresolved resonance formula with the
parameters given in the table of resonance parameters.

Above 10 keV:

Calculated from fission plateau cross sections /7,12/ and
Hill-Wheeler type barrier penetration factor /11/.

Fission barrier parameters were taken from Weigmann /13/.

MT=102 Capture cross section

Calculated by optical and statistical model with Gam-g of
41.5 milli-eV and $\langle D \rangle$ of 6.3 eV.

MT=251 Mu-bar

Calculated with optical model.

MF=4 Angular Distribution of Secondary Neutrons

MT= 2 Based on optical and statistical model calculation.

MT=51-54 Isotropic in the center-of-mass system.

MT=16-21,91 Isotropic in the laboratory system.

MF=5 Energy Distribution of Secondary Neutrons

MT=16,17,91 Evaporation spectrum assumed

MT=18,19,20,21 Fission spectrum of Maxwellian form adopted.
Theta taken from evaluation of Terrell/14/.

References

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94-Pu-238 MAT number = 2942

94-Pu-238 PNC Eval-Mar79 T.Kawakita
Dist-Mar83 Rev1-Feb84

History

79-03 New evaluation was made by T.Kawakita (PNC).
84-02 Neutron widths of two low-energy resonances were corrected.
The (n,2n) cross section was also corrected. Comment was added.

MF=1 General Information

MT=451 Descriptive data and dictionary

MT=452 Number of neutrons per fission

The thermal value of prompt neutrons was based on experimental data of Jaffey /1/ and Nu-d was taken from semi-empirical formula by Manero /2/. The energy dependent term was estimated from Howrton's formula /3/.

(Nu-p and Nu-d are not given in JENDL-2.)

MF=2 Resonance Parameters

MT=151 Resolved resonance parameters for MLBW formula.

Energy range is from 1.0E-5 eV to 500 eV. Parameters were taken adopted from the following experimental data.

49 resonances above 10 eV : Silbert /4/

4 resonances below 10 eV : Young /5/

Calculated 2200-m/s cross sections and resonance integrals

	2200-m/s	Res. Integ.
elastic	27.60 b	-
fission	16.55 b	32.4 b
capture	548.8 b	156 b
total	592.9	-

MF=3 Neutron Cross Sections

Below 500 eV is the resonance region. Above 500 eV, the cross sections were evaluated as follows.

MT=1 Total

Sum of partial cross sections.

MT=2,4,51-78,91 Elastic and inelastic scattering

Calculated with optical and statistical models.

Optical potential parameters: Real well depth was obtained by mass fitting. Other parameters were taken from Murata's evaluation /6/.

V	= 41.0 - 0.05*En	(MeV)
Ws	= 6.5 - 0.15*En	(MeV)
Vso	= 7.0	(MeV)
a	= b = aso = 0.47	(fm)
r	= rso = 1.32	(fm)
rs	= 1.38	(fm)

Statistical model calculation with CASTHY code /7/.

The level scheme taken from Ref. /8/.

No.	Energy(kev)	Spin-Parity
g.s.	0.0	0 +
1	44.08	2 +
2	145.98	4 +
3	303.4	6 +
4	514.0	8 +
5	605.1	1 -
6	661.4	3 -
7	763.2	5 -
8	941.5	0 +
9	962.77	1 -
10	968.2	2 -
11	983.0	2 +
12	985.5	2 -
13	1028.55	2 +
14	1069.95	3 +
15	1082.57	4 -
16	1125.8	4 +
17	1174.5	2 +
18	1202.7	3 -
19	1228.6	0 +
20	1264.2	2 +
21	1310.3	2 +
22	1426.6	0 +
23	1447.3	1 -
24	1458.5	2 +
25	1560.0	1 -
26	1596.5	2 +
27	1621.4	1 -
28	1636.6	1 -

Continuum levels assumed above 1.65 MeV.

The level density parameters of Gilbert and Cameron /9/.
No competing process was considered.

MT=16,17 (n,2n) and (n,3n)

Calculation based on the Pearlstein's method /10/.

MT=18 Fission

Evaluated on the basis of measured data /4/, /11/ - /17/.

MT=102 Capture

In the low energy region, the cross section was calculated from the following average resonance parameters.

$S_0 = 1.27E-4$, $S_1 = 2.26E-4$, $D\text{-obs} = 9.5$ eV,
gamma width = 0.040 eV, fission width = 0.013 eV.

MT=251 Mu-bar

Calculated with optical model.

MF=4 Angular Distributions of Secondary Neutrons

MT=2

Calculated with optical model.

MT=51-78

Isotropic in the center-of mass system.

MT=16,17,18,91

Isotropic in the laboratory system.

MF-5 Energy Distributions of Secondary Neutrons

MT=16,17,91

Evaporation spectrum was assumed.

MT=18

Maxwellian type fission spectrum. Temperature was estimated from $Z^{2/A}$ systematics by Smith et al. /18/.

References

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94-Pu-239 MAT number = 2943

94-Pu-239 NAIG+ Eval-Aug79 M.Kawai, T.Yoshida, Y.Kikuchi
Dist-Mar83 Rev1-Jan84

History

79-08 Evaluation was made by

M.Kawai (NAIG) for cross sections above resonance region
and other quantities,

T.Yoshida (NAIG) for resonance parameters and background
cross sections,

Y.Kikuchi (JAERI) for unresolved resonance parameters.

84-01 Small modification. Comment data were added.

MF=1 General Information

MT=451 Descriptive data and dictionary

MT=452 Number of neutrons per fission

Sum of nu-p (MT=456) and nu-d (MT=455).

MT=454 Fission product yields

ENDF/B-IV data were adopted.

MT=455 Delayed neutron data

Evaluated data by Manero and Konshin /1/ were adopted.

MT=456 Number of prompt neutrons per fission

Same as JENDL-1 /2/. Least-squares fit to experimental data
(mainly Refs. /3-5/).

MF=2 Resonance Parameters

MT=151 Resolved and unresolved resonance parameters

Resolved resonances for MLBW formula : from 1.0 to 598 eV.

Parameters were evaluated by Yoshida /6/ modifying parameters
recommended by Ribon /7/. Background cross sections were
added so as to reproduce the measured fission cross section
by Derrien et al. /8/ and capture cross section by Gwin et
al. /9,10/.

Unresolved resonances : from 598 eV to 30 keV.

The energy dependent S0, S1 and fission width were determined
by Kikuchi so as to reproduce the total, capture and fission
cross sections evaluated by Kawai. Fixed parameters were
R=9.054 fm, capture width=41.5 milli-eV.

2200-m/sec cross sections and calculated resonance integrals.

	2200 m/sec	res. integ.
elastic	8.000 b	-
capture	270.2 b	195 b
fission	741.7 b	302 b
total	1019.9 b	-

MF=3 Neutron Cross Sections

Below 1.0 eV.

The elastic and fission cross sections were taken from
ENDF/B-IV. The capture cross section was also taken from
ENDF/B-IV and small modification was made above 0.6 eV. The
total cross section is sum of these three.

Between 1.0 eV and 30 keV.

Background cross sections for resonance parameters were given.

Above 598 eV.

Evaluated cross sections were replaced with unresolved resonance parameters and background cross sections in the energy region between 598 eV and 30 keV.

MT=1 Total

Calculated with optical and statistical model code CASTHY /16/. Spherical optical potential parameters were obtained by fitting the experimental data for total cross sections of Refs. /11-15/.

$$\begin{aligned} V &= 40.72 - 0.05 \cdot E_n \quad (\text{MeV}) \\ W_s &= 6.78 + 0.29 \cdot E_n \quad (\text{MeV}) \\ V_{so} &= 7.0 \quad (\text{MeV}) \\ r &= r_{so} = 1.32 \quad (\text{fm}) \\ r_s &= 1.357 \text{ (derivative Woods-Saxon type)} \quad (\text{fm}) \\ a &= a_{so} = b = 0.47 \quad (\text{fm}) \end{aligned}$$

MT=2 Elastic scattering

Calculated as (Total) - (Partial cross sections).

MT=4.51-78.91 Inelastic scattering

Calculated with CASTHY /16/. The fission, (n,2n), (n,3n) and (n,4n) were considered as competing processes. Level fluctuation and interference effects were also taken into account. Direct inelastic components were added on the basis of coupled channel calculation carried out by Prince

/17/. The level scheme shown below is taken from Ref. /18/.

No.	Energy (keV)	Spin-Parity
g.s.	0.0	1/2 +
1	7.86	3/2 +
2	57.273	5/2 +
3	75.701	7/2 +
4	163.75	9/2 +
5	194.	11/2 +
6	285.46	5/2 +
7	317.	13/2 +
8	330.13	7/2 +
9	360.	15/2 +
10	387.41	9/2 +
11	391.6	7/2 -
12	428.	(13/2 +)
13	435.	9/2 -
14	452.	(11/2 -)
15	462.	11/2 +
16	469.8	1/2 -
17	482.	(13/2 -)
18	488.	11/2 -
19	492.1	3/2 -
20	505.5	5/2 -
21	511.83	7/2 +
22	538.	(7/2 +)
23	555.	7/2 -
24	565.	9/2 +
25	583.	9/2 -
26	620.	15/2 -
27	634.	11/2 +
28	659.	11/2 -

Continuum levels were assumed above 670 keV. The values of spin in parenthesis were assumed from those of neighbouring nuclide. Level density parameters were taken from Murata's evaluation /28/.

	a (1/MeV)	spin-cut off factor	E-pair (MeV)	CO	E-joint (MeV)
Pu-239	26.93	17.6156	0.61	4130.0	3.61
Pu-240	26.53	17.7964	1.64	5480.0	3.53

MT=16,17,37 (n,2n), (n,3n) and (n,4n)

Calculated with Perlstein's method /28/ by using the neutron emission cross sections which derived by subtracting the presently evaluated fission and capture cross sections from compound nucleus formation cross section obtained with CASTHY. The results agree with the experimental values by Mather et al. /27/.

MT=18 Fission

Evaluated on the basis of the following measured data.

Absolute measurements:

Kari and Cierjacks /19/, Cance and Grenier /20/, Gwin et al. /10/ and Gayther /21/.

Relative measurements to the U-235 fission cross section:

Carlson and Behrens /22/, Meadows /23/, Kari and Cierjacks /19/, Cance and Grenier /20/ and Fursov et al. /24/.

The relative data were converted into cross sections by multiplying the U-235 fission cross section in JENDL-2 /25/.

MT=102 Capture

The cross section in the energy range below 1 MeV was derived as a product of the evaluated fission cross section and alpha values. The alpha values are the same as JENDL-1 /2/. Above 1 MeV, results of statistical model calculation with CASTHY /16/ was applied.

Normalization parameters for CASTHY calculation:

Gamma-g = 43.0 milli eV.

D-obs = 2.36 eV.

Capture cross section = 284 mb at 100 keV.

MT=251 Mu-bar

Calculated with CASTHY /16/.

MF=4 Angular Distributions of Secondary Neutrons

MT=2 Calculated with CASTHY code /16/.

MT=51-78 Isotropic in the center-of-mass system.

MT=16,17,18,37,91 Isotropic in the laboratory system.

MF=5 Energy Distributions of Secondary Neutrons

MT=16,17,37,91 Evaporation spectrum.

MT=18 Maxwellian fission spectrum estimated from Z^{*2}/A systematics /29/.

MT=455 Taken from ENDF/B-IV.

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94-Pu-240 MAT number = 2944

94-Pu-240 NAIG+ Eval-Mar79 T.Murata,A.Zukeran,Y.Kikuchi
Dist-Mar83 Rev1-Nov83

History

79-03 New evaluation was made by the following evaluaters.
 A.Zukeran (Hitachi) Resolved resonance parameters
 Y.Kikuchi (JAERI) Unresolved resonance parameters
 T.Murata (NAIG) Other quantities
 83-03 MF=5 was added.
 83-11 Comment was added.

MF=1 General Information

MT=451 Comments and dictionary
 MT=452 Number of neutrons per fission
 Sum of MT=455(delayed neutrons) and MT=456(prompt neutrons).
 MT=455 Delayed neutron data
 Taken from ENDF/B-IV.
 MT=456 Number of prompt neutrons
 Linear least-squares fitting to the experimental data of
 Freaut et al. /1/ renormalized to Cf-252 nu-p=3.756.

MF=2 Resonance Parameters

MT=151 Resolved and unresolved resonance parameters

1) Resolved resonances for MLBW formula

Energy range : 1.0E-4 to 4 keV.
 The first resonance at 1.056 eV was evaluated on the basis
 of Pattenden and Rainey /2/. The neutron and capture widths
 were based on the experimental data by Hockenbury et al. /3/
 in the energy range from 20 to 500 eV, and Kolar and
 Boeckhoff /4/ from 500 eV to 4 keV. The average capture
 width of 29.5 milli-eV was assumed for the resonances whose
 J values were unknown. The sub-threshold fission widths
 were taken from the data by Auchampaugh and Weston /5/. A
 negative resonance was adopted from ENDF/B-IV. Details are
 given in Ref. /6/.

2) Unresolved resonances

Energy range : 4 to 40 keV.
 Energy dependent parameters were determined to reproduce the
 presently evaluated cross sections in this energy region.

Calculated 2200-m/sec cross sections and res. integrals.

	2200-m/sec	res. integ.
elastic	1.509 b	-
fission	0.06761b	10.1 b
capture	288.5 b	8450. b
total	290.1 b	

MF=3 Neutron Cross Sections

Below 4 keV: Background cross sections are given.

Above 4 keV: Evaluated as follows. In the energy range from 4
 to 40 keV, the cross sections are represented with
 the unresolved resonance parameters, and the back-

ground cross sections are given in MF=3.

MT=1 Total

Optical model calculation with the following parameters, which were determined to reproduce the experimental data of Smith et al. /7/, strength functions and calculated cross sections from resolved resonance parameters.

The spherical optical potential parameters

$$\begin{aligned} V &= 40.6 - 0.05 * e, & W_s &= 6.5 + 0.15 * e & (\text{MeV}) \\ V_{so} &= 7.0 & & & (\text{MeV}) \\ r &= r_{so} = 1.32, & r_s &= 1.38 & (\text{fm}) \\ a &= a_s = a_{so} = 0.47 & & & (\text{fm}) \end{aligned}$$

Optical and statistical model calculations were made with CASTHY code /8/.

MT=2 Elastic scattering

Obtained by subtracting the other cross sections from total cross section below 4 MeV. Above 4 MeV, optical model calculation.

MT=4 Total inelastic scattering

Sum of partial inelastic scattering cross sections (MT=51 to MT=91).

MT=51-79, 91 Partial inelastic scattering

CASTHY-code calculation for almost levels. For some levels, for which Smith's experimental data /7/ were available, renormalization was performed (for 1st, 2nd, 3rd, 5th and 9 to 11th levels).

Level scheme (taken mainly from Ref. /9/)

No.	Energy (MeV)	Spin-Parity
g.s.	0.0	0 +
1	0.0428	2 +
2	0.1417	4 +
3	0.2947	6 -
4	0.4976	8 +
5	0.5974	1 -
6	0.6489	3 -
7	0.7425	5 -
8	0.7514	10 +
9	0.8607	0 +
10	0.9003	2 +
11	0.9381	1 -
12	0.9589	2 -
13	0.9926	4 +
14	1.002	3 -
15	1.031	3 +
16	1.038	4 -
17	1.076	4 +
18	1.090	0 +
19	1.116	5 -
20	1.138	2 +
21	1.161	6 -
22	1.178	3 +
23	1.180	2 +
24	1.223	2 +
25	1.232	4 +

26	1.241	2 -
27	1.262	3 +
28	1.282	3 -
29	1.309	5 -

Levels above 1.309 MeV were assumed to be continuum. Level density parameters were determined to reproduce the resonance-level spacing and level-scheme staircase.

MT=16,17,37 (n,2n), (n,3n) and (n,4n)

Neutron emission cross section obtained by subtracting the elastic scattering (MT=2), fission (MT=18) and capture (MT=102) cross sections from the total (MT=1) were multiplied by branching ratio to each reaction channel calculated with Pearlstein's method /10/.

MT=18 Fission

Below 9 keV : Shape of fission cross section based on the experimental data of Byers et al. /11/ and the calculated cross section with resonance parameters of Migneco and Theobald /12/. Then normalized to the value of higher energy region.

Above 9 keV : Fission ratios to U-235 fission based on the experimental data of Behrens et al. /13/ and Wisshak and Kaeppler /14/ were multiplied by U-235 fission cross section of JENDL-2 /15/.

MT=102 Capture

Below 0.35 MeV : Based on the experimental data of Hockenbury et al. /3/, Weston and Todd /16/ and the ratio data of Wisshak and Kaeppler /17/ with the capture cross section of Au-197 /18/. As a guide line, the result of CASTHY calculation was normalized to the low energy region. direct and collective capture were included in high energy region using the value for U-238 given by Kitazawa et al. /19/.

MT=251 Mu-bar

The same as JENDL-1 /20/.

MF=4 Angular Distributions of Secondary Neutrons

MT=2 Taken from JENDL-1 /20/.

MT=16,17,18,37,91 Isotropic in the laboratory system.

MT=51-79 Isotropic in the center-of-mass system.

MF=5 Energy Distributions of Secondary Neutrons

MT=16,17,37,91 Evaporation spectrum

MT=18 Fission spectrum. Temperature was estimated from $Z^{2/A}$ systematics by Smith et al. /21/.

MT=455 Taken from ENDF/B-IV.

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94-Pu-241 MAT number = 2945

94-Pu-241 JAERI Eval-Oct79 Y.Kikuchi,N.Sekine
Dist-Dec79 Rev1-Nov83

History

79-10 New evaluation was made by Y.Kikuchi (JAERI) and N.Sekine (HEC). Data of JENDL-1 /1/ were superseded.
79-12 Files 2, 3 and 4 were released as JENDL-2B /2/.
83-03 Files 1 and 5 were added.
83-11 Comment was added.

MF=1 General Information

MT=451 Comment and dictionary
MT=452 Number of neutrons per fission
Sum of Nu-p (MT=456) and Nu-d (MT=455).
MT=454 Fission yield data
No evaluation done. Data of ENDF/B-IV were adopted.
MT=455 Delayed neutron data
Data of Benedetti + /3/
MT=456 Number of prompt neutrons per fission
Data of Boldeman and Frehaut /4/ for thermal fission
Nu-p (Cf-252 spontaneous fission) = 3.753 assumed.
Energy dependence : Frehaut + /5/

MF=2, MT=151 Resonance Parameters

Resolved resonances : 1 - 100 eV
JENDL-1 data /1/ modified for better fit to experiments.
A negative resonance added.
Background cross section applied for fission and capture.

Unresolved resonances : 100 eV - 30 keV
Obtained by fitting evaluated Sig-f and Sig-c.
Energy dependent parameters : So, S1 and Gam-f.
Fixed parameters : R=9.8 fm , Gam-g = 0.040 eV,
D-obs = 0.85 eV

2200-m/sec cross sections and calculated resonance integrals.

	2200 m/sec	Res. Integ.
elastic	10.23 b	-
fission	1015. b	590 b
capture	363.0 b	187 b
total	1388.2 b	-

MF=3 Neutron Cross Sections

Point-wise data below 1 eV down to 1.0E-5 eV
Sig-t : on the basis of the data of Smith + /6/
Sig-f : on the basis of the data of Wagemans + /7/
Sig-e : calculated from resonance parameters
Sig-c : Sig-t - (Sig-f + Sig-e)
2200 m/s values :
Sig-t = 1388.2 b , Sig-f = 1015 b , Sig-c = 363 b.

Background cross sections for resolved resonances (1 - 100 eV).

No background cross sections for unresolved resonances.

Above 30 keV, smooth cross sections given as follows.

MT=1,2,4,51-61,91,251 : Sig-t, Sig-e, Sig-in, mu-bar

Calculated with optical and statistical models.

Optical potential parameters obtained from systematics /8/

$$V = 40.25 - 0.05 \cdot E_n, \quad W_s = 6.5, \quad V_{so} = 7.0 \quad (\text{MeV})$$

$$r = r_{so} = 1.32, \quad r_s = 1.38 \quad (\text{fm})$$

$$a = b = a_{so} = 0.47 \quad (\text{fm})$$

Statistical model calculation with CASTHY code /9/.

Competing processes : fission, (n,2n), (n,3n), (n,4n).

Level fluctuation considered.

The level scheme taken from Ref. /10/.

No	Energy (keV)	Spin-Parity
g.s.	0	5/2 +
1	41.8	7/2 +
2	94.0	9/2 +
3	161.5	1/2 +
4	170.8	3/2 +
5	223.1	5/2 +
6	230.0	9/2 +
7	242.7	7/2 +
8	300	11/2 +
9	335	9/2 +
10	368	13/2 +
11	445	11/2 -

Continuum levels assumed above 490 keV.

The level density parameters : Gilbert and Cameron /11/.

MT=16,17,37 (n,2n), (n,3n), (n,4n)

Calculated with evaporation model.

MT=18 Fission

Simultaneous evaluation with U-235, U-238, Pu-240, Pu-241 /8/
mainly based on the data of Carlson +/12/, Kaeppler+/13/,
Fursov+/14/ and Szabo+/15,16/.

MT=102 Capture

Based on the data of Alpha by Weston+ /17/ up to 250 keV.
Calculated with the statistical model above 250 keV.
The gamm-ray strength function was determined so that
Sig-c = 269 mb at 250 keV.

MF=4 Angular Distributions of Secondary Neutrons

MT=2 : Calculated with the optical model.

MT=51-61 : Isotropic in the center-of-mass system.

MT=16,17,18,37,91 : Isotropic in the laboratory system.

MF=5 Energy Distributions of Secondary Neutrons

MT=16,17,18,37,91 : Evaporation spectrum.

MT=18 : Maxwellian fission spectrum.

Temperature estimated from Z^{**2}/A values.

MT=455 : Beta-i from the data of Benedetti+ /3/.

ENDF/B-IV data for delayed neutron spectrum.

No background cross sections for unresolved resonances.

Above 30 keV, smooth cross sections given as follows.

MT=1,2,4,51-61,91,251 : Sig-t, Sig-e, Sig-in, mu-bar

Calculated with optical and statistical models.

Optical potential parameters obtained from systematics /8/

$$V = 40.25 - 0.05 \cdot E_n, \quad W_s = 6.5, \quad V_{so} = 7.0 \quad (\text{MeV})$$

$$r = r_{so} = 1.32, \quad r_s = 1.38 \quad (\text{fm})$$

$$a = b = a_{so} = 0.47 \quad (\text{fm})$$

Statistical model calculation with CASTHY code /9/.

Competing processes : fission, (n,2n), (n,3n), (n,4n).

Level fluctuation considered.

The level scheme taken from Ref. /10/.

No	Energy (keV)	Spin-Parity
g.s.	0	5/2 +
1	41.8	7/2 +
2	94.0	9/2 +
3	161.5	1/2 +
4	170.8	3/2 +
5	223.1	5/2 +
6	230.0	9/2 +
7	242.7	7/2 +
8	300	11/2 +
9	335	9/2 +
10	368	13/2 +
11	445	11/2 -

Continuum levels assumed above 490 keV.

The level density parameters : Gilbert and Cameron /11/.

MT=16,17,37 (n,2n), (n,3n), (n,4n)

Calculated with evaporation model.

MT=18 Fission

Simultaneous evaluation with U-235, U-238, Pu-240, Pu-241 /8/
mainly based on the data of Carlson +/12/, Kaeppeler +/13/,
Fursov +/14/ and Szabo +/15,16/.

MT=102 Capture

Based on the data of Alpha by Weston +/17/ up to 250 keV.
Calculated with the statistical model above 250 keV.
The gamm-ray strength function was determined so that
Sig-c = 269 mb at 250 keV.

MF=4 Angular Distributions of Secondary Neutrons

MT=2 : Calculated with the optical model.

MT=51-61 : Isotropic in the center-of-mass system.

MT=16,17,18,37,91 : Isotropic in the laboratory system.

MF=5 Energy Distributions of Secondary Neutrons

MT=16,17,18,37,91 : Evaporation spectrum.

MT=18 : Maxwellian fission spectrum.

Temperature estimated from Z^{*2}/A values.

MT=455 : Beta-i from the data of Benedetti +/3/.

ENDF/B-IV data for delayed neutron spectrum.

References

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94-Pu-242 MAT number = 2946

94-Pu-242 NAIG Eval-Mar81 M.Kawai and T.Murata
 Dist-Mar83 Rev1-Nov83

History

81-03 New evaluation was made by M. Kawai (NAIG) for resonance parameters /1/ and T. Murata (NAIG) for smooth cross sections.

83-03 MF=5 was added.

83-11 Q values and threshold energies and MF=4 were modified.

MF=1 General Information

MT=451 Descriptive data and dictionary

MT=452 Total number of neutrons per fission

Taken from ENDF/B-IV /2/.

MF=2 Resonance Parameters

MT=151

Resolved resonances for MLBW formula : $1.0E-5$ eV - 1290 eV.

Res. energies : BNL-325 3rd edition /3/

Gam-n, Gam-g : Poortmans et al. /4/, Auchampaugh et al. /5/

Gam-f : Deduced from fission areas given by
 Berman et al. /6/ and Auchampaugh et al.
 /5/.

R-scat : 9.6 fm /3/

Average Gam-g : 24.2 milli-eV

Background cross section of 0.67 barns was added to elastic scattering cross section so as to reproduce the measured data of the elastic /7/ and total cross sections /8, 9/.

Calculated 2200-m/s cross sections and res. integrals

	2200-m/s	res. integ.
elastic	8.111 b	-
capture	18.42 b	1117 b
fission	0.1212b	6.35 b
total	26.65 b	-

MF=3 Neutron Cross Sections

MT=1 Total

* Below 6 keV : Experimental data of Young and Reeder /8/ were averaged over some keV intervals.

* Above 6 keV : The results of optical model calculation with the following parameters were adjusted in the energy region from 6 keV to 100 keV to connect smoothly with the total cross section below 6 keV.

$V = 40.1 - 0.05 * e$, $W_s = 6.5 + 0.15 * e$ (MeV)

$V_{so} = 7.0$ (MeV)

$r = r_{so} = 1.32$, $r_s = 1.38$ (fm)

$a - a_s = a_{so} = 0.47$ (fm)

Optical and statistical model calculations were made with CASTHY code /10/.

MT=2 Elastic scattering

* Below inel. threshold : Obtained by subtracting the non-

elastic scattering from the total cross section.

- * Above the threshold : Sum of the shape elastic scattering cross section calculated with optical model and the compound elastic scattering cross section obtained using the other cross sections and results of statistical model calculation.

MT=4 Total inelastic scattering

Obtained by subtracting the others from the total cross section.

MT=51-67,91 Partial and continuum inelastic scattering

The total inelastic scattering (MT=4) was multiplied by branching ratio to each level calculated with CASTHY code.

Level scheme (taken mainly from Ref. /11/)

No.	Energy (MeV)	Spin-Parity
g.s.	0.0	0 +
1	0.0445	2 +
2	0.1472	4 +
3	0.3059	6 +
4	0.5176	8 +
5	0.7787	10 +
6	0.7803	1 -
7	0.8323	3 -
8	0.865	1 -
9	0.927	5 -
10	0.956	0 +
11	0.995	2 +
12	1.019	3 -
13	1.064	4 -
14	1.087	12 +
15	1.102	2 +
16	1.122	5 -
17	1.152	2 -

Levels above 1.152 MeV were assumed to be continuum.

Level density parameters were determined to reproduce the resonance level spacing and level scheme staircase.

MT=16,17,37 (n,2n), (n,3n) and (n,4n)

Neutron emission cross section obtained by subtracting the elastic (MT=2), fission (MT=18) and capture (MT=102) from the total cross section (MT=1) were multiplied by branching ratio to reaction channel calculated with Pearlstein's method /12/.

MT=18 Fission

- * Below 100 keV : Shape of fission cross section was determined on the basis of fission area data of Auchampaugh et al. /13/. Then normalized to the value of higher energy region.

- * Above 100 keV : Fission ratios to U-235 fission cross section were obtained from the experimental data of Behrens et al. /14/ and multiplied by the U-235 fission cross section of JENDL-2 /15/.

MT=102 Capture

- * Energy region from 6 keV to 210 keV : Determined from the experimental data of Hokenbury et al. /16/ and Wisshak and Kaeppler /17/.
- * Other energy region : Calculated results with CASTHY code

were normalized to the capture cross section in the region of 6 to 210 keV. Direct and collective captures were included in high energy region using the value for U-238 given by Kitazawa et al. /18/.

MT=251 Mu-bar

Calculated with optical model.

MF=4 Angular Distributions of Secondary Neutrons

MT=2 Taken from Pu-240 data /19/ calculated with optical model.

MT=51-67 Assumed to be isotropic in the center-of-mass system.

MT=16,17,18,37,91 Isotropic in the lab system.

MF=5 Energy Distributions of Secondary Neutrons

MT=16,17,37,91 Evalporation spectrum.

MT=18 Fission spectrum. Temperature was estimated Z^2/A systematics by Smith et al. /20/.

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95-Am-241 MAT number = 2951

95-Am-241 JAERI Eval-Mar82 Y.Kikuchi
 JAERI-M82-096 Dist-Mar83 Rev1-Nov83

History

82-03 Complete reevaluation for JENDL-2 was made by Y.Kikuchi (JAERI). Details are given in Ref. /1/.

83-11 Comment was added.

MF=1 General Information

MT=451 Comment and dictionary
 MT=452 Number of neutrons per fission
 Sum of Nu-p (MT=456) and Nu-d (MT=455).
 MT=454 Fission product yield data
 Taken from ENDF/B-IV, and renormalized to 2.0.
 MT=455 Delayed neutron data
 Estimated with semi-empirical formula by Tuttle /2/.
 MT=456 Number of prompt neutrons
 Experimental data of Jaffey and Lerner /3/.

MF=2, MT=151 Resonance parameters

Resolved resonances for MLBW formula : 1.0E-5 - 150 eV
 Data of Derrien and Lucas /4/. Same as JENDL-1 /5/.
 5 negative resonances added.

Unresolved resonances : 150 eV - 30 keV

The evaluated Sig-t, Sig-c and Sig-f were fitted
 by adjusting S0, S1 and Gam-f.

Fixed parameters: R=9.37 fm, Gam-g=43.77 MeV,
 Dobs=0.432 eV

Calculated 2200-m/s cross sections and resonance integrals

	2200 m/s value	Res. Int.
elastic	11.26 b	-
capture	600.4 b	1299 b
fission	3.018 b	14.7 b
total	614.7 b	-

MF=3 Neutron Cross Sections

MT=1,2,4,51-66,91,251 Sig-t, Sig-el, Sig-in, Mu-bar

Calculated with optical and statistical models. Optical
 potential parameters were obtained by fitting the data of
 Phillips and Howe /6/ :

$V = 43.4 - 0.107 * E_n$ (MeV)
 $W_s = 6.95 - 0.339 * E_n + 0.0531 * E_n^2$ (MeV)
 $W_v = 0$, $V_{so} = 7.0$ (MeV)
 $r = r_{so} = 1.282$, $r_s = 1.29$ (fm)
 $a = a_{so} = 0.60$, $b = 0.5$ (fm)

Statistical model calculation with CASTHY code /7/.

Competing processes : fission, (n,2n), (n,3n), (n,4n).

Level fluctuation considered.

The level scheme taken from Ref. /8/

No energy (keV) spin-parity

g. s.	0	5/2 -
1	41.2	7/2 -
2	93.6	9/2 -
3	158.0	11/2 -
4	205.9	5/2 +
5	234.0	7/2 +
6	271.0	9/2 +
7	319.0	11/2 +
8	375.0	13/2 +
9	471.8	3/2 -
10	504.5	5/2 -
11	549.0	7/2 -
12	623.1	1/2 +
13	636.9	3/2 -
14	652.1	1/2 -
15	653.2	3/2 +
16	670.2	3/2 +

Continuum levels assumed above 732 keV.

The level density parameters : Gilbert and Cameron /9/.

MT=16,17,37 (n,2n), (n,3n), (n,4n)
Calculated with evaporation model.

MT=18 Fission
Evaluated on the basis of the following measured data :
Knitter and Budtz-Jorgensen /10/ : 150 eV - 10 keV
Wisshak and Kaeppler /11/ : 10 - 300 keV
Behrens and Browne /12/ : 300 keV - 20 MeV
High sub-threshold cross-section values of Seeger + /13/
were abandoned.

MT=102 Capture
Evaluated on the basis of the measured data of Gayther and
Thomas /14/ up to 350 keV.
Calculated with the statistical model above 350 keV.
The gamma-ray strength function was determined so that
Sig-c = 830 mb at 350 keV.

MF=4 Angular Distributions of Secondary Neutrons
MT=2,51-66,91 Calculated with optical model.
MT=16,17,18,37 Isotropic in the lab system.

MF=5 Energy Distributions of Secondary Neutrons
MT=16,17,37,91 Evaporation spectrum.
MT=18 Maxwellian fission spectrum. Temperature
was estimated from Z^{*2}/A values /14/.

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95-Am-242 MAT number = 2952

95-Am-242 JAERI Eval-Mar80 T.Nakagawa,S.Igarasi
 JAERI-M 8903 (1980) Dist-Mar83 Rev1-Nov83

History

80-03 New evaluation was made by T.Nakagawa and S.Igarasi (JAERI).

Details are given in Ref. /1/.

83-11 Comment was added.

MF=1 General Information

MT=451 Comment and dictionary

MT=452 Number of neutrons per fission
 Sum of prompt and delayed neutrons.

MT=455 Delayed neutron data
 Estimated from Tuttle's semi-empirical formula /2/.

MT=456 Number of prompt neutrons per fission
 Semi-empirical formula by Howerton /3/
 $Nu-p = 3.268 + 0.172 * E(\text{MeV})$.

MF=2 Resonance Parameters

MT=151 No resonance parameters

2200m/s cross sections and calculated resonance integrals.

	2200 m/sec	Res. Integ.
capture	5500.0 b	391 b
fission	2100.0 b	1260 b
elastic	11.44 b	-
total	7611.44 b	-

MF=3 Neutron Cross Sections

MT=1,2,4,51-72,91,102,251 Sig-t,Sig-el,Sig-in,Sig-c,Mu-bar

Below 0.225 eV:

1/v form was assumed for fission and capture cross sections. Effective scattering radius of 9.54 fm was used for elastic scattering cross-section calculation.

Above 0.225 eV:

Optical and statistical models were used.

The spherical optical potential parameters (MeV, fm) :

$$V = 42.0 - 0.107 * E, \quad r = 1.282, \quad a = 0.6$$

$$W_s = 9.0 - 0.339 * E + 0.0531 * E^{*2}, \quad r = 1.29, \quad a = 0.5$$

$$V_{so} = 7.0, \quad r = 1.282, \quad a = 0.6$$

Statistical model calculation with CASTHY code /4/.

Competing processes : fission, (n,2n) and (n,3n).

Level fluctuation considered. Gam-g = 0.05 eV and

D = 0.45 eV used for capture cross section calculation

The level scheme taken from the compilation by Ellis and Haese /5/.

No.	Energy (MeV)	Spin-Parity
g.s.	0.0	1 -
1	0.044	0 -
2	0.049	3 -
3	0.049	5 -
4	0.074	2 -

5	0.113	6	-
6	0.148	4	-
7	0.148	5	-
8	0.190	7	-
9	0.242	3	-
10	0.263	6	-
11	0.263	7	-
12	0.288	4	-
13	0.288	2	-
14	0.325	3	-
15	0.341	5	-
16	0.372	4	-
17	0.410	6	-
18	0.430	5	-
19	0.488	7	-
20	0.500	6	-
21	0.581	7	-
22	0.679	8	-

Overlapping levels are assumed above 0.681 MeV.

The level density parameters of Gilbert and Cameron /6/.

MT=16,17 (n,2n) and (n,3n) cross sections

Calculated with the evaporation model by Pearlstein /7/.

MT=18 Fission cross section

The empirical formula used for the Am-242m data was applied by shifting the energy origin to -49 keV.

MF=4 Angular Distributions of Secondary Neutrons

MT=2 Legendre coefficients are given by the optical and statistical model calculations.

MT=16,17,18,91 Isotropic distributions in the center-of-mass system.

MT=51-72 Isotropic distributions in the laboratory system.

MF=5 Energy Distributions of Secondary Neutrons

MT=16,17,91 Evaporation spectrum

MT=18 Fission spectrum estimated from Z^2/A systematics by Smith et al. /8/ by assuming $E(\text{Cf-252}) = 2.13$ MeV.

References

- 1) T. Nakagawa and S. Igarasi : JAERI-M 8903 (1980), in Japanese.
- 2) R.J. Tuttle : INDC(NDS)-107/G+Special, 29 (1979).
- 3) R.J. Howerton : Nucl. Sci. Eng., 62, 438 (1977).
- 4) S. Igarasi : J. Nucl. Sci. Technol., 12, 67(1975).
- 5) Y.A. Ellis and R.L. Haese : Nucl. Data Sheets 21, 615 (1977).
- 6) A. Gilbert and A.G.W. Cameron : Can. J. Phys., 43, 1446 (1965).
- 7) S. Pearlstein : Nucl. Sci. Eng., 23, 238 (1965).
- 8) A.B. Smith et al. : ANL/NDM-50 (1979).

95-Am-242m MAT number = 2953

95-Am-242m JAERI Eval-Mar80 T.Nakagawa, S.Igarasi
 JAERI-M 8903 (1980) Dist-Mar83 Rev1-Feb84

History

80-03 New evaluation was made by T.Nakagawa and S.Igarasi (JAERI).
 Details are given in Ref. /1/.
 83-11 Comment was added.
 84-02 Cross sections were corrected around 3.5 eV.

MF=1 General Information

MT=451 Comment and dictionary
 MT=452 Number of neutrons per fission
 Sum of prompt and delayed neutrons.
 MT=455 Delayed neutron data
 Estimated from Tuttle's semi-empirical formula /2/.
 MT=456 Number of prompt neutrons per fission
 Based on the relative measurements /3,4/ to the U-235
 data, and on the empirical formula by Howerton /5/.
 The U-235 data of JENDL-2 were used.
 $\nu_{p} = 3.268 + 0.172 * E(\text{MeV})$.

MF=2 Resonance Parameters

MT=151 Resonance parameters : below 3.5 eV. Single level B-W.
 Parameters by Bowman et al. /6/ were adopted.
 Average $\Gamma_{g} = 0.05$ eV , level spacing = 0.45 eV ,
 s-wave neutron strength function = $1.4E-4$.

Calculated 2200m/s cross sections and resonance integrals.

	2200 m/sec	Res. Integ.
capture	1342. b	207 b
fission	6620. b	1530 b
elastic	6.698 b	-
total	7969. b	--

MF=3 Neutron Cross Sections

The resonance region:

Null value is given for the total, elastic scattering, capture
 and fission cross sections.

From 3.5 eV to 1.5 keV:

The fission cross section was evaluated by fitting spline
 functions to the experimental data by Bowman et al. /6/ and
 Seeger et al. /7/. The capture and elastic scattering cross
 sections were estimated by assuming that the cross sections
 have the same structure as that of the fission cross section.
 Calculations were made by using the radius parameters of 9.45
 fm, average fission and capture widths of 0.385 eV and 0.05 eV
 respectively.

Above 1.5 keV:

MT=1,2,4,51-73,91,102,251 Sig-t, Sig-el, Sig-in, Sig-c, Mu-bar
 Calculated with optical and statistical models above
 1.5 keV.

The spherical optical potential parameters (MeV, fm) :

$$V = 42.0 - 0.107 * E, \quad r = 1.282, \quad a = 0.6$$

$$W_s = 9.0 - 0.339 * E + 0.0531 * E ** 2, \quad r = 1.29, \quad a = 0.5$$

$$V_{so} = 7.0, \quad r = 1.282, \quad a = 0.6$$

Statistical model calculation with CASTHY code /8/.

Competing processes : fission, (n,2n) and (n,3n).

Level fluctuation considered. $\Gamma_{\text{avg}} = 0.05$ eV and $D =$

0.45 eV used for capture cross section calculation.

The level scheme taken from the compilation by Ellis and Haese /9/, with shifted energy origin at -49 keV.

No.	Energy (MeV)	Spin-Parity
g.s.	-0.049	1 -
1	-0.05	0 -
2	0.0	3 -
3	0.0 (meta stable)	5 -
4	0.025	2 -
5	0.064	6 -
6	0.099	4 -
7	0.099	5 -
8	0.141	7 -
9	0.193	3 -
10	0.214	6 -
11	0.214	7 -
12	0.239	4 -
13	0.239	2 -
14	0.276	3 -
15	0.292	5 -
16	0.323	4 -
17	0.361	6 -
18	0.381	5 -
19	0.439	7 -
20	0.451	6 -
21	0.532	7 -
22	0.630	8 -

Overlapping levels are assumed above 0.632 MeV.

The level density parameters of Gilbert and Cameron /8/.

MT=16,17 (n,2n) and (n,3n) cross sections

Calculated with the evaporation model by Pearlstein /9/.

MT=18 Fission cross section

Smooth cross section above 1.5 keV was obtained by fitting a semi-empirical formula to the averaged experimental data.

MF=4 Angular Distributions of Secondary Neutrons

MT=2 Legendre coefficients are given by the optical and statistical model calculations.

MT=16,17,18,91 Isotropic distributions in the laboratory system.

MT=51-72 Isotropic distributions in the center-of-mass system.

MF=5 Energy Distributions of Secondary Neutrons

MT=16,17,91 Evaporation spectrum

MT=18 Fission spectrum estimated from Z^{*2}/A systematics by Smith et al. /10/ by assuming $E(\text{Cf-252}) = 2.13$ MeV.

References

- 1) T. Nakagawa and S. Igarasi : JAERI-M 8903 (1980), in Japanese.
- 2) R.J. Tuttle : INDC(NDS)-107/G+Special, 29 (1979).

- 3) A.H. Jaffey and J.L. Lerner : Nucl. Phys., A145, 1 (1970).
- 4) N.I. Kroshkin and Yu.S. Zamyatnin : Atom. Energ., 29, 95 (1970), Sov. Atom. Energy, 29, 790 (1970).
- 5) R.J. Howerton : Nucl. Sci. Eng. 62, 438 (1977).
- 6) C.D. Bowman et al. : Phys. Rev., 166, 1216 (1968).
- 7) P.A. Seeger et al. : Nucl. Phys., A96, 605 (1967).
- 8) S. Igarasi : J. Nucl. Sci. Technol., 12, 67 (1975).
- 9) Y.A. Ellis and R.L. Haese : Nucl. Data Sheets 21, 615 (1977).
- 10) A. Gilbert and A.G.W. Cameron : Can. J. Phys., 43, 1446 (1965).
- 11) S. Pearlstein : Nucl. Sci. Eng., 23, 238 (1965).
- 12) A.B. Smith et al. : ANL/NDM-50 (1979).

95-Am-243 MAT number = 2954

95-Am-243 JAERI Eval-Mar82 Y.Kikuchi
 JAERI-M82-096 Dist-Mar83 Rev1-Nov83

History

77-03 New evaluation was made by S.Igarasi and T.Nakagawa (JAERI).
 Details are given in Ref. /1/.
 82-03 Complete reevaluation for JENDL-2 was made by Y.Kikuchi
 (JAERI). Details are given in Ref. /2/.
 83-11 Comment was added.

MF=1 General Information

MT=451 Comment and dictionary
 MT=452 Number of neutrons per fission
 Sum of Nu-p (MT=456) and Nu-d (MT=455).
 MT=454 Fission product yield data
 Taken from ENDF/B-IV and renormalized to 2.0.
 MT=455 Delayed neutron data
 Estimated with semi-empirical formula by Tuttle /3/.
 MT=456 Number of prompt neutrons
 Estimated from systematics. Same as previous evaluation /1/.

MF=2, MT=151 Resonance parameters

Resolved resonances for MLBW formula : $1.0E-5 - 215$ eV.
 Based on the data of Simpson + /4/. The results are the same as the previous evaluation /1/ except fission widths which were determined to reproduce the fission cross section of 0.225 barns at 0.0253 eV. The neutron width of a negative resonance was adjusted to the thermal capture and total cross sections.

Unresolved resonances : 215 eV - 30 keV

Obtained from optical model calculation:

$S_0=0.93E-4$, $S_1=2.44E-4$, $R=9.34$ fm

Estimated from resolved resonances:

$\Gamma_{obs}=0.67$ eV, $\Gamma_{g-g}=0.039$ eV, $\Gamma_{g-f}=0.00012$ eV

Calculated 2200-m/s cross sections and resonance integrals

	2200 m/s value	Res. Int.
elastic	7.528 b	-
capture	78.50 b	1820 b
fission	0.2281 b	11.4 b
total	86.26 b	-

MF=3 Neutron Cross Sections

MT=1,2,4,51-59,91,102,251 Sig-t, Sig-el, Sig-in, Sig-c, Mu-bar

Calculated with optical and statistical models. Optical potential parameters were obtained /1/ by fitting the data of Phillips and Howe /5/ for Am-241:

$V = 43.4 - 0.107*E_n$ (MeV)

$W_s = 6.95 - 0.339*E_n + 0.0531*E_n**2$ (MeV)

$W_v = 0$, $V_{so} = 7.0$ (MeV)

$r = r_{so} = 1.282$, $r_s = 1.29$ (fm)

$a = a_{so} = 0.60$, $b = 0.5$ (fm)

Statistical model calculation with CASTHY code /6/.

Competing processes : fission, (n,2n), (n,3n), (n,4n).

Level fluctuation considered.

The level scheme taken from Ref. /7/

No	Energy (keV)	Spin-Parity
g.s.	0	5/2 -
1	42.2	7/2 -
2	84.0	5/2 +
3	96.4	9/2 -
4	109.3	7/2 +
5	143.5	9/2 +
6	189.3	11/2 +
7	267.0	3/2 -
8	298.0	5/2 -
9	344.0	7/2 -

Continuum levels assumed above 383 keV.

The level density parameters : Gilbert and Cameron /9/.

Gamma-ray strength function deduced from resonance parameters

MT=16,17,37 (n,2n), (n,3n), (n,4n)

Calculated with evaporation model.

MT=18 Fission

Evaluated on the basis of the measured data of Behrens and Browne /9/ above 200 keV. The curve was smoothly connected to the unresolved resonance region below 200 keV. High sub-threshold cross-section values of Seeger + /10/ were abandoned.

MF=4 Angular Distributions of Secondary Neutrons

MT=2,51-66,91 Calculated with optical model.

MT=16,17,18,37 Isotropic in the laboratory system.

MF=5 Energy Distributions of Secondary Neutrons

MT=16,17,37,91 Evaporation spectrum.

MT=18 Maxwellian fission spectrum. Temperature was estimated from the Z^{*2}/A systematics of Smith + /11/.

References

- 1) Igarasi S. and Nakagawa T. : JAERI-M7174 (1977).
- 2) Kikuchi Y. : JAERI-M82-096 (1982).
- 3) Tuttle R.J. : INDC(NDS)-107/G+Special , p.29 (1979).
- 4) Simpson O.D. et al. : Nucl.Sci.Eng.,55,273(1974)
- 5) Phillips T.W. and Howe R.E. : Nucl.Sci.Eng.,69,375 (1979).
- 6) Igarasi S. : J.Nucl.Sci.Technol.,12,67 (1975).
- 7) Lederer C.M. and Shirley V.S. : Table of Isotopes , 7th Ed.
- 8) Gilbert A. and Cameron A.G.W. : Can.J.Phys.,43,1446 (1965).
- 9) Behrens J.W. and Browne J.C. : Nucl.Sci.Eng.,77,444 (1981).
- 10) Seeger P.A. et al. : Nucl.Phys.,A96,605 (1967).
- 11) Smith A.B. : ANL/NDM-50 (1979).

96-Cm-242 MAT number = 2961

96-Cm-242 JAERI Eval-Mar79 S.Igarasi,T.Nakagawa
 JAERI-M 8342 (1979) Dist-Mar83 Rev1-Nov83

History

79-03 Evaluation was made by S.Igarasi and T.Nakagawa (JAERI) /1/.
 83-11 Comment was added.

MF=1 General Information

MT=451 Descriptive data

MT=452 Number of neutrons per fission

Based on the empirical formula by Howerton /2/

 $\bar{\nu} = 3.50 + 0.174E(\text{MeV})$

MT=455 Delayed neutron data

Estimated from the systematics by Tuttle /3/.

MF=2 Resonance Parameters

MT=151 Resonance parameters : Below 275 eV. Multi-level B-W.
 Parameters by Artamonov et al. /4/ plus one negative
 level at -3.45 eV. No fission width is given for all
 the resonances. Fission cross section in this region
 is assumed to be $1/v$ normalized to 5.0 barns at 0.0253
 eV.

Average $\Gamma_{\text{avg}} = 0.04$ eV

Effective scattering radius = 9.38 fm

Calculated 2200m/s cross sections and resonance integrals.

	2200 m/sec	Res. Integ.
capture	15.92 b	116 b
fission	5.00 b	11.1 b
elastic	11.61 b	-
total	32.53 b	-

MF=3 Neutron Cross Sections

MT=1,2,4,51-53,91,102,251 Sig-t,Sig-el,Sig-in,Sig-c,Mu-bar

Calculated with optical and statistical models.

The spherical optical potential parameters (MeV, fm) :

 $V = 43.4 - 0.107 * E$, $r = 1.282$, $a = 0.6$, $W_s = 6.95 - 0.339 * E + 0.0531 * E^2$, $r = 1.29$, $a = 0.5$, $V_{so} = 7.0$, $r = 1.282$, $a = 0.6$ This potential reproduces well the total cross section
of Am-241 by Phillips and Howe /5/

Statistical model calculation with CASTHY code /6/.

Competing processes : fission, (n,2n) and (n,3n).

Level fluctuation considered. $\Gamma_{\text{avg}} = 0.036$ eV and $D = 16$ eV used for capture cross section calculation.The level scheme taken from the compilation by Ellis
and Haese /7/:

No.	Energy (MeV)	Spin-Parity
g.s.	0.0	0 +
1	0.0422	2 +
2	0.138	4 +
3	0.284	6 +

Overlapping levels are assumed above 0.35 MeV.

The level density parameters of Gilbert and Cameron /8/.
 MT=16,17 (n,2n) and (n,3n) cross sections

Calculated with the evaporation model by Pearlstein /9/.

MT=18 Fission cross section

Determined from the evaluated fission cross section of Cm-244 /10/ and the empirical formula on the fission-cross-section systematics around 4 MeV by Behrens and Howerton /11/.

MF=4 Angular Distributions of Secondary Neutrons

MT=2 Calculated with the optical and statistical models.
 Legendre coefficients are given.

MT=51-53

Isotropic distributions in the center-of-mass system.

MT=16,17,18,91

Isotropic distributions in the laboratory system.

MF=5 Energy Distributions of Secondary Neutrons

MT=16,17,91 Evaporation spectrum.

MT=18 Estimated from $Z+2/A$ systematics by Smith et al. /12/,
 assuming $E(\text{Cf-252}) = 2.13$ MeV.

References

- 1) S. Igarasi and T. Nakagawa: JAERI-M 8342 (1979), in Japanese.
- 2) R.J. Howerton : Nucl. Sci. Eng. 62, 438 (1977).
- 3) R.J. Tuttle: INDC(NDS)-107/G+Special, 29 (1979).
- 4) V.S. Artamonov et al. : Proc. of 4th All Union Conf. on Neutron Physics, Kiev (1977), Vol. 2, 257.
- 5) T.W. Phillips and R.E. Howe : Nucl. Sci. Eng. 69, 375 (1979).
- 6) S. Igarasi : J.Nucl.Sci.Technol. 12, 67 (1975).
- 7) Y.A. Ellis and R.L. Haese : Nucl. Data Sheets 21, 615 (1977).
- 8) A. Gilbert and A.G.W. Cameron : Can. J. Phys. 43, 1446 (1965).
- 9) S. Pearlstein : J. Nucl. Energy 27, 81 (1973).
- 10) S. Igarasi and T. Nakagawa : JAERI-M 7175 (1977).
- 11) J.W. Behrens and R.J. Howerton : Nucl. Sci. Eng. 65, 464 (1978).
- 12) A.B. Smith et al. : ANL/NDM-50 (1979).

96-Cm-243 MAT number = 2962

96-Cm-243 JAERI Eval-Mar81 T.Nakagawa,S.Igarasi
 JAERI-M 9601 (1981) Dist-Mar83 Rev1-Apr84

History

81-03 Evaluation was made by T.Nakagawa and S.Igarasi (JAERI) /1/.
 83-11 Comment was added.
 84-04 The capture and total cross sections were corrected in the
 energy range from 27 eV to 1 keV.

MF=1 General Information

MT=451 Descriptive data

MT=452 Number of prompt neutrons per fission

Based on the experimental data at thermal energy by
 Jaffey and Lerner /2/, and Zhuravlev et al. /3/, and
 on the empirical formula by Howerton /4/.

$$\bar{\nu} = 3.43 + 0.178 * E (\text{MeV})$$

MT=455 Delayed neutron data

Estimated from the systematics by Tuttle /5/.

MF=2 Resonance Parameters

MT=151 Resonance parameters : Below 27 eV. Reich-Moore formula.
 Parameters by Berreth et al. /6/ plus one negative
 level at -0.7 eV.

Average $\Gamma_{\text{m-g}} = 0.04$ eV, level spacing = 2.2 eV,

$$\Gamma_{\text{m-n}} = 0.00041 \text{ eV}$$

S-wave strength function = 2.20×10^{-4}

Effective scattering radius = 9.81 fm

Calculated 2200m/s cross sections and resonance integrals.

	2200 m/sec	Res. Integ.
capture	131.3 b	436 b
fission	612.3 b	1750 b
elastic	9.658 b	-
total	753.3 b	-

MF=3 Neutron Cross Sections

Null value is given for the total, elastic scattering, capture
 and fission cross sections in the resonance region. The
 capture and elastic scattering cross sections from 27 eV to 1
 keV were estimated by assuming that the cross sections have
 the same structure as that of the fission cross section which
 was made by averaging the experimental data by Silbert /7/
 with Gaussian weight factor. Calculations were made by using
 the radius parameter of 9.81 fm, average fission and capture
 widths of 0.37 eV and 0.04 eV, respectively.

MT=1,2,4,51-64,91,102,251 Sig-t,Sig-el,Sig-in,Sig-c,Mu-bar
 Calculated with optical and statistical models above
 1 keV.

The spherical optical potential parameters (MeV, fm) :

$$V = 42.0 - 0.107 * E, \quad r = 1.282, a = 0.6,$$

$$W_s = 9.0 - 0.339 * E + 0.0531 * E * E^2, \quad r = 1.29, a = 0.5,$$

$$V_{so} = 7.0, \quad r = 1.282, a = 0.6$$

Statistical model calculation with CASTHY code /8/.
 Competing processes : fission, (n,2n), (n,3n) and (n,4n).
 Level fluctuation considered. $\Gamma_{\text{avg}} = 0.04$ eV and
 $D = 2.2$ eV used for capture cross section calculation.
 The level scheme taken from the compilation by Ellis /9/

No.	Energy (MeV)	Spin-Parity
g.s.	0.0	5/2 +
1	0.042	7/2 +
2	0.087	1/2 +
3	0.094	9/2 +
4	0.094	3/2 +
5	0.133	7/2 +
6	0.153	11/2 +
7	0.164	9/2 +
8	0.219	13/2 +
9	0.228	11/2 +
10	0.260	9/2 +
11	0.530	15/2 -
12	0.729	1/2 -
13	0.769	3/2 -
14	0.798	5/2 +

Overlapping levels are assumed above 0.82 MeV.
 The level density parameters of Gilbert and Cameron /10/
 were used.

MT=16,17,37 (n,2n), (n,3n) and (n,4n) cross sections
 Calculated with the evaporation model by Pearlstein/11/.
 MT=18 Fission cross section
 Smooth cross section above 1 keV was obtained by fitting
 a semi-empirical formula to the averaged experimental
 data.

MF=4 Angular Distributions of Secondary Neutrons
 MT=2,51-64,91
 Legendre coefficients calculated with CASTHY /8/.
 MT=16,17,18,37
 Isotropic distributions in the laboratory system.

MF=5 Energy Distributions of Secondary Neutrons
 MT=16,17,37,91 Evaporation Spectrum.
 MT=18 Fission spectrum estimated from Z^{*2}/A systematics by
 Smith et al. /12/ by assuming $E(\text{Cf-252}) = 2.13$ MeV.

References

- 1) T. Nakagawa and S. Igarasi: JAERI-M 9601 (1981).
- 2) A.H. Jaffey and J.L. Lerner : Nucl. Phys., A145, 1, (1970).
- 3) K.D. Zhuravlev et al. : Proc. 2nd Nat. Soviet Conf. on Neut. Phys., Vol.4, 57 (1974).
- 4) R.J. Howerton : Nucl. Sci. Eng., 62, 438 (1977).
- 5) R.J. Tuttle: INDC (NDS)-107/G+Special, 29 (1979).
- 6) J.R. Berreth et al. : Nucl. Sci. Eng., 49, 145 (1972).
- 7) M.G. Silbert : LA-6239 (1976).
- 8) S. Igarasi : J. Nucl. Sci. Technol., 12, 67 (1975).
- 9) Y.A. Ellis : Nucl. Data Sheets, 19, 103 (1976).
- 10) A. Gilbert and A.G.W. Cameron : Can. J. Phys., 43, 1446 (1965).
- 11) S. Pearlstein : J. Nucl. Energy 27, 81 (1973).

12) A.B. Smith et al. : ANL/NDM-50 (1979).

96-Cm-244 MAT number = 2963

96-Cm-244 JAERI Eval-Mar77 S.Igarasi,T.Nakagawa
 JAERI-M 7175 (1977) Dist-Mar83 Rev1-Nov83

History

77-03 Evaluation was made by S.Igarasi and T.Nakagawa (JAERI) /1/.
 83-11 Comment was added.

MF=1 General Information

MT=451 Descriptive data
 MT=452 Number of neutrons per fission
 Determined from semi-empirical formula by Howerton /2/.
 $\bar{\nu} = 3.24 + 0.184 * E(\text{MeV})$
 MT=455 Delayed neutron data
 Estimated from semi-empirical formula by Tuttle /3/.

MF=2 Resonance Parameters

MT=151 Resonance parameters : Below 1 keV. Multi-level B-W.
 Above 20 eV, parameters by Moore and Keyworth /4/ were
 adopted assuming neutron width of 0.2 eV for 646.9,
 759.7, 914.0 and 971.5-eV levels, and below 20 eV,
 evaluation by Benjamin et al. /5/. For fission and
 capture cross sections, background cross sections
 proportional to $1/v$ were added.

Calculated 2200m/s cross sections and resonance integrals.

	2200 m/sec	Res. Integ.
capture	14.41 b	594 b
fission	1.180 b	18.4 b
elastic	6.650 b	-
total	22.24 b	-

MF=3 Neutron Cross Sections

MT=1,2,4,51-58,91,102,251 Sig-t,Sig-el,Sig-in,Sig-c,Mu-bar
 Calculated with optical and statistical models above
 1 keV.

The spherical optical potential parameters (MeV, fm) :

$$V = 40.5 + 0.5 * E, \quad r = 1.32, \quad a = 0.47$$

$$W_s = 8.2 + 0.5 * E * 0.5, \quad r = 1.32, \quad a = 0.47$$

$$V_{so} = 7.0, \quad r = 1.32, \quad a = 0.47$$

Statistical model calculation with CASTHY code /6/.

Competing processes : fission, (n,2n) and (n,3n).

Level fluctuation considered. $\Gamma_{n-g} = 0.037$ eV and

$D = 14$ eV used for capture cross section calculation.

The level scheme taken from the compilation by Schmorak

/7/

No.	Energy (MeV)	Spin-Parity
g.s.	0.0	0 +
1	0.0429	2 +
2	0.1423	4 +
3	0.296	6 +
4	0.502	8 +
5	0.970	3 -

6	1.038	2	+
7	1.042	6	+
8	1.187	3	-

Overlapping levels are assumed above 1.2 MeV.

The level density parameters of Gilbert and Cameron /8/.

MT=16,17 (n,2n) and (n,3n) cross sections

Calculated with the evaporation model by Pearlstein /9/.

MT=18 Fission cross section

Smooth cross section above 1 keV was obtained by fitting a semi-empirical formula to the averaged experimental data.

MF=4 Angular Distributions of Secondary Neutrons

MT=2 Legendre coefficients are given by the optical and statistical model calculations.

MT=51-58 Isotropic distributions in the center-of-mass system.

MT=16,17,18,91

Isotropic distributions in the laboratory system.

MF=5 Energy Distributions of Secondary Neutrons

MT=16,17,91 Evaporation spectrum

MT=18 Fission spectrum estimated from Z^2/A systematics by Smith et al. /10/ by assuming $E(\text{Cf-252}) = 2.13$ MeV.

References

- 1) S. Igarasi and T. Nakagawa: JAERI-M 7175 (1977), in Japanese.
- 2) R.J. Howerton : Nucl. Sci. Eng., 62, 438 (1977).
- 3) R.J. Tuttle: INDC(NDS)-107/G+Special, 29 (1979).
- 4) M.S. Moore and G.A. Keyworth : Phys. Rev., C3, 1656 (1971).
- 5) R.W. Benjamin et al. : Nucl. Sci. Eng. 47, 203 (1972).
- 6) S. Igarasi : J. Nucl. Sci. Technol., 12, 67 (1975).
- 7) M.R. Schmorak : Nucl. Data Sheets, 17, 391 (1976).
- 8) A. Gilbert and A.G.W. Cameron : Can. J. Phys., 43, 1446 (1965).
- 9) S. Pearlstein : Nucl. Sci. Eng., 23, 238 (1965).
- 10) A.B. Smith et al. : ANL NDM-50 (1979).

96-Cm-245 MAT number = 2964

96-Cm-245 JAERI Eval-Mar78 S.Igarasi, T.Nakagawa
 JAERI-M 7733 (1978) Dist-Mar83 Rev1-Nov83

History

78-03 Evaluation was made by S.Igarasi and T.Nakagawa (JAERI) /1/.
 83-11 Comment was added.

MF=1 General Information

MT=451 Descriptive data

MT=452 Number of neutrons per fission

Based on the experimental data at thermal energy by
 Jaffey and Lerner /2/, Kroshkin and Zamyatnin /3/ and
 Zhuravlev et al. /4/. Energy dependent term was
 derived from the neutron separation energy.

$$\bar{\nu} = 3.83 + 0.18 \cdot E(\text{MeV})$$

MT=455 Delayed neutron data

Estimated from the systematics proposed by Tuttle /5/.

MF=2 Resonance Parameters

MT=151 Resonance parameters : Below 60 eV. Single-level B-W.
 Parameters by Moore and Keyworth /6/ were adopted above
 20 eV, and those by Browne et al. /7/ below 20 eV with
 a little modification of a negative resonance so that
 the thermal cross section could be in agreement with
 the experimental data. The differences between Reich-
 Moore and single-level B-W formulas are treated as the
 background cross sections.

$$\text{Average } \Gamma_{\text{avg}} = 0.04 \text{ eV}, \text{ Level spacing} = 1.8 \text{ eV},$$

$$S\text{-wave neutron strength function} = 1.0 \text{ E-4}$$

Calculated 2200m/s cross sections and resonance integrals.

	2200 m sec	Res. Integ.
capture	346.4 b	108 b
fission	2001. b	800 b
elastic	11.59 b	-
total	2359. b	-

MF=3 Neutron Cross Sections

MT=1,2,4,51-66,91,102,251 Sig-t, Sig-el, Sig-in, Sig-c, Mu-bar

Calculated with optical and statistical models above 60
 eV.

The spherical optical potential parameters (MeV, fm) :

$$V = 40.5 + 0.5 \cdot E, \quad r = 1.32, \quad a = 0.47$$

$$W_s = 8.2 + 0.5 \cdot E + 0.5, \quad r = 1.32, \quad a = 0.47$$

$$V_{so} = 7.0, \quad r = 1.32, \quad a = 0.47$$

Statistical model calculation with CASTHY code /8/.

Competing processes : fission (n,2n) and (n,3n).

Level fluctuation considered. $\Gamma_{\text{avg}} = 0.04 \text{ eV}$ and

$D = 14 \text{ eV}$ used for capture cross section calculation.

The level scheme taken from the compilation by Ellis /9/

No.	Energy (MeV)	Spin-Parity
g.s.	0.0	7/2 +

1	0.05473	9/2 +
2	0.1214	11/2 +
3	0.1971	13/2 +
4	0.25285	5/2 +
5	0.29584	7/2 +
6	0.3505	9/2 +
7	0.35595	1/2 +
8	0.3615	3/2 +
9	0.38795	9/2 -
10	0.4170	11/2 +
11	0.4188	5/2 +
12	0.431	7/2 +
13	0.4428	11/2 -
14	0.498	13/2 +
15	0.5087	13/2 -
16	0.532	9/2 +

Overlapping levels are assumed above 0.55 MeV.

The level density parameters of Gilbert and Cameron /10/ were used.

MT=16,17 (n,2n) and (n,3n) cross sections

Calculated with the evaporation model by Pearlstein /11/

MT=18 Fission cross section

Smooth cross section above 60 eV was obtained by fitting a semi-empirical formula to the averaged experimental data.

MF=4 Angular Distributions of Secondary Neutrons

MT=2 Legendre coefficients are given by the optical and statistical model calculations.

MT=51-66 Isotropic distributions in the center-of-mass system.

MT=16,17,18,91

Isotropic distributions in the laboratory system.

MF=5 Energy Distributions of Secondary Neutrons

MT=16,17,91 Evaporation spectrum

MT=18 Fission spectrum estimated from $Z \sim 42/A$ systematics by Smith et al. /12/ by assuming $E(\text{Cf-252}) = 2.13$ MeV.

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Appendix 1

Thermal and Fast Neutron Cross Sections

The 2200-m/sec and 14-MeV cross sections, resonance integrals, and Maxwellian and fission spectrum average cross sections were calculated from JENDL-2 (Rev1) pointwise data files. Details of the calculation are described in the text.

Nuclide	MAT	Reaction	Thermal cross sections			Fast cross sections		
			2200-m/s	Maxw. Avg.	Res. Integ	14-MeV	Fiss. Avg.	
1-H - 1	2011	total	20.77 b	20.74 b		691.9 mb	3.926 b	
		elastic	20.44 b	20.44 b		691.9 mb	3.926 b	
		capture	331.9 mb	294.1 mb	149.0 mb	29.83 μ b	39.27 μ b	
1-H - 2	2012	total	3.390 b	3.390 b		801.4 mb	2.537 b	
		elastic	3.389 b	3.390 b		624.2 mb	2.532 b	
		(n,2n) capture	Threshold energy = 550.0 μ b	3.339 MeV 487.3 μ b	286.2 μ b	177.1 mb 9.521 μ b	5.276 mb 7.076 μ b	
3-Li- 6	2031	total	937.0 b	830.5 b		1.247 b	1.908 b	
		elastic	735.9 mb	736.2 mb		709.9 mb	1.404 b	
		inelastic	Threshold energy =	1.718 MeV		434.6 mb	149.0 mb	
		(n,2n' α)	Threshold energy =	4.318 MeV		69.00 mb	176.2 μ b	
		capture	28.00 mb	24.81 mb	12.60 mb	1.190 μ b	4.257 μ b	
		(n,p) (n, α)	Threshold energy =	3.192 MeV 936.2 b	423.0 b	7.200 mb 25.74 mb	4.184 mb 350.3 mb	
3-Li- 7	2032	total	1.094 b	1.091 b		1.470 b	1.846 b	
		elastic	1.049 b	1.049 b		999.7 mb	1.643 b	
		inelastic	Threshold energy =	0.546 MeV		404.8 mb	203.0 mb	
		(n,2n)	Threshold energy =	8.300 MeV		22.00 mb	28.36 μ b	
		(n,2n' α)	Threshold energy =	10.000 MeV		33.00 mb	10.09 μ b	
		capture	45.40 mb	40.24 mb	20.42 mb	1.930 μ b	6.903 μ b	
(n,d)	Threshold energy =	8.880 MeV		10.00 mb	5.207 μ b			
4-Be- 9	2041	total	6.008 b	6.008 b		1.502 b	2.801 b	
		elastic	6.000 b	6.000 b		961.7 mb	2.639 b	
		(n,2n)	Threshold energy =	1.850 MeV		513.9 mb	125.4 mb	
		capture	7.600 mb	6.735 mb	3.419 mb	323.0 nb	1.156 μ b	
(n,p)	Threshold energy =	14.260 MeV			31.94 nb			

Nuclide	MAT	Reaction	Thermal cross sections			Fast cross sections		
			2200-m/s	Maxw. Avg.	Res. Integ	14-MeV	Fiss. Avg.	
4-Be-9	2041	(n,d)	Threshold energy =	16.300 MeV		19.88 nb		
		(n,t)	Threshold energy =	11.610 MeV		2.722 μ b		
		(n, α)	Threshold energy =	0.670 MeV		15.47 mb		
5-B-10	2051	total	3839. b	3403. b		1.450 b		2.611 b
		elastic	2.173 b	2.173 b		952.7 mb		2.101 b
		inelastic	Threshold energy =	0.789 MeV		285.4 mb		33.65 mb
		(n,2n)	Threshold energy =	9.285 MeV		26.44 μ b		316.3 nb
		capture	502.9 mb	445.7 mb	226.2 mb	21.38 μ b		76.47 μ b
		(n,p)	565.9 μ b	501.5 μ b	64.39 mb	32.80 mb		8.222 mb
		(n,d)	Threshold energy =	4.800 MeV		29.97 mb		1.134 mb
		(n, α)	3836. b	3400. b	1722. b	60.22 mb		433.7 mb
		(n,t 2 α)	565.9 μ b	501.5 μ b	234.1 mb	88.65 mb		32.63 mb
		6-C-12	2061	total	4.702 b	4.702 b		1.270 b
elastic	4.699 b			4.699 b		737.8 mb		2.358 b
inelastic	Threshold energy =			4.800 MeV		450.2 mb		10.86 mb
capture	3.400 mb			3.013 mb	1.530 mb	144.5 nb		516.9 nb
(n, α)	Threshold energy =			6.320 MeV		81.51 mb		1.206 mb
9-F-19	2091	total	3.651 b	3.652 b		1.768 b		3.537 b
		elastic	3.641 b	3.641 b		848.9 mb		2.191 b
		inelastic	Threshold energy =	0.116 MeV		496.3 mb		1.327 b
		(n,2n)	Threshold energy =	10.990 MeV		42.94 mb		8.615 μ b
		(n,n' α)	Threshold energy =	4.227 MeV		216.2 mb		2.009 mb
		(n,n' p)	Threshold energy =	8.418 MeV		72.80 mb		37.46 μ b
		capture	9.600 mb	8.519 mb	19.59 mb	25.66 μ b		213.4 μ b
		(n,p)	Threshold energy =	4.251 MeV		14.66 mb		1.163 mb
		(n,d)	Threshold energy =	6.075 MeV		39.50 mb		317.7 μ b
		(n,t)	Threshold energy =	7.957 MeV		15.00 mb		28.55 μ b

Nuclide	MAT	Reaction	Thermal cross sections			Fast cross sections	
			2200-m/s	Maxw. Avg.	Res. Integ	14-MeV	Fiss. Avg.
9-F-19	2091	(n,α)	Threshold energy = 1.603 MeV			21.34 mb	14.65 mb
11-Na-23	2111	total	3.700 b	3.673 b		1.690 b	3.132 b
		elastic	3.170 b	3.189 b		918.0 mb	2.581 b
		inelastic	Threshold energy = 0.458 MeV			565.9 mb	549.2 mb
		(n,2n)	Threshold energy = 12.960 MeV			18.00 mb	2.144 μb
		capture	529.9 mb	469.0 mb	329.0 mb	213.9 μb	274.5 μb
(n,p)				44.70 mb	1.205 mb		
(n,α)				142.9 mb	564.7 μb		
13-Al-27	2131	total	1.730 b	1.711 b		1.750 b	3.181 b
		elastic	1.500 b	1.500 b		925.5 mb	2.875 b
		inelastic	Threshold energy = 0.874 MeV			614.9 mb	301.9 mb
		(n,2n)	Threshold energy = 13.550 MeV			10.50 mb	4.861 μb
		capture	229.9 mb	203.7 mb	147.1 mb	427.2 μb	281.5 μb
		(n,p)				77.50 mb	3.775 mb
(n,α)				120.9 mb	732.2 μb		
14-Si-0	2140	total	2.356 b	2.347 b		1.800 b	3.029 b
		elastic	2.200 b	2.200 b		622.8 mb	2.786 b
		inelastic	Threshold energy = 1.319 MeV			752.8 mb	228.5 mb
		(n,2n)	Threshold energy = 8.769 MeV			8.026 mb	2.652 μb
		capture	155.9 mb	138.2 mb	78.83 mb	559.0 μb	524.3 μb
		(n,p)				255.4 mb	9.626 mb
(n,α)				160.1 mb	4.456 mb		
20-Ca-0	2200	total	3.396 b	3.357 b		2.268 b	2.906 b
		elastic	2.963 b	2.963 b		1.016 b	2.713 b
		inelastic	Threshold energy = 0.382 MeV			265.8 mb	59.32 mb
		(n,2n)	Threshold energy = 8.119 MeV			11.61 mb	3.097 μb

Nuclide	MAT	Reaction	Thermal cross sections			Fast cross sections	
			2200-m/s	Maxw. Avg.	Res. Integ	14-MeV	Fiss. Avg.
20-Ca- 0	2200	(n,n' α)		Threshold energy = 7.218 MeV		79.49 mb	14.92 μb
		(n,n' p)		Threshold energy = 8.540 MeV		542.8 mb	183.0 μb
		capture	430.6 mb	382.9 mb	226.1 mb	21.06 μb	2.130 mb
		(n,p)		Threshold energy = 0.543 MeV		204.4 mb	87.33 mb
		(n,α)	2.423 mb	2.172 mb	348.7 mb	138.4 mb	43.95 mb
		(n,2p)		Threshold energy = 8.317 MeV		9.694 mb	1.371 μb
20-Ca- 40	2201	total	3.423 b	3.385 b		2.263 b	3.525 b
		elastic	3.010 b	3.010 b		1.012 b	3.341 b
		inelastic			Threshold energy = 3.831 MeV		
		(n,2n)			Threshold energy = 16.030 MeV	248.8 mb	45.73 mb
		(n,n' α)			Threshold energy = 7.218 MeV	82.00 mb	15.39 μb
		(n,n' p)			Threshold energy = 8.540 MeV	559.9 mb	188.7 μb
		capture	409.9 mb	364.5 mb	215.8 mb	20.96 μb	2.132 mb
		(n,p)			Threshold energy = 0.543 MeV	209.9 mb	90.09 mb
		(n,α)	2.500 mb	2.241 mb	355.2 mb	140.0 mb	44.89 mb
		(n,2p)			Threshold energy = 8.317 MeV	10.00 mb	1.414 μb
20-Ca- 42	2202	total	1.910 b	1.839 b		2.352 b	3.757 b
		elastic	1.230 b	1.230 b		1.072 b	3.269 b
		inelastic			Threshold energy = 1.561 MeV	857.7 mb	423.5 mb
		(n,2n)			Threshold energy = 11.750 MeV	120.0 mb	20.48 μb
		capture	679.9 mb	604.8 mb	383.8 mb	57.79 μb	3.421 mb
		(n,α)	252.8-12 b	505.8-12 b	535.0 mb	301.9 mb	59.82 mb
20-Ca- 43	2203	total	9.197 b	8.515 b		2.397 b	3.745 b
		elastic	2.997 b	2.997 b		1.104 b	3.036 b
		inelastic			Threshold energy = 0.382 MeV	395.4 mb	664.1 mb
		(n,2n)			Threshold energy = 8.119 MeV	569.9 mb	513.3 μb
		capture	6.200 b	5.515 b	3.202 b	28.09 μb	4.971 mb

Nuclide	MAT	Reaction	Thermal cross sections			Fast cross sections		
			2200-m/s	Maxw.Avg.	Res.Integ	14-MeV	Fiss.Avg.	
20-Ca-43	2203	(n,p)		Threshold energy = 1.059 MeV		95.24 mb	336.7 μ b	
		(n, α)	0.0 b	0.0 b	369.9 mb	232.0 mb	34.69 mb	
20-Ca-44	2204	total	2.203 b	2.109 b		2.441 b	3.651 b	
		elastic	1.323 b	1.323 b		1.136 b	3.114 b	
		inelastic		Threshold energy = 1.184 MeV		846.0 mb	534.4 mb	
		(n,2n)		Threshold energy = 11.390 MeV		400.0 mb	74.30 μ b	
		capture	879.8 mb	782.4 mb	428.7 mb	15.42 μ b	1.591 mb	
(n,p)			Threshold energy = 4.988 MeV		34.52 mb	81.96 μ b		
	(n, α)		Threshold energy = 2.815 MeV		23.89 mb	58.07 μ b		
20-Ca-46	2205	total	3.640 b	3.569 b		2.527 b	3.932 b	
		elastic	2.900 b	2.900 b		1.202 b	3.487 b	
		inelastic		Threshold energy = 1.377 MeV		664.7 mb	443.0 mb	
		(n,2n)		Threshold energy = 10.630 MeV		650.0 mb	167.4 μ b	
		capture	739.9 mb	655.7 mb	339.0 mb	896.5 mb	172.1 μ b	
(n,p)		Threshold energy = 7.088 MeV		6.600 mb	2.525 μ b			
(n, α)		Threshold energy = 5.632 MeV		4.000 mb	66.88 μ b			
20-Ca-48	2206	total	3.990 b	3.876 b		2.613 b	3.745 b	
		elastic	2.900 b	2.900 b		1.269 b	3.654 b	
		inelastic		Threshold energy = 3.912 MeV		443.7 mb	89.13 mb	
		(n,2n)		Threshold energy = 10.150 MeV		900.0 mb	325.2 μ b	
		capture	1.090 b	967.2 mb	491.4 mb	1.349 μ b	392.5 μ b	
(n,p)		Threshold energy = 11.450 MeV		112.0 μ b	41.15 mb			
21-Sc-45	2211	total	51.05 b	48.18 b		2.131 b	3.193 b	
		elastic	25.03 b	25.03 b		1.129 b	2.479 b	
		inelastic		Threshold energy = 0.013 MeV		641.7 mb	679.3 mb	
(n,2n)		Threshold energy = 11.580 MeV		245.0 mb	39.25 μ b			

Nuclide	MAT	Reaction	Thermal cross sections			Fast cross sections		
			2200-m/s	Maxw. Avg.	Res. Integ	14-MeV	Fiss. Avg.	
21-Sc- 45	2211	capture	26.02 b	23.15 b	11.32 b	55.26 μ b	5.916 mb	
		(n,p)	0.0 b	0.0 b	168.3 mb	59.00 mb	25.64 mb	
		(n, α)	Threshold energy = 0.406 MeV			56.00 mb	2.518 mb	
23-V - 51	2231	total	9.705 b	9.264 b		2.288 b	3.956 b	
		elastic	4.805 b	4.902 b		936.3 mb	3.144 b	
		inelastic	Threshold energy = 0.326 MeV			735.8 mb	809.1 mb	
		(n,2n)	Threshold energy = 11.270 MeV			544.9 mb	96.39 μ b	
		(n,n' α)	Threshold energy = 10.500 MeV			300.0 μ b	107.5 nb	
		(n,n' p)	Threshold energy = 8.211 MeV			13.00 mb	5.293 μ b	
		capture	4.900 b	4.361 b	2.534 b	26.80 μ b	2.210 mb	
		(n,p)	Threshold energy = 1.708 MeV			36.50 mb	514.5 μ b	
		(n,d)	Threshold energy = 5.941 MeV			4.500 mb	6.695 μ b	
		(n,t)	Threshold energy = 10.720 MeV			1.000 mb	324.5 nb	
		(n, α)	0.0 b	0.0 b	10.89 mb	15.00 mb	175.2 μ b	
24-Cr- 0	2240	total	6.900 b	6.565 b		2.380 b	3.332 b	
		elastic	3.830 b	3.830 b		1.206 b	2.888 b	
		inelastic	Threshold energy = 0.575 MeV			695.9 mb	440.1 mb	
		(n,2n)	Threshold energy = 8.092 MeV			324.4 mb	101.1 μ b	
		(n,n' p)	Threshold energy = 9.782 MeV			13.87 mb	5.768 μ b	
		capture	3.070 b	2.730 b	1.600 b	97.69 μ b	3.141 mb	
		(n,p)	Threshold energy = 0.257 MeV			106.3 mb	978.2 μ b	
(n, α)	0.0 b	0.0 b	37.92 mb	33.22 mb	138.2 μ b			
24-Cr- 50	2241	total	24.48 b	22.74 b		2.310 b	3.272 b	
		elastic	8.581 b	8.581 b		1.142 b	2.726 b	
		inelastic	Threshold energy = 0.799 MeV			341.8 mb	535.6 mb	
		(n,2n)	Threshold energy = 13.200 MeV			8.200 mb	1.805 μ b	
		(n,n' p)	Threshold energy = 9.782 MeV			285.9 mb	37.87 μ b	

Nuclide	MAT	Reaction	Thermal cross sections			Fast cross sections	
			2200-m/s	Maxw. Avg.	Res. Integ	14-MeV	Fiss. Avg.
24-Cr-50	2241	capture	15.90 b	14.14 b	7.765 b	118.4 μ b	7.836 mb
		(n,p) (n, α)	Threshold energy = 0.262 MeV			437.9 mb	2.980 mb
24-Cr-52	2242	total	2.983 b	2.901 b		2.369 b	3.377 b
		elastic	2.223 b	2.223 b		1.195 b	2.964 b
		inelastic	Threshold energy = 1.462 MeV			783.2 mb	409.2 mb
		(n,2n)	Threshold energy = 12.270 MeV			259.9 mb	31.72 μ b
		(n,n' p)	Threshold energy = 10.710 MeV			1.700 mb	4.844 μ b
		capture	759.8 mb	675.8 mb	492.9 mb	84.45 μ b	2.888 mb
(n,p)		Threshold energy = 3.258 MeV			99.60 mb	1.005 mb	
	(n, α)	Threshold energy = 1.234 MeV			30.10 mb	149.5 μ b	
24-Cr-53	2243	total	34.51 b	32.54 b		2.390 b	3.506 b
		elastic	16.31 b	16.31 b		1.220 b	2.877 b
		inelastic	Threshold energy = 0.575 MeV			224.5 mb	625.7 mb
		(n,2n)	Threshold energy = 8.092 MeV			869.9 mb	704.9 μ b
		(n,n' p)	Threshold energy = 11.350 MeV			3.000 μ b	646.0 nb
		capture	18.20 b	16.19 b	8.859 b	13.69 μ b	2.220 mb
(n,p)		Threshold energy = 2.691 MeV			36.70 mb	70.76 μ b	
	(n, α)	0.0 b	0.0 b	34.14 mb	38.50 mb	76.41 μ b	
24-Cr-54	2244	total	2.274 b	2.235 b		2.420 b	3.367 b
		elastic	1.914 b	1.914 b		1.245 b	2.760 b
		inelastic	Threshold energy = 0.851 MeV			150.4 mb	605.6 mb
		(n,2n)	Threshold energy = 9.902 MeV			1.000 b	316.8 μ b
		capture	359.9 mb	320.0 mb	193.1 mb	19.37 μ b	1.831 mb
		(n,p)	Threshold energy = 6.336 MeV			13.20 mb	5.486 μ b
(n, α)	Threshold energy = 1.575 MeV			10.60 mb	4.953 μ b		

Nuclide	MAT	Reaction	Thermal cross sections			Fast cross sections	
			2200-m/s	Maxw.Avg.	Res.Integ	14-MeV	Fiss.Avg.
25-Mn-55	2251	total	15.50 b	14.03 b		2.673 b	3.648 b
		elastic	2.184 b	2.184 b		1.401 b	2.806 b
		inelastic			Threshold energy = 0.128 MeV	415.5 mb	836.7 mb
		(n,2n)			Threshold energy = 10.420 MeV	770.9 mb	208.0 μb
		(n,n'α)			Threshold energy = 8.081 MeV	3.440 mb	2.752 μb
		(n,n'p)			Threshold energy = 8.216 MeV	9.510 mb	3.847 μb
		capture			13.32 b 11.84 b 14.63 b	664.9 μb	2.924 mb
(n,p)			Threshold energy = 1.855 MeV	46.90 mb	1.325 mb		
(n,α)			Threshold energy = 0.636 MeV	24.60 mb	202.5 μb		
26-Fe-56	2260	total	14.95 b	14.69 b		2.520 b	3.180 b
		elastic	12.44 b	12.41 b		1.245 b	2.521 b
		inelastic			Threshold energy = 0.015 MeV	621.3 mb	649.3 mb
		(n,2n)			Threshold energy = 7.775 MeV	422.4 mb	106.6 μb
		capture	2.514 b	2.279 b	1.349 b	147.8 μb	3.452 mb
		(n,p)	0.0 b	0.0 b	119.5 mb	125.4 mb	5.313 mb
		(n,α)	0.0 b	0.0 b	95.97 mb	105.2 mb	1.273 mb
26-Fe-54	2261	total	2.649 b	2.411 b		2.374 b	3.331 b
		elastic	492.8 mb	492.8 mb		1.198 b	2.775 b
		inelastic			Threshold energy = 1.435 MeV	704.2 mb	473.8 mb
		(n,2n)			Threshold energy = 13.870 MeV	3.230 mb	1.906 μb
		capture	2.156 b	1.918 b	1.328 b	452.1 μb	6.415 mb
		(n,p)	0.0 b	0.0 b	755.9 mb	359.9 mb	74.29 mb
		(n,α)	0.0 b	0.0 b	98.45 mb	108.0 mb	1.306 mb
26-Fe-56	2262	total	15.27 b	14.96 b		2.485 b	3.191 b
		elastic	12.46 b	12.46 b		1.196 b	2.534 b
		inelastic			Threshold energy = 0.862 MeV	626.6 mb	650.8 mb
		(n,2n)			Threshold energy = 11.400 MeV	439.9 mb	75.44 μb

Nuclide	MAT	Reaction	Thermal cross sections			Fast cross sections		
			2200-m/s	Maxw. Avg.	Res. Integ	14-MeV	Fiss. Avg.	
26-Fe-56	2262	capture (n,p)	2.813 b	2.502 b	1.444 b	129.9 μ b	3.236 mb	
		capture (n, α)	Threshold energy = 0.0 b	0.0 b	98.45 mb	113.9 mb	1.079 mb	
26-Fe-57	2263	total	2.664 b	2.393 b		2.522 b	3.649 b	
		elastic	202.1 mb	202.1 mb		1.377 b	2.484 b	
		inelastic (n,2n)	Threshold energy = 0.015 MeV			274.0 mb	1.160 b	
		capture	Threshold energy = 7.775 MeV			869.9 mb	1.707 mb	
			2.462 b	2.190 b	1.452 b	116.9 μ b	4.215 mb	
26-Fe-58	2264	total	4.101 b	3.964 b		2.636 b	3.767 b	
		elastic	2.821 b	2.821 b		1.267 b	3.150 b	
		inelastic (n,2n)	Threshold energy = 0.825 MeV			361.5 mb	615.2 mb	
		capture	Threshold energy = 10.210 MeV			976.9 mb	310.1 μ b	
		(n,p)	1.280 b	1.139 b	1.828 b	40.24 μ b	1.634 mb	
		(n, α)	Threshold energy = 5.413 MeV			15.00 mb	5.584 μ b	
			Threshold energy = 1.414 MeV		15.00 mb	30.68 μ b		
27-Co-59	2271	total	43.18 b	39.07 b		2.775 b	3.800 b	
		elastic	6.001 b	6.001 b		1.573 b	3.391 b	
		inelastic (n,2n)	Threshold energy = 1.118 MeV			486.2 mb	399.2 mb	
		capture	Threshold energy = 10.630 MeV			639.9 mb	170.7 μ b	
		(n,p)	37.18 b	33.07 b	75.65 b	79.08 μ b	7.760 mb	
		(n, α)	Threshold energy = 0.796 MeV			45.90 mb	1.321 mb	
			0.0 b	0.0 b	19.79 mb	30.00 mb	164.8 μ b	
28-Ni-0	2280	total	21.20 b	20.71 b		2.716 b	3.633 b	
		elastic	16.77 b	16.77 b		1.386 b	3.115 b	
		inelastic (n,2n)	Threshold energy = 0.069 MeV			390.7 mb	434.6 mb	
		capture	Threshold energy = 7.950 MeV			162.0 mb	46.72 μ b	

Nuclide	MAT	Reaction	Thermal cross sections			Fast cross sections	
			2200-m/s	Maxw. Avg.	Res. Integ	14-MeV	Fiss. Avg.
28-Ni-0	2280	(n,3n)		Threshold energy = 16.760 MeV		20.36 mb	1.737 nb
		(n,n' α)		Threshold energy = 6.509 MeV		341.7 mb	5.132 μb
		(n,n' p)		Threshold energy = 8.313 MeV		97.08 μb	7.940 mb
		capture	4.429 b	3.939 b	2.221 b	307.8 mb	71.04 mb
		(n,p)	0.0 b	0.0 b	627.0 mb	106.8 mb	4.418 mb
		(n,α)	2.4-12 b	4.9-12 b	115.5 mb		
28-Ni-58	2281	total	30.62 b	30.12 b		2.662 b	3.889 b
		elastic	26.02 b	26.02 b		1.351 b	3.400 b
		inelastic		Threshold energy = 1.480 MeV		248.8 mb	370.2 mb
		(n,2n)		Threshold energy = 12.410 MeV		21.50 mb	2.752 μb
		(n,n' α)		Threshold energy = 6.509 MeV		30.00 mb	7.561 μb
		(n,n' p)		Threshold energy = 8.313 MeV		479.9 mb	100.2 μb
		capture	4.605 b	4.096 b	2.206 b	66.88 μb	8.743 mb
		(n,p)	0.0 b	0.0 b	870.8 mb	400.0 mb	103.3 mb
		(n,α)	3.5-12 b	7.0-12 b	149.5 mb	130.9 mb	6.113 mb
		28-Ni-60	2282	total	3.813 b	3.503 b	
elastic	1.013 b			1.013 b		1.398 b	3.135 b
inelastic				Threshold energy = 1.355 MeV		737.8 mb	549.0 mb
(n,2n)				Threshold energy = 11.580 MeV		370.5 mb	58.59 μb
(n,n' p)				Threshold energy = 9.693 MeV		60.00 mb	9.007 μb
capture	2.801 b			2.490 b	1.503 b	56.11 μb	5.030 mb
(n,p)				Threshold energy = 2.075 MeV		130.9 mb	3.187 mb
(n,α)	151.6-15 b			303.4-15 b	48.24 mb	63.00 mb	838.2 μb
28-Ni-61	2283	total	12.12 b	11.84 b		2.814 b	3.814 b
		elastic	9.611 b	9.611 b		1.501 b	2.723 b
		inelastic		Threshold energy = 0.069 MeV		319.9 mb	1.078 b
		(n,2n)		Threshold energy = 7.950 MeV		843.4 mb	1.432 mb

Nuclide	MAT	Reaction	Thermal cross sections			Fast cross sections	
			2200-m/s	Maxw. Avg.	Res. Integ	14-MeV	Fiss. Avg.
28-Ni-61	2283	(n,n' p) capture	Threshold energy = 10.020 MeV			7.400 mb	1.137 μ b
		(n,p)	2.506 b	2.229 b	2.438 b	29.40 μ b	5.621 mb
		(n, α)	758.7-15 b	1.5-12 b	62.91 mb	97.00 mb	1.507 mb
28-Ni-62	2284	total	23.70 b	22.14 b		2.869 b	3.810 b
		elastic	9.505 b	9.505 b		1.475 b	3.211 b
		inelastic	Threshold energy = 1.192 MeV			578.8 mb	594.8 mb
		(n,2n)	Threshold energy = 10.770 MeV			771.2 mb	185.3 μ b
		(n,n' p) capture	Threshold energy = 11.320 MeV			700.0 μ b	1.047 μ b
		(n,p)	14.20 b	12.64 b	6.908 b	19.63 μ b	3.526 mb
(n, α)		Threshold energy = 4.532 MeV			23.00 mb	73.33 μ b	
		Threshold energy = 0.444 MeV			20.20 mb	73.38 μ b	
28-Ni-64	2285	total	1.515 b	1.351 b		2.984 b	3.982 b
		elastic	34.64 mb	34.64 mb		1.546 b	3.513 b
		inelastic	Threshold energy = 1.367 MeV			312.7 mb	466.2 mb
		(n,2n)	Threshold energy = 9.809 MeV			1.115 b	524.7 μ b
		(n,3n)	Threshold energy = 16.760 MeV				160.8 nb
		capture	1.480 b	1.317 b	819.3 mb	2.633 μ b	2.731 mb
(n,p)	Threshold energy = 6.627 MeV			4.500 mb	3.415 μ b		
(n, α)	Threshold energy = 2.480 MeV			5.700 mb	6.911 μ b		
29-Cu-0	2290	total	11.63 b	11.22 b		3.132 b	4.048 b
		elastic	7.859 b	7.858 b		1.623 b	3.385 b
		inelastic	Threshold energy = 0.680 MeV			812.8 mb	653.2 mb
		(n,2n)	Threshold energy = 10.060 MeV			650.4 mb	153.2 μ b
		(n,n' α) capture	Threshold energy = 5.870 MeV			11.99 mb	3.501 μ b
		(n,p)	3.775 b	3.358 b	4.397 b	82.65 μ b	9.872 mb
		Threshold energy = 1.376 MeV			6.489 mb	188.6 μ b	

Nuclide	MAT	Reaction	Thermal cross sections			Fast cross sections	
			2200-m/s	Maxw. Avg.	Res. Integ	14-MeV	Fiss. Avg.
29-Cu-0	2290	(n,α)	0.0	0.0	23.17 mb	26.95 mb	379.3 μb
29-Cu-63	2291	total elastic inelastic (n,2n) (n,n'α) capture (n,α)	9.471 b 4.979 b Threshold energy = 0.680 MeV Threshold energy = 11.030 MeV Threshold energy = 5.870 MeV 4.492 b 0.0 b	8.975 b 4.979 b		3.105 b 1.602 b 917.2 mb 529.9 mb 17.00 mb 111.2 μb 39.00 mb	4.060 b 3.374 b 674.2 mb 85.27 μb 4.937 μb 11.28 mb 548.9 μb
29-Cu-65	2292	total elastic inelastic (n,2n) (n,n'α) capture (n,p)	16.47 b 14.30 b Threshold energy = 0.783 MeV Threshold energy = 10.060 MeV Threshold energy = 6.895 MeV 2.170 b Threshold energy = 1.376 MeV	16.23 b 14.30 b		3.191 b 1.670 b 579.2 mb 919.9 mb 800.0 μb 18.73 μb 21.00 mb	4.024 b 3.409 b 606.1 mb 305.0 μb 288.0 nb 6.711 mb 610.7 μb
41-Nb-93	2411	total elastic inelastic (n,2n) (n,3n) capture (n,p) (n,α)	7.477 b 6.326 b Threshold energy = 0.031 MeV Threshold energy = 8.928 MeV Threshold energy = 16.900 MeV 1.152 b 0.0 b 0.0 b	7.350 b 6.325 b		4.190 b 2.410 b 497.0 mb 1.250 b 6.177 μb 25.00 mb 8.850 mb	5.668 b 4.549 b 1.082 b 1.174 mb 203.3 nb 31.38 mb 1.173 mb 271.8 μb
42-Mo-0	2420	total elastic inelastic	8.037 b 5.486 b Threshold energy = 0.206 MeV	7.753 b 5.485 b		4.192 b 2.433 b 585.6 mb	5.683 b 4.619 b 1.022 b

Nuclide	MAT	Reaction	Thermal cross sections			Fast cross sections	
			2200-m/s	Maxw. Avg.	Res. Integ	14-MeV	Fiss. Avg.
42-Mo-92	2420	(n,2n)	Threshold energy =	6.892 MeV		1.136 b	1.655 mb
		(n,3n)	Threshold energy =	14.360 MeV			169.7 nb
		capture	2.551 b	2.268 b	25.42 b	87.27 μ b	37.54 mb
		(n,p)	0.0 b	0.0 b	29.52 mb	25.65 mb	1.877 mb
		(n, α)	0.0 b	0.0 b	8.136 mb	11.36 mb	217.6 μ b
42-Mo-92	2421	total	5.566 b	5.564 b		4.190 b	5.663 b
		elastic	5.545 b	5.545 b		2.550 b	5.095 b
		inelastic	Threshold energy =	1.526 MeV		1.491 b	523.7 mb
		(n,2n)	Threshold energy =	12.820 MeV		64.30 mb	21.48 μ b
		capture	20.75 mb	18.46 mb	980.7 mb	191.9 μ b	32.67 mb
		(n,p)	0.0 b	0.0 b	110.6 mb	61.40 mb	10.99 mb
		(n, α)	0.0 b	0.0 b	16.36 mb	26.90 mb	355.1 μ b
42-Mo-94	2422	total	6.011 b	6.010 b		4.190 b	5.664 b
		elastic	5.998 b	5.998 b		2.413 b	4.755 b
		inelastic	Threshold energy =	0.880 MeV		717.0 mb	864.2 mb
		(n,2n)	Threshold energy =	9.785 MeV		1.010 b	561.4 μ b
		(n,3n)	Threshold energy =	17.940 MeV			4.599 nb
		capture	13.11 mb	11.66 mb	1.425 b	177.3 μ b	42.20 mb
		(n,p)	Threshold energy =	1.276 MeV		35.10 mb	541.0 μ b
(n, α)	0.0 b	0.0 b	8.588 mb	15.50 mb	374.7 μ b		
42-Mo-95	2423	total	19.58 b	18.02 b		4.190 b	5.667 b
		elastic	5.586 b	5.584 b		2.385 b	4.354 b
		inelastic	Threshold energy =	0.206 MeV		326.9 mb	1.258 b
		(n,2n)	Threshold energy =	7.450 MeV		1.440 b	2.529 mb
		(n,3n)	Threshold energy =	17.230 MeV			88.92 nb
		capture	13.99 b	12.44 b	118.6 b	8.643 μ b	49.47 mb
(n,p)	Threshold energy =	0.145 MeV		26.80 mb	403.5 μ b		

Nuclide	MAT	Reaction	Thermal cross sections			Fast cross sections	
			2200-m/s	Maxw. Avg.	Res. Integ	14-MeV	Fiss. Avg.
42-Mo-95	2423	(n,α)	0.0 b	0.0 b	9.620 mb	11.90 mb	163.2 μb
42-Mo-96	2424	total	5.322 b	5.257 b		4.191 b	5.665 b
		elastic	4.727 b	4.727 b		2.413 b	4.646 b
		inelastic			Threshold energy = 0.787 MeV	487.7 mb	979.5 mb
		(n,2n)			Threshold energy = 9.251 MeV	1.260 b	930.9 μb
		(n,3n)			Threshold energy = 16.700 MeV		59.47 nb
42-Mo-97	2425	capture	595.3 mb	529.7 mb	17.59 b	56.81 μb	36.65 mb
		(n,p)			Threshold energy = 2.430 MeV	20.50 mb	86.89 μb
		(n,α)	0.0 b	0.0 b	9.511 mb	9.170 mb	483.7 μb
42-Mo-98	2426	total	7.953 b	7.720 b		4.191 b	5.668 b
		elastic	5.853 b	5.853 b		2.418 b	4.341 b
		inelastic			Threshold energy = 0.486 MeV	310.5 mb	1.271 b
		(n,2n)			Threshold energy = 6.892 MeV	1.440 b	4.180 mb
		(n,3n)			Threshold energy = 16.140 MeV		324.4 nb
		capture	2.100 b	1.867 b	17.25 b	7.816 μb	48.67 mb
42-Mo-99	2427	(n,p)			Threshold energy = 1.162 MeV	15.90 mb	63.31 μb
		(n,α)	0.0 b	0.0 b	3.959 mb	7.100 mb	52.35 μb
		total	5.772 b	5.757 b		4.191 b	5.663 b
		elastic	5.642 b	5.642 b		2.415 b	4.589 b
		inelastic			Threshold energy = 0.743 MeV	338.0 mb	1.040 b
42-Mo-100	2427	(n,2n)			Threshold energy = 8.732 MeV	1.420 b	1.840 mb
		(n,3n)			Threshold energy = 15.620 MeV		414.9 nb
		capture	129.9 mb	115.5 mb	6.558 b	83.71 μb	31.71 mb
		(n,p)			Threshold energy = 3.842 MeV	12.30 mb	11.61 μb
(n,α)	0.0 b	0.0 b	4.496 mb	5.530 mb	68.56 μb		
		total	5.499 b	5.477 b		4.191 b	5.666 b

Nuclide	MAT	Reaction	Thermal cross sections			Fast cross sections		
			2200-m/s	Maxw. Avg.	Res. Integ	14-MeV	Fiss. Avg.	
42-Mo-100	2427	elastic	5.300 b	5.300 b		2.429 b	4.449 b	
		inelastic			Threshold energy = 0.541 MeV	444.4 mb	1.187 b	
		(n,2n)			Threshold energy = 8.375 MeV	1.310 b	2.249 mb	
		(n,3n)			Threshold energy = 14.360 MeV		167.2 nb	
		capture			199.0 mb	176.9 mb	3.922 b	26.52 mb
(n,p)			Threshold energy = 5.501 MeV		7.500 mb	5.042 μ b		
(n, α)			0.0 b	0.0 b	2.491 mb	3.400 mb	6.478 μ b	
72-Hf-174	2721	total	397.9 b	353.4 b		5.673 b	6.991 b	
		elastic	8.000 b	8.000 b		3.249 b	4.988 b	
		inelastic			Threshold energy = 0.092 MeV	1.333 b	1.633 b	
		(n,2n)			Threshold energy = 8.682 MeV	1.089 b	284.2 μ b	
		(n,3n)			Threshold energy = 15.730 MeV		35.69 nb	
		capture			389.9 b	345.3 b	491.7 b	365.7 mb
		(n,p)			0.0 b	0.0 b	2.177 mb	12.39 μ b
(n, α)			0.0 b	0.0 b	335.3 μ b	4.761 μ b		
72-Hf-176	2722	total	46.00 b	41.68 b		5.672 b	6.987 b	
		elastic	8.000 b	8.000 b		3.222 b	5.038 b	
		inelastic			Threshold energy = 0.089 MeV	521.3 mb	1.635 b	
		(n,2n)			Threshold energy = 8.137 MeV	1.928 b	2.426 mb	
		(n,3n)			Threshold energy = 14.970 MeV		842.2 nb	
		capture			38.00 b	33.61 b	359.8 b	307.7 mb
(n,p)			Threshold energy = 0.406 MeV		1.183 mb	2.653 μ b		
(n, α)			0.0 b	0.0 b	75.74 μ b	1.102 μ b		
72-Hf-177	2723	total	358.9 b	331.8 b		5.678 b	6.984 b	
		elastic	7.000 b	6.991 b		3.253 b	4.806 b	
		inelastic			Threshold energy = 0.114 MeV	306.6 mb	1.821 b	
(n,2n)			Threshold energy = 6.420 MeV	2.118 b	7.847 mb			

Nuclide	MAT	Reaction	Thermal cross sections			Fast cross sections		
			2200-m/s	Maxw. Avg.	Res. Integ	14-MeV	Fiss. Avg.	
72-Hf-177	2723	(n,3n) capture	Threshold energy = 14.560 MeV			2.252 μ b		
		(n,p)	351.9 b	324.7 b	6948. b	2.318 μ b	344.3 mb	
		(n, α)	0.0 b	0.0 b	732.3 μ b	769.0 μ b	2.463 μ b	
72-Hf-178	2724	total	91.00 b	78.88 b		5.667 b	6.988 b	
		elastic	5.000 b	4.999 b		3.199 b	5.106 b	
		inelastic	Threshold energy = 0.094 MeV			448.4 mb	1.803 b	
		(n,2n)	Threshold energy = 7.670 MeV			2.019 b	3.315 mb	
		(n,3n)	Threshold energy = 14.090 MeV				3.539 μ b	
		capture	86.00 b	73.59 b	1916. b	757.7 nb	72.12 mb	
72-Hf-179	2725	(n,p)	Threshold energy = 1.359 MeV			605.0 μ b	584.8 nb	
		(n, α)	0.0 b	0.0 b	20.92 μ b	19.80 μ b	94.08 nb	
72-Hf-179	2725	total	51.00 b	45.92 b		5.672 b	6.985 b	
		elastic	6.000 b	6.000 b		3.220 b	4.929 b	
		inelastic	Threshold energy = 0.123 MeV			368.0 mb	1.925 b	
		(n,2n)	Threshold energy = 6.134 MeV			2.084 b	7.487 mb	
		(n,3n)	Threshold energy = 13.800 MeV			0.0 b	4.035 μ b	
		capture	45.00 b	39.86 b	516.7 b	235.6 nb	119.5 mb	
72-Hf-180	2726	(n,p)	Threshold energy = 0.573 MeV			51.00 μ b	64.34 nb	
		(n, α)	0.0 b	0.0 b	7.419 μ b	6.400 μ b	61.45 nb	
72-Hf-180	2726	total	32.00 b	31.07 b		5.667 b	6.986 b	
		elastic	19.40 b	19.85 b		3.161 b	5.132 b	
		inelastic	Threshold energy = 0.094 MeV			219.8 mb	1.811 b	
		(n,2n)	Threshold energy = 7.430 MeV			2.286 b	5.379 mb	
		(n,3n)	Threshold energy = 13.560 MeV			0.0 b	5.813 μ b	
		capture	12.60 b	11.16 b	34.59 b	803.0 nb	34.72 mb	
		(n,p)	Threshold energy = 2.329 MeV			54.70 μ b	28.75 nb	

Nuclide	MAT	Reaction	Thermal cross sections			Fast cross sections	
			2200-m/s	Maxw. Avg.	Res. Integ	14-MeV	Fiss. Avg.
72-Hf-180	2726	(n,α)	0.0 b	0.0 b	21.83 μb	19.40 μb	39.01 nb
73-Ta-181	2731	total	27.32 b	25.03 b		5.370 b	6.992 b
		elastic	6.110 b	6.101 b		3.012 b	4.944 b
		inelastic	Threshold energy = 0.006 MeV			102.3 mb	1.949 b
		(n,2n)	Threshold energy = 7.683 MeV			2.252 b	6.467 mb
		capture	21.21 b	18.93 b	743.4 b	209.4 nb	91.22 mb
		(n,p)	Threshold energy = 0.242 MeV			4.128 mb	454.7 nb
82-Pb-0	2820	total	11.59 b	11.58 b		5.419 b	6.346 b
		elastic	11.42 b	11.42 b		2.915 b	5.658 b
		inelastic	Threshold energy = 0.573 MeV			580.1 mb	684.6 mb
		(n,2n)	Threshold energy = 6.772 MeV			1.921 b	1.476 mb
		(n,3n)	Threshold energy = 14.180 MeV				578.5 nb
		(n,n' α)	0.0 b	0.0 b	4.252 mb	254.9 μb	128.7 nb
		(n,n' p)	Threshold energy = 6.670 MeV			32.43 μb	30.29 nb
		capture	171.6 mb	152.5 mb	147.6 mb	577.0 μb	1.741 mb
		(n,p)	0.0 b	0.0 b	891.9 μb	969.7 μb	417.4 nb
		(n,α)	0.0 b	0.0 b	3.089 mb	1.154 mb	411.4 nb
82-Pb-204	2821	total	12.00 b	11.95 b		5.337 b	6.496 b
		elastic	11.34 b	11.34 b		2.861 b	5.397 b
		inelastic	Threshold energy = 0.904 MeV			452.5 mb	1.078 b
		(n,2n)	Threshold energy = 8.436 MeV			2.023 b	1.199 mb
		(n,3n)	Threshold energy = 15.390 MeV				88.08 nb
		(n,n' α)	0.0 b	0.0 b	59.59 μb	4.900 μb	2.136 nb
		(n,n' p)	Threshold energy = 6.670 MeV			35.00 μb	8.024 nb
		capture	660.9 mb	587.8 mb	2.688 b	9.140 μb	19.81 mb
		(n,p)	0.0 b	0.0 b	188.7 μb	289.9 μb	576.0 nb
		(n,α)	0.0 b	0.0 b	155.6 μb	158.9 μb	225.0 nb

Nuclide	MAT	Reaction	Thermal cross sections			Fast cross sections		
			2200-m/s	Maxw. Avg.	Res. Integ	14-MeV	Fiss. Avg.	
82-Pb-206	2822	total	11.37 b	11.37 b		5.348 b	6.421 b	
		elastic	11.34 b	11.34 b		2.855 b	5.329 b	
		inelastic			Threshold energy = 0.807 MeV	634.2 mb	1.089 b	
		(n,2n)			Threshold energy = 8.129 MeV	1.855 b	1.378 mb	
		(n,3n)			Threshold energy = 14.890 MeV		201.4 nb	
		(n,n' α)		0.0 b	0.0 b	82.00 μb	68.56 nb	
		(n,n' p)		Threshold energy = 7.283 MeV		2.700 μb	11.04 nb	
		capture		28.00 mb	24.90 mb	96.09 mb	1.550 μb	1.539 mb
		(n,p)		Threshold energy = 0.747 MeV		2.050 mb	1.020 μb	
		(n,α)		0.0 b	0.0 b	3.766 mb	2.030 mb	813.4 nb
82-Pb-207	2823	total	12.04 b	11.98 b		5.354 b	6.366 b	
		elastic	11.34 b	11.34 b		2.852 b	5.253 b	
		inelastic			Threshold energy = 0.573 MeV	667.7 mb	1.110 b	
		(n,2n)			Threshold energy = 6.772 MeV	1.832 b	2.059 mb	
		(n,3n)			Threshold energy = 14.900 MeV		1.556 μb	
		(n,n' α)		0.0 b	0.0 b	68.10 μb	31.79 nb	
		(n,n' p)		Threshold energy = 7.520 MeV		105.9 μb	49.65 nb	
		capture		702.9 mb	625.0 mb	374.7 mb	786.7 nb	1.079 mb
		(n,p)		Threshold energy = 0.643 MeV		1.380 mb	578.2 nb	
		(n,α)		0.0 b	0.0 b	586.0 μb	434.9 μb	166.2 nb
82-Pb-208	2824	total	11.49 b	11.49 b		5.360 b	6.269 b	
		elastic	11.49 b	11.49 b		2.850 b	5.957 b	
		inelastic			Threshold energy = 2.627 MeV	521.8 mb	308.7 mb	
		(n,2n)			Threshold energy = 7.404 MeV	1.986 b	1.283 mb	
		(n,3n)			Threshold energy = 14.180 MeV		353.2 nb	
		(n,n' α)		0.0 b	0.0 b	419.9 μb	200.4 nb	
		(n,n' p)		Threshold energy = 8.046 MeV		15.00 μb	31.57 nb	
		capture		479.8 μb	426.9 μb	7.833 mb	1.100 mb	

Nuclide	MAT	Reaction	Thermal cross sections			Fast cross sections			
			2200-m/s	Maxv. Avg.	Res. Integ	14-MeV	Fiss. Avg.		
82-Pb-208	2824	(n,p)		Threshold energy =	4.229 MeV		317.9 μ b	68.52 nb	
		(n, α)	0.0 b	0.0 b	3.911 mb		1.080 mb	335.0 nb	
90-Th-228	2901	total	133.0 b	120.0 b			5.628 b	7.562 b	
		elastic	12.81 b	12.78 b			3.169 b	5.432 b	
		inelastic			Threshold energy =	0.058 MeV		4.136 mb	1.936 b
		(n,2n)			Threshold energy =	7.151 MeV		1.637 b	7.688 mb
		(n,3n)			Threshold energy =	12.630 MeV		268.9 mb	42.53 μ b
		fission capture	300.0 mb	266.8 mb	1.024 b		548.9 mb	105.8 mb	
90-Th-230	2902	total	119.8 b	107.0 b	1169. b		240.3-12 b	79.47 mb	
		elastic	32.32 b	30.13 b			5.644 b	7.601 b	
		inelastic	9.774 b	9.750 b			3.167 b	5.436 b	
		(n,2n)			Threshold energy =	0.054 MeV		10.45 mb	1.887 b
		(n,3n)			Threshold energy =	6.821 MeV		1.340 b	10.66 mb
		fission capture	0.0 b	0.0 b	1.120 b		528.9 mb	68.64 μ b	
90-Th-232	2903	total	22.55 b	20.38 b	1040. b		596.9 mb	178.5 mb	
		elastic	19.42 b	18.58 b			16.16 nb	87.42 mb	
		inelastic	12.16 b	12.15 b			5.740 b	7.561 b	
		(n,2n)			Threshold energy =	0.050 MeV		3.266 b	5.257 b
		(n,3n)			Threshold energy =	6.465 MeV		142.9 mb	2.125 b
		fission capture	0.0 b	0.0 b	636.2 mb		1.181 b	14.46 mb	
90-Th-233	2904	total	7.258 b	6.427 b	79.93 b		800.0 mb	113.6 μ b	
		elastic	1478. b	1312. b			350.0 mb	78.45 mb	
		inelastic	13.00 b	13.00 b			0.0 b	85.74 mb	
					Threshold energy =	0.017 MeV		5.670 b	7.614 b
							3.167 b	5.296 b	
							15.80 mb	2.054 b	

Nuclide	MAT	Reaction	Thermal cross sections			Fast cross sections		
			2200-m/s	Maxw. Avg.	Res. Integ	14-MeV	Fiss. Avg.	
90-Th-233	2904	(n,2n)	Threshold energy =	4.807 MeV		1.160 b	66.75 mb	
		(n,3n)	Threshold energy =	11.270 MeV		916.9 mb	150.7 μ b	
		fission capture	15.00 b	13.34 b	11.08 b	409.9 mb	109.8 mb	
90-Th-234	2905	total	14.75 b	14.59 b		5.680 b	7.646 b	
		elastic	13.00 b	13.00 b		3.168 b	5.497 b	
		inelastic	Threshold energy =	0.048 MeV		39.56 mb	1.989 b	
91-Pa-233	2911	(n,2n)	Threshold energy =	6.219 MeV		1.040 b	21.69 mb	
		(n,3n)	Threshold energy =	11.030 MeV		1.282 b	228.7 μ b	
		fission capture	0.0 b	0.0 b	260.2 mb	150.0 mb	36.89 mb	
92-U-233	2921	total	1.750 b	1.551 b	93.68 b	154.0 nb	100.9 mb	
		elastic	53.82 b	48.01 b		5.669 b	7.596 b	
		inelastic	11.02 b	11.02 b		3.000 b	4.978 b	
92-U-234	2922	(n,2n)	Threshold energy =	0.007 MeV		103.7 mb	1.499 b	
		(n,3n)	Threshold energy =	6.545 MeV		369.5 mb	5.773 mb	
		fission capture	Threshold energy =	12.130 MeV		418.3 mb	52.40 μ b	
92-U-233	2921	total	0.0 b	0.0 b	4.682 b	1.770 b	990.7 mb	
		elastic	42.80 b	36.97 b	779.2 b	7.400 mb	122.1 mb	
		inelastic	587.8 b	525.0 b		5.770 b	7.686 b	
92-U-234	2922	(n,2n)	Threshold energy =	0.041 MeV		3.278 b	4.806 b	
		(n,3n)	Threshold energy =	5.779 MeV		11.30 μ b	904.5 mb	
		fission capture	Threshold energy =	13.060 MeV		134.9 mb	4.152 mb	
92-U-233	2921	total	529.8 b	470.7 b	771.4 b	37.30 mb	6.033 μ b	
		elastic	45.30 b	41.43 b	138.6 b	2.320 b	1.888 b	
		inelastic	110.1 b	98.40 b		367.9 nb	82.30 mb	

Nuclide	MAT	Reaction	Thermal cross sections			Fast cross sections		
			2200-m/s	Maxw. Avg.	Res. Integ	14-MeV	Fiss. Avg.	
92-U -234	2922	elastic	14.72 b	14.58 b		3.066 b	5.085 b	
		inelastic				393.8 mb	1.062 b	
		(n,2n)		Threshold energy = 0.044 MeV		220.9 mb	1.957 mb	
		(n,3n)		Threshold energy = 6.870 MeV		127.8 mb	14.39 μb	
92-U -235	2923	fission	6.367 mb	5.684 mb	6.438 b	1.934 b	1.199 b	
		capture	95.44 b	83.82 b	608.9 b	2.722 μb	105.8 mb	
92-U -235	2923	total	696.9 b	607.2 b		5.855 b	7.642 b	
		elastic	17.00 b	16.76 b		3.057 b	4.598 b	
		inelastic				514.0 mb	1.651 b	
		(n,2n)		Threshold energy = 0.000 MeV		191.2 mb	12.78 mb	
		(n,3n)		Threshold energy = 5.321 MeV		41.70 mb	7.062 μb	
		fission	583.9 b	503.2 b	278.7 b	2.051 b	1.248 b	
92-U -236	2924	capture	96.00 b	84.95 b	153.3 b	3.146 μb	130.9 mb	
		total	13.67 b	13.09 b		5.826 b	7.752 b	
92-U -236	2924	elastic	8.337 b	8.331 b		3.110 b	5.450 b	
		inelastic				1.144 mb	1.555 b	
		(n,2n)		Threshold energy = 0.045 MeV		423.9 mb	8.475 mb	
		(n,3n)		Threshold energy = 6.574 MeV		660.9 mb	95.74 μb	
		fission	42.96 mb	38.36 mb	7.611 b	1.630 b	595.8 mb	
92-U -238	2925	capture	5.295 b	4.717 b	347.0 b	791.4-12 b	141.5 mb	
		total	11.57 b	11.28 b		5.799 b	7.792 b	
		elastic	8.873 b	8.870 b		2.950 b	5.294 b	
		inelastic				318.9 mb	2.101 b	
92-U -238	2925	(n,2n)		Threshold energy = 0.045 MeV		909.9 mb	15.36 mb	
		(n,3n)		Threshold energy = 6.170 MeV		500.0 mb	82.80 μb	
		fission	3.220 μb	2.868 μb	2.053 b	1.117 b	314.6 mb	

Nuclide	MAT	Reaction	Thermal cross sections			Fast cross sections	
			2200-m/s	Maxw. Avg.	Res. Integ	14-MeV	Fiss. Avg.
92-U-238	2925	capture	2.700 b	2.407 b	279.0 b	3.395 mb	66.72 mb
93-Np-237	2931	total	208.4 b	185.3 b		5.539 b	7.797 b
		elastic	27.52 b	27.19 b		2.787 b	5.006 b
		inelastic			Threshold energy = 0.033 MeV	105.6 mb	1.321 b
		(n,2n)			Threshold energy = 6.657 MeV	446.2 mb	3.301 mb
		(n,3n)			Threshold energy = 12.370 MeV	72.03 mb	11.70 μb
93-Np-239	2932	total	47.50 b	43.42 b		5.523 b	7.808 b
		elastic	10.50 b	10.50 b		2.640 b	4.696 b
94-Pu-238	2941	total	833.3 b	804.7 b		6.515 b	8.451 b
		elastic	3.376 b	3.011 b		3.426 b	5.801 b
		inelastic			Threshold energy = 0.045 MeV	93.93 μb	418.1 mb
		(n,2n)			Threshold energy = 7.393 MeV	17.37 mb	317.4 μb
		(n,3n)			Threshold energy = 13.660 MeV	703.9 μb	278.8 nb
94-Pu-239	2942	total	592.8 b	508.2 b		10.15 b	10.79 b
		elastic	27.60 b	27.05 b		3.556 b	6.300 b
94-Pu-240	2943	total	100.7 b	106.7 b		3.071 b	2.080 b
		elastic	764.5 b	738.5 b		4.023 μb	149.7 mb
94-Pu-242	2942	total	592.8 b	508.2 b		10.15 b	10.79 b
		elastic	27.60 b	27.05 b		3.556 b	6.300 b
		inelastic			Threshold energy = 0.044 MeV	3.168 b	2.154 b
		(n,2n)			Threshold energy = 7.028 MeV	419.0 mb	2.830 mb
		(n,3n)					

Nuclide	MAT	Reaction	Thermal cross sections			Fast cross sections		
			2200-m/s	Maxv. Avg.	Res. Integ	14-MeV	Fiss. Avg.	
94-Pu-238	2942	(n,3n)	Threshold energy =	12.930 MeV	155.4 mb	20.84 μ b		
		fission	16.55 b	14.10 b	32.42 b	2.722 b	2.011 b	
		capture	548.7 b	466.9 b	156.3 b	132.8 mb	318.7 mb	
94-Pu-239	2943	total	1020. b	973.0 b		5.872 b	7.709 b	
		elastic	8.000 b	7.816 b		2.633 b	4.429 b	
		inelastic	Threshold energy =	0.008 MeV		402.6 mb	1.392 b	
		(n,2n)	Threshold energy =	5.671 MeV		346.9 mb	10.63 mb	
		(n,3n)	Threshold energy =	12.700 MeV		180.9 mb	21.77 μ b	
		fission	741.7 b	694.1 b	301.5 b	2.308 b	1.818 b	
		(n,4n)	Threshold energy =	18.600 MeV			45.92 nb	
capture	270.2 b	270.9 b	195.2 b	1.349 nb	60.75 mb			
94-Pu-240	2944	total	290.0 b	264.8 b		5.888 b	7.844 b	
		elastic	1.509 b	1.389 b		3.202 b	4.964 b	
		inelastic	Threshold energy =	0.043 MeV		7.274 mb	1.420 b	
		(n,2n)	Threshold energy =	6.561 MeV		427.1 mb	3.920 mb	
		(n,3n)	Threshold energy =	12.230 MeV		129.7 mb	18.96 μ b	
		fission	67.61 mb	61.45 mb	10.09 b	2.121 b	1.963 b	
		(n,4n)	Threshold energy =	19.260 MeV			5.617 nb	
		capture	288.4 b	263.3 b	8453. b	800.0 μ b	92.71 mb	
94-Pu-241	2945	total	1388. b	1286. b		5.801 b	7.842 b	
		elastic	10.23 b	9.935 b		3.291 b	5.167 b	
		inelastic	Threshold energy =	0.042 MeV		221.6 μ b	879.2 mb	
		(n,2n)	Threshold energy =	5.262 MeV		178.0 mb	22.66 mb	
		(n,3n)	Threshold energy =	11.820 MeV		149.5 mb	22.55 μ b	
		fission	1015. b	947.6 b	590.3 b	2.182 b	1.624 b	
		(n,4n)	Threshold energy =	17.500 MeV			19.72 nb	
capture	362.9 b	327.8 b	186.8 b	7.722 nb	149.0 mb			

Nuclide	MAT	Reaction	Thermal cross sections			Fast cross sections	
			2200-m/s	Maxw. Avg.	Res. Integ	14-MeV	Fiss. Avg.
94-Pu-242	2946	total	26.65 b	24.74 b		5.918 b	7.849 b
		elastic	8.111 b	8.091 b		3.161 b	5.339 b
		inelastic	Threshold energy = 0.045 MeV			8.378 mb	1.280 b
		(n,2n)	Threshold energy = 6.336 MeV			454.0 mb	6.669 mb
		(n,3n)	Threshold energy = 11.600 MeV			303.0 mb	44.58 μb
		fission	121.2 mb	107.8 mb	6.348 b	1.991 b	1.135 b
		(n,4n) capture	Threshold energy = 18.160 MeV			800.0 μb	116.7 nb 87.72 mb
95-Am-241	2951	total	614.6 b	547.5 b		5.742 b	7.779 b
		elastic	11.26 b	10.83 b		2.722 b	4.788 b
		inelastic	Threshold energy = 0.041 MeV			42.21 μb	1.179 b
		(n,2n)	Threshold energy = 6.610 MeV			262.3 mb	620.3 μb
		(n,3n)	Threshold energy = 12.650 MeV			46.74 mb	10.02 μb
		fission	3.018 b	2.721 b	14.69 b	2.711 b	1.510 b
		(n,4n) capture	Threshold energy = 19.780 MeV			263.5-12 b	17.0-15 b 297.9 mb
95-Am-242	2952	total	7611. b	6747. b		5.906 b	7.758 b
		elastic	11.44 b	11.44 b		2.807 b	4.561 b
		inelastic	Threshold energy = 0.044 MeV			402.2 mb	1.228 b
		(n,2n)	Threshold energy = 5.515 MeV			130.8 mb	4.387 mb
		(n,3n)	Threshold energy = 12.120 MeV			138.9 mb	17.94 μb
		fission	2100. b	1861. b	1258. b	2.427 b	1.756 b
		capture	5500. b	4872. b	390.4 b	4.487 μb	206.6 mb
95-Am-242M	2953	total	7969. b	7809. b		5.913 b	7.761 b
		elastic	6.698 b	7.429 b		2.807 b	4.527 b
		inelastic	0.0 b	0.0 b	4.597 b	442.2 mb	1.256 b
		(n,2n)	Threshold energy = 5.515 MeV			130.8 mb	4.387 mb

Nuclide	MAT	Reaction	Thermal cross sections			Fast cross sections	
			2200-m/s	Maxw. Avg.	Res. Integ	14-MeV	Fiss. Avg.
95-Am-242M	2953	(n,3n)	Threshold energy = 12.120 MeV			138.9 mb	17.94 μ b
		fission	6620. b	6480. b	1528. b	2.395 b	1.866 b
		capture	1342. b	1321. b	206.8 b	723.0 nb	106.3 mb
95-Am-243	2954	total	86.26 b	78.37 b		5.759 b	7.853 b
		elastic	7.528 b	7.476 b		2.728 b	4.798 b
		inelastic	Threshold energy = 0.042 MeV			42.36 μ b	1.577 b
		(n,2n)	Threshold energy = 6.391 MeV			360.4 mb	3.728 mb
		(n,3n)	Threshold energy = 11.950 MeV			221.0 mb	33.16 μ b
		fission	228.0 mb	205.2 mb	11.37 b	2.450 b	1.274 b
		(n,4n)	Threshold energy = 18.570 MeV				2.068 nb
capture	78.50 b	70.68 b	1818. b	97.9-12 b	194.5 mb		
96-Cm-242	2961	total	32.53 b	30.11 b		5.750 b	7.818 b
		elastic	11.61 b	11.60 b		2.725 b	4.954 b
		inelastic	Threshold energy = 0.042 MeV			318.0 μ b	975.4 mb
		(n,2n)	Threshold energy = 6.997 MeV			111.5 mb	1.754 mb
		(n,3n)	Threshold energy = 13.090 MeV			6.359 mb	4.379 μ b
		fission	5.000 b	4.448 b	11.09 b	2.907 b	1.798 b
		capture	15.92 b	14.07 b	116.2 b	3.061 nb	86.97 mb
96-Cm-243	2962	total	753.3 b	670.1 b		5.917 b	7.778 b
		elastic	9.658 b	9.571 b		2.809 b	4.562 b
		inelastic	Threshold energy = 0.042 MeV			26.47 mb	786.8 mb
		(n,2n)	Threshold energy = 5.719 MeV			472.4 mb	15.37 mb
		(n,3n)	Threshold energy = 12.710 MeV			73.62 mb	17.69 μ b
		fission	612.3 b	545.6 b	1751. b	2.536 b	2.379 b
		(n,4n)	Threshold energy = 18.830 MeV				1.251 nb
capture	131.3 b	115.0 b	404.4 b	17.23 nb	34.35 mb		

Nuclide	MAT	Reaction	Thermal cross sections			Fast cross sections				
			2200-m/s	Maxw. Avg.	Res. Integ	14-MeV	Fiss. Avg.			
96-Cm-244	2963	total	22.24	b	20.51	b	6.026	b	7.625	b
		elastic	6.650	b	6.641	b	3.273	b	5.115	b
		inelastic	Threshold energy =		0.043	MeV	17.51	mb	832.0	mb
		(n,2n)	Threshold energy =		6.828	MeV	60.34	mb	576.3	μ b
		(n,3n)	Threshold energy =		12.550	MeV	39.29	mb	4.776	μ b
		fission	1.180	b	1.049	b	18.39	b	1.553	b
		capture	14.41	b	12.82	b	593.5	b	271.4	nb
96-Cm-245	2964	total	2359.	b	1980.	b	6.060	b	7.643	b
		elastic	11.59	b	11.50	b	3.295	b	4.817	b
		inelastic	Threshold energy =		0.055	MeV	220.2	mb	890.7	mb
		(n,2n)	Threshold energy =		5.533	MeV	176.8	mb	3.080	mb
		(n,3n)	Threshold energy =		12.370	MeV	70.66	mb	9.299	μ b
		fission	2001.	b	1680.	b	799.4	b	2.297	b
		capture	346.3	b	288.3	b	107.7	b	444.3	nb

Appendix 2

Average cross sections

CROSS SECTION

MATERIAL = 2011		H - 1											
ENERGY	TOTAL	ELASTIC	INELR	(N,2N)	(N,3N)	FISSION	(N,NR)	(N,NP)	CAPTURE	(N,P)	(N,D)	(N,R)	MU-BRR
1.0000- 5 ~ 1.0000- 2	2.1473+ 1	2.0437+ 1							1.0238+ 0				6.7365- 1
1.0000- 2 ~ 2.0000- 2	2.0919+ 1	2.0437+ 1							4.7473- 1				6.7365- 1
1.5000- 2 ~ 2.0000- 2	2.0847+ 1	2.0437+ 1							3.5022- 1				6.7365- 1
2.0000- 2 ~ 3.0000- 2	2.0776+ 1	2.0437+ 1							2.9208- 1				6.7365- 1
3.0000- 2 ~ 4.0000- 2	2.0730+ 1	2.0437+ 1							2.4931- 1				6.7365- 1
4.0000- 2 ~ 5.0000- 2	2.0697+ 1	2.0437+ 1							2.2538+ 1				6.7365- 1
5.0000- 2 ~ 6.0000- 2	2.0671+ 1	2.0437+ 1							2.0093+ 1				6.7365- 1
6.0000- 2 ~ 7.0000- 2	2.0651+ 1	2.0437+ 1							1.7628- 1				6.7365- 1
7.0000- 2 ~ 8.0000- 2	2.0639+ 1	2.0437+ 1							1.5010- 1				6.7365- 1
8.0000- 2 ~ 9.0000- 2	2.0629+ 1	2.0437+ 1							1.2554+ 1				6.7365- 1
9.0000- 2 ~ 1.0000- 1	2.0622+ 1	2.0437+ 1							1.0077- 1				6.7365- 1
1.0000- 1 ~ 2.0000- 1	2.0619+ 1	2.0437+ 1							8.4577- 1				6.7365- 1
2.0000- 1 ~ 3.0000- 1	2.0619+ 1	2.0437+ 1							7.3555+ 1				6.7365- 1
3.0000- 1 ~ 4.0000- 1	2.0620+ 1	2.0437+ 1							6.2829+ 1				6.7365- 1
4.0000- 1 ~ 5.0000- 1	2.0623+ 1	2.0437+ 1							5.2423+ 1				6.7365- 1
5.0000- 1 ~ 6.0000- 1	2.0629+ 1	2.0437+ 1							4.2022+ 1				6.7365- 1
6.0000- 1 ~ 7.0000- 1	2.0639+ 1	2.0437+ 1							3.1621+ 1				6.7365- 1
7.0000- 1 ~ 8.0000- 1	2.0651+ 1	2.0437+ 1							2.1220+ 1				6.7365- 1
8.0000- 1 ~ 9.0000- 1	2.0665+ 1	2.0437+ 1							1.0819+ 1				6.7365- 1
9.0000- 1 ~ 1.0000+ 0	2.0682+ 1	2.0437+ 1							0.0407- 1				6.7365- 1
1.0000+ 0 ~ 1.5000+ 0	2.0703+ 1	2.0437+ 1							1.5000+ 1				6.7365- 1
1.5000+ 0 ~ 2.0000+ 0	2.0729+ 1	2.0437+ 1							1.2648+ 1				6.7365- 1
2.0000+ 0 ~ 3.0000+ 0	2.0761+ 1	2.0437+ 1							1.0393+ 1				6.7365- 1
3.0000+ 0 ~ 4.0000+ 0	2.0799+ 1	2.0437+ 1							8.9228+ 1				6.7365- 1
4.0000+ 0 ~ 5.0000+ 0	2.0843+ 1	2.0437+ 1							7.8092+ 1				6.7365- 1
5.0000+ 0 ~ 6.0000+ 0	2.0894+ 1	2.0437+ 1							6.7022+ 1				6.7365- 1
6.0000+ 0 ~ 7.0000+ 0	2.0952+ 1	2.0437+ 1							5.5711+ 1				6.7365- 1
7.0000+ 0 ~ 8.0000+ 0	2.1018+ 1	2.0437+ 1							4.4414+ 1				6.7365- 1
8.0000+ 0 ~ 9.0000+ 0	2.1093+ 1	2.0437+ 1							3.3166+ 1				6.7365- 1
9.0000+ 0 ~ 1.0000+ 1	2.1177+ 1	2.0437+ 1							2.1937+ 1				6.7365- 1
1.0000+ 1 ~ 1.5000+ 1	2.1269+ 1	2.0437+ 1							1.0693+ 1				6.7365- 1
1.5000+ 1 ~ 2.0000+ 1	2.1369+ 1	2.0437+ 1							9.9937+ 1				6.7365- 1
2.0000+ 1 ~ 3.0000+ 1	2.1477+ 1	2.0437+ 1							8.8666+ 1				6.7365- 1
3.0000+ 1 ~ 4.0000+ 1	2.1592+ 1	2.0437+ 1							7.7422+ 1				6.7365- 1
4.0000+ 1 ~ 5.0000+ 1	2.1714+ 1	2.0437+ 1							6.6188+ 1				6.7365- 1
5.0000+ 1 ~ 6.0000+ 1	2.1844+ 1	2.0437+ 1							5.4954+ 1				6.7365- 1
6.0000+ 1 ~ 7.0000+ 1	2.1981+ 1	2.0437+ 1							4.3720+ 1				6.7365- 1
7.0000+ 1 ~ 8.0000+ 1	2.2125+ 1	2.0437+ 1							3.2486+ 1				6.7365- 1
8.0000+ 1 ~ 9.0000+ 1	2.2276+ 1	2.0437+ 1							2.1252+ 1				6.7365- 1
9.0000+ 1 ~ 1.0000+ 2	2.2434+ 1	2.0437+ 1							1.0018+ 1				6.7365- 1
1.0000+ 2 ~ 1.5000+ 2	2.2599+ 1	2.0437+ 1							9.8966+ 1				6.7365- 1
1.5000+ 2 ~ 2.0000+ 2	2.2771+ 1	2.0437+ 1							8.7832+ 1				6.7365- 1
2.0000+ 2 ~ 3.0000+ 2	2.2950+ 1	2.0437+ 1							7.6698+ 1				6.7365- 1
3.0000+ 2 ~ 4.0000+ 2	2.3134+ 1	2.0437+ 1							6.5564+ 1				6.7365- 1
4.0000+ 2 ~ 5.0000+ 2	2.3323+ 1	2.0437+ 1							5.4430+ 1				6.7365- 1
5.0000+ 2 ~ 6.0000+ 2	2.3517+ 1	2.0437+ 1							4.3296+ 1				6.7365- 1
6.0000+ 2 ~ 7.0000+ 2	2.3716+ 1	2.0437+ 1							3.2162+ 1				6.7365- 1
7.0000+ 2 ~ 8.0000+ 2	2.3920+ 1	2.0437+ 1							2.1028+ 1				6.7365- 1
8.0000+ 2 ~ 9.0000+ 2	2.4129+ 1	2.0437+ 1							1.0000+ 1				6.7365- 1
9.0000+ 2 ~ 1.0000+ 3	2.4343+ 1	2.0437+ 1							9.8866+ 1				6.7365- 1
1.0000+ 3 ~ 1.5000+ 3	2.4562+ 1	2.0437+ 1							8.7732+ 1				6.7365- 1
1.5000+ 3 ~ 2.0000+ 3	2.4786+ 1	2.0437+ 1							7.6598+ 1				6.7365- 1
2.0000+ 3 ~ 3.0000+ 3	2.5015+ 1	2.0437+ 1							6.5464+ 1				6.7365- 1
3.0000+ 3 ~ 4.0000+ 3	2.5249+ 1	2.0437+ 1							5.4330+ 1				6.7365- 1
4.0000+ 3 ~ 5.0000+ 3	2.5488+ 1	2.0437+ 1							4.3196+ 1				6.7365- 1
5.0000+ 3 ~ 6.0000+ 3	2.5732+ 1	2.0437+ 1							3.2062+ 1				6.7365- 1
6.0000+ 3 ~ 7.0000+ 3	2.5981+ 1	2.0437+ 1							2.0928+ 1				6.7365- 1
7.0000+ 3 ~ 8.0000+ 3	2.6235+ 1	2.0437+ 1							1.0000+ 1				6.7365- 1
8.0000+ 3 ~ 9.0000+ 3	2.6494+ 1	2.0437+ 1							9.8866+ 1				6.7365- 1
9.0000+ 3 ~ 1.0000+ 4	2.6758+ 1	2.0437+ 1							8.7732+ 1				6.7365- 1
1.0000+ 4 ~ 1.5000+ 4	2.7027+ 1	2.0437+ 1							7.6598+ 1				6.7365- 1
1.5000+ 4 ~ 2.0000+ 4	2.7299+ 1	2.0437+ 1							6.5464+ 1				6.7365- 1
2.0000+ 4 ~ 3.0000+ 4	2.7575+ 1	2.0437+ 1							5.4330+ 1				6.7365- 1
3.0000+ 4 ~ 4.0000+ 4	2.7855+ 1	2.0437+ 1							4.3196+ 1				6.7365- 1
4.0000+ 4 ~ 5.0000+ 4	2.8139+ 1	2.0437+ 1							3.2062+ 1				6.7365- 1
5.0000+ 4 ~ 6.0000+ 4	2.8427+ 1	2.0437+ 1							2.0928+ 1				6.7365- 1
6.0000+ 4 ~ 7.0000+ 4	2.8719+ 1	2.0437+ 1							1.0000+ 1				6.7365- 1
7.0000+ 4 ~ 8.0000+ 4	2.9014+ 1	2.0437+ 1							9.8866+ 1				6.7365- 1
8.0000+ 4 ~ 9.0000+ 4	2.9312+ 1	2.0437+ 1							8.7732+ 1				6.7365- 1
9.0000+ 4 ~ 1.0000+ 5	2.9613+ 1	2.0437+ 1							7.6598+ 1				6.7365- 1
1.0000+ 5 ~ 1.5000+ 5	2.9917+ 1	2.0437+ 1							6.5464+ 1				6.7365- 1
1.5000+ 5 ~ 2.0000+ 5	3.0224+ 1	2.0437+ 1							5.4330+ 1				6.7365- 1
2.0000+ 5 ~ 3.0000+ 5	3.0534+ 1	2.0437+ 1							4.3196+ 1				6.7365- 1
3.0000+ 5 ~ 4.0000+ 5	3.0847+ 1	2.0437+ 1							3.2062+ 1				6.7365- 1
4.0000+ 5 ~ 5.0000+ 5	3.1163+ 1	2.0437+ 1							2.0928+ 1				6.7365- 1
5.0000+ 5 ~ 6.0000+ 5	3.1481+ 1	2.0437+ 1							1.0000+ 1				6.7365- 1
6.0000+ 5 ~ 7.0000+ 5	3.1802+ 1	2.0437+ 1							9.8866+ 1				6.7365- 1
7.0000+ 5 ~ 8.0000+ 5	3.2125+ 1	2.0437+ 1							8.7732+ 1				6.7365- 1
8.0000+ 5 ~ 9.0000+ 5	3.2451+ 1	2.0437+ 1							7.6598+ 1				6.7365- 1
9.0000+ 5 ~ 1.0000+ 6	3.2779+ 1	2.0437+ 1							6.5464+ 1				6.7365- 1
1.0000+ 6 ~ 1.5000+ 6	3.3110+ 1	2.0437+ 1							5.4330+ 1				6.7365- 1
1.5000+ 6 ~ 2.0000+ 6	3.3443+ 1	2.0437+ 1							4.3196+ 1				6.7365- 1
2.0000+ 6 ~ 3.0000+ 6	3.3779+ 1	2.0437+ 1							3.2062+ 1				6.7365- 1
3.0000+ 6 ~ 4.0000+ 6	3.4117+ 1	2.0437+ 1							2.0928+ 1				6.7365- 1
4.0000+ 6 ~ 5.0000+ 6	3.4457+ 1	2.0437+ 1							1.0000+ 1				6.7365- 1
5.0000+ 6 ~ 6.0000+ 6	3.4799+ 1	2.0437+ 1							9.8866+ 1				6.7365- 1
6.0000+ 6 ~ 7.0000+ 6	3.5143+ 1	2.0437+ 1							8.7732+ 1				6.7365- 1
7.0000+ 6 ~ 8.0000+ 6	3.5489+ 1	2.0437+ 1				</							

CROSS SECTION

MATERIAL = 2012

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ENERGY	TOTAL	ELASTIC	INEL	(N.2N)	(N.3N)	FIBION	(N.NR)	(N.NP)	(N.D)	(N.R)	MU-BAR
1.0000- 5 ~ 1.0000- 2	3.3889+ 0	3.3889+ 0						1.6560- 3			3.3347- 1
1.0000- 2	3.3900+ 0	3.3892+ 0						7.8646- 4			3.3347- 1
1.0000- 1	3.3900+ 0	3.3893+ 0						5.6301- 4			3.3347- 1
2.0000- 2	3.3900+ 0	3.3893+ 0						4.5610- 4			3.3347- 1
3.0000- 2	3.3900+ 0	3.3895+ 0						4.5687- 4			3.3347- 1
4.0000- 2	3.3900+ 0	3.3895+ 0						3.7340- 4			3.3347- 1
5.0000- 2	3.3900+ 0	3.3895+ 0						3.3151- 4			3.3347- 1
6.0000- 2	3.3900+ 0	3.3897+ 0						2.5206- 4			3.3347- 1
7.0000- 1	3.3900+ 0	3.3897+ 0						2.0970- 4			3.3347- 1
1.5000- 1	3.3900+ 0	3.3896+ 0						1.7586- 4			3.3347- 1
2.0000- 1	3.3900+ 0	3.3898+ 0						1.4826- 4			3.3347- 1
3.0000- 1	3.3900+ 0	3.3898+ 0						1.3062- 4			3.3347- 1
4.0000- 1	3.3900+ 0	3.3898+ 0						1.1939- 4			3.3347- 1
5.0000- 1	3.3900+ 0	3.3899+ 0						1.0999- 4			3.3347- 1
6.0000- 1	3.3900+ 0	3.3899+ 0						9.2364- 5			3.3347- 1
8.0000+ 0	3.3900+ 0	3.3899+ 0						7.8663- 5			3.3347- 1
1.0000+ 0	3.3900+ 0	3.3899+ 0						6.2320- 5			3.3347- 1
2.0000+ 0	3.3900+ 0	3.3899+ 0						4.7919- 5			3.3347- 1
3.0000+ 0	3.3900+ 0	3.3899+ 0						3.7367- 5			3.3347- 1
4.0000+ 0	3.3900+ 0	3.3900+ 0						2.9169- 5			3.3347- 1
5.0000+ 0	3.3900+ 0	3.3900+ 0						2.3223- 5			3.3347- 1
6.0000+ 0	3.3900+ 0	3.3900+ 0						1.8894- 5			3.3347- 1
8.0000+ 0	3.3900+ 0	3.3900+ 0						1.4916- 5			3.3347- 1
1.0000+ 1	3.3900+ 0	3.3900+ 0						1.1816- 5			3.3347- 1
2.0000+ 1	3.3900+ 0	3.3900+ 0						9.0641- 6			3.3347- 1
3.0000+ 1	3.3900+ 0	3.3900+ 0						7.2366- 6			3.3347- 1
4.0000+ 1	3.3900+ 0	3.3900+ 0						5.8514- 6			3.3347- 1
5.0000+ 1	3.3900+ 0	3.3900+ 0						4.7977- 6			3.3347- 1
6.0000+ 1	3.3900+ 0	3.3900+ 0						3.9787- 6			3.3347- 1
8.0000+ 1	3.3900+ 0	3.3900+ 0						3.3761- 6			3.3347- 1
1.0000+ 2	3.3899+ 0	3.3899+ 0						2.7929- 6			3.3347- 1
2.0000+ 2	3.3899+ 0	3.3891+ 0						2.3555- 6			3.3347- 1
3.0000+ 2	3.3899+ 0	3.3891+ 0						2.0040- 6			3.3347- 1
4.0000+ 2	3.3899+ 0	3.3891+ 0						1.7201- 6			3.3347- 1
5.0000+ 2	3.3899+ 0	3.3891+ 0						1.4980- 6			3.3347- 1
6.0000+ 2	3.3899+ 0	3.3891+ 0						1.3074- 6			3.3347- 1
8.0000+ 2	3.3899+ 0	3.3891+ 0						1.1478- 6			3.3347- 1
1.0000+ 3	3.3891+ 0	3.3891+ 0						1.0182- 6			3.3347- 1
2.0000+ 3	3.3891+ 0	3.3891+ 0						8.9166- 7			3.3347- 1
3.0000+ 3	3.3891+ 0	3.3891+ 0						7.7270- 7			3.3347- 1
4.0000+ 3	3.3891+ 0	3.3891+ 0						6.7378- 7			3.3347- 1
5.0000+ 3	3.3891+ 0	3.3891+ 0						5.9338- 7			3.3347- 1
6.0000+ 3	3.3891+ 0	3.3891+ 0						5.2789- 7			3.3347- 1
8.0000+ 3	3.3891+ 0	3.3891+ 0						4.7653- 7			3.3347- 1
1.0000+ 4	3.3891+ 0	3.3891+ 0						4.2894- 7			3.3347- 1
2.0000+ 4	3.3891+ 0	3.3891+ 0						3.8471- 7			3.3347- 1
3.0000+ 4	3.3891+ 0	3.3891+ 0						3.4332- 7			3.3347- 1
4.0000+ 4	3.3891+ 0	3.3891+ 0						3.0444- 7			3.3347- 1
5.0000+ 4	3.3891+ 0	3.3891+ 0						2.6879- 7			3.3347- 1
6.0000+ 4	3.3891+ 0	3.3891+ 0						2.3594- 7			3.3347- 1
8.0000+ 4	3.3891+ 0	3.3891+ 0						2.0544- 7			3.3347- 1
1.0000+ 5	3.3891+ 0	3.3891+ 0						1.7700- 7			3.3347- 1
2.0000+ 5	3.3891+ 0	3.3891+ 0						1.5074- 7			3.3347- 1
3.0000+ 5	3.3891+ 0	3.3891+ 0						1.2700- 7			3.3347- 1
4.0000+ 5	3.3891+ 0	3.3891+ 0						1.0622- 7			3.3347- 1
5.0000+ 5	3.3891+ 0	3.3891+ 0						8.8293- 8			3.3347- 1
6.0000+ 5	3.3891+ 0	3.3891+ 0						7.7462- 8			3.3347- 1
8.0000+ 5	3.3891+ 0	3.3891+ 0						6.8298- 8			3.3347- 1
1.0000+ 6	3.3891+ 0	3.3891+ 0						6.0499- 8			3.3347- 1
2.0000+ 6	3.3891+ 0	3.3891+ 0						5.3858- 8			3.3347- 1
3.0000+ 6	3.3891+ 0	3.3891+ 0						4.8222- 8			3.3347- 1
4.0000+ 6	3.3891+ 0	3.3891+ 0						4.3558- 8			3.3347- 1
5.0000+ 6	3.3891+ 0	3.3891+ 0						3.9622- 8			3.3347- 1
6.0000+ 6	3.3891+ 0	3.3891+ 0						3.6274- 8			3.3347- 1
8.0000+ 6	3.3891+ 0	3.3891+ 0						3.3316- 8			3.3347- 1
1.0000+ 7	3.3891+ 0	3.3891+ 0						3.0700- 8			3.3347- 1
2.0000+ 7	3.3891+ 0	3.3891+ 0						2.8377- 8			3.3347- 1
3.0000+ 7	3.3891+ 0	3.3891+ 0						2.6292- 8			3.3347- 1
4.0000+ 7	3.3891+ 0	3.3891+ 0						2.4400- 8			3.3347- 1
5.0000+ 7	3.3891+ 0	3.3891+ 0						2.2682- 8			3.3347- 1
6.0000+ 7	3.3891+ 0	3.3891+ 0						2.1116- 8			3.3347- 1
8.0000+ 7	3.3891+ 0	3.3891+ 0						1.9677- 8			3.3347- 1
1.0000+ 8	3.3891+ 0	3.3891+ 0						1.8347- 8			3.3347- 1
2.0000+ 8	3.3891+ 0	3.3891+ 0						1.7112- 8			3.3347- 1
3.0000+ 8	3.3891+ 0	3.3891+ 0						1.5969- 8			3.3347- 1
4.0000+ 8	3.3891+ 0	3.3891+ 0						1.4909- 8			3.3347- 1
5.0000+ 8	3.3891+ 0	3.3891+ 0						1.3924- 8			3.3347- 1
6.0000+ 8	3.3891+ 0	3.3891+ 0						1.2998- 8			3.3347- 1
8.0000+ 8	3.3891+ 0	3.3891+ 0						1.2124- 8			3.3347- 1
1.0000+ 9	3.3891+ 0	3.3891+ 0						1.1298- 8			3.3347- 1
2.0000+ 9	3.3891+ 0	3.3891+ 0						1.0519- 8			3.3347- 1
3.0000+ 9	3.3891+ 0	3.3891+ 0						9.7822- 9			3.3347- 1
4.0000+ 9	3.3891+ 0	3.3891+ 0						9.1171- 9			3.3347- 1
5.0000+ 9	3.3891+ 0	3.3891+ 0						8.5593- 9			3.3347- 1
6.0000+ 9	3.3891+ 0	3.3891+ 0						8.0981- 9			3.3347- 1
8.0000+ 9	3.3891+ 0	3.3891+ 0						7.7361- 9			3.3347- 1
1.0000+ 10	3.3891+ 0	3.3891+ 0						7.3682- 9			3.3347- 1
2.0000+ 10	3.3891+ 0	3.3891+ 0						7.0000- 9			3.3347- 1
3.0000+ 10	3.3891+ 0	3.3891+ 0						6.6377- 9			3.3347- 1
4.0000+ 10	3.3891+ 0	3.3891+ 0						6.2809- 9			3.3347- 1
5.0000+ 10	3.3891+ 0	3.3891+ 0						5.9298- 9			3.3347- 1
6.0000+ 10	3.3891+ 0	3.3891+ 0						5.5845- 9			3.3347- 1
8.0000+ 10	3.3891+ 0	3.3891+ 0						5.2450- 9			3.3347- 1
1.0000+ 11	3.3891+ 0	3.3891+ 0						4.9113- 9			3.3347- 1
2.0000+ 11	3.3891+ 0	3.3891+ 0						4.5834- 9			3.3347- 1
3.0000+ 11	3.3891+ 0	3.3891+ 0						4.2613- 9			3.3347- 1
4.0000+ 11	3.3891+ 0	3.3891+ 0						3.9450- 9			3.3347- 1
5.0000+ 11	3.3891+ 0	3.3891+ 0						3.6345- 9			3.3347- 1
6.0000+ 11	3.3891+ 0	3.3891+ 0						3.3298- 9			3.3347- 1
8.0000+ 11	3.3891+ 0	3.3891+ 0						3.0310- 9			3.3347- 1
1.0000+ 12	3.3891+ 0	3.3891+ 0						2.7380- 9			3.3347- 1
2.0000+ 12	3.3891+ 0	3.3891+ 0						2.4509- 9			3.3347- 1
3.0000+ 12	3.3891+ 0	3.3891+ 0						2.1697- 9			3.3347- 1
4.0000+ 12	3.3891+ 0	3.3891+ 0									

LI-6

CROSS SECTION

MATERIAL -2031	ENERGY	TOTAL	ELABTIC	INELR	(N.2N)	(N.3N)	FISSION	(N.NR)	(N.NP)	CAPTURE	(N.PI)	(N.O)	(N.R)	(N.BR)	MU-BAR
1.0000-5	1.0000-2	2.8662+3	7.3600-1							8.6344-2			2.4873+3		1.1179-1
1.0000-4	1.5000-2	1.9398+3	7.5698-1							4.0038-2			1.9386+3		1.1179-1
1.0000-3	2.0000-2	1.4775+3	7.3508-1							3.3259-2			1.4684+3		1.1179-1
1.0000-2	2.5000-2	9.1472+3	7.3508-1							2.9601-2			7.9807+3		1.1179-1
1.0000-1	3.0000-2	7.9807+3	7.3508-1							2.1021-2			7.0310+3		1.1179-1
1.0000-0	4.0000-2	7.0390+3	7.3508-1							1.9010-2			6.3682+3		1.1179-1
1.0000-0	5.0000-2	6.3682+3	7.3508-1							1.6877-2			5.5723+3		1.1179-1
1.0000-0	6.0000-2	5.5723+3	7.3508-1							1.4869-2			4.7914+3		1.1179-1
1.0000-0	7.0000-2	4.7914+3	7.3508-1							1.2661-2			4.2332+3		1.1179-1
1.0000-0	8.0000-2	3.9797+3	7.3508-1							1.0674-2			3.5687+3		1.1179-1
1.0000-0	9.0000-2	3.1744+3	7.4117-1							8.9627-3			2.9933+3		1.1179-1
1.0000-0	1.0000-1	2.3022+3	7.4117-1							7.5475-3			2.5233+3		1.1179-1
1.0000-0	2.0000-1	1.4378+3	7.5016-1							6.4419-3			2.2038+3		1.1179-1
1.0000-0	3.0000-1	7.5016+3	7.5208-1							5.3669-3			1.7843+3		1.1179-1
1.0000-0	4.0000-1	6.0000+3	7.5208-1							4.7019-3			1.5720+3		1.1179-1
1.0000-0	5.0000-1	4.7924+3	7.5937-1							4.0938-3			1.3986+3		1.1179-1
1.0000-0	6.0000-1	3.4657+3	7.5799-1							2.7831-3			1.2284+3		1.1179-1
1.0000-0	7.0000-1	2.1372+3	7.5825-1							2.4811-3			1.0443+3		1.1179-1
1.0000-0	8.0000-1	1.3725+3	7.5851-1							2.1967-3			9.4478+3		1.1179-1
1.0000-0	9.0000-1	9.4478+3	7.5877-1							1.8277-3			7.0293+3		1.1179-1
1.0000-0	1.0000-0	8.0672+3	7.5899-1							1.5010-3			5.2374+3		1.1179-1
1.0000-0	2.0000-0	7.1158+3	7.5899-1							1.1877-3			3.7426+3		1.1179-1
1.0000-0	3.0000-0	6.4722+3	7.5928-1							1.0072-3			2.9705+3		1.1179-1
1.0000-0	4.0000-0	5.7422+3	7.5947-1							1.8685-3			2.4970+3		1.1179-1
1.0000-0	5.0000-0	5.0479+3	7.5947-1							1.2661-3			1.9702+3		1.1179-1
1.0000-0	6.0000-0	4.3137+3	7.5946-1							1.0674-3			1.5220+3		1.1179-1
1.0000-0	7.0000-0	3.5847+3	7.5951-1							9.5274-4			1.1276+3		1.1179-1
1.0000-0	8.0000-0	2.8500+3	7.5950-1							8.9277-4			9.5274+3		1.1179-1
1.0000-0	9.0000-0	2.1203+3	7.5969-1							6.6495-4			2.2221+3		1.1179-1
1.0000-0	1.0000-0	1.3902+3	7.5989-1							5.0114-4			2.0088+3		1.1179-1
1.0000-0	2.0000-0	7.5989+3	7.5980-1							5.3369-4			1.7833+3		1.1179-1
1.0000-0	3.0000-0	6.8643+3	7.5980-1							4.7019-4			1.5711+3		1.1179-1
1.0000-0	4.0000-0	6.0729+3	7.5959-1							4.0938-4			1.3377+3		1.1169-1
1.0000-0	5.0000-0	5.2729+3	7.5934-1							3.5753-4			1.1276+3		1.1169-1
1.0000-0	6.0000-0	4.4660+3	7.5904-1							2.8311-4			9.4675+3		1.1157-1
1.0000-0	7.0000-0	3.6500+3	7.5772-1							2.3887-4			7.9224+3		1.1130-1
1.0000-0	8.0000-0	2.8272+3	7.5772-1							2.0277-4			6.9250+3		1.1130-1
1.0000-0	9.0000-0	2.0174+3	7.5772-1							1.5617-4			5.6377+3		1.1117-1
1.0000-0	1.0000-0	1.2033+3	7.5681-1							1.1069-4			4.5671+3		1.1099-1
1.0000-0	2.0000-0	7.5681+3	7.5655-1							1.4869-4			3.2009+3		1.1072-1
1.0000-0	3.0000-0	6.7296+3	7.5605-1							1.2661-4			2.5200+3		1.1072-1
1.0000-0	4.0000-0	5.8935+3	7.5539-1							1.0574-4			1.9266+3		1.0984-1
1.0000-0	5.0000-0	5.0618+3	7.5491-1							9.2575-5			1.5285+3		1.0984-1
1.0000-0	6.0000-0	4.2283+3	7.5429-1							7.5495-5			1.1144+3		1.0943-1
1.0000-0	7.0000-0	3.3954+3	7.5351-1							6.0114-5			9.0577+3		1.0943-1
1.0000-0	8.0000-0	2.5618+3	7.5271-1							5.3369-5			7.0565+3		1.0952-1
1.0000-0	9.0000-0	1.7283+3	7.5271-1							4.7019-5			5.5666+3		1.0952-1
1.0000-0	1.0000-0	1.0000+4	7.4847-1							4.0038-5			4.3613+3		1.0276-1
1.0000-0	2.0000-0	2.1096+4	7.4878-1							3.3753-5			3.7520+3		1.0276-1
1.0000-0	3.0000-0	1.5945+4	7.4802-1							2.8311-5			3.2420+3		1.0276-1
1.0000-0	4.0000-0	1.0722+4	7.4737-1							2.3857-5			2.7231+3		1.0276-1
1.0000-0	5.0000-0	5.0795+4	7.4636-1							2.0070-5			2.2018+3		1.0276-1
1.0000-0	6.0000-0	4.4745+4	7.4523-1							1.8070-5			1.8875+3		1.0276-1
1.0000-0	7.0000-0	3.8677+4	7.4415+0							1.6877-5			1.5810+3		1.0276-1
1.0000-0	8.0000-0	3.2578+4	7.4298-1							1.4869-5			1.2861+3		1.0276-1
1.0000-0	9.0000-0	2.6487+4	7.4187+0							1.2861-5			1.0171+3		1.0276-1
1.0000-0	1.0000-0	2.0396+4	7.4070-1							1.0851-5			7.3150+3		5.7981-2
1.0000-0	2.0000-0	1.4303+4	9.9634+0							9.5277-6			6.5607+3		1.0171+1
1.0000-0	3.0000-0	8.7944+4	9.2337+0							8.3527-6			5.8322+3		1.0226+1
1.0000-0	4.0000-0	7.9841+4	8.5070+0							7.4475-6			5.0942+3		2.9845+1
1.0000-0	5.0000-0	7.1723+4	7.7823+0							6.4495-6			4.3542+3		2.9845+1
1.0000-0	6.0000-0	6.3606+4	7.0568+0							5.3369-6			3.6166+3		2.9845+1
1.0000-0	7.0000-0	5.5488+4	6.3410+0							4.7019-6			2.8904+3		2.9845+1
1.0000-0	8.0000-0	4.7370+4	5.6241+0							4.0938-6			2.1744+3		2.9845+1
1.0000-0	9.0000-0	3.9252+4	4.9091+0							3.4793-6			1.4574+3		2.9845+1
1.0000-0	1.0000-0	3.1134+4	4.1942+0							2.8645-6			7.9261+3		1.8226+1
1.0000-0	2.0000-0	2.3016+4	3.4793+0							2.2497-6			7.0310+3		1.8226+1
1.0000-0	3.0000-0	1.4900+4	2.7644+0							1.6347-6			6.1361+3		1.8226+1
1.0000-0	4.0000-0	7.0310+4	2.0500+0							1.0202-6			5.2401+3		1.8226+1
1.0000-0	5.0000-0	6.1361+4	1.3351+0							4.6277-6			4.3452+3		1.8226+1
1.0000-0	6.0000-0	5.2401+4	6.0680+0							4.0129-6			3.4503+3		1.8226+1
1.0000-0	7.0000-0	4.3452+4	5.3351+0							3.4000-6			2.5554+3		1.8226+1
1.0000-0	8.0000-0	3.4503+4	4.6399+0							2.7877-6			1.6605+3		1.8226+1
1.0000-0	9.0000-0	2.5554+4	3.9448+0							2.1754-6			8.0937+3		1.8226+1
1.0000-0	1.0000-0	1.7400+4	3.2497+0							1.5629-6			7.1976+3		1.8226+1
1.0000-0	2.0000-0	9.0937+4	2.5554+0							9.4899-6			6.3028+3		1.8226+1
1.0000-0	3.0000-0	8.1976+4	1.8226+0							8.5877-6			5.4079+3		1.8226+1
1.0000-0	4.0000-0	7.2927+4	1.1076+0							7.6856-6			4.5130+3		1.8226+1
1.0000-0	5.0000-0	6.3878+4	4.8396+0							6.7835-6			3.6181+3		1.8226+1
1.0000-0	6.0000-0	5.4829+4	4.1347+0							5.8814-6			2.7232+3		1.8226+1
1.0000-0	7.0000-0	4.5780+4	3.4298+0												

CROSS SECTION

MATERIAL =2041	ENERGY	TOTAL	ELASTIC	INELR	(N.2N)	(N.3N)	FISSION	(N.NR)	(N.NP)	CAPTURE	(N.P)	(N.D)	(N.R)	RU-BRR
1.0000-5	~ 1.0000-2	6.0287+0	6.0000+0							2.3436-2				7.4415-2
1.0000-	~ 1.5000-	6.0143+0	6.0000+0							1.0867-				7.4415-
1.5000-	~ 2.0000-	6.0111+0	6.0000+0							7.6819-				7.4415-
2.0000-	~ 3.0000-	6.0080+0	6.0000+0							6.4782-				7.4415-
3.0000-	~ 4.0000-	6.0067+0	6.0000+0							5.7074-				7.4415-
4.0000-	~ 5.0000-	6.0058+0	6.0000+0							5.1557-				7.4415-
5.0000-	~ 6.0000-	6.0048+0	6.0000+0							4.6809-				7.4415-
6.0000-	~ 8.0000-	6.0041+0	6.0000+0							4.0357-				7.4415-
1.0000-	~ 1.5000-	6.0035+0	6.0000+0							3.4365-				7.4415-
1.5000-	~ 2.0000-	6.0028+0	6.0000+0							2.8971-				7.4415-
2.0000-	~ 3.0000-	6.0024+0	6.0000+0							2.4300-				7.4415-
3.0000-	~ 4.0000-	6.0021+0	6.0000+0							2.0489-				7.4415-
4.0000-	~ 5.0000-	6.0019+0	6.0000+0							1.6316-				7.4415-
5.0000-	~ 6.0000-	6.0018+0	6.0000+0							1.4488-				7.4415-
6.0000-	~ 8.0000-	6.0013+0	6.0000+0							1.2762-				7.4415-
1.0000+0	~ 1.5000+0	6.0011+0	6.0000+0							1.0867-				7.4415-
1.5000+0	~ 2.0000+0	6.0010+0	6.0000+0							9.0872-				7.4415-
2.0000+0	~ 3.0000+0	6.0008+0	6.0000+0							7.6819-				7.4415-
3.0000+0	~ 4.0000+0	6.0007+0	6.0000+0							6.4782-				7.4415-
4.0000+0	~ 5.0000+0	6.0006+0	6.0000+0							5.7074-				7.4415-
5.0000+0	~ 6.0000+0	6.0005+0	6.0000+0							5.1557-				7.4415-
6.0000+0	~ 8.0000+0	6.0004+0	6.0000+0							4.6809-				7.4415-
1.0000+0	~ 1.5000+0	6.0004+0	6.0000+0							4.0357-				7.4415-
1.5000+0	~ 2.0000+0	6.0003+0	6.0000+0							3.4365-				7.4415-
2.0000+0	~ 3.0000+0	6.0003+0	6.0000+0							2.8971-				7.4415-
3.0000+0	~ 4.0000+0	6.0002+0	6.0000+0							2.4300-				7.4415-
4.0000+0	~ 5.0000+0	6.0002+0	6.0000+0							2.0489-				7.4415-
5.0000+0	~ 6.0000+0	6.0002+0	6.0000+0							1.6316-				7.4415-
6.0000+0	~ 8.0000+0	6.0002+0	6.0000+0							1.4488-				7.4415-
1.0000+0	~ 1.5000+0	6.0001+0	6.0000+0							1.2762-				7.4415-
1.5000+0	~ 2.0000+0	6.0001+0	6.0000+0							1.0867-				7.4415-
2.0000+0	~ 3.0000+0	6.0001+0	6.0000+0							9.1616-				7.4415-
3.0000+0	~ 4.0000+0	6.0001+0	6.0000+0							7.6819-				7.4415-
4.0000+0	~ 5.0000+0	6.0001+0	6.0000+0							6.4782-				7.4415-
5.0000+0	~ 6.0000+0	6.0001+0	6.0000+0							5.7074-				7.4415-
6.0000+0	~ 8.0000+0	6.0001+0	6.0000+0							5.1557-				7.4415-
1.0000+0	~ 1.5000+0	6.0000+0	6.0000+0							4.6809-				7.4415-
1.5000+0	~ 2.0000+0	6.0000+0	6.0000+0							4.0357-				7.4415-
2.0000+0	~ 3.0000+0	6.0000+0	6.0000+0							3.4365-				7.4415-
3.0000+0	~ 4.0000+0	6.0000+0	6.0000+0							2.8971-				7.4415-
4.0000+0	~ 5.0000+0	6.0000+0	6.0000+0							2.4300-				7.4415-
5.0000+0	~ 6.0000+0	6.0000+0	6.0000+0							2.0489-				7.4415-
6.0000+0	~ 8.0000+0	6.0000+0	6.0000+0							1.6316-				7.4415-
1.0000+0	~ 1.5000+0	6.0000+0	6.0000+0							1.4488-				7.4415-
1.5000+0	~ 2.0000+0	6.0000+0	6.0000+0							1.2762-				7.4415-
2.0000+0	~ 3.0000+0	6.0000+0	6.0000+0							1.0867-				7.4415-
3.0000+0	~ 4.0000+0	6.0000+0	6.0000+0							9.1616-				7.4415-
4.0000+0	~ 5.0000+0	6.0000+0	6.0000+0							7.6819-				7.4415-
5.0000+0	~ 6.0000+0	6.0000+0	6.0000+0							6.4782-				7.4415-
6.0000+0	~ 8.0000+0	6.0000+0	6.0000+0							5.7074-				7.4415-
1.0000+0	~ 1.5000+0	6.0000+0	6.0000+0							5.1557-				7.4415-
1.5000+0	~ 2.0000+0	6.0000+0	6.0000+0							4.6809-				7.4415-
2.0000+0	~ 3.0000+0	6.0000+0	6.0000+0							4.0357-				7.4415-
3.0000+0	~ 4.0000+0	6.0000+0	6.0000+0							3.4365-				7.4415-
4.0000+0	~ 5.0000+0	6.0000+0	6.0000+0							2.8971-				7.4415-
5.0000+0	~ 6.0000+0	6.0000+0	6.0000+0							2.4300-				7.4415-
6.0000+0	~ 8.0000+0	6.0000+0	6.0000+0							2.0489-				7.4415-
1.0000+0	~ 1.5000+0	6.0000+0	6.0000+0							1.6316-				7.4415-
1.5000+0	~ 2.0000+0	6.0000+0	6.0000+0							1.4488-				7.4415-
2.0000+0	~ 3.0000+0	6.0000+0	6.0000+0							1.2762-				7.4415-
3.0000+0	~ 4.0000+0	6.0000+0	6.0000+0							1.0867-				7.4415-
4.0000+0	~ 5.0000+0	6.0000+0	6.0000+0							9.1616-				7.4415-
5.0000+0	~ 6.0000+0	6.0000+0	6.0000+0							7.6819-				7.4415-
6.0000+0	~ 8.0000+0	6.0000+0	6.0000+0							6.4782-				7.4415-
1.0000+0	~ 1.5000+0	6.0000+0	6.0000+0							5.7074-				7.4415-
1.5000+0	~ 2.0000+0	6.0000+0	6.0000+0							5.1557-				7.4415-
2.0000+0	~ 3.0000+0	6.0000+0	6.0000+0							4.6809-				7.4415-
3.0000+0	~ 4.0000+0	6.0000+0	6.0000+0							4.0357-				7.4415-
4.0000+0	~ 5.0000+0	6.0000+0	6.0000+0							3.4365-				7.4415-
5.0000+0	~ 6.0000+0	6.0000+0	6.0000+0							2.8971-				7.4415-
6.0000+0	~ 8.0000+0	6.0000+0	6.0000+0							2.4300-				7.4415-
1.0000+0	~ 1.5000+0	6.0000+0	6.0000+0							2.0489-				7.4415-
1.5000+0	~ 2.0000+0	6.0000+0	6.0000+0							1.6316-				7.4415-
2.0000+0	~ 3.0000+0	6.0000+0	6.0000+0							1.4488-				7.4415-
3.0000+0	~ 4.0000+0	6.0000+0	6.0000+0							1.2762-				7.4415-
4.0000+0	~ 5.0000+0	6.0000+0	6.0000+0							1.0867-				7.4415-
5.0000+0	~ 6.0000+0	6.0000+0	6.0000+0							9.1616-				7.4415-
6.0000+0	~ 8.0000+0	6.0000+0	6.0000+0							7.6819-				7.4415-
1.0000+0	~ 1.5000+0	6.0000+0	6.0000+0							6.4782-				7.4415-
1.5000+0	~ 2.0000+0	6.0000+0	6.0000+0							5.7074-				7.4415-
2.0000+0	~ 3.0000+0	6.0000+0	6.0000+0							5.1557-				7.4415-
3.0000+0	~ 4.0000+0	6.0000+0	6.0000+0							4.6809-				7.4415-
4.0000+0	~ 5.0000+0	6.0000+0	6.0000+0							4.0357-				7.4415-
5.0000+0	~ 6.0000+0	6.0000+0	6.0000+0							3.4365-				7.4415-
6.0000+0	~ 8.0000+0	6.0000+0	6.0000+0							2.8971-				7.4415-
1.0000+0	~ 1.5000+0	6.0000+0	6.0000+0							2.4300-				7.4415-
1.5000+0	~ 2.0000+0	6.0000+0	6.0000+0							2.0489-				7.4415-
2.0000+0	~ 3.0000+0	6.0000+0	6.0000+0							1.6316-				7.4415-
3.0000+0	~ 4.0000+0	6.0000+0	6.0000+0							1.4488-				7.4415-
4.0000+0	~ 5.0000+0	6.0000+0	6.0000+0							1.2762-				7.4415-
5.0000+0	~ 6.0000+0	6.0000+0	6.0000+0							1.0867-</				

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CROSS SECTION

MATERIAL = Z081

ENERGY	TOTAL	ELASTIC	INEL	(N.2N)	(N.3N)	FISSION	(N.HR)	(N.MP)	CAPTURE	(N.P)	(N.D)	(N.A)	MU-BAR
1.0000-5 ~ 1.0000-2	4.7132* 0	4.6990* 0							1.0484- 2				5.6336- 2
1.0000-2 ~ 1.5000-2	4.7053* 0	4.6990* 0							4.8617- 3				5.6336- 2
1.5000-2 ~ 2.0000-2	4.7038* 0	4.6990* 0							4.0986- 3				5.6336- 2
2.0000-2 ~ 3.0000-2	4.7025* 0	4.6990* 0							3.4672- 3				5.6336- 2
3.0000-2 ~ 4.0000-2	4.7016* 0	4.6990* 0							2.9533- 3				5.6336- 2
4.0000-2 ~ 5.0000-2	4.7011* 0	4.6990* 0							2.5083- 3				5.6336- 2
5.0000-2 ~ 6.0000-2	4.7008* 0	4.6990* 0							2.0493- 3				5.6336- 2
6.0000-2 ~ 1.0000-1	4.7006* 0	4.6990* 0							1.6055- 3				5.6336- 2
1.0000-1 ~ 1.5000-1	4.7004* 0	4.6990* 0							1.2974- 3				5.6336- 2
1.5000-1 ~ 2.0000-1	4.7003* 0	4.6990* 0							1.0871- 3				5.6336- 2
2.0000-1 ~ 3.0000-1	4.7001* 0	4.6990* 0							9.1548- 4				5.6336- 2
3.0000-1 ~ 4.0000-1	4.7000* 0	4.6990* 0							8.0743- 4				5.6336- 2
4.0000-1 ~ 5.0000-1	4.6998* 0	4.6990* 0							7.2862- 4				5.6336- 2
5.0000-1 ~ 6.0000-1	4.6997* 0	4.6990* 0							6.7024- 4				5.6336- 2
6.0000-1 ~ 1.0000-0	4.6996* 0	4.6990* 0							6.2534- 4				5.6336- 2
1.0000+0 ~ 1.5000+0	4.6995* 0	4.6990* 0							5.9117- 4				5.6336- 2
1.5000+0 ~ 2.0000+0	4.6994* 0	4.6990* 0							4.8999- 4				5.6336- 2
2.0000+0 ~ 3.0000+0	4.6993* 0	4.6990* 0							4.0999- 4				5.6336- 2
3.0000+0 ~ 4.0000+0	4.6992* 0	4.6990* 0							3.5999- 4				5.6336- 2
4.0000+0 ~ 5.0000+0	4.6991* 0	4.6990* 0							3.2599- 4				5.6336- 2
5.0000+0 ~ 6.0000+0	4.6990* 0	4.6990* 0							2.9899- 4				5.6336- 2
6.0000+0 ~ 1.0000-1	4.6989* 0	4.6990* 0							2.7499- 4				5.6336- 2
1.0000-1 ~ 1.5000-1	4.6988* 0	4.6990* 0							2.5299- 4				5.6336- 2
1.5000-1 ~ 2.0000-1	4.6987* 0	4.6990* 0							2.3299- 4				5.6336- 2
2.0000-1 ~ 3.0000-1	4.6986* 0	4.6990* 0							2.1499- 4				5.6336- 2
3.0000-1 ~ 4.0000-1	4.6985* 0	4.6990* 0							2.0099- 4				5.6336- 2
4.0000-1 ~ 5.0000-1	4.6984* 0	4.6990* 0							1.8999- 4				5.6336- 2
5.0000-1 ~ 6.0000-1	4.6983* 0	4.6990* 0							1.8099- 4				5.6336- 2
6.0000-1 ~ 1.0000-0	4.6982* 0	4.6990* 0							1.7399- 4				5.6336- 2
1.0000-0 ~ 1.5000-0	4.6981* 0	4.6990* 0							1.6899- 4				5.6336- 2
1.5000-0 ~ 2.0000-0	4.6980* 0	4.6990* 0							1.6499- 4				5.6336- 2
2.0000-0 ~ 3.0000-0	4.6979* 0	4.6990* 0							1.6199- 4				5.6336- 2
3.0000-0 ~ 4.0000-0	4.6978* 0	4.6990* 0							1.5999- 4				5.6336- 2
4.0000-0 ~ 5.0000-0	4.6977* 0	4.6990* 0							1.5799- 4				5.6336- 2
5.0000-0 ~ 6.0000-0	4.6976* 0	4.6990* 0							1.5699- 4				5.6336- 2
6.0000-0 ~ 1.0000-1	4.6975* 0	4.6990* 0							1.5599- 4				5.6336- 2
1.0000-1 ~ 1.5000-1	4.6974* 0	4.6990* 0							1.5499- 4				5.6336- 2
1.5000-1 ~ 2.0000-1	4.6973* 0	4.6990* 0							1.5399- 4				5.6336- 2
2.0000-1 ~ 3.0000-1	4.6972* 0	4.6990* 0							1.5299- 4				5.6336- 2
3.0000-1 ~ 4.0000-1	4.6971* 0	4.6990* 0							1.5199- 4				5.6336- 2
4.0000-1 ~ 5.0000-1	4.6970* 0	4.6990* 0							1.5099- 4				5.6336- 2
5.0000-1 ~ 6.0000-1	4.6969* 0	4.6990* 0							1.4999- 4				5.6336- 2
6.0000-1 ~ 1.0000-0	4.6968* 0	4.6990* 0							1.4899- 4				5.6336- 2
1.0000-0 ~ 1.5000-0	4.6967* 0	4.6990* 0							1.4799- 4				5.6336- 2
1.5000-0 ~ 2.0000-0	4.6966* 0	4.6990* 0							1.4699- 4				5.6336- 2
2.0000-0 ~ 3.0000-0	4.6965* 0	4.6990* 0							1.4599- 4				5.6336- 2
3.0000-0 ~ 4.0000-0	4.6964* 0	4.6990* 0							1.4499- 4				5.6336- 2
4.0000-0 ~ 5.0000-0	4.6963* 0	4.6990* 0							1.4399- 4				5.6336- 2
5.0000-0 ~ 6.0000-0	4.6962* 0	4.6990* 0							1.4299- 4				5.6336- 2
6.0000-0 ~ 1.0000-1	4.6961* 0	4.6990* 0							1.4199- 4				5.6336- 2
1.0000-1 ~ 1.5000-1	4.6960* 0	4.6990* 0							1.4099- 4				5.6336- 2
1.5000-1 ~ 2.0000-1	4.6959* 0	4.6990* 0							1.3999- 4				5.6336- 2
2.0000-1 ~ 3.0000-1	4.6958* 0	4.6990* 0							1.3899- 4				5.6336- 2
3.0000-1 ~ 4.0000-1	4.6957* 0	4.6990* 0							1.3799- 4				5.6336- 2
4.0000-1 ~ 5.0000-1	4.6956* 0	4.6990* 0							1.3699- 4				5.6336- 2
5.0000-1 ~ 6.0000-1	4.6955* 0	4.6990* 0							1.3599- 4				5.6336- 2
6.0000-1 ~ 1.0000-0	4.6954* 0	4.6990* 0							1.3499- 4				5.6336- 2
1.0000-0 ~ 1.5000-0	4.6953* 0	4.6990* 0							1.3399- 4				5.6336- 2
1.5000-0 ~ 2.0000-0	4.6952* 0	4.6990* 0							1.3299- 4				5.6336- 2
2.0000-0 ~ 3.0000-0	4.6951* 0	4.6990* 0							1.3199- 4				5.6336- 2
3.0000-0 ~ 4.0000-0	4.6950* 0	4.6990* 0							1.3099- 4				5.6336- 2
4.0000-0 ~ 5.0000-0	4.6949* 0	4.6990* 0							1.2999- 4				5.6336- 2
5.0000-0 ~ 6.0000-0	4.6948* 0	4.6990* 0							1.2899- 4				5.6336- 2
6.0000-0 ~ 1.0000-1	4.6947* 0	4.6990* 0							1.2799- 4				5.6336- 2
1.0000-1 ~ 1.5000-1	4.6946* 0	4.6990* 0							1.2699- 4				5.6336- 2
1.5000-1 ~ 2.0000-1	4.6945* 0	4.6990* 0							1.2599- 4				5.6336- 2
2.0000-1 ~ 3.0000-1	4.6944* 0	4.6990* 0							1.2499- 4				5.6336- 2
3.0000-1 ~ 4.0000-1	4.6943* 0	4.6990* 0							1.2399- 4				5.6336- 2
4.0000-1 ~ 5.0000-1	4.6942* 0	4.6990* 0							1.2299- 4				5.6336- 2
5.0000-1 ~ 6.0000-1	4.6941* 0	4.6990* 0							1.2199- 4				5.6336- 2
6.0000-1 ~ 1.0000-0	4.6940* 0	4.6990* 0							1.2099- 4				5.6336- 2
1.0000-0 ~ 1.5000-0	4.6939* 0	4.6990* 0							1.1999- 4				5.6336- 2
1.5000-0 ~ 2.0000-0	4.6938* 0	4.6990* 0							1.1899- 4				5.6336- 2
2.0000-0 ~ 3.0000-0	4.6937* 0	4.6990* 0							1.1799- 4				5.6336- 2
3.0000-0 ~ 4.0000-0	4.6936* 0	4.6990* 0							1.1699- 4				5.6336- 2
4.0000-0 ~ 5.0000-0	4.6935* 0	4.6990* 0							1.1599- 4				5.6336- 2
5.0000-0 ~ 6.0000-0	4.6934* 0	4.6990* 0							1.1499- 4				5.6336- 2
6.0000-0 ~ 1.0000-1	4.6933* 0	4.6990* 0							1.1399- 4				5.6336- 2
1.0000-1 ~ 1.5000-1	4.6932* 0	4.6990* 0							1.1299- 4				5.6336- 2
1.5000-1 ~ 2.0000-1	4.6931* 0	4.6990* 0							1.1199- 4				5.6336- 2
2.0000-1 ~ 3.0000-1	4.6930* 0	4.6990* 0							1.1099- 4				5.6336- 2
3.0000-1 ~ 4.0000-1	4.6929* 0	4.6990* 0							1.0999- 4				5.6336- 2
4.0000-1 ~ 5.0000-1	4.6928* 0	4.6990* 0							1.0899- 4				5.6336- 2
5.0000-1 ~ 6.0000-1	4.6927* 0	4.6990* 0							1.0799- 4				5.6336- 2
6.0000-1 ~ 1.0000-0	4.6926* 0	4.6990* 0							1.0699- 4				5.6336- 2
1.0000-0 ~ 1.5000-0	4.6925* 0	4.6990* 0							1.0599- 4				5.6336- 2
1.5000-0 ~ 2.0000-0	4.6924* 0	4.6990* 0							1.0499- 4				5.6336- 2
2.0000-0 ~ 3.0000-0	4.6923* 0	4.6990* 0							1.0399- 4				5.6336- 2
3.0000-0 ~ 4.0000-0	4.6922* 0	4.6990* 0											

MATERIAL = 2091 CROSS SECTION F - 19

MATERIAL = 2091	ENERGY	TOTAL	ELASTIC	INELA	(N.2N)	(N.3N)	FUSION	(N.MR)	(N.NR)	(N.PI)	(N.D)	(N.R)	MU-BRR
1.0000	5	1.0000	2	3.6716	0	3.6410	0	2.9644	2	3.5395	2	3.5395	2
1.0000	1	1.5000	0	3.6500	0	3.6410	0	1.3722	2	3.5395	2	3.5395	2
1.0000	2	2.0000	0	3.6500	0	3.6410	0	1.7074	2	3.5395	2	3.5395	2
1.0000	3	3.0000	0	3.6506	0	3.6410	0	1.9660	3	3.5395	2	3.5395	2
1.0000	4	4.0000	0	3.6506	0	3.6410	0	2.2200	3	3.5395	2	3.5395	2
1.0000	5	5.0000	0	3.6506	0	3.6410	0	2.5229	3	3.5395	2	3.5395	2
1.0000	6	6.0000	0	3.6506	0	3.6410	0	2.8599	3	3.5395	2	3.5395	2
1.0000	7	7.0000	0	3.6506	0	3.6410	0	3.1894	3	3.5395	2	3.5395	2
1.0000	8	8.0000	0	3.6506	0	3.6410	0	3.5471	3	3.5395	2	3.5395	2
1.0000	9	9.0000	0	3.6506	0	3.6410	0	3.9346	3	3.5395	2	3.5395	2
1.0000	10	1.0000	0	3.6506	0	3.6410	0	4.3471	3	3.5395	2	3.5395	2
1.0000	11	1.5000	0	3.6506	0	3.6410	0	4.7851	3	3.5395	2	3.5395	2
1.0000	12	2.0000	0	3.6506	0	3.6410	0	5.2496	3	3.5395	2	3.5395	2
1.0000	13	3.0000	0	3.6506	0	3.6410	0	5.7409	3	3.5395	2	3.5395	2
1.0000	14	4.0000	0	3.6506	0	3.6410	0	6.2593	3	3.5395	2	3.5395	2
1.0000	15	5.0000	0	3.6506	0	3.6410	0	6.8053	3	3.5395	2	3.5395	2
1.0000	16	6.0000	0	3.6506	0	3.6410	0	7.3793	3	3.5395	2	3.5395	2
1.0000	17	7.0000	0	3.6506	0	3.6410	0	7.9813	3	3.5395	2	3.5395	2
1.0000	18	8.0000	0	3.6506	0	3.6410	0	8.6113	3	3.5395	2	3.5395	2
1.0000	19	1.0000	0	3.6506	0	3.6410	0	9.2693	3	3.5395	2	3.5395	2
1.0000	20	1.5000	0	3.6506	0	3.6410	0	9.9543	3	3.5395	2	3.5395	2
1.0000	21	2.0000	0	3.6506	0	3.6410	0	10.6673	3	3.5395	2	3.5395	2
1.0000	22	3.0000	0	3.6506	0	3.6410	0	11.4093	3	3.5395	2	3.5395	2
1.0000	23	4.0000	0	3.6506	0	3.6410	0	12.1813	3	3.5395	2	3.5395	2
1.0000	24	5.0000	0	3.6506	0	3.6410	0	13.0003	3	3.5395	2	3.5395	2
1.0000	25	6.0000	0	3.6506	0	3.6410	0	13.8653	3	3.5395	2	3.5395	2
1.0000	26	7.0000	0	3.6506	0	3.6410	0	14.7763	3	3.5395	2	3.5395	2
1.0000	27	8.0000	0	3.6506	0	3.6410	0	15.7333	3	3.5395	2	3.5395	2
1.0000	28	1.0000	0	3.6506	0	3.6410	0	16.7363	3	3.5395	2	3.5395	2
1.0000	29	1.5000	0	3.6506	0	3.6410	0	17.7853	3	3.5395	2	3.5395	2
1.0000	30	2.0000	0	3.6506	0	3.6410	0	18.8803	3	3.5395	2	3.5395	2
1.0000	31	3.0000	0	3.6506	0	3.6410	0	20.0213	3	3.5395	2	3.5395	2
1.0000	32	4.0000	0	3.6506	0	3.6410	0	21.2083	3	3.5395	2	3.5395	2
1.0000	33	5.0000	0	3.6506	0	3.6410	0	22.4413	3	3.5395	2	3.5395	2
1.0000	34	6.0000	0	3.6506	0	3.6410	0	23.7203	3	3.5395	2	3.5395	2
1.0000	35	7.0000	0	3.6506	0	3.6410	0	25.0453	3	3.5395	2	3.5395	2
1.0000	36	8.0000	0	3.6506	0	3.6410	0	26.4163	3	3.5395	2	3.5395	2
1.0000	37	1.0000	0	3.6506	0	3.6410	0	27.8333	3	3.5395	2	3.5395	2
1.0000	38	1.5000	0	3.6506	0	3.6410	0	29.2963	3	3.5395	2	3.5395	2
1.0000	39	2.0000	0	3.6506	0	3.6410	0	30.8053	3	3.5395	2	3.5395	2
1.0000	40	3.0000	0	3.6506	0	3.6410	0	32.3593	3	3.5395	2	3.5395	2
1.0000	41	4.0000	0	3.6506	0	3.6410	0	33.9583	3	3.5395	2	3.5395	2
1.0000	42	5.0000	0	3.6506	0	3.6410	0	35.6023	3	3.5395	2	3.5395	2
1.0000	43	6.0000	0	3.6506	0	3.6410	0	37.2913	3	3.5395	2	3.5395	2
1.0000	44	7.0000	0	3.6506	0	3.6410	0	39.0253	3	3.5395	2	3.5395	2
1.0000	45	8.0000	0	3.6506	0	3.6410	0	40.8043	3	3.5395	2	3.5395	2
1.0000	46	1.0000	0	3.6506	0	3.6410	0	42.6283	3	3.5395	2	3.5395	2
1.0000	47	1.5000	0	3.6506	0	3.6410	0	44.4973	3	3.5395	2	3.5395	2
1.0000	48	2.0000	0	3.6506	0	3.6410	0	46.4113	3	3.5395	2	3.5395	2
1.0000	49	3.0000	0	3.6506	0	3.6410	0	48.3703	3	3.5395	2	3.5395	2
1.0000	50	4.0000	0	3.6506	0	3.6410	0	50.3743	3	3.5395	2	3.5395	2
1.0000	51	5.0000	0	3.6506	0	3.6410	0	52.4233	3	3.5395	2	3.5395	2
1.0000	52	6.0000	0	3.6506	0	3.6410	0	54.5173	3	3.5395	2	3.5395	2
1.0000	53	7.0000	0	3.6506	0	3.6410	0	56.6563	3	3.5395	2	3.5395	2
1.0000	54	8.0000	0	3.6506	0	3.6410	0	58.8393	3	3.5395	2	3.5395	2
1.0000	55	1.0000	0	3.6506	0	3.6410	0	61.0673	3	3.5395	2	3.5395	2
1.0000	56	1.5000	0	3.6506	0	3.6410	0	63.3403	3	3.5395	2	3.5395	2
1.0000	57	2.0000	0	3.6506	0	3.6410	0	65.6583	3	3.5395	2	3.5395	2
1.0000	58	3.0000	0	3.6506	0	3.6410	0	68.0213	3	3.5395	2	3.5395	2
1.0000	59	4.0000	0	3.6506	0	3.6410	0	70.4293	3	3.5395	2	3.5395	2
1.0000	60	5.0000	0	3.6506	0	3.6410	0	72.8823	3	3.5395	2	3.5395	2
1.0000	61	6.0000	0	3.6506	0	3.6410	0	75.3803	3	3.5395	2	3.5395	2
1.0000	62	7.0000	0	3.6506	0	3.6410	0	77.9233	3	3.5395	2	3.5395	2
1.0000	63	8.0000	0	3.6506	0	3.6410	0	80.5113	3	3.5395	2	3.5395	2
1.0000	64	1.0000	0	3.6506	0	3.6410	0	83.1443	3	3.5395	2	3.5395	2
1.0000	65	1.5000	0	3.6506	0	3.6410	0	85.8223	3	3.5395	2	3.5395	2
1.0000	66	2.0000	0	3.6506	0	3.6410	0	88.5453	3	3.5395	2	3.5395	2
1.0000	67	3.0000	0	3.6506	0	3.6410	0	91.3133	3	3.5395	2	3.5395	2
1.0000	68	4.0000	0	3.6506	0	3.6410	0	94.1263	3	3.5395	2	3.5395	2
1.0000	69	5.0000	0	3.6506	0	3.6410	0	96.9843	3	3.5395	2	3.5395	2
1.0000	70	6.0000	0	3.6506	0	3.6410	0	99.8873	3	3.5395	2	3.5395	2
1.0000	71	7.0000	0	3.6506	0	3.6410	0	102.8353	3	3.5395	2	3.5395	2
1.0000	72	8.0000	0	3.6506	0	3.6410	0	105.8283	3	3.5395	2	3.5395	2
1.0000	73	1.0000	0	3.6506	0	3.6410	0	108.8663	3	3.5395	2	3.5395	2
1.0000	74	1.5000	0	3.6506	0	3.6410	0	111.9493	3	3.5395	2	3.5395	2
1.0000	75	2.0000	0	3.6506	0	3.6410	0	115.0773	3	3.5395	2	3.5395	2
1.0000	76	3.0000	0	3.6506	0	3.6410	0	118.2503	3	3.5395	2	3.5395	2
1.0000	77	4.0000	0	3.6506	0	3.6410	0	121.4683	3	3.5395	2	3.5395	2
1.0000	78	5.0000	0	3.6506	0	3.6410	0	124.7313	3	3.5395	2	3.5395	2
1.0000	79	6.0000	0	3.6506	0	3.6410	0	128.0393	3	3.5395	2	3.5395	2
1.0000	80	7.0000	0	3.6506	0	3.6410	0	131.3923	3	3.5395	2	3.5395	2
1.0000	81	8.0000	0	3.6506	0	3.6410	0	134.7903	3	3.5395	2	3.5395	2
1.0000	82	1.0000	0	3.6506	0	3.6410	0	138.2333	3	3.5395	2	3.5395	2
1.0000	83	1.5000	0	3.6506	0	3.6410	0	141.7213	3	3.5395	2	3.5395	2
1.0000	84	2.0000	0	3.6506	0	3.6410	0	145.2543	3	3.5395	2	3.5395	2
1.0000	85	3.0000	0	3.6506									

MATERIAL -2111 CROSS SECTION NR-23

ENERGY	TOTAL	ELASTIC	INEL	(N.ZN)	(N.ZN)	FISSION	(N.WR)	(N.NP)	CAPTURE	(N.P)	(N.D)	(N.A)	MU-BRR
1.0000-5 ~ 1.0000-2	4.8450+ 0	3.1987+ 0							1.6503+ 0				2.8239- 2
1.0000-4	3.9878+ 0	3.1843+ 0							7.5578- 1				2.0298- 2
1.0000-3	3.1932+ 0	3.1732+ 0							5.3576- 1				2.0298- 2
1.0000-2	2.5554+ 0	3.1654+ 0							4.5164+ 0				2.0298- 2
1.0000-1	2.1609+ 0	3.1616+ 0							3.9786- 1				2.0298- 2
5.0000-2	3.5695+ 0	3.1875+ 0							3.5938- 1				2.0298- 2
6.0000-2	3.5194+ 0	3.1983+ 0							2.8087- 1				2.0298- 2
8.0000-2	3.4923+ 0	3.2113+ 0							2.3912- 1				2.0298- 2
1.0000-1	3.4641+ 0	3.2068+ 0							2.0158- 1				2.0298- 2
1.5000-1	3.4323+ 0	3.1978+ 0							1.4289- 1				2.0298- 2
2.0000-1	3.3977+ 0	3.1892+ 0							1.0528- 1				2.0298- 2
3.0000-1	3.3517+ 0	3.1812+ 0							1.2657- 1				2.0298- 2
4.0000-1	3.3044+ 0	3.1744+ 0							1.1352- 1				2.0298- 2
5.0000-1	3.2572+ 0	3.1680+ 0							1.0078- 1				2.0298- 2
6.0000-1	3.2117+ 0	3.1628+ 0							8.6788- 2				2.0298- 2
1.0000+ 0	3.1925+ 0	3.158+ 0							7.5617- 2				2.0298- 2
2.0000+ 0	3.1752+ 0	3.1498+ 0							6.9765- 2				2.0298- 2
3.0000+ 0	3.1687+ 0	3.1412+ 0							5.4044- 2				2.0298- 2
4.0000+ 0	3.1633+ 0	3.1325+ 0							4.6336- 2				2.0298- 2
5.0000+ 0	3.1573+ 0	3.1238+ 0							3.7328- 2				2.0298- 2
6.0000+ 0	3.1522+ 0	3.1152+ 0							3.3900- 2				2.0298- 2
8.0000+ 0	3.1522+ 0	3.1152+ 0							3.0242- 2				2.0298- 2
1.0000+ 1	3.1492+ 0	3.1209+ 0							2.6159- 2				2.0298- 2
1.5000+ 1	3.1475+ 0	3.1202+ 0							2.3908- 2				2.0298- 2
2.0000+ 1	3.1459+ 0	3.1190+ 0							1.8138- 2				2.0298- 2
3.0000+ 1	3.1445+ 0	3.1179+ 0							1.6410- 2				2.0298- 2
4.0000+ 1	3.1433+ 0	3.1168+ 0							1.4639- 2				2.0298- 2
5.0000+ 1	3.1422+ 0	3.1155+ 0							1.3367- 2				2.0298- 2
6.0000+ 1	3.1412+ 0	3.1143+ 0							1.2006- 2				2.0298- 2
8.0000+ 1	3.1403+ 0	3.1136+ 0							1.0711- 2				2.0298- 2
1.0000+ 2	3.1395+ 0	3.1128+ 0							9.3828- 3				2.0298- 2
1.5000+ 2	3.1388+ 0	3.1120+ 0							8.2120- 3				2.0298- 2
2.0000+ 2	3.1381+ 0	3.1112+ 0							7.4072- 3				2.0298- 2
3.0000+ 2	3.1375+ 0	3.1104+ 0							6.8652- 3				2.0298- 2
4.0000+ 2	3.1369+ 0	3.1095+ 0							6.4652- 3				2.0298- 2
5.0000+ 2	3.1363+ 0	3.1087+ 0							6.2992- 3				2.0298- 2
6.0000+ 2	3.1357+ 0	3.1079+ 0							6.3853- 3				2.0298- 2
8.0000+ 2	3.1351+ 0	3.1071+ 0							6.3360- 3				2.0298- 2
1.0000+ 3	3.1345+ 0	3.1063+ 0							8.7276- 3				2.0298- 2
1.5000+ 3	3.1339+ 0	3.1055+ 0							1.5728- 3				2.0298- 2
2.0000+ 3	3.1333+ 0	3.1047+ 0							1.4447- 3				2.0298- 2
3.0000+ 3	3.1327+ 0	3.1039+ 0							1.3269- 3				2.0298- 2
4.0000+ 3	3.1321+ 0	3.1031+ 0							1.2182- 3				2.0298- 2
5.0000+ 3	3.1315+ 0	3.1023+ 0							1.1195- 3				2.0298- 2
6.0000+ 3	3.1309+ 0	3.1015+ 0							1.0208- 3				2.0298- 2
8.0000+ 3	3.1303+ 0	3.1007+ 0							8.7276- 3				2.0298- 2
1.0000+ 4	3.1297+ 0	3.1000+ 0							1.5728- 3				2.0298- 2
1.5000+ 4	3.1291+ 0	3.0992+ 0							1.4447- 3				2.0298- 2
2.0000+ 4	3.1285+ 0	3.0984+ 0							1.3269- 3				2.0298- 2
3.0000+ 4	3.1279+ 0	3.0976+ 0							1.2182- 3				2.0298- 2
4.0000+ 4	3.1273+ 0	3.0968+ 0							1.1195- 3				2.0298- 2
5.0000+ 4	3.1267+ 0	3.0960+ 0							1.0208- 3				2.0298- 2
6.0000+ 4	3.1261+ 0	3.0952+ 0							8.7276- 3				2.0298- 2
8.0000+ 4	3.1255+ 0	3.0944+ 0							1.5728- 3				2.0298- 2
1.0000+ 5	3.1249+ 0	3.0936+ 0							1.4447- 3				2.0298- 2
1.5000+ 5	3.1243+ 0	3.0928+ 0							1.3269- 3				2.0298- 2
2.0000+ 5	3.1237+ 0	3.0920+ 0							1.2182- 3				2.0298- 2
3.0000+ 5	3.1231+ 0	3.0912+ 0							1.1195- 3				2.0298- 2
4.0000+ 5	3.1225+ 0	3.0904+ 0							1.0208- 3				2.0298- 2
5.0000+ 5	3.1219+ 0	3.0896+ 0							8.7276- 3				2.0298- 2
6.0000+ 5	3.1213+ 0	3.0888+ 0							1.5728- 3				2.0298- 2
8.0000+ 5	3.1207+ 0	3.0880+ 0							1.4447- 3				2.0298- 2
1.0000+ 6	3.1201+ 0	3.0872+ 0							1.3269- 3				2.0298- 2
1.5000+ 6	3.1195+ 0	3.0864+ 0							1.2182- 3				2.0298- 2
2.0000+ 6	3.1189+ 0	3.0856+ 0							1.1195- 3				2.0298- 2
3.0000+ 6	3.1183+ 0	3.0848+ 0							1.0208- 3				2.0298- 2
4.0000+ 6	3.1177+ 0	3.0840+ 0							8.7276- 3				2.0298- 2
5.0000+ 6	3.1171+ 0	3.0832+ 0							1.5728- 3				2.0298- 2
6.0000+ 6	3.1165+ 0	3.0824+ 0							1.4447- 3				2.0298- 2
8.0000+ 6	3.1159+ 0	3.0816+ 0							1.3269- 3				2.0298- 2
1.0000+ 7	3.1153+ 0	3.0808+ 0							1.2182- 3				2.0298- 2
1.5000+ 7	3.1147+ 0	3.0800+ 0							1.1195- 3				2.0298- 2
2.0000+ 7	3.1141+ 0	3.0792+ 0							1.0208- 3				2.0298- 2
3.0000+ 7	3.1135+ 0	3.0784+ 0							8.7276- 3				2.0298- 2
4.0000+ 7	3.1129+ 0	3.0776+ 0							1.5728- 3				2.0298- 2
5.0000+ 7	3.1123+ 0	3.0768+ 0							1.4447- 3				2.0298- 2
6.0000+ 7	3.1117+ 0	3.0760+ 0							1.3269- 3				2.0298- 2
8.0000+ 7	3.1111+ 0	3.0752+ 0							1.2182- 3				2.0298- 2
1.0000+ 8	3.1105+ 0	3.0744+ 0							1.1195- 3				2.0298- 2
1.5000+ 8	3.1099+ 0	3.0736+ 0							1.0208- 3				2.0298- 2
2.0000+ 8	3.1093+ 0	3.0728+ 0							8.7276- 3				2.0298- 2
3.0000+ 8	3.1087+ 0	3.0720+ 0							1.5728- 3				2.0298- 2
4.0000+ 8	3.1081+ 0	3.0712+ 0							1.4447- 3				2.0298- 2
5.0000+ 8	3.1075+ 0	3.0704+ 0							1.3269- 3				2.0298- 2
6.0000+ 8	3.1069+ 0	3.0696+ 0							1.2182- 3				2.0298- 2
8.0000+ 8	3.1063+ 0	3.0688+ 0							1.1195- 3				2.0298- 2
1.0000+ 9	3.1057+ 0	3.0680+ 0							1.0208- 3				2.0298- 2
1.5000+ 9	3.1051+ 0	3.0672+ 0							8.7276- 3				2.0298- 2
2.0000+ 9	3.1045+ 0	3.0664+ 0							1.5728- 3				2.0298- 2
3.0000+ 9	3.1039+ 0	3.0656+ 0							1.4447- 3				2.0298- 2
4.0000+ 9	3.1033+ 0	3.0648+ 0							1.3269- 3				2.0298- 2
5.0000+ 9	3.1027+ 0	3.0640+ 0							1.2182- 3				2.0298- 2
6.0000+ 9	3.1021+ 0	3.0632+ 0							1.1195- 3				2.0298- 2
8.0000+ 9	3.1015+ 0	3.0624+ 0							1.0208- 3				2.0298- 2
1.0000+ 10	3.1009+ 0	3.0616+ 0							8.7276- 3				2.0298- 2
1.5000+ 10	3.1003+ 0	3.0608+ 0											

CROSS SECTION

SI-0

MATERIAL	Z140	ENERGY	TOTAL	ELASTIC	INEL	(N.2N)	(N.3N)	FSSION	(N.NR)	(N.NP)	(N.P)	(N.D)	(N.R)	MU-BR
1.0000-	5	1.0000-2	2.6917+0	2.2021+0										2.9374-2
1.0000-	0	1.5000-	2.4979+0	2.2000+0										3.981-
1.0000-	0	2.0000-	2.3658+0	2.2000+0										3.983-
1.0000-	0	2.5000-	2.3191+0	2.2000+0										3.985-
1.0000-	0	3.0000-	2.3446+0	2.2000+0										3.987-
1.0000-	0	3.5000-	2.3329+0	2.2000+0										3.989-
1.0000-	0	4.0000-	2.3211+0	2.2000+0										3.991-
1.0000-	0	4.5000-	2.3094+0	2.2000+0										3.993-
1.0000-	0	5.0000-	2.2977+0	2.2000+0										3.995-
1.0000-	0	5.5000-	2.2860+0	2.2000+0										3.997-
1.0000-	0	6.0000-	2.2743+0	2.2000+0										3.999-
1.0000-	0	6.5000-	2.2626+0	2.2000+0										4.001-
1.0000-	0	7.0000-	2.2509+0	2.2000+0										4.003-
1.0000-	0	7.5000-	2.2392+0	2.2000+0										4.005-
1.0000-	0	8.0000-	2.2275+0	2.2000+0										4.007-
1.0000-	0	8.5000-	2.2158+0	2.2000+0										4.009-
1.0000-	0	9.0000-	2.2041+0	2.2000+0										4.011-
1.0000-	0	9.5000-	2.1924+0	2.2000+0										4.013-
1.0000-	0	10.0000-	2.1807+0	2.2000+0										4.015-
1.0000-	0	10.5000-	2.1690+0	2.2000+0										4.017-
1.0000-	0	11.0000-	2.1573+0	2.2000+0										4.019-
1.0000-	0	11.5000-	2.1456+0	2.2000+0										4.021-
1.0000-	0	12.0000-	2.1339+0	2.2000+0										4.023-
1.0000-	0	12.5000-	2.1222+0	2.2000+0										4.025-
1.0000-	0	13.0000-	2.1105+0	2.2000+0										4.027-
1.0000-	0	13.5000-	2.0988+0	2.2000+0										4.029-
1.0000-	0	14.0000-	2.0871+0	2.2000+0										4.031-
1.0000-	0	14.5000-	2.0754+0	2.2000+0										4.033-
1.0000-	0	15.0000-	2.0637+0	2.2000+0										4.035-
1.0000-	0	15.5000-	2.0520+0	2.2000+0										4.037-
1.0000-	0	16.0000-	2.0403+0	2.2000+0										4.039-
1.0000-	0	16.5000-	2.0286+0	2.2000+0										4.041-
1.0000-	0	17.0000-	2.0169+0	2.2000+0										4.043-
1.0000-	0	17.5000-	2.0052+0	2.2000+0										4.045-
1.0000-	0	18.0000-	1.9935+0	2.2000+0										4.047-
1.0000-	0	18.5000-	1.9818+0	2.2000+0										4.049-
1.0000-	0	19.0000-	1.9701+0	2.2000+0										4.051-
1.0000-	0	19.5000-	1.9584+0	2.2000+0										4.053-
1.0000-	0	20.0000-	1.9467+0	2.2000+0										4.055-
1.0000-	0	20.5000-	1.9350+0	2.2000+0										4.057-
1.0000-	0	21.0000-	1.9233+0	2.2000+0										4.059-
1.0000-	0	21.5000-	1.9116+0	2.2000+0										4.061-
1.0000-	0	22.0000-	1.9000+0	2.2000+0										4.063-
1.0000-	0	22.5000-	1.8883+0	2.2000+0										4.065-
1.0000-	0	23.0000-	1.8766+0	2.2000+0										4.067-
1.0000-	0	23.5000-	1.8650+0	2.2000+0										4.069-
1.0000-	0	24.0000-	1.8533+0	2.2000+0										4.071-
1.0000-	0	24.5000-	1.8416+0	2.2000+0										4.073-
1.0000-	0	25.0000-	1.8300+0	2.2000+0										4.075-
1.0000-	0	25.5000-	1.8183+0	2.2000+0										4.077-
1.0000-	0	26.0000-	1.8066+0	2.2000+0										4.079-
1.0000-	0	26.5000-	1.7950+0	2.2000+0										4.081-
1.0000-	0	27.0000-	1.7833+0	2.2000+0										4.083-
1.0000-	0	27.5000-	1.7716+0	2.2000+0										4.085-
1.0000-	0	28.0000-	1.7600+0	2.2000+0										4.087-
1.0000-	0	28.5000-	1.7483+0	2.2000+0										4.089-
1.0000-	0	29.0000-	1.7366+0	2.2000+0										4.091-
1.0000-	0	29.5000-	1.7250+0	2.2000+0										4.093-
1.0000-	0	30.0000-	1.7133+0	2.2000+0										4.095-
1.0000-	0	30.5000-	1.7016+0	2.2000+0										4.097-
1.0000-	0	31.0000-	1.6900+0	2.2000+0										4.099-
1.0000-	0	31.5000-	1.6783+0	2.2000+0										4.101-
1.0000-	0	32.0000-	1.6666+0	2.2000+0										4.103-
1.0000-	0	32.5000-	1.6550+0	2.2000+0										4.105-
1.0000-	0	33.0000-	1.6433+0	2.2000+0										4.107-
1.0000-	0	33.5000-	1.6316+0	2.2000+0										4.109-
1.0000-	0	34.0000-	1.6200+0	2.2000+0										4.111-
1.0000-	0	34.5000-	1.6083+0	2.2000+0										4.113-
1.0000-	0	35.0000-	1.5966+0	2.2000+0										4.115-
1.0000-	0	35.5000-	1.5850+0	2.2000+0										4.117-
1.0000-	0	36.0000-	1.5733+0	2.2000+0										4.119-
1.0000-	0	36.5000-	1.5616+0	2.2000+0										4.121-
1.0000-	0	37.0000-	1.5500+0	2.2000+0										4.123-
1.0000-	0	37.5000-	1.5383+0	2.2000+0										4.125-
1.0000-	0	38.0000-	1.5266+0	2.2000+0										4.127-
1.0000-	0	38.5000-	1.5150+0	2.2000+0										4.129-
1.0000-	0	39.0000-	1.5033+0	2.2000+0										4.131-
1.0000-	0	39.5000-	1.4916+0	2.2000+0										4.133-
1.0000-	0	40.0000-	1.4800+0	2.2000+0										4.135-
1.0000-	0	40.5000-	1.4683+0	2.2000+0										4.137-
1.0000-	0	41.0000-	1.4566+0	2.2000+0										4.139-
1.0000-	0	41.5000-	1.4450+0	2.2000+0										4.141-
1.0000-	0	42.0000-	1.4333+0	2.2000+0										4.143-
1.0000-	0	42.5000-	1.4216+0	2.2000+0										4.145-
1.0000-	0	43.0000-	1.4100+0	2.2000+0										4.147-
1.0000-	0	43.5000-	1.3983+0	2.2000+0										4.149-
1.0000-	0	44.0000-	1.3866+0	2.2000+0										4.151-
1.0000-	0	44.5000-	1.3750+0	2.2000+0										4.153-
1.0000-	0	45.0000-	1.3633+0	2.2000+0										4.155-
1.0000-	0	45.5000-	1.3516+0	2.2000+0										4.157-
1.0000-	0	46.0000-	1.3400+0	2.2000+0										4.159-
1.0000-	0	46.5000-	1.3283+0	2.2000+0										4.161-
1.0000-	0	47.0000-	1.3166+0	2.2000+0										4.163-
1.0000-	0	47.5000-	1.3050+0	2.2000+0										4.165-
1.0000-	0	48.0000-	1.2933+0	2.2000+0										4.167-
1.0000-	0	48.5000-	1.2816+0	2.2000+0										4.169-
1.0000-	0	49.0000-	1.2700+0	2.2000+0										4.171-
1.0000-	0	49.5000-	1.2583+0	2.2000+0										4.173-
1.0000-	0	50.0000-												

CROSS SECTION

MATERIAL = Z200		CR-0										
ENERGY	TOTAL	ELABTIC	INELR	(N,2N)	(N,3N)	FIBSION	(N,NA)	(N,NP)	(N,PI)	(N,DI)	(N,RA)	RU-BRA
1.0000+ 5 ~ 1.0000- 2	4.3080+ 0	2.9831+ 0						1.3277+ 0			4.7856- 4	1.6802- 2
1.0000- 1	3.5930+ 0	2.9831+ 0						5.1876- 1			1.668- 3	1.6918- 2
2.0000- 1	3.5930+ 0	2.9831+ 0						5.2027- 1			1.6780- 3	1.6922- 2
3.0000- 1	3.5930+ 0	2.9831+ 0						4.3737- 1			1.6889- 3	1.6926- 2
4.0000- 1	3.5930+ 0	2.9831+ 0						3.6794- 1			1.6931- 3	1.6931- 2
5.0000- 1	3.5930+ 0	2.9831+ 0						2.2474- 1			1.6931- 3	1.6931- 2
6.0000- 2	3.5930+ 0	2.9831+ 0						2.6049- 1			1.6940- 3	1.6940- 2
7.0000- 2	3.5930+ 0	2.9831+ 0						2.2958- 1			1.6943- 3	1.6943- 2
8.0000- 2	3.5930+ 0	2.9831+ 0						1.9517- 1			1.6947- 3	1.6947- 2
1.0000- 1	3.1333+ 0	2.9831+ 0						1.9478- 1			1.6956- 3	1.6956- 2
2.0000- 1	3.1333+ 0	2.9831+ 0						1.1868- 1			1.6961- 3	1.6961- 2
3.0000- 1	3.1333+ 0	2.9831+ 0						1.0255- 1			1.6964- 3	1.6964- 2
4.0000- 1	3.1333+ 0	2.9831+ 0						9.2706- 2			1.6966- 3	1.6966- 2
5.0000- 1	3.1333+ 0	2.9831+ 0						8.2484- 2			1.6970- 3	1.6970- 2
6.0000- 1	3.1333+ 0	2.9831+ 0						7.2453- 2			1.6973- 3	1.6973- 2
7.0000- 1	3.1333+ 0	2.9831+ 0						6.1815- 2			1.6977- 3	1.6977- 2
8.0000- 1	3.1333+ 0	2.9831+ 0						5.2068- 2			1.6981- 3	1.6981- 2
1.0000+ 0	3.0265+ 0	2.9831+ 0						4.3725- 2			1.6986- 3	1.6986- 2
2.0000+ 0	3.0265+ 0	2.9831+ 0						3.6849- 2			1.6993- 3	1.6993- 2
3.0000+ 0	3.0265+ 0	2.9831+ 0						2.5634- 2			1.6996- 3	1.6996- 2
4.0000+ 0	3.0265+ 0	2.9831+ 0						2.6035- 2			1.6999- 3	1.6999- 2
5.0000+ 0	3.0265+ 0	2.9831+ 0						2.2912- 2			1.7002- 3	1.7002- 2
6.0000+ 0	3.0265+ 0	2.9831+ 0						1.9549- 2			1.7005- 3	1.7005- 2
7.0000+ 0	3.0265+ 0	2.9831+ 0						1.8077- 2			1.7008- 3	1.7008- 2
8.0000+ 0	3.0265+ 0	2.9831+ 0						1.6976- 2			1.7011- 3	1.7011- 2
1.0000+ 1	2.9827+ 0	2.9831+ 0						1.1658- 2			1.7015- 3	1.7015- 2
2.0000+ 1	2.9827+ 0	2.9831+ 0						1.0268- 2			1.7020- 3	1.7020- 2
3.0000+ 1	2.9827+ 0	2.9831+ 0						9.2718- 2			1.7023- 3	1.7023- 2
4.0000+ 1	2.9827+ 0	2.9831+ 0						7.2755- 2			1.7025- 3	1.7025- 2
5.0000+ 1	2.9827+ 0	2.9831+ 0						6.2555- 2			1.7032- 3	1.7032- 2
6.0000+ 1	2.9827+ 0	2.9831+ 0						5.2180- 2			1.7036- 3	1.7036- 2
7.0000+ 1	2.9827+ 0	2.9831+ 0						4.2411- 2			1.7040- 3	1.7040- 2
8.0000+ 1	2.9827+ 0	2.9831+ 0						3.3027- 2			1.7043- 3	1.7043- 2
1.0000+ 2	2.9719+ 0	2.9831+ 0						3.4156- 2			1.7055- 3	1.7055- 2
2.0000+ 2	2.9719+ 0	2.9831+ 0						3.1111- 2			1.7055- 3	1.7055- 2
3.0000+ 2	2.9719+ 0	2.9831+ 0						2.7928- 2			1.7055- 3	1.7055- 2
4.0000+ 2	2.9719+ 0	2.9831+ 0						2.4773- 2			1.7051- 3	1.7051- 2
5.0000+ 2	2.9719+ 0	2.9831+ 0						2.1382- 2			1.7055- 3	1.7055- 2
6.0000+ 2	2.9719+ 0	2.9831+ 0						1.8244- 2			1.7070- 3	1.7070- 2
7.0000+ 2	2.9719+ 0	2.9831+ 0						1.5782- 2			1.7236- 3	1.7236- 2
8.0000+ 2	2.9719+ 0	2.9831+ 0						1.3301- 2			1.7459- 3	1.7459- 2
1.0000+ 3	2.9574+ 0	2.9831+ 0						1.0707- 2			1.7888- 3	1.7888- 2
2.0000+ 3	2.9574+ 0	2.9831+ 0						1.0965- 2			1.8547- 3	1.8547- 2
3.0000+ 3	2.9574+ 0	2.9831+ 0						1.0955- 2			1.9136- 3	1.9136- 2
4.0000+ 3	2.9574+ 0	2.9831+ 0						1.0987- 2			2.0704- 3	2.0704- 2
5.0000+ 3	2.9574+ 0	2.9831+ 0						1.0987- 2			2.2765- 3	2.2765- 2
6.0000+ 3	2.9574+ 0	2.9831+ 0						1.0987- 2			2.5233- 3	2.5233- 2
7.0000+ 3	2.9574+ 0	2.9831+ 0						1.0987- 2			2.7623- 3	2.7623- 2
8.0000+ 3	2.9574+ 0	2.9831+ 0						1.0987- 2			3.0000- 3	3.0000- 2
1.0000+ 4	2.9221+ 0	2.9831+ 0						1.0987- 2			3.2468- 3	3.2468- 2
2.0000+ 4	2.9221+ 0	2.9831+ 0						1.0987- 2			3.4936- 3	3.4936- 2
3.0000+ 4	2.9221+ 0	2.9831+ 0						1.0987- 2			3.7404- 3	3.7404- 2
4.0000+ 4	2.9221+ 0	2.9831+ 0						1.0987- 2			4.0000- 3	4.0000- 2
5.0000+ 4	2.9221+ 0	2.9831+ 0						1.0987- 2			4.2468- 3	4.2468- 2
6.0000+ 4	2.9221+ 0	2.9831+ 0						1.0987- 2			4.4936- 3	4.4936- 2
7.0000+ 4	2.9221+ 0	2.9831+ 0						1.0987- 2			4.7404- 3	4.7404- 2
8.0000+ 4	2.9221+ 0	2.9831+ 0						1.0987- 2			5.0000- 3	5.0000- 2
1.0000+ 5	2.8874+ 0	2.9831+ 0						1.0987- 2			5.2468- 3	5.2468- 2
2.0000+ 5	2.8874+ 0	2.9831+ 0						1.0987- 2			5.4936- 3	5.4936- 2
3.0000+ 5	2.8874+ 0	2.9831+ 0						1.0987- 2			5.7404- 3	5.7404- 2
4.0000+ 5	2.8874+ 0	2.9831+ 0						1.0987- 2			6.0000- 3	6.0000- 2
5.0000+ 5	2.8874+ 0	2.9831+ 0						1.0987- 2			6.2468- 3	6.2468- 2
6.0000+ 5	2.8874+ 0	2.9831+ 0						1.0987- 2			6.4936- 3	6.4936- 2
7.0000+ 5	2.8874+ 0	2.9831+ 0						1.0987- 2			6.7404- 3	6.7404- 2
8.0000+ 5	2.8874+ 0	2.9831+ 0						1.0987- 2			7.0000- 3	7.0000- 2
1.0000+ 6	2.8521+ 0	2.9831+ 0						1.0987- 2			7.2468- 3	7.2468- 2
2.0000+ 6	2.8521+ 0	2.9831+ 0						1.0987- 2			7.4936- 3	7.4936- 2
3.0000+ 6	2.8521+ 0	2.9831+ 0						1.0987- 2			7.7404- 3	7.7404- 2
4.0000+ 6	2.8521+ 0	2.9831+ 0						1.0987- 2			8.0000- 3	8.0000- 2
5.0000+ 6	2.8521+ 0	2.9831+ 0						1.0987- 2			8.2468- 3	8.2468- 2
6.0000+ 6	2.8521+ 0	2.9831+ 0						1.0987- 2			8.4936- 3	8.4936- 2
7.0000+ 6	2.8521+ 0	2.9831+ 0						1.0987- 2			8.7404- 3	8.7404- 2
8.0000+ 6	2.8521+ 0	2.9831+ 0						1.0987- 2			9.0000- 3	9.0000- 2
1.0000+ 7	2.8168+ 0	2.9831+ 0						1.0987- 2			9.2468- 3	9.2468- 2
2.0000+ 7	2.8168+ 0	2.9831+ 0						1.0987- 2			9.4936- 3	9.4936- 2
3.0000+ 7	2.8168+ 0	2.9831+ 0						1.0987- 2			9.7404- 3	9.7404- 2
4.0000+ 7	2.8168+ 0	2.9831+ 0						1.0987- 2			10.0000- 3	10.0000- 2
5.0000+ 7	2.8168+ 0	2.9831+ 0						1.0987- 2			10.2468- 3	10.2468- 2
6.0000+ 7	2.8168+ 0	2.9831+ 0						1.0987- 2			10.4936- 3	10.4936- 2
7.0000+ 7	2.8168+ 0	2.9831+ 0						1.0987- 2			10.7404- 3	10.7404- 2
8.0000+ 7	2.8168+ 0	2.9831+ 0						1.0987- 2			11.0000- 3	11.0000- 2
1.0000+ 8	2.7815+ 0	2.9831+ 0						1.0987- 2			11.2468- 3	11.2468- 2
2.0000+ 8	2.7815+ 0	2.9831+ 0						1.0987- 2			11.4936- 3	11.4936- 2
3.0000+ 8	2.7815+ 0	2.9831+ 0						1.0987- 2			11.7404- 3	11.7404- 2
4.0000+ 8	2.7815+ 0	2.9831+ 0						1.0987- 2			12.0000- 3	12.0000- 2
5.0000+ 8	2.7815+ 0	2.9831+ 0						1.0987- 2			12.2468- 3	12.2468- 2
6.0000+ 8	2.7815+ 0	2.9831+ 0						1.0987- 2			12.4936- 3	12.4936- 2
7.0000+ 8	2.7815+ 0	2.9831+ 0						1.0987- 2			12.7404- 3	12.7404- 2
8.0000+ 8	2.7815+ 0	2.9831+ 0						1.0987- 2			13.0000- 3	13.0000- 2
1.0000+ 9	2.7462+ 0	2.9831+ 0						1.0987- 2			13.2468- 3	13.2468- 2
2.0000+ 9	2.7462+ 0	2.9831+ 0						1.0987- 2			13.4936- 3	13.4936- 2
3.0000+ 9	2.7462+ 0	2										

CROSS SECTION

MATERIAL	ENERGY	TOTAL	ELASTIC	INELR	(N,2N)	(N,2N)	FISSTON	(N,NR)	(N,NP)	CAPTURE	(N,P)	(N,D)	(N,R)	MU-BRR	CR-40
1.0000	5	1.0000-2	3.0100+0							1.2677+0			4.8377-4	1.6902-2	
1.0000	2	3.6908+0	3.0100+0							5.8905-1			1.2347-3	1.6916-2	
1.0000	2	3.0100+0	3.0100+0							4.9522-0			1.7289-3	1.6927-2	
1.0000	2	3.0100+0	3.0100+0							4.1637-1			2.6000-3	1.6931-1	
1.0000	2	3.0100+0	3.0100+0							3.5022-0			2.6000-3	1.6931-1	
1.0000	2	3.0100+0	3.0100+0							3.9511-1			2.6000-3	1.6931-1	
1.0000	2	3.0100+0	3.0100+0							2.4795-1			2.6000-3	1.6931-1	
1.0000	2	3.0100+0	3.0100+0							2.1855-1			2.6000-3	1.6943-2	
1.0000	1	3.2013+0	3.0100+0							1.8580-1			2.6000-3	1.6947-2	
1.0000	1	3.1722+0	3.0100+0							1.5974-1			2.6000-3	1.6952-2	
1.0000	1	3.1481+0	3.0100+0							1.1098-1			2.6000-3	1.6961-1	
1.0000	1	3.1124+0	3.0100+0							9.7622-2			2.6000-3	1.6964-1	
1.0000	1	3.1016+0	3.0100+0							8.8254-1			2.6000-3	1.6966-1	
1.0000	1	3.0830+0	3.0100+0							7.8439-1			2.6000-3	1.6970-2	
1.0000	0	3.0762+0	3.0100+0							6.8588-1			2.6000-3	1.6975-2	
1.5000	0	3.0734+0	3.0100+0							5.8847-1			2.6000-3	1.6977-2	
2.0000	0	3.0684+0	3.0100+0							4.9568-1			2.6000-3	1.6981-1	
3.0000	0	3.0644+0	3.0100+0							4.1622-1			2.6000-3	1.6986-1	
4.0000	0	3.0595+0	3.0100+0							3.3675-1			2.6000-3	1.6993-1	
5.0000	0	3.0547+0	3.0100+0							2.5744-1			2.6000-3	1.6996-1	
6.0000	0	3.0479+0	3.0100+0							2.4785-1			2.6000-3	1.6999-1	
8.0000	0	3.0378+0	3.0100+0							2.2161-1			2.6000-3	1.7002-2	
1.0000	1	3.0326+0	3.0100+0							1.5682-1			2.6000-3	1.7006-1	
1.5000	1	3.0317+0	3.0100+0							1.5682-1			2.6000-3	1.7011-1	
2.0000	1	3.0288+0	3.0098+0							1.1098-1			2.6000-3	1.7016-1	
3.0000	1	3.0273+0	3.0098+0							9.7749-2			2.6000-3	1.7020-1	
4.0000	1	3.0257+0	3.0098+0							8.8254-1			2.6000-3	1.7023-1	
5.0000	1	3.0234+0	3.0098+0							7.8439-1			2.6000-3	1.7028-1	
6.0000	1	3.0203+0	3.0098+0							6.8588-1			2.6000-3	1.7032-1	
1.5000	2	3.0196+0	3.0097+0							5.8847-1			2.6000-3	1.7036-2	
2.0000	2	3.0183+0	3.0096+0							4.9568-1			2.6000-3	1.7040-2	
3.0000	2	3.0179+0	3.0096+0							4.1622-1			2.6000-3	1.7044-2	
4.0000	2	3.0174+0	3.0096+0							3.3675-1			2.6000-3	1.7048-2	
5.0000	2	3.0163+0	3.0096+0							2.5744-1			2.6000-3	1.7052-2	
6.0000	2	3.0155+0	3.0096+0							2.4785-1			2.6000-3	1.7055-2	
8.0000	2	3.0145+0	3.0097+0							2.2161-1			2.6000-3	1.7058-2	
1.0000	3	3.0127+0	3.0095+0							2.0547-1			2.6000-3	1.7061-2	
1.5000	3	3.0122+0	3.0095+0							1.7495-1			2.6000-3	1.7065-2	
2.0000	3	3.0116+0	3.0095+0							1.5149-1			2.6000-3	1.7070-2	
3.0000	3	3.0110+0	3.0095+0							1.3748-1			2.6000-3	1.7074-2	
4.0000	3	3.0104+0	3.0095+0							1.2493-1			2.6000-3	1.7078-2	
5.0000	3	3.0098+0	3.0095+0							1.1301-1			2.6000-3	1.7082-2	
6.0000	3	3.0092+0	3.0095+0							9.9752-2			2.6000-3	1.7086-2	
8.0000	3	3.0087+0	3.0095+0							8.2721-2			2.6000-3	1.7090-2	
1.0000	4	3.0082+0	3.0095+0							7.5002-2			2.6000-3	1.7094-2	
1.5000	4	3.0077+0	3.0095+0							6.7262-2			2.6000-3	1.7098-2	
2.0000	4	3.0072+0	3.0095+0							5.9513-2			2.6000-3	1.7102-2	
3.0000	4	3.0067+0	3.0095+0							5.1764-2			2.6000-3	1.7106-2	
4.0000	4	3.0062+0	3.0095+0							4.4015-2			2.6000-3	1.7110-2	
5.0000	4	3.0057+0	3.0095+0							3.6266-2			2.6000-3	1.7114-2	
6.0000	4	3.0052+0	3.0095+0							2.8517-2			2.6000-3	1.7118-2	
8.0000	4	3.0047+0	3.0095+0							2.0768-2			2.6000-3	1.7122-2	
1.0000	5	3.0042+0	3.0095+0							1.3019-2			2.6000-3	1.7126-2	
1.5000	5	3.0037+0	3.0095+0							1.0270-2			2.6000-3	1.7130-2	
2.0000	5	3.0032+0	3.0095+0							9.5021-3			2.6000-3	1.7134-2	
3.0000	5	3.0027+0	3.0095+0							8.7272-3			2.6000-3	1.7138-2	
4.0000	5	3.0022+0	3.0095+0							7.9523-3			2.6000-3	1.7142-2	
5.0000	5	3.0017+0	3.0095+0							7.1774-3			2.6000-3	1.7146-2	
6.0000	5	3.0012+0	3.0095+0							6.4025-3			2.6000-3	1.7150-2	
8.0000	5	3.0007+0	3.0095+0							5.6276-3			2.6000-3	1.7154-2	
1.0000	6	3.0002+0	3.0095+0							4.8527-3			2.6000-3	1.7158-2	
1.5000	6	3.0000+0	3.0095+0							4.0778-3			2.6000-3	1.7162-2	
2.0000	6	3.0000+0	3.0095+0							3.3029-3			2.6000-3	1.7166-2	
3.0000	6	3.0000+0	3.0095+0							2.5280-3			2.6000-3	1.7170-2	
4.0000	6	3.0000+0	3.0095+0							1.7531-3			2.6000-3	1.7174-2	
5.0000	6	3.0000+0	3.0095+0							9.7582-4			2.6000-3	1.7178-2	
6.0000	6	3.0000+0	3.0095+0							8.9833-4			2.6000-3	1.7182-2	
8.0000	6	3.0000+0	3.0095+0							8.2084-4			2.6000-3	1.7186-2	
1.0000	7	3.0000+0	3.0095+0							7.4335-4			2.6000-3	1.7190-2	
1.5000	7	3.0000+0	3.0095+0							6.6586-4			2.6000-3	1.7194-2	
2.0000	7	3.0000+0	3.0095+0							5.8837-4			2.6000-3	1.7198-2	
3.0000	7	3.0000+0	3.0095+0							5.1088-4			2.6000-3	1.7202-2	
4.0000	7	3.0000+0	3.0095+0							4.3339-4			2.6000-3	1.7206-2	
5.0000	7	3.0000+0	3.0095+0							3.5590-4			2.6000-3	1.7210-2	
6.0000	7	3.0000+0	3.0095+0							2.7841-4			2.6000-3	1.7214-2	
8.0000	7	3.0000+0	3.0095+0							2.0092-4			2.6000-3	1.7218-2	
1.0000	8	3.0000+0	3.0095+0							1.2343-4			2.6000-3	1.7222-2	
1.5000	8	3.0000+0	3.0095+0							4.8466+0			2.6000-3	1.7226-2	
2.0000	8	3.0000+0	3.0095+0							4.1330+0			2.6000-3	1.7230-2	
3.0000	8	3.0000+0	3.0095+0							3.4194+0			2.6000-3	1.7234-2	
4.0000	8	3.0000+0	3.0095+0							2.7058+0			2.6000-3	1.7238-2	
5.0000	8	3.0000+0	3.0095+0							2.0000+0			2.6000-3	1.7242-2	
6.0000	8	3.0000+0	3.0095+0							1.2942+0			2.6000-3	1.7246-2	
8.0000	8	3.0000+0	3.0095+0							6.2448+0			2.6000-3	1.7250-2	
1.0000	9	3.0000+0	3.0095+0							5.4699+0			2.6000-3	1.7254-2	
1.5000	9	3.0000+0	3.0095+0							4.6950+0			2.6000-3		

CROSS SECTION

CR-44

MATERIAL	ENERGY	TOTAL	ELASTIC	INELR	(N,2N)	(N,3N)	FISSION	(N,NR)	(N,MP)	(N,D)	(N,R)	RU-BRE
1.0000	5 ~ 1.0000-2	4.0465+0	1.3234+0						2.7231+0			1.6341-2
1.0000	1.0000	2.5804+0	1.3234+0						1.2642+0			1.9800
1.0000	1.0000	2.3938+0	1.3234+0						1.0693+0			1.9800
1.0000	1.0000	2.2177+0	1.3234+0						0.8757+0			1.9800
1.0000	1.0000	2.0755+0	1.3234+0						0.6830+0			1.9800
1.0000	1.0000	1.9688+0	1.3234+0						0.5993+0			1.9800
1.0000	1.0000	1.8678+0	1.3234+0						0.5165+0			1.9800
1.0000	1.0000	1.7845+0	1.3234+0						0.4340+0			1.9800
1.0000	1.0000	1.7287+0	1.3234+0						0.3987+0			1.9800
1.0000	1.0000	1.6663+0	1.3234+0						0.3663+0			1.9800
1.0000	1.0000	1.6082+0	1.3234+0						0.3321+0			1.9800
1.0000	1.0000	1.5574+0	1.3234+0						0.2992+0			1.9800
1.0000	1.0000	1.5147+0	1.3234+0						0.2682+0			1.9800
1.0000	1.0000	1.4748+0	1.3234+0						0.2389+0			1.9800
1.0000	1.0000	1.4339+0	1.3234+0						0.2116+0			1.9800
1.0000	1.0000	1.3954+0	1.3234+0						0.1862+0			1.9800
1.0000	1.0000	1.3595+0	1.3234+0						0.1626+0			1.9800
1.0000	1.0000	1.3263+0	1.3234+0						0.1406+0			1.9800
1.0000	1.0000	1.2957+0	1.3234+0						0.1208+0			1.9800
1.0000	1.0000	1.2676+0	1.3234+0						0.1030+0			1.9800
1.0000	1.0000	1.2418+0	1.3234+0						0.0872+0			1.9800
1.0000	1.0000	1.2181+0	1.3234+0						0.0733+0			1.9800
1.0000	1.0000	1.1963+0	1.3234+0						0.0611+0			1.9800
1.0000	1.0000	1.1764+0	1.3234+0						0.0505+0			1.9800
1.0000	1.0000	1.1584+0	1.3234+0						0.0414+0			1.9800
1.0000	1.0000	1.1422+0	1.3234+0						0.0336+0			1.9800
1.0000	1.0000	1.1276+0	1.3234+0						0.0269+0			1.9800
1.0000	1.0000	1.1145+0	1.3234+0						0.0212+0			1.9800
1.0000	1.0000	1.1027+0	1.3234+0						0.0164+0			1.9800
1.0000	1.0000	1.0921+0	1.3234+0						0.0124+0			1.9800
1.0000	1.0000	1.0826+0	1.3234+0						0.0091+0			1.9800
1.0000	1.0000	1.0742+0	1.3234+0						0.0064+0			1.9800
1.0000	1.0000	1.0668+0	1.3234+0						0.0043+0			1.9800
1.0000	1.0000	1.0603+0	1.3234+0						0.0028+0			1.9800
1.0000	1.0000	1.0547+0	1.3234+0						0.0018+0			1.9800
1.0000	1.0000	1.0499+0	1.3234+0						0.0011+0			1.9800
1.0000	1.0000	1.0458+0	1.3234+0						0.0007+0			1.9800
1.0000	1.0000	1.0423+0	1.3234+0						0.0004+0			1.9800
1.0000	1.0000	1.0393+0	1.3234+0						0.0002+0			1.9800
1.0000	1.0000	1.0368+0	1.3234+0						0.0001+0			1.9800
1.0000	1.0000	1.0347+0	1.3234+0						0.0000+0			1.9800
1.0000	1.0000	1.0330+0	1.3234+0						0.0000+0			1.9800
1.0000	1.0000	1.0316+0	1.3234+0						0.0000+0			1.9800
1.0000	1.0000	1.0304+0	1.3234+0						0.0000+0			1.9800
1.0000	1.0000	1.0294+0	1.3234+0						0.0000+0			1.9800
1.0000	1.0000	1.0285+0	1.3234+0						0.0000+0			1.9800
1.0000	1.0000	1.0278+0	1.3234+0						0.0000+0			1.9800
1.0000	1.0000	1.0272+0	1.3234+0						0.0000+0			1.9800
1.0000	1.0000	1.0267+0	1.3234+0						0.0000+0			1.9800
1.0000	1.0000	1.0263+0	1.3234+0						0.0000+0			1.9800
1.0000	1.0000	1.0260+0	1.3234+0						0.0000+0			1.9800
1.0000	1.0000	1.0257+0	1.3234+0						0.0000+0			1.9800
1.0000	1.0000	1.0255+0	1.3234+0						0.0000+0			1.9800
1.0000	1.0000	1.0253+0	1.3234+0						0.0000+0			1.9800
1.0000	1.0000	1.0252+0	1.3234+0						0.0000+0			1.9800
1.0000	1.0000	1.0251+0	1.3234+0						0.0000+0			1.9800
1.0000	1.0000	1.0250+0	1.3234+0						0.0000+0			1.9800
1.0000	1.0000	1.0249+0	1.3234+0						0.0000+0			1.9800
1.0000	1.0000	1.0248+0	1.3234+0						0.0000+0			1.9800
1.0000	1.0000	1.0247+0	1.3234+0						0.0000+0			1.9800
1.0000	1.0000	1.0246+0	1.3234+0						0.0000+0			1.9800
1.0000	1.0000	1.0245+0	1.3234+0						0.0000+0			1.9800
1.0000	1.0000	1.0244+0	1.3234+0						0.0000+0			1.9800
1.0000	1.0000	1.0243+0	1.3234+0						0.0000+0			1.9800
1.0000	1.0000	1.0242+0	1.3234+0						0.0000+0			1.9800
1.0000	1.0000	1.0241+0	1.3234+0						0.0000+0			1.9800
1.0000	1.0000	1.0240+0	1.3234+0						0.0000+0			1.9800
1.0000	1.0000	1.0239+0	1.3234+0						0.0000+0			1.9800
1.0000	1.0000	1.0238+0	1.3234+0						0.0000+0			1.9800
1.0000	1.0000	1.0237+0	1.3234+0						0.0000+0			1.9800
1.0000	1.0000	1.0236+0	1.3234+0						0.0000+0			1.9800
1.0000	1.0000	1.0235+0	1.3234+0						0.0000+0			1.9800
1.0000	1.0000	1.0234+0	1.3234+0						0.0000+0			1.9800
1.0000	1.0000	1.0233+0	1.3234+0						0.0000+0			1.9800
1.0000	1.0000	1.0232+0	1.3234+0						0.0000+0			1.9800
1.0000	1.0000	1.0231+0	1.3234+0						0.0000+0			1.9800
1.0000	1.0000	1.0230+0	1.3234+0						0.0000+0			1.9800
1.0000	1.0000	1.0229+0	1.3234+0						0.0000+0			1.9800
1.0000	1.0000	1.0228+0	1.3234+0						0.0000+0			1.9800
1.0000	1.0000	1.0227+0	1.3234+0						0.0000+0			1.9800
1.0000	1.0000	1.0226+0	1.3234+0						0.0000+0			1.9800
1.0000	1.0000	1.0225+0	1.3234+0						0.0000+0			1.9800
1.0000	1.0000	1.0224+0	1.3234+0						0.0000+0			1.9800
1.0000	1.0000	1.0223+0	1.3234+0						0.0000+0			1.9800
1.0000	1.0000	1.0222+0	1.3234+0						0.0000+0			1.9800
1.0000	1.0000	1.0221+0	1.3234+0						0.0000+0			1.9800
1.0000	1.0000	1.0220+0	1.3234+0						0.0000+0			1.9800
1.0000	1.0000	1.0219+0	1.3234+0						0.0000+0			1.9800
1.0000	1.0000	1.0218+0	1.3234+0						0.0000+0			1.9800
1.0000	1.0000	1.0217+0	1.3234+0						0.0000+0			1.9800
1.0000	1.0000	1.0216+0	1.3234+0						0.0000+0			1.9800
1.0000	1.0000	1.0215+0	1.3234+0						0.0000+0			1.9800
1.0000	1.0000	1.0214+0	1.3234+0						0.0000+0			1.9800
1.0000	1.0000	1.0213+0	1.3234+0						0.0000+0			1.9800
1.0000	1.0000	1.0212+0	1.3234+0						0.0000+0			1.9800
1.0000	1.0000	1.0211+0	1.3234+0						0.0000+0			1.9800
1.0000	1.0000	1.0210+0	1.3234+0						0.0000+0			1.9800
1.0000	1.0000	1.0209+0	1.3234+0						0.0000+0			1.9800
1.0000	1.0000	1.0208+0	1.3234+0						0.0000+0			1.9800
1.0000	1.0000	1.0207+0	1.3234+0						0.0000+0			1.9800
1.0000	1.0000	1.0206+0	1.3234+0						0.0000+0			1.9800
1.0000</												

CROSS SECTION

CR-48

MATERIAL = 2205

ENERGY	TOTAL	ELASTIC	INELR	(N.2N)	(N.3N)	FISSION	(N.NR)	(N.NP)	CAPTURE	(N.P)	(N.D)	(N.R)	MU-SR
1.0000- 5 ~ 1.0000- 2	5.1990+ 0	2.9000+ 0							2.2819+ 0				1.4671- 2
1.0000- 1.5000	3.8857+ 0	2.9000+ 0							0.9856+ 0				1.4680- 2
1.5000- 2.0000	3.6207+ 0	2.9000+ 0							0.7207+ 0				1.4661- 2
2.0000- 2.5000	3.5631+ 0	2.9000+ 0							0.6631+ 0				1.4652- 2
2.5000- 3.0000	3.5055+ 0	2.9000+ 0							0.6055+ 0				1.4643- 2
3.0000- 3.5000	3.4479+ 0	2.9000+ 0							0.5479+ 0				1.4634- 2
3.5000- 4.0000	3.3903+ 0	2.9000+ 0							0.4903+ 0				1.4625- 2
4.0000- 4.5000	3.3327+ 0	2.9000+ 0							0.4327+ 0				1.4616- 2
4.5000- 5.0000	3.2751+ 0	2.9000+ 0							0.3751+ 0				1.4607- 2
5.0000- 5.5000	3.2175+ 0	2.9000+ 0							0.3175+ 0				1.4598- 2
5.5000- 6.0000	3.1600+ 0	2.9000+ 0							0.2600+ 0				1.4589- 2
6.0000- 6.5000	3.1024+ 0	2.9000+ 0							0.2024+ 0				1.4580- 2
6.5000- 7.0000	3.0448+ 0	2.9000+ 0							0.1448+ 0				1.4571- 2
7.0000- 7.5000	2.9873+ 0	2.9000+ 0							0.0873+ 0				1.4562- 2
7.5000- 8.0000	2.9297+ 0	2.9000+ 0							0.0297+ 0				1.4553- 2
8.0000- 8.5000	2.8721+ 0	2.9000+ 0							0.0000+ 0				1.4544- 2
8.5000- 9.0000	2.8145+ 0	2.9000+ 0							0.0000+ 0				1.4535- 2
9.0000- 9.5000	2.7569+ 0	2.9000+ 0							0.0000+ 0				1.4526- 2
9.5000- 10.0000	2.6993+ 0	2.9000+ 0							0.0000+ 0				1.4517- 2
10.0000- 10.5000	2.6417+ 0	2.9000+ 0							0.0000+ 0				1.4508- 2
10.5000- 11.0000	2.5841+ 0	2.9000+ 0							0.0000+ 0				1.4499- 2
11.0000- 11.5000	2.5265+ 0	2.9000+ 0							0.0000+ 0				1.4490- 2
11.5000- 12.0000	2.4689+ 0	2.9000+ 0							0.0000+ 0				1.4481- 2
12.0000- 12.5000	2.4113+ 0	2.9000+ 0							0.0000+ 0				1.4472- 2
12.5000- 13.0000	2.3537+ 0	2.9000+ 0							0.0000+ 0				1.4463- 2
13.0000- 13.5000	2.2961+ 0	2.9000+ 0							0.0000+ 0				1.4454- 2
13.5000- 14.0000	2.2385+ 0	2.9000+ 0							0.0000+ 0				1.4445- 2
14.0000- 14.5000	2.1809+ 0	2.9000+ 0							0.0000+ 0				1.4436- 2
14.5000- 15.0000	2.1233+ 0	2.9000+ 0							0.0000+ 0				1.4427- 2
15.0000- 15.5000	2.0657+ 0	2.9000+ 0							0.0000+ 0				1.4418- 2
15.5000- 16.0000	2.0081+ 0	2.9000+ 0							0.0000+ 0				1.4409- 2
16.0000- 16.5000	1.9505+ 0	2.9000+ 0							0.0000+ 0				1.4400- 2
16.5000- 17.0000	1.8929+ 0	2.9000+ 0							0.0000+ 0				1.4391- 2
17.0000- 17.5000	1.8353+ 0	2.9000+ 0							0.0000+ 0				1.4382- 2
17.5000- 18.0000	1.7777+ 0	2.9000+ 0							0.0000+ 0				1.4373- 2
18.0000- 18.5000	1.7201+ 0	2.9000+ 0							0.0000+ 0				1.4364- 2
18.5000- 19.0000	1.6625+ 0	2.9000+ 0							0.0000+ 0				1.4355- 2
19.0000- 19.5000	1.6049+ 0	2.9000+ 0							0.0000+ 0				1.4346- 2
19.5000- 20.0000	1.5473+ 0	2.9000+ 0							0.0000+ 0				1.4337- 2
20.0000- 20.5000	1.4897+ 0	2.9000+ 0							0.0000+ 0				1.4328- 2
20.5000- 21.0000	1.4321+ 0	2.9000+ 0							0.0000+ 0				1.4319- 2
21.0000- 21.5000	1.3745+ 0	2.9000+ 0							0.0000+ 0				1.4310- 2
21.5000- 22.0000	1.3169+ 0	2.9000+ 0							0.0000+ 0				1.4301- 2
22.0000- 22.5000	1.2593+ 0	2.9000+ 0							0.0000+ 0				1.4292- 2
22.5000- 23.0000	1.2017+ 0	2.9000+ 0							0.0000+ 0				1.4283- 2
23.0000- 23.5000	1.1441+ 0	2.9000+ 0							0.0000+ 0				1.4274- 2
23.5000- 24.0000	1.0865+ 0	2.9000+ 0							0.0000+ 0				1.4265- 2
24.0000- 24.5000	1.0289+ 0	2.9000+ 0							0.0000+ 0				1.4256- 2
24.5000- 25.0000	9713+ 0	2.9000+ 0							0.0000+ 0				1.4247- 2
25.0000- 25.5000	9137+ 0	2.9000+ 0							0.0000+ 0				1.4238- 2
25.5000- 26.0000	8561+ 0	2.9000+ 0							0.0000+ 0				1.4229- 2
26.0000- 26.5000	7985+ 0	2.9000+ 0							0.0000+ 0				1.4220- 2
26.5000- 27.0000	7409+ 0	2.9000+ 0							0.0000+ 0				1.4211- 2
27.0000- 27.5000	6833+ 0	2.9000+ 0							0.0000+ 0				1.4202- 2
27.5000- 28.0000	6257+ 0	2.9000+ 0							0.0000+ 0				1.4193- 2
28.0000- 28.5000	5681+ 0	2.9000+ 0							0.0000+ 0				1.4184- 2
28.5000- 29.0000	5105+ 0	2.9000+ 0							0.0000+ 0				1.4175- 2
29.0000- 29.5000	4529+ 0	2.9000+ 0							0.0000+ 0				1.4166- 2
29.5000- 30.0000	3953+ 0	2.9000+ 0							0.0000+ 0				1.4157- 2
30.0000- 30.5000	3377+ 0	2.9000+ 0							0.0000+ 0				1.4148- 2
30.5000- 31.0000	2801+ 0	2.9000+ 0							0.0000+ 0				1.4139- 2
31.0000- 31.5000	2225+ 0	2.9000+ 0							0.0000+ 0				1.4130- 2
31.5000- 32.0000	1649+ 0	2.9000+ 0							0.0000+ 0				1.4121- 2
32.0000- 32.5000	1073+ 0	2.9000+ 0							0.0000+ 0				1.4112- 2
32.5000- 33.0000	497+ 0	2.9000+ 0							0.0000+ 0				1.4103- 2
33.0000- 33.5000	0	2.9000+ 0							0.0000+ 0				1.4094- 2
33.5000- 34.0000	0	2.9000+ 0							0.0000+ 0				1.4085- 2
34.0000- 34.5000	0	2.9000+ 0							0.0000+ 0				1.4076- 2
34.5000- 35.0000	0	2.9000+ 0							0.0000+ 0				1.4067- 2
35.0000- 35.5000	0	2.9000+ 0							0.0000+ 0				1.4058- 2
35.5000- 36.0000	0	2.9000+ 0							0.0000+ 0				1.4049- 2
36.0000- 36.5000	0	2.9000+ 0							0.0000+ 0				1.4040- 2
36.5000- 37.0000	0	2.9000+ 0							0.0000+ 0				1.4031- 2
37.0000- 37.5000	0	2.9000+ 0							0.0000+ 0				1.4022- 2
37.5000- 38.0000	0	2.9000+ 0							0.0000+ 0				1.4013- 2
38.0000- 38.5000	0	2.9000+ 0							0.0000+ 0				1.4004- 2
38.5000- 39.0000	0	2.9000+ 0							0.0000+ 0				1.3995- 2
39.0000- 39.5000	0	2.9000+ 0							0.0000+ 0				1.3986- 2
39.5000- 40.0000	0	2.9000+ 0							0.0000+ 0				1.3977- 2
40.0000- 40.5000	0	2.9000+ 0							0.0000+ 0				1.3968- 2
40.5000- 41.0000	0	2.9000+ 0							0.0000+ 0				1.3959- 2
41.0000- 41.5000	0	2.9000+ 0							0.0000+ 0				1.3950- 2
41.5000- 42.0000	0	2.9000+ 0							0.0000+ 0				1.3941- 2
42.0000- 42.5000	0	2.9000+ 0							0.0000+ 0				1.3932- 2
42.5000- 43.0000	0	2.9000+ 0							0.0000+ 0				1.3923- 2
43.0000- 43.5000	0	2.9000+ 0							0.0000+ 0				1.3914- 2
43.5000- 44.0000	0	2.9000+ 0							0.0000+ 0				1.3905- 2
44.0000- 44.5000	0	2.9000+ 0							0.0000+ 0				1.3896- 2
44.5000- 45.0000	0	2.9000+ 0							0.0000+ 0				1.3887- 2
45.0000- 45.5000	0	2.9000+ 0							0.0000+ 0				1.3878- 2
45.5000- 46.0000	0	2.9000+ 0							0.0000+ 0				1.3869- 2
46.0000- 46.5000	0	2.9000+ 0							0.0000+ 0				1.3860- 2
46.5000- 47.0000	0	2.9000+ 0				</							

CROSS SECTION

CR-48

MATERIAL = 2206

ENERGY	(N.2N)	(N.3N)	FISSION	(N.WR)	(N.MP)	CAPTURE	(N.PI)	(N.D)	(N.R)	MU-BAR
1.0000-5	1.0000-2					3.3662-0				1.4089-2
1.0000-4	1.5000-1					1.5603+0				1.4087-2
1.0000-3	2.0000-0					1.3151+0				1.4089-2
1.0000-2	3.0000+0					1.0727+0				1.4073-2
1.0000-1	4.0000+0					9.2017-1				1.4075-2
1.0000-0	5.0000+0					7.4120+0				1.4076-2
1.0000+1	6.0000-1					6.6765-1				1.4077-2
1.0000+2	7.0000-2					5.7824-1				1.4079-2
1.0000+3	8.0000-3					4.9362-1				1.4081-2
1.0000+4	9.0000-4					4.1831-1				1.4083-2
1.0000+5	1.0000-1					3.4800-1				1.4085-2
1.0000+6	2.0000-0					2.9306-1				1.4087-2
1.0000+7	3.0000+0					2.5935-1				1.4089-2
1.0000+8	4.0000+0					2.3780-1				1.4091-2
1.0000+9	5.0000+0					2.2690-1				1.4093-2
1.0000+0	6.0000-1					2.1833-1				1.4095-2
1.0000+1	7.0000-2					2.1156-1				1.4097-2
1.0000+2	8.0000-3					2.0600-1				1.4099-2
1.0000+3	9.0000-4					2.0141-1				1.4101-2
1.0000+4	1.0000-1					1.9759-1				1.4103-2
1.0000+5	2.0000-0					1.9438-1				1.4104-2
1.0000+6	3.0000+0					1.9168-1				1.4105-2
1.0000+7	4.0000+0					1.8941-1				1.4106-2
1.0000+8	5.0000+0					1.8750-1				1.4107-2
1.0000+9	6.0000-1					1.8591-1				1.4109-2
1.0000+0	7.0000-2					1.8458-1				1.4111-2
1.0000+1	8.0000-3					1.8346-1				1.4113-2
1.0000+2	9.0000-4					1.8251-1				1.4115-2
1.0000+3	1.0000-1					1.8171-1				1.4117-2
1.0000+4	2.0000-0					1.8102-1				1.4119-2
1.0000+5	3.0000+0					1.8043-1				1.4121-2
1.0000+6	4.0000+0					1.8000-1				1.4123-2
1.0000+7	5.0000+0					1.7972-1				1.4125-2
1.0000+8	6.0000-1					1.7953-1				1.4127-2
1.0000+9	7.0000-2					1.7943-1				1.4129-2
1.0000+0	8.0000-3					1.7941-1				1.4131-2
1.0000+1	9.0000-4					1.7945-1				1.4133-2
1.0000+2	1.0000-1					1.7953-1				1.4135-2
1.0000+3	2.0000-0					1.7965-1				1.4137-2
1.0000+4	3.0000+0					1.7980-1				1.4139-2
1.0000+5	4.0000+0					1.7997-1				1.4141-2
1.0000+6	5.0000+0					1.8016-1				1.4143-2
1.0000+7	6.0000-1					1.8037-1				1.4145-2
1.0000+8	7.0000-2					1.8060-1				1.4147-2
1.0000+9	8.0000-3					1.8085-1				1.4149-2
1.0000+0	9.0000-4					1.8112-1				1.4151-2
1.0000+1	1.0000-1					1.8141-1				1.4153-2
1.0000+2	2.0000-0					1.8171-1				1.4155-2
1.0000+3	3.0000+0					1.8203-1				1.4157-2
1.0000+4	4.0000+0					1.8236-1				1.4159-2
1.0000+5	5.0000+0					1.8271-1				1.4161-2
1.0000+6	6.0000-1					1.8307-1				1.4163-2
1.0000+7	7.0000-2					1.8345-1				1.4165-2
1.0000+8	8.0000-3					1.8384-1				1.4167-2
1.0000+9	9.0000-4					1.8425-1				1.4169-2
1.0000+0	1.0000-1					1.8467-1				1.4171-2
1.0000+1	2.0000-0					1.8510-1				1.4173-2
1.0000+2	3.0000+0					1.8554-1				1.4175-2
1.0000+3	4.0000+0					1.8600-1				1.4177-2
1.0000+4	5.0000+0					1.8647-1				1.4179-2
1.0000+5	6.0000-1					1.8695-1				1.4181-2
1.0000+6	7.0000-2					1.8744-1				1.4183-2
1.0000+7	8.0000-3					1.8794-1				1.4185-2
1.0000+8	9.0000-4					1.8845-1				1.4187-2
1.0000+9	1.0000-1					1.8897-1				1.4189-2
1.0000+0	2.0000-0					1.8950-1				1.4191-2
1.0000+1	3.0000+0					1.9004-1				1.4193-2
1.0000+2	4.0000+0					1.9059-1				1.4195-2
1.0000+3	5.0000+0					1.9115-1				1.4197-2
1.0000+4	6.0000-1					1.9172-1				1.4199-2
1.0000+5	7.0000-2					1.9230-1				1.4201-2
1.0000+6	8.0000-3					1.9289-1				1.4203-2
1.0000+7	9.0000-4					1.9349-1				1.4205-2
1.0000+8	1.0000-1					1.9410-1				1.4207-2
1.0000+9	2.0000-0					1.9472-1				1.4209-2
1.0000+0	3.0000+0					1.9535-1				1.4211-2
1.0000+1	4.0000+0					1.9599-1				1.4213-2
1.0000+2	5.0000+0					1.9664-1				1.4215-2
1.0000+3	6.0000-1					1.9730-1				1.4217-2
1.0000+4	7.0000-2					1.9797-1				1.4219-2
1.0000+5	8.0000-3					1.9865-1				1.4221-2
1.0000+6	9.0000-4					1.9934-1				1.4223-2
1.0000+7	1.0000-1					2.0004-1				1.4225-2
1.0000+8	2.0000-0					2.0075-1				1.4227-2
1.0000+9	3.0000+0					2.0147-1				1.4229-2
1.0000+0	4.0000+0					2.0220-1				1.4231-2
1.0000+1	5.0000+0					2.0294-1				1.4233-2
1.0000+2	6.0000-1					2.0369-1				1.4235-2
1.0000+3	7.0000-2					2.0445-1				1.4237-2
1.0000+4	8.0000-3					2.0522-1				1.4239-2
1.0000+5	9.0000-4					2.0600-1				1.4241-2
1.0000+6	1.0000-1					2.0679-1				1.4243-2
1.0000+7	2.0000-0					2.0759-1				1.4245-2
1.0000+8	3.0000+0					2.0840-1				1.4247-2
1.0000+9	4.0000+0					2.0922-1				1.4249-2
1.0000+0	5.0000+0					2.1005-1				1.4251-2
1.0000+1	6.0000-1					2.1089-1				1.4253-2
1.0000+2	7.0000-2					2.1174-1				1.4255-2
1.0000+3	8.0000-3					2.1260-1				1.4257-2
1.0000+4	9.0000-4					2.1347-1				1.4259-2
1.0000+5	1.0000-1					2.1435-1				1.4261-2
1.0000+6	2.0000-0					2.1524-1				1.4263-2
1.0000+7	3.0000+0					2.1614-1				1.4265-2
1.0000+8	4.0000+0					2.1705-1				1.4267-2
1.0000+9	5.0000+0					2.1797-1				1.4269-2
1.0000+0	6.0000-1					2.1890-1				1.4271-2
1.0000+1	7.0000-2					2.1984-1				1.4273-2
1.0000+2	8.0000-3					2.2079-1				1.4275-2
1.0000+3	9.0000-4					2.2175-1				1.4277-2
1.0000+4	1.0000-1					2.2272-1				1.4279-2
1.0000+5	2.0000-0					2.2370-1				1.4281-2
1.0000+6	3.0000+0					2.2469-1				1.4283-2
1.0000+7	4.0000+0					2.2569-1				1.4285-2
1.0000+8	5.0000+0					2.2670-1				1.4287-2
1.0000+9	6.0000-1					2.2772-1				1.4289-2
1.0000+0	7.0000-2					2.2875-1				1.4291-2
1.0000+1	8.0000-3					2.2979-1				1.4293-2
1.0000+2	9.0000-4					2.3084-1				1.4295-2
1.0000+3	1.0000-1					2.3190-1				1.4297-2
1.0000+4	2.0000-0					2.3297-1				1.4299-2
1.0000+5	3.0000+0					2.3405-1				1.4301-2
1.0000+6	4.0000+0					2.3514-1				1.4303-2
1.0000+7	5.0000+0					2.3624-1				1.4305-2
1.0000+8	6.0000-1					2.3735-1				

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CROSS SECTION

MATERIAL	ENERGY	TOTAL	ELASTIC	INEL	(N,2N)	(N,3N)	FISSION	(N,NA)	(N,NP)	(N,D)	(N,A)	MU-BRR
1.0000	5 - 1.0000 - 2	1.9988 + 1	4.6045 + 0									1.3204 - 2
1.0000	1.5000 - 2	1.9988 + 1	4.6045 + 0									1.3205 - 2
1.0000	2.0000 - 2	1.9988 + 1	4.6045 + 0									1.3206 - 2
1.0000	3.0000 - 2	1.9988 + 1	4.6045 + 0									1.3207 - 2
1.0000	4.0000 - 2	1.9988 + 1	4.6045 + 0									1.3208 - 2
1.0000	5.0000 - 2	1.9988 + 1	4.6045 + 0									1.3209 - 2
1.0000	6.0000 - 2	1.9988 + 1	4.6045 + 0									1.3210 - 2
1.0000	7.0000 - 2	1.9988 + 1	4.6045 + 0									1.3211 - 2
1.0000	8.0000 - 2	1.9988 + 1	4.6045 + 0									1.3212 - 2
1.0000	1.0000 - 1	7.3284 + 0	5.0976 + 0									1.3209 - 2
1.0000	2.0000 - 1	6.9770 + 0	5.1031 + 0									1.3209 - 2
1.0000	3.0000 - 1	6.6256 + 0	5.1116 + 0									1.3209 - 2
1.0000	4.0000 - 1	6.2742 + 0	5.1201 + 0									1.3209 - 2
1.0000	5.0000 - 1	5.9228 + 0	5.1286 + 0									1.3209 - 2
1.0000	6.0000 - 1	5.5714 + 0	5.1371 + 0									1.3209 - 2
1.0000	7.0000 - 1	5.2200 + 0	5.1456 + 0									1.3209 - 2
1.0000	8.0000 - 1	4.8686 + 0	5.1541 + 0									1.3209 - 2
1.0000	1.0000 - 0	5.9877 + 0	5.1626 + 0									1.3209 - 2
1.0000	2.0000 - 0	5.6363 + 0	5.1711 + 0									1.3209 - 2
1.0000	3.0000 - 0	5.2849 + 0	5.1796 + 0									1.3209 - 2
1.0000	4.0000 - 0	4.9335 + 0	5.1881 + 0									1.3209 - 2
1.0000	5.0000 - 0	4.5821 + 0	5.1966 + 0									1.3209 - 2
1.0000	6.0000 - 0	4.2307 + 0	5.2051 + 0									1.3209 - 2
1.0000	7.0000 - 0	3.8793 + 0	5.2136 + 0									1.3209 - 2
1.0000	8.0000 - 0	3.5279 + 0	5.2221 + 0									1.3209 - 2
1.0000	1.0000 - 1	5.1325 + 0	5.2306 + 0									1.3210 - 2
1.0000	2.0000 - 1	4.7811 + 0	5.2391 + 0									1.3210 - 2
1.0000	3.0000 - 1	4.4297 + 0	5.2476 + 0									1.3210 - 2
1.0000	4.0000 - 1	4.0783 + 0	5.2561 + 0									1.3210 - 2
1.0000	5.0000 - 1	3.7269 + 0	5.2646 + 0									1.3210 - 2
1.0000	6.0000 - 1	3.3755 + 0	5.2731 + 0									1.3210 - 2
1.0000	7.0000 - 1	3.0241 + 0	5.2816 + 0									1.3210 - 2
1.0000	8.0000 - 1	2.6727 + 0	5.2901 + 0									1.3210 - 2
1.0000	1.0000 - 0	4.6466 + 0	5.2986 + 0									1.3210 - 2
1.0000	2.0000 - 0	4.2952 + 0	5.3071 + 0									1.3210 - 2
1.0000	3.0000 - 0	3.9438 + 0	5.3156 + 0									1.3210 - 2
1.0000	4.0000 - 0	3.5924 + 0	5.3241 + 0									1.3210 - 2
1.0000	5.0000 - 0	3.2410 + 0	5.3326 + 0									1.3210 - 2
1.0000	6.0000 - 0	2.8896 + 0	5.3411 + 0									1.3210 - 2
1.0000	7.0000 - 0	2.5382 + 0	5.3496 + 0									1.3210 - 2
1.0000	8.0000 - 0	2.1868 + 0	5.3581 + 0									1.3210 - 2
1.0000	1.0000 - 1	4.8466 + 0	5.3666 + 0									1.3210 - 2
1.0000	2.0000 - 1	4.4952 + 0	5.3751 + 0									1.3210 - 2
1.0000	3.0000 - 1	4.1438 + 0	5.3836 + 0									1.3210 - 2
1.0000	4.0000 - 1	3.7924 + 0	5.3921 + 0									1.3210 - 2
1.0000	5.0000 - 1	3.4410 + 0	5.4006 + 0									1.3210 - 2
1.0000	6.0000 - 1	3.0896 + 0	5.4091 + 0									1.3210 - 2
1.0000	7.0000 - 1	2.7382 + 0	5.4176 + 0									1.3210 - 2
1.0000	8.0000 - 1	2.3868 + 0	5.4261 + 0									1.3210 - 2
1.0000	1.0000 - 0	4.6466 + 0	5.4346 + 0									1.3210 - 2
1.0000	2.0000 - 0	4.2952 + 0	5.4431 + 0									1.3210 - 2
1.0000	3.0000 - 0	3.9438 + 0	5.4516 + 0									1.3210 - 2
1.0000	4.0000 - 0	3.5924 + 0	5.4601 + 0									1.3210 - 2
1.0000	5.0000 - 0	3.2410 + 0	5.4686 + 0									1.3210 - 2
1.0000	6.0000 - 0	2.8896 + 0	5.4771 + 0									1.3210 - 2
1.0000	7.0000 - 0	2.5382 + 0	5.4856 + 0									1.3210 - 2
1.0000	8.0000 - 0	2.1868 + 0	5.4941 + 0									1.3210 - 2
1.0000	1.0000 - 1	4.6466 + 0	5.5026 + 0									1.3210 - 2
1.0000	2.0000 - 1	4.2952 + 0	5.5111 + 0									1.3210 - 2
1.0000	3.0000 - 1	3.9438 + 0	5.5196 + 0									1.3210 - 2
1.0000	4.0000 - 1	3.5924 + 0	5.5281 + 0									1.3210 - 2
1.0000	5.0000 - 1	3.2410 + 0	5.5366 + 0									1.3210 - 2
1.0000	6.0000 - 1	2.8896 + 0	5.5451 + 0									1.3210 - 2
1.0000	7.0000 - 1	2.5382 + 0	5.5536 + 0									1.3210 - 2
1.0000	8.0000 - 1	2.1868 + 0	5.5621 + 0									1.3210 - 2
1.0000	1.0000 - 0	4.6466 + 0	5.5706 + 0									1.3210 - 2
1.0000	2.0000 - 0	4.2952 + 0	5.5791 + 0									1.3210 - 2
1.0000	3.0000 - 0	3.9438 + 0	5.5876 + 0									1.3210 - 2
1.0000	4.0000 - 0	3.5924 + 0	5.5961 + 0									1.3210 - 2
1.0000	5.0000 - 0	3.2410 + 0	5.6046 + 0									1.3210 - 2
1.0000	6.0000 - 0	2.8896 + 0	5.6131 + 0									1.3210 - 2
1.0000	7.0000 - 0	2.5382 + 0	5.6216 + 0									1.3210 - 2
1.0000	8.0000 - 0	2.1868 + 0	5.6301 + 0									1.3210 - 2
1.0000	1.0000 - 1	4.6466 + 0	5.6386 + 0									1.3210 - 2
1.0000	2.0000 - 1	4.2952 + 0	5.6471 + 0									1.3210 - 2
1.0000	3.0000 - 1	3.9438 + 0	5.6556 + 0									1.3210 - 2
1.0000	4.0000 - 1	3.5924 + 0	5.6641 + 0									1.3210 - 2
1.0000	5.0000 - 1	3.2410 + 0	5.6726 + 0									1.3210 - 2
1.0000	6.0000 - 1	2.8896 + 0	5.6811 + 0									1.3210 - 2
1.0000	7.0000 - 1	2.5382 + 0	5.6896 + 0									1.3210 - 2
1.0000	8.0000 - 1	2.1868 + 0	5.6981 + 0									1.3210 - 2
1.0000	1.0000 - 0	4.6466 + 0	5.7066 + 0									1.3210 - 2
1.0000	2.0000 - 0	4.2952 + 0	5.7151 + 0									1.3210 - 2
1.0000	3.0000 - 0	3.9438 + 0	5.7236 + 0									1.3210 - 2
1.0000	4.0000 - 0	3.5924 + 0	5.7321 + 0									1.3210 - 2
1.0000	5.0000 - 0	3.2410 + 0	5.7406 + 0									1.3210 - 2
1.0000	6.0000 - 0	2.8896 + 0	5.7491 + 0									1.3210 - 2
1.0000	7.0000 - 0	2.5382 + 0	5.7576 + 0									1.3210 - 2
1.0000	8.0000 - 0	2.1868 + 0	5.7661 + 0									1.3210 - 2
1.0000	1.0000 - 1	4.6466 + 0	5.7746 + 0									1.3210 - 2
1.0000	2.0000 - 1	4.2952 + 0	5.7831 + 0									1.3210 - 2
1.0000	3.0000 - 1	3.9438 + 0	5.7916 + 0									1.3210 - 2
1.0000	4.0000 - 1	3.5924 + 0	5.8001 + 0									1.3210 - 2
1.0000	5.0000 - 1	3.2410 + 0	5.8086 + 0									1.3210 - 2
1.0000	6.0000 - 1	2.8896 + 0	5.8171 + 0									1.3210 - 2
1.0000	7.0000 - 1	2.5382 + 0	5.8256 + 0									1.3210 - 2
1.0000	8.0000 - 1	2.1868 + 0	5.8341 + 0									1.3210 - 2
1.0000	1.0000 - 0	4.6466 + 0	5.8426 + 0									1.3210 - 2
1.0000	2.0000 - 0	4.2952 + 0	5.8511 + 0									1.3210 - 2
1.0000	3.0000 - 0	3.9438 + 0	5.8596 + 0									1.3210 - 2
1.0000	4.0000 - 0	3.5924 + 0	5.8681 + 0									1.3210 - 2
1.0000	5.0000 - 0	3.2410 + 0	5.8766 + 0		</							

CROSS SECTION

CR-0

MATERIAL = 2240	ENERGY	TOTAL	ELASTIC	INELR	(N.2N)	(N.3N)	FISSION	(N.NP)	(N.NP)	(N.D)	(N.R)	NU-BAR
1.0000	5	1.3535+1	9.6501+0					9.4939+0			0.0000+0	1.2826-2
1.0000	1.5000	8.2428+0	3.8301+0					4.4077+0			0.0000+0	1.2826-2
1.0000	2.0000	7.5638+0	3.8301+0					3.7083+0			0.0000+0	1.2826-2
1.0000	3.0000	6.8848+0	3.8301+0					3.0293+0			0.0000+0	1.2826-2
1.0000	4.0000	6.2058+0	3.8301+0					2.3503+0			0.0000+0	1.2826-2
1.0000	5.0000	5.5268+0	3.8301+0					1.6713+0			0.0000+0	1.2826-2
1.0000	6.0000	4.8478+0	3.8301+0					1.0000+0			0.0000+0	1.2826-2
1.0000	7.0000	4.1688+0	3.8301+0					0.3210+0			0.0000+0	1.2826-2
1.0000	8.0000	3.4898+0	3.8301+0					0.0000+0			0.0000+0	1.2826-2
1.0000	1.5000	5.2955+0	3.8301+0					1.3918+0			0.0000+0	1.2826-2
1.0000	2.0000	4.6165+0	3.8301+0					0.7128+0			0.0000+0	1.2826-2
1.0000	3.0000	3.9375+0	3.8301+0					0.0338+0			0.0000+0	1.2826-2
1.0000	4.0000	3.2585+0	3.8301+0					0.0000+0			0.0000+0	1.2826-2
1.0000	5.0000	2.5795+0	3.8301+0					0.0000+0			0.0000+0	1.2826-2
1.0000	6.0000	1.9005+0	3.8301+0					0.0000+0			0.0000+0	1.2826-2
1.0000	7.0000	1.2215+0	3.8301+0					0.0000+0			0.0000+0	1.2826-2
1.0000	8.0000	0.5425+0	3.8301+0					0.0000+0			0.0000+0	1.2826-2
1.0000	1.5000	4.2773+0	3.8306+0					4.4078+0			0.0000+0	1.2826-2
1.0000	2.0000	3.5983+0	3.8316+0					3.7189+0			0.0000+0	1.2826-2
1.0000	3.0000	2.9193+0	3.8326+0					3.0290+0			0.0000+0	1.2826-2
1.0000	4.0000	2.2403+0	3.8336+0					2.3391+0			0.0000+0	1.2826-2
1.0000	5.0000	1.5613+0	3.8346+0					1.6492+0			0.0000+0	1.2826-2
1.0000	6.0000	0.8823+0	3.8356+0					0.9593+0			0.0000+0	1.2826-2
1.0000	7.0000	0.2033+0	3.8366+0					0.2694+0			0.0000+0	1.2826-2
1.0000	8.0000	0.0000+0	3.8376+0					0.0000+0			0.0000+0	1.2826-2
1.0000	1.5000	3.9788+0	3.8370+0					1.3980+0			0.0000+0	1.2826-2
1.0000	2.0000	3.2998+0	3.8380+0					0.7190+0			0.0000+0	1.2826-2
1.0000	3.0000	2.6208+0	3.8390+0					0.0400+0			0.0000+0	1.2826-2
1.0000	4.0000	1.9418+0	3.8400+0					0.0000+0			0.0000+0	1.2826-2
1.0000	5.0000	1.2628+0	3.8410+0					0.0000+0			0.0000+0	1.2826-2
1.0000	6.0000	0.5838+0	3.8420+0					0.0000+0			0.0000+0	1.2826-2
1.0000	7.0000	0.0000+0	3.8430+0					0.0000+0			0.0000+0	1.2826-2
1.0000	8.0000	0.0000+0	3.8440+0					0.0000+0			0.0000+0	1.2826-2
1.0000	1.5000	5.9028+0	3.9028+0					4.5622+0			0.0000+0	1.2826-2
1.0000	2.0000	5.2238+0	3.9339+0					3.8833+0			0.0000+0	1.2826-2
1.0000	3.0000	4.5448+0	3.9650+0					3.2044+0			0.0000+0	1.2826-2
1.0000	4.0000	3.8658+0	3.9961+0					2.5255+0			0.0000+0	1.2826-2
1.0000	5.0000	3.1868+0	4.0272+0					1.8466+0			0.0000+0	1.2826-2
1.0000	6.0000	2.5078+0	4.0583+0					1.1677+0			0.0000+0	1.2826-2
1.0000	7.0000	1.8288+0	4.0894+0					0.4888+0			0.0000+0	1.2826-2
1.0000	8.0000	1.1498+0	4.1205+0					0.0000+0			0.0000+0	1.2826-2
1.0000	1.5000	6.0435+0	5.0241+0					1.9117+0			0.0000+0	1.2826-2
1.0000	2.0000	5.3645+0	5.0552+0					1.2328+0			0.0000+0	1.2826-2
1.0000	3.0000	4.6855+0	5.0863+0					0.5539+0			0.0000+0	1.2826-2
1.0000	4.0000	4.0065+0	5.1174+0					0.0000+0			0.0000+0	1.2826-2
1.0000	5.0000	3.3275+0	5.1485+0					0.0000+0			0.0000+0	1.2826-2
1.0000	6.0000	2.6485+0	5.1796+0					0.0000+0			0.0000+0	1.2826-2
1.0000	7.0000	1.9695+0	5.2107+0					0.0000+0			0.0000+0	1.2826-2
1.0000	8.0000	1.2905+0	5.2418+0					0.0000+0			0.0000+0	1.2826-2
1.0000	1.5000	7.2981+0	4.2805+0					7.5922+0			0.0000+0	1.2826-2
1.0000	2.0000	6.6191+0	4.3116+0					6.8506+0			0.0000+0	1.2826-2
1.0000	3.0000	5.9401+0	4.3427+0					6.1091+0			0.0000+0	1.2826-2
1.0000	4.0000	5.2611+0	4.3738+0					5.3676+0			0.0000+0	1.2826-2
1.0000	5.0000	4.5821+0	4.4049+0					4.6261+0			0.0000+0	1.2826-2
1.0000	6.0000	3.9031+0	4.4360+0					3.8846+0			0.0000+0	1.2826-2
1.0000	7.0000	3.2241+0	4.4671+0					3.1431+0			0.0000+0	1.2826-2
1.0000	8.0000	2.5451+0	4.4982+0					2.4016+0			0.0000+0	1.2826-2
1.0000	1.5000	5.2534+0	4.9530+0					9.4247+0			0.0000+0	1.2826-2
1.0000	2.0000	4.5744+0	4.9841+0					8.6832+0			0.0000+0	1.2826-2
1.0000	3.0000	3.8954+0	5.0152+0					7.9417+0			0.0000+0	1.2826-2
1.0000	4.0000	3.2164+0	5.0463+0					7.2002+0			0.0000+0	1.2826-2
1.0000	5.0000	2.5374+0	5.0774+0					6.4587+0			0.0000+0	1.2826-2
1.0000	6.0000	1.8584+0	5.1085+0					5.7172+0			0.0000+0	1.2826-2
1.0000	7.0000	1.1794+0	5.1396+0					4.9757+0			0.0000+0	1.2826-2
1.0000	8.0000	0.5004+0	5.1707+0					4.2342+0			0.0000+0	1.2826-2
1.0000	1.5000	4.9673+0	5.6311+0					9.4247+0			0.0000+0	1.2826-2
1.0000	2.0000	4.2883+0	5.6622+0					8.6832+0			0.0000+0	1.2826-2
1.0000	3.0000	3.6093+0	5.6933+0					7.9417+0			0.0000+0	1.2826-2
1.0000	4.0000	2.9303+0	5.7244+0					7.2002+0			0.0000+0	1.2826-2
1.0000	5.0000	2.2513+0	5.7555+0					6.4587+0			0.0000+0	1.2826-2
1.0000	6.0000	1.5723+0	5.7866+0					5.7172+0			0.0000+0	1.2826-2
1.0000	7.0000	0.8933+0	5.8177+0					4.9757+0			0.0000+0	1.2826-2
1.0000	8.0000	0.2143+0	5.8488+0					4.2342+0			0.0000+0	1.2826-2
1.0000	1.5000	5.8442+0	6.3031+0					9.4247+0			0.0000+0	1.2826-2
1.0000	2.0000	5.1652+0	6.3342+0					8.6832+0			0.0000+0	1.2826-2
1.0000	3.0000	4.4862+0	6.3653+0					7.9417+0			0.0000+0	1.2826-2
1.0000	4.0000	3.8072+0	6.3964+0					7.2002+0			0.0000+0	1.2826-2
1.0000	5.0000	3.1282+0	6.4275+0					6.4587+0			0.0000+0	1.2826-2
1.0000	6.0000	2.4492+0	6.4586+0					5.7172+0			0.0000+0	1.2826-2
1.0000	7.0000	1.7702+0	6.4897+0					4.9757+0			0.0000+0	1.2826-2
1.0000	8.0000	1.0912+0	6.5208+0					4.2342+0			0.0000+0	1.2826-2
1.0000	1.5000	6.9673+0	7.9673+0					9.4247+0			0.0000+0	1.2826-2
1.0000	2.0000	6.2883+0	8.0000+0					8.6832+0			0.0000+0	1.2826-2
1.0000	3.0000	5.6093+0	8.0331+0					7.9417+0			0.0000+0	1.2826-2
1.0000	4.0000	4.9303+0	8.0662+0					7.2002+0			0.0000+0	1.2826-2
1.0000	5.0000	4.2513+0	8.1000+0					6.4587+0			0.0000+0	1.2826-2
1.0000	6.0000	3.5723+0	8.1331+0					5.7172+0			0.0000+0	1.2826-2
1.0000	7.0000	2.8933+0	8.1662+0					4.9757+0			0.0000+0	1.2826-2
1.0000	8.0000	2.2143+0	8.2000+0					4.2342+0			0.0000+0	1.2826-2
1.0000	1.5000	7.9673+0	9.0073+0					9.4247+0			0.0000+0	1.2826-2
1.0000	2.0000	7.2883+0	9.0404+0					8.6832+0			0.0000+0	1.2826-2
1.0000	3.0000	6.6093+0	9.0735+0					7.9417+0			0.0000+0	1.2826-2
1.0000	4.0000	5.9303+										

CROSS SECTION

MATERIAL = 2241

CR-50

ENERGY	TOTAL	ELASTIC	INELR	(N.2N)	(N.3N)	FSSION	(N.NR)	(N.NP)	CAPTURE	(N.P)	(N.D)	(N.A)	MU-BRE
1.0000- 5	1.0000- 2	6.5813+ 0							4.9201+ 1			0.0000+ 0	1.3483- 2
1.0000- 4	1.5000- 2	6.5814+ 0							2.2844+ 0			0.0000+ 0	1.3483- 2
1.0000- 3	2.0000- 2	6.5814+ 0							1.6208+ 1			0.0000+ 0	1.3483- 2
1.0000- 2	3.0000- 2	6.5814+ 0							1.6146+ 1			0.0000+ 0	1.3483- 2
1.0000- 1	4.0000- 2	6.5814+ 0							1.3586+ 1			0.0000+ 0	1.3483- 2
5.0000- 2	5.0000- 2	6.5815+ 0							1.1864+ 1			0.0000+ 0	1.3483- 2
6.0000- 2	6.0000- 2	6.5815+ 0							8.9571+ 0			0.0000+ 0	1.3483- 2
8.0000- 2	1.0000- 1	6.5815+ 0							8.4653+ 0			0.0000+ 0	1.3483- 2
1.0000- 1	1.5000- 1	6.5816+ 0							7.2317+ 0			0.0000+ 0	1.3483- 2
2.0000- 1	2.0000- 1	6.5818+ 0							6.0816+ 0			0.0000+ 0	1.3483- 2
3.0000- 1	3.0000- 1	6.5819+ 0							4.9036+ 0			0.0000+ 0	1.3483- 2
4.0000- 1	4.0000- 1	6.5821+ 0							3.7854+ 0			0.0000+ 0	1.3483- 2
5.0000- 1	5.0000- 1	6.5827+ 0							3.4264+ 0			0.0000+ 0	1.3483- 2
6.0000- 1	6.0000- 1	6.5830+ 0							3.0435+ 0			0.0000+ 0	1.3483- 2
8.0000- 1	1.0000+ 0	6.5835+ 0							2.6783+ 0			0.0000+ 0	1.3483- 2
1.0000+ 0	1.5000+ 0	6.5844+ 0							2.2836+ 0			0.0000+ 0	1.3483- 2
2.0000+ 0	2.0000+ 0	6.5856+ 0							1.9226+ 0			0.0000+ 0	1.3483- 2
3.0000+ 0	3.0000+ 0	6.5874+ 0							1.6156+ 0			0.0000+ 0	1.3483- 2
4.0000+ 0	4.0000+ 0	6.5898+ 0							1.3600+ 0			0.0000+ 0	1.3483- 2
5.0000+ 0	5.0000+ 0	6.5927+ 0							1.1684+ 0			0.0000+ 0	1.3483- 2
6.0000+ 0	6.0000+ 0	6.5954+ 0							1.0247+ 0			0.0000+ 0	1.3483- 2
8.0000+ 0	1.0000+ 0	6.6032+ 0							9.6246+ 0			0.0000+ 0	1.3483- 2
1.0000+ 1	1.5000+ 1	6.6118+ 0							8.5028+ 0			0.0000+ 0	1.3483- 2
2.0000+ 1	2.0000+ 1	6.6240+ 0							7.2349+ 0			0.0000+ 0	1.3483- 2
3.0000+ 1	3.0000+ 1	6.6362+ 0							5.1302+ 0			0.0000+ 0	1.3483- 2
4.0000+ 1	4.0000+ 1	6.6484+ 0							3.3444+ 0			0.0000+ 0	1.3483- 2
5.0000+ 1	5.0000+ 1	6.6606+ 0							3.8916+ 0			0.0000+ 0	1.3483- 2
6.0000+ 1	6.0000+ 1	6.6728+ 0							3.4680+ 0			0.0000+ 0	1.3483- 2
8.0000+ 1	1.0000+ 2	6.6851+ 0							2.9333+ 0			0.0000+ 0	1.3483- 2
1.0000+ 2	1.5000+ 2	6.6971+ 0							2.3538+ 0			0.0000+ 0	1.3483- 2
2.0000+ 2	2.0000+ 2	6.7093+ 0							2.0112+ 0			0.0000+ 0	1.3483- 2
3.0000+ 2	3.0000+ 2	6.7215+ 0							1.7195+ 0			0.0000+ 0	1.3483- 2
4.0000+ 2	4.0000+ 2	6.7337+ 0							1.4781+ 0			0.0000+ 0	1.3483- 2
5.0000+ 2	5.0000+ 2	6.7459+ 0							1.2861+ 0			0.0000+ 0	1.3483- 2
6.0000+ 2	6.0000+ 2	6.7581+ 0							1.1256+ 0			0.0000+ 0	1.3483- 2
8.0000+ 2	8.0000+ 2	6.7703+ 0							1.0134+ 0			0.0000+ 0	1.3483- 2
1.0000+ 3	1.5000+ 3	6.7825+ 0							1.0914+ 0			0.0000+ 0	1.3483- 2
2.0000+ 3	2.0000+ 3	6.7947+ 0							1.0482+ 0			0.0000+ 0	1.3483- 2
3.0000+ 3	3.0000+ 3	6.8069+ 0							1.0795+ 0			0.0000+ 0	1.3483- 2
4.0000+ 3	4.0000+ 3	6.8191+ 0							1.2933+ 0			0.0000+ 0	1.3483- 2
5.0000+ 3	5.0000+ 3	6.8313+ 0							2.1209+ 0			0.0000+ 0	1.3483- 2
6.0000+ 3	6.0000+ 3	6.8435+ 0							1.6715+ 0			0.0000+ 0	1.3483- 2
8.0000+ 3	8.0000+ 3	6.8557+ 0							1.3429+ 0			0.0000+ 0	1.3483- 2
1.0000+ 4	1.5000+ 4	6.8679+ 0							1.0332+ 0			0.0000+ 0	1.3483- 2
2.0000+ 4	2.0000+ 4	6.8801+ 0							1.8316+ 0			0.0000+ 0	1.3483- 2
3.0000+ 4	3.0000+ 4	6.8923+ 0							1.5960+ 0			0.0000+ 0	1.3483- 2
4.0000+ 4	4.0000+ 4	6.9045+ 0							1.3754+ 0			0.0000+ 0	1.3483- 2
5.0000+ 4	5.0000+ 4	6.9167+ 0							1.1826+ 0			0.0000+ 0	1.3483- 2
6.0000+ 4	6.0000+ 4	6.9289+ 0							1.0332+ 0			0.0000+ 0	1.3483- 2
8.0000+ 4	8.0000+ 4	6.9411+ 0							1.8316+ 0			0.0000+ 0	1.3483- 2
1.0000+ 5	1.5000+ 5	6.9533+ 0							1.5960+ 0			0.0000+ 0	1.3483- 2
2.0000+ 5	2.0000+ 5	6.9655+ 0							1.3754+ 0			0.0000+ 0	1.3483- 2
3.0000+ 5	3.0000+ 5	6.9777+ 0							1.1826+ 0			0.0000+ 0	1.3483- 2
4.0000+ 5	4.0000+ 5	6.9899+ 0							1.0332+ 0			0.0000+ 0	1.3483- 2
5.0000+ 5	5.0000+ 5	6.9999+ 0							1.8316+ 0			0.0000+ 0	1.3483- 2
6.0000+ 5	6.0000+ 5	7.0111+ 0							1.5960+ 0			0.0000+ 0	1.3483- 2
8.0000+ 5	8.0000+ 5	7.0233+ 0							1.3754+ 0			0.0000+ 0	1.3483- 2
1.0000+ 6	1.5000+ 6	7.0355+ 0							1.1826+ 0			0.0000+ 0	1.3483- 2
2.0000+ 6	2.0000+ 6	7.0477+ 0							1.0332+ 0			0.0000+ 0	1.3483- 2
3.0000+ 6	3.0000+ 6	7.0599+ 0							1.8316+ 0			0.0000+ 0	1.3483- 2
4.0000+ 6	4.0000+ 6	7.0721+ 0							1.5960+ 0			0.0000+ 0	1.3483- 2
5.0000+ 6	5.0000+ 6	7.0843+ 0							1.3754+ 0			0.0000+ 0	1.3483- 2
6.0000+ 6	6.0000+ 6	7.0965+ 0							1.1826+ 0			0.0000+ 0	1.3483- 2
8.0000+ 6	8.0000+ 6	7.1087+ 0							1.0332+ 0			0.0000+ 0	1.3483- 2
1.0000+ 7	1.5000+ 7	7.1209+ 0							1.8316+ 0			0.0000+ 0	1.3483- 2
2.0000+ 7	2.0000+ 7	7.1331+ 0							1.5960+ 0			0.0000+ 0	1.3483- 2
3.0000+ 7	3.0000+ 7	7.1453+ 0							1.3754+ 0			0.0000+ 0	1.3483- 2
4.0000+ 7	4.0000+ 7	7.1575+ 0							1.1826+ 0			0.0000+ 0	1.3483- 2
5.0000+ 7	5.0000+ 7	7.1697+ 0							1.0332+ 0			0.0000+ 0	1.3483- 2
6.0000+ 7	6.0000+ 7	7.1819+ 0							1.8316+ 0			0.0000+ 0	1.3483- 2
8.0000+ 7	8.0000+ 7	7.1941+ 0							1.5960+ 0			0.0000+ 0	1.3483- 2
1.0000+ 8	1.5000+ 8	7.2063+ 0							1.3754+ 0			0.0000+ 0	1.3483- 2
2.0000+ 8	2.0000+ 8	7.2185+ 0							1.1826+ 0			0.0000+ 0	1.3483- 2
3.0000+ 8	3.0000+ 8	7.2307+ 0							1.0332+ 0			0.0000+ 0	1.3483- 2
4.0000+ 8	4.0000+ 8	7.2429+ 0							1.8316+ 0			0.0000+ 0	1.3483- 2
5.0000+ 8	5.0000+ 8	7.2551+ 0							1.5960+ 0			0.0000+ 0	1.3483- 2
6.0000+ 8	6.0000+ 8	7.2673+ 0							1.3754+ 0			0.0000+ 0	1.3483- 2
8.0000+ 8	8.0000+ 8	7.2795+ 0							1.1826+ 0			0.0000+ 0	1.3483- 2
1.0000+ 9	1.5000+ 9	7.2917+ 0							1.8316+ 0			0.0000+ 0	1.3483- 2
2.0000+ 9	2.0000+ 9	7.3039+ 0							1.5960+ 0			0.0000+ 0	1.3483- 2
3.0000+ 9	3.0000+ 9	7.3161+ 0							1.3754+ 0			0.0000+ 0	1.3483- 2
4.0000+ 9	4.0000+ 9	7.3283+ 0							1.1826+ 0			0.0000+ 0	1.3483- 2
5.0000+ 9	5.0000+ 9	7.3405+ 0							1.0332+ 0			0.0000+ 0	1.3483- 2
6.0000+ 9	6.0000+ 9	7.3527+ 0							1.8316+ 0			0.0000+ 0	1.3483- 2
8.0000+ 9	8.0000+ 9	7.3649+ 0							1.5960+ 0			0.0000+ 0	1.3483- 2
1.0000+ 10	1.5000+ 10	7.3771+ 0							1.3754+ 0			0.0000+ 0	1.3483- 2
2.0000+ 10	2.0000+ 10	7.3893+ 0							1.1826+ 0			0.0000+ 0	1.3483- 2
3.0000+ 10	3.0000+ 10	7.4015+ 0							1.0332+ 0			0.0000+ 0	1.3483- 2
4.0000+ 10	4.0000+ 10	7.4137+ 0											

CROSS SECTION

CR-52

MATERIAL = 2242	ENERGY	TOTAL	ELASTIC	INELR	(N,2N)	(N,2N)	FUSION	(N,NR)	(N,NP)	(N,D)	(N,R)	MURR
1.0000-	5 ~ 1.0000-2	4.5766+ 0	2.2227+ 0						2.3516+ 0			1.2946- 2
1.0000-	1.5000-2	3.3149+ 0	2.2227+ 0						1.0916+ 0			1.2946- 2
1.0000-	2.0000-2	3.1466+ 0	2.2227+ 0						9.1802+ 0			1.2946- 2
1.0000-	3.0000-2	2.9956+ 0	2.2227+ 0						7.7199+ 0			1.2946- 2
1.0000-	4.0000-2	2.9596+ 0	2.2227+ 0						6.4914+ 0			1.2946- 2
1.0000-	5.0000-2	2.9366+ 0	2.2227+ 0						5.7359+ 0			1.2946- 2
1.0000-	6.0000-2	2.9216+ 0	2.2227+ 0						5.1938+ 0			1.2946- 2
1.0000-	7.0000-2	2.9116+ 0	2.2227+ 0						4.6907+ 0			1.2946- 2
1.0000-	8.0000-2	2.9036+ 0	2.2227+ 0						4.0558+ 0			1.2946- 2
1.0000-	1.5000-	2.5107+ 0	2.2227+ 0						3.4452+ 0			1.2946- 2
1.0000-	2.0000-	2.5141+ 0	2.2227+ 0						2.9083+ 0			1.2946- 2
1.0000-	3.0000-	2.4682+ 0	2.2227+ 0						2.4948+ 0			1.2946- 2
1.0000-	4.0000-	2.4290+ 0	2.2227+ 0						2.0959+ 0			1.2946- 2
1.0000-	5.0000-	2.4071+ 0	2.2227+ 0						1.6946+ 0			1.2946- 2
1.0000-	6.0000-	2.3915+ 0	2.2227+ 0						1.2948+ 0			1.2946- 2
1.0000-	7.0000-	2.3827+ 0	2.2227+ 0						1.4551+ 0			1.2946- 2
1.0000-	8.0000-	2.3827+ 0	2.2227+ 0						1.2790+ 0			1.2946- 2
1.0000+	0 ~ 1.5000+	2.3548+ 0	2.2227+ 0						1.0907+ 0			1.2946- 2
1.0000+	2.0000+	2.3500+ 0	2.2227+ 0						9.1897+ 0			1.2946- 2
1.0000+	3.0000+	2.3481+ 0	2.2227+ 0						7.7147+ 0			1.2946- 2
1.0000+	4.0000+	2.3481+ 0	2.2227+ 0						6.4914+ 0			1.2946- 2
1.0000+	5.0000+	2.3481+ 0	2.2227+ 0						5.7359+ 0			1.2946- 2
1.0000+	6.0000+	2.3481+ 0	2.2227+ 0						5.1938+ 0			1.2946- 2
1.0000+	7.0000+	2.3481+ 0	2.2227+ 0						4.6907+ 0			1.2946- 2
1.0000+	8.0000+	2.3481+ 0	2.2227+ 0						4.0558+ 0			1.2946- 2
1.0000+	1.5000+	2.2593+ 0	2.2227+ 0						3.4452+ 0			1.2946- 2
1.0000+	2.0000+	2.2566+ 0	2.2227+ 0						2.9083+ 0			1.2946- 2
1.0000+	3.0000+	2.2527+ 0	2.2227+ 0						2.4948+ 0			1.2946- 2
1.0000+	4.0000+	2.2430+ 0	2.2227+ 0						2.0959+ 0			1.2946- 2
1.0000+	5.0000+	2.2383+ 0	2.2227+ 0						1.6946+ 0			1.2946- 2
1.0000+	6.0000+	2.2383+ 0	2.2227+ 0						1.2948+ 0			1.2946- 2
1.0000+	7.0000+	2.2366+ 0	2.2227+ 0						1.4551+ 0			1.2946- 2
1.0000+	8.0000+	2.2345+ 0	2.2227+ 0						1.2830+ 0			1.2946- 2
1.0000+	1.5000+	2.2293+ 0	2.2227+ 0						1.0889+ 0			1.2946- 2
1.0000+	2.0000+	2.2270+ 0	2.2227+ 0						9.2177+ 0			1.2946- 2
1.0000+	3.0000+	2.2252+ 0	2.2227+ 0						7.7199+ 0			1.2946- 2
1.0000+	4.0000+	2.2234+ 0	2.2227+ 0						6.4914+ 0			1.2946- 2
1.0000+	5.0000+	2.2219+ 0	2.2227+ 0						5.7359+ 0			1.2946- 2
1.0000+	6.0000+	2.2219+ 0	2.2227+ 0						5.1938+ 0			1.2946- 2
1.0000+	7.0000+	2.2215+ 0	2.2227+ 0						4.6907+ 0			1.2946- 2
1.0000+	8.0000+	2.2215+ 0	2.2227+ 0						4.0558+ 0			1.2946- 2
1.0000+	1.5000+	2.2180+ 0	2.2227+ 0						3.4452+ 0			1.2946- 2
1.0000+	2.0000+	2.2170+ 0	2.2227+ 0						2.9083+ 0			1.2946- 2
1.0000+	3.0000+	2.2159+ 0	2.2227+ 0						2.4948+ 0			1.2946- 2
1.0000+	4.0000+	2.2159+ 0	2.2227+ 0						2.0959+ 0			1.2946- 2
1.0000+	5.0000+	2.2159+ 0	2.2227+ 0						1.6946+ 0			1.2946- 2
1.0000+	6.0000+	2.2159+ 0	2.2227+ 0						1.2948+ 0			1.2946- 2
1.0000+	7.0000+	2.2151+ 0	2.2227+ 0						1.4551+ 0			1.2946- 2
1.0000+	8.0000+	2.2151+ 0	2.2227+ 0						1.2830+ 0			1.2946- 2
1.0000+	1.5000+	2.2093+ 0	2.2227+ 0						1.0889+ 0			1.2946- 2
1.0000+	2.0000+	2.2083+ 0	2.2227+ 0						9.2177+ 0			1.2946- 2
1.0000+	3.0000+	2.2078+ 0	2.2227+ 0						7.7199+ 0			1.2946- 2
1.0000+	4.0000+	2.2078+ 0	2.2227+ 0						6.4914+ 0			1.2946- 2
1.0000+	5.0000+	2.2078+ 0	2.2227+ 0						5.7359+ 0			1.2946- 2
1.0000+	6.0000+	2.2078+ 0	2.2227+ 0						5.1938+ 0			1.2946- 2
1.0000+	7.0000+	2.2078+ 0	2.2227+ 0						4.6907+ 0			1.2946- 2
1.0000+	8.0000+	2.2078+ 0	2.2227+ 0						4.0558+ 0			1.2946- 2
1.0000+	1.5000+	2.1973+ 0	2.2227+ 0						3.4452+ 0			1.2946- 2
1.0000+	2.0000+	2.1973+ 0	2.2227+ 0						2.9083+ 0			1.2946- 2
1.0000+	3.0000+	2.1973+ 0	2.2227+ 0						2.4948+ 0			1.2946- 2
1.0000+	4.0000+	2.1973+ 0	2.2227+ 0						2.0959+ 0			1.2946- 2
1.0000+	5.0000+	2.1973+ 0	2.2227+ 0						1.6946+ 0			1.2946- 2
1.0000+	6.0000+	2.1973+ 0	2.2227+ 0						1.2948+ 0			1.2946- 2
1.0000+	7.0000+	2.1973+ 0	2.2227+ 0						1.4551+ 0			1.2946- 2
1.0000+	8.0000+	2.1973+ 0	2.2227+ 0						1.2830+ 0			1.2946- 2
1.0000+	1.5000+	2.1874+ 0	2.2227+ 0						1.0889+ 0			1.2946- 2
1.0000+	2.0000+	2.1874+ 0	2.2227+ 0						9.2177+ 0			1.2946- 2
1.0000+	3.0000+	2.1874+ 0	2.2227+ 0						7.7199+ 0			1.2946- 2
1.0000+	4.0000+	2.1874+ 0	2.2227+ 0						6.4914+ 0			1.2946- 2
1.0000+	5.0000+	2.1874+ 0	2.2227+ 0						5.7359+ 0			1.2946- 2
1.0000+	6.0000+	2.1874+ 0	2.2227+ 0						5.1938+ 0			1.2946- 2
1.0000+	7.0000+	2.1874+ 0	2.2227+ 0						4.6907+ 0			1.2946- 2
1.0000+	8.0000+	2.1874+ 0	2.2227+ 0						4.0558+ 0			1.2946- 2
1.0000+	1.5000+	2.1770+ 0	2.2227+ 0						3.4452+ 0			1.2946- 2
1.0000+	2.0000+	2.1770+ 0	2.2227+ 0						2.9083+ 0			1.2946- 2
1.0000+	3.0000+	2.1770+ 0	2.2227+ 0						2.4948+ 0			1.2946- 2
1.0000+	4.0000+	2.1770+ 0	2.2227+ 0						2.0959+ 0			1.2946- 2
1.0000+	5.0000+	2.1770+ 0	2.2227+ 0						1.6946+ 0			1.2946- 2
1.0000+	6.0000+	2.1770+ 0	2.2227+ 0						1.2948+ 0			1.2946- 2
1.0000+	7.0000+	2.1770+ 0	2.2227+ 0						1.4551+ 0			1.2946- 2
1.0000+	8.0000+	2.1770+ 0	2.2227+ 0						1.2830+ 0			1.2946- 2
1.0000+	1.5000+	2.1674+ 0	2.2227+ 0						1.0889+ 0			1.2946- 2
1.0000+	2.0000+	2.1674+ 0	2.2227+ 0						9.2177+ 0			1.2946- 2
1.0000+	3.0000+	2.1674+ 0	2.2227+ 0						7.7199+ 0			1.2946- 2
1.0000+	4.0000+	2.1674+ 0	2.2227+ 0						6.4914+ 0			1.2946- 2
1.0000+	5.0000+	2.1674+ 0	2.2227+ 0						5.7359+ 0			1.2946- 2
1.0000+	6.0000+	2.1674+ 0	2.2227+ 0						5.1938+ 0			1.2946- 2
1.0000+	7.0000+	2.1674+ 0	2.2227+ 0						4.6907+ 0			1.2946- 2
1.0000+	8.0000+	2.1674+ 0	2.2227+ 0						4.0558+ 0			1.2946- 2
1.0000+	1.5000+	2.1574+ 0	2.2227+ 0						3.4452+ 0			1.2946- 2
1.0000+	2.0000+	2.1574+ 0	2.2227+ 0						2.9083+ 0			1.2946- 2
1.0000+	3.0000+	2.1574+ 0	2.2227+ 0						2.4948+ 0			1.2946- 2
1.0000+	4.0000+	2.1574+ 0	2.2227+ 0						2.0959+ 0			1.2946- 2
1.0000+	5.0000+	2.1574+ 0	2.2227+ 0						1.6946+ 0			1.2946- 2
1.0000+	6.0000+	2.1574+ 0	2.2227+ 0						1.2948+ 0			1.2946- 2
1.0000+	7.0000+	2.1574+ 0	2.2227+ 0						1.455			

CROSS SECTION

CR-53

MATERIAL = 2243	ENERGY	TOTL	ELASTIC	INELR	(N,2N)	(N,3N)	FLIBIDN	(N,NR)	(N,NP)	(N,D)	(N,R)	MU-BRR
1.0000	5 ~ 1.0000-2	7.2656+1	1.6306+1								0.0000+0	1.2702-2
1.0000	1.5000-2	4.2480+1	1.6305+1								0.0000+0	1.2702-2
1.0000	2.0000-2	3.6362+1	1.6305+1								0.0000+0	1.2702-2
1.0000	3.0000-2	3.4824+1	1.6305+1								0.0000+0	1.2702-2
1.0000	4.0000-2	3.3008+1	1.6305+1								0.0000+0	1.2702-2
1.0000	5.0000-2	3.0977+1	1.6305+1								0.0000+0	1.2702-2
1.0000	6.0000-2	2.8714+1	1.6305+1								0.0000+0	1.2702-2
1.0000	8.0000-2	2.7367+1	1.6305+1								0.0000+0	1.2702-2
1.0000	1.0000-1	2.6040+1	1.6306+1								0.0000+0	1.2702-2
1.0000	1.5000-1	2.4621+1	1.6306+1								0.0000+0	1.2702-2
1.0000	2.0000-1	2.3311+1	1.6306+1								0.0000+0	1.2702-2
1.0000	3.0000-1	2.2189+1	1.6307+1								0.0000+0	1.2702-2
1.0000	4.0000-1	2.1291+1	1.6307+1								0.0000+0	1.2702-2
1.0000	5.0000-1	2.0592+1	1.6308+1								0.0000+0	1.2702-2
1.0000	6.0000-1	1.9942+1	1.6308+1								0.0000+0	1.2702-2
1.0000	8.0000-1	1.9406+1	1.6309+1								0.0000+0	1.2702-2
1.0000	0 ~ 1.5000+0	1.8968+1	1.6311+1								0.0000+0	1.2702-2
1.0000	0 ~ 2.0000+0	1.8559+1	1.6311+1								0.0000+0	1.2702-2
1.0000	0 ~ 3.0000+0	1.8177+1	1.6322+1								0.0000+0	1.2702-2
1.0000	0 ~ 4.0000+0	1.7817+1	1.6327+1								0.0000+0	1.2702-2
1.0000	0 ~ 5.0000+0	1.7472+1	1.6332+1								0.0000+0	1.2702-2
1.0000	0 ~ 6.0000+0	1.7142+1	1.6339+1								0.0000+0	1.2702-2
1.0000	0 ~ 8.0000+0	1.6828+1	1.6349+1								0.0000+0	1.2702-2
1.0000	1 ~ 1.5000+1	1.7221+1	1.6366+1								0.0000+0	1.2702-2
1.0000	1 ~ 2.0000+1	1.7148+1	1.6391+1								0.0000+0	1.2702-2
1.0000	1 ~ 3.0000+1	1.7083+1	1.6428+1								0.0000+0	1.2702-2
1.0000	1 ~ 4.0000+1	1.7027+1	1.6478+1								0.0000+0	1.2702-2
1.0000	1 ~ 5.0000+1	1.6977+1	1.6527+1								0.0000+0	1.2702-2
1.0000	1 ~ 6.0000+1	1.6930+1	1.6578+1								0.0000+0	1.2702-2
1.0000	1 ~ 8.0000+1	1.6880+1	1.6632+1								0.0000+0	1.2702-2
1.0000	1 ~ 1.0000+2	1.7011+1	1.6654+1								0.0000+0	1.2702-2
1.0000	1 ~ 1.5000+2	1.7073+1	1.6757+1								0.0000+0	1.2702-2
1.0000	2 ~ 2.0000+2	1.7261+1	1.6842+1								0.0000+0	1.2702-2
1.0000	2 ~ 3.0000+2	1.7459+1	1.7213+1								0.0000+0	1.2702-2
1.0000	2 ~ 4.0000+2	1.7642+1	1.7642+1								0.0000+0	1.2702-2
1.0000	2 ~ 5.0000+2	1.8465+1	1.8252+1								0.0000+0	1.2702-2
1.0000	2 ~ 6.0000+2	1.9112+1	1.8911+1								0.0000+0	1.2702-2
1.0000	2 ~ 8.0000+2	1.9623+1	1.9523+1								0.0000+0	1.2702-2
1.0000	3 ~ 1.0000+3	2.2823+1	2.2862+1								0.0000+0	1.2702-2
1.0000	3 ~ 2.0000+3	2.7023+1	2.6872+1								0.0000+0	1.2702-2
1.0000	3 ~ 3.0000+3	3.0969+1	3.0969+1								0.0000+0	1.2702-2
1.0000	3 ~ 4.0000+3	3.4000+1	3.4000+1								0.0000+0	1.2702-2
1.0000	3 ~ 5.0000+3	3.6220+2	3.6220+2								0.0000+0	1.2702-2
1.0000	3 ~ 6.0000+3	3.7555+2	3.7555+2								0.0000+0	1.2702-2
1.0000	3 ~ 8.0000+3	3.8554+2	3.8554+2								0.0000+0	1.2702-2
1.0000	4 ~ 1.5000+4	2.6344+1	2.6344+1								0.0000+0	1.2702-2
1.0000	4 ~ 2.0000+4	1.2040+1	1.2007+1								0.0000+0	1.2702-2
1.0000	4 ~ 3.0000+4	1.4325+1	1.4228+1								0.0000+0	1.2702-2
1.0000	4 ~ 4.0000+4	8.0750+1	8.0750+1								0.0000+0	1.2702-2
1.0000	4 ~ 5.0000+4	1.8220+2	1.8032+2								0.0000+0	1.2702-2
1.0000	4 ~ 6.0000+4	1.9173+2	1.9173+2								0.0000+0	1.2702-2
1.0000	4 ~ 8.0000+4	1.4457+2	1.4354+2								0.0000+0	1.2702-2
1.0000	4 ~ 1.0000+5	1.8552+1	1.2531+1								0.0000+0	1.2702-2
1.0000	5 ~ 1.5000+5	5.9847+1	1.0980+1								0.0000+0	1.2702-2
1.0000	5 ~ 2.0000+5	3.2524+1	3.2524+1								0.0000+0	1.2702-2
1.0000	5 ~ 3.0000+5	3.8795+1	3.8795+1								0.0000+0	1.2702-2
1.0000	5 ~ 4.0000+5	3.3777+1	3.3777+1								0.0000+0	1.2702-2
1.0000	5 ~ 5.0000+5	3.1177+1	3.1144+1								0.0000+0	1.2702-2
1.0000	5 ~ 6.0000+5	2.9938+1	2.9938+1								0.0000+0	1.2702-2
1.0000	5 ~ 8.0000+5	2.8681+1	2.8681+1								0.0000+0	1.2702-2
1.0000	6 ~ 1.0000+6	1.9000+1	1.9000+1								0.0000+0	1.2702-2
1.0000	6 ~ 2.0000+6	1.5000+1	1.5000+1								0.0000+0	1.2702-2
1.0000	6 ~ 3.0000+6	1.3555+1	1.3555+1								0.0000+0	1.2702-2
1.0000	6 ~ 4.0000+6	1.2000+1	1.2000+1								0.0000+0	1.2702-2
1.0000	6 ~ 5.0000+6	1.0500+1	1.0500+1								0.0000+0	1.2702-2
1.0000	6 ~ 6.0000+6	0.9000+1	0.9000+1								0.0000+0	1.2702-2
1.0000	6 ~ 8.0000+6	0.7500+1	0.7500+1								0.0000+0	1.2702-2
1.0000	7 ~ 1.5000+7	2.5666+1	1.3775+1								0.0000+0	1.2702-2
1.0000	7 ~ 2.0000+7	2.2250+1	1.0252+1								0.0000+0	1.2702-2
1.0000	7 ~ 3.0000+7	1.9250+1	0.6250+1								0.0000+0	1.2702-2
1.0000	7 ~ 4.0000+7	1.6250+1	0.2250+1								0.0000+0	1.2702-2
1.0000	7 ~ 5.0000+7	1.3250+1	0.0250+1								0.0000+0	1.2702-2
1.0000	7 ~ 6.0000+7	1.0250+1	0.0000+0								0.0000+0	1.2702-2
1.0000	7 ~ 8.0000+7	0.7250+1	0.0000+0								0.0000+0	1.2702-2
1.0000	8 ~ 1.5000+8	7.9045-4	7.9045-4								0.0000+0	1.2702-2
1.0000	8 ~ 2.0000+8	5.3615-2	5.3615-2								0.0000+0	1.2702-2
1.0000	8 ~ 3.0000+8	2.9377-5	2.9377-5								0.0000+0	1.2702-2
1.0000	8 ~ 4.0000+8	1.4533-3	1.4533-3								0.0000+0	1.2702-2
1.0000	8 ~ 5.0000+8	7.0489-7	7.0489-7								0.0000+0	1.2702-2
1.0000	8 ~ 6.0000+8	3.4227-9	3.4227-9								0.0000+0	1.2702-2
1.0000	8 ~ 8.0000+8	9.2725-9	9.2725-9								0.0000+0	1.2702-2

CROSS SECTION

MH-85

MATERIAL = 2251

ENERGY	TOTAL	ELASTIC	(M,2N)	(M,3N)	FISSION	(M,NR)	(M,NP)	CAPTURE	(N,P)	(N,D)	(N,R)	MU-BRR
1.0000-5	4.3994+1	2.1638+0						4.1210+1				1.2276-2
1.0000-4	2.1318+1	0.0000+0						1.9138+1				1.2287-2
1.5000-4	1.8773+1	0.0000+0						1.3523+1				1.2290-2
2.0000-4	1.5708+1	0.0000+0						1.1331+1				1.2293-2
3.0000-4	1.2920+1	0.0000+0						1.0034+1				1.2296-2
4.0000-4	1.0820+1	0.0000+0						8.0632+0				1.2299-2
5.0000-4	1.1247+1	0.0000+0						9.0618+0				1.2302-2
6.0000-4	1.0246+1	0.0000+0						7.1088+0				1.2305-2
8.0000-4	9.2805+0	0.0000+0						6.0579+0				1.2308-2
1.0000-3	8.2427+0	0.0000+0						5.0976+0				1.2311-2
1.5000-3	7.2627+0	0.0000+0						4.2735+0				1.2314-2
2.0000-3	6.4551+0	0.0000+0						3.7072+0				1.2317-2
3.0000-3	5.7945+0	0.0000+0						3.1742+0				1.2320-2
4.0000-3	5.3615+0	0.0000+0						2.8780+0				1.2323-2
5.0000-3	5.0000+0	0.0000+0						2.6549+0				1.2326-2
6.0000-3	4.7054+0	0.0000+0						2.4811+0				1.2329-2
8.0000-3	4.4353+0	0.0000+0						2.2481+0				1.2332-2
1.0000-2	4.1146+0	0.0000+0						1.9218+0				1.2335-2
1.5000-2	3.8150+0	0.0000+0						1.6198+0				1.2338-2
2.0000-2	3.5815+0	0.0000+0						1.3655+0				1.2341-2
3.0000-2	3.3823+0	0.0000+0						1.1593+0				1.2344-2
4.0000-2	3.2407+0	0.0000+0						1.0238+0				1.2347-2
5.0000-2	3.1510+0	0.0000+0						9.2322+0				1.2350-2
6.0000-2	3.0627+0	0.0000+0						8.2322+0				1.2353-2
8.0000-2	2.9850+0	0.0000+0						7.3359+0				1.2356-2
1.0000-1	2.9152+0	0.0000+0						6.3420+0				1.2359-2
1.5000-1	2.8722+0	0.0000+0						5.4709+0				1.2362-2
2.0000-1	2.8791+0	0.0000+0						4.7231+0				1.2365-2
3.0000-1	2.9250+0	0.0000+0						4.1154+0				1.2368-2
4.0000-1	3.0447+0	0.0000+0						3.6480+0				1.2371-2
5.0000-1	3.1471+0	0.0000+0						3.2627+0				1.2374-2
6.0000-1	3.2405+0	0.0000+0						2.9519+0				1.2377-2
8.0000-1	3.3855+0	0.0000+0						2.7359+0				1.2380-2
1.0000-0	3.5295+0	0.0000+0						2.5821+0				1.2383-2
1.5000-0	3.6730+0	0.0000+0						2.4778+0				1.2386-2
2.0000-0	3.8222+0	0.0000+0						2.4057+0				1.2389-2
3.0000-0	3.9791+0	0.0000+0						2.3517+0				1.2392-2
4.0000-0	4.1439+0	0.0000+0						2.3165+0				1.2395-2
5.0000-0	4.3159+0	0.0000+0						2.2985+0				1.2398-2
6.0000-0	4.4947+0	0.0000+0						2.2951+0				1.2401-2
8.0000-0	4.6788+0	0.0000+0						2.3031+0				1.2404-2
1.0000+1	4.8658+0	0.0000+0						2.3211+0				1.2407-2
1.5000+1	5.0539+0	0.0000+0						2.3481+0				1.2410-2
2.0000+1	5.2430+0	0.0000+0						2.3831+0				1.2413-2
3.0000+1	5.4332+0	0.0000+0						2.4261+0				1.2416-2
4.0000+1	5.6243+0	0.0000+0						2.4771+0				1.2419-2
5.0000+1	5.8164+0	0.0000+0						2.5351+0				1.2422-2
6.0000+1	6.0105+0	0.0000+0						2.5991+0				1.2425-2
8.0000+1	6.2066+0	0.0000+0						2.6691+0				1.2428-2
1.0000+2	6.4047+0	0.0000+0						2.7451+0				1.2431-2
1.5000+2	6.6048+0	0.0000+0						2.8271+0				1.2434-2
2.0000+2	6.8069+0	0.0000+0						2.9151+0				1.2437-2
3.0000+2	7.0110+0	0.0000+0						3.0091+0				1.2440-2
4.0000+2	7.2171+0	0.0000+0						3.1091+0				1.2443-2
5.0000+2	7.4252+0	0.0000+0						3.2151+0				1.2446-2
6.0000+2	7.6353+0	0.0000+0						3.3271+0				1.2449-2
8.0000+2	7.8474+0	0.0000+0						3.4451+0				1.2452-2
1.0000+3	8.0615+0	0.0000+0						3.5691+0				1.2455-2
1.5000+3	8.2776+0	0.0000+0						3.6991+0				1.2458-2
2.0000+3	8.4957+0	0.0000+0						3.8351+0				1.2461-2
3.0000+3	8.7158+0	0.0000+0						3.9771+0				1.2464-2
4.0000+3	8.9379+0	0.0000+0						4.1251+0				1.2467-2
5.0000+3	9.1620+0	0.0000+0						4.2791+0				1.2470-2
6.0000+3	9.3881+0	0.0000+0						4.4391+0				1.2473-2
8.0000+3	9.6162+0	0.0000+0						4.6051+0				1.2476-2
1.0000+4	9.8473+0	0.0000+0						4.7771+0				1.2479-2
1.5000+4	1.0082+1	0.0000+0						4.9551+0				1.2482-2
2.0000+4	1.0291+1	0.0000+0						5.1391+0				1.2485-2
3.0000+4	1.0500+1	0.0000+0						5.3291+0				1.2488-2
4.0000+4	1.0710+1	0.0000+0						5.5251+0				1.2491-2
5.0000+4	1.0920+1	0.0000+0						5.7271+0				1.2494-2
6.0000+4	1.1130+1	0.0000+0						5.9351+0				1.2497-2
8.0000+4	1.1340+1	0.0000+0						6.1491+0				1.2500-2
1.0000+5	1.1550+1	0.0000+0						6.3691+0				1.2503-2
1.5000+5	1.1760+1	0.0000+0						6.5951+0				1.2506-2
2.0000+5	1.1970+1	0.0000+0						6.8271+0				1.2509-2
3.0000+5	1.2180+1	0.0000+0						7.0651+0				1.2512-2
4.0000+5	1.2390+1	0.0000+0						7.3091+0				1.2515-2
5.0000+5	1.2600+1	0.0000+0						7.5591+0				1.2518-2
6.0000+5	1.2810+1	0.0000+0						7.8151+0				1.2521-2
8.0000+5	1.3020+1	0.0000+0						8.0771+0				1.2524-2
1.0000+6	1.3230+1	0.0000+0						8.3451+0				1.2527-2
1.5000+6	1.3440+1	0.0000+0						8.6191+0				1.2530-2
2.0000+6	1.3650+1	0.0000+0						8.8991+0				1.2533-2
3.0000+6	1.3860+1	0.0000+0						9.1851+0				1.2536-2
4.0000+6	1.4070+1	0.0000+0						9.4771+0				1.2539-2
5.0000+6	1.4280+1	0.0000+0						9.7751+0				1.2542-2
6.0000+6	1.4490+1	0.0000+0						1.0079+1				1.2545-2
8.0000+6	1.4700+1	0.0000+0						1.0419+1				1.2548-2
1.0000+7	1.4910+1	0.0000+0						1.0771+1				1.2551-2
1.5000+7	1.5120+1	0.0000+0						1.1131+1				1.2554-2
2.0000+7	1.5330+1	0.0000+0						1.1501+1				1.2557-2
3.0000+7	1.5540+1	0.0000+0						1.1881+1				1.2560-2
4.0000+7	1.5750+1	0.0000+0						1.2271+1				1.2563-2
5.0000+7	1.5960+1	0.0000+0						1.2671+1				1.2566-2
6.0000+7	1.6170+1	0.0000+0						1.3081+1				1.2569-2
8.0000+7	1.6380+1	0.0000+0						1.3501+1				1.2572-2
1.0000+8	1.6590+1	0.0000+0						1.3931+1				1.2575-2
1.5000+8	1.6800+1	0.0000+0						1.4371+1				1.2578-2
2.0000+8	1.7010+1	0.0000+0						1.4821+1				1.2581-2
3.0000+8	1.7220+1	0.0000+0						1.5281+1				1.2584-2
4.0000+8	1.7430+1	0.0000+0						1.5751+1				1.2587-2
5.0000+8	1.7640+1	0.0000+0						1.6231+1				1.2590-2
6.0000+8	1.7850+1	0.0000+0						1.6721+1				1.2593-2
8.0000+8	1.8060+1	0.0000+0						1.7221+1				1.2596-2
1.0000+9	1.8270+1	0.0000+0						1.7731+1				1.2599-2
1.5000+9	1.8480+1	0.0000+0						1.8251+1				1.2602-2
2.0000+9	1.8690+1	0.0000+0						1.8781+1				1.2605-2
3.0000+9	1.8900+1	0.0000+0						1.9321+1				1.2608-2
4.0000+9	1.9110+1	0.0000+0						1.9871+1				1.2611-2
5.0000+9	1.9320+1	0.0000+0						2.0431+1				1.2614-2
6.0000+9	1.9530+1	0.0000+0						2.1001+1				1.2617-2
8.0000+9	1.9740+1	0.0000+0						2.1581+1				1.2620-2
1.0000+10	1.9950+1	0.0000+0						2.2171+1				1.2623-2
1.5000+10	2.0160+1	0.0000+0						2.2771+1				1.2626-2
2.0000+10	2.0370+1	0.0000+0						2.3381+1				1.2629-2
3.0000+10	2.0580+1	0.0000+0						2.4001+1				1.2632-2
4.0000+10	2.0790+1	0.0000+0						2.4631+1				1.2635-2
5.0000+10	2.1000+1	0.0000+0						2.5271+1			</	

CROSS SECTION

FE-0

MATERIAL = 2280

ENERGY	TOTAL	ELABRIC	INELR	(N,2N)	(N,3N)	FISSION	(N,NR)	(N,NP)	CAPTURE	(N,P)	(N,O)	(N,A)	MU-BRR
1.0000-5	2.1950+1	1.1934+1							9.4166+0	0.0000+0		0.0000+0	1.2480-2
1.0000-4	1.6171+1	1.2404+1							3.7674+0	0.0000+0		0.0000+0	1.2582-2
1.0000-3	1.5626+1	1.2293+1							3.0927+0	0.0000+0		0.0000+0	1.2607-2
1.0000-2	1.4657+1	1.2088+1							2.5684+0	0.0000+0		0.0000+0	1.2634-2
1.0000-1	1.4283+1	1.2010+1							2.1591+0	0.0000+0		0.0000+0	1.2660-2
5.0000-2	1.4095+1	1.2421+1							1.8920+0	0.0000+0		0.0000+0	1.2679-2
6.0000-2	1.3905+1	1.2461+1							1.9672+0	0.0000+0		0.0000+0	1.2695-2
8.0000-2	1.3717+1	1.2480+1							1.2571+0	0.0000+0		0.0000+0	1.2732-2
1.0000-1	1.3521+1	1.2462+1							1.0890+0	0.0000+0		0.0000+0	1.2757-2
1.5000-1	1.3339+1	1.2417+1							9.3273-1	0.0000+0		0.0000+0	1.2782-2
2.0000-1	1.3190+1	1.2405+1							8.2470-1	0.0000+0		0.0000+0	1.2806-2
3.0000-1	1.3072+1	1.2383+1							7.1611-1	0.0000+0		0.0000+0	1.2830-2
4.0000-1	1.2981+1	1.2363+1							6.0761-1	0.0000+0		0.0000+0	1.2854-2
5.0000-1	1.2911+1	1.2345+1							5.0087-1	0.0000+0		0.0000+0	1.2869-2
6.0000-1	1.2862+1	1.2329+1							4.5859-1	0.0000+0		0.0000+0	1.2889-2
8.0000-1	1.2822+1	1.2316+1							4.2410-1	0.0000+0		0.0000+0	1.2907-2
1.0000-0	2.7650+1	1.2385+1							3.7523+1	0.0000+0		0.0000+0	1.2931-2
1.5000-0	1.7266+1	1.2355+1							3.0963+1	0.0000+0		0.0000+0	1.2957-2
2.0000-0	1.2641+1	1.2338+1							2.5265+1	0.0000+0		0.0000+0	1.2984-2
3.0000-0	1.2552+1	1.2330+1							2.1053+1	0.0000+0		0.0000+0	1.3010-2
4.0000-0	1.2577+1	1.2371+1							1.7933+1	0.0000+0		0.0000+0	1.3036-2
5.0000-0	1.2582+1	1.2368+1							1.4933+1	0.0000+0		0.0000+0	1.3062-2
6.0000-0	1.2582+1	1.2368+1							1.2656+1	0.0000+0		0.0000+0	1.3088-2
8.0000-0	1.2474+1	1.2338+1							1.3831+1	0.0000+0		0.0000+0	1.3114-2
1.0000-1	1.2430+1	1.2318+1							1.1471+1	0.0000+0		0.0000+0	1.3140-2
1.5000-1	1.2361+1	1.2289+1							8.4745-1	0.0000+0		0.0000+0	1.3166-2
2.0000-1	1.2276+1	1.2271+1							7.2431-1	0.0000+0		0.0000+0	1.3192-2
3.0000-1	1.2176+1	1.2216+1							6.0428-1	0.0000+0		0.0000+0	1.3218-2
4.0000-1	1.2114+1	1.2165+1							5.4991-1	0.0000+0		0.0000+0	1.3244-2
5.0000-1	1.2021+1	1.2098+1							4.5991-1	0.0000+0		0.0000+0	1.3270-2
6.0000-1	1.1901+1	1.1951+1							4.3753-1	0.0000+0		0.0000+0	1.3296-2
1.0000-2	1.1702+1	1.1850+1							4.1291-1	0.0000+0		0.0000+0	1.3322-2
1.5000-2	1.1489+1	1.1799+1							3.8439-1	0.0000+0		0.0000+0	1.3348-2
2.0000-2	1.1051+1	1.1024+1							2.6601-1	0.0000+0		0.0000+0	1.3374-2
3.0000-2	1.0693+1	1.0678+1							1.7951-1	0.0000+0		0.0000+0	1.3400-2
4.0000-2	9.8072+0	9.7688+0							1.4563-1	0.0000+0		0.0000+0	1.3426-2
5.0000-2	9.3065+0	9.2345+0							1.1946-1	0.0000+0		0.0000+0	1.3452-2
6.0000-2	8.7255+0	8.7151+0							9.7061-2	0.0000+0		0.0000+0	1.3478-2
8.0000-2	8.2293+0	7.9425+0							8.4752-2	0.0000+0		0.0000+0	1.3504-2
1.0000-3	6.1416+0	6.1371+0							7.0566-2	0.0000+0		0.0000+0	1.3530-2
1.5000-3	6.0495+0	6.0384+0							6.4174-2	0.0000+0		0.0000+0	1.3556-2
2.0000-3	5.4754+0	5.4651+0							5.2373-2	0.0000+0		0.0000+0	1.3582-2
3.0000-3	5.6754+0	5.6699+0							4.9252-2	0.0000+0		0.0000+0	1.3608-2
4.0000-3	4.1259+1	4.1188+1							4.2211-2	0.0000+0		0.0000+0	1.3634-2
5.0000-3	4.8892+0	4.8756+0							3.5722-2	0.0000+0		0.0000+0	1.3660-2
6.0000-3	2.9864+0	2.9692+0							2.1973-2	0.0000+0		0.0000+0	1.3686-2
8.0000-3	2.7470+0	2.7297+0							1.6440-2	0.0000+0		0.0000+0	1.3712-2
1.0000-4	2.0745+0	2.0604+0							1.1615-2	0.0000+0		0.0000+0	1.3738-2
1.5000-4	1.4434+0	1.4394+0							9.6853-3	0.0000+0		0.0000+0	1.3764-2
2.0000-4	3.7205+0	3.6803+0							7.7084-3	0.0000+0		0.0000+0	1.3790-2
3.0000-4	6.0064+0	5.9769+0							1.7859-2	0.0000+0		0.0000+0	1.3816-2
4.0000-4	3.8268+0	3.8773+0							8.6399-3	0.0000+0		0.0000+0	1.3842-2
5.0000-4	3.0717+0	3.0448+0							7.6935-3	0.0000+0		0.0000+0	1.3868-2
6.0000-4	3.1449+0	3.1224+0							6.9345-3	0.0000+0		0.0000+0	1.3894-2
8.0000-4	2.9411+0	2.9259+0							5.2629-3	0.0000+0		0.0000+0	1.3920-2
1.0000-5	2.8343+0	2.8056+0							6.5000-3	0.0000+0		0.0000+0	1.3946-2
1.5000-5	2.5048+0	2.4652+0							4.0221-3	0.0000+0		0.0000+0	1.3972-2
2.0000-5	2.2500+0	2.1865+0							3.5852-3	0.0000+0		0.0000+0	1.4000-2
3.0000-5	1.9471+0	1.9116+0							2.6080-3	0.0000+0		0.0000+0	1.4026-2
4.0000-5	1.4634+0	1.4474+0							2.3257-3	0.0000+0		0.0000+0	1.4052-2
5.0000-5	3.6400+0	3.6209+0							1.8055-3	0.0000+0		0.0000+0	1.4078-2
6.0000-5	3.1503+0	3.1254+0							1.7150-3	0.0000+0		0.0000+0	1.4104-2
8.0000-5	2.7045+0	2.6797+0							1.5893-3	0.0000+0		0.0000+0	1.4130-2
1.0000-7	2.3020+0	2.2735+0							2.0489-1	0.0000+0		0.0000+0	1.4156-2
1.5000-7	2.0455+0	2.0162+0							1.7193-1	0.0000+0		0.0000+0	1.4182-2
2.0000-7	1.7500+0	1.7193+0							1.4789-1	0.0000+0		0.0000+0	1.4208-2
3.0000-7	1.5000+0	1.4684+0							1.2532-1	0.0000+0		0.0000+0	1.4234-2
4.0000-7	1.2500+0	1.2150+0							1.0539-1	0.0000+0		0.0000+0	1.4260-2
5.0000-7	1.0000+0	9.6000+0							8.6200+0	0.0000+0		0.0000+0	1.4286-2
6.0000-7	8.0000+0	7.7500+0							7.5000+0	0.0000+0		0.0000+0	1.4312-2
8.0000-7	7.0000+0	6.7500+0							6.4000+0	0.0000+0		0.0000+0	1.4338-2
1.0000-8	6.0000+0	5.7500+0							5.3000+0	0.0000+0		0.0000+0	1.4364-2
1.5000-8	5.0000+0	4.7500+0							4.2000+0	0.0000+0		0.0000+0	1.4390-2
2.0000-8	4.0000+0	3.7500+0							3.1000+0	0.0000+0		0.0000+0	1.4416-2
3.0000-8	3.0000+0	2.7500+0							2.0000+0	0.0000+0		0.0000+0	1.4442-2
4.0000-8	2.0000+0	1.7500+0							1.0000+0	0.0000+0		0.0000+0	1.4468-2
5.0000-8	1.0000+0	0.7500+0							0.5000+0	0.0000+0		0.0000+0	1.4494-2
6.0000-8	0.5000+0	0.4000+0							0.2500+0	0.0000+0		0.0000+0	1.4520-2
8.0000-8	0.2500+0	0.2000+0							0.1250+0	0.0000+0		0.0000+0	1.4546-2
1.0000-9	0.1250+0	0.1000+0							0.0625+0	0.0000+0		0.0000+0	1.4572-2
1.5000-9	0.0625+0	0.0500+0							0.0312+0	0.0000+0		0.0000+0	1.4598-2
2.0000-9	0.0312+0	0.0250+0							0.0156+0	0.0000+0		0.0000+0	1.4624-2
3.0000-9	0.0156+0	0.0125+0							0.0078+0	0.0000+0		0.0000+0	1.4650-2
4.0000-9	0.0078+0	0.0062+0							0.0039+0	0.0000+0		0.0000+0	1.4676-2
5.0000-9	0.0039+0	0.0031+0							0.0019+0	0.0000+0		0.0000+0	1.4702-2
6.0000-9	0.0019+0	0.0015+0							0.0009+0	0.0000+0		0.0000+	

CROSS SECTION

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MATERIAL -2261	ENERGY	TOTAL	ELASTIC	INELR	(N.2N)	(N.3N)	FIBSION	(N.MR)	(N.NP)	CAPTURE	(M.P)	(N.D)	(N.A)	MU-BRE
1.0000	5 ~ 1.0000	7.1643+ 0	4.9283- 1							6.8714+ 0	0.0000+ 0		0.0000+ 0	1.3022- 2
1.0000	2 ~ 1.5000	3.6504+ 0	4.9283- 1							2.0875+ 0	0.0000+ 0		0.0000+ 0	1.3048- 2
1.0000	3 ~ 2.0000	3.0840+ 0	4.9283- 1							2.6044+ 0	0.0000+ 0		0.0000+ 0	1.3068- 2
1.0000	4 ~ 2.5000	2.9384+ 0	4.9283- 1							1.8474+ 0	0.0000+ 0		0.0000+ 0	1.3122- 2
1.0000	5 ~ 3.0000	2.1233+ 0	4.9284- 1							1.4688+ 0	0.0000+ 0		0.0000+ 0	1.3136- 2
1.0000	6 ~ 3.5000	1.8619+ 0	4.9284- 1							1.3034+ 0	0.0000+ 0		0.0000+ 0	1.3156- 2
1.0000	7 ~ 4.0000	1.7953+ 0	4.9285- 1							1.1510+ 0	0.0000+ 0		0.0000+ 0	1.3176- 2
1.0000	8 ~ 4.5000	1.8440+ 0	4.9285- 1							0.9761+ 0	0.0000+ 0		0.0000+ 0	1.3201- 2
1.0000	9 ~ 5.0000	1.4711+ 0	4.9296- 1							0.8398- 1	0.0000+ 0		0.0000+ 0	1.3226- 2
1.0000	10 ~ 5.5000	1.3163+ 0	4.9297- 1							0.7519- 1	0.0000+ 0		0.0000+ 0	1.3255- 2
1.0000	11 ~ 6.0000	1.1948+ 0	4.9289- 1							0.6823- 1	0.0000+ 0		0.0000+ 0	1.3282- 2
1.0000	12 ~ 6.5000	1.1007+ 0	4.9304- 1							0.6145- 1	0.0000+ 0		0.0000+ 0	1.3301- 2
1.0000	13 ~ 7.0000	0.9742+ 0	4.9306- 1							0.5436- 1	0.0000+ 0		0.0000+ 0	1.3336- 2
1.0000	14 ~ 7.5000	0.8530+ 0	4.9309- 1							0.4730- 1	0.0000+ 0		0.0000+ 0	1.3365- 2
1.0000	15 ~ 8.0000	0.7568+ 0	4.9314- 1							0.4036- 1	0.0000+ 0		0.0000+ 0	1.3395- 2
1.0000	16 ~ 8.5000	0.6824+ 0	4.9323- 1							0.3392- 1	0.0000+ 0		0.0000+ 0	1.3431- 2
1.0000	17 ~ 9.0000	0.6245+ 0	4.9335- 1							0.2812- 1	0.0000+ 0		0.0000+ 0	1.3476- 2
1.0000	18 ~ 9.5000	0.5722+ 0	4.9353- 1							0.2297- 1	0.0000+ 0		0.0000+ 0	1.3481- 2
1.0000	19 ~ 10.0000	0.5255+ 0	4.9376- 1							0.1824- 1	0.0000+ 0		0.0000+ 0	1.3481- 2
1.0000	20 ~ 10.5000	0.4837+ 0	4.9401- 1							0.1398- 1	0.0000+ 0		0.0000+ 0	1.3481- 2
1.0000	21 ~ 11.0000	0.4460+ 0	4.9430- 1							0.1019- 1	0.0000+ 0		0.0000+ 0	1.3481- 2
1.0000	22 ~ 11.5000	0.4125+ 0	4.9468- 1							0.0692- 1	0.0000+ 0		0.0000+ 0	1.3481- 2
1.0000	23 ~ 12.0000	0.3831+ 0	4.9522- 1							0.0398- 1	0.0000+ 0		0.0000+ 0	1.3580- 2
1.0000	24 ~ 12.5000	0.3578+ 0	4.9581- 1							0.0198- 1	0.0000+ 0		0.0000+ 0	1.3611- 2
1.0000	25 ~ 13.0000	0.3356+ 0	4.9642- 1							0.0094- 1	0.0000+ 0		0.0000+ 0	1.3656- 2
1.0000	26 ~ 13.5000	0.3163+ 0	4.9707- 1							0.0049- 1	0.0000+ 0		0.0000+ 0	1.3711- 2
1.0000	27 ~ 14.0000	0.2997+ 0	4.9776- 1							0.0026- 1	0.0000+ 0		0.0000+ 0	1.3776- 2
1.0000	28 ~ 14.5000	0.2855+ 0	4.9848- 1							0.0014- 1	0.0000+ 0		0.0000+ 0	1.3844- 2
1.0000	29 ~ 15.0000	0.2734+ 0	4.9922- 1							0.0007- 1	0.0000+ 0		0.0000+ 0	1.3911- 2
1.0000	30 ~ 15.5000	0.2631+ 0	5.0000+ 1							0.0004- 1	0.0000+ 0		0.0000+ 0	1.3984- 2
1.0000	31 ~ 16.0000	0.2544+ 0	5.0000+ 1							0.0002- 1	0.0000+ 0		0.0000+ 0	1.4061- 2
1.0000	32 ~ 16.5000	0.2472+ 0	5.0000+ 1							0.0001- 1	0.0000+ 0		0.0000+ 0	1.4141- 2
1.0000	33 ~ 17.0000	0.2413+ 0	5.0000+ 1							0.0000- 1	0.0000+ 0		0.0000+ 0	1.4224- 2
1.0000	34 ~ 17.5000	0.2364+ 0	5.0000+ 1							0.0000- 1	0.0000+ 0		0.0000+ 0	1.4309- 2
1.0000	35 ~ 18.0000	0.2323+ 0	5.0000+ 1							0.0000- 1	0.0000+ 0		0.0000+ 0	1.4396- 2
1.0000	36 ~ 18.5000	0.2289+ 0	5.0000+ 1							0.0000- 1	0.0000+ 0		0.0000+ 0	1.4483- 2
1.0000	37 ~ 19.0000	0.2261+ 0	5.0000+ 1							0.0000- 1	0.0000+ 0		0.0000+ 0	1.4571- 2
1.0000	38 ~ 19.5000	0.2238+ 0	5.0000+ 1							0.0000- 1	0.0000+ 0		0.0000+ 0	1.4660- 2
1.0000	39 ~ 20.0000	0.2220+ 0	5.0000+ 1							0.0000- 1	0.0000+ 0		0.0000+ 0	1.4750- 2
1.0000	40 ~ 20.5000	0.2206+ 0	5.0000+ 1							0.0000- 1	0.0000+ 0		0.0000+ 0	1.4841- 2
1.0000	41 ~ 21.0000	0.2195+ 0	5.0000+ 1							0.0000- 1	0.0000+ 0		0.0000+ 0	1.4933- 2
1.0000	42 ~ 21.5000	0.2187+ 0	5.0000+ 1							0.0000- 1	0.0000+ 0		0.0000+ 0	1.5026- 2
1.0000	43 ~ 22.0000	0.2181+ 0	5.0000+ 1							0.0000- 1	0.0000+ 0		0.0000+ 0	1.5120- 2
1.0000	44 ~ 22.5000	0.2177+ 0	5.0000+ 1							0.0000- 1	0.0000+ 0		0.0000+ 0	1.5215- 2
1.0000	45 ~ 23.0000	0.2174+ 0	5.0000+ 1							0.0000- 1	0.0000+ 0		0.0000+ 0	1.5311- 2
1.0000	46 ~ 23.5000	0.2172+ 0	5.0000+ 1							0.0000- 1	0.0000+ 0		0.0000+ 0	1.5408- 2
1.0000	47 ~ 24.0000	0.2171+ 0	5.0000+ 1							0.0000- 1	0.0000+ 0		0.0000+ 0	1.5506- 2
1.0000	48 ~ 24.5000	0.2170+ 0	5.0000+ 1							0.0000- 1	0.0000+ 0		0.0000+ 0	1.5605- 2
1.0000	49 ~ 25.0000	0.2169+ 0	5.0000+ 1							0.0000- 1	0.0000+ 0		0.0000+ 0	1.5705- 2
1.0000	50 ~ 25.5000	0.2168+ 0	5.0000+ 1							0.0000- 1	0.0000+ 0		0.0000+ 0	1.5806- 2
1.0000	51 ~ 26.0000	0.2167+ 0	5.0000+ 1							0.0000- 1	0.0000+ 0		0.0000+ 0	1.5908- 2
1.0000	52 ~ 26.5000	0.2166+ 0	5.0000+ 1							0.0000- 1	0.0000+ 0		0.0000+ 0	1.6011- 2
1.0000	53 ~ 27.0000	0.2165+ 0	5.0000+ 1							0.0000- 1	0.0000+ 0		0.0000+ 0	1.6115- 2
1.0000	54 ~ 27.5000	0.2164+ 0	5.0000+ 1							0.0000- 1	0.0000+ 0		0.0000+ 0	1.6220- 2
1.0000	55 ~ 28.0000	0.2163+ 0	5.0000+ 1							0.0000- 1	0.0000+ 0		0.0000+ 0	1.6326- 2
1.0000	56 ~ 28.5000	0.2162+ 0	5.0000+ 1							0.0000- 1	0.0000+ 0		0.0000+ 0	1.6433- 2
1.0000	57 ~ 29.0000	0.2161+ 0	5.0000+ 1							0.0000- 1	0.0000+ 0		0.0000+ 0	1.6541- 2
1.0000	58 ~ 29.5000	0.2160+ 0	5.0000+ 1							0.0000- 1	0.0000+ 0		0.0000+ 0	1.6650- 2
1.0000	59 ~ 30.0000	0.2159+ 0	5.0000+ 1							0.0000- 1	0.0000+ 0		0.0000+ 0	1.6760- 2
1.0000	60 ~ 30.5000	0.2158+ 0	5.0000+ 1							0.0000- 1	0.0000+ 0		0.0000+ 0	1.6871- 2
1.0000	61 ~ 31.0000	0.2157+ 0	5.0000+ 1							0.0000- 1	0.0000+ 0		0.0000+ 0	1.6983- 2
1.0000	62 ~ 31.5000	0.2156+ 0	5.0000+ 1							0.0000- 1	0.0000+ 0		0.0000+ 0	1.7096- 2
1.0000	63 ~ 32.0000	0.2155+ 0	5.0000+ 1							0.0000- 1	0.0000+ 0		0.0000+ 0	1.7210- 2
1.0000	64 ~ 32.5000	0.2154+ 0	5.0000+ 1							0.0000- 1	0.0000+ 0		0.0000+ 0	1.7325- 2
1.0000	65 ~ 33.0000	0.2153+ 0	5.0000+ 1							0.0000- 1	0.0000+ 0		0.0000+ 0	1.7441- 2
1.0000	66 ~ 33.5000	0.2152+ 0	5.0000+ 1							0.0000- 1	0.0000+ 0		0.0000+ 0	1.7558- 2
1.0000	67 ~ 34.0000	0.2151+ 0	5.0000+ 1							0.0000- 1	0.0000+ 0		0.0000+ 0	1.7676- 2
1.0000	68 ~ 34.5000	0.2150+ 0	5.0000+ 1							0.0000- 1	0.0000+ 0		0.0000+ 0	1.7795- 2
1.0000	69 ~ 35.0000	0.2149+ 0	5.0000+ 1							0.0000- 1	0.0000+ 0		0.0000+ 0	1.7915- 2
1.0000	70 ~ 35.5000	0.2148+ 0	5.0000+ 1							0.0000- 1	0.0000+ 0		0.0000+ 0	1.8036- 2
1.0000	71 ~ 36.0000	0.2147+ 0	5.0000+ 1							0.0000- 1	0.0000+ 0		0.0000+ 0	1.8158- 2
1.0000	72 ~ 36.5000	0.2146+ 0	5.0000+ 1							0.0000- 1	0.0000+ 0		0.0000+ 0	1.8281- 2
1.0000	73 ~ 37.0000	0.2145+ 0	5.0000+ 1							0.0000- 1	0.0000+ 0		0.0000+ 0	1.8405- 2
1.0000	74 ~ 37.5000	0.2144+ 0	5.0000+ 1							0.0000- 1	0.0000+ 0		0.0000+ 0	1.8530- 2
1.0000	75 ~ 38.0000	0.2143+ 0	5.0000+ 1							0.0000- 1	0.0000+ 0		0.0000+ 0	1.8656- 2
1.0000	76 ~ 38.5000	0.2142+ 0	5.0000+ 1											

CROSS SECTION

FE-66

MATERIAL = 2282	ENERGY	TOTAL	ELASTIC	INELR	(N,2N)	(N,3N)	FISSION	(N,NA)	(N,NP)	CAPTURE	(N,P)	(N,D)	(N,R)	MU-BAR
1.0000-5	1.0000-2	2.1163+1	1.2458+1						8.7053+0	0.0000+0			0.0000+0	1.6366-2
1.5000-5	1.5000-2	1.6500+1	1.2458+1						4.0408+0	0.0000+0			0.0000+0	1.7281-2
2.0000-5	2.0000-2	1.5877+1	1.2458+1						2.2650+0	0.0000+0			0.0000+0	1.7532-2
3.0000-5	3.0000-2	1.5319+1	1.2458+1						2.4078+0	0.0000+0			0.0000+0	1.7792-2
4.0000-5	4.0000-2	1.4867+1	1.2458+1						2.1172+0	0.0000+0			0.0000+0	1.8043-2
5.0000-5	5.0000-2	1.4516+1	1.2458+1						1.9123+0	0.0000+0			0.0000+0	1.8293-2
6.0000-5	6.0000-2	1.4160+1	1.2458+1						1.7275+0	0.0000+0			0.0000+0	1.8543-2
8.0000-5	1.0000-1	1.3956+1	1.2458+1						1.4375+0	0.0000+0			0.0000+0	1.8794-2
1.0000-1	1.5000-1	1.3788+1	1.2458+1						1.2788+0	0.0000+0			0.0000+0	1.8880-2
1.5000-1	2.0000-1	1.3620+1	1.2458+1						1.0748+0	0.0000+0			0.0000+0	1.9131-2
2.0000-1	3.0000-1	1.3217+1	1.2457+1						9.0015+0	0.0000+0			0.0000+0	1.9382-2
3.0000-1	4.0000-1	1.3177+1	1.2457+1						6.6972+0	0.0000+0			0.0000+0	1.9633-2
4.0000-1	5.0000-1	1.3062+1	1.2456+1						6.0827+0	0.0000+0			0.0000+0	1.9884-2
5.0000-1	6.0000-1	1.2993+1	1.2455+1						5.3719+0	0.0000+0			0.0000+0	2.0135-2
6.0000-1	1.0000-0	1.2928+1	1.2454+1						4.7389+0	0.0000+0			0.0000+0	2.0386-2
1.0000-0	2.0000-0	1.2855+1	1.2452+1						4.0305+0	0.0000+0			0.0000+0	2.0637-2
1.5000-0	3.0000-0	1.2789+1	1.2449+1						3.3381+0	0.0000+0			0.0000+0	2.0888-2
2.0000-0	4.0000-0	1.2730+1	1.2445+1						2.6465+0	0.0000+0			0.0000+0	2.1139-2
3.0000-0	5.0000-0	1.2675+1	1.2441+1						2.3592+0	0.0000+0			0.0000+0	2.1390-2
4.0000-0	6.0000-0	1.2624+1	1.2437+1						2.1113+0	0.0000+0			0.0000+0	2.1641-2
5.0000-0	1.0000-0	1.2578+1	1.2432+1						1.8910+0	0.0000+0			0.0000+0	2.1892-2
6.0000-0	2.0000-0	1.2535+1	1.2428+1						1.6910+0	0.0000+0			0.0000+0	2.2143-2
1.0000+1	1.5000+1	1.2494+1	1.2419+1						1.4884+0	0.0000+0			0.0000+0	2.2394-2
1.5000+1	2.0000+1	1.2456+1	1.2388+1						1.2894+0	0.0000+0			0.0000+0	2.2645-2
2.0000+1	3.0000+1	1.2408+1	1.2350+1						1.0852+0	0.0000+0			0.0000+0	2.2896-2
3.0000+1	4.0000+1	1.2339+1	1.2318+1						7.3674+0	0.0000+0			0.0000+0	2.3147-2
4.0000+1	5.0000+1	1.2272+1	1.2283+1						6.4168+0	0.0000+0			0.0000+0	2.3398-2
5.0000+1	6.0000+1	1.2215+1	1.2249+1						5.5042+0	0.0000+0			0.0000+0	2.3649-2
6.0000+1	1.0000+0	1.2158+1	1.2214+1						4.6315+0	0.0000+0			0.0000+0	2.3900-2
8.0000+1	1.0000+2	1.2103+1	1.2170+1						3.8015+0	0.0000+0			0.0000+0	2.4151-2
1.0000+2	2.0000+2	1.1930+1	1.1784+1						3.0978+0	0.0000+0			0.0000+0	2.4402-2
1.5000+2	3.0000+2	1.1830+1	1.1593+1						2.4961+0	0.0000+0			0.0000+0	2.4653-2
2.0000+2	4.0000+2	1.1750+1	1.1408+1						2.0000+0	0.0000+0			0.0000+0	2.4904-2
3.0000+2	5.0000+2	1.1682+1	1.1230+1						1.6050+0	0.0000+0			0.0000+0	2.5155-2
4.0000+2	6.0000+2	1.1624+1	1.1061+1						1.2709+0	0.0000+0			0.0000+0	2.5406-2
5.0000+2	1.0000+3	1.1574+1	1.0907+1						9.6943+0	0.0000+0			0.0000+0	2.5657-2
6.0000+2	2.0000+3	1.1532+1	1.0759+1						8.7815+0	0.0000+0			0.0000+0	2.5908-2
8.0000+2	3.0000+3	1.1497+1	1.0616+1						7.9235+0	0.0000+0			0.0000+0	2.6159-2
1.0000+3	4.0000+3	1.1468+1	1.0478+1						7.1200+0	0.0000+0			0.0000+0	2.6410-2
1.5000+3	5.0000+3	1.1443+1	1.0344+1						6.3729+0	0.0000+0			0.0000+0	2.6661-2
2.0000+3	6.0000+3	1.1422+1	1.0214+1						5.6807+0	0.0000+0			0.0000+0	2.6912-2
3.0000+3	1.0000+4	1.1404+1	1.0087+1						5.0428+0	0.0000+0			0.0000+0	2.7163-2
4.0000+3	2.0000+4	1.1389+1	9.9643+0						4.4589+0	0.0000+0			0.0000+0	2.7414-2
5.0000+3	3.0000+4	1.1376+1	9.9519+0						3.9293+0	0.0000+0			0.0000+0	2.7665-2
6.0000+3	4.0000+4	1.1364+1	9.9400+0						3.4500+0	0.0000+0			0.0000+0	2.7916-2
8.0000+3	5.0000+4	1.1353+1	9.9286+0						3.0116+0	0.0000+0			0.0000+0	2.8167-2
1.0000+4	6.0000+4	1.1343+1	9.9176+0						2.6125+0	0.0000+0			0.0000+0	2.8418-2
1.5000+4	1.0000+5	1.1334+1	9.9070+0						2.2531+0	0.0000+0			0.0000+0	2.8669-2
2.0000+4	2.0000+5	1.1326+1	9.8967+0						1.9331+0	0.0000+0			0.0000+0	2.8920-2
3.0000+4	3.0000+5	1.1318+1	9.8867+0						1.6529+0	0.0000+0			0.0000+0	2.9171-2
4.0000+4	4.0000+5	1.1311+1	9.8769+0						1.4127+0	0.0000+0			0.0000+0	2.9422-2
5.0000+4	5.0000+5	1.1304+1	9.8673+0						1.2023+0	0.0000+0			0.0000+0	2.9673-2
6.0000+4	6.0000+5	1.1297+1	9.8579+0						1.0213+0	0.0000+0			0.0000+0	2.9924-2
8.0000+4	7.0000+5	1.1290+1	9.8486+0						0.8693+0	0.0000+0			0.0000+0	3.0175-2
1.0000+5	8.0000+5	1.1283+1	9.8394+0						0.7358+0	0.0000+0			0.0000+0	3.0426-2
1.5000+5	1.0000+6	1.1276+1	9.8303+0						0.6116+0	0.0000+0			0.0000+0	3.0677-2
2.0000+5	2.0000+6	1.1269+1	9.8213+0						0.5000+0	0.0000+0			0.0000+0	3.0928-2
3.0000+5	3.0000+6	1.1262+1	9.8124+0						0.4000+0	0.0000+0			0.0000+0	3.1179-2
4.0000+5	4.0000+6	1.1255+1	9.8035+0						0.3116+0	0.0000+0			0.0000+0	3.1430-2
5.0000+5	5.0000+6	1.1248+1	9.7946+0						0.2331+0	0.0000+0			0.0000+0	3.1681-2
6.0000+5	6.0000+6	1.1241+1	9.7857+0						0.1645+0	0.0000+0			0.0000+0	3.1932-2
8.0000+5	7.0000+6	1.1234+1	9.7768+0						0.1059+0	0.0000+0			0.0000+0	3.2183-2
1.0000+6	8.0000+6	1.1227+1	9.7679+0						0.0573+0	0.0000+0			0.0000+0	3.2434-2
1.5000+6	1.0000+7	1.1220+1	9.7590+0						0.0187+0	0.0000+0			0.0000+0	3.2685-2
2.0000+6	2.0000+7	1.1213+1	9.7501+0						0.0000+0	0.0000+0			0.0000+0	3.2936-2
3.0000+6	3.0000+7	1.1206+1	9.7412+0						0.0000+0	0.0000+0			0.0000+0	3.3187-2
4.0000+6	4.0000+7	1.1199+1	9.7323+0						0.0000+0	0.0000+0			0.0000+0	3.3438-2
5.0000+6	5.0000+7	1.1192+1	9.7234+0						0.0000+0	0.0000+0			0.0000+0	3.3689-2
6.0000+6	6.0000+7	1.1185+1	9.7145+0						0.0000+0	0.0000+0			0.0000+0	3.3940-2
8.0000+6	7.0000+7	1.1178+1	9.7056+0						0.0000+0	0.0000+0			0.0000+0	3.4191-2
1.0000+7	8.0000+7	1.1171+1	9.6967+0						0.0000+0	0.0000+0			0.0000+0	3.4442-2
1.5000+7	1.0000+8	1.1164+1	9.6878+0						0.0000+0	0.0000+0			0.0000+0	3.4693-2
2.0000+7	2.0000+8	1.1157+1	9.6789+0						0.0000+0	0.0000+0			0.0000+0	3.4944-2
3.0000+7	3.0000+8	1.1150+1	9.6700+0						0.0000+0	0.0000+0			0.0000+0	3.5195-2
4.0000+7	4.0000+8	1.1143+1	9.6611+0						0.0000+0	0.0000+0			0.0000+0	3.5446-2
5.0000+7	5.0000+8	1.1136+1	9.6522+0						0.0000+0	0.0000+0			0.0000+0	3.5697-2
6.0000+7	6.0000+8	1.1129+1	9.6433+0						0.0000+0	0.0000+0			0.0000+0	3.5948-2
8.0000+7	7.0000+8	1.1122+1	9.6344+0						0.0000+0	0.0000+0			0.0000+0	3.6199-2
1.0000+8	8.0000+8	1.1115+1	9.6255+											

FE-57

CROSS SECTION

MATERIAL =2283

ENERGY	TOTAL	ELASTIC	INEL	(N,2N)	(N,3N)	Fission	(N,NB)	(N,NP)	CAPTURE	(N,P)	(N,D)	(N,R)	MU-BAR
1.0000- 5 ~ 1.0000- 2	7.8217+ 0	2.0211- 1							7.6196+ 0				1.2698- 2
1.0000- 2 ~ 1.0000- 1	3.7398+ 0	2.0211- 1							3.5377+ 0				1.5890- 1
1.0000- 1 ~ 1.0000- 0	3.1787+ 0	2.0211- 1							2.9149+ 0				1.2981- 1
2.0000- 2 ~ 2.0000- 1	2.7043+ 0	2.0210- 1							2.1033+ 0				1.3036- 1
3.0000- 2 ~ 3.0000- 1	2.3088+ 0	2.0210- 1							1.8599+ 0				1.3073- 1
4.0000- 2 ~ 4.0000- 1	2.0823+ 0	2.0210- 1							1.6774+ 0				1.3102- 1
5.0000- 2 ~ 5.0000- 1	1.8945+ 0	2.0210- 1							1.4974+ 0				1.3177- 1
6.0000- 2 ~ 6.0000- 1	1.7182+ 0	2.0210- 1							1.3151+ 0				1.3277- 1
7.0000- 2 ~ 7.0000- 1	1.5194+ 0	2.0209- 1							1.1193+ 0				1.3377- 1
8.0000- 2 ~ 8.0000- 1	1.3194+ 0	2.0209- 1							9.4195- 1				1.3477- 1
9.0000- 2 ~ 9.0000- 1	1.1194+ 0	2.0207- 1							7.8945- 1				1.3577- 1
1.0000- 1 ~ 1.0000- 0	9.9752+ 0	2.0207- 1							6.3690- 1				1.3677- 1
2.0000- 1 ~ 2.0000- 0	8.6781+ 0	2.0206- 1							4.8434- 1				1.3777- 1
3.0000- 1 ~ 3.0000- 0	7.4893+ 0	2.0204- 1							3.3179- 1				1.3877- 1
4.0000- 1 ~ 4.0000- 0	6.3203+ 0	2.0203- 1							1.7925- 1				1.3977- 1
5.0000- 1 ~ 5.0000- 0	5.1723+ 0	2.0203- 1							2.2619- 1				1.4077- 1
6.0000- 1 ~ 6.0000- 0	4.0243+ 0	2.0199- 1							1.7461- 1				1.4177- 1
7.0000- 1 ~ 7.0000- 0	2.8763+ 0	2.0198- 1							1.2297- 1				1.4277- 1
8.0000- 1 ~ 8.0000- 0	1.7283+ 0	2.0198- 1							6.7259- 1				1.4377- 1
9.0000- 1 ~ 9.0000- 0	5.5517- 1	2.0193- 1							3.2394- 1				1.4477- 1
1.0000+ 0 ~ 1.5000+ 0	4.5160+ 0	2.0188- 1							2.7095- 1				1.4577- 1
2.0000+ 0 ~ 2.5000+ 0	3.4698+ 0	2.0179- 1							2.1796- 1				1.4677- 1
3.0000+ 0 ~ 3.5000+ 0	2.4236+ 0	2.0174- 1							1.6497- 1				1.4777- 1
4.0000+ 0 ~ 4.5000+ 0	1.3774+ 0	2.0174- 1							1.1198- 1				1.4877- 1
5.0000+ 0 ~ 5.5000+ 0	3.8307- 1	2.0168- 1							6.2008- 1				1.4977- 1
6.0000+ 0 ~ 6.5000+ 0	3.1328+ 0	2.0036- 1							5.5036- 1				1.5077- 1
7.0000+ 0 ~ 7.5000+ 0	2.4349+ 0	1.9966- 1							4.8064- 1				1.5177- 1
8.0000+ 0 ~ 8.5000+ 0	1.7370+ 0	1.9861- 1							4.1092- 1				1.5277- 1
9.0000+ 0 ~ 9.5000+ 0	1.0391+ 0	1.9721- 1							3.4120- 1				1.5377- 1
1.0000+ 1 ~ 1.5000+ 1	2.5480+ 0	1.9681- 1							2.7148- 1				1.5477- 1
2.0000+ 1 ~ 2.5000+ 1	2.0502+ 0	1.9531- 1							2.0176- 1				1.5577- 1
3.0000+ 1 ~ 3.5000+ 1	1.5524+ 0	1.9382- 1							1.3204- 1				1.5677- 1
4.0000+ 1 ~ 4.5000+ 1	1.0546+ 0	1.9233- 1							6.6205- 1				1.5777- 1
5.0000+ 1 ~ 5.5000+ 1	5.3144- 1	1.8952- 1							5.9233- 1				1.5877- 1
6.0000+ 1 ~ 6.5000+ 1	4.6166- 1	1.8671- 1							5.2261- 1				1.5977- 1
7.0000+ 1 ~ 7.5000+ 1	3.9188- 1	1.8390- 1							4.5289- 1				1.6077- 1
8.0000+ 1 ~ 8.5000+ 1	3.2210- 1	1.8109- 1							3.8317- 1				1.6177- 1
9.0000+ 1 ~ 9.5000+ 1	2.5232- 1	1.7828- 1							3.1345- 1				1.6277- 1
1.0000+ 2 ~ 1.5000+ 2	1.8254- 1	1.7547- 1							2.4373- 1				1.6377- 1
2.0000+ 2 ~ 2.5000+ 2	1.1276- 1	1.7266- 1							1.7401- 1				1.6477- 1
3.0000+ 2 ~ 3.5000+ 2	4.6195- 2	1.6985- 1							1.0429- 1				1.6577- 1
4.0000+ 2 ~ 4.5000+ 2	3.9217- 2	1.6704- 1							3.4778- 2				1.6677- 1
5.0000+ 2 ~ 5.5000+ 2	3.2239- 2	1.6423- 1							2.7800- 2				1.6777- 1
6.0000+ 2 ~ 6.5000+ 2	2.5261- 2	1.6142- 1							2.0822- 2				1.6877- 1
7.0000+ 2 ~ 7.5000+ 2	1.8283- 2	1.5861- 1							1.3844- 2				1.6977- 1
8.0000+ 2 ~ 8.5000+ 2	1.1305- 2	1.5580- 1							6.6873+ 0				1.7077- 1
9.0000+ 2 ~ 9.5000+ 2	4.5554+ 0	1.5300- 1							5.9901+ 0				1.7177- 1
1.0000+ 3 ~ 1.5000+ 3	3.8576+ 0	1.5020- 1							5.2923+ 0				1.7277- 1
2.0000+ 3 ~ 2.5000+ 3	3.1598+ 0	1.4740- 1							4.5945+ 0				1.7377- 1
3.0000+ 3 ~ 3.5000+ 3	2.4620+ 0	1.4460- 1							3.8967+ 0				1.7477- 1
4.0000+ 3 ~ 4.5000+ 3	1.7642+ 0	1.4180- 1							3.1989+ 0				1.7577- 1
5.0000+ 3 ~ 5.5000+ 3	1.0664+ 0	1.3900- 1							2.5011+ 0				1.7677- 1
6.0000+ 3 ~ 6.5000+ 3	3.9630+ 0	1.3620- 1							1.8033+ 0				1.7777- 1
7.0000+ 3 ~ 7.5000+ 3	3.2652+ 0	1.3340- 1							1.1055+ 0				1.7877- 1
8.0000+ 3 ~ 8.5000+ 3	2.5674+ 0	1.3060- 1							4.4014- 1				1.7977- 1
9.0000+ 3 ~ 9.5000+ 3	1.8696+ 0	1.2780- 1							3.7036- 1				1.8077- 1
1.0000+ 4 ~ 1.5000+ 4	1.1718+ 0	1.2500- 1							3.0058- 1				1.8177- 1
2.0000+ 4 ~ 2.5000+ 4	4.6195+ 0	1.2220- 1							2.3080- 1				1.8277- 1
3.0000+ 4 ~ 3.5000+ 4	3.9217+ 0	1.1940- 1							1.6102- 1				1.8377- 1
4.0000+ 4 ~ 4.5000+ 4	3.2239+ 0	1.1660- 1							9.5492- 2				1.8477- 1
5.0000+ 4 ~ 5.5000+ 4	2.5261+ 0	1.1380- 1							8.8514- 2				1.8577- 1
6.0000+ 4 ~ 6.5000+ 4	1.8283+ 0	1.1100- 1							8.1536- 2				1.8677- 1
7.0000+ 4 ~ 7.5000+ 4	1.1305+ 0	1.0820- 1							7.4558- 2				1.8777- 1
8.0000+ 4 ~ 8.5000+ 4	4.5554+ 0	1.0540- 1							6.7580- 2				1.8877- 1
9.0000+ 4 ~ 9.5000+ 4	3.8576+ 0	1.0260- 1							6.0602- 2				1.8977- 1
1.0000+ 5 ~ 1.5000+ 5	3.1598+ 0	1.0000- 1							5.3624- 2				1.9077- 1
2.0000+ 5 ~ 2.5000+ 5	2.4620+ 0	1.0000- 1							4.6646- 2				1.9177- 1
3.0000+ 5 ~ 3.5000+ 5	1.7642+ 0	1.0000- 1							3.9668- 2				1.9277- 1
4.0000+ 5 ~ 4.5000+ 5	1.0664+ 0	1.0000- 1							3.2690- 2				1.9377- 1
5.0000+ 5 ~ 5.5000+ 5	3.9630+ 0	1.0000- 1							2.5712- 2				1.9477- 1
6.0000+ 5 ~ 6.5000+ 5	3.2652+ 0	1.0000- 1							1.8734- 2				1.9577- 1
7.0000+ 5 ~ 7.5000+ 5	2.5674+ 0	1.0000- 1							1.1756- 2				1.9677- 1
8.0000+ 5 ~ 8.5000+ 5	1.8696+ 0	1.0000- 1							4.7081- 2				1.9777- 1
9.0000+ 5 ~ 9.5000+ 5	1.1718+ 0	1.0000- 1							4.0103- 2				1.9877- 1
1.0000+ 6 ~ 1.5000+ 6	4.6195+ 0	1.0000- 1							3.3125- 2				1.9977- 1
2.0000+ 6 ~ 2.5000+ 6	3.9217+ 0	1.0000- 1							2.6147- 2				2.0077- 1
3.0000+ 6 ~ 3.5000+ 6	3.2239+ 0	1.0000- 1							1.9169- 2				2.0177- 1
4.0000+ 6 ~ 4.5000+ 6	2.5261+ 0	1.0000- 1							1.2191- 2				2.0277- 1
5.0000+ 6 ~ 5.5000+ 6	1.8283+ 0	1.0000- 1							5.9711- 2				2.0377- 1
6.0000+ 6 ~ 6.5000+ 6	1.1305+ 0	1.0000- 1							5.2733- 2				2.0477- 1
7.0000+ 6 ~ 7.5000+ 6	4.5554+ 0	1.0000- 1							4.5755- 2				2.0577- 1
8.0000+ 6 ~ 8.5000+ 6	3.8576+ 0	1.0000- 1							3.8777- 2				2.0677- 1
9.0000+ 6 ~ 9.5000+ 6	3.1598+ 0	1.0000- 1							3.1799- 2				2.0777- 1
1.0000+ 7 ~ 1.5000+ 7	2.4620+ 0	1.0000- 1							2.4821- 2				2.0877- 1
2.0000+ 7 ~ 2.5000+ 7	1.7642+ 0	1.0000- 1							1.7843- 2				2.0977- 1
3.0000+ 7 ~ 3.5000+ 7	1.0664+ 0	1.0000- 1							1.0865- 2				2.1077- 1
4.0000+ 7 ~ 4.5000+ 7	3.9630+ 0	1.0000- 1							3.5801- 2				2.1177- 1
5.0000+ 7 ~ 5.5000+ 7	3												

CROSS SECTION

MI-56

MATERIAL	ENERGY	TOTAL	ELASTIC	INELA	(N.2N)	(N.3N)	FIBRATION	(N.NR)	(N.WP)	CAPTURE	(N.P)	(N.D)	(N.A)	RU-BRR
1.0000	5.0000	4.0266	2.6019							1.4248	0.0000		8.4830	1.1607
1.0000	2.0000	3.2635	2.6019							5.6186	0.0000		1.7488	1.1607
1.0000	1.5000	3.1562	2.6019							5.5223	0.0000		2.4488	1.1607
1.0000	1.0000	3.0489	2.6019							5.4366	0.0000		3.1488	1.1607
1.0000	0.5000	2.9416	2.6019							5.3504	0.0000		3.8488	1.1607
1.0000	0.2000	2.8343	2.6019							5.2642	0.0000		4.5488	1.1607
1.0000	0.1000	2.7270	2.6019							5.1780	0.0000		5.2488	1.1607
1.0000	0.0500	2.6197	2.6019							5.0918	0.0000		5.9488	1.1607
1.0000	0.0200	2.5124	2.6019							5.0056	0.0000		6.6488	1.1607
1.0000	0.0100	2.4051	2.6019							4.9194	0.0000		7.3488	1.1607
1.0000	0.0050	2.2978	2.6019							4.8332	0.0000		8.0488	1.1607
1.0000	0.0020	2.1905	2.6019							4.7470	0.0000		8.7488	1.1607
1.0000	0.0010	2.0832	2.6019							4.6608	0.0000		9.4488	1.1607
1.0000	0.0005	1.9759	2.6019							4.5746	0.0000		10.1488	1.1607
1.0000	0.0002	1.8686	2.6019							4.4884	0.0000		10.8488	1.1607
1.0000	0.0001	1.7613	2.6019							4.4022	0.0000		11.5488	1.1607
1.0000	0.0000	1.6540	2.6019							4.3160	0.0000		12.2488	1.1607
1.0000	0.0000	1.5467	2.6019							4.2298	0.0000		12.9488	1.1607
1.0000	0.0000	1.4394	2.6019							4.1436	0.0000		13.6488	1.1607
1.0000	0.0000	1.3321	2.6019							4.0574	0.0000		14.3488	1.1607
1.0000	0.0000	1.2248	2.6019							3.9712	0.0000		15.0488	1.1607
1.0000	0.0000	1.1175	2.6019							3.8850	0.0000		15.7488	1.1607
1.0000	0.0000	1.0102	2.6019							3.7988	0.0000		16.4488	1.1607
1.0000	0.0000	0.9029	2.6019							3.7126	0.0000		17.1488	1.1607
1.0000	0.0000	0.7956	2.6019							3.6264	0.0000		17.8488	1.1607
1.0000	0.0000	0.6883	2.6019							3.5402	0.0000		18.5488	1.1607
1.0000	0.0000	0.5810	2.6019							3.4540	0.0000		19.2488	1.1607
1.0000	0.0000	0.4737	2.6019							3.3678	0.0000		19.9488	1.1607
1.0000	0.0000	0.3664	2.6019							3.2816	0.0000		20.6488	1.1607
1.0000	0.0000	0.2591	2.6019							3.1954	0.0000		21.3488	1.1607
1.0000	0.0000	0.1518	2.6019							3.1092	0.0000		22.0488	1.1607
1.0000	0.0000	0.0445	2.6019							3.0230	0.0000		22.7488	1.1607
1.0000	0.0000	0.0000	2.6019							2.9368	0.0000		23.4488	1.1607
1.0000	0.0000	0.0000	2.6019							2.8506	0.0000		24.1488	1.1607
1.0000	0.0000	0.0000	2.6019							2.7644	0.0000		24.8488	1.1607
1.0000	0.0000	0.0000	2.6019							2.6782	0.0000		25.5488	1.1607
1.0000	0.0000	0.0000	2.6019							2.5920	0.0000		26.2488	1.1607
1.0000	0.0000	0.0000	2.6019							2.5058	0.0000		26.9488	1.1607
1.0000	0.0000	0.0000	2.6019							2.4196	0.0000		27.6488	1.1607
1.0000	0.0000	0.0000	2.6019							2.3334	0.0000		28.3488	1.1607
1.0000	0.0000	0.0000	2.6019							2.2472	0.0000		29.0488	1.1607
1.0000	0.0000	0.0000	2.6019							2.1610	0.0000		29.7488	1.1607
1.0000	0.0000	0.0000	2.6019							2.0748	0.0000		30.4488	1.1607
1.0000	0.0000	0.0000	2.6019							1.9886	0.0000		31.1488	1.1607
1.0000	0.0000	0.0000	2.6019							1.9024	0.0000		31.8488	1.1607
1.0000	0.0000	0.0000	2.6019							1.8162	0.0000		32.5488	1.1607
1.0000	0.0000	0.0000	2.6019							1.7300	0.0000		33.2488	1.1607
1.0000	0.0000	0.0000	2.6019							1.6438	0.0000		33.9488	1.1607
1.0000	0.0000	0.0000	2.6019							1.5576	0.0000		34.6488	1.1607
1.0000	0.0000	0.0000	2.6019							1.4714	0.0000		35.3488	1.1607
1.0000	0.0000	0.0000	2.6019							1.3852	0.0000		36.0488	1.1607
1.0000	0.0000	0.0000	2.6019							1.2990	0.0000		36.7488	1.1607
1.0000	0.0000	0.0000	2.6019							1.2128	0.0000		37.4488	1.1607
1.0000	0.0000	0.0000	2.6019							1.1266	0.0000		38.1488	1.1607
1.0000	0.0000	0.0000	2.6019							1.0404	0.0000		38.8488	1.1607
1.0000	0.0000	0.0000	2.6019							0.9542	0.0000		39.5488	1.1607
1.0000	0.0000	0.0000	2.6019							0.8680	0.0000		40.2488	1.1607
1.0000	0.0000	0.0000	2.6019							0.7818	0.0000		40.9488	1.1607
1.0000	0.0000	0.0000	2.6019							0.6956	0.0000		41.6488	1.1607
1.0000	0.0000	0.0000	2.6019							0.6094	0.0000		42.3488	1.1607
1.0000	0.0000	0.0000	2.6019							0.5232	0.0000		43.0488	1.1607
1.0000	0.0000	0.0000	2.6019							0.4370	0.0000		43.7488	1.1607
1.0000	0.0000	0.0000	2.6019							0.3508	0.0000		44.4488	1.1607
1.0000	0.0000	0.0000	2.6019							0.2646	0.0000		45.1488	1.1607
1.0000	0.0000	0.0000	2.6019							0.1784	0.0000		45.8488	1.1607
1.0000	0.0000	0.0000	2.6019							0.0922	0.0000		46.5488	1.1607
1.0000	0.0000	0.0000	2.6019							0.0060	0.0000		47.2488	1.1607
1.0000	0.0000	0.0000	2.6019							0.0000	0.0000		47.9488	1.1607
1.0000	0.0000	0.0000	2.6019							0.0000	0.0000		48.6488	1.1607
1.0000	0.0000	0.0000	2.6019							0.0000	0.0000		49.3488	1.1607
1.0000	0.0000	0.0000	2.6019							0.0000	0.0000		50.0488	1.1607
1.0000	0.0000	0.0000	2.6019							0.0000	0.0000		50.7488	1.1607
1.0000	0.0000	0.0000	2.6019							0.0000	0.0000		51.4488	1.1607
1.0000	0.0000	0.0000	2.6019							0.0000	0.0000		52.1488	1.1607
1.0000	0.0000	0.0000	2.6019							0.0000	0.0000		52.8488	1.1607
1.0000	0.0000	0.0000	2.6019							0.0000	0.0000		53.5488	1.1607
1.0000	0.0000	0.0000	2.6019							0.0000	0.0000		54.2488	1.1607
1.0000	0.0000	0.0000	2.6019							0.0000	0.0000		54.9488	1.1607
1.0000	0.0000	0.0000	2.6019							0.0000	0.0000		55.6488	1.1607
1.0000	0.0000	0.0000	2.6019							0.0000	0.0000		56.3488	1.1607
1.0000	0.0000	0.0000	2.6019							0.0000	0.0000		57.0488	1.1607
1.0000	0.0000	0.0000	2.6019							0.0000	0.0000		57.7488	1.1607
1.0000	0.0000	0.0000	2.6019							0.0000	0.0000		58.4488	1.1607
1.0000	0.0000	0.0000	2.6019							0.0000	0.0000		59.1488	1.1607
1.0000	0.0000	0.0000	2.6019							0.0000	0.0000		59.8488	1.1607
1.0000	0.0000	0.0000	2.6019							0.0000	0.0000		60.5488	1.1607
1.0000	0.0000	0.0000	2.6019							0.0000	0.0000		61.2488	1.1607
1.0000	0.0000	0.0000	2.											

MI-60

CROSS SECTION

MATERIAL	ENERGY	TOTAL	ELASTIC	INELR	(N,2N)	(N,3N)	FISSION	(N,NR)	(N,NP)	CAPTURE	(N,P)	(N,D)	(N,R)	MI-BRR
1.0000*	5 ~ 1.0000-2	9.6791+ 0	1.0126+ 0							6.6665+ 0			2.9970-14	1.1220-2
1.0000*	1.5000-2	5.0864+ 0	1.0126+ 0							4.0238+ 0			7.4940-14	1.1220-2
1.0000*	2.0000-2	3.8561+ 0	1.0126+ 0							2.8433+ 0			7.4940-14	1.1220-2
3.0000*	1.0000-2	3.4659+ 0	1.0126+ 0							2.4533+ 0			2.0894-13	1.1220-2
4.0000*	1.0000-2	3.1225+ 0	1.0126+ 0							2.1099+ 0			2.0894-13	1.1220-2
5.0000*	1.0000-2	2.9160+ 0	1.0126+ 0							1.9054+ 0			3.4594-13	1.1220-2
6.0000*	1.0000-2	2.7502+ 0	1.0126+ 0							1.7516+ 0			3.4594-13	1.1220-2
1.0000*	1.5000-1	2.2858+ 0	1.0126+ 0							1.2733+ 0			7.4894-13	1.1220-2
1.5000*	1.0000-1	2.0633+ 0	1.0126+ 0							1.0711+ 0			1.0499-12	1.1220-2
2.0000*	1.0000-1	1.9703+ 0	1.0126+ 0							0.9500+ 0			1.0499-12	1.1220-2
3.0000*	1.0000-1	1.6787+ 0	1.0126+ 0							0.6291+ 0			0.6291-12	1.1220-2
5.0000*	1.0000-1	1.6169+ 0	1.0126+ 0							0.5044+ 0			0.5044-12	1.1220-2
6.0000*	1.0000-1	1.5479+ 0	1.0126+ 0							0.3556+ 0			0.3556-12	1.1220-2
8.0000*	1.0000-1	1.4834+ 0	1.0126+ 0							0.4711+ 0			0.4711-12	1.1220-2
1.0000*	2.0000-0	1.4144+ 0	1.0119+ 0							0.9265+ 0			7.4899-12	1.1220-2
1.5000*	1.5000-0	1.2961+ 0	1.0118+ 0							0.8244+ 0			1.0500-11	1.1220-2
2.0000*	1.0000-0	1.2504+ 0	1.0112+ 0							2.3917+ 0			1.0500-11	1.1220-2
3.0000*	1.0000-0	1.2274+ 0	1.0104+ 0							2.1152+ 0			2.1000-11	1.1220-2
4.0000*	1.0000-0	1.2169+ 0	1.0104+ 0							1.9075+ 0			2.1000-11	1.1220-2
5.0000*	1.0000-0	1.2169+ 0	1.0098+ 0							1.7493+ 0			2.1000-11	1.1220-2
6.0000*	1.0000-0	1.1595+ 0	1.0090+ 0							1.4953+ 0			5.4000-10	1.1220-2
1.0000*	1.5000+ 1	1.1345+ 0	1.0078+ 0							1.2687+ 0			7.5000-10	1.1220-2
1.5000*	1.2000+ 1	1.0923+ 0	1.0026+ 0							1.0720+ 0			1.5000-10	1.1220-2
2.0000*	1.0000+ 1	1.0714+ 0	0.9964+ 0							0.9545+ 0			2.1000-10	1.1220-2
3.0000*	1.0000+ 1	1.0612+ 0	0.9946+ 0							0.8493+ 0			2.7000-10	1.1220-2
5.0000*	1.0000+ 1	1.0507+ 0	0.9907+ 0							0.6052+ 0			3.3000-10	1.1220-2
6.0000*	1.0000+ 1	1.0382+ 0	0.9876+ 0							5.3432+ 0			5.2000-10	1.1220-2
8.0000*	1.0000+ 2	1.0239+ 0	0.9851+ 0							4.5824+ 0			5.4000-10	1.1220-2
1.0000*	2.0000+ 2	1.0032+ 0	0.9825+ 0							3.9923+ 0			7.5000-10	1.1227-2
1.5000*	2.0000+ 2	0.97745- 1	0.94391- 1							3.9545+ 0			1.0500-9	1.1238-2
2.0000*	2.0000+ 2	0.94345- 1	0.91588- 1							2.8070+ 0			1.5000-9	1.1240-2
3.0000*	2.0000+ 2	0.92821- 1	0.84195- 1							2.7000+ 0			1.5000-9	1.1248-2
4.0000*	2.0000+ 2	0.92481- 1	0.80637- 1							2.6748+ 0			1.5000-9	1.1255-2
5.0000*	2.0000+ 2	0.91995- 1	0.75409- 1							1.6572+ 0			3.3000-9	1.1263-2
6.0000*	2.0000+ 2	0.91195- 1	0.68735- 1							1.4600+ 0			4.2000-9	1.1281-2
1.0000*	3.0000+ 2	0.8955- 1	0.7803- 1							1.653+ 0			7.5000-9	1.1380-2
1.5000*	3.0000+ 2	0.8692- 1	0.73533- 1							1.3778+ 0			1.1614+ 0	1.1614-2
2.0000*	3.0000+ 2	0.84010- 2	0.69382- 1							1.0902+ 0			1.1653+ 0	1.1653-2
3.0000*	3.0000+ 2	0.821210- 2	0.65419- 2							9.4902+ 0			1.787+ 0	1.787-2
4.0000*	3.0000+ 2	0.80981- 2	0.61952- 2							5.4278+ 0			2.7000+ 0	2.7000-2
5.0000*	3.0000+ 2	0.79981- 2	0.58981- 2							1.0055+ 0			2.4018+ 0	2.4018-2
6.0000*	3.0000+ 2	0.79153+ 0	0.56229+ 0							1.0231+ 0			2.737+ 0	2.737-2
8.0000*	4.0000+ 2	0.7855+ 0	0.54752+ 0							1.0237+ 0			3.9353+ 0	3.9353-2
1.0000*	4.0000+ 4	0.78113+ 0	0.53147+ 0							1.3940+ 0			5.4000-7	5.4000-2
1.5000*	5.0000+ 5	0.77713+ 0	0.51610+ 0							0.9806+ 0			7.5000-7	7.5000-2
2.0000*	5.0000+ 5	0.76086+ 0	0.50089+ 0							0.9398+ 0			1.0500-6	1.0500-2
3.0000*	5.0000+ 5	0.74221+ 0	0.48471+ 0							0.8145+ 0			1.5000-6	1.5000-2
4.0000*	5.0000+ 5	0.72192+ 0	0.46792+ 0							0.7000+ 0			2.7000-6	2.7000-2
5.0000*	5.0000+ 5	0.70310+ 0	0.45148+ 0							0.5937+ 0			3.4000-6	3.4000-2
6.0000*	5.0000+ 5	0.68369+ 0	0.43510+ 0							0.4839+ 0			4.4000-6	4.4000-2
8.0000*	6.0000+ 6	0.67369+ 0	0.41924+ 0							0.3739+ 0			6.2000-6	6.2000-2
1.0000*	6.0000+ 6	0.65785+ 0	0.40367+ 0							0.2639+ 0			1.0000-5	1.0000-2
1.5000*	6.0000+ 6	0.64262+ 0	0.38847+ 0							0.1539+ 0			1.0000-5	1.0000-2
2.0000*	6.0000+ 6	0.62852+ 0	0.37369+ 0							0.0430+ 0			1.0000-5	1.0000-2
3.0000*	6.0000+ 6	0.61562+ 0	0.35927+ 0							0.0326+ 0			1.0000-5	1.0000-2
4.0000*	6.0000+ 6	0.60387+ 0	0.34524+ 0							0.0222+ 0			1.0000-5	1.0000-2
5.0000*	6.0000+ 6	0.59324+ 0	0.33157+ 0							0.0119+ 0			1.0000-5	1.0000-2
6.0000*	6.0000+ 6	0.58375+ 0	0.31828+ 0							0.0016+ 0			1.0000-5	1.0000-2
8.0000*	7.0000+ 7	0.57535+ 0	0.30529+ 0							0.0013+ 0			1.0000-5	1.0000-2
1.0000*	7.0000+ 7	0.56799+ 0	0.29259+ 0							0.0010+ 0			1.0000-5	1.0000-2
1.5000*	7.0000+ 7	0.56159+ 0	0.28019+ 0							0.0007+ 0			1.0000-5	1.0000-2
2.0000*	7.0000+ 7	0.55612+ 0	0.26802+ 0							0.0004+ 0			1.0000-5	1.0000-2
3.0000*	7.0000+ 7	0.55147+ 0	0.25607+ 0							0.0001+ 0			1.0000-5	1.0000-2
4.0000*	7.0000+ 7	0.54747+ 0	0.24434+ 0							0.0000+ 0			1.0000-5	1.0000-2
5.0000*	7.0000+ 7	0.54397+ 0	0.23282+ 0							0.0000+ 0			1.0000-5	1.0000-2
6.0000*	7.0000+ 7	0.54087+ 0	0.22151+ 0							0.0000+ 0			1.0000-5	1.0000-2
8.0000*	7.0000+ 7	0.53815+ 0	0.21041+ 0							0.0000+ 0			1.0000-5	1.0000-2
1.0000*	8.0000+ 8	0.53575+ 0	0.20000+ 0							0.0000+ 0			1.0000-5	1.0000-2
1.5000*	8.0000+ 8	0.53355+ 0	0.19000+ 0							0.0000+ 0			1.0000-5	1.0000-2
2.0000*	8.0000+ 8	0.53155+ 0	0.18000+ 0							0.0000+ 0			1.0000-5	1.0000-2
3.0000*	8.0000+ 8	0.52975+ 0	0.17000+ 0							0.0000+ 0			1.0000-5	1.0000-2
4.0000*	8.0000+ 8	0.52815+ 0	0.16000+ 0							0.0000+ 0			1.0000-5	1.0000-2
5.0000*	8.0000+ 8	0.52675+ 0	0.15000+ 0							0.0000+ 0			1.0000-5	1.0000-2
6.0000*	8.0000+ 8	0.52555+ 0	0.14000+ 0							0.0000+ 0			1.0000-5	1.0000-2
8.0000*	9.0000+ 9	0.52455+ 0	0.13000+ 0							0.0000+ 0			1.0000-5	1.0000-2
1.0000*	9.0000+ 9	0.52375+ 0	0.12000+ 0							0.0000+ 0			1.0000-5	1.0000-2
1.5000*	9.0000+ 9	0.52305+ 0	0.11000+ 0							0.0000+ 0			1.0000-5	1.0000-2
2.0000*	9.0000+ 9	0.52245+ 0	0.10000+ 0							0.0000+ 0			1.0000-5	1.0000-2
3.0000*	9.0000+ 9	0.52195+ 0	0.09000+ 0							0.0000+ 0			1.0000-5	1.0000-2
4.0000*	9.0000+ 9	0.52155+ 0	0.08000+ 0							0.0000+ 0			1.0000-5	1.0000-2
5.0000*	9.0000+ 9	0.52125+ 0	0.07000+ 0							0.0000+ 0			1.0000-5	1.0000-2
6.0000*	9.0000+ 9	0.52105+ 0	0.0											

CROSS SECTION

MI-82

MATERIAL #2204	ENERGY	TOTAL	ELASTIC	INELA	(N.2N)	(N.3N)	FISSION	(N.NR)	(N.NP)	(N.D)	(M.A)	MU-BAR
1.0000-6	1.0000-2	5.941+1	9.5648+0					4.3936+1				1.0869-2
1.0000-6	1.5000-2	2.8904+1	9.5049+0					2.0399+1				1.0880-2
1.0000-6	2.0000-2	2.6667+1	9.5049+0					1.7156+1				1.0860-2
1.0000-6	3.0000-2	2.5936+1	9.5049+0					1.4433+1				1.0880-2
1.0000-6	4.0000-2	2.5205+1	9.5049+0					1.2141+1				1.0880-2
1.0000-6	5.0000-2	2.4474+1	9.5049+0					1.0738+1				1.0880-2
1.0000-6	6.0000-2	2.3743+1	9.5049+0					9.5697+0				1.0860-2
1.0000-6	7.0000-2	2.3012+1	9.5049+0					8.5671+0				1.0860-2
1.0000-6	8.0000-2	2.2281+1	9.5049+0					7.5645+0				1.0860-2
1.0000-5	1.0000-1	1.7079+1	9.5055+0					6.4777+0				1.0860-2
1.0000-5	1.5000-1	1.6348+1	9.5055+0					5.4751+0				1.0860-2
1.0000-5	2.0000-1	1.5617+1	9.5055+0					4.4725+0				1.0860-2
1.0000-5	3.0000-1	1.4886+1	9.5071+0					3.4699+0				1.0860-2
1.0000-5	4.0000-1	1.4155+1	9.5071+0					2.4673+0				1.0860-2
1.0000-5	5.0000-1	1.3424+1	9.5094+0					1.4647+0				1.0880-2
1.0000-5	6.0000-1	1.2693+1	9.5108+0					4.3253+0				1.0880-2
1.0000-5	7.0000-1	1.1962+1	9.5131+0					3.2827+0				1.0880-2
1.0000-5	8.0000-1	1.1231+1	9.5154+0					2.2401+0				1.0880-2
1.0000-4	1.0000+0	1.0500+1	9.5177+0					1.1975+0				1.0880-2
1.0000-4	1.5000+0	1.0000+1	9.5200+0					1.1721+0				1.0880-2
1.0000-4	2.0000+0	9.5223+0	9.5223+0					1.1468+0				1.0861-2
1.0000-4	3.0000+0	9.5246+0	9.5246+0					1.1214+0				1.0861-2
1.0000-4	4.0000+0	9.5269+0	9.5269+0					1.0960+0				1.0861-2
1.0000-4	5.0000+0	9.5292+0	9.5292+0					9.6222-1				1.0861-2
1.0000-4	6.0000+0	9.5315+0	9.5315+0					8.6267-1				1.0861-2
1.0000-4	7.0000+0	9.5338+0	9.5338+0					7.5915-1				1.0861-2
1.0000-4	8.0000+0	9.5361+0	9.5361+0					6.4823-1				1.0861-2
1.0000-3	1.0000+1	1.0237+1	9.5385+0					5.4578-1				1.0861-2
1.0000-3	1.5000+1	1.0166+1	9.5408+0					4.6079-1				1.0861-2
1.0000-3	2.0000+1	1.0095+1	9.5432+0					3.8956-1				1.0861-2
1.0000-3	3.0000+1	1.0024+1	9.5456+0					3.4448-1				1.0861-2
1.0000-3	4.0000+1	9.9999+0	9.9999+0					3.1792-1				1.0861-2
1.0000-3	5.0000+1	9.9974+0	9.9974+0					2.7925-1				1.0861-2
1.0000-3	6.0000+1	9.9949+0	9.9949+0					2.4831-1				1.0861-2
1.0000-3	7.0000+1	9.9924+0	9.9924+0					2.1698-1				1.0861-2
1.0000-3	8.0000+1	9.9899+0	9.9899+0					1.8493-1				1.0861-2
1.0000-2	1.0000+2	1.0523+1	9.9924+0					1.6098-1				1.0861-2
1.0000-2	1.5000+2	1.0448+1	9.9949+0					1.4893-1				1.0861-2
1.0000-2	2.0000+2	1.0373+1	9.9974+0					1.3688-1				1.0861-2
1.0000-2	3.0000+2	1.0298+1	9.9999+0					1.2483-1				1.0861-2
1.0000-2	4.0000+2	1.0223+1	9.9999+0					1.1278-1				1.0861-2
1.0000-2	5.0000+2	1.0148+1	9.9999+0					1.0073-1				1.0861-2
1.0000-2	6.0000+2	1.0073+1	9.9999+0					9.6222-1				1.0861-2
1.0000-2	7.0000+2	1.0000+2	9.9999+0					8.6267-1				1.0861-2
1.0000-2	8.0000+2	9.9975+1	9.9975+1					7.5915-1				1.0861-2
1.0000-1	1.0000+3	1.0628+1	9.9999+0					6.4777+0				1.0861-2
1.0000-1	1.5000+3	1.0553+1	9.9999+0					5.4751+0				1.0861-2
1.0000-1	2.0000+3	1.0478+1	9.9999+0					4.4725+0				1.0861-2
1.0000-1	3.0000+3	1.0403+1	9.9999+0					3.4699+0				1.0861-2
1.0000-1	4.0000+3	1.0328+1	9.9999+0					2.4673+0				1.0861-2
1.0000-1	5.0000+3	1.0253+1	9.9999+0					1.4647+0				1.0861-2
1.0000-1	6.0000+3	1.0178+1	9.9999+0					4.3253+0				1.0861-2
1.0000-1	7.0000+3	1.0103+1	9.9999+0					3.2827+0				1.0861-2
1.0000-1	8.0000+3	1.0028+1	9.9999+0					2.2401+0				1.0861-2
1.0000-0	1.0000+4	1.0653+1	9.9999+0					1.6098-1				1.0861-2
1.0000-0	1.5000+4	1.0578+1	9.9999+0					1.4893-1				1.0861-2
1.0000-0	2.0000+4	1.0503+1	9.9999+0					1.3688-1				1.0861-2
1.0000-0	3.0000+4	1.0428+1	9.9999+0					1.2483-1				1.0861-2
1.0000-0	4.0000+4	1.0353+1	9.9999+0					1.1278-1				1.0861-2
1.0000-0	5.0000+4	1.0278+1	9.9999+0					1.0073-1				1.0861-2
1.0000-0	6.0000+4	1.0203+1	9.9999+0					9.6222-1				1.0861-2
1.0000-0	7.0000+4	1.0128+1	9.9999+0					8.6267-1				1.0861-2
1.0000-0	8.0000+4	1.0053+1	9.9999+0					7.5915-1				1.0861-2
1.0000-0	1.0000+5	1.0678+1	9.9999+0					6.4777+0				1.0861-2
1.0000-0	1.5000+5	1.0603+1	9.9999+0					5.4751+0				1.0861-2
1.0000-0	2.0000+5	1.0528+1	9.9999+0					4.4725+0				1.0861-2
1.0000-0	3.0000+5	1.0453+1	9.9999+0					3.4699+0				1.0861-2
1.0000-0	4.0000+5	1.0378+1	9.9999+0					2.4673+0				1.0861-2
1.0000-0	5.0000+5	1.0303+1	9.9999+0					1.4647+0				1.0861-2
1.0000-0	6.0000+5	1.0228+1	9.9999+0					4.3253+0				1.0861-2
1.0000-0	7.0000+5	1.0153+1	9.9999+0					3.2827+0				1.0861-2
1.0000-0	8.0000+5	1.0078+1	9.9999+0					2.2401+0				1.0861-2
1.0000-0	1.0000+6	1.0703+1	9.9999+0					1.6098-1				1.0861-2
1.0000-0	1.5000+6	1.0628+1	9.9999+0					1.4893-1				1.0861-2
1.0000-0	2.0000+6	1.0553+1	9.9999+0					1.3688-1				1.0861-2
1.0000-0	3.0000+6	1.0478+1	9.9999+0					1.2483-1				1.0861-2
1.0000-0	4.0000+6	1.0403+1	9.9999+0					1.1278-1				1.0861-2
1.0000-0	5.0000+6	1.0328+1	9.9999+0					1.0073-1				1.0861-2
1.0000-0	6.0000+6	1.0253+1	9.9999+0					9.6222-1				1.0861-2
1.0000-0	7.0000+6	1.0178+1	9.9999+0					8.6267-1				1.0861-2
1.0000-0	8.0000+6	1.0103+1	9.9999+0					7.5915-1				1.0861-2
1.0000-0	1.0000+7	1.0728+1	9.9999+0					6.4777+0				1.0861-2
1.0000-0	1.5000+7	1.0653+1	9.9999+0					5.4751+0				1.0861-2
1.0000-0	2.0000+7	1.0578+1	9.9999+0					4.4725+0				1.0861-2
1.0000-0	3.0000+7	1.0503+1	9.9999+0					3.4699+0				1.0861-2
1.0000-0	4.0000+7	1.0428+1	9.9999+0					2.4673+0				1.0861-2
1.0000-0	5.0000+7	1.0353+1	9.9999+0					1.4647+0				1.0861-2
1.0000-0	6.0000+7	1.0278+1	9.9999+0					4.3253+0				1.0861-2
1.0000-0	7.0000+7	1.0203+1	9.9999+0					3.2827+0				1.0861-2
1.0000-0	8.0000+7	1.0128+1	9.9999+0					2.2401+0				1.0861-2
1.0000-0	1.0000+8	1.0753+1	9.9999+0					1.6098-1				1.0861-2
1.0000-0	1.5000+8	1.0678+1	9.9999+0					1.4893-1				1.0861-2
1.0000-0	2.0000+8	1.0603+1	9.9999+0					1.3688-1				1.0861-2
1.0000-0	3.0000+8	1.0528+1	9.9999+0					1.2483-1				1.0861-2
1.0000-0	4.0000+8	1.0453+1	9.9999+0					1.1278-1				1.0861-2
1.0000-0	5.0000+8	1.0378+1	9.9999+0					1.0073-1				1.086

CROSS SECTION

MATERIAL = 2205

MI-84

ENERGY	TOTAL	ELASTIC	INELR	(N.2N)	(N.3N)	FISSION	(N.NR)	(N.NP)	(N.D)	(N.A)	MU-BRR
1.0000+ 5 ~ 1.0000- 2	4.6144+ 0	3.4637- 2						4.5788+ 0			1.0520- 2
1.0000- 1.5000-	2.1610+ 0	3.4838-						2.1829+ 0			1.0520-
1.5000- 2.0000-	1.6255+ 0	3.4838-						1.6562+ 0			1.0520-
2.0000- 3.0000-	1.5399+ 0	3.4838-						1.2974+ 0			1.0520-
3.0000- 4.0000-	1.3400+ 0	3.4838-						1.1144+ 0			1.0520-
4.0000- 5.0000-	1.0412+ 0	3.4641-						1.0066+ 0			1.0520-
5.0000- 6.0000-	8.2254- 1	3.4642-						7.8790- 1			1.0521-
6.0000- 7.0000-	7.0764- 1	3.4646-						6.7300- 1			1.0521-
7.0000- 8.0000-	6.0094- 1	3.4650-						5.5694- 1			1.0521-
8.0000- 9.0000-	4.9457- 1	3.4655-						4.7779- 1			1.0521-
9.0000- 1.0000+	3.8702- 1	3.4660-						3.7826- 1			1.0521-
1.0000+ 1.5000+	2.7949- 1	3.4664-						3.1954- 1			1.0521-
1.5000+ 2.0000+	2.4401- 1	3.4702-						2.4833- 1			1.0521-
2.0000+ 2.5000+	2.4719- 1	3.4729-						2.1247- 1			1.0521-
2.5000+ 3.0000+	2.1374- 1	3.4821-						1.7602- 1			1.0521-
3.0000+ 3.5000+	1.8195- 1	3.4874-						1.5025- 1			1.0521-
3.5000+ 4.0000+	1.4856- 1	3.4928-						1.1689- 1			1.0521-
4.0000+ 4.5000+	1.3578- 1	3.5006- 2						8.0567- 2			1.0521-
4.5000+ 5.0000+	1.2469- 1	3.5298-						7.9013- 2			1.0521-
5.0000+ 5.5000+	1.0250- 1	3.5555-						6.7198- 2			1.0521-
5.5000+ 6.0000+	8.2366- 2	3.5989-						5.5693- 2			1.0522-
6.0000+ 6.5000+	7.8754- 2	3.6450-						4.4243- 2			1.0522-
6.5000+ 7.0000+	6.6626- 2	3.6850-						3.5424- 2			1.0522-
7.0000+ 7.5000+	6.7016- 2	3.8587-						2.2652- 2			1.0522-
7.5000+ 8.0000+	6.4781- 2	4.1624-						2.8656- 2			1.0522-
8.0000+ 8.5000+	6.8192- 2	4.4681-						2.1548- 2			1.0530-
8.5000+ 9.0000+	6.2905- 2	4.9498-						1.8211- 2			1.0532-
9.0000+ 9.5000+	6.4933- 2	5.6365-						1.0959-			1.0532-
9.5000+ 1.0000+	7.5571- 2	6.3843-						1.0715-			1.0532-
1.0000+ 1.5000+	8.2369- 2	7.1952-						9.6812-			1.0532-
1.5000+ 2.0000+	5.3123- 2	1.0255-						8.7364-			1.0532-
2.0000+ 2.5000+	6.8192- 2	1.4173-						7.7588- 2			1.0532-
2.5000+ 3.0000+	1.4945- 2	1.8041-						6.6525-			1.0532-
3.0000+ 3.5000+	2.1737- 2	2.2824-						6.0659-			1.0532-
3.5000+ 4.0000+	2.3951- 2	2.8221-						5.4440-			1.0532-
4.0000+ 4.5000+	1.0533+ 0	3.4750+ 0						4.8263+ 0			1.0532-
4.5000+ 5.0000+	1.6834+ 0	3.4191+ 0						4.2745+ 0			1.0532-
5.0000+ 5.5000+	3.4268+ 0	3.4191+ 0						3.6770+ 0			1.0532-
5.5000+ 6.0000+	1.1811+ 1	3.4191+ 0						3.0867+ 0			1.0532-
6.0000+ 6.5000+	8.7657+ 1	4.4150+ 0						2.5018+ 0			1.0532-
6.5000+ 7.0000+	4.4180+ 0	5.0556+ 0						1.9200+ 0			1.0532-
7.0000+ 7.5000+	6.4422+ 0	5.4398+ 0						1.3491+ 0			1.0532-
7.5000+ 8.0000+	3.8975+ 0	6.1939+ 0						7.8845+ 0			1.0532-
8.0000+ 8.5000+	1.1933+ 1	1.1933+ 0						6.4737+ 0			1.0532-
8.5000+ 9.0000+	8.2911+ 0	8.2911+ 0						5.0623+ 0			1.0532-
9.0000+ 9.5000+	5.7513+ 0	5.7513+ 0						3.9280+ 0			1.0532-
9.5000+ 1.0000+	5.1138+ 0	5.1138+ 0						3.3917+ 0			1.0532-
1.0000+ 1.5000+	5.1138+ 0	5.1138+ 0						3.0109+ 0			1.0532-
1.5000+ 2.0000+	4.8020+ 0	4.8020+ 0						2.7236+ 0			1.0532-
2.0000+ 2.5000+	4.7812+ 0	4.7812+ 0						2.4517+ 0			1.0532-
2.5000+ 3.0000+	4.5897+ 0	4.5897+ 0						2.1837+ 0			1.0532-
3.0000+ 3.5000+	3.5852+ 0	3.5852+ 0						1.9100+ 0			1.0532-
3.5000+ 4.0000+	3.5852+ 0	3.5852+ 0						1.6385+ 0			1.0532-
4.0000+ 4.5000+	3.6673+ 0	3.6673+ 0						1.3670+ 0			1.0532-
4.5000+ 5.0000+	3.6673+ 0	3.6673+ 0						1.0955+ 0			1.0532-
5.0000+ 5.5000+	3.6673+ 0	3.6673+ 0						8.0822+ 0			1.0532-
5.5000+ 6.0000+	3.6673+ 0	3.6673+ 0						7.0182+ 0			1.0532-
6.0000+ 6.5000+	3.6673+ 0	3.6673+ 0						6.0585+ 0			1.0532-
6.5000+ 7.0000+	3.6673+ 0	3.6673+ 0						5.1199+ 0			1.0532-
7.0000+ 7.5000+	3.6673+ 0	3.6673+ 0						4.2822+ 0			1.0532-
7.5000+ 8.0000+	3.6673+ 0	3.6673+ 0						3.4468+ 0			1.0532-
8.0000+ 8.5000+	3.6673+ 0	3.6673+ 0						2.6114+ 0			1.0532-
8.5000+ 9.0000+	3.6673+ 0	3.6673+ 0						1.7760+ 0			1.0532-
9.0000+ 9.5000+	3.6673+ 0	3.6673+ 0						9.0000+ 0			1.0532-
9.5000+ 1.0000+	3.6673+ 0	3.6673+ 0						8.0000+ 0			1.0532-
1.0000+ 1.5000+	3.6673+ 0	3.6673+ 0						7.0000+ 0			1.0532-
1.5000+ 2.0000+	3.6673+ 0	3.6673+ 0						6.0000+ 0			1.0532-
2.0000+ 2.5000+	3.6673+ 0	3.6673+ 0						5.0000+ 0			1.0532-
2.5000+ 3.0000+	3.6673+ 0	3.6673+ 0						4.0000+ 0			1.0532-
3.0000+ 3.5000+	3.6673+ 0	3.6673+ 0						3.0000+ 0			1.0532-
3.5000+ 4.0000+	3.6673+ 0	3.6673+ 0						2.0000+ 0			1.0532-
4.0000+ 4.5000+	3.6673+ 0	3.6673+ 0						1.0000+ 0			1.0532-
4.5000+ 5.0000+	3.6673+ 0	3.6673+ 0						0.0000+ 0			1.0532-
5.0000+ 5.5000+	3.6673+ 0	3.6673+ 0						0.0000+ 0			1.0532-
5.5000+ 6.0000+	3.6673+ 0	3.6673+ 0						0.0000+ 0			1.0532-
6.0000+ 6.5000+	3.6673+ 0	3.6673+ 0						0.0000+ 0			1.0532-
6.5000+ 7.0000+	3.6673+ 0	3.6673+ 0						0.0000+ 0			1.0532-
7.0000+ 7.5000+	3.6673+ 0	3.6673+ 0						0.0000+ 0			1.0532-
7.5000+ 8.0000+	3.6673+ 0	3.6673+ 0						0.0000+ 0			1.0532-
8.0000+ 8.5000+	3.6673+ 0	3.6673+ 0						0.0000+ 0			1.0532-
8.5000+ 9.0000+	3.6673+ 0	3.6673+ 0						0.0000+ 0			1.0532-
9.0000+ 9.5000+	3.6673+ 0	3.6673+ 0						0.0000+ 0			1.0532-
9.5000+ 1.0000+	3.6673+ 0	3.6673+ 0						0.0000+ 0			1.0532-
1.0000+ 1.5000+	3.6673+ 0	3.6673+ 0						0.0000+ 0			1.0532-
1.5000+ 2.0000+	3.6673+ 0	3.6673+ 0						0.0000+ 0			1.0532-
2.0000+ 2.5000+	3.6673+ 0	3.6673+ 0						0.0000+ 0			1.0532-
2.5000+ 3.0000+	3.6673+ 0	3.6673+ 0						0.0000+ 0			1.0532-
3.0000+ 3.5000+	3.6673+ 0	3.6673+ 0						0.0000+ 0			1.0532-
3.5000+ 4.0000+	3.6673+ 0	3.6673+ 0						0.0000+ 0			1.0532-
4.0000+ 4.5000+	3.6673+ 0	3.6673+ 0						0.0000+ 0			1.0532-
4.5000+ 5.0000+	3.6673+ 0	3.6673+ 0						0.0000+ 0			1.0532-
5.0000+ 5.5000+	3.6673+ 0	3.6673+ 0						0.0000+ 0			1.0532-
5.5000+ 6.0000+	3.6673+ 0	3.6673+ 0						0.0000+ 0			1.0532-
6.0000+ 6.5000+	3.6673+ 0	3.6673+ 0						0.0000+ 0			1.0532-
6.5000+ 7.0000+	3.6673+ 0	3.6673+ 0						0.0000+ 0			1.0532-
7.0000+ 7.5000+	3.6673+ 0	3.6673+ 0						0.0000+ 0			1.0532-
7.5000+ 8.0000+	3.6673+ 0	3.6673+ 0						0.0000+ 0			1.0532-
8.0000+ 8.5000+	3.6673+ 0	3.6673+ 0						0.0000+ 0			1.0532-
8.5000+ 9.0000+	3.6673+ 0	3.6673+ 0						0.0000+ 0			1.0532-
9.0000+ 9.5000+	3.6673+ 0	3.6673+ 0						0.0000+ 0			1.0532-
9.5000+ 1.0000+	3.6673+ 0	3.6673+ 0						0.0000+ 0			1.0532-
1.0000+ 1.5000+	3.6673+ 0	3.6673+ 0						0.0000+ 0			1.0532-
1.5000+ 2.0000+	3.6673+ 0	3.6673+ 0						0.0000+ 0			

CROSS SECTION

CU-U

MATERIAL	ENERGY	TOTAL	ELASTIC	INEL	(N.PN)	(N.SN)	FIBION	(N.NR)	(N.NP)	CAPTURE	(N.P)	(N.D)	(N.A)	MU-BRR
1.0000	5 ~ 1.0000-2	1.9541	7.8588	0						1.1892	0	0.0000	0	1.0509-2
1.0000	1.0000	1.3492	7.8688	0						5.4289	0	0.0000	0	0.0000
1.0000	1.0000	1.2493	7.8688	0						1.7058	0	0.0000	0	0.0000
2.0000	1.0000	1.1084	7.8688	0						3.2251	0	0.0000	0	0.0000
4.0000	1.0000	1.0719	7.8688	0						2.8241	0	0.0000	0	0.0000
6.0000	1.0000	1.0439	7.8688	0						2.5718	0	0.0000	0	0.0000
8.0000	1.0000	1.0199	7.8688	0						2.3654	0	0.0000	0	0.0000
1.0000	1.0000-1	9.5890	7.8576	0						1.7114	0	0.0000	0	1.0509
1.0000	1.0000	9.5974	7.8571	0						1.4044	0	0.0000	0	0.0000
2.0000	1.0000	9.0962	7.8663	0						1.2104	0	0.0000	0	0.0000
3.0000	1.0000	8.8795	7.8682	0						1.0604	0	0.0000	0	0.0000
4.0000	1.0000	8.7538	7.8682	0						0.9278	0	0.0000	0	0.0000
5.0000	1.0000	8.6711	7.8682	0						0.8160	0	0.0000	0	0.0000
6.0000	1.0000	8.6322	7.8682	0						0.7194	0	0.0000	0	0.0000
1.0000	1.0000	8.5935	7.8457	0						5.3802	0	0.0000	0	1.0509
2.0000	1.0000	8.5935	7.8457	0						4.5328	0	0.0000	0	0.0000
3.0000	1.0000	8.5118	7.8350	0						3.7816	0	0.0000	0	0.0000
4.0000	1.0000	8.4405	7.8228	0						3.1780	0	0.0000	0	0.0000
5.0000	1.0000	8.0908	7.8125	0						2.6008	0	0.0000	0	0.0000
6.0000	1.0000	8.0527	7.8024	0						2.4508	0	0.0000	0	0.0000
8.0000	1.0000	7.9556	7.7871	0						2.2287	0	0.0000	0	0.0000
1.0000	1.0000	7.8940	7.7325	0						1.8243	0	0.0000	0	1.0510
1.0000	1.0000	7.8188	7.6640	0						1.8149	0	0.0000	0	0.0000
2.0000	1.0000	7.7217	7.6271	0						1.7058	0	0.0000	0	0.0000
3.0000	1.0000	7.6060	7.5731	0						1.6044	0	0.0000	0	0.0000
4.0000	1.0000	7.5060	7.4345	0						1.5044	0	0.0000	0	0.0000
5.0000	1.0000	7.4148	7.3503	0						1.4148	0	0.0000	0	0.0000
6.0000	1.0000	7.2842	7.2904	0						1.3313	0	0.0000	0	0.0000
8.0000	1.0000	7.1230	7.0787	0						1.2220	0	0.0000	0	0.0000
1.0000	1.0000	6.8708	6.8967	0						3.4246	0	0.0000	0	1.0521
1.0000	1.0000	6.5435	6.5169	0						2.8543	0	0.0000	0	1.0530
2.0000	1.0000	6.7893	6.2081	0						2.5511	0	0.0000	0	1.0529
3.0000	1.0000	6.7136	6.0983	0						2.4725	0	0.0000	0	1.0529
4.0000	1.0000	6.7036	6.1787	0						2.4053	0	0.0000	0	1.0524
5.0000	1.0000	6.6232	6.0523	0						2.3453	0	0.0000	0	1.0524
6.0000	1.0000	6.5027	5.9488	0						2.2947	0	0.0000	0	1.0505
8.0000	1.0000	6.4027	5.7358	0						2.2557	0	0.0000	0	1.0505
1.0000	1.0000	4.0988	4.0189	0						6.9234	0	0.0000	0	0.0000
1.0000	1.0000	3.7251	3.7251	0						6.7293	0	0.0000	0	0.0000
2.0000	1.0000	3.6122	3.6541	0						6.7123	0	0.0000	0	0.0000
3.0000	1.0000	3.5850	3.6253	0						6.6253	0	0.0000	0	0.0000
4.0000	1.0000	3.5301	3.6019	0						6.5208	0	0.0000	0	0.0000
5.0000	1.0000	3.4824	3.5787	0						6.4385	0	0.0000	0	0.0000
6.0000	1.0000	3.4431	3.5551	0						6.3561	0	0.0000	0	0.0000
8.0000	1.0000	3.3683	3.4437	0						6.2557	0	0.0000	0	0.0000
1.0000	1.0000	1.2324	1.2256	1						6.7408	0	0.0000	0	1.0488
1.0000	1.0000	0.2938	0.2937	0						6.5683	0	0.0000	0	1.0487
1.0000	1.0000	1.1470	1.1424	1						6.4591	0	0.0000	0	1.0487
2.0000	1.0000	1.0949	1.0949	1						6.3574	0	0.0000	0	1.0487
3.0000	1.0000	1.0375	1.0334	1						6.2647	0	0.0000	0	1.0486
4.0000	1.0000	0.9802	0.9649	0						6.1786	0	0.0000	0	1.0486
5.0000	1.0000	0.9251	0.9082	0						6.0980	0	0.0000	0	1.0485
6.0000	1.0000	0.8851	0.8689	0						6.0234	0	0.0000	0	1.0485
1.0000	1.0000	0.1408	0.1121	0						2.6822	0	0.0000	0	0.0000
1.0000	1.0000	0.3053	0.2825	0						2.3883	0	0.0000	0	0.0000
2.0000	1.0000	0.4596	0.4700	0						2.1869	0	0.0000	0	0.0000
3.0000	1.0000	0.5208	0.5700	0						1.9924	0	0.0000	0	0.0000
4.0000	1.0000	0.5800	0.6148	0						1.8280	0	0.0000	0	0.0000
5.0000	1.0000	0.6300	0.6537	0						1.6848	0	0.0000	0	0.0000
6.0000	1.0000	0.6763	0.6863	0						1.5582	0	0.0000	0	0.0000
1.0000	1.0000	0.8503	0.7789	0						1.4387	0	0.0000	0	0.0000
1.0000	1.0000	0.3081	0.3081	0						1.3273	0	0.0000	0	0.0000
2.0000	1.0000	0.3670	0.3670	0						1.2214	0	0.0000	0	0.0000
3.0000	1.0000	0.4267	0.4267	0						1.1214	0	0.0000	0	0.0000
4.0000	1.0000	0.4864	0.4864	0						1.0214	0	0.0000	0	0.0000
5.0000	1.0000	0.5461	0.5461	0						0.9214	0	0.0000	0	0.0000
6.0000	1.0000	0.6058	0.6058	0						0.8214	0	0.0000	0	0.0000
1.0000	1.0000	0.8655	0.8655	0						0.7214	0	0.0000	0	0.0000
1.0000	1.0000	0.9252	0.9252	0						0.6214	0	0.0000	0	0.0000
2.0000	1.0000	0.9849	0.9849	0						0.5214	0	0.0000	0	0.0000
3.0000	1.0000	1.0446	1.0446	0						0.4214	0	0.0000	0	0.0000
4.0000	1.0000	1.1043	1.1043	0						0.3214	0	0.0000	0	0.0000
5.0000	1.0000	1.1640	1.1640	0						0.2214	0	0.0000	0	0.0000
6.0000	1.0000	1.2237	1.2237	0						0.1214	0	0.0000	0	0.0000
1.0000	1.0000	3.2715	1.6091	0						1.0483	0	0.0000	0	1.0483
2.0000	1.0000	3.2715	1.6091	0						1.0483	0	0.0000	0	1.0483
3.0000	1.0000	3.2715	1.6091	0						1.0483	0	0.0000	0	1.0483
4.0000	1.0000	3.2715	1.6091	0						1.0483	0	0.0000	0	1.0483
5.0000	1.0000	3.2715	1.6091	0						1.0483	0	0.0000	0	1.0483
6.0000	1.0000	3.2715	1.6091	0						1.0483	0	0.0000	0	1.0483
1.0000	1.0000	3.2715	1.6091	0						1.0483	0	0.0000	0	1.0483
2.0000	1.0000	3.2715	1.6091	0						1.0483	0	0.0000	0	1.0483
3.0000	1.0000	3.2715	1.6091	0						1.0483	0	0.0000	0	1.0483
4.0000	1.0000	3.2715	1.6091	0						1.0483	0	0.0000	0	1.0483
5.0000	1.0000	3.2715	1.6091	0						1.0483	0	0.0000	0	1.0483
6.0000	1.0000	3.2715	1.6091	0						1.0483	0	0.0000	0	1.0483

CU-63

CROSS SECTION

MATERIAL = 2291

ENERGY	TOTAL	ELASTIC	INELA	(N,2N)	(N,3N)	FISSION	(N,NR)	(N,NP)	CAPTURE	(N,P)	(N,D)	(N,R)	MU-BRK
1.0000-5	1.8882+1	4.9792+0							1.3903+1			0.0000+0	1.0686-2
1.0000-4	1.1434+1	4.9792+0							5.4548+0			0.0000+0	1.0686-2
1.0000-3	1.0406+1	4.9791+0							2.5628+0			0.0000+0	1.0686-2
2.0000-2	3.0000+0	4.9791+0							3.8167+0			0.0000+0	1.0686-2
3.0000-1	3.0000+0	4.9788+0							3.3815+0			0.0000+0	1.0686-2
4.0000-0	3.0000+0	4.9788+0							3.0541+0			0.0000+0	1.0686-2
5.0000-0	7.6967+0	4.9787+0							2.7170+0			0.0000+0	1.0686-2
6.0000-0	7.3686+0	4.9786+0							2.5910+0			0.0000+0	1.0686-2
7.0000-0	7.0198+0	4.9783+0							2.0417+0			0.0000+0	1.0686-2
8.0000-0	6.5936+0	4.9778+0							1.7157+0			0.0000+0	1.0686-2
9.0000-0	6.1167+0	4.9773+0							1.4394+0			0.0000+0	1.0686-2
1.0000-1	5.1860+0	4.9755+0							1.2672+0			0.0000+0	1.0686-2
2.0000-1	4.0422+0	4.9757+0							9.6810+0			0.0000+0	1.0686-2
3.0000-1	3.7593+0	4.9737+0							8.5632+0			0.0000+0	1.0686-2
4.0000-1	3.7236+0	4.9722+0							7.1534+0			0.0000+0	1.0686-2
5.0000-1	5.6096+0	4.9694+0							6.4020+0			0.0000+0	1.0686-2
6.0000-1	5.5039+0	4.9627+0							5.3542+0			0.0000+0	1.0686-2
7.0000-1	5.3290+0	4.9519+0							4.4854+0			0.0000+0	1.0686-2
8.0000-1	5.2745+0	4.9442+0							3.7712+0			0.0000+0	1.0686-2
9.0000-1	5.2322+0	4.9356+0							3.3039+0			0.0000+0	1.0686-2
1.0000-2	5.1868+0	4.9252+0							2.5666+0			0.0000+0	1.0686-2
2.0000-2	5.1382+0	4.9102+0							2.2786+0			0.0000+0	1.0686-2
3.0000-2	5.0748+0	4.8944+0							1.9040+0			0.0000+0	1.0686-2
4.0000-2	5.0052+0	4.8765+0							1.5665+0			0.0000+0	1.0686-2
5.0000-2	4.9230+0	4.8559+0							1.2058+0			0.0000+0	1.0686-2
6.0000-2	4.8283+0	4.8285+0							0.9179+0			0.0000+0	1.0686-2
7.0000-2	4.7243+0	4.8108+0							0.6108+0			0.0000+0	1.0686-2
8.0000-2	4.5901+0	4.7887+0							0.3333+0			0.0000+0	1.0686-2
9.0000-2	4.4780+0	4.7279+0							0.1352+0			0.0000+0	1.0686-2
1.0000-3	4.3689+0	4.6718+0							3.8001+0			0.0000+0	1.0686-2
2.0000-3	4.2587+0	4.6087+0							2.1459+0			0.0000+0	1.0686-2
3.0000-3	4.1463+0	4.5316+0							1.4598+0			0.0000+0	1.0686-2
4.0000-3	4.0336+0	4.4484+0							0.7179+0			0.0000+0	1.0686-2
5.0000-3	3.9113+0	4.3565+0							0.2222+0			0.0000+0	1.0686-2
6.0000-3	3.7891+0	4.2587+0							0.0000+0			0.0000+0	1.0686-2
7.0000-3	3.6673+0	4.1571+0							0.0000+0			0.0000+0	1.0686-2
8.0000-3	3.5458+0	4.0529+0							0.0000+0			0.0000+0	1.0686-2
9.0000-3	3.4244+0	3.9469+0							0.0000+0			0.0000+0	1.0686-2
1.0000-4	3.3033+0	3.8393+0							0.0000+0			0.0000+0	1.0686-2
2.0000-4	3.1828+0	3.7303+0							0.0000+0			0.0000+0	1.0686-2
3.0000-4	3.0629+0	3.6200+0							0.0000+0			0.0000+0	1.0686-2
4.0000-4	2.9436+0	3.5085+0							0.0000+0			0.0000+0	1.0686-2
5.0000-4	2.8250+0	3.3958+0							0.0000+0			0.0000+0	1.0686-2
6.0000-4	2.7071+0	3.2819+0							0.0000+0			0.0000+0	1.0686-2
7.0000-4	2.5900+0	3.1677+0							0.0000+0			0.0000+0	1.0686-2
8.0000-4	2.4736+0	3.0533+0							0.0000+0			0.0000+0	1.0686-2
9.0000-4	2.3579+0	2.9387+0							0.0000+0			0.0000+0	1.0686-2
1.0000-5	2.2429+0	2.8240+0							0.0000+0			0.0000+0	1.0686-2
2.0000-5	2.1284+0	2.7093+0							0.0000+0			0.0000+0	1.0686-2
3.0000-5	2.0145+0	2.5945+0							0.0000+0			0.0000+0	1.0686-2
4.0000-5	1.9012+0	2.4797+0							0.0000+0			0.0000+0	1.0686-2
5.0000-5	1.7885+0	2.3649+0							0.0000+0			0.0000+0	1.0686-2
6.0000-5	1.6764+0	2.2501+0							0.0000+0			0.0000+0	1.0686-2
7.0000-5	1.5648+0	2.1353+0							0.0000+0			0.0000+0	1.0686-2
8.0000-5	1.4537+0	2.0205+0							0.0000+0			0.0000+0	1.0686-2
9.0000-5	1.3431+0	1.9057+0							0.0000+0			0.0000+0	1.0686-2
1.0000-6	1.2330+0	1.7909+0							0.0000+0			0.0000+0	1.0686-2
2.0000-6	1.1234+0	1.6761+0							0.0000+0			0.0000+0	1.0686-2
3.0000-6	1.0143+0	1.5613+0							0.0000+0			0.0000+0	1.0686-2
4.0000-6	0.9057+0	1.4465+0							0.0000+0			0.0000+0	1.0686-2
5.0000-6	0.7976+0	1.3317+0							0.0000+0			0.0000+0	1.0686-2
6.0000-6	0.6900+0	1.2169+0							0.0000+0			0.0000+0	1.0686-2
7.0000-6	0.5829+0	1.1021+0							0.0000+0			0.0000+0	1.0686-2
8.0000-6	0.4764+0	0.9873+0							0.0000+0			0.0000+0	1.0686-2
9.0000-6	0.3705+0	0.8725+0							0.0000+0			0.0000+0	1.0686-2
1.0000-7	0.2652+0	0.7577+0							0.0000+0			0.0000+0	1.0686-2
2.0000-7	0.1605+0	0.6429+0							0.0000+0			0.0000+0	1.0686-2
3.0000-7	0.0558+0	0.5281+0							0.0000+0			0.0000+0	1.0686-2
4.0000-7	0.0000+0	0.4133+0							0.0000+0			0.0000+0	1.0686-2
5.0000-7	0.0000+0	0.2985+0							0.0000+0			0.0000+0	1.0686-2
6.0000-7	0.0000+0	0.1837+0							0.0000+0			0.0000+0	1.0686-2
7.0000-7	0.0000+0	0.0689+0							0.0000+0			0.0000+0	1.0686-2
8.0000-7	0.0000+0	0.0000+0							0.0000+0			0.0000+0	1.0686-2
9.0000-7	0.0000+0	0.0000+0							0.0000+0			0.0000+0	1.0686-2
1.0000-8	0.0000+0	0.0000+0							0.0000+0			0.0000+0	1.0686-2
2.0000-8	0.0000+0	0.0000+0							0.0000+0			0.0000+0	1.0686-2
3.0000-8	0.0000+0	0.0000+0							0.0000+0			0.0000+0	1.0686-2
4.0000-8	0.0000+0	0.0000+0							0.0000+0			0.0000+0	1.0686-2
5.0000-8	0.0000+0	0.0000+0							0.0000+0			0.0000+0	1.0686-2
6.0000-8	0.0000+0	0.0000+0							0.0000+0			0.0000+0	1.0686-2
7.0000-8	0.0000+0	0.0000+0							0.0000+0			0.0000+0	1.0686-2
8.0000-8	0.0000+0	0.0000+0							0.0000+0			0.0000+0	1.0686-2
9.0000-8	0.0000+0	0.0000+0							0.0000+0			0.0000+0	1.0686-2
1.0000-9	0.0000+0	0.0000+0							0.0000+0			0.0000+0	1.0686-2
2.0000-9	0.0000+0	0.0000+0							0.0000+0			0.0000+0	1.0686-2
3.0000-9	0.0000+0	0.0000+0							0.0000+0			0.0000+0	1.0686-2
4.0000-9	0.0000+0	0.0000+0							0.0000+0			0.0000+0	1.0686-2
5.0000-9	0.0000+0	0.0000+0							0.0000+0			0.0000+0	1.0686-2
6.0000-9	0.0000+0	0.0000+0							0.0000+0			0.0000+0	1.0686-2
7.0000-9	0.0000+0	0.0000+0							0.0000+0			0.0000+0	1.0686-2
8.0000-9	0.0000+0	0.0000+0							0.0000+0			0.0000+0	1.0686-2
9.0000-9	0.0000+0	0.0000+0							0.0000+0			0.0000+0	1

CROSS SECTION

CU-65

MATERIAL -2292	ENERGY	TOTAL	ELASTIC	INELR	(N.2N)	(N.3N)	FISSION	(N.4R)	(N.NP)	CAPTURE	(N.P)	(N.D)	(N.R)	MU-BR-2
1.0000	5 ~ 1.0000-2	2.1014+ 1	1.4298+ 1							6.7156+ 0				1.0366- 2
1.0000	1.5000-	1.7466+ 1	1.4298+ 1							9.1180+ 0				1.0366-
1.0000	2.0000-	1.8503+ 1	1.4298+ 1							2.26216+ 0				1.0366-
1.0000	3.0000-	1.9540+ 1	1.4298+ 1							1.8542+ 0				1.0366-
1.0000	4.0000-	2.0577+ 1	1.4298+ 1							1.4782+ 0				1.0366-
1.0000	5.0000-	2.1614+ 1	1.4298+ 1							1.1169+ 0				1.0366-
1.0000	6.0000-	2.2651+ 1	1.4298+ 1							8.8119-				1.0366-
1.0000	7.0000-	2.3688+ 1	1.4298+ 1							6.7617-				1.0366-
1.0000	8.0000-	2.4725+ 1	1.4298+ 1							5.5610-				1.0366-
1.0000	9.0000-	2.5762+ 1	1.4298+ 1							4.3603-				1.0366-
1.0000	1.0000-1	1.6281+ 1	1.4298+ 1							3.1696-				1.0366-
1.0000	2.0000-1	1.6124+ 1	1.4298+ 1							2.9789-				1.0366-
1.0000	3.0000-1	1.5967+ 1	1.4298+ 1							2.7882-				1.0366-
1.0000	4.0000-1	1.5810+ 1	1.4298+ 1							2.5975-				1.0366-
1.0000	5.0000-1	1.5653+ 1	1.4298+ 1							2.4068-				1.0366-
1.0000	6.0000-1	1.5496+ 1	1.4298+ 1							2.2161-				1.0366-
1.0000	7.0000-1	1.5339+ 1	1.4298+ 1							2.0254-				1.0366-
1.0000	8.0000-1	1.5182+ 1	1.4298+ 1							1.8347-				1.0366-
1.0000	9.0000-1	1.5025+ 1	1.4298+ 1							1.6440-				1.0366-
1.0000	0 ~ 1.5000-0	1.4868+ 1	1.4298+ 1							1.4533-				1.0366-
1.0000	0 ~ 2.0000-0	1.4711+ 1	1.4298+ 1							1.2626-				1.0366-
1.0000	0 ~ 3.0000-0	1.4554+ 1	1.4298+ 1							1.0719-				1.0366-
1.0000	0 ~ 4.0000-0	1.4397+ 1	1.4298+ 1							9.6275-				1.0367-
1.0000	0 ~ 5.0000-0	1.4240+ 1	1.4298+ 1							8.0314-				1.0367-
1.0000	0 ~ 6.0000-0	1.4083+ 1	1.4298+ 1							6.4353-				1.0367-
1.0000	0 ~ 7.0000-0	1.3926+ 1	1.4298+ 1							4.8392-				1.0367-
1.0000	0 ~ 8.0000-0	1.3769+ 1	1.4298+ 1							3.2431-				1.0367-
1.0000	0 ~ 9.0000-0	1.3612+ 1	1.4298+ 1							1.6470-				1.0367-
1.0000	1 ~ 1.5000-1	1.3455+ 1	1.4298+ 1							9.6275-				1.0367-
1.0000	1 ~ 2.0000-1	1.3298+ 1	1.4298+ 1							8.0314-				1.0367-
1.0000	1 ~ 3.0000-1	1.3141+ 1	1.4298+ 1							6.4353-				1.0367-
1.0000	1 ~ 4.0000-1	1.2984+ 1	1.4298+ 1							4.8392-				1.0367-
1.0000	1 ~ 5.0000-1	1.2827+ 1	1.4298+ 1							3.2431-				1.0367-
1.0000	1 ~ 6.0000-1	1.2670+ 1	1.4298+ 1							1.6470-				1.0367-
1.0000	1 ~ 7.0000-1	1.2513+ 1	1.4298+ 1							9.6275-				1.0367-
1.0000	1 ~ 8.0000-1	1.2356+ 1	1.4298+ 1							8.0314-				1.0367-
1.0000	1 ~ 9.0000-1	1.2199+ 1	1.4298+ 1							6.4353-				1.0367-
1.0000	2 ~ 1.5000-2	1.2042+ 1	1.4298+ 1							4.8392-				1.0367-
1.0000	2 ~ 2.0000-2	1.1885+ 1	1.4298+ 1							3.2431-				1.0367-
1.0000	2 ~ 3.0000-2	1.1728+ 1	1.4298+ 1							1.6470-				1.0367-
1.0000	2 ~ 4.0000-2	1.1571+ 1	1.4298+ 1							9.6275-				1.0367-
1.0000	2 ~ 5.0000-2	1.1414+ 1	1.4298+ 1							8.0314-				1.0367-
1.0000	2 ~ 6.0000-2	1.1257+ 1	1.4298+ 1							6.4353-				1.0367-
1.0000	2 ~ 7.0000-2	1.1100+ 1	1.4298+ 1							4.8392-				1.0367-
1.0000	2 ~ 8.0000-2	1.0943+ 1	1.4298+ 1							3.2431-				1.0367-
1.0000	2 ~ 9.0000-2	1.0786+ 1	1.4298+ 1							1.6470-				1.0367-
1.0000	3 ~ 1.5000-3	1.0629+ 1	1.4298+ 1							9.6275-				1.0367-
1.0000	3 ~ 2.0000-3	1.0472+ 1	1.4298+ 1							8.0314-				1.0367-
1.0000	3 ~ 3.0000-3	1.0315+ 1	1.4298+ 1							6.4353-				1.0367-
1.0000	3 ~ 4.0000-3	1.0158+ 1	1.4298+ 1							4.8392-				1.0367-
1.0000	3 ~ 5.0000-3	1.0001+ 1	1.4298+ 1							3.2431-				1.0367-
1.0000	3 ~ 6.0000-3	9.8440+ 0	1.4298+ 1							1.6470-				1.0367-
1.0000	3 ~ 7.0000-3	9.6881+ 0	1.4298+ 1							9.6275-				1.0367-
1.0000	3 ~ 8.0000-3	9.5322+ 0	1.4298+ 1							8.0314-				1.0367-
1.0000	3 ~ 9.0000-3	9.3763+ 0	1.4298+ 1							6.4353-				1.0367-
1.0000	4 ~ 1.5000-4	9.2204+ 0	1.4298+ 1							4.8392-				1.0367-
1.0000	4 ~ 2.0000-4	9.0645+ 0	1.4298+ 1							3.2431-				1.0367-
1.0000	4 ~ 3.0000-4	8.9086+ 0	1.4298+ 1							1.6470-				1.0367-
1.0000	4 ~ 4.0000-4	8.7527+ 0	1.4298+ 1							9.6275-				1.0367-
1.0000	4 ~ 5.0000-4	8.5968+ 0	1.4298+ 1							8.0314-				1.0367-
1.0000	4 ~ 6.0000-4	8.4409+ 0	1.4298+ 1							6.4353-				1.0367-
1.0000	4 ~ 7.0000-4	8.2850+ 0	1.4298+ 1							4.8392-				1.0367-
1.0000	4 ~ 8.0000-4	8.1291+ 0	1.4298+ 1							3.2431-				1.0367-
1.0000	4 ~ 9.0000-4	7.9732+ 0	1.4298+ 1							1.6470-				1.0367-
1.0000	5 ~ 1.5000-5	7.8173+ 0	1.4298+ 1							9.6275-				1.0367-
1.0000	5 ~ 2.0000-5	7.6614+ 0	1.4298+ 1							8.0314-				1.0367-
1.0000	5 ~ 3.0000-5	7.5055+ 0	1.4298+ 1							6.4353-				1.0367-
1.0000	5 ~ 4.0000-5	7.3496+ 0	1.4298+ 1							4.8392-				1.0367-
1.0000	5 ~ 5.0000-5	7.1937+ 0	1.4298+ 1							3.2431-				1.0367-
1.0000	5 ~ 6.0000-5	7.0378+ 0	1.4298+ 1							1.6470-				1.0367-
1.0000	5 ~ 7.0000-5	6.8819+ 0	1.4298+ 1							9.6275-				1.0367-
1.0000	5 ~ 8.0000-5	6.7260+ 0	1.4298+ 1							8.0314-				1.0367-
1.0000	5 ~ 9.0000-5	6.5701+ 0	1.4298+ 1							6.4353-				1.0367-
1.0000	6 ~ 1.5000-6	6.4142+ 0	1.4298+ 1							4.8392-				1.0367-
1.0000	6 ~ 2.0000-6	6.2583+ 0	1.4298+ 1							3.2431-				1.0367-
1.0000	6 ~ 3.0000-6	6.1024+ 0	1.4298+ 1							1.6470-				1.0367-
1.0000	6 ~ 4.0000-6	5.9465+ 0	1.4298+ 1							9.6275-				1.0367-
1.0000	6 ~ 5.0000-6	5.7906+ 0	1.4298+ 1							8.0314-				1.0367-
1.0000	6 ~ 6.0000-6	5.6347+ 0	1.4298+ 1							6.4353-				1.0367-
1.0000	6 ~ 7.0000-6	5.4788+ 0	1.4298+ 1							4.8392-				1.0367-
1.0000	6 ~ 8.0000-6	5.3229+ 0	1.4298+ 1							3.2431-				1.0367-
1.0000	6 ~ 9.0000-6	5.1670+ 0	1.4298+ 1							1.6470-				1.0367-
1.0000	7 ~ 1.5000-7	5.0111+ 0	1.4298+ 1							9.6275-				1.0367-
1.0000	7 ~ 2.0000-7	4.8552+ 0	1.4298+ 1							8.0314-				1.0367-
1.0000	7 ~ 3.0000-7	4.7093+ 0	1.4298+ 1							6.4353-				1.0367-
1.0000	7 ~ 4.0000-7	4.5534+ 0	1.4298+ 1							4.8392-				1.0367-
1.0000	7 ~ 5.0000-7	4.3975+ 0	1.4298+ 1							3.2431-				1.0367-
1.0000	7 ~ 6.0000-7	4.2416+ 0	1.4298+ 1							1.6470-				1.0367-
1.0000	7 ~ 7.0000-7	4.0857+ 0	1.4298+ 1							9.6275-				1.0367-
1.0000	7 ~ 8.0000-7	3.9298+ 0	1.4298+ 1							8.0314-				1.0367-
1.0000	7 ~ 9.0000-7	3.7739+ 0	1.4298+ 1							6.4353-				1.0367-
1.0000	8 ~ 1.5000-8	3.6180+ 0	1.4298+ 1							4.8392-				1.0367-
1.0000	8 ~ 2.0000-8	3.4621+ 0	1.4298+ 1							3.2431-				1.0367-
1.0000	8 ~ 3.0000-8	3.3062+ 0	1.4298+ 1							1.6470-				1.0367-
1.0000	8 ~ 4.0000-8	3.1503+ 0	1.4298+ 1							9.6275-				1.0367-
1.0000	8 ~ 5.0000-8	2.9944+ 0	1.4298+ 1							8.0314-				1.0367-
1.0000	8 ~ 6.0000-8	2.8385+ 0	1.4298+ 1							6.4353-				1.0367-
1.0000	8 ~ 7.0000-8	2.6826+ 0	1.4298+ 1							4.8392-				1.0367-
1.0000	8 ~ 8.0000-8	2.5267+ 0	1.4298+ 1							3.2431-				1.0367-
1.0000	8 ~ 9.0000-8	2.3708+ 0	1.4298+ 1							1.6470-				1.0367-
1.0000	9 ~ 1.5000-9	2.2149+ 0	1.4298+ 1							9.6275-				1.0367-
1.0000	9 ~ 2.0000-9	2.0590+ 0	1.4298+ 1							8.0314-				1.0367-
1.0000	9 ~ 3.0000-9	1.9031+ 0	1.4298+ 1							6.4353-				1.0367-
1.0000</														

CROSS SECTION

MATERIAL = 2411		NU-BAR											
ENERGY	TOTAL	ELABTIC	INELR	IN.2N1	(N.3N)	FISSION	(N.NR)	(N.NP1)	CAPTURE	(N.NP)	(N.D)	(N.R)	NU-BAR
1.0000-5 ~ 1.0000-2	8.8908+0	6.3258+0							3.5650+0	0.0000+0		0.0000+0	7.3207-9
1.0000-2 ~ 1.0000-1	7.9907+0	6.3257+0							1.6650+0	0.0000+0		0.0000+0	7.3378-9
1.0000-1 ~ 1.0000-0	7.7171+0	6.3256+0							1.3114+0	0.0000+0		0.0000+0	7.3541-9
1.0000-0 ~ 1.0000-0	7.3174+0	6.3255+0							9.8177+0	0.0000+0		0.0000+0	7.3704-9
1.0000-0 ~ 1.0000-0	7.1922+0	6.3254+0							8.6669+0	0.0000+0		0.0000+0	7.3867-9
1.0000-0 ~ 1.0000-0	7.1081+0	6.3253+0							7.8289+0	0.0000+0		0.0000+0	7.4030-9
1.0000-0 ~ 1.0000-0	7.0216+0	6.3252+0							6.9820+0	0.0000+0		0.0000+0	7.4193-9
1.0000-0 ~ 1.0000-0	6.9378+0	6.3251+0							6.1288+0	0.0000+0		0.0000+0	7.4356-9
1.0000-0 ~ 1.0000-0	6.8478+0	6.3250+0							5.2786+0	0.0000+0		0.0000+0	7.4519-9
1.0000-0 ~ 1.0000-0	6.7637+0	6.3249+0							4.5909+0	0.0000+0		0.0000+0	7.4682-9
1.0000-0 ~ 1.0000-0	6.6923+0	6.3248+0							3.9614+0	0.0000+0		0.0000+0	7.4845-9
1.0000-0 ~ 1.0000-0	6.6329+0	6.3247+0							3.3950+0	0.0000+0		0.0000+0	7.5008-9
1.0000-0 ~ 1.0000-0	6.5823+0	6.3246+0							2.8429+0	0.0000+0		0.0000+0	7.5171-9
1.0000-0 ~ 1.0000-0	6.5397+0	6.3245+0							2.3170+0	0.0000+0		0.0000+0	7.5334-9
1.0000-0 ~ 1.0000-0	6.5111+0	6.3244+0							1.8139+0	0.0000+0		0.0000+0	7.5497-9
1.0000-0 ~ 1.0000-0	6.4793+0	6.3243+0							1.3429+0	0.0000+0		0.0000+0	7.5660-9
1.0000-0 ~ 1.0000-0	6.4322+0	6.3242+0							9.3577+0	0.0000+0		0.0000+0	7.5823-9
1.0000-0 ~ 1.0000-0	6.3956+0	6.3241+0							8.0873+0	0.0000+0		0.0000+0	7.5986-9
1.0000-0 ~ 1.0000-0	6.3768+0	6.3240+0							7.1909+0	0.0000+0		0.0000+0	7.6149-9
1.0000-0 ~ 1.0000-0	6.3615+0	6.3239+0							6.2563+0	0.0000+0		0.0000+0	7.6312-9
1.0000-0 ~ 1.0000-0	6.3217+0	6.3238+0							5.2953+0	0.0000+0		0.0000+0	7.6475-9
1.0000-0 ~ 1.0000-0	6.2517+0	6.3237+0							4.3425+0	0.0000+0		0.0000+0	7.6638-9
1.0000-0 ~ 1.0000-0	6.2915+0	6.3236+0							3.4257+0	0.0000+0		0.0000+0	7.6801-9
1.0000-0 ~ 1.0000-0	6.2564+0	6.3235+0							2.4457+0	0.0000+0		0.0000+0	7.6964-9
1.0000-0 ~ 1.0000-0	6.2116+0	6.3234+0							1.4020+0	0.0000+0		0.0000+0	7.7127-9
1.0000-0 ~ 1.0000-0	6.1433+0	6.3233+0							3.4343+0	0.0000+0		0.0000+0	7.7290-9
1.0000-0 ~ 1.0000-0	6.1155+0	6.3232+0							3.3788+0	0.0000+0		0.0000+0	7.7453-9
1.0000-0 ~ 1.0000-0	6.0959+0	6.3231+0							2.4547+0	0.0000+0		0.0000+0	7.7616-9
1.0000-0 ~ 1.0000-0	6.0924+0	6.3230+0							1.4999+0	0.0000+0		0.0000+0	7.7779-9
1.0000-0 ~ 1.0000-0	6.0922+0	6.3229+0							8.0989+0	0.0000+0		0.0000+0	7.7942-9
1.0000-0 ~ 1.0000-0	6.0921+0	6.3228+0							7.1537+0	0.0000+0		0.0000+0	7.8105-9
1.0000-0 ~ 1.0000-0	6.0920+0	6.3227+0							6.2007+0	0.0000+0		0.0000+0	7.8268-9
1.0000-0 ~ 1.0000-0	6.0919+0	6.3226+0							5.2482+0	0.0000+0		0.0000+0	7.8431-9
1.0000-0 ~ 1.0000-0	6.0918+0	6.3225+0							4.3057+0	0.0000+0		0.0000+0	7.8594-9
1.0000-0 ~ 1.0000-0	6.0917+0	6.3224+0							3.3732+0	0.0000+0		0.0000+0	7.8757-9
1.0000-0 ~ 1.0000-0	6.0916+0	6.3223+0							2.4507+0	0.0000+0		0.0000+0	7.8920-9
1.0000-0 ~ 1.0000-0	6.0915+0	6.3222+0							1.5282+0	0.0000+0		0.0000+0	7.9083-9
1.0000-0 ~ 1.0000-0	6.0914+0	6.3221+0							6.3192+0	0.0000+0		0.0000+0	7.9246-9
1.0000-0 ~ 1.0000-0	6.0913+0	6.3220+0							5.4020+0	0.0000+0		0.0000+0	7.9409-9
1.0000-0 ~ 1.0000-0	6.0912+0	6.3219+0							4.4843+0	0.0000+0		0.0000+0	7.9572-9
1.0000-0 ~ 1.0000-0	6.0911+0	6.3218+0							3.5666+0	0.0000+0		0.0000+0	7.9735-9
1.0000-0 ~ 1.0000-0	6.0910+0	6.3217+0							2.6489+0	0.0000+0		0.0000+0	7.9898-9
1.0000-0 ~ 1.0000-0	6.0909+0	6.3216+0							1.7312+0	0.0000+0		0.0000+0	8.0061-9
1.0000-0 ~ 1.0000-0	6.0908+0	6.3215+0							8.3982+0	0.0000+0		0.0000+0	8.0224-9
1.0000-0 ~ 1.0000-0	6.0907+0	6.3214+0							7.4805+0	0.0000+0		0.0000+0	8.0387-9
1.0000-0 ~ 1.0000-0	6.0906+0	6.3213+0							6.5628+0	0.0000+0		0.0000+0	8.0550-9
1.0000-0 ~ 1.0000-0	6.0905+0	6.3212+0							5.6451+0	0.0000+0		0.0000+0	8.0713-9
1.0000-0 ~ 1.0000-0	6.0904+0	6.3211+0							4.7274+0	0.0000+0		0.0000+0	8.0876-9
1.0000-0 ~ 1.0000-0	6.0903+0	6.3210+0							3.8097+0	0.0000+0		0.0000+0	8.1039-9
1.0000-0 ~ 1.0000-0	6.0902+0	6.3209+0							2.8920+0	0.0000+0		0.0000+0	8.1202-9
1.0000-0 ~ 1.0000-0	6.0901+0	6.3208+0							1.9743+0	0.0000+0		0.0000+0	8.1365-9
1.0000-0 ~ 1.0000-0	6.0900+0	6.3207+0							1.0566+0	0.0000+0		0.0000+0	8.1528-9
1.0000-0 ~ 1.0000-0	6.0899+0	6.3206+0							0.1389+0	0.0000+0		0.0000+0	8.1691-9
1.0000-0 ~ 1.0000-0	6.0898+0	6.3205+0							9.2802+0	0.0000+0		0.0000+0	8.1854-9
1.0000-0 ~ 1.0000-0	6.0897+0	6.3204+0							8.3625+0	0.0000+0		0.0000+0	8.2017-9
1.0000-0 ~ 1.0000-0	6.0896+0	6.3203+0							7.4448+0	0.0000+0		0.0000+0	8.2180-9
1.0000-0 ~ 1.0000-0	6.0895+0	6.3202+0							6.5271+0	0.0000+0		0.0000+0	8.2343-9
1.0000-0 ~ 1.0000-0	6.0894+0	6.3201+0							5.6094+0	0.0000+0		0.0000+0	8.2506-9
1.0000-0 ~ 1.0000-0	6.0893+0	6.3200+0							4.6917+0	0.0000+0		0.0000+0	8.2669-9
1.0000-0 ~ 1.0000-0	6.0892+0	6.3199+0							3.7740+0	0.0000+0		0.0000+0	8.2832-9
1.0000-0 ~ 1.0000-0	6.0891+0	6.3198+0							2.8563+0	0.0000+0		0.0000+0	8.2995-9
1.0000-0 ~ 1.0000-0	6.0890+0	6.3197+0							1.9386+0	0.0000+0		0.0000+0	8.3158-9
1.0000-0 ~ 1.0000-0	6.0889+0	6.3196+0							1.0209+0	0.0000+0		0.0000+0	8.3321-9
1.0000-0 ~ 1.0000-0	6.0888+0	6.3195+0							0.1032+0	0.0000+0		0.0000+0	8.3484-9
1.0000-0 ~ 1.0000-0	6.0887+0	6.3194+0							9.1855+0	0.0000+0		0.0000+0	8.3647-9
1.0000-0 ~ 1.0000-0	6.0886+0	6.3193+0							8.2678+0	0.0000+0		0.0000+0	8.3810-9
1.0000-0 ~ 1.0000-0	6.0885+0	6.3192+0							7.3501+0	0.0000+0		0.0000+0	8.3973-9
1.0000-0 ~ 1.0000-0	6.0884+0	6.3191+0							6.4324+0	0.0000+0		0.0000+0	8.4136-9
1.0000-0 ~ 1.0000-0	6.0883+0	6.3190+0							5.5147+0	0.0000+0		0.0000+0	8.4299-9
1.0000-0 ~ 1.0000-0	6.0882+0	6.3189+0							4.5970+0	0.0000+0		0.0000+0	8.4462-9
1.0000-0 ~ 1.0000-0	6.0881+0	6.3188+0							3.6793+0	0.0000+0		0.0000+0	8.4625-9
1.0000-0 ~ 1.0000-0	6.0880+0	6.3187+0							2.7616+0	0.0000+0		0.0000+0	8.4788-9
1.0000-0 ~ 1.0000-0	6.0879+0	6.3186+0							1.8439+0	0.0000+0		0.0000+0	8.4951-9
1.0000-0 ~ 1.0000-0	6.0878+0	6.3185+0							0.9262+0	0.0000+0		0.0000+0	8.5114-9
1.0000-0 ~ 1.0000-0	6.0877+0	6.3184+0							0.0085+0	0.0000+0		0.0000+0	8.5277-9
1.0000-0 ~ 1.0000-0	6.0876+0	6.3183+0							9.0908+0	0.0000+0		0.0000+0	8.5440-9
1.0000-0 ~ 1.0000-0	6.0875+0	6.3182+0							8.1731+0	0.0000+0		0.0000+0	8.5603-9
1.0000-0 ~ 1.0000-0	6.0874+0	6.3181+0							7.2554+0	0.0000+0		0.0000+0	8.5766-9
1.0000-0 ~ 1.0000-0	6.0873+0	6.3180+0							6.3377+0	0.0000+0		0.0000+0	8.5929-9
1.0000-0 ~ 1.0000-0	6.0872+0	6.3179+0							5.4200+0	0.0000+0		0.0000+0	8.6092-9
1.0000-0 ~ 1.0000-0	6.0871+0	6.3178+0											

CROSS SECTION

MO-82

MATERIAL	ENERGY	TOTAL	ELASTIC	INEL	(N.2N)	(N.2N)	FISSON	(N.MP)	(N.NPI)	CAPTURE	(N.P)	(H.O)	(N.P)	(N.P)	MU-SR
1.0000	5 ~ 1.0000-2	5.6095+0	5.5452+0							6.4215-2	0.0000+0		0.0000+0	7.3656-3	
1.5000	1 ~ 1.5000-1	5.5751+0	5.5452+0							2.9815-2	0.0000+0		0.0000+0	7.3973-3	
2.0000	2 ~ 2.0000-2	5.5703+0	5.5452+0							2.5069-2	0.0000+0		0.0000+0	7.4012-3	
3.0000	3 ~ 3.0000-3	5.5683+0	5.5452+0							1.7073-2	0.0000+0		0.0000+0	7.4062-3	
4.0000	4 ~ 4.0000-4	5.5690+0	5.5452+0							1.5734-2	0.0000+0		0.0000+0	7.4084-3	
5.0000	5 ~ 5.0000-5	5.5694+0	5.5452+0							1.4725-2	0.0000+0		0.0000+0	7.4112-3	
6.0000	6 ~ 6.0000-6	5.5678+0	5.5452+0							1.2567-2	0.0000+0		0.0000+0	7.4189-3	
8.0000	8 ~ 8.0000-8	5.5583+0	5.5452+0							1.1060-2	0.0000+0		0.0000+0	7.4189-3	
1.0000	1 ~ 1.5000-1	5.5247+0	5.5452+0							9.4422-3	0.0000+0		0.0000+0	7.4234-3	
2.0000	2 ~ 2.0000-2	5.5247+0	5.5452+0							7.9561-3	0.0000+0		0.0000+0	7.4273-3	
3.0000	3 ~ 3.0000-3	5.5219+0	5.5452+0							6.6631-3	0.0000+0		0.0000+0	7.4313-3	
4.0000	4 ~ 4.0000-4	5.5208+0	5.5452+0							5.6200-3	0.0000+0		0.0000+0	7.4362-3	
5.0000	5 ~ 5.0000-5	5.5201+0	5.5452+0							4.9441-3	0.0000+0		0.0000+0	7.4380-3	
6.0000	6 ~ 6.0000-6	5.5197+0	5.5452+0							3.5743-3	0.0000+0		0.0000+0	7.4403-3	
8.0000	8 ~ 8.0000-8	5.5187+0	5.5452+0							3.0883-3	0.0000+0		0.0000+0	7.4439-3	
1.0000	0 ~ 1.5000+0	5.5481+0	5.5451+0							2.9857-3	0.0000+0		0.0000+0	7.4486-3	
1.5000	0 ~ 2.0000+0	5.5476+0	5.5451+0							2.5159-3	0.0000+0		0.0000+0	7.4534-3	
2.0000	0 ~ 3.0000+0	5.5470+0	5.5450+0							1.7843-3	0.0000+0		0.0000+0	7.4573-3	
3.0000	0 ~ 4.0000+0	5.5464+0	5.5448+0							1.5786-3	0.0000+0		0.0000+0	7.4611-3	
4.0000	0 ~ 5.0000+0	5.5458+0	5.5447+0							1.4269-3	0.0000+0		0.0000+0	7.4654-3	
5.0000	0 ~ 6.0000+0	5.5452+0	5.5446+0							1.2694-3	0.0000+0		0.0000+0	7.4691-3	
6.0000	0 ~ 8.0000+0	5.5445+0	5.5444+0							1.1252-3	0.0000+0		0.0000+0	7.4720-3	
1.0000	1 ~ 1.5000+1	5.5450+0	5.5441+0							9.6184-4	0.0000+0		0.0000+0	7.4757-3	
1.5000	1 ~ 2.0000+1	5.5444+0	5.5436+0							8.1374-4	0.0000+0		0.0000+0	7.4795-3	
2.0000	1 ~ 3.0000+1	5.5436+0	5.5429+0							6.9610-4	0.0000+0		0.0000+0	7.4835-3	
3.0000	1 ~ 4.0000+1	5.5425+0	5.5419+0							5.9866-4	0.0000+0		0.0000+0	7.4874-3	
4.0000	1 ~ 5.0000+1	5.5415+0	5.5409+0							5.2075-4	0.0000+0		0.0000+0	7.4912-3	
5.0000	1 ~ 6.0000+1	5.5408+0	5.5394+0							4.5620-4	0.0000+0		0.0000+0	7.4952-3	
6.0000	1 ~ 8.0000+1	5.5397+0	5.5383+0							4.0285-4	0.0000+0		0.0000+0	7.4991-3	
1.0000	2 ~ 1.5000+2	5.5327+0	5.5323+0							4.0904-4	0.0000+0		0.0000+0	7.5018-3	
1.5000	2 ~ 2.0000+2	5.5320+0	5.5313+0							3.5276-4	0.0000+0		0.0000+0	7.5056-3	
2.0000	2 ~ 3.0000+2	5.5313+0	5.5303+0							3.0576-4	0.0000+0		0.0000+0	7.5094-3	
3.0000	2 ~ 4.0000+2	5.5305+0	5.5294+0							2.7224-4	0.0000+0		0.0000+0	7.5132-3	
4.0000	2 ~ 5.0000+2	5.5297+0	5.5285+0							2.4723-4	0.0000+0		0.0000+0	7.5170-3	
5.0000	2 ~ 6.0000+2	5.5288+0	5.5278+0							2.2820-4	0.0000+0		0.0000+0	7.5208-3	
6.0000	2 ~ 8.0000+2	5.5280+0	5.5270+0							1.9578-4	0.0000+0		0.0000+0	7.5246-3	
1.0000	3 ~ 1.5000+3	5.4814+0	5.4814+0							1.7446-4	0.0000+0		0.0000+0	7.5284-3	
1.5000	3 ~ 2.0000+3	5.4808+0	5.4802+0							2.0880-4	0.0000+0		0.0000+0	7.5322-3	
2.0000	3 ~ 3.0000+3	5.4801+0	5.4801+0							2.0299-4	0.0000+0		0.0000+0	7.5360-3	
3.0000	3 ~ 4.0000+3	5.4794+0	5.4804+0							1.0115-4	0.0000+0		0.0000+0	7.5398-3	
4.0000	3 ~ 5.0000+3	5.4787+0	5.4803+0							9.1256-5	0.0000+0		0.0000+0	7.5436-3	
5.0000	3 ~ 6.0000+3	5.4780+0	5.4802+0							8.1735-5	0.0000+0		0.0000+0	7.5474-3	
6.0000	3 ~ 8.0000+3	5.4773+0	5.4801+0							7.2135-5	0.0000+0		0.0000+0	7.5512-3	
1.0000	4 ~ 1.5000+4	5.4356+0	5.4356+0							2.2167-4	0.0000+0		0.0000+0	7.5550-3	
1.5000	4 ~ 2.0000+4	5.4349+0	5.4349+0							1.7476-4	0.0000+0		0.0000+0	7.5588-3	
2.0000	4 ~ 3.0000+4	5.4342+0	5.4342+0							8.5941-2	0.0000+0		0.0000+0	7.5626-3	
3.0000	4 ~ 4.0000+4	5.4335+0	5.4335+0							7.8204-2	0.0000+0		0.0000+0	7.5664-3	
4.0000	4 ~ 5.0000+4	5.4328+0	5.4328+0							7.9969-2	0.0000+0		0.0000+0	7.5702-3	
5.0000	4 ~ 6.0000+4	5.4321+0	5.4321+0							7.9600-2	0.0000+0		0.0000+0	7.5740-3	
6.0000	4 ~ 8.0000+4	5.4314+0	5.4314+0							0.0000-0	0.0000+0		0.0000+0	7.5778-3	
1.0000	5 ~ 1.5000+5	5.3512+0	5.3512+0							3.5188-2	0.0000+0		0.0000+0	7.5816-3	
1.5000	5 ~ 2.0000+5	5.3505+0	5.3505+0							3.1198-2	0.0000+0		0.0000+0	7.5854-3	
2.0000	5 ~ 3.0000+5	5.3498+0	5.3498+0							2.9449-2	0.0000+0		0.0000+0	7.5892-3	
3.0000	5 ~ 4.0000+5	5.3491+0	5.3491+0							2.8449-2	0.0000+0		0.0000+0	7.5930-3	
4.0000	5 ~ 5.0000+5	5.3484+0	5.3484+0							2.8097-2	0.0000+0		0.0000+0	7.5968-3	
5.0000	5 ~ 6.0000+5	5.3477+0	5.3477+0							2.8350-2	0.0000+0		0.0000+0	7.6006-3	
6.0000	5 ~ 8.0000+5	5.3470+0	5.3470+0							3.3500-2	0.0000+0		0.0000+0	7.6044-3	
1.0000	6 ~ 1.5000+6	5.3016+0	5.3016+0							4.2497-2	0.0000+0		0.0000+0	7.6082-3	
1.5000	6 ~ 2.0000+6	5.3009+0	5.3009+0							4.2719-2	0.0000+0		0.0000+0	7.6120-3	
2.0000	6 ~ 3.0000+6	5.3002+0	5.3002+0							3.4270-2	0.0000+0		0.0000+0	7.6158-3	
3.0000	6 ~ 4.0000+6	5.2995+0	5.2995+0							3.4820-2	0.0000+0		0.0000+0	7.6196-3	
4.0000	6 ~ 5.0000+6	5.2988+0	5.2988+0							1.4479-2	0.0000+0		0.0000+0	7.6234-3	
5.0000	6 ~ 6.0000+6	5.2981+0	5.2981+0							1.4772-2	0.0000+0		0.0000+0	7.6272-3	
6.0000	6 ~ 8.0000+6	5.2974+0	5.2974+0							1.1772-2	0.0000+0		0.0000+0	7.6310-3	
1.0000	7 ~ 1.5000+7	5.2529+0	5.2529+0							4.0420-2	0.0000+0		0.0000+0	7.6348-3	
1.5000	7 ~ 2.0000+7	5.2522+0	5.2522+0							4.0420-2	0.0000+0		0.0000+0	7.6386-3	
2.0000	7 ~ 3.0000+7	5.2515+0	5.2515+0							3.5200-2	0.0000+0		0.0000+0	7.6424-3	
3.0000	7 ~ 4.0000+7	5.2508+0	5.2508+0							3.5200-2	0.0000+0		0.0000+0	7.6462-3	
4.0000	7 ~ 5.0000+7	5.2501+0	5.2501+0							4.2497-2	0.0000+0		0.0000+0	7.6500-3	
5.0000	7 ~ 6.0000+7	5.2494+0	5.2494+0							4.2719-2	0.0000+0		0.0000+0	7.6538-3	
6.0000	7 ~ 8.0000+7	5.2487+0	5.2487+0							3.4270-2	0.0000+0		0.0000+0	7.6576-3	
1.0000	8 ~ 1.5000+8	5.2031+0	5.2031+0							3.4820-2	0.0000+0		0.0000+0	7.6614-3	
1.5000	8 ~ 2.0000+8	5.2024+0	5.2024+0							1.4479-2	0.0000+0		0.0000+0	7.6652-3	
2.0000	8 ~ 3.0000+8	5.2017+0	5.2017+0							1.4772-2	0.0000+0		0.0000+0	7.6690-3	
3.0000	8 ~ 4.0000+8	5.2010+0	5.2010+0							1.1772-2	0.0000+0		0.0000+0	7.6728-3	
4.0000	8 ~ 5.0000+8	5.2003+0	5.2003+0							1.0420-2	0.0000+0		0.0000+0	7.6766-3	
5.0000	8 ~ 6.0000+8	5.2000+0	5.2000+0							4.0420-2	0.0000+0		0.0000+0	7.6804-3	
6.0000	8 ~ 8.0000+8	5.1993+0	5.1993+0							4.0420-2	0.0000+0		0.0000+0	7.6842-3	
1.0000	9 ~ 1.5000														

CROSS SECTION

MATERIAL = 2422

MO-94

ENERGY	TOTAL	ELASTIC	INELA	(N,2d)	(N,3N)	FISSION	(N,NR)	(N,NP)	CAPTURE	(N,P)	(N,D)	(N,A)	MU-BRR
1.0000+ 0	6.0365+ 0	5.9980+ 0							4.0668- 2			0.0000+ 0	7.2475- 3
1.5000+ 0	6.0188+ 0	5.9880+ 0							1.5835- 2			0.0000+ 0	7.2516- 3
2.0000+ 0	6.0139+ 0	5.9830+ 0							1.5836- 2			0.0000+ 0	7.2558- 3
3.0000+ 0	6.0091+ 0	5.9780+ 0							1.5837- 2			0.0000+ 0	7.2601- 3
4.0000+ 0	6.0043+ 0	5.9730+ 0							1.5838- 2			0.0000+ 0	7.2643- 3
5.0000+ 0	6.0000+ 0	5.9680+ 0							1.5839- 2			0.0000+ 0	7.2686- 3
6.0000+ 0	6.0059+ 0	5.9739+ 0							1.5840- 2			0.0000+ 0	7.2728- 3
8.0000+ 0	6.0050+ 0	5.9729+ 0							1.5841- 2			0.0000+ 0	7.2771- 3
1.0000+ 0	6.0039+ 0	5.9679+ 0							1.5842- 2			0.0000+ 0	7.2813- 3
1.5000+ 0	6.0021+ 0	5.9661+ 0							1.5843- 2			0.0000+ 0	7.2855- 3
2.0000+ 0	6.0015+ 0	5.9655+ 0							1.5844- 2			0.0000+ 0	7.2897- 3
3.0000+ 0	6.0010+ 0	5.9650+ 0							1.5845- 2			0.0000+ 0	7.2939- 3
4.0000+ 0	6.0007+ 0	5.9647+ 0							1.5846- 2			0.0000+ 0	7.2981- 3
5.0000+ 0	6.0004+ 0	5.9644+ 0							1.5847- 2			0.0000+ 0	7.3023- 3
6.0000+ 0	6.0001+ 0	5.9641+ 0							1.5848- 2			0.0000+ 0	7.3065- 3
8.0000+ 0	6.0000+ 0	5.9640+ 0							1.5849- 2			0.0000+ 0	7.3107- 3
1.0000+ 0	6.0000+ 0	5.9639+ 0							1.5850- 2			0.0000+ 0	7.3149- 3
1.5000+ 0	6.0000+ 0	5.9638+ 0							1.5851- 2			0.0000+ 0	7.3191- 3
2.0000+ 0	6.0000+ 0	5.9637+ 0							1.5852- 2			0.0000+ 0	7.3233- 3
3.0000+ 0	6.0000+ 0	5.9636+ 0							1.5853- 2			0.0000+ 0	7.3275- 3
4.0000+ 0	6.0000+ 0	5.9635+ 0							1.5854- 2			0.0000+ 0	7.3317- 3
5.0000+ 0	6.0000+ 0	5.9634+ 0							1.5855- 2			0.0000+ 0	7.3359- 3
6.0000+ 0	6.0000+ 0	5.9633+ 0							1.5856- 2			0.0000+ 0	7.3401- 3
8.0000+ 0	6.0000+ 0	5.9632+ 0							1.5857- 2			0.0000+ 0	7.3443- 3
1.0000+ 0	6.0000+ 0	5.9631+ 0							1.5858- 2			0.0000+ 0	7.3485- 3
1.5000+ 0	6.0000+ 0	5.9630+ 0							1.5859- 2			0.0000+ 0	7.3527- 3
2.0000+ 0	6.0000+ 0	5.9629+ 0							1.5860- 2			0.0000+ 0	7.3569- 3
3.0000+ 0	6.0000+ 0	5.9628+ 0							1.5861- 2			0.0000+ 0	7.3611- 3
4.0000+ 0	6.0000+ 0	5.9627+ 0							1.5862- 2			0.0000+ 0	7.3653- 3
5.0000+ 0	6.0000+ 0	5.9626+ 0							1.5863- 2			0.0000+ 0	7.3695- 3
6.0000+ 0	6.0000+ 0	5.9625+ 0							1.5864- 2			0.0000+ 0	7.3737- 3
8.0000+ 0	6.0000+ 0	5.9624+ 0							1.5865- 2			0.0000+ 0	7.3779- 3
1.0000+ 0	6.0000+ 0	5.9623+ 0							1.5866- 2			0.0000+ 0	7.3821- 3
1.5000+ 0	6.0000+ 0	5.9622+ 0							1.5867- 2			0.0000+ 0	7.3863- 3
2.0000+ 0	6.0000+ 0	5.9621+ 0							1.5868- 2			0.0000+ 0	7.3905- 3
3.0000+ 0	6.0000+ 0	5.9620+ 0							1.5869- 2			0.0000+ 0	7.3947- 3
4.0000+ 0	6.0000+ 0	5.9619+ 0							1.5870- 2			0.0000+ 0	7.3989- 3
5.0000+ 0	6.0000+ 0	5.9618+ 0							1.5871- 2			0.0000+ 0	7.4031- 3
6.0000+ 0	6.0000+ 0	5.9617+ 0							1.5872- 2			0.0000+ 0	7.4073- 3
8.0000+ 0	6.0000+ 0	5.9616+ 0							1.5873- 2			0.0000+ 0	7.4115- 3
1.0000+ 0	6.0000+ 0	5.9615+ 0							1.5874- 2			0.0000+ 0	7.4157- 3
1.5000+ 0	6.0000+ 0	5.9614+ 0							1.5875- 2			0.0000+ 0	7.4199- 3
2.0000+ 0	6.0000+ 0	5.9613+ 0							1.5876- 2			0.0000+ 0	7.4241- 3
3.0000+ 0	6.0000+ 0	5.9612+ 0							1.5877- 2			0.0000+ 0	7.4283- 3
4.0000+ 0	6.0000+ 0	5.9611+ 0							1.5878- 2			0.0000+ 0	7.4325- 3
5.0000+ 0	6.0000+ 0	5.9610+ 0							1.5879- 2			0.0000+ 0	7.4367- 3
6.0000+ 0	6.0000+ 0	5.9609+ 0							1.5880- 2			0.0000+ 0	7.4409- 3
8.0000+ 0	6.0000+ 0	5.9608+ 0							1.5881- 2			0.0000+ 0	7.4451- 3
1.0000+ 0	6.0000+ 0	5.9607+ 0							1.5882- 2			0.0000+ 0	7.4493- 3
1.5000+ 0	6.0000+ 0	5.9606+ 0							1.5883- 2			0.0000+ 0	7.4535- 3
2.0000+ 0	6.0000+ 0	5.9605+ 0							1.5884- 2			0.0000+ 0	7.4577- 3
3.0000+ 0	6.0000+ 0	5.9604+ 0							1.5885- 2			0.0000+ 0	7.4619- 3
4.0000+ 0	6.0000+ 0	5.9603+ 0							1.5886- 2			0.0000+ 0	7.4661- 3
5.0000+ 0	6.0000+ 0	5.9602+ 0							1.5887- 2			0.0000+ 0	7.4703- 3
6.0000+ 0	6.0000+ 0	5.9601+ 0							1.5888- 2			0.0000+ 0	7.4745- 3
8.0000+ 0	6.0000+ 0	5.9600+ 0							1.5889- 2			0.0000+ 0	7.4787- 3
1.0000+ 0	6.0000+ 0	5.9599+ 0							1.5890- 2			0.0000+ 0	7.4829- 3
1.5000+ 0	6.0000+ 0	5.9598+ 0							1.5891- 2			0.0000+ 0	7.4871- 3
2.0000+ 0	6.0000+ 0	5.9597+ 0							1.5892- 2			0.0000+ 0	7.4913- 3
3.0000+ 0	6.0000+ 0	5.9596+ 0							1.5893- 2			0.0000+ 0	7.4955- 3
4.0000+ 0	6.0000+ 0	5.9595+ 0							1.5894- 2			0.0000+ 0	7.4997- 3
5.0000+ 0	6.0000+ 0	5.9594+ 0							1.5895- 2			0.0000+ 0	7.5039- 3
6.0000+ 0	6.0000+ 0	5.9593+ 0							1.5896- 2			0.0000+ 0	7.5081- 3
8.0000+ 0	6.0000+ 0	5.9592+ 0							1.5897- 2			0.0000+ 0	7.5123- 3
1.0000+ 0	6.0000+ 0	5.9591+ 0							1.5898- 2			0.0000+ 0	7.5165- 3
1.5000+ 0	6.0000+ 0	5.9590+ 0							1.5899- 2			0.0000+ 0	7.5207- 3
2.0000+ 0	6.0000+ 0	5.9589+ 0							1.5900- 2			0.0000+ 0	7.5249- 3
3.0000+ 0	6.0000+ 0	5.9588+ 0							1.5901- 2			0.0000+ 0	7.5291- 3
4.0000+ 0	6.0000+ 0	5.9587+ 0							1.5902- 2			0.0000+ 0	7.5333- 3
5.0000+ 0	6.0000+ 0	5.9586+ 0							1.5903- 2			0.0000+ 0	7.5375- 3
6.0000+ 0	6.0000+ 0	5.9585+ 0							1.5904- 2			0.0000+ 0	7.5417- 3
8.0000+ 0	6.0000+ 0	5.9584+ 0							1.5905- 2			0.0000+ 0	7.5459- 3
1.0000+ 0	6.0000+ 0	5.9583+ 0							1.5906- 2			0.0000+ 0	7.5501- 3
1.5000+ 0	6.0000+ 0	5.9582+ 0							1.5907- 2			0.0000+ 0	7.5543- 3
2.0000+ 0	6.0000+ 0	5.9581+ 0							1.5908- 2			0.0000+ 0	7.5585- 3
3.0000+ 0	6.0000+ 0	5.9580+ 0							1.5909- 2			0.0000+ 0	7.5627- 3
4.0000+ 0	6.0000+ 0	5.9579+ 0							1.5910- 2			0.0000+ 0	7.5669- 3
5.0000+ 0	6.0000+ 0	5.9578+ 0							1.5911- 2			0.0000+ 0	7.5711- 3
6.0000+ 0	6.0000+ 0	5.9577+ 0							1.5912- 2			0.0000+ 0	7.5753- 3
8.0000+ 0	6.0000+ 0	5.9576+ 0							1.5913- 2			0.0000+ 0	7.5795- 3
1.0000+ 0	6.0000+ 0	5.9575+ 0							1.5914- 2			0.0000+ 0	7.5837- 3
1.5000+ 0	6.0000+ 0	5.9574+ 0							1.5915- 2			0.0000+ 0	7.5879- 3
2.0000+ 0	6.0000+ 0	5.9573+ 0							1.5916- 2			0.0000+ 0	7.5921- 3
3.0000+ 0	6.0000+ 0	5.9572+ 0							1.5917- 2			0.0000+ 0	7.5963- 3
4.0000+ 0	6.0000+ 0	5.9571+ 0							1.5918- 2			0.0000+ 0	7.6005- 3
5.0000+ 0	6.0000+ 0	5.9570+ 0							1.5919- 2			0.0000+ 0	7.6047- 3
6.0000+ 0	6.0000+ 0	5.9569+ 0							1.5920- 2			0.0000+ 0	7.6089- 3
8.0000+ 0	6.0000+ 0	5.9568+ 0							1.5921- 2			0.0000+ 0	

MATERIAL - 2423 CROSS SECTION MO-98

ENERGY	TOTAL	ELASTIC	INELR	(N.2N)	(N.3N)	FISSION	(N.NR)	(N.NP)	CAPTURE	(N.P)	(N.D)	(N.R)	MU-SRR
1.0000-5	4.6928+1	5.5877+0							4.3341+1			0.0000+0	7.1728-5
1.0000-4	2.6702+1	5.5870+0							2.0115+1			0.0000+0	7.1907-5
1.0000-3	2.4798+1	5.5868+0							1.6308+1			0.0000+0	7.1958-5
1.0000-2	1.7656+1	5.5850+0							1.4210+1			0.0000+0	7.2010-5
1.0000-1	1.6155+1	5.5841+0							1.1950+1			0.0000+0	7.2060-5
5.0000-2	1.5096+1	5.5832+0							1.0541+1			0.0000+0	7.2097-5
5.0000-1	1.4039+1	5.5818+0							8.4475+0			0.0000+0	7.2118-5
1.0000-1	1.1691+1	5.5788+0							7.4390+0			0.0000+0	7.2200-5
1.5000-1	1.0691+1	5.5724+0							5.3141+0			0.0000+0	7.2248-5
2.0000-1	1.0007+1	5.5667+0							5.3105+0			0.0000+0	7.2271-5
3.0000-1	8.7395+0	5.5620+0							3.7367+0			0.0000+0	7.2340-5
5.0000-1	8.4873+0	5.5592+0							3.2756+0			0.0000+0	7.2438-5
8.0000-1	7.7848+0	5.5282+0							2.9481+0			0.0000+0	7.2468-5
1.0000-0	7.9871+0	5.4781+0							2.6071+0			0.0000+0	7.2507-5
2.0000-0	7.7275+0	5.4381+0							2.2757+0			0.0000+0	7.2571-5
3.0000-0	6.8873+0	5.3918+0							1.9177+0			0.0000+0	7.2639-5
4.0000-0	6.3810+0	5.3018+0							1.3084+0			0.0000+0	7.2691-5
5.0000-0	5.1879+0	5.2284+0							0.9782+0			0.0000+0	7.2778-5
8.0000-0	5.9595+0	5.1573+0							8.4214+0			0.0000+0	7.2808-5
1.0000+0	5.3591+0	4.9211+0							7.4773+0			0.0000+0	7.2844-5
1.5000+0	5.3141+0	4.8912+0							6.6992+0			0.0000+0	7.2881-5
2.0000+0	5.0016+0	4.8483+0							5.2988+0			0.0000+0	7.2939-5
3.0000+0	4.7250+0	4.8078+0							4.5639+0			0.0000+0	7.3002-5
5.0000+0	4.0212+0	4.7474+0							3.9483+0			0.0000+0	7.3092-5
8.0000+0	3.5196+0	4.6891+0							3.0971+0			0.0000+0	7.3119-5
1.0000+1	3.1000+0	4.6332+0							2.0971+0			0.0000+0	7.3174-5
1.5000+1	2.8000+0	4.5800+0							1.0487+0			0.0000+0	7.3222-5
2.0000+1	2.5000+0	4.5300+0							0.2988+0			0.0000+0	7.3289-5
3.0000+1	2.2000+0	4.4847+0							0.6298+0			0.0000+0	7.3378-5
5.0000+1	2.0000+0	4.4419+0							0.8073+0			0.0000+0	7.3490-5
8.0000+1	1.8000+0	4.4021+0							0.5084+0			0.0000+0	7.3650-5
1.0000+2	1.6000+0	4.3672+0							0.3969+0			0.0000+0	7.3822-5
1.5000+2	1.5000+0	4.3354+0							1.5222+0			0.0000+0	7.3922-5
2.0000+2	1.4000+0	4.3060+0							2.0127+0			0.0000+0	7.4070-5
3.0000+2	1.3000+0	4.2791+0							3.9410+0			0.0000+0	7.4332-5
5.0000+2	1.2000+0	4.2549+0							5.5092+0			0.0000+0	7.4622-5
8.0000+2	1.1000+0	4.2328+0							5.5084+0			0.0000+0	7.4950-5
1.0000+3	1.0000+0	4.2124+0							3.3969+0			0.0000+0	7.5322-5
1.5000+3	0.9000+0	4.1934+0							2.3539+0			0.0000+0	7.5855-5
2.0000+3	0.8000+0	4.1756+0							1.6080+0			0.0000+0	8.1573-5
3.0000+3	0.7000+0	4.1597+0							1.4744+0			0.0000+0	8.1558-5
5.0000+3	0.6000+0	4.1454+0							1.2654+0			0.0000+0	8.1622-5
8.0000+3	0.5000+0	4.1325+0							1.0725+0			0.0000+0	8.1685-5
1.0000+4	0.4000+0	4.1209+0							0.8826+0			0.0000+0	8.1740-5
1.5000+4	0.3000+0	4.1104+0							0.7119+0			0.0000+0	8.1792-5
2.0000+4	0.2000+0	4.1009+0							0.5688+0			0.0000+0	8.1840-5
3.0000+4	0.1000+0	4.0924+0							0.4488+0			0.0000+0	8.1890-5
5.0000+4	0.0000+0	4.0849+0							0.3537+0			0.0000+0	8.1940-5
8.0000+4	0.0000+0	4.0784+0							0.2821+0			0.0000+0	8.2000-5
1.0000+5	0.0000+0	4.0729+0							1.0391+0			0.0000+0	8.2060-5
1.5000+5	0.0000+0	4.0684+0							1.4820+0			0.0000+0	1.0836-1
2.0000+5	0.0000+0	4.0649+0							1.2155+0			0.0000+0	1.4550-1
3.0000+5	0.0000+0	4.0624+0							0.9180+0			0.0000+0	2.2674-1
5.0000+5	0.0000+0	4.0609+0							0.7059+0			0.0000+0	3.1180-1
8.0000+5	0.0000+0	4.0604+0							0.5639+0			0.0000+0	3.4600-1
1.0000+6	0.0000+0	4.0609+0							0.4062+0			0.0000+0	4.5760-1
1.5000+6	0.0000+0	4.0614+0							0.2866+0			0.0000+0	4.8022-1
2.0000+6	0.0000+0	4.0629+0							0.1979+0			0.0000+0	5.0733-1
3.0000+6	0.0000+0	4.0654+0							0.1350+0			0.0000+0	5.2971-1
5.0000+6	0.0000+0	4.0689+0							0.0922+0			0.0000+0	5.3151-1
8.0000+6	0.0000+0	4.0734+0							0.0665+0			0.0000+0	5.3468-1
1.0000+7	0.0000+0	4.0789+0							0.0468+0			0.0000+0	5.3856-1
1.5000+7	0.0000+0	4.0844+0							0.0321+0			0.0000+0	5.4250-1
2.0000+7	0.0000+0	4.0909+0							0.0221+0			0.0000+0	5.4650-1
3.0000+7	0.0000+0	4.0984+0							0.0143+0			0.0000+0	5.5050-1
5.0000+7	0.0000+0	4.1069+0							0.0087+0			0.0000+0	5.5450-1
8.0000+7	0.0000+0	4.1164+0							0.0052+0			0.0000+0	5.5850-1
1.0000+8	0.0000+0	4.1269+0							0.0037+0			0.0000+0	5.6250-1
1.5000+8	0.0000+0	4.1384+0							0.0022+0			0.0000+0	5.6650-1
2.0000+8	0.0000+0	4.1509+0							0.0017+0			0.0000+0	5.7050-1
3.0000+8	0.0000+0	4.1644+0							0.0012+0			0.0000+0	5.7450-1
5.0000+8	0.0000+0	4.1789+0							0.0007+0			0.0000+0	5.7850-1
8.0000+8	0.0000+0	4.1944+0							0.0002+0			0.0000+0	5.8250-1
1.0000+9	0.0000+0	4.2109+0							0.0001+0			0.0000+0	5.8650-1
1.5000+9	0.0000+0	4.2284+0							0.0000+0			0.0000+0	5.9050-1
2.0000+9	0.0000+0	4.2469+0							0.0000+0			0.0000+0	5.9450-1
3.0000+9	0.0000+0	4.2664+0							0.0000+0			0.0000+0	5.9850-1
5.0000+9	0.0000+0	4.2869+0							0.0000+0			0.0000+0	6.0250-1
8.0000+9	0.0000+0	4.3084+0							0.0000+0			0.0000+0	6.0650-1
1.0000+10	0.0000+0	4.3309+0							0.0000+0			0.0000+0	6.1050-1
1.5000+10	0.0000+0	4.3544+0							0.0000+0			0.0000+0	6.1450-1
2.0000+10	0.0000+0	4.3789+0							0.0000+0			0.0000+0	6.1850-1
3.0000+10	0.0000+0	4.4044+0							0.0000+0			0.0000+0	6.2250-1
5.0000+10	0.0000+0	4.4309+0							0.0000+0			0.0000+0	6.2650-1
8.0000+10	0.0000+0	4.4584+0							0.0000+0			0.0000+0	6.3050-1
1.0000+11	0.0000+0	4.4869+0							0.0000+0			0.0000+0	6.3450-1
1.5000+11	0.0000+0	4.5164+0							0.0000+0			0.0000+0	6.3850-1
2.0000+11	0.0000+0	4.5469+0							0.0000+0			0.0000+0	6.4250-1
3.0000+11	0.0000+0	4.5784+0							0.0000+0			0.0000+0	6.4650-1
5.0000+11	0.0000+0	4.6109+0							0.0000+0			0.0000+0	6.5050-1
8.0000+11	0.0000+0	4.6444+0							0.0000+0			0.0000+0	6.5450-1
1.0000+12	0.0000+0	4.6789+0							0.0000+0			0.0000+0	6.5850-1
1.5000+12	0.0000+0	4.7144+0											

CROSS SECTION

MATERIAL = 2424

NO-88

ENERGY	TOTAL	ELASTIC	INELR	(N.2N)	(N.3N)	FISSION	(N.WA)	(N.MPI)	CAPTURE	(N.P)	(N.O)	(N.A)	KU-BAR
1.0000- 5 ~ 1.0000- 2	8.5686+ 0	4.7270+ 0						1.8418+ 0				0.0000+ 0	7.0034- 3
1.0000- 2	5.5822+ 0	4.7270+ 0						8.5620- 0				0.0000+ 0	7.0034- 3
1.0000- 2	5.4461+ 0	4.7268+ 0						7.1916- 1				0.0000+ 0	7.1023- 3
1.0000- 2	5.3119+ 0	4.7268+ 0						6.0805- 0				0.0000+ 0	7.1065- 3
1.0000- 2	5.2315+ 0	4.7268+ 0						4.5032- 1				0.0000+ 0	7.1118- 3
1.0000- 2	5.1721+ 0	4.7269+ 0						3.2075- 1				0.0000+ 0	7.1162- 3
1.0000- 2	5.0867+ 0	4.7268+ 0						3.6005- 1				0.0000+ 0	7.1191- 3
1.0000- 2	5.0448+ 0	4.7265+ 0						3.1833- 1				0.0000+ 0	7.1222- 3
1.0000- 1	4.8957+ 0	4.7263+ 0						2.7044- 1				0.0000+ 0	7.1261- 3
1.0000- 1	4.8732+ 0	4.7255+ 0						2.2786- 1				0.0000+ 0	7.1303- 3
1.0000- 1	4.8566+ 0	4.7249+ 0						1.9167- 1				0.0000+ 0	7.1346- 3
1.0000- 1	4.8466+ 0	4.7243+ 0						1.6168- 1				0.0000+ 0	7.1387- 3
1.0000- 1	4.8422+ 0	4.7237+ 0						1.4285- 1				0.0000+ 0	7.1419- 3
1.0000- 1	4.8423+ 0	4.7230+ 0						1.2707- 1				0.0000+ 0	7.1471- 3
1.0000- 1	4.8423+ 0	4.7228+ 0						1.1365- 1				0.0000+ 0	7.1502- 3
1.0000- 1	4.8423+ 0	4.7218+ 0						1.0165+ 0				0.0000+ 0	7.1562- 3
1.0000+ 0	4.8084+ 0	4.7195+ 0						8.6821- 1				0.0000+ 0	7.1641- 3
1.0000+ 0	4.7903+ 0	4.7164+ 0						7.3844- 1				0.0000+ 0	7.1682- 3
1.0000+ 0	4.7744+ 0	4.7118+ 0						5.5664- 1				0.0000+ 0	7.1723- 3
1.0000+ 0	4.7597+ 0	4.7072+ 0						4.7916- 1				0.0000+ 0	7.1764- 3
1.0000+ 0	4.7507+ 0	4.7027+ 0						4.4019- 1				0.0000+ 0	7.1805- 3
1.0000+ 0	4.7428+ 0	4.6982+ 0						4.0024- 1				0.0000+ 0	7.1846- 3
1.0000+ 0	4.7357+ 0	4.6937+ 0						3.6222- 1				0.0000+ 0	7.1887- 3
1.0000+ 0	4.7288+ 0	4.6892+ 0						3.2733- 1				0.0000+ 0	7.1928- 3
1.0000+ 0	4.7228+ 0	4.6847+ 0						2.9377- 1				0.0000+ 0	7.1969- 3
1.0000+ 0	4.7178+ 0	4.6802+ 0						2.6173- 1				0.0000+ 0	7.2010- 3
1.0000+ 0	4.7128+ 0	4.6757+ 0						2.3108- 1				0.0000+ 0	7.2051- 3
1.0000+ 0	4.7078+ 0	4.6712+ 0						2.0182- 1				0.0000+ 0	7.2092- 3
1.0000+ 0	4.7028+ 0	4.6667+ 0						1.7392- 1				0.0000+ 0	7.2133- 3
1.0000+ 0	4.6978+ 0	4.6622+ 0						1.4725- 1				0.0000+ 0	7.2174- 3
1.0000+ 0	4.6928+ 0	4.6577+ 0						1.2205+ 0				0.0000+ 0	7.2215- 3
1.0000+ 0	4.6878+ 0	4.6532+ 0						1.0000+ 0				0.0000+ 0	7.2256- 3
1.0000+ 0	4.6828+ 0	4.6487+ 0						8.2281- 1				0.0000+ 0	7.2297- 3
1.0000+ 0	4.6778+ 0	4.6442+ 0						7.2257- 1				0.0000+ 0	7.2338- 3
1.0000+ 0	4.6728+ 0	4.6397+ 0						6.2257- 1				0.0000+ 0	7.2379- 3
1.0000+ 0	4.6678+ 0	4.6352+ 0						5.2257- 1				0.0000+ 0	7.2420- 3
1.0000+ 0	4.6628+ 0	4.6307+ 0						4.2257- 1				0.0000+ 0	7.2461- 3
1.0000+ 0	4.6578+ 0	4.6262+ 0						3.2257- 1				0.0000+ 0	7.2502- 3
1.0000+ 0	4.6528+ 0	4.6217+ 0						2.2257- 1				0.0000+ 0	7.2543- 3
1.0000+ 0	4.6478+ 0	4.6172+ 0						1.2257- 1				0.0000+ 0	7.2584- 3
1.0000+ 0	4.6428+ 0	4.6127+ 0						0.2257- 1				0.0000+ 0	7.2625- 3
1.0000+ 0	4.6378+ 0	4.6082+ 0						0.2257- 1				0.0000+ 0	7.2666- 3
1.0000+ 0	4.6328+ 0	4.6037+ 0						0.2257- 1				0.0000+ 0	7.2707- 3
1.0000+ 0	4.6278+ 0	4.5992+ 0						0.2257- 1				0.0000+ 0	7.2748- 3
1.0000+ 0	4.6228+ 0	4.5947+ 0						0.2257- 1				0.0000+ 0	7.2789- 3
1.0000+ 0	4.6178+ 0	4.5902+ 0						0.2257- 1				0.0000+ 0	7.2830- 3
1.0000+ 0	4.6128+ 0	4.5857+ 0						0.2257- 1				0.0000+ 0	7.2871- 3
1.0000+ 0	4.6078+ 0	4.5812+ 0						0.2257- 1				0.0000+ 0	7.2912- 3
1.0000+ 0	4.6028+ 0	4.5767+ 0						0.2257- 1				0.0000+ 0	7.2953- 3
1.0000+ 0	4.5978+ 0	4.5722+ 0						0.2257- 1				0.0000+ 0	7.2994- 3
1.0000+ 0	4.5928+ 0	4.5677+ 0						0.2257- 1				0.0000+ 0	7.3035- 3
1.0000+ 0	4.5878+ 0	4.5632+ 0						0.2257- 1				0.0000+ 0	7.3076- 3
1.0000+ 0	4.5828+ 0	4.5587+ 0						0.2257- 1				0.0000+ 0	7.3117- 3
1.0000+ 0	4.5778+ 0	4.5542+ 0						0.2257- 1				0.0000+ 0	7.3158- 3
1.0000+ 0	4.5728+ 0	4.5497+ 0						0.2257- 1				0.0000+ 0	7.3199- 3
1.0000+ 0	4.5678+ 0	4.5452+ 0						0.2257- 1				0.0000+ 0	7.3240- 3
1.0000+ 0	4.5628+ 0	4.5407+ 0						0.2257- 1				0.0000+ 0	7.3281- 3
1.0000+ 0	4.5578+ 0	4.5362+ 0						0.2257- 1				0.0000+ 0	7.3322- 3
1.0000+ 0	4.5528+ 0	4.5317+ 0						0.2257- 1				0.0000+ 0	7.3363- 3
1.0000+ 0	4.5478+ 0	4.5272+ 0						0.2257- 1				0.0000+ 0	7.3404- 3
1.0000+ 0	4.5428+ 0	4.5227+ 0						0.2257- 1				0.0000+ 0	7.3445- 3
1.0000+ 0	4.5378+ 0	4.5182+ 0						0.2257- 1				0.0000+ 0	7.3486- 3
1.0000+ 0	4.5328+ 0	4.5137+ 0						0.2257- 1				0.0000+ 0	7.3527- 3
1.0000+ 0	4.5278+ 0	4.5092+ 0						0.2257- 1				0.0000+ 0	7.3568- 3
1.0000+ 0	4.5228+ 0	4.5047+ 0						0.2257- 1				0.0000+ 0	7.3609- 3
1.0000+ 0	4.5178+ 0	4.5002+ 0						0.2257- 1				0.0000+ 0	7.3650- 3
1.0000+ 0	4.5128+ 0	4.4957+ 0						0.2257- 1				0.0000+ 0	7.3691- 3
1.0000+ 0	4.5078+ 0	4.4912+ 0						0.2257- 1				0.0000+ 0	7.3732- 3
1.0000+ 0	4.5028+ 0	4.4867+ 0						0.2257- 1				0.0000+ 0	7.3773- 3
1.0000+ 0	4.4978+ 0	4.4822+ 0						0.2257- 1				0.0000+ 0	7.3814- 3
1.0000+ 0	4.4928+ 0	4.4777+ 0						0.2257- 1				0.0000+ 0	7.3855- 3
1.0000+ 0	4.4878+ 0	4.4732+ 0						0.2257- 1				0.0000+ 0	7.3896- 3
1.0000+ 0	4.4828+ 0	4.4687+ 0						0.2257- 1				0.0000+ 0	7.3937- 3
1.0000+ 0	4.4778+ 0	4.4642+ 0						0.2257- 1				0.0000+ 0	7.3978- 3
1.0000+ 0	4.4728+ 0	4.4597+ 0						0.2257- 1				0.0000+ 0	7.4019- 3
1.0000+ 0	4.4678+ 0	4.4552+ 0						0.2257- 1				0.0000+ 0	7.4060- 3
1.0000+ 0	4.4628+ 0	4.4507+ 0						0.2257- 1				0.0000+ 0	7.4101- 3
1.0000+ 0	4.4578+ 0	4.4462+ 0						0.2257- 1				0.0000+ 0	7.4142- 3
1.0000+ 0	4.4528+ 0	4.4417+ 0						0.2257- 1				0.0000+ 0	7.4183- 3
1.0000+ 0	4.4478+ 0	4.4372+ 0						0.2257- 1				0.0000+ 0	7.4224- 3
1.0000+ 0	4.4428+ 0	4.4327+ 0						0.2257- 1				0.0000+ 0	7.4265- 3
1.0000+ 0	4.4378+ 0	4.4282+ 0						0.2257- 1				0.0000+ 0	7.4306- 3
1.0000+ 0	4.4328+ 0	4.4237+ 0						0.2257- 1				0.0000+ 0	7.4347- 3
1.0000+ 0	4.4278+ 0	4.4192+ 0						0.2257- 1				0.0000+ 0	7.4388- 3
1.0000+ 0	4.4228+ 0	4.4147+ 0						0.2257- 1				0.0000+ 0	7.4429- 3
1.0000+ 0	4.4178+ 0	4.4102+ 0						0.2257- 1				0.0000+ 0	7.4470- 3
1.0000+ 0	4.4128+ 0	4.4057+ 0						0.2257- 1				0.0000+ 0	7.4511- 3
1.0000+ 0	4.4078+ 0	4.4012+ 0						0.2257- 1					

CROSS SECTION

HQ-97

MATERIAL = 2425

ENERGY	(N.2N)	(N.3H)	F165TON	(N.NA)	(N.MP)	(N.D)	(N.A)	MU-BRR
1.0000-5 ~ 1.0000-2	1.2364+ 1	5.6635+ 0	6.5108+ 0	0.0000+ 0	0.0000+ 0	0.0000+ 0	0.0000+ 0	7.0261- 9
1.0000-2 ~ 1.5000-1	8.8740+ 0	5.8534+ 0	3.0206+ 0	0.0000+ 0	0.0000+ 0	0.0000+ 0	0.0000+ 0	7.0483- 9
1.5000-1 ~ 2.0000-1	8.9610+ 0	5.8534+ 0	2.5386+ 0	0.0000+ 0	0.0000+ 0	0.0000+ 0	0.0000+ 0	7.0614- 9
2.0000-1 ~ 3.0000-1	7.8881+ 0	5.8534+ 0	2.1548+ 0	0.0000+ 0	0.0000+ 0	0.0000+ 0	0.0000+ 0	7.0667- 9
3.0000-1 ~ 4.0000-1	7.6477+ 0	5.8534+ 0	1.7848+ 0	0.0000+ 0	0.0000+ 0	0.0000+ 0	0.0000+ 0	7.0818- 9
4.0000-1 ~ 5.0000-1	7.4373+ 0	5.8534+ 0	1.5848+ 0	0.0000+ 0	0.0000+ 0	0.0000+ 0	0.0000+ 0	7.0887- 9
5.0000-1 ~ 6.0000-1	7.2616+ 0	5.8534+ 0	1.4265+ 0	0.0000+ 0	0.0000+ 0	0.0000+ 0	0.0000+ 0	7.0957- 9
6.0000-1 ~ 7.0000-1	6.9653+ 0	5.8534+ 0	1.1131+ 0	0.0000+ 0	0.0000+ 0	0.0000+ 0	0.0000+ 0	7.0761- 9
7.0000-1 ~ 8.0000-1	6.7975+ 0	5.8534+ 0	9.4579- 1	0.0000+ 0	0.0000+ 0	0.0000+ 0	0.0000+ 0	7.0890- 9
8.0000-1 ~ 9.0000-1	6.6426+ 0	5.8534+ 0	6.6066- 1	0.0000+ 0	0.0000+ 0	0.0000+ 0	0.0000+ 0	7.0914- 9
9.0000-1 ~ 1.0000-0	6.3971+ 0	5.8534+ 0	5.5146- 1	0.0000+ 0	0.0000+ 0	0.0000+ 0	0.0000+ 0	7.0966- 9
1.0000-0 ~ 2.0000-0	6.3226+ 0	5.8534+ 0	4.8901- 1	0.0000+ 0	0.0000+ 0	0.0000+ 0	0.0000+ 0	7.1093- 9
2.0000-0 ~ 3.0000-0	6.2773+ 0	5.8534+ 0	4.3197- 1	0.0000+ 0	0.0000+ 0	0.0000+ 0	0.0000+ 0	7.1093- 9
3.0000-0 ~ 4.0000-0	6.2215+ 0	5.8534+ 0	3.7294- 1	0.0000+ 0	0.0000+ 0	0.0000+ 0	0.0000+ 0	7.1093- 9
4.0000-0 ~ 5.0000-0	6.1693+ 0	5.8534+ 0	3.2594- 1	0.0000+ 0	0.0000+ 0	0.0000+ 0	0.0000+ 0	7.1107- 9
5.0000-0 ~ 6.0000-0	6.1098+ 0	5.8534+ 0	2.7137- 1	0.0000+ 0	0.0000+ 0	0.0000+ 0	0.0000+ 0	7.1156- 9
6.0000-0 ~ 7.0000-0	6.0490+ 0	5.8534+ 0	2.2038- 1	0.0000+ 0	0.0000+ 0	0.0000+ 0	0.0000+ 0	7.1207- 9
7.0000-0 ~ 8.0000-0	5.9932+ 0	5.8534+ 0	1.7402- 1	0.0000+ 0	0.0000+ 0	0.0000+ 0	0.0000+ 0	7.1261- 9
8.0000-0 ~ 9.0000-0	5.9431+ 0	5.8534+ 0	1.3201- 1	0.0000+ 0	0.0000+ 0	0.0000+ 0	0.0000+ 0	7.1346- 9
9.0000-0 ~ 1.0000+0	5.8921+ 0	5.8534+ 0	9.4760- 2	0.0000+ 0	0.0000+ 0	0.0000+ 0	0.0000+ 0	7.1379- 9
1.0000+0 ~ 2.0000+0	5.8419+ 0	5.8534+ 0	9.4760- 2	0.0000+ 0	0.0000+ 0	0.0000+ 0	0.0000+ 0	7.1415- 9
2.0000+0 ~ 3.0000+0	5.7925+ 0	5.8534+ 0	6.0756- 2	0.0000+ 0	0.0000+ 0	0.0000+ 0	0.0000+ 0	7.1483- 9
3.0000+0 ~ 4.0000+0	5.7439+ 0	5.8534+ 0	4.5345- 2	0.0000+ 0	0.0000+ 0	0.0000+ 0	0.0000+ 0	7.1502- 9
4.0000+0 ~ 5.0000+0	5.6954+ 0	5.8534+ 0	3.3691- 2	0.0000+ 0	0.0000+ 0	0.0000+ 0	0.0000+ 0	7.1553- 9
5.0000+0 ~ 6.0000+0	5.6479+ 0	5.8534+ 0	2.6870- 2	0.0000+ 0	0.0000+ 0	0.0000+ 0	0.0000+ 0	7.1605- 9
6.0000+0 ~ 7.0000+0	5.6014+ 0	5.8534+ 0	2.1088+ 2	0.0000+ 0	0.0000+ 0	0.0000+ 0	0.0000+ 0	7.1667- 9
7.0000+0 ~ 8.0000+0	5.5559+ 0	5.8534+ 0	1.6584+ 2	0.0000+ 0	0.0000+ 0	0.0000+ 0	0.0000+ 0	7.1732- 9
8.0000+0 ~ 9.0000+0	5.5114+ 0	5.8534+ 0	1.3391+ 2	0.0000+ 0	0.0000+ 0	0.0000+ 0	0.0000+ 0	7.1800- 9
9.0000+0 ~ 1.0000+1	5.4679+ 0	5.8534+ 0	1.0833+ 2	0.0000+ 0	0.0000+ 0	0.0000+ 0	0.0000+ 0	7.1886- 9
1.0000+1 ~ 2.0000+1	5.4254+ 0	5.8534+ 0	8.0333- 1	0.0000+ 0	0.0000+ 0	0.0000+ 0	0.0000+ 0	7.1983- 9
2.0000+1 ~ 3.0000+1	5.3839+ 0	5.8534+ 0	6.0333- 1	0.0000+ 0	0.0000+ 0	0.0000+ 0	0.0000+ 0	7.2004- 9
3.0000+1 ~ 4.0000+1	5.3424+ 0	5.8534+ 0	4.3603+ 0	0.0000+ 0	0.0000+ 0	0.0000+ 0	0.0000+ 0	7.2024- 9
4.0000+1 ~ 5.0000+1	5.3010+ 0	5.8534+ 0	3.2826+ 0	0.0000+ 0	0.0000+ 0	0.0000+ 0	0.0000+ 0	7.2072- 9
5.0000+1 ~ 6.0000+1	5.2606+ 0	5.8534+ 0	2.3630+ 0	0.0000+ 0	0.0000+ 0	0.0000+ 0	0.0000+ 0	7.2108- 9
6.0000+1 ~ 7.0000+1	5.2212+ 0	5.8534+ 0	1.8398+ 0	0.0000+ 0	0.0000+ 0	0.0000+ 0	0.0000+ 0	7.2146- 9
7.0000+1 ~ 8.0000+1	5.1828+ 0	5.8534+ 0	1.4388+ 0	0.0000+ 0	0.0000+ 0	0.0000+ 0	0.0000+ 0	7.2184- 9
8.0000+1 ~ 9.0000+1	5.1454+ 0	5.8534+ 0	1.1185+ 0	0.0000+ 0	0.0000+ 0	0.0000+ 0	0.0000+ 0	7.2222- 9
9.0000+1 ~ 1.0000+2	5.1090+ 0	5.8534+ 0	8.8944+ 0	0.0000+ 0	0.0000+ 0	0.0000+ 0	0.0000+ 0	7.2260- 9
1.0000+2 ~ 2.0000+2	5.0736+ 0	5.8534+ 0	6.8944+ 0	0.0000+ 0	0.0000+ 0	0.0000+ 0	0.0000+ 0	7.2298- 9
2.0000+2 ~ 3.0000+2	5.0392+ 0	5.8534+ 0	5.2524+ 0	0.0000+ 0	0.0000+ 0	0.0000+ 0	0.0000+ 0	7.2336- 9
3.0000+2 ~ 4.0000+2	5.0058+ 0	5.8534+ 0	4.0288+ 0	0.0000+ 0	0.0000+ 0	0.0000+ 0	0.0000+ 0	7.2374- 9
4.0000+2 ~ 5.0000+2	4.9734+ 0	5.8534+ 0	3.0071+ 0	0.0000+ 0	0.0000+ 0	0.0000+ 0	0.0000+ 0	7.2412- 9
5.0000+2 ~ 6.0000+2	4.9420+ 0	5.8534+ 0	2.2279+ 0	0.0000+ 0	0.0000+ 0	0.0000+ 0	0.0000+ 0	7.2450- 9
6.0000+2 ~ 7.0000+2	4.9116+ 0	5.8534+ 0	1.7267+ 0	0.0000+ 0	0.0000+ 0	0.0000+ 0	0.0000+ 0	7.2488- 9
7.0000+2 ~ 8.0000+2	4.8822+ 0	5.8534+ 0	1.3037+ 0	0.0000+ 0	0.0000+ 0	0.0000+ 0	0.0000+ 0	7.2526- 9
8.0000+2 ~ 9.0000+2	4.8538+ 0	5.8534+ 0	1.0000+ 0	0.0000+ 0	0.0000+ 0	0.0000+ 0	0.0000+ 0	7.2564- 9
9.0000+2 ~ 1.0000+3	4.8264+ 0	5.8534+ 0	8.8944+ 0	0.0000+ 0	0.0000+ 0	0.0000+ 0	0.0000+ 0	7.2602- 9
1.0000+3 ~ 2.0000+3	4.8000+ 0	5.8534+ 0	6.8944+ 0	0.0000+ 0	0.0000+ 0	0.0000+ 0	0.0000+ 0	7.2640- 9
2.0000+3 ~ 3.0000+3	4.7746+ 0	5.8534+ 0	5.2524+ 0	0.0000+ 0	0.0000+ 0	0.0000+ 0	0.0000+ 0	7.2678- 9
3.0000+3 ~ 4.0000+3	4.7500+ 0	5.8534+ 0	4.0288+ 0	0.0000+ 0	0.0000+ 0	0.0000+ 0	0.0000+ 0	7.2716- 9
4.0000+3 ~ 5.0000+3	4.7264+ 0	5.8534+ 0	3.0071+ 0	0.0000+ 0	0.0000+ 0	0.0000+ 0	0.0000+ 0	7.2754- 9
5.0000+3 ~ 6.0000+3	4.7038+ 0	5.8534+ 0	2.2279+ 0	0.0000+ 0	0.0000+ 0	0.0000+ 0	0.0000+ 0	7.2792- 9
6.0000+3 ~ 7.0000+3	4.6822+ 0	5.8534+ 0	1.7267+ 0	0.0000+ 0	0.0000+ 0	0.0000+ 0	0.0000+ 0	7.2830- 9
7.0000+3 ~ 8.0000+3	4.6616+ 0	5.8534+ 0	1.3037+ 0	0.0000+ 0	0.0000+ 0	0.0000+ 0	0.0000+ 0	7.2868- 9
8.0000+3 ~ 9.0000+3	4.6420+ 0	5.8534+ 0	1.0000+ 0	0.0000+ 0	0.0000+ 0	0.0000+ 0	0.0000+ 0	7.2906- 9
9.0000+3 ~ 1.0000+4	4.6234+ 0	5.8534+ 0	8.8944+ 0	0.0000+ 0	0.0000+ 0	0.0000+ 0	0.0000+ 0	7.2944- 9
1.0000+4 ~ 2.0000+4	4.6058+ 0	5.8534+ 0	6.8944+ 0	0.0000+ 0	0.0000+ 0	0.0000+ 0	0.0000+ 0	7.2982- 9
2.0000+4 ~ 3.0000+4	4.5892+ 0	5.8534+ 0	5.2524+ 0	0.0000+ 0	0.0000+ 0	0.0000+ 0	0.0000+ 0	7.3020- 9
3.0000+4 ~ 4.0000+4	4.5736+ 0	5.8534+ 0	4.0288+ 0	0.0000+ 0	0.0000+ 0	0.0000+ 0	0.0000+ 0	7.3058- 9
4.0000+4 ~ 5.0000+4	4.5590+ 0	5.8534+ 0	3.0071+ 0	0.0000+ 0	0.0000+ 0	0.0000+ 0	0.0000+ 0	7.3096- 9
5.0000+4 ~ 6.0000+4	4.5454+ 0	5.8534+ 0	2.2279+ 0	0.0000+ 0	0.0000+ 0	0.0000+ 0	0.0000+ 0	7.3134- 9
6.0000+4 ~ 7.0000+4	4.5328+ 0	5.8534+ 0	1.7267+ 0	0.0000+ 0	0.0000+ 0	0.0000+ 0	0.0000+ 0	7.3172- 9
7.0000+4 ~ 8.0000+4	4.5212+ 0	5.8534+ 0	1.3037+ 0	0.0000+ 0	0.0000+ 0	0.0000+ 0	0.0000+ 0	7.3210- 9
8.0000+4 ~ 9.0000+4	4.5106+ 0	5.8534+ 0	1.0000+ 0	0.0000+ 0	0.0000+ 0	0.0000+ 0	0.0000+ 0	7.3248- 9
9.0000+4 ~ 1.0000+5	4.5010+ 0	5.8534+ 0	8.8944+ 0	0.0000+ 0	0.0000+ 0	0.0000+ 0	0.0000+ 0	7.3286- 9
1.0000+5 ~ 2.0000+5	4.4924+ 0	5.8534+ 0	6.8944+ 0	0.0000+ 0	0.0000+ 0	0.0000+ 0	0.0000+ 0	7.3324- 9
2.0000+5 ~ 3.0000+5	4.4848+ 0	5.8534+ 0	5.2524+ 0	0.0000+ 0	0.0000+ 0	0.0000+ 0	0.0000+ 0	7.3362- 9
3.0000+5 ~ 4.0000+5	4.4782+ 0	5.8534+ 0	4.0288+ 0	0.0000+ 0	0.0000+ 0	0.0000+ 0	0.0000+ 0	7.3400- 9
4.0000+5 ~ 5.0000+5	4.4726+ 0	5.8534+ 0	3.0071+ 0	0.0000+ 0	0.0000+ 0	0.0000+ 0	0.0000+ 0	7.3438- 9
5.0000+5 ~ 6.0000+5	4.4680+ 0	5.8534+ 0	2.2279+ 0	0.0000+ 0	0.0000+ 0	0.0000+ 0	0.0000+ 0	7.3476- 9
6.0000+5 ~ 7.0000+5	4.4644+ 0	5.8534+ 0	1.7267+ 0	0.0000+ 0	0.0000+ 0	0.0000+ 0	0.0000+ 0	7.3514- 9
7.0000+5 ~ 8.0000+5	4.4618+ 0	5.8534+ 0	1.3037+ 0	0.0000+ 0	0.0000+ 0	0.0000+ 0	0.0000+ 0	7.3552- 9
8.0000+5 ~ 9.0000+5	4.4602+ 0	5.8534+ 0	1.0000+ 0	0.0000+ 0	0.0000+ 0	0.0000+ 0	0.0000+ 0	7.3590- 9
9.0000+5 ~ 1.0000+6	4.4596+ 0	5.8534+ 0	8.8944+ 0	0.0000+ 0	0.0000+ 0	0.0000+ 0	0.0000+ 0	7.3628- 9
1.0000+6 ~ 2.0000+6	4.4590+ 0	5.8534+ 0	6.8944+ 0	0.0000+ 0	0.0000+ 0	0.0000+ 0	0.0000+ 0	7.3666- 9
2.0000+6 ~ 3.0000+6	4.4584+ 0	5.8534+ 0	5.2524+ 0	0.0000+ 0	0.0000+ 0	0.0000+ 0	0.0000+ 0	7.3704- 9
3.0000+6 ~ 4.0000+6	4.4578+ 0	5.8534+ 0	4.0288+ 0	0.0000+ 0	0.0000+ 0	0.0000+ 0	0.0000+ 0	7.3742- 9
4.0000+6 ~ 5.0000+6	4.4572+ 0	5.8534+ 0	3.0071+ 0	0.0000+ 0	0.0000+ 0	0.0000+ 0	0.0000+ 0	7.3780- 9
5.0000+6 ~ 6.0000+6	4.4566+ 0	5.8534+ 0	2.2279+ 0	0.0000+ 0	0.0000+ 0	0.0000+ 0	0.0000+ 0	7.3818- 9
6.0000+6 ~ 7.0000+6	4.4560+ 0	5.8534+ 0	1.7267+ 0	0.0000+ 0	0.0000+ 0	0.0000+ 0	0.0000+ 0	7.3856- 9
7.0000+6 ~ 8.0000+6	4.4554+ 0	5.8534+ 0	1.3037+ 0</					

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CROSS SECTION

MATERIAL =2426	ENERGY	TOTAL	ELASTIC	INEL	(N,2N)	(N,3N)	FISSDN	(H,NR)	(N,MP)	CAPTURE	(N,P)	(N,D)	(N,A)	MU-BAR
1.0000-6	1.0000-2	5.0439+0	5.6418+0							4.0187-1			0.0000+0	6.9401-5
1.0000-4	1.5000-2	5.5285+0	5.6418+0							1.6865-1			0.0000+0	8.8647-5
1.0000-3	2.0000-2	5.6418+0	5.6418+0							1.5697-1			0.0000+0	9.299-5
1.0000-2	3.0000-2	5.6418+0	5.6418+0							1.3702-1			0.0000+0	9.867-5
1.0000-1	4.0000-2	5.6418+0	5.6418+0							9.8157-1			0.0000+0	9.9703-5
1.0000-0	5.0000-2	5.6418+0	5.6418+0							9.8157-1			0.0000+0	9.9703-5
1.0000-0	6.0000-2	5.6418+0	5.6418+0							6.8681-2			0.0000+0	8.8787-5
1.0000-0	7.0000-2	5.6418+0	5.6418+0							6.8681-2			0.0000+0	8.8787-5
1.0000-0	8.0000-2	5.6418+0	5.6418+0							5.9142			0.0000+0	8.9827-5
1.0000-0	9.0000-2	5.6417+0	5.6417+0							5.0005			0.0000+0	8.9866-5
1.0000-0	1.0000-1	5.6417+0	5.6417+0							4.2020			0.0000+0	8.9911-5
1.0000-0	2.0000-1	5.6414+0	5.6414+0							3.5639			0.0000+0	8.9952-5
1.0000-0	3.0000-1	5.6413+0	5.6413+0							3.1482			0.0000+0	8.9997-5
1.0000-0	4.0000-1	5.6412+0	5.6412+0							2.5998			0.0000+0	9.0007-5
1.0000-0	5.0000-1	5.6410+0	5.6410+0							2.2288			0.0000+0	9.0036-5
1.0000-0	6.0000-1	5.6407+0	5.6407+0							1.9703			0.0000+0	9.0067-5
1.0000-0	7.0000-1	5.6399+0	5.6399+0							1.8728			0.0000+0	9.0107-5
1.0000-0	8.0000-1	5.6395+0	5.6395+0							1.7096			0.0000+0	9.0149-5
1.0000-0	9.0000-1	5.6393+0	5.6393+0							1.5668			0.0000+0	9.0190-5
1.0000-0	1.0000-0	5.6392+0	5.6392+0							1.3933			0.0000+0	9.0231-5
1.0000-0	2.0000-0	5.6392+0	5.6392+0							1.2491			0.0000+0	9.0262-5
1.0000-0	3.0000-0	5.6392+0	5.6392+0							1.1970			0.0000+0	9.0298-5
1.0000-0	4.0000-0	5.6392+0	5.6392+0							1.1503			0.0000+0	9.0334-5
1.0000-0	5.0000-0	5.6392+0	5.6392+0							1.1091			0.0000+0	9.0368-5
1.0000-0	6.0000-0	5.6392+0	5.6392+0							1.0681			0.0000+0	9.0401-5
1.0000-0	7.0000-0	5.6392+0	5.6392+0							1.0285			0.0000+0	9.0432-5
1.0000-0	8.0000-0	5.6392+0	5.6392+0							9.9476+0			0.0000+0	9.0462-5
1.0000-0	9.0000-0	5.6392+0	5.6392+0							2.4758			0.0000+0	9.0491-5
1.0000-0	1.0000+1	5.6392+0	5.6392+0							1.412			0.0000+0	9.0519-5
1.0000-0	2.0000+1	5.6392+0	5.6392+0							3.0974			0.0000+0	9.0541-5
1.0000-0	3.0000+1	5.6392+0	5.6392+0							3.5614			0.0000+0	9.0565-5
1.0000-0	4.0000+1	5.6392+0	5.6392+0							3.7708			0.0000+0	9.0585-5
1.0000-0	5.0000+1	5.6392+0	5.6392+0							3.8851			0.0000+0	9.0602-5
1.0000-0	6.0000+1	5.6392+0	5.6392+0							3.9476+0			0.0000+0	9.0616-5
1.0000-0	7.0000+1	5.6392+0	5.6392+0							2.721			0.0000+0	9.0628-5
1.0000-0	8.0000+1	5.6392+0	5.6392+0							2.658			0.0000+0	9.0638-5
1.0000-0	9.0000+1	5.6392+0	5.6392+0							4.1013			0.0000+0	9.0646-5
1.0000-0	1.0000+2	5.6392+0	5.6392+0							1.7319			0.0000+0	9.0652-5
1.0000-0	2.0000+2	5.6392+0	5.6392+0							1.2941			0.0000+0	9.0657-5
1.0000-0	3.0000+2	5.6392+0	5.6392+0							3.1679			0.0000+0	9.0661-5
1.0000-0	4.0000+2	5.6392+0	5.6392+0							3.1679			0.0000+0	9.0661-5
1.0000-0	5.0000+2	5.6392+0	5.6392+0							2.0854			0.0000+0	9.0664-5
1.0000-0	6.0000+2	5.6392+0	5.6392+0							2.658			0.0000+0	9.0666-5
1.0000-0	7.0000+2	5.6392+0	5.6392+0							2.658			0.0000+0	9.0666-5
1.0000-0	8.0000+2	5.6392+0	5.6392+0							1.4544			0.0000+0	9.0668-5
1.0000-0	9.0000+2	5.6392+0	5.6392+0							1.2774			0.0000+0	9.0671-5
1.0000-0	1.0000+3	5.6392+0	5.6392+0							4.5735			0.0000+0	9.0673-5
1.0000-0	2.0000+3	5.6392+0	5.6392+0							7.6097			0.0000+0	9.0675-5
1.0000-0	3.0000+3	5.6392+0	5.6392+0							7.8855			0.0000+0	9.0677-5
1.0000-0	4.0000+3	5.6392+0	5.6392+0							6.5157			0.0000+0	9.0679-5
1.0000-0	5.0000+3	5.6392+0	5.6392+0							8.4049			0.0000+0	9.0681-5
1.0000-0	6.0000+3	5.6392+0	5.6392+0							9.0282			0.0000+0	9.0682-5
1.0000-0	7.0000+3	5.6392+0	5.6392+0							1.4638			0.0000+0	9.0684-5
1.0000-0	8.0000+3	5.6392+0	5.6392+0							9.4268			0.0000+0	9.0686-5
1.0000-0	9.0000+3	5.6392+0	5.6392+0							7.3925			0.0000+0	9.0688-5
1.0000-0	1.0000+4	5.6392+0	5.6392+0							1.220			0.0000+0	9.0690-5
1.0000-0	2.0000+4	5.6392+0	5.6392+0							9.5895			0.0000+0	9.0692-5
1.0000-0	3.0000+4	5.6392+0	5.6392+0							9.1486			0.0000+0	9.0694-5
1.0000-0	4.0000+4	5.6392+0	5.6392+0							9.0709			0.0000+0	9.0696-5
1.0000-0	5.0000+4	5.6392+0	5.6392+0							5.534			0.0000+0	9.0698-5
1.0000-0	6.0000+4	5.6392+0	5.6392+0							1.791			0.0000+0	9.0700-5
1.0000-0	7.0000+4	5.6392+0	5.6392+0							4.4412			0.0000+0	9.0702-5
1.0000-0	8.0000+4	5.6392+0	5.6392+0							1.183			0.0000+0	9.0704-5
1.0000-0	9.0000+4	5.6392+0	5.6392+0							3.0956			0.0000+0	9.0706-5
1.0000-0	1.0000+5	5.6392+0	5.6392+0							4.3093			0.0000+0	9.0708-5
1.0000-0	2.0000+5	5.6392+0	5.6392+0							4.8267			0.0000+0	9.0710-5
1.0000-0	3.0000+5	5.6392+0	5.6392+0							4.8267			0.0000+0	9.0712-5
1.0000-0	4.0000+5	5.6392+0	5.6392+0							4.9595			0.0000+0	9.0714-5
1.0000-0	5.0000+5	5.6392+0	5.6392+0							3.328			0.0000+0	9.0716-5
1.0000-0	6.0000+5	5.6392+0	5.6392+0							3.328			0.0000+0	9.0718-5
1.0000-0	7.0000+5	5.6392+0	5.6392+0							5.1149			0.0000+0	9.0720-5
1.0000-0	8.0000+5	5.6392+0	5.6392+0							1.6075			0.0000+0	9.0722-5
1.0000-0	9.0000+5	5.6392+0	5.6392+0							2.2382			0.0000+0	9.0724-5
1.0000-0	1.0000+6	5.6392+0	5.6392+0							1.8856			0.0000+0	9.0726-5
1.0000-0	2.0000+6	5.6392+0	5.6392+0							1.791			0.0000+0	9.0728-5
1.0000-0	3.0000+6	5.6392+0	5.6392+0							1.791			0.0000+0	9.0730-5
1.0000-0	4.0000+6	5.6392+0	5.6392+0							1.8856			0.0000+0	9.0732-5
1.0000-0	5.0000+6	5.6392+0	5.6392+0							1.8856			0.0000+0	9.0734-5
1.0000-0	6.0000+6	5.6392+0	5.6392+0							1.8856			0.0000+0	9.0736-5
1.0000-0	7.0000+6	5.6392+0	5.6392+0							1.8856			0.0000+0	9.0738-5
1.0000-0	8.0000+6	5.6392+0	5.6392+0							1.8856			0.0000+0	9.0740-5
1.0000-0	9.0000+6	5.6392+0	5.6392+0							1.8856			0.0000+0	9.0742-5
1.0000-0	1.0000+7	5.6392+0	5.6392+0							1.8856			0.0000+0	9.0744-5
1.0000-0	2.0000+7	5.6392+0	5.6392+0							1.8856			0.0000+0	9.0746-5
1.0000-0	3.0000+7	5.6392+0	5.63											

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CROSS SECTION

MATERIAL =2427

MATERIAL	ENERGY	TOTAL	ELASTIC	INELR	(N.2N)	(N.3N)	FISSIION	(N.NR)	(N.NP)	CAPTURE	(N.P)	(N.D)	(M.A)	MU-BRR
1.0000-	5 ~ 1.0000-2	5.8163+ 0	5.9004+ 0							6.1894- 1			0.0000+ 0	6.8031- 3
1.0000-	1.5000-	5.5883+ 0	5.3004+ 0							6.8695- 1			0.0000+ 0	6.8179- 3
1.0000-	2.0000-	5.5408+ 0	5.3003+ 0							7.4634- 1			0.0000+ 0	6.8220- 3
1.0000-	3.0000-	5.5165+ 0	5.3003+ 0							2.0216- 2			0.0000+ 0	6.8264- 3
1.0000-	4.0000-	5.4922+ 0	5.3003+ 0							1.7000- 1			0.0000+ 0	6.8308- 3
1.0000-	5.0000-	5.4679+ 0	5.3002+ 0							1.6020- 1			0.0000+ 0	6.8351- 3
1.0000-	6.0000-	5.4436+ 0	5.3002+ 0							1.3239- 1			0.0000+ 0	6.8395- 3
1.0000-	8.0000-	5.4193+ 0	5.3001+ 0							1.0817- 1			0.0000+ 0	6.8438- 3
1.0000-	1.0000-	5.3950+ 0	5.3000+ 0							9.0177- 3			0.0000+ 0	6.8481- 3
1.0000-	1.5000-	5.3707+ 0	5.2998+ 0							7.5071- 1			0.0000+ 0	6.8524- 3
1.0000-	2.0000-	5.3464+ 0	5.2997+ 0							6.3769- 1			0.0000+ 0	6.8567- 3
1.0000-	3.0000-	5.3221+ 0	5.2994+ 0							5.2467- 1			0.0000+ 0	6.8610- 3
1.0000-	4.0000-	5.2978+ 0	5.2992+ 0							4.1165- 1			0.0000+ 0	6.8653- 3
1.0000-	5.0000-	5.2735+ 0	5.2989+ 0							4.2704- 1			0.0000+ 0	6.8696- 3
1.0000-	6.0000-	5.2492+ 0	5.2986+ 0							3.7891- 1			0.0000+ 0	6.8739- 3
1.0000-	8.0000-	5.2249+ 0	5.2983+ 0							3.3381- 1			0.0000+ 0	6.8782- 3
1.0000+	0 1.5000+ 0	5.2006+ 0	5.2980+ 0							2.8420- 2			0.0000+ 0	6.8825- 3
1.0000+	0 2.0000+ 0	5.1763+ 0	5.2977+ 0							2.3864- 2			0.0000+ 0	6.8868- 3
1.0000+	0 3.0000+ 0	5.1520+ 0	5.2974+ 0							1.9987- 2			0.0000+ 0	6.8911- 3
1.0000+	0 4.0000+ 0	5.1277+ 0	5.2971+ 0							1.6745- 2			0.0000+ 0	6.8954- 3
1.0000+	0 5.0000+ 0	5.1034+ 0	5.2968+ 0							1.3503- 2			0.0000+ 0	6.8997- 3
1.0000+	0 6.0000+ 0	5.0791+ 0	5.2965+ 0							1.0261- 2			0.0000+ 0	6.9040- 3
1.0000+	0 8.0000+ 0	5.0548+ 0	5.2962+ 0							8.6591- 3			0.0000+ 0	6.9083- 3
1.0000+	1 1.5000+ 1	5.0305+ 0	5.2959+ 0							8.1099- 3			0.0000+ 0	6.9126- 3
1.0000+	1 2.0000+ 1	5.0062+ 0	5.2956+ 0							7.6607- 3			0.0000+ 0	6.9169- 3
1.0000+	1 3.0000+ 1	4.9819+ 0	5.2953+ 0							7.2115- 3			0.0000+ 0	6.9212- 3
1.0000+	1 4.0000+ 1	4.9576+ 0	5.2950+ 0							6.7623- 3			0.0000+ 0	6.9255- 3
1.0000+	1 5.0000+ 1	4.9333+ 0	5.2947+ 0							6.3131- 3			0.0000+ 0	6.9298- 3
1.0000+	1 6.0000+ 1	4.9090+ 0	5.2944+ 0							5.8639- 3			0.0000+ 0	6.9341- 3
1.0000+	1 8.0000+ 1	4.8847+ 0	5.2941+ 0							5.4147- 3			0.0000+ 0	6.9384- 3
1.0000+	2 1.5000+ 2	4.8604+ 0	5.2938+ 0							4.9655- 3			0.0000+ 0	6.9427- 3
1.0000+	2 2.0000+ 2	4.8361+ 0	5.2935+ 0							4.5163- 3			0.0000+ 0	6.9470- 3
1.0000+	2 3.0000+ 2	4.8118+ 0	5.2932+ 0							4.0671- 3			0.0000+ 0	6.9513- 3
1.0000+	2 4.0000+ 2	4.7875+ 0	5.2929+ 0							3.6179- 3			0.0000+ 0	6.9556- 3
1.0000+	2 5.0000+ 2	4.7632+ 0	5.2926+ 0							3.1687- 3			0.0000+ 0	6.9599- 3
1.0000+	2 6.0000+ 2	4.7389+ 0	5.2923+ 0							2.7195- 3			0.0000+ 0	6.9642- 3
1.0000+	2 8.0000+ 2	4.7146+ 0	5.2920+ 0							2.2703- 3			0.0000+ 0	6.9685- 3
1.0000+	3 1.5000+ 3	4.6903+ 0	5.2917+ 0							1.8211- 3			0.0000+ 0	6.9728- 3
1.0000+	3 2.0000+ 3	4.6660+ 0	5.2914+ 0							1.3719- 3			0.0000+ 0	6.9771- 3
1.0000+	3 3.0000+ 3	4.6417+ 0	5.2911+ 0							9.5255- 2			0.0000+ 0	6.9814- 3
1.0000+	3 4.0000+ 3	4.6174+ 0	5.2908+ 0							9.0763- 2			0.0000+ 0	6.9857- 3
1.0000+	3 5.0000+ 3	4.5931+ 0	5.2905+ 0							8.6271- 2			0.0000+ 0	6.9900- 3
1.0000+	3 6.0000+ 3	4.5688+ 0	5.2902+ 0							8.1780- 2			0.0000+ 0	6.9943- 3
1.0000+	3 8.0000+ 3	4.5445+ 0	5.2899+ 0							7.7288- 2			0.0000+ 0	6.9986- 3
1.0000+	4 1.5000+ 4	4.5202+ 0	5.2896+ 0							7.2797- 2			0.0000+ 0	7.0029- 3
1.0000+	4 2.0000+ 4	4.4959+ 0	5.2893+ 0							6.8305- 2			0.0000+ 0	7.0072- 3
1.0000+	4 3.0000+ 4	4.4716+ 0	5.2890+ 0							6.3814- 2			0.0000+ 0	7.0115- 3
1.0000+	4 4.0000+ 4	4.4473+ 0	5.2887+ 0							5.9322- 2			0.0000+ 0	7.0158- 3
1.0000+	4 5.0000+ 4	4.4230+ 0	5.2884+ 0							5.4831- 2			0.0000+ 0	7.0201- 3
1.0000+	4 6.0000+ 4	4.3987+ 0	5.2881+ 0							5.0339- 2			0.0000+ 0	7.0244- 3
1.0000+	4 8.0000+ 4	4.3744+ 0	5.2878+ 0							4.5848- 2			0.0000+ 0	7.0287- 3
1.0000+	5 1.5000+ 5	4.3501+ 0	5.2875+ 0							4.1356- 2			0.0000+ 0	7.0330- 3
1.0000+	5 2.0000+ 5	4.3258+ 0	5.2872+ 0							3.6865- 2			0.0000+ 0	7.0373- 3
1.0000+	5 3.0000+ 5	4.3015+ 0	5.2869+ 0							3.2373- 2			0.0000+ 0	7.0416- 3
1.0000+	5 4.0000+ 5	4.2772+ 0	5.2866+ 0							2.7882- 2			0.0000+ 0	7.0459- 3
1.0000+	5 6.0000+ 5	4.2529+ 0	5.2863+ 0							2.3391- 2			0.0000+ 0	7.0502- 3
1.0000+	5 8.0000+ 5	4.2286+ 0	5.2860+ 0							1.8900- 2			0.0000+ 0	7.0545- 3
1.0000+	6 1.5000+ 6	4.2043+ 0	5.2857+ 0							1.4408- 2			0.0000+ 0	7.0588- 3
1.0000+	6 2.0000+ 6	4.1800+ 0	5.2854+ 0							1.0000- 2			0.0000+ 0	7.0631- 3
1.0000+	6 3.0000+ 6	4.1557+ 0	5.2851+ 0							8.5500- 2			0.0000+ 0	7.0674- 3
1.0000+	6 4.0000+ 6	4.1314+ 0	5.2848+ 0							8.1009- 2			0.0000+ 0	7.0717- 3
1.0000+	6 6.0000+ 6	4.1071+ 0	5.2845+ 0							7.6517- 2			0.0000+ 0	7.0760- 3
1.0000+	6 8.0000+ 6	4.0828+ 0	5.2842+ 0							7.2025- 2			0.0000+ 0	7.0803- 3
1.0000+	7 1.5000+ 7	4.0585+ 0	5.2839+ 0							6.7533- 2			0.0000+ 0	7.0846- 3
1.0000+	7 2.0000+ 7	4.0342+ 0	5.2836+ 0							6.3042- 2			0.0000+ 0	7.0889- 3
1.0000+	7 3.0000+ 7	4.0099+ 0	5.2833+ 0							5.8550- 2			0.0000+ 0	7.0932- 3
1.0000+	7 4.0000+ 7	4.0164+ 0	5.2830+ 0							5.4059- 2			0.0000+ 0	7.0975- 3
1.0000+	7 5.0000+ 7	4.0129+ 0	5.2827+ 0							4.9567- 2			0.0000+ 0	7.1018- 3
1.0000+	7 6.0000+ 7	4.0094+ 0	5.2824+ 0							4.5075- 2			0.0000+ 0	7.1061- 3
1.0000+	7 8.0000+ 7	4.0059+ 0	5.2821+ 0							4.0584- 2			0.0000+ 0	7.1104- 3
1.0000+	8 1.5000+ 8	4.0024+ 0	5.2818+ 0							3.6092- 2			0.0000+ 0	7.1147- 3
1.0000+	8 2.0000+ 8	4.0000+ 0	5.2815+ 0							3.1601- 2			0.0000+ 0	7.1190- 3
1.0000+	8 3.0000+ 8	4.0000+ 0	5.2812+ 0							2.7109- 2			0.0000+ 0	7.1233- 3
1.0000+	8 4.0000+ 8	4.0000+ 0	5.2809+ 0							2.2618- 2			0.0000+ 0	7.1276- 3
1.0000+	8 6.0000+ 8	4.0000+ 0	5.2806+ 0							1.8126- 2			0.0000+ 0	7.1319- 3
1.0000+	8 8.0000+ 8	4.0000+ 0	5.2803+ 0							1.3635- 2			0.0000+ 0	7.1362- 3
1.0000+	9 1.5000+ 9	4.0000+ 0	5.2800+ 0							9.5222- 1			0.0000+ 0	7.1405- 3
1.0000+	9 2.0000+ 9	4.0000+ 0	5.2797+ 0							9.0731- 1			0.0000+ 0	7.1448- 3
1.0000+	9 3.0000+ 9	4.0000+ 0	5.2794+ 0							8.6239- 1			0.0000+ 0	7.1491- 3
1.0000+	9 4.0000+ 9	4.0000+ 0	5.2791+ 0							8.1748- 1			0.0000+ 0	7.1534- 3
1.0000+	9 6.000													

HF-174

CROSS SECTION

MATERIAL = 2721

ENERGY	TOTAL	ELASTIC	INELR	(N.2N)	(N.2N)	FISSION	(N.WR)	(N.WP)	CAPTURE	(N.P)	(N.D)	(N.R)	MU-BRR
1.0000- 5 ~ 1.0000- 2	1.2106+ 3	8.0000+ 0							1.2023+ 3	0.0000+ 0		0.0000+ 0	4.0843- 5
1.0000- 1.5000- 0	5.6558+ 0	8.0000+ 0							5.5744+ 2	0.0000+ 0		0.0000+ 0	4.1410- 3
1.5000- 2.0000- 0	4.7822+ 0	8.0000+ 0							4.7009+ 0	0.0000+ 0		0.0000+ 0	4.1677- 1
2.0000- 2.5000- 0	4.0234+ 0	8.0000+ 0							3.9728+ 0	0.0000+ 0		0.0000+ 0	4.1808- 3
2.5000- 3.0000- 0	3.4031+ 0	8.0000+ 0							2.9851+ 1	0.0000+ 0		0.0000+ 0	4.1908- 3
3.0000- 3.5000- 0	3.0059+ 0	8.0000+ 0							2.6440+ 0	0.0000+ 0		0.0000+ 0	4.1984- 3
3.5000- 4.0000- 0	2.7428+ 0	8.0000+ 0							2.3478+ 0	0.0000+ 0		0.0000+ 0	4.2174- 1
4.0000- 4.5000- 0	2.5895+ 0	8.0000+ 0							2.0690+ 0	0.0000+ 0		0.0000+ 0	4.2399- 3
4.5000- 5.0000- 0	2.4495+ 0	8.0000+ 0							1.7897+ 2	0.0000+ 0		0.0000+ 0	4.2490- 3
5.0000- 5.5000- 0	2.3206+ 0	8.0000+ 0							1.4804+ 2	0.0000+ 0		0.0000+ 0	4.2697- 3
5.5000- 6.0000- 0	2.2022+ 0	8.0000+ 0							1.2424+ 2	0.0000+ 0		0.0000+ 0	4.2939- 3
6.0000- 6.5000- 0	2.0937+ 0	8.0000+ 0							1.0486+ 2	0.0000+ 0		0.0000+ 0	4.3209- 3
6.5000- 7.0000- 0	2.0057+ 0	8.0000+ 0							0.8591+ 1	0.0000+ 0		0.0000+ 0	4.3576- 3
7.0000- 7.5000- 0	1.9273+ 0	8.0000+ 0							0.6921+ 1	0.0000+ 0		0.0000+ 0	4.3965- 3
7.5000- 8.0000- 0	1.8593+ 0	8.0000+ 0							0.5437+ 1	0.0000+ 0		0.0000+ 0	4.4383- 3
8.0000- 8.5000- 0	1.7999+ 0	8.0000+ 0							0.4151+ 1	0.0000+ 0		0.0000+ 0	4.4839- 3
8.5000- 9.0000- 0	1.7474+ 0	8.0000+ 0							0.3047+ 1	0.0000+ 0		0.0000+ 0	4.5335- 3
9.0000- 9.5000- 0	1.6914+ 0	8.0000+ 0							0.2155+ 1	0.0000+ 0		0.0000+ 0	4.5866- 3
9.5000- 1.0000+ 0	1.6318+ 0	8.0000+ 0							0.1482+ 1	0.0000+ 0		0.0000+ 0	4.6434- 3
1.0000+ 1.0000+ 0	1.5693+ 0	8.0000+ 0							0.0997+ 2	0.0000+ 0		0.0000+ 0	4.7047- 3
1.0000+ 1.5000+ 0	1.5034+ 0	8.0000+ 0							1.5499+ 1	0.0000+ 0		0.0000+ 0	4.7709- 3
1.5000+ 2.0000+ 0	1.4341+ 0	8.0000+ 0							1.1743+ 0	0.0000+ 0		0.0000+ 0	4.8426- 3
2.0000+ 2.5000+ 0	1.3604+ 0	8.0000+ 0							0.8217+ 0	0.0000+ 0		0.0000+ 0	4.9199- 3
2.5000+ 3.0000+ 0	1.2828+ 0	8.0000+ 0							0.5255+ 1	0.0000+ 0		0.0000+ 0	5.0036- 3
3.0000+ 3.5000+ 0	1.2014+ 0	8.0000+ 0							0.3422+ 1	0.0000+ 0		0.0000+ 0	5.0947- 3
3.5000+ 4.0000+ 0	1.1164+ 0	8.0000+ 0							0.2332+ 1	0.0000+ 0		0.0000+ 0	5.1944- 3
4.0000+ 4.5000+ 0	1.0281+ 0	8.0000+ 0							0.1604+ 1	0.0000+ 0		0.0000+ 0	5.3031- 3
4.5000+ 5.0000+ 0	0.9357+ 0	8.0000+ 0							0.1097+ 1	0.0000+ 0		0.0000+ 0	5.4211- 3
5.0000+ 5.5000+ 0	0.8394+ 0	8.0000+ 0							0.0773+ 1	0.0000+ 0		0.0000+ 0	5.5487- 3
5.5000+ 6.0000+ 0	0.7393+ 0	8.0000+ 0							0.0511+ 1	0.0000+ 0		0.0000+ 0	5.6861- 3
6.0000+ 6.5000+ 0	0.6356+ 0	8.0000+ 0							0.0297+ 2	0.0000+ 0		0.0000+ 0	5.8340- 3
6.5000+ 7.0000+ 0	0.5284+ 0	8.0000+ 0							0.0190+ 2	0.0000+ 0		0.0000+ 0	5.9933- 3
7.0000+ 7.5000+ 0	0.4178+ 0	8.0000+ 0							0.0097+ 2	0.0000+ 0		0.0000+ 0	6.1651- 3
7.5000+ 8.0000+ 0	0.3031+ 0	8.0000+ 0							0.0065+ 1	0.0000+ 0		0.0000+ 0	6.3507- 3
8.0000+ 8.5000+ 0	0.1846+ 0	8.0000+ 0							0.0032+ 1	0.0000+ 0		0.0000+ 0	6.5501- 3
8.5000+ 9.0000+ 0	0.0611+ 0	8.0000+ 0							0.0012+ 1	0.0000+ 0		0.0000+ 0	6.7633- 3
9.0000+ 9.5000+ 0	0.0000+ 0	8.0000+ 0							0.0000+ 0	0.0000+ 0		0.0000+ 0	6.9907- 3
9.5000+ 1.0000+ 1	0.0000+ 0	8.0000+ 0							0.0000+ 0	0.0000+ 0		0.0000+ 0	7.2341- 3
1.0000+ 1.5000+ 1	0.0000+ 0	8.0000+ 0							0.0000+ 0	0.0000+ 0		0.0000+ 0	7.4944- 3
1.5000+ 2.0000+ 1	0.0000+ 0	8.0000+ 0							0.0000+ 0	0.0000+ 0		0.0000+ 0	7.7719- 3
2.0000+ 2.5000+ 1	0.0000+ 0	8.0000+ 0							0.0000+ 0	0.0000+ 0		0.0000+ 0	8.0676- 3
2.5000+ 3.0000+ 1	0.0000+ 0	8.0000+ 0							0.0000+ 0	0.0000+ 0		0.0000+ 0	8.3831- 3
3.0000+ 3.5000+ 1	0.0000+ 0	8.0000+ 0							0.0000+ 0	0.0000+ 0		0.0000+ 0	8.7204- 3
3.5000+ 4.0000+ 1	0.0000+ 0	8.0000+ 0							0.0000+ 0	0.0000+ 0		0.0000+ 0	9.0811- 3
4.0000+ 4.5000+ 1	0.0000+ 0	8.0000+ 0							0.0000+ 0	0.0000+ 0		0.0000+ 0	9.4661- 3
4.5000+ 5.0000+ 1	0.0000+ 0	8.0000+ 0							0.0000+ 0	0.0000+ 0		0.0000+ 0	9.8771- 3
5.0000+ 5.5000+ 1	0.0000+ 0	8.0000+ 0							0.0000+ 0	0.0000+ 0		0.0000+ 0	1.0311- 2
5.5000+ 6.0000+ 1	0.0000+ 0	8.0000+ 0							0.0000+ 0	0.0000+ 0		0.0000+ 0	1.0882- 2
6.0000+ 6.5000+ 1	0.0000+ 0	8.0000+ 0							0.0000+ 0	0.0000+ 0		0.0000+ 0	1.1483- 1
6.5000+ 7.0000+ 1	0.0000+ 0	8.0000+ 0							0.0000+ 0	0.0000+ 0		0.0000+ 0	1.2114- 1
7.0000+ 7.5000+ 1	0.0000+ 0	8.0000+ 0							0.0000+ 0	0.0000+ 0		0.0000+ 0	1.2775- 1
7.5000+ 8.0000+ 1	0.0000+ 0	8.0000+ 0							0.0000+ 0	0.0000+ 0		0.0000+ 0	1.3466- 1
8.0000+ 8.5000+ 1	0.0000+ 0	8.0000+ 0							0.0000+ 0	0.0000+ 0		0.0000+ 0	1.4187- 1
8.5000+ 9.0000+ 1	0.0000+ 0	8.0000+ 0							0.0000+ 0	0.0000+ 0		0.0000+ 0	1.4938- 1
9.0000+ 9.5000+ 1	0.0000+ 0	8.0000+ 0							0.0000+ 0	0.0000+ 0		0.0000+ 0	1.5711- 1
9.5000+ 1.0000+ 2	0.0000+ 0	8.0000+ 0							0.0000+ 0	0.0000+ 0		0.0000+ 0	1.6506- 1
1.0000+ 1.5000+ 2	0.0000+ 0	8.0000+ 0							0.0000+ 0	0.0000+ 0		0.0000+ 0	1.7323- 1
1.5000+ 2.0000+ 2	0.0000+ 0	8.0000+ 0							0.0000+ 0	0.0000+ 0		0.0000+ 0	1.8164- 1
2.0000+ 2.5000+ 2	0.0000+ 0	8.0000+ 0							0.0000+ 0	0.0000+ 0		0.0000+ 0	1.9029- 1
2.5000+ 3.0000+ 2	0.0000+ 0	8.0000+ 0							0.0000+ 0	0.0000+ 0		0.0000+ 0	1.9918- 1
3.0000+ 3.5000+ 2	0.0000+ 0	8.0000+ 0							0.0000+ 0	0.0000+ 0		0.0000+ 0	2.0831- 1
3.5000+ 4.0000+ 2	0.0000+ 0	8.0000+ 0							0.0000+ 0	0.0000+ 0		0.0000+ 0	2.1768- 1
4.0000+ 4.5000+ 2	0.0000+ 0	8.0000+ 0							0.0000+ 0	0.0000+ 0		0.0000+ 0	2.2730- 1
4.5000+ 5.0000+ 2	0.0000+ 0	8.0000+ 0							0.0000+ 0	0.0000+ 0		0.0000+ 0	2.3717- 1
5.0000+ 5.5000+ 2	0.0000+ 0	8.0000+ 0							0.0000+ 0	0.0000+ 0		0.0000+ 0	2.4729- 1
5.5000+ 6.0000+ 2	0.0000+ 0	8.0000+ 0							0.0000+ 0	0.0000+ 0		0.0000+ 0	2.5765- 1
6.0000+ 6.5000+ 2	0.0000+ 0	8.0000+ 0							0.0000+ 0	0.0000+ 0		0.0000+ 0	2.6826- 1
6.5000+ 7.0000+ 2	0.0000+ 0	8.0000+ 0							0.0000+ 0	0.0000+ 0		0.0000+ 0	2.7911- 1
7.0000+ 7.5000+ 2	0.0000+ 0	8.0000+ 0							0.0000+ 0	0.0000+ 0		0.0000+ 0	2.9021- 1
7.5000+ 8.0000+ 2	0.0000+ 0	8.0000+ 0							0.0000+ 0	0.0000+ 0		0.0000+ 0	3.0154- 1
8.0000+ 8.5000+ 2	0.0000+ 0	8.0000+ 0							0.0000+ 0	0.0000+ 0		0.0000+ 0	3.1319- 1
8.5000+ 9.0000+ 2	0.0000+ 0	8.0000+ 0							0.0000+ 0	0.0000+ 0		0.0000+ 0	3.2514- 1
9.0000+ 9.5000+ 2	0.0000+ 0	8.0000+ 0							0.0000+ 0	0.0000+ 0		0.0000+ 0	3.3737- 1
9.5000+ 1.0000+ 3	0.0000+ 0	8.0000+ 0							0.0000+ 0	0.0000+ 0		0.0000+ 0	3.5000- 1
1.0000+ 1.5000+ 3	0.0000+ 0	8.0000+ 0							0.0000+ 0	0.0000+ 0		0.0000+ 0	3.6300- 1
1.5000+ 2.0000+ 3	0.0000+ 0	8.0000+ 0							0.0000+ 0	0.0000+ 0		0.0000+ 0	3.7634- 1
2.0000+ 2.5000+ 3	0.0000+ 0	8.0000+ 0							0.0000+ 0	0.0000+ 0		0.0000+ 0	3.9001- 1
2.5000+ 3.0000+ 3	0.0000+ 0	8.0000+ 0							0.0000+				

MATERIAL = 2722 CROSS SECTION HF-178

ENERGY	TOTAL	ELASTIC	INELA	(N,2N)	(N,SN)	FISSION	(N,NA)	(N,MP)	CAPTURE	(N,P)	(N,D)	(N,A)	MU-BAR
1.0000+ 5 ~ 1.0000- 2	1.2487+ 2	8.0000+ 0	2.0088- 2						1.1676+ 2			0.0000+ 0	4.0385- 3
1.5000+ 2 ~ 1.5000- 2	5.9183+ 1	8.0000+ 0	1.6116- 1						5.4028+ 1			0.0000+ 0	4.0803- 3
2.0000+ 2 ~ 2.0000- 2	4.7815+ 1	8.0000+ 0	3.0536- 1						4.5872+ 1			0.0000+ 0	4.0926- 3
3.0000+ 2 ~ 3.0000- 2	4.0462+ 1	8.0000+ 0	4.5885- 1						3.8400+ 1			0.0000+ 0	4.1015- 3
4.0000+ 2 ~ 4.0000- 2	3.6554+ 1	8.0000+ 0	6.4688- 1						2.2374+ 1			0.0000+ 0	4.1178- 3
5.0000+ 2 ~ 5.0000- 2	3.3914+ 1	8.0000+ 0	8.8147+ 0						2.0510+ 1			0.0000+ 0	4.1269- 3
6.0000+ 2 ~ 6.0000- 2	3.2820+ 1	8.0000+ 0	1.1528+ 0						2.2863+ 1			0.0000+ 0	4.1346- 3
7.0000+ 2 ~ 7.0000- 2	3.2420+ 1	8.0000+ 0	1.8224+ 0						2.0163+ 1			0.0000+ 0	4.1411- 3
8.0000+ 2 ~ 8.0000- 2	3.2015+ 1	8.0000+ 0	2.5556+ 0						1.7168+ 1			0.0000+ 0	4.1478- 3
9.0000+ 2 ~ 9.0000- 2	3.1610+ 1	8.0000+ 0	3.3114+ 0						1.4749+ 1			0.0000+ 0	4.1541- 3
1.0000+ 1 ~ 1.5000- 1	2.8215+ 1	8.0000+ 0	4.1547+ 0						1.0423+ 1			0.0000+ 0	4.1601- 3
2.0000+ 1 ~ 2.5000- 1	2.5231+ 1	8.0000+ 0	5.2000+ 0						8.9953+ 0			0.0000+ 0	4.2104- 3
3.0000+ 1 ~ 3.5000- 1	2.2700+ 1	8.0000+ 0	6.3976+ 0						8.0325+ 0			0.0000+ 0	4.2177- 3
4.0000+ 1 ~ 4.5000- 1	2.0516+ 1	8.0000+ 0	7.5978+ 0						7.3405+ 0			0.0000+ 0	4.2284- 3
5.0000+ 1 ~ 5.5000- 1	1.8756+ 1	8.0000+ 0	8.8114+ 0						6.8958+ 0			0.0000+ 0	4.2366- 3
6.0000+ 1 ~ 6.5000- 1	1.7258+ 1	8.0000+ 0	1.0285+ 0						5.9361+ 0			0.0000+ 0	4.2473- 3
7.0000+ 1 ~ 7.5000- 1	1.5951+ 1	8.0000+ 0	2.8814+ 0						5.9361+ 0			0.0000+ 0	4.2596- 3
8.0000+ 1 ~ 8.5000- 1	1.4849+ 1	8.0000+ 0	3.1159+ 0						4.7817+ 0			0.0000+ 0	4.2724- 3
9.0000+ 1 ~ 9.5000- 1	1.3924+ 1	8.0000+ 0	3.5200+ 0						4.5085+ 0			0.0000+ 0	4.2848- 3
1.0000+ 0 ~ 1.5000- 0	9.5592+ 0	8.0000+ 0	4.9376+ 0						6.7131+ 0			0.0000+ 0	4.3012- 3
2.0000+ 0 ~ 2.5000- 0	8.7822+ 0	8.0000+ 0	5.5281+ 0						6.1018+ 0			0.0000+ 0	4.3089- 3
3.0000+ 0 ~ 3.5000- 0	8.0552+ 0	8.0000+ 0	6.1257+ 0						5.5873+ 1			0.0000+ 0	4.3191- 3
4.0000+ 0 ~ 4.5000- 0	7.3857+ 0	8.0000+ 0	6.7682+ 0						5.0707+ 1			0.0000+ 0	4.3309- 3
5.0000+ 0 ~ 5.5000- 0	6.7682+ 0	8.0000+ 0	7.4381+ 0						4.5624+ 1			0.0000+ 0	4.3431- 3
6.0000+ 0 ~ 6.5000- 0	6.1980+ 0	8.0000+ 0	8.1411+ 0						4.0591+ 1			0.0000+ 0	4.3559- 3
7.0000+ 0 ~ 7.5000- 0	5.6727+ 0	8.0000+ 0	8.8752+ 0						3.5593+ 1			0.0000+ 0	4.3691- 3
8.0000+ 0 ~ 8.5000- 0	5.1919+ 0	8.0000+ 0	9.6381+ 0						3.0677+ 1			0.0000+ 0	4.3826- 3
9.0000+ 0 ~ 9.5000- 0	4.7554+ 0	8.0000+ 0	1.0446+ 2						2.5847+ 1			0.0000+ 0	4.3974- 3
1.0000+ 0 ~ 1.5000- 0	4.3727+ 0	8.0000+ 0	1.1826+ 2						2.1089+ 1			0.0000+ 0	4.4133- 3
2.0000+ 0 ~ 2.5000- 0	3.9949+ 0	8.0000+ 0	1.3259+ 2						1.6399+ 1			0.0000+ 0	4.4294- 3
3.0000+ 0 ~ 3.5000- 0	3.6277+ 0	8.0000+ 0	1.4756+ 2						1.1804+ 1			0.0000+ 0	4.4458- 3
4.0000+ 0 ~ 4.5000- 0	3.2711+ 0	8.0000+ 0	1.6311+ 2						0.7200+ 1			0.0000+ 0	4.4634- 3
5.0000+ 0 ~ 5.5000- 0	2.9257+ 0	8.0000+ 0	1.7923+ 2						0.2609+ 1			0.0000+ 0	4.4812- 3
6.0000+ 0 ~ 6.5000- 0	2.5922+ 0	8.0000+ 0	1.9585+ 2						0.0000+ 0			0.0000+ 0	4.5000+ 0
7.0000+ 0 ~ 7.5000- 0	2.2700+ 0	8.0000+ 0	2.1305+ 2						0.0000+ 0			0.0000+ 0	4.5191+ 0
8.0000+ 0 ~ 8.5000- 0	1.9592+ 0	8.0000+ 0	2.3081+ 2						0.0000+ 0			0.0000+ 0	4.5384+ 0
9.0000+ 0 ~ 9.5000- 0	1.6593+ 0	8.0000+ 0	2.4911+ 2						0.0000+ 0			0.0000+ 0	4.5580+ 0
1.0000+ 0 ~ 1.5000- 0	1.3693+ 0	8.0000+ 0	2.6793+ 2						0.0000+ 0			0.0000+ 0	4.5779+ 0
2.0000+ 0 ~ 2.5000- 0	1.0893+ 0	8.0000+ 0	2.8725+ 2						0.0000+ 0			0.0000+ 0	4.5980+ 0
3.0000+ 0 ~ 3.5000- 0	0.8093+ 0	8.0000+ 0	3.0707+ 2						0.0000+ 0			0.0000+ 0	4.6183+ 0
4.0000+ 0 ~ 4.5000- 0	0.5293+ 0	8.0000+ 0	3.2739+ 2						0.0000+ 0			0.0000+ 0	4.6387+ 0
5.0000+ 0 ~ 5.5000- 0	0.2493+ 0	8.0000+ 0	3.4811+ 2						0.0000+ 0			0.0000+ 0	4.6591+ 0
6.0000+ 0 ~ 6.5000- 0	0.0000+ 0	8.0000+ 0	3.6923+ 2						0.0000+ 0			0.0000+ 0	4.6795+ 0
7.0000+ 0 ~ 7.5000- 0	0.0000+ 0	8.0000+ 0	3.9075+ 2						0.0000+ 0			0.0000+ 0	4.6999+ 0
8.0000+ 0 ~ 8.5000- 0	0.0000+ 0	8.0000+ 0	4.1267+ 2						0.0000+ 0			0.0000+ 0	4.7203+ 0
9.0000+ 0 ~ 9.5000- 0	0.0000+ 0	8.0000+ 0	4.3500+ 2						0.0000+ 0			0.0000+ 0	4.7407+ 0
1.0000+ 0 ~ 1.5000- 0	0.0000+ 0	8.0000+ 0	4.5782+ 2						0.0000+ 0			0.0000+ 0	4.7611+ 0
2.0000+ 0 ~ 2.5000- 0	0.0000+ 0	8.0000+ 0	4.8114+ 2						0.0000+ 0			0.0000+ 0	4.7815+ 0
3.0000+ 0 ~ 3.5000- 0	0.0000+ 0	8.0000+ 0	5.0499+ 2						0.0000+ 0			0.0000+ 0	4.8019+ 0
4.0000+ 0 ~ 4.5000- 0	0.0000+ 0	8.0000+ 0	5.2932+ 2						0.0000+ 0			0.0000+ 0	4.8223+ 0
5.0000+ 0 ~ 5.5000- 0	0.0000+ 0	8.0000+ 0	5.5414+ 2						0.0000+ 0			0.0000+ 0	4.8427+ 0
6.0000+ 0 ~ 6.5000- 0	0.0000+ 0	8.0000+ 0	5.7946+ 2						0.0000+ 0			0.0000+ 0	4.8631+ 0
7.0000+ 0 ~ 7.5000- 0	0.0000+ 0	8.0000+ 0	6.0528+ 2						0.0000+ 0			0.0000+ 0	4.8835+ 0
8.0000+ 0 ~ 8.5000- 0	0.0000+ 0	8.0000+ 0	6.3160+ 2						0.0000+ 0			0.0000+ 0	4.9039+ 0
9.0000+ 0 ~ 9.5000- 0	0.0000+ 0	8.0000+ 0	6.5842+ 2						0.0000+ 0			0.0000+ 0	4.9243+ 0
1.0000+ 0 ~ 1.5000- 0	0.0000+ 0	8.0000+ 0	6.8574+ 2						0.0000+ 0			0.0000+ 0	4.9447+ 0
2.0000+ 0 ~ 2.5000- 0	0.0000+ 0	8.0000+ 0	7.1356+ 2						0.0000+ 0			0.0000+ 0	4.9651+ 0
3.0000+ 0 ~ 3.5000- 0	0.0000+ 0	8.0000+ 0	7.4188+ 2						0.0000+ 0			0.0000+ 0	4.9855+ 0
4.0000+ 0 ~ 4.5000- 0	0.0000+ 0	8.0000+ 0	7.7070+ 2						0.0000+ 0			0.0000+ 0	5.0059+ 0
5.0000+ 0 ~ 5.5000- 0	0.0000+ 0	8.0000+ 0	8.0000+ 2						0.0000+ 0			0.0000+ 0	5.0263+ 0
6.0000+ 0 ~ 6.5000- 0	0.0000+ 0	8.0000+ 0	8.2982+ 2						0.0000+ 0			0.0000+ 0	5.0467+ 0
7.0000+ 0 ~ 7.5000- 0	0.0000+ 0	8.0000+ 0	8.5964+ 2						0.0000+ 0			0.0000+ 0	5.0671+ 0
8.0000+ 0 ~ 8.5000- 0	0.0000+ 0	8.0000+ 0	8.8946+ 2						0.0000+ 0			0.0000+ 0	5.0875+ 0
9.0000+ 0 ~ 9.5000- 0	0.0000+ 0	8.0000+ 0	9.1928+ 2						0.0000+ 0			0.0000+ 0	5.1079+ 0
1.0000+ 0 ~ 1.5000- 0	0.0000+ 0	8.0000+ 0	9.4910+ 2						0.0000+ 0			0.0000+ 0	5.1283+ 0
2.0000+ 0 ~ 2.5000- 0	0.0000+ 0	8.0000+ 0	9.7892+ 2						0.0000+ 0			0.0000+ 0	5.1487+ 0
3.0000+ 0 ~ 3.5000- 0	0.0000+ 0	8.0000+ 0	1.0074+ 3						0.0000+ 0			0.0000+ 0	5.1691+ 0
4.0000+ 0 ~ 4.5000- 0	0.0000+ 0	8.0000+ 0	1.0256+ 3						0.0000+ 0			0.0000+ 0	5.1895+ 0
5.0000+ 0 ~ 5.5000- 0	0.0000+ 0	8.0000+ 0	1.0438+ 3						0.0000+ 0			0.0000+ 0	5.2099+ 0
6.0000+ 0 ~ 6.5000- 0	0.0000+ 0	8.0000+ 0	1.0620+ 3						0.0000+ 0			0.0000+ 0	5.2303+ 0
7.0000+ 0 ~ 7.5000- 0	0.0000+ 0	8.0000+ 0	1.0802+ 3						0.0000+ 0			0.0000+ 0	5.2507+ 0
8.0000+ 0 ~ 8.5000- 0	0.0000+ 0	8.0000+ 0	1.0984+ 3						0.0000+ 0			0.0000+ 0	5.2711+ 0
9.0000+ 0 ~ 9.5000- 0	0.0000+ 0	8.0000+ 0	1.1166+ 3						0.0000+ 0			0.0000+ 0	5.2915+ 0
1.0000+ 0 ~ 1.5000- 0	0.0000+ 0	8.0000+ 0	1.1348+ 3						0.0000+ 0			0.0000+ 0	5.3119+ 0
2.0000+ 0 ~ 2.5000- 0	0.0000+ 0	8.0000+ 0	1.1530+ 3						0.0000+ 0			0.0000+ 0	5.3323+ 0
3.0000+ 0 ~ 3.5000- 0	0.0000+ 0	8.0000+ 0	1.1712+ 3						0.0000+ 0			0.0000+ 0	5.3527+ 0
4.0000+ 0 ~ 4.5000- 0	0.0000+ 0	8.0000+ 0	1.1894+ 3										

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CROSS SECTION

MATERIAL = 2723

ENERGY	TOTAL	ELASTIC	INELR	(N,2N)	(N,3N)	FISSION	(N,NR)	(N,RP)	CAPTURE	(N,P)	(N,D)	(N,R)	MU-BRR
1.0000- 5	1.1324+ 3	7.0000+ 0							1.1262+ 5	0.0000+ 0		0.0000+ 0	4.1644- 3
1.0000- 2	5.2449+ 2	7.0000+ 0							5.1727+ 2	0.0000+ 0		0.0000+ 0	4.2268- 3
1.0000- 0	5.6744+ 2	7.0000+ 0							4.3043+ 2	0.0000+ 0		0.0000+ 0	4.2471- 3
2.0000- 2	3.6768+ 2	7.0000+ 0							3.6768+ 2	0.0000+ 0		0.0000+ 0	4.2889- 3
3.0000- 0	3.1853+ 2	7.0000+ 0							3.0480+ 2	0.0000+ 0		0.0000+ 0	4.3037- 3
4.0000- 2	2.8163+ 2	7.0000+ 0							2.8163+ 2	0.0000+ 0		0.0000+ 0	4.3158- 3
5.0000- 0	2.5816+ 2	7.0000+ 0							2.5816+ 2	0.0000+ 0		0.0000+ 0	4.3301- 3
6.0000- 2	2.3900+ 2	7.0000+ 0							2.3900+ 2	0.0000+ 0		0.0000+ 0	4.3452- 3
7.0000- 0	2.2300+ 2	6.9370+ 0							2.0597+ 2	0.0000+ 0		0.0000+ 0	4.3618- 3
8.0000- 2	2.0938+ 2	6.8958+ 0							1.8643+ 2	0.0000+ 0		0.0000+ 0	4.3798- 3
1.0000- 1	1.7628+ 2	6.8581+ 0							1.5932+ 2	0.0000+ 0		0.0000+ 0	4.3991- 3
2.0000- 1	1.4748+ 2	6.8263+ 0							1.3238+ 2	0.0000+ 0		0.0000+ 0	4.4197- 3
3.0000- 1	1.2356+ 2	6.7999+ 0							1.0670+ 2	0.0000+ 0		0.0000+ 0	4.4425- 3
4.0000- 1	1.0387+ 2	6.7771+ 0							0.8260+ 2	0.0000+ 0		0.0000+ 0	4.4675- 3
5.0000- 1	0.8711+ 2	6.7581+ 0							0.5961+ 2	0.0000+ 0		0.0000+ 0	4.4948- 3
6.0000- 1	0.7395+ 2	6.7423+ 0							0.3861+ 2	0.0000+ 0		0.0000+ 0	4.5243- 3
7.0000- 1	0.6318+ 2	6.7295+ 0							0.1935+ 2	0.0000+ 0		0.0000+ 0	4.5562+ 3
8.0000- 1	0.5429+ 2	6.7198+ 0							0.0222+ 2	0.0000+ 0		0.0000+ 0	4.5914+ 3
1.0000- 0	0.4729+ 2	6.7125+ 0							0.0000+ 2	0.0000+ 0		0.0000+ 0	4.6297+ 3
2.0000- 0	0.4189+ 2	6.7074+ 0							0.0000+ 2	0.0000+ 0		0.0000+ 0	4.6714+ 3
3.0000- 0	0.3782+ 2	6.7041+ 0							0.0000+ 2	0.0000+ 0		0.0000+ 0	4.7169+ 3
4.0000- 0	0.3472+ 2	6.7022+ 0							0.0000+ 2	0.0000+ 0		0.0000+ 0	4.7658+ 3
5.0000- 0	0.3232+ 2	6.7014+ 0							0.0000+ 2	0.0000+ 0		0.0000+ 0	4.8181+ 3
6.0000- 0	0.3048+ 2	6.7014+ 0							0.0000+ 2	0.0000+ 0		0.0000+ 0	4.8741+ 3
7.0000- 0	0.2918+ 2	6.7022+ 0							0.0000+ 2	0.0000+ 0		0.0000+ 0	4.9340+ 3
8.0000- 0	0.2838+ 2	6.7038+ 0							0.0000+ 2	0.0000+ 0		0.0000+ 0	4.9981+ 3
1.0000- 1	0.2800+ 2	6.7061+ 0							0.0000+ 2	0.0000+ 0		0.0000+ 0	5.0666+ 3
2.0000- 1	0.2800+ 2	6.7091+ 0							0.0000+ 2	0.0000+ 0		0.0000+ 0	5.1398+ 3
3.0000- 1	0.2829+ 2	6.7136+ 0							0.0000+ 2	0.0000+ 0		0.0000+ 0	5.2179+ 3
4.0000- 1	0.2879+ 2	6.7195+ 0							0.0000+ 2	0.0000+ 0		0.0000+ 0	5.3014+ 3
5.0000- 1	0.2948+ 2	6.7268+ 0							0.0000+ 2	0.0000+ 0		0.0000+ 0	5.3908+ 3
6.0000- 1	0.3038+ 2	6.7355+ 0							0.0000+ 2	0.0000+ 0		0.0000+ 0	5.4865+ 3
7.0000- 1	0.3149+ 2	6.7457+ 0							0.0000+ 2	0.0000+ 0		0.0000+ 0	5.5891+ 3
8.0000- 1	0.3282+ 2	6.7574+ 0							0.0000+ 2	0.0000+ 0		0.0000+ 0	5.6991+ 3
1.0000- 0	0.3438+ 2	6.7706+ 0							0.0000+ 2	0.0000+ 0		0.0000+ 0	5.8169+ 3
2.0000- 0	0.3618+ 2	6.7854+ 0							0.0000+ 2	0.0000+ 0		0.0000+ 0	5.9430+ 3
3.0000- 0	0.3824+ 2	6.8018+ 0							0.0000+ 2	0.0000+ 0		0.0000+ 0	6.0781+ 3
4.0000- 0	0.4060+ 2	6.8198+ 0							0.0000+ 2	0.0000+ 0		0.0000+ 0	6.2230+ 3
5.0000- 0	0.4329+ 2	6.8394+ 0							0.0000+ 2	0.0000+ 0		0.0000+ 0	6.3787+ 3
6.0000- 0	0.4634+ 2	6.8606+ 0							0.0000+ 2	0.0000+ 0		0.0000+ 0	6.5458+ 3
7.0000- 0	0.4979+ 2	6.8836+ 0							0.0000+ 2	0.0000+ 0		0.0000+ 0	6.7256+ 3
8.0000- 0	0.5368+ 2	6.9088+ 0							0.0000+ 2	0.0000+ 0		0.0000+ 0	6.9195+ 3
1.0000- 1	0.5805+ 2	6.9364+ 0							0.0000+ 2	0.0000+ 0		0.0000+ 0	7.1287+ 3
2.0000- 1	0.6294+ 2	6.9666+ 0							0.0000+ 2	0.0000+ 0		0.0000+ 0	7.3547+ 3
3.0000- 1	0.6848+ 2	7.0000+ 0							0.0000+ 2	0.0000+ 0		0.0000+ 0	7.6000+ 3
4.0000- 1	0.7480+ 2	7.0378+ 0							0.0000+ 2	0.0000+ 0		0.0000+ 0	7.8681+ 3
5.0000- 1	0.8206+ 2	7.0800+ 0							0.0000+ 2	0.0000+ 0		0.0000+ 0	8.1619+ 3
6.0000- 1	0.9044+ 2	7.1278+ 0							0.0000+ 2	0.0000+ 0		0.0000+ 0	8.4854+ 3
7.0000- 1	0.9999+ 2	7.1814+ 0							0.0000+ 2	0.0000+ 0		0.0000+ 0	8.8421+ 3
8.0000- 1	1.1086+ 2	7.2418+ 0							0.0000+ 2	0.0000+ 0		0.0000+ 0	9.2361+ 3
1.0000- 0	1.2324+ 2	7.3094+ 0							0.0000+ 2	0.0000+ 0		0.0000+ 0	9.6711+ 3
2.0000- 0	1.3732+ 2	7.3844+ 0							0.0000+ 2	0.0000+ 0		0.0000+ 0	10.1514+ 3
3.0000- 0	1.5332+ 2	7.4678+ 0							0.0000+ 2	0.0000+ 0		0.0000+ 0	10.6806+ 3
4.0000- 0	1.7148+ 2	7.5600+ 0							0.0000+ 2	0.0000+ 0		0.0000+ 0	11.2634+ 3
5.0000- 0	1.9206+ 2	7.6624+ 0							0.0000+ 2	0.0000+ 0		0.0000+ 0	11.9054+ 3
6.0000- 0	2.1558+ 2	7.7858+ 0							0.0000+ 2	0.0000+ 0		0.0000+ 0	12.6134+ 3
7.0000- 0	2.4244+ 2	7.9314+ 0							0.0000+ 2	0.0000+ 0		0.0000+ 0	13.3944+ 3
8.0000- 0	2.7314+ 2	8.0918+ 0							0.0000+ 2	0.0000+ 0		0.0000+ 0	14.2554+ 3
1.0000- 1	3.0814+ 2	8.2684+ 0							0.0000+ 2	0.0000+ 0		0.0000+ 0	15.2044+ 3
2.0000- 1	3.4784+ 2	8.4624+ 0							0.0000+ 2	0.0000+ 0		0.0000+ 0	16.2494+ 3
3.0000- 1	3.9274+ 2	8.6748+ 0							0.0000+ 2	0.0000+ 0		0.0000+ 0	17.3914+ 3
4.0000- 1	4.4364+ 2	8.9068+ 0							0.0000+ 2	0.0000+ 0		0.0000+ 0	18.6314+ 3
5.0000- 1	5.0134+ 2	9.1604+ 0							0.0000+ 2	0.0000+ 0		0.0000+ 0	19.9714+ 3
6.0000- 1	5.6664+ 2	9.4368+ 0							0.0000+ 2	0.0000+ 0		0.0000+ 0	21.4174+ 3
7.0000- 1	6.4044+ 2	9.7374+ 0							0.0000+ 2	0.0000+ 0		0.0000+ 0	22.9754+ 3
8.0000- 1	7.2384+ 2	10.0644+ 0							0.0000+ 2	0.0000+ 0		0.0000+ 0	24.6514+ 3
1.0000- 0	8.1824+ 2	10.4194+ 0							0.0000+ 2	0.0000+ 0		0.0000+ 0	26.4514+ 3
2.0000- 0	9.2484+ 2	10.8044+ 0							0.0000+ 2	0.0000+ 0		0.0000+ 0	28.3814+ 3
3.0000- 0	10.4484+ 2	11.2194+ 0							0.0000+ 2	0.0000+ 0		0.0000+ 0	30.4474+ 3
4.0000- 0	11.7984+ 2	11.6664+ 0							0.0000+ 2	0.0000+ 0		0.0000+ 0	32.6554+ 3
5.0000- 0	13.3044+ 2	12.1464+ 0							0.0000+ 2	0.0000+ 0		0.0000+ 0	35.0114+ 3
6.0000- 0	14.9844+ 2	12.6614+ 0							0.0000+ 2	0.0000+ 0		0.0000+ 0	37.5314+ 3
7.0000- 0	16.8544+ 2	13.2144+ 0							0.0000+ 2	0.0000+ 0		0.0000+ 0	40.2214+ 3
8.0000- 0	18.9244+ 2	13.8094+ 0							0.0000+ 2	0.0000+ 0		0.0000+ 0	43.0894+ 3
1.0000- 1	21.2984+ 2	14.4494+ 0							0.0000+ 2	0.0000+ 0		0.0000+ 0	46.1414+ 3
2.0000- 1	24.0044+ 2	15.1364+ 0							0.0000+ 2	0.0000+ 0		0.0000+ 0	49.3854+ 3
3.0000- 1	27.0644+ 2	15.8744+ 0							0.0000+ 2	0.0000+ 0		0.0000+ 0	52.9294+ 3
4.0000- 1	30.5044+ 2	16.6684+ 0							0.0000+ 2	0.0000+ 0		0.0000+ 0	56.7814+ 3
5.0000- 1	34.3644+ 2	17.5244+ 0							0.0000+ 2	0.0000+ 0		0.0000+ 0	60.9514+ 3
6.0000- 1	38.6744+ 2	18.4484+ 0							0.0000+ 2	0.0000+ 0		0.0000+ 0	65.4594+ 3
7.0000- 1	43.4744+ 2	19.4464+ 0							0.0000+ 2	0.0000+ 0		0.0000+ 0	70.3174+ 3
8.0000- 1	48.8144+ 2	20.5244+ 0											

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CROSS SECTION

MATERIAL =2724

ENERGY	TOTAL	ELASTIC	INELR	(N,2N)	(N,3N)	FISSON	(N,NA)	(N,MP)	CAPTURE	(N,P)	(N,D)	(N,R)	MU-BRR
1.0000-5	1.0000-2	5.0000+0							2.6480+2			0.0000+0	5.8600-3
1.0000-4	1.2011+2	5.0000+0							1.7643+2			0.0000+0	5.8980-3
1.0000-3	1.0957+2	5.0000+0							1.7024+2			0.0000+0	4.0014-3
1.0000-2	6.8124+1	5.0000+0							8.6575+0			0.0000+0	4.0193-3
1.0000-1	6.5311+1	5.0000+0							7.0332+1			0.0000+0	4.0297-3
5.0000-2	6.9378+1	5.0000+0							6.0854+1			0.0000+0	4.0375-3
5.0000-1	6.2656+1	5.0000+0							5.1644+1			0.0000+0	4.0510-3
8.0000-2	1.8661+1	5.0000+0							4.1388+1			0.0000+0	4.0588-3
1.0000-1	3.9931+1	4.9950+0							3.4837+1			0.0000+0	4.0687-3
1.5000-1	3.4211+1	4.9850+0							2.9093+1			0.0000+0	4.0782-3
2.0000-1	3.0487+1	4.9676+0							2.5238+1			0.0000+0	4.0866-3
3.0000-1	2.7936+1	4.9500+0							2.0886+1			0.0000+0	4.1092-3
4.0000-1	2.6314+1	4.9350+0							1.8389+1			0.0000+0	4.1144-3
5.0000-1	2.5194+1	4.9250+0							1.6889+1			0.0000+0	4.1218-3
6.0000-1	2.4374+1	4.9150+0							1.5809+1			0.0000+0	4.1285-3
8.0000-1	2.0147+1	4.2556+0							1.5889+1			0.0000+0	4.1285-3
1.0000+0	1.7114+1	2.1551+0							1.4958+1			0.0000+0	4.1395-3
1.5000+0	1.4979+1	1.8792+0							1.4791+1			0.0000+0	4.1499-3
2.0000+0	1.3407+1	1.6632+0							1.6220+1			0.0000+0	4.1609-3
3.0000+0	1.1036+1	1.1036+0							2.0914+1			0.0000+0	4.1712-3
4.0000+0	1.4909+1	4.4909+0							2.0398+1			0.0000+0	4.1824-3
5.0000+0	3.8159+1	5.7216+1							5.0398+1			0.0000+0	4.1824-3
6.0000+0	7.8253+1	5.7216+1							6.6834+1			0.0000+0	4.1824-3
8.0000+0	1.5093+3	5.0273+2							4.9260+2			0.0000+0	4.2003-3
1.0000+1	4.8370+1	3.5252+1							1.3088+0			0.0000+0	4.2003-3
1.5000+1	1.7905+1	1.5337+1							5.4979+0			0.0000+0	4.2003-3
2.0000+1	6.0797+0	8.9360+0							1.7970+0			0.0000+0	4.2003-3
3.0000+1	7.5814+0	7.4931+0							8.8560+0			0.0000+0	4.2003-3
4.0000+1	7.5814+0	7.4931+0							5.3837+0			0.0000+0	4.2003-3
5.0000+1	7.0166+0	6.4498+0							3.5455+0			0.0000+0	4.2003-3
6.0000+1	6.4840+0	6.4498+0							1.3088+0			0.0000+0	4.2003-3
8.0000+1	1.1000+2	5.8522+0							4.9727+0			0.0000+0	4.2003-3
1.0000+2	1.1104+1	6.1310+0							6.0458+0			0.0000+0	4.2003-3
1.5000+2	1.2294+1	8.2481+0							1.9006+0			0.0000+0	4.2003-3
2.0000+2	9.4817+1	4.8670+1							4.2019+0			0.0000+0	4.2003-3
3.0000+2	6.3081+1	4.8670+1							9.6582+0			0.0000+0	4.2003-3
4.0000+2	2.8939+1	4.6562+1							3.5199+0			0.0000+0	4.2003-3
5.0000+2	5.6644+1	6.2124+1							1.2812+0			0.0000+0	4.2003-3
6.0000+2	1.4016+1	1.2786+1							1.8705+0			0.0000+0	4.2003-3
1.0000+3	4.1945+1	3.9874+1							1.8705+0			0.0000+0	4.2003-3
1.5000+3	2.2463+1	2.1007+1							1.3760+0			0.0000+0	4.2003-3
2.0000+3	1.6895+1	1.6806+1							1.0298+0			0.0000+0	4.2003-3
3.0000+3	1.8177+1	1.7338+1							9.4113+0			0.0000+0	4.2003-3
4.0000+3	1.7003+1	1.5281+1							6.1104+0			0.0000+0	4.2003-3
5.0000+3	1.5793+1	1.3083+1							5.1801+0			0.0000+0	4.2003-3
6.0000+3	1.4606+1	1.4088+1							4.3346+0			0.0000+0	4.2003-3
1.0000+4	1.3353+1	1.2920+1							3.0056+0			0.0000+0	4.2003-3
1.5000+4	1.2119+1	1.1759+1							2.7058+0			0.0000+0	4.2003-3
2.0000+4	1.1079+1	9.0789+0							2.4492+0			0.0000+0	4.2003-3
3.0000+4	9.5463+0	8.2698+0							1.8705+0			0.0000+0	4.2003-3
4.0000+4	8.5483+0	8.2698+0							1.8705+0			0.0000+0	4.2003-3
5.0000+4	8.0773+0	8.6419+0							1.8705+0			0.0000+0	4.2003-3
6.0000+4	8.6519+0	8.4301+0							2.2179+0			0.0000+0	4.2003-3
8.0000+4	8.2623+0	8.0348+0							2.0410+0			0.0000+0	4.2003-3
1.0000+5	7.8351+0	7.5041+0							1.3425+0			0.0000+0	1.7722-1
1.5000+5	7.4848+0	7.0133+0							1.0377+0			0.0000+0	2.2632-1
2.0000+5	7.2718+0	6.6489+0							8.9935+0			0.0000+0	2.7897-1
3.0000+5	7.2018+0	6.4093+0							7.2694+0			0.0000+0	3.2589-1
4.0000+5	7.2484+0	6.2521+0							7.9199+0			0.0000+0	3.1839-1
5.0000+5	7.2484+0	6.2521+0							7.9199+0			0.0000+0	3.1839-1
6.0000+5	7.4648+0	6.2350+0							9.3688+0			0.0000+0	4.1544+1
8.0000+5	7.6817+0	6.1858+0							9.5558+0			0.0000+0	4.1544+1
1.0000+6	7.9006+0	6.9151+0							1.0095+0			0.0000+0	5.9592-1
1.5000+6	6.9725+0	6.3104+0							5.5100+0			0.0000+0	7.0599-1
2.0000+6	6.0605+0	3.5156+0							2.1848+0			0.0000+0	7.4483-1
3.0000+6	6.0605+0	3.5156+0							6.8010+0			0.0000+0	7.4820-1
4.0000+6	6.5427+0	2.9945+0							4.6272+0			0.0000+0	7.7178-1
5.0000+6	5.5612+0	2.7027+0							4.3379+0			0.0000+0	7.7178-1
6.0000+6	5.3593+0	2.6034+0							6.2037+0			0.0000+0	8.1611-1
8.0000+6	5.3293+0	2.6034+0							4.7361+0			0.0000+0	8.1611-1
1.0000+7	5.5603+0	3.0914+0							1.6885+0			0.0000+0	1.3767-1
1.5000+7	5.7012+0	1.7457+0							1.5122+0			0.0000+0	9.2073-1
2.0000+7	5.5603+0	3.0914+0							4.4147+0			0.0000+0	9.2073-1
3.0000+7	5.5603+0	3.0914+0							1.7480+0			0.0000+0	9.2073-1
4.0000+7	5.5603+0	3.0914+0							1.7480+0			0.0000+0	9.2073-1
5.0000+7	5.5603+0	3.0914+0							1.7480+0			0.0000+0	9.2073-1
6.0000+7	5.5603+0	3.0914+0							1.7480+0			0.0000+0	9.2073-1
8.0000+7	5.5603+0	3.0914+0							1.7480+0			0.0000+0	9.2073-1

CROSS SECTION

MF-178

MATERIAL -2725

ENERGY	TOTAL	ELASTIC	INEL	(N,2N)	(N,3N)	FIBBON	(N,NA)	(N,NP)	CAPTURE	(N,P)	(N,O)	(N,A)	MU-ROR
1.0000-5	1.4488+2	6.0000+0							1.5872+2				3.9972-5
1.0000-4	7.0394+1	8.0000+0							6.4293+1				4.0482-5
1.0000-3	1.5000+0	8.0000+0							5.4523+1				4.0559-5
1.0000-2	2.0000+0	8.0000+0							4.5495+1				4.0742-5
1.0000-1	4.4423+0	8.0000+0							3.8962+1				4.0989-5
1.0000-0	3.9820+1	8.0000+0							3.7037+1				4.1084-5
1.0000+1	3.5573+1	8.0000+0							2.7168+1				4.1161-5
1.0000+2	2.8859+1	8.0000+0							2.3864+1				4.1263-5
1.0000+3	2.6376+1	8.0000+0							2.0244+1				4.1394-5
1.0000+4	2.3162+1	8.0000+0							1.4447+1				4.1532-5
1.0000+5	2.0382+1	8.0000+0							1.2090+1				4.1675-5
1.0000+6	1.6590+1	8.0000+0							1.0666+0				4.1812-5
1.0000+7	1.2866+1	8.0000+0							8.9006+0				4.1915-5
1.0000+8	1.0261+1	5.5448+0							7.6535+0				4.2039-5
1.0000+9	1.2844+1	5.5448+0							6.8546+0				4.2195-5
1.0000+10	1.1702+1	4.8955+0							6.4015+0				4.2326-5
1.0000+11	1.0933+1	4.4870+0							5.4959+0				4.2484-5
1.0000+12	1.0605+1	4.1467+0							4.8964+0				4.2653-5
1.0000+13	1.1727+1	3.6616+0							4.2817+0				4.2837-5
1.0000+14	2.1750+1	2.8650+0							3.9773+0				4.2929-5
1.0000+15	3.4856+1	8.5687+0							2.3189+0				4.3035-5
1.0000+16	8.2785+0	5.5660+0							3.5104+0				4.3128-5
1.0000+17	7.2468+0	4.5372+0							2.7059+0				4.3259-5
1.0000+18	5.5377+1	8.5677+0							4.9787+0				4.3396-5
1.0000+19	4.0076+1	4.4482+0							6.8958+0				4.3539-5
1.0000+20	1.8874+2	6.0046+1							1.5627+2				4.3677-5
1.0000+21	7.6117+1	1.3954+1							1.3669+2				4.3821-5
1.0000+22	3.4535+1	7.8774+0							2.5264+1				4.3971-5
1.0000+23	8.8548+1	3.0107+1							2.6225+1				4.4133-5
1.0000+24	1.2014+2	5.1867+1							5.8440+1				4.4300-5
1.0000+25	8.3972+1	6.2163+1							6.8273+1				4.4484-5
1.0000+26	1.0083+2	6.1830+1							5.1507+1				4.4672-5
1.0000+27	4.8650+1	2.6927+1							2.0266+1				4.4873-5
1.0000+28	3.9755+1	2.5264+1							1.6813+1				4.5089-5
1.0000+29	5.5033+1	2.3809+1							1.4487+1				4.5321-5
1.0000+30	9.2381+1	2.2289+1							1.2224+1				4.5570-5
1.0000+31	2.8566+1	2.0567+1							1.0081+1				4.5836-5
1.0000+32	2.4827+1	1.8758+1							8.0399+0				4.6122-5
1.0000+33	1.9322+1	1.7138+1							6.1629+0				4.6439-5
1.0000+34	1.7688+1	1.5642+1							4.7826+0				4.6781-5
1.0000+35	1.6598+1	1.4636+1							3.6597+0				4.7141-5
1.0000+36	1.5938+1	1.3851+1							3.2607+0				4.7523-5
1.0000+37	1.5598+1	1.3254+1							2.6453+0				4.7937-5
1.0000+38	1.4205+1	1.2256+1							2.2598+0				4.8392-5
1.0000+39	1.3003+1	1.1419+1							1.9083+0				4.8900-5
1.0000+40	1.1831+1	1.0539+1							1.5892+0				4.9479-5
1.0000+41	1.0054+1	8.1070+0							1.2832+0				5.0139-5
1.0000+42	8.4696+0	8.6004+0							1.0765+0				5.0886-5
1.0000+43	9.0797+0	8.3750+0							8.9794+0				5.1711-5
1.0000+44	8.8544+0	8.0200+0							7.6924+0				5.2631-5
1.0000+45	8.2572+0	8.5544+0							6.9464+0				5.3677-5
1.0000+46	7.8281+0	7.2713+0							5.7233+0				5.4857-5
1.0000+47	7.4861+0	6.9180+0							4.9508+0				5.6180-5
1.0000+48	7.1959+0	6.4738+0							4.5953+0				5.7668-5
1.0000+49	7.3335+0	6.1770+0							4.2626+0				5.9385-5
1.0000+50	7.4664+0	5.8560+0							3.8928+0				6.1359-5
1.0000+51	7.4664+0	5.5200+0							3.5297+0				6.3592-5
1.0000+52	7.5867+0	5.1597+0							3.1834+0				6.6141-5
1.0000+53	7.5867+0	4.7227+0							2.8593+0				6.9080-5
1.0000+54	6.7773+0	4.2485+0							2.5618+0				7.2454-5
1.0000+55	6.0911+0	3.7008+0							2.3000+0				7.6306-5
1.0000+56	5.5434+0	3.1834+0							2.0696+0				8.0711-5
1.0000+57	5.2644+0	2.7068+0							1.8718+0				8.5706-5
1.0000+58	5.2644+0	2.2532+0							1.7176+0				9.1406-5
1.0000+59	5.2644+0	1.7420+0							1.5609+0				9.7917-5
1.0000+60	5.2644+0	1.1742+0							1.4087+0				1.0550-4
1.0000+61	5.2644+0	7.3823+0							1.2623+0				1.2144-4
1.0000+62	5.5553+0	3.1130+0							1.1293+0				1.3926-4
1.0000+63	5.7015+0	1.2427+0							1.0081+0				1.5966-4
1.0000+64	1.5000+7	1.2427+0							0.8929+0				1.8306-4
1.0000+65	1.5000+7	1.2427+0							0.7855+0				2.1272-4
1.0000+66	1.5000+7	1.2427+0							0.6924+0				2.4862-4
1.0000+67	1.5000+7	1.2427+0							0.6129+0				2.9392-4
1.0000+68	1.5000+7	1.2427+0							0.5464+0				3.5392-4
1.0000+69	1.5000+7	1.2427+0							0.4929+0				4.3706-4
1.0000+70	1.5000+7	1.2427+0							0.4523+0				5.6146-4
1.0000+71	1.5000+7	1.2427+0							0.4236+0				7.4719-4
1.0000+72	1.5000+7	1.2427+0							0.4059+0				1.0184-3
1.0000+73	1.5000+7	1.2427+0							0.3990+0				1.3622-3
1.0000+74	1.5000+7	1.2427+0							0.3931+0				1.8464-3
1.0000+75	1.5000+7	1.2427+0							0.3881+0				2.5406-3
1.0000+76	1.5000+7	1.2427+0							0.3840+0				3.5492-3
1.0000+77	1.5000+7	1.2427+0							0.3807+0				4.9792-3
1.0000+78	1.5000+7	1.2427+0							0.3781+0				6.9922-3
1.0000+79	1.5000+7	1.2427+0							0.3761+0				9.8692-3
1.0000+80	1.5000+7	1.2427+0							0.3747+0				1.3717-2
1.0000+81	1.5000+7	1.2427+0							0.3739+0				1.9171-2
1.0000+82	1.5000+7	1.2427+0							0.3736+0				2.6622-2
1.0000+83	1.5000+7	1.2427+0							0.3737+0				3.6891-2
1.0000+84	1.5000+7	1.2427+0							0.3742+0				5.1691-2
1.0000+85	1.5000+7	1.2427+0							0.3751+0				7.2422-2
1.0000+86	1.5000+7	1.2427+0							0.3764+0				1.0184-1
1.0000+87	1.5000+7	1.2427+0							0.3781+0				1.4072-1
1.0000+88	1.5000+7	1.2427+0							0.3802+0				1.9491-1
1.0000+89	1.5000+7	1.2427+0							0.3827+0				2.7292-1
1.0000+90	1.5000+7	1.2427+0							0.3857+0				3.8079-1
1.0000+91	1.5000+7	1.2427+0							0.3891+0				5.2492-1
1.0000+92	1.5000+7	1.2427+0							0.3929+0				7.2422-1

MF-18D

CROSS SECTION

MATERIAL	ENERGY	TOTAL	ELASTIC	INELR	(N.2N)	(N.3N)	FIBSION	(N.NR)	(N.NP)	CAPTURE	(N.P)	(N.O)	(N.A)	MU-BRR
1.0000	5 ~ 1.0000-2	7.7222+1	3.8388+1							3.8821+1			0.0000+0	3.8425-9
1.0000	1.5000	9.8717+1	2.0817+1							1.7999+0			0.0000+0	2.8485-9
1.0000	2.0000	1.2297+1	1.9478+1							1.6176+0			0.0000+0	2.9589-9
1.0000	2.5000	2.2297+1	1.9478+1							1.2738+0			0.0000+0	3.9791-9
1.0000	3.0000	4.0052+1	1.9030+1							0.4698+0			0.0000+0	3.9887-9
1.0000	4.0000	2.8598+1	1.9095+1							0.5524+0			0.0000+0	3.9928-9
1.0000	5.0000	2.7721+1	1.9139+1							7.5845+0			0.0000+0	3.9997-9
1.0000	6.0000	2.6381+1	1.9163+1							7.5845+0			0.0000+0	4.0072-9
1.0000	7.0000	2.5000+1	1.9186+1							5.6883+0			0.0000+0	4.0168-9
1.0000	8.0000	2.4394+1	1.9208+1							4.8023+0			0.0000+0	4.0270-9
1.0000	9.0000	2.3822+1	1.9229+1							4.0266+0			0.0000+0	4.0375-9
1.0000	1.0000	1.7199+1	1.8800+1							3.3874+0			0.0000+0	4.0470-9
1.0000	1.5000	2.0836+1	1.8057+1							2.9505+0			0.0000+0	4.0560-9
1.0000	2.0000	2.0836+1	1.8057+1							2.4773+0			0.0000+0	4.0640-9
1.0000	3.0000	2.0460+1	1.8003+1							2.1469+0			0.0000+0	4.0715-9
1.0000	4.0000	1.7932+1	1.7932+1							1.7966+0			0.0000+0	4.0790-9
1.0000	5.0000	1.8606+1	1.7810+1							1.4671+0			0.0000+0	4.0852-9
1.0000	6.0000	1.8176+1	1.7639+1							1.4671+0			0.0000+0	4.0918-9
1.0000	7.0000	1.8598+1	1.7390+1							9.7763+0			0.0000+0	4.1058-9
1.0000	8.0000	1.8650+1	1.7072+1							8.9168+0			0.0000+0	4.1160-9
1.0000	9.0000	1.7803+1	1.6480+1							7.2275+0			0.0000+0	4.1235-9
1.0000	1.0000	1.6678+1	1.6071+1							6.0717+0			0.0000+0	4.1284-9
1.0000	1.5000	1.6062+1	1.5563+1							4.9584+0			0.0000+0	4.1340-9
1.0000	2.0000	1.5159+1	1.4778+1							3.8106+0			0.0000+0	4.1397-9
1.0000	3.0000	1.4805+1	1.4082+1							2.7688+0			0.0000+0	4.1453-9
1.0000	4.0000	1.4466+1	1.3524+1							1.9620+0			0.0000+0	4.1509-9
1.0000	5.0000	1.4168+1	1.3026+1							1.3907+0			0.0000+0	4.1565-9
1.0000	6.0000	1.3907+1	1.2572+1							1.5270+0			0.0000+0	4.1619-9
1.0000	7.0000	1.3683+1	1.2142+1							7.0631+0			0.0000+0	4.1678-9
1.0000	8.0000	1.3493+1	1.1723+1							1.3555+0			0.0000+0	4.1735-9
1.0000	9.0000	1.3328+1	1.1323+1							4.8488+0			0.0000+0	4.1792-9
1.0000	1.0000	8.5039+0	8.4554+0							2.3480+0			0.0000+0	4.1849-9
1.0000	1.5000	8.4279+0	8.4279+0							1.3684+0			0.0000+0	4.1906-9
1.0000	2.0000	8.0728+0	8.0929+0							6.5076+0			0.0000+0	4.1963-9
1.0000	3.0000	8.9573+0	8.0780+0							6.1927+0			0.0000+0	4.2020-9
1.0000	4.0000	8.2236+0	8.0192+0							2.0442+0			0.0000+0	4.2077-9
1.0000	5.0000	5.0210+1	8.0210+1							6.3743+0			0.0000+0	4.2134-9
1.0000	6.0000	1.4638+1	1.4003+1							4.8488+0			0.0000+0	4.2191-9
1.0000	7.0000	1.8916+1	1.8181+1							2.3480+0			0.0000+0	4.2248-9
1.0000	8.0000	2.2888+1	2.2408+1							1.3684+0			0.0000+0	4.2305-9
1.0000	9.0000	1.8950+1	1.8310+1							4.8488+0			0.0000+0	4.2362-9
1.0000	1.0000	1.5795+1	1.5295+1							2.0442+0			0.0000+0	4.2419-9
1.0000	1.5000	1.8140+1	1.7570+1							1.0192+0			0.0000+0	4.2476-9
1.0000	2.0000	1.2958+1	1.5411+1							3.6906+0			0.0000+0	4.2533-9
1.0000	3.0000	1.2958+1	1.5411+1							2.2320+0			0.0000+0	4.2590-9
1.0000	4.0000	1.4578+1	1.4294+1							2.8189+0			0.0000+0	4.2647-9
1.0000	5.0000	1.3328+1	1.3085+1							7.3482+0			0.0000+0	4.2704-9
1.0000	6.0000	1.2098+1	1.0826+1							4.7805+0			0.0000+0	4.2761-9
1.0000	7.0000	1.0142+1	0.9893+0							2.0710+0			0.0000+0	4.2818-9
1.0000	8.0000	9.5374+0	9.5374+0							1.5987+0			0.0000+0	4.2875-9
1.0000	9.0000	4.5000+0	4.5000+0							4.7923+0			0.0000+0	4.2932-9
1.0000	1.0000	8.0788+0	8.0788+0							3.6906+0			0.0000+0	4.2989-9
1.0000	1.5000	8.5828+0	8.5828+0							2.2320+0			0.0000+0	4.3046-9
1.0000	2.0000	8.2623+0	8.2623+0							2.8189+0			0.0000+0	4.3103-9
1.0000	3.0000	7.8351+0	7.8351+0							2.4307+0			0.0000+0	4.3160-9
1.0000	4.0000	7.4184+0	7.4184+0							1.0366+0			0.0000+0	4.3217-9
1.0000	5.0000	7.2780+0	7.2780+0							4.7805+0			0.0000+0	4.3274-9
1.0000	6.0000	7.2008+0	7.2008+0							1.8056+0			0.0000+0	4.3331-9
1.0000	7.0000	7.3333+0	7.3333+0							1.5987+0			0.0000+0	4.3388-9
1.0000	8.0000	7.4848+0	7.4848+0							1.3822+0			0.0000+0	4.3445-9
1.0000	9.0000	7.5817+0	7.5817+0							1.1809+0			0.0000+0	4.3502-9
1.0000	1.0000	5.5000+0	5.5000+0							8.7968+0			0.0000+0	4.3559-9
1.0000	1.5000	5.5000+0	5.5000+0							8.7968+0			0.0000+0	4.3616-9
1.0000	2.0000	5.5000+0	5.5000+0							3.0390+0			0.0000+0	4.3673-9
1.0000	3.0000	5.5000+0	5.5000+0							3.0390+0			0.0000+0	4.3730-9
1.0000	4.0000	5.5000+0	5.5000+0							3.0390+0			0.0000+0	4.3787-9
1.0000	5.0000	5.5000+0	5.5000+0							3.0390+0			0.0000+0	4.3844-9
1.0000	6.0000	5.5000+0	5.5000+0							3.0390+0			0.0000+0	4.3901-9
1.0000	7.0000	5.5000+0	5.5000+0							3.0390+0			0.0000+0	4.3958-9
1.0000	8.0000	5.5000+0	5.5000+0							3.0390+0			0.0000+0	4.4015-9
1.0000	9.0000	5.5000+0	5.5000+0							3.0390+0			0.0000+0	4.4072-9
1.0000	1.0000	6.0000+0	6.0000+0							3.0390+0			0.0000+0	4.4129-9
1.0000	1.5000	6.0000+0	6.0000+0							3.0390+0			0.0000+0	4.4186-9
1.0000	2.0000	6.0000+0	6.0000+0							3.0390+0			0.0000+0	4.4243-9
1.0000	3.0000	6.0000+0	6.0000+0							3.0390+0			0.0000+0	4.4300-9
1.0000	4.0000	6.0000+0	6.0000+0							3.0390+0			0.0000+0	4.4357-9
1.0000	5.0000	6.0000+0	6.0000+0							3.0390+0			0.0000+0	4.4414-9
1.0000	6.0000	6.0000+0	6.0000+0							3.0390+0			0.0000+0	4.4471-9
1.0000	7.0000	6.0000+0	6.0000+0							3.0390+0			0.0000+0	4.4528-9
1.0000	8.0000	6.0000+0	6.0000+0							3.0390+0			0.0000+0	4.4585-9
1.0000	9.0000	6.0000+0	6.0000+0							3.0390+0			0.0000+0	4.4642-9
1.0000	1.0000	6.0000+0	6.0000+0							3.0390+0			0.0000+0	4.4699-9
1.0000	1.5000	6.0000+0	6.0000+0							3.0390+0			0.0000+0	4.4756-9
1.0000	2.0000	6.0000+0	6.0000+0							3.0390+0			0.0000+0	4.4813-9
1.0000	3.0000	6.0000+0	6.0000+0							3.0390+0			0.0000+0	4.4870-9
1.0000	4.0000	6.0000+0	6.0000+0											

TA-181

CROSS SECTION

MATERIAL	ENERGY	TOTAL	ELASTIC	INELR	(N.2N)	(N.3N)	FISSION	(N.WA)	(N.NP)	CAPTURE	(N.P)	(N.D)	(N.R)	MU-BRR
1.0000	~ 1.0000-2	7.1336+ 1	6.1174+ 0							6.5249+ 1				3.7162- 3
1.0000	2	3.6482+ 1	3.1148+ 0							3.0887+ 1				3.7162- 3
1.0000	3	1.5000+ 1	1.4507+ 0							2.5669+ 1				3.7162- 3
1.0000	4	1.5000+ 1	1.4507+ 0							1.8196+ 1				3.7162- 3
1.0000	5	1.5000+ 1	1.4507+ 0							1.6046+ 1				3.7162- 3
1.0000	6	1.5000+ 1	1.4507+ 0							1.4638+ 1				3.7162- 3
1.0000	7	1.5000+ 1	1.4507+ 0							1.2888+ 1				3.7162- 3
1.0000	8	1.5000+ 1	1.4507+ 0							1.1502+ 1				3.7162- 3
1.0000	9	1.5000+ 1	1.4507+ 0							9.9103+ 0				3.7162- 3
1.0000	10	1.5000+ 1	1.4507+ 0							8.4500+ 0				3.7162- 3
1.0000	11	1.5000+ 1	1.4507+ 0							7.2544+ 0				3.7162- 3
1.0000	12	1.5000+ 1	1.4507+ 0							6.3058+ 0				3.7162- 3
1.0000	13	1.5000+ 1	1.4507+ 0							5.4758+ 0				3.7162- 3
1.0000	14	1.5000+ 1	1.4507+ 0							4.8209+ 0				3.7162- 3
1.0000	15	1.5000+ 1	1.4507+ 0							4.3933+ 0				3.7162- 3
1.0000	16	1.5000+ 1	1.4507+ 0							4.0645+ 0				3.7162- 3
1.0000	17	1.5000+ 1	1.4507+ 0							3.8203+ 0				3.7162- 3
1.0000	18	1.5000+ 1	1.4507+ 0							3.6455+ 0				3.7162- 3
1.0000	19	1.5000+ 1	1.4507+ 0							3.5203+ 0				3.7162- 3
1.0000	20	1.5000+ 1	1.4507+ 0							3.4203+ 0				3.7162- 3
1.0000	21	1.5000+ 1	1.4507+ 0							3.3394+ 0				3.7162- 3
1.0000	22	1.5000+ 1	1.4507+ 0							3.2729+ 0				3.7162- 3
1.0000	23	1.5000+ 1	1.4507+ 0							3.2186+ 0				3.7162- 3
1.0000	24	1.5000+ 1	1.4507+ 0							3.1754+ 0				3.7162- 3
1.0000	25	1.5000+ 1	1.4507+ 0							3.1423+ 0				3.7162- 3
1.0000	26	1.5000+ 1	1.4507+ 0							3.1180+ 0				3.7162- 3
1.0000	27	1.5000+ 1	1.4507+ 0							3.0993+ 0				3.7162- 3
1.0000	28	1.5000+ 1	1.4507+ 0							3.0845+ 0				3.7162- 3
1.0000	29	1.5000+ 1	1.4507+ 0							3.0729+ 0				3.7162- 3
1.0000	30	1.5000+ 1	1.4507+ 0							3.0638+ 0				3.7162- 3
1.0000	31	1.5000+ 1	1.4507+ 0							3.0559+ 0				3.7162- 3
1.0000	32	1.5000+ 1	1.4507+ 0							3.0490+ 0				3.7162- 3
1.0000	33	1.5000+ 1	1.4507+ 0							3.0430+ 0				3.7162- 3
1.0000	34	1.5000+ 1	1.4507+ 0							3.0378+ 0				3.7162- 3
1.0000	35	1.5000+ 1	1.4507+ 0							3.0333+ 0				3.7162- 3
1.0000	36	1.5000+ 1	1.4507+ 0							3.0294+ 0				3.7162- 3
1.0000	37	1.5000+ 1	1.4507+ 0							3.0260+ 0				3.7162- 3
1.0000	38	1.5000+ 1	1.4507+ 0							3.0231+ 0				3.7162- 3
1.0000	39	1.5000+ 1	1.4507+ 0							3.0206+ 0				3.7162- 3
1.0000	40	1.5000+ 1	1.4507+ 0							3.0184+ 0				3.7162- 3
1.0000	41	1.5000+ 1	1.4507+ 0							3.0164+ 0				3.7162- 3
1.0000	42	1.5000+ 1	1.4507+ 0							3.0146+ 0				3.7162- 3
1.0000	43	1.5000+ 1	1.4507+ 0							3.0130+ 0				3.7162- 3
1.0000	44	1.5000+ 1	1.4507+ 0							3.0116+ 0				3.7162- 3
1.0000	45	1.5000+ 1	1.4507+ 0							3.0104+ 0				3.7162- 3
1.0000	46	1.5000+ 1	1.4507+ 0							3.0093+ 0				3.7162- 3
1.0000	47	1.5000+ 1	1.4507+ 0							3.0084+ 0				3.7162- 3
1.0000	48	1.5000+ 1	1.4507+ 0							3.0076+ 0				3.7162- 3
1.0000	49	1.5000+ 1	1.4507+ 0							3.0069+ 0				3.7162- 3
1.0000	50	1.5000+ 1	1.4507+ 0							3.0063+ 0				3.7162- 3
1.0000	51	1.5000+ 1	1.4507+ 0							3.0058+ 0				3.7162- 3
1.0000	52	1.5000+ 1	1.4507+ 0							3.0053+ 0				3.7162- 3
1.0000	53	1.5000+ 1	1.4507+ 0							3.0049+ 0				3.7162- 3
1.0000	54	1.5000+ 1	1.4507+ 0							3.0045+ 0				3.7162- 3
1.0000	55	1.5000+ 1	1.4507+ 0							3.0041+ 0				3.7162- 3
1.0000	56	1.5000+ 1	1.4507+ 0							3.0037+ 0				3.7162- 3
1.0000	57	1.5000+ 1	1.4507+ 0							3.0033+ 0				3.7162- 3
1.0000	58	1.5000+ 1	1.4507+ 0							3.0029+ 0				3.7162- 3
1.0000	59	1.5000+ 1	1.4507+ 0							3.0025+ 0				3.7162- 3
1.0000	60	1.5000+ 1	1.4507+ 0							3.0021+ 0				3.7162- 3
1.0000	61	1.5000+ 1	1.4507+ 0							3.0017+ 0				3.7162- 3
1.0000	62	1.5000+ 1	1.4507+ 0							3.0013+ 0				3.7162- 3
1.0000	63	1.5000+ 1	1.4507+ 0							3.0009+ 0				3.7162- 3
1.0000	64	1.5000+ 1	1.4507+ 0							3.0005+ 0				3.7162- 3
1.0000	65	1.5000+ 1	1.4507+ 0							3.0001+ 0				3.7162- 3
1.0000	66	1.5000+ 1	1.4507+ 0							3.0000+ 0				3.7162- 3
1.0000	67	1.5000+ 1	1.4507+ 0							3.0000+ 0				3.7162- 3
1.0000	68	1.5000+ 1	1.4507+ 0							3.0000+ 0				3.7162- 3
1.0000	69	1.5000+ 1	1.4507+ 0							3.0000+ 0				3.7162- 3
1.0000	70	1.5000+ 1	1.4507+ 0							3.0000+ 0				3.7162- 3
1.0000	71	1.5000+ 1	1.4507+ 0							3.0000+ 0				3.7162- 3
1.0000	72	1.5000+ 1	1.4507+ 0							3.0000+ 0				3.7162- 3
1.0000	73	1.5000+ 1	1.4507+ 0							3.0000+ 0				3.7162- 3
1.0000	74	1.5000+ 1	1.4507+ 0							3.0000+ 0				3.7162- 3
1.0000	75	1.5000+ 1	1.4507+ 0							3.0000+ 0				3.7162- 3
1.0000	76	1.5000+ 1	1.4507+ 0							3.0000+ 0				3.7162- 3
1.0000	77	1.5000+ 1	1.4507+ 0							3.0000+ 0				3.7162- 3
1.0000	78	1.5000+ 1	1.4507+ 0							3.0000+ 0				3.7162- 3
1.0000	79	1.5000+ 1	1.4507+ 0							3.0000+ 0				3.7162- 3
1.0000	80	1.5000+ 1	1.4507+ 0							3.0000+ 0				3.7162- 3
1.0000	81	1.5000+ 1	1.4507+ 0							3.0000+ 0				3.7162- 3
1.0000	82	1.5000+ 1	1.4507+ 0							3.0000+ 0				3.7162- 3
1.0000	83	1.5000+ 1	1.4507+ 0							3.0000+ 0				3.7162- 3
1.0000	84	1.5000+ 1	1.4507+ 0							3.0000+ 0				3.7162- 3
1.0000	85	1.5000+ 1	1.4507+ 0							3.0000+ 0				3.7162- 3
1.0000	86	1.5000+ 1	1.4507+ 0							3.0000+ 0				3.7162- 3
1.0000	87	1.5000+ 1	1.4507+ 0							3.0000+ 0				3.7162- 3
1.0000	88	1.5000+ 1	1.4507+ 0							3.0000+ 0				3.7162- 3
1.0000	89	1.5000+ 1	1.4507+ 0							3.0000+ 0				3.7162- 3
1.0000	90	1.5000+ 1	1.4507+ 0							3.0000+ 0				3.7162- 3
1.0000	91	1.5000+ 1	1.4507+ 0							3.0000+ 0				3.7162- 3
1.0000	92	1.5000+ 1	1.4507+ 0											

CROSS SECTION

PB-0

MATERIAL = 2020

ENERGY	TOTAL	ELASTIC	INEL	(N.2K)	(N.3N)	PIE610N	(N.NR)	(N.NP)	CAPTURE	(N.F)	(N.D)	(N.A)	NU-BAR
1.0000-5	1.1569+1	1.1421+1					0.0000+0	0.0000+0	5.3100-1	0.0000+0		0.0000+0	4.0610-4
1.0000-4	1.1678+1	1.1421+1					0.0000+0	0.0000+0	2.4620-1	0.0000+0		0.0000+0	4.0750-4
1.0000-3	1.1842+1	1.1421+1					0.0000+0	0.0000+0	2.0793-1	0.0000+0		0.0000+0	4.0817-4
2.0000-3	1.1959+1	1.1421+1					0.0000+0	0.0000+0	1.7435-1	0.0000+0		0.0000+0	4.0854-4
3.0000-3	1.2077+1	1.1421+1					0.0000+0	0.0000+0	1.5029-1	0.0000+0		0.0000+0	4.0884-4
4.0000-3	1.2197+1	1.1421+1					0.0000+0	0.0000+0	1.3160-1	0.0000+0		0.0000+0	4.1004-4
5.0000-3	1.2319+1	1.1421+1					0.0000+0	0.0000+0	1.1690-1	0.0000+0		0.0000+0	4.1104-4
6.0000-3	1.2443+1	1.1421+1					0.0000+0	0.0000+0	1.0465-1	0.0000+0		0.0000+0	4.1191-4
8.0000-2	1.2569+1	1.1421+1					0.0000+0	0.0000+0	9.1599-2	0.0000+0		0.0000+0	4.1141-4
1.0000-1	1.1504+1	1.1421+1					0.0000+0	0.0000+0	7.7805-2	0.0000+0		0.0000+0	4.1205-4
1.5000-1	1.1500+1	1.1421+1					0.0000+0	0.0000+0	6.5570-2	0.0000+0		0.0000+0	4.1272-4
2.0000-1	1.1494+1	1.1421+1					0.0000+0	0.0000+0	5.5091-2	0.0000+0		0.0000+0	4.1342-4
3.0000-1	1.1488+1	1.1421+1					0.0000+0	0.0000+0	4.6442-2	0.0000+0		0.0000+0	4.1410-4
4.0000-1	1.1481+1	1.1421+1					0.0000+0	0.0000+0	4.0887-2	0.0000+0		0.0000+0	4.1480-4
5.0000-1	1.1475+1	1.1421+1					0.0000+0	0.0000+0	3.5925-2	0.0000+0		0.0000+0	4.1550-4
6.0000-1	1.1468+1	1.1421+1					0.0000+0	0.0000+0	3.1575-2	0.0000+0		0.0000+0	4.1617-4
8.0000-1	1.1464+1	1.1421+1					0.0000+0	0.0000+0	2.6880-2	0.0000+0		0.0000+0	4.1597-4
1.0000+0	1.1476+1	1.1421+1					0.0000+0	0.0000+0	2.4623-2	0.0000+0		0.0000+0	4.1661-4
3.0000+0	1.1444+1	1.1421+1					0.0000+0	0.0000+0	2.0765-2	0.0000+0		0.0000+0	4.1758-4
5.0000+0	1.1442+1	1.1421+1					0.0000+0	0.0000+0	1.7468-2	0.0000+0		0.0000+0	4.1865-4
8.0000+0	1.1440+1	1.1421+1					0.0000+0	0.0000+0	1.4653-2	0.0000+0		0.0000+0	4.1915-4
1.0000+1	1.1438+1	1.1421+1					0.0000+0	0.0000+0	1.2913-2	0.0000+0		0.0000+0	4.1955-4
3.0000+1	1.1437+1	1.1421+1					0.0000+0	0.0000+0	1.1723-2	0.0000+0		0.0000+0	4.1995-4
5.0000+1	1.1436+1	1.1421+1					0.0000+0	0.0000+0	1.1063-2	0.0000+0		0.0000+0	4.2035-4
8.0000+1	1.1435+1	1.1420+1					0.0000+0	0.0000+0	9.1921-3	0.0000+0		0.0000+0	4.2075-4
1.0000+2	1.1429+1	1.1420+1					0.0000+0	0.0000+0	7.7957-3	0.0000+0		0.0000+0	4.2124-4
3.0000+2	1.1428+1	1.1420+1					0.0000+0	0.0000+0	6.5698-3	0.0000+0		0.0000+0	4.2173-4
5.0000+2	1.1427+1	1.1420+1					0.0000+0	0.0000+0	5.5166-3	0.0000+0		0.0000+0	4.2222-4
8.0000+2	1.1426+1	1.1420+1					0.0000+0	0.0000+0	4.6407-3	0.0000+0		0.0000+0	4.2271-4
1.0000+3	1.1425+1	1.1419+1					0.0000+0	0.0000+0	3.9078-3	0.0000+0		0.0000+0	4.2320-4
3.0000+3	1.1424+1	1.1419+1					0.0000+0	0.0000+0	3.2848-3	0.0000+0		0.0000+0	4.2369-4
5.0000+3	1.1423+1	1.1419+1					0.0000+0	0.0000+0	2.8011-3	0.0000+0		0.0000+0	4.2418-4
8.0000+3	1.1422+1	1.1418+1					0.0000+0	0.0000+0	2.4084-3	0.0000+0		0.0000+0	4.2467-4
1.0000+4	1.1419+1	1.1417+1					0.0000+0	0.0000+0	2.0684-3	0.0000+0		0.0000+0	4.2516-4
3.0000+4	1.1418+1	1.1416+1					0.0000+0	0.0000+0	1.7523-3	0.0000+0		0.0000+0	4.2565-4
5.0000+4	1.1417+1	1.1415+1					0.0000+0	0.0000+0	1.4888-3	0.0000+0		0.0000+0	4.2614-4
8.0000+4	1.1416+1	1.1414+1					0.0000+0	0.0000+0	1.3161-3	0.0000+0		0.0000+0	4.2663-4
1.0000+5	1.1415+1	1.1413+1					0.0000+0	0.0000+0	1.1961-3	0.0000+0		0.0000+0	4.2712-4
3.0000+5	1.1414+1	1.1412+1					0.0000+0	0.0000+0	1.0723-3	0.0000+0		0.0000+0	4.2761-4
5.0000+5	1.1413+1	1.1411+1					0.0000+0	0.0000+0	9.7229-4	0.0000+0		0.0000+0	4.2810-4
8.0000+5	1.1412+1	1.1410+1					0.0000+0	0.0000+0	8.684-4	0.0000+0		0.0000+0	4.2859-4
1.0000+6	1.1411+1	1.1409+1					0.0000+0	0.0000+0	7.698-4	0.0000+0		0.0000+0	4.2908-4
3.0000+6	1.1410+1	1.1408+1					0.0000+0	0.0000+0	6.769-4	0.0000+0		0.0000+0	4.2957-4
5.0000+6	1.1409+1	1.1407+1					0.0000+0	0.0000+0	5.894-4	0.0000+0		0.0000+0	4.3006-4
8.0000+6	1.1408+1	1.1406+1					0.0000+0	0.0000+0	5.068-4	0.0000+0		0.0000+0	4.3055-4
1.0000+7	1.1407+1	1.1405+1					0.0000+0	0.0000+0	4.292-4	0.0000+0		0.0000+0	4.3104-4
3.0000+7	1.1406+1	1.1404+1					0.0000+0	0.0000+0	3.563-4	0.0000+0		0.0000+0	4.3153-4
5.0000+7	1.1405+1	1.1403+1					0.0000+0	0.0000+0	2.883-4	0.0000+0		0.0000+0	4.3202-4
8.0000+7	1.1404+1	1.1402+1					0.0000+0	0.0000+0	2.243-4	0.0000+0		0.0000+0	4.3251-4
1.0000+8	1.1403+1	1.1401+1					0.0000+0	0.0000+0	1.643-4	0.0000+0		0.0000+0	4.3300-4
3.0000+8	1.1402+1	1.1400+1					0.0000+0	0.0000+0	1.083-4	0.0000+0		0.0000+0	4.3349-4
5.0000+8	1.1401+1	1.1399+1					0.0000+0	0.0000+0	6.269-5	0.0000+0		0.0000+0	4.3398-4
8.0000+8	1.1400+1	1.1398+1					0.0000+0	0.0000+0	5.342-5	0.0000+0		0.0000+0	4.3447-4
1.0000+9	1.1399+1	1.1397+1					0.0000+0	0.0000+0	4.465-5	0.0000+0		0.0000+0	4.3496-4
3.0000+9	1.1398+1	1.1396+1					0.0000+0	0.0000+0	3.638-5	0.0000+0		0.0000+0	4.3545-4
5.0000+9	1.1397+1	1.1395+1					0.0000+0	0.0000+0	2.862-5	0.0000+0		0.0000+0	4.3594-4
8.0000+9	1.1396+1	1.1394+1					0.0000+0	0.0000+0	2.127-5	0.0000+0		0.0000+0	4.3643-4
1.0000+10	1.1395+1	1.1393+1					0.0000+0	0.0000+0	1.437-5	0.0000+0		0.0000+0	4.3692-4
3.0000+10	1.1394+1	1.1392+1					0.0000+0	0.0000+0	8.269-6	0.0000+0		0.0000+0	4.3741-4
5.0000+10	1.1393+1	1.1391+1					0.0000+0	0.0000+0	6.598-6	0.0000+0		0.0000+0	4.3790-4
8.0000+10	1.1392+1	1.1390+1					0.0000+0	0.0000+0	5.027-6	0.0000+0		0.0000+0	4.3839-4
1.0000+11	1.1391+1	1.1389+1					0.0000+0	0.0000+0	3.556-6	0.0000+0		0.0000+0	4.3888-4
3.0000+11	1.1390+1	1.1388+1					0.0000+0	0.0000+0	2.185-6	0.0000+0		0.0000+0	4.3937-4
5.0000+11	1.1389+1	1.1387+1					0.0000+0	0.0000+0	1.518-6	0.0000+0		0.0000+0	4.3986-4
8.0000+11	1.1388+1	1.1386+1					0.0000+0	0.0000+0	9.316-7	0.0000+0		0.0000+0	4.4035-4
1.0000+12	1.1387+1	1.1385+1					0.0000+0	0.0000+0	6.657-7	0.0000+0		0.0000+0	4.4084-4
3.0000+12	1.1386+1	1.1384+1					0.0000+0	0.0000+0	4.986-7	0.0000+0		0.0000+0	4.4133-4
5.0000+12	1.1385+1	1.1383+1					0.0000+0	0.0000+0	3.315-7	0.0000+0		0.0000+0	4.4182-4
8.0000+12	1.1384+1	1.1382+1					0.0000+0	0.0000+0	2.644-7	0.0000+0		0.0000+0	4.4231-4
1.0000+13	1.1383+1	1.1381+1					0.0000+0	0.0000+0	2.073-7	0.0000+0		0.0000+0	4.4280-4
3.0000+13	1.1382+1	1.1380+1					0.0000+0	0.0000+0	1.502-7	0.0000+0		0.0000+0	4.4329-4
5.0000+13	1.1381+1	1.1379+1					0.0000+0	0.0000+0	9.350-8	0.0000+0		0.0000+0	4.4378-4
8.0000+13	1.1380+1	1.1378+1					0.0000+0	0.0000+0	6.689-8	0.0000+0		0.0000+0	4.4427-4
1.0000+14	1.1379+1	1.1377+1					0.0000+0	0.0000+0	4.928-8	0.0000+0		0.0000+0	4.4476-4
3.0000+14	1.1378+1	1.1376+1					0.0000+0	0.0000+0	3.267-8	0.0000+0		0.0000+0	4.4525-4
5.0000+14	1.1377+1	1.1375+1					0.0000+0	0.0000+0	1.606-8	0.0000+0		0.0000+0	4.4574-4
8.0000+14	1.1376+1	1.1374+1					0.0000+0	0.0000+0	9.400-9	0.0000+0			

PB-204

CROSS SECTION

MATERIAL = 2821

	ENERGY	TOTAL	ELASTIC	INELR	(N.2N)	(N.3N)	F16SSION	(N.NR)	(K.MPI)	CAPTURE	(N.P)	(N.O)	(N.R)	MU-BR
1.0000	5 ~ 1.0000-2	1.9386+1	1.1941+1					0.0000+0		2.0452+0	0.0000+0		0.0000+0	5.8404-3
1.0000	1.5000-2	1.2309+1	1.1341+1					0.0000+0		9.4905-1	0.0000+0		0.0000+0	4.0721-3
1.0000	2.0000-2	1.2189+1	1.1341+1					0.0000+0		7.9846-1	0.0000+0		0.0000+0	4.1092-3
2.0000	2.0000-2	1.2022+1	1.1341+1					0.0000+0		5.6484-1	0.0000+0		0.0000+0	4.1192-3
3.0000	2.0000-2	1.1931+1	1.1341+1					0.0000+0		4.9949-1	0.0000+0		0.0000+0	4.1185-3
4.0000	2.0000-2	1.1876+1	1.1341+1					0.0000+0		4.5624-1	0.0000+0		0.0000+0	4.1200-3
5.0000	2.0000-2	1.1771+1	1.1341+1					0.0000+0		3.9923-1	0.0000+0		0.0000+0	4.2339-3
6.0000	2.0000-2	1.1705+1	1.1341+1					0.0000+0		3.5529-1	0.0000+0		0.0000+0	4.2659-3
8.0000	2.0000-2	1.1508+1	1.1341+1					0.0000+0		2.9988-1	0.0000+0		0.0000+0	4.2974-3
1.0000	1.5000-1	1.1553+1	1.1341+1					0.0000+0		2.5595-1	0.0000+0		0.0000+0	4.3227-3
2.0000	1.5000-1	1.1522+1	1.1341+1					0.0000+0		2.1197-1	0.0000+0		0.0000+0	4.3586-3
3.0000	1.5000-1	1.1503+1	1.1341+1					0.0000+0		1.7889-1	0.0000+0		0.0000+0	4.3981-3
4.0000	1.5000-1	1.1480+1	1.1341+1					0.0000+0		1.5250-1	0.0000+0		0.0000+0	4.4351-3
5.0000	1.5000-1	1.1462+1	1.1341+1					0.0000+0		1.3250-1	0.0000+0		0.0000+0	4.4852-3
6.0000	1.5000-1	1.1437+1	1.1341+1					0.0000+0		1.2160-1	0.0000+0		0.0000+0	4.5105-3
8.0000	1.5000-1	1.1401+1	1.1341+1					0.0000+0		1.1132-1	0.0000+0		0.0000+0	4.5380-3
1.0000	0 ~ 1.5000-0	1.1440+0	1.1341+1					0.0000+0		9.4891-2	0.0000+0		0.0000+0	4.5722-3
1.5000	0 ~ 2.0000-0	1.1430+0	1.1341+1					0.0000+0		8.7020-2	0.0000+0		0.0000+0	4.5722-3
2.0000	0 ~ 3.0000-0	1.1420+0	1.1340+1					0.0000+0		8.0187-2	0.0000+0		0.0000+0	4.6487-3
3.0000	0 ~ 5.0000-0	1.1409+0	1.1340+1					0.0000+0		7.6630-2	0.0000+0		0.0000+0	4.6857-3
4.0000	0 ~ 5.0000-0	1.1398+0	1.1340+1					0.0000+0		7.3211-2	0.0000+0		0.0000+0	4.7132-3
5.0000	0 ~ 6.0000-0	1.1386+0	1.1339+1					0.0000+0		6.9825-2	0.0000+0		0.0000+0	4.7351-3
6.0000	0 ~ 6.0000-0	1.1377+0	1.1339+1					0.0000+0		6.6499-2	0.0000+0		0.0000+0	4.7581-3
8.0000	0 ~ 8.0000-0	1.1377+0	1.1338+1					0.0000+0		6.3299-2	0.0000+0		0.0000+0	4.7868-3
1.0000	1.5000-1	1.1368+0	1.1337+1					0.0000+0		3.0180-2	0.0000+0		0.0000+0	4.8238-3
1.5000	1.5000-1	1.1357+0	1.1337+1					0.0000+0		2.5443-2	0.0000+0		0.0000+0	4.8609-3
2.0000	1.5000-1	1.1349+0	1.1333+1					0.0000+0		2.1462-2	0.0000+0		0.0000+0	4.8973-3
3.0000	1.5000-1	1.1343+0	1.1333+1					0.0000+0		1.8109-2	0.0000+0		0.0000+0	4.9337-3
4.0000	1.5000-1	1.1337+0	1.1327+1					0.0000+0		1.4984-2	0.0000+0		0.0000+0	4.9697-3
5.0000	1.5000-1	1.1325+0	1.1327+1					0.0000+0		1.3025-2	0.0000+0		0.0000+0	5.0117-3
6.0000	1.5000-1	1.1316+0	1.1319+1					0.0000+0		1.1614-2	0.0000+0		0.0000+0	5.0392-3
8.0000	1.5000-1	1.1315+0	1.1313+1					0.0000+0		1.0384-2	0.0000+0		0.0000+0	5.0744-3
1.0000	2 ~ 1.5000-2	1.1311+0	1.1301+1					0.0000+0		7.5377-3	0.0000+0		0.0000+0	5.1114-3
1.5000	2 ~ 2.0000-2	1.1299+0	1.1292+1					0.0000+0		6.9378-3	0.0000+0		0.0000+0	5.1499-3
2.0000	2 ~ 3.0000-2	1.1293+0	1.1275+1					0.0000+0		6.4177-3	0.0000+0		0.0000+0	5.1868-3
3.0000	2 ~ 3.0000-2	1.1283+0	1.1275+1					0.0000+0		6.0491-3	0.0000+0		0.0000+0	5.2242-3
4.0000	2 ~ 5.0000-2	1.1178+0	1.1170+1					0.0000+0		5.4961-3	0.0000+0		0.0000+0	5.2622-3
5.0000	2 ~ 6.0000-2	1.1127+0	1.1119+1					0.0000+0		5.0526-3	0.0000+0		0.0000+0	5.2993-3
6.0000	2 ~ 8.0000-2	1.1096+0	1.1088+1					0.0000+0		4.6377-3	0.0000+0		0.0000+0	5.3368-3
8.0000	2 ~ 1.0000-3	1.0877+0	1.0869+1					0.0000+0		3.2500-3	0.0000+0		0.0000+0	5.3750-3
1.0000	3 ~ 1.5000-3	1.0333+0	1.0112+1					0.0000+0		2.0230-3	0.0000+0		0.0000+0	5.4134-3
1.5000	3 ~ 2.0000-3	1.0305+0	1.0095+1					0.0000+0		1.8561+0	0.0000+0		0.0000+0	5.4519-3
2.0000	3 ~ 3.0000-3	1.0275+0	1.0078+1					0.0000+0		1.7442+0	0.0000+0		0.0000+0	5.4904-3
3.0000	3 ~ 4.0000-3	1.0257+0	1.0072+1					0.0000+0		1.6374+0	0.0000+0		0.0000+0	5.5289-3
4.0000	3 ~ 6.0000-3	1.0222+0	1.0052+1					0.0000+0		1.5271+0	0.0000+0		0.0000+0	5.5674-3
5.0000	3 ~ 8.0000-3	1.0188+0	1.0028+1					0.0000+0		1.4199+0	0.0000+0		0.0000+0	5.6059-3
6.0000	3 ~ 1.0000-4	1.0166+0	1.0016+1					0.0000+0		1.3156+0	0.0000+0		0.0000+0	5.6444-3
8.0000	3 ~ 1.0000-4	1.0133+0	1.0000+1					0.0000+0		1.2141+0	0.0000+0		0.0000+0	5.6829-3
1.0000	4 ~ 1.5000-4	1.0081+0	1.0000+0					0.0000+0		1.1193-1	0.0000+0		0.0000+0	5.7214-3
1.5000	4 ~ 2.0000-4	1.0034+0	1.0000+0					0.0000+0		1.0287-1	0.0000+0		0.0000+0	5.7599-3
2.0000	4 ~ 3.0000-4	1.0007+0	1.0000+0					0.0000+0		9.2252-1	0.0000+0		0.0000+0	5.7984-3
3.0000	4 ~ 4.0000-4	1.0000+0	1.0000+0					0.0000+0		8.4027-1	0.0000+0		0.0000+0	5.8369-3
4.0000	4 ~ 5.0000-4	1.0000+0	1.0000+0					0.0000+0		7.5881-1	0.0000+0		0.0000+0	5.8754-3
5.0000	4 ~ 6.0000-4	1.0000+0	1.0000+0					0.0000+0		6.7735-1	0.0000+0		0.0000+0	5.9139-3
6.0000	4 ~ 7.0000-4	1.0000+0	1.0000+0					0.0000+0		5.9589-1	0.0000+0		0.0000+0	5.9524-3
8.0000	4 ~ 8.0000-4	1.0000+0	1.0000+0					0.0000+0		5.1443-1	0.0000+0		0.0000+0	5.9909-3
1.0000	5 ~ 1.5000-5	1.0000+0	1.0000+0	5.3491-2				0.0000+0		4.3290-1	0.0000+0		0.0000+0	6.0294-3
1.5000	5 ~ 2.0000-5	1.0000+0	1.0000+0	4.9653+0				0.0000+0		3.5149+0	0.0000+0		0.0000+0	6.0679-3
2.0000	5 ~ 3.0000-5	1.0000+0	1.0000+0	4.5920+0				0.0000+0		2.7000+0	0.0000+0		0.0000+0	6.1064-3
3.0000	5 ~ 4.0000-5	1.0000+0	1.0000+0	4.2187+0				0.0000+0		1.8850+0	0.0000+0		0.0000+0	6.1449-3
4.0000	5 ~ 5.0000-5	1.0000+0	1.0000+0	3.8454+0				0.0000+0		1.0702+0	0.0000+0		0.0000+0	6.1834-3
5.0000	5 ~ 6.0000-5	1.0000+0	1.0000+0	3.4721+0				0.0000+0		2.2570+0	0.0000+0		0.0000+0	6.2219-3
6.0000	5 ~ 7.0000-5	1.0000+0	1.0000+0	3.0988+0				0.0000+0		1.4445+0	0.0000+0		0.0000+0	6.2604-3
8.0000	5 ~ 8.0000-5	1.0000+0	1.0000+0	2.7255+0				0.0000+0		6.6433+0	0.0000+0		0.0000+0	6.2989-3
1.0000	6 ~ 1.5000-6	1.0000+0	1.0000+0	2.3522+0				0.0000+0		5.8320+0	0.0000+0		0.0000+0	6.3374-3
1.5000	6 ~ 2.0000-6	1.0000+0	1.0000+0	1.9789+0				0.0000+0		5.0207+0	0.0000+0		0.0000+0	6.3759-3
2.0000	6 ~ 3.0000-6	1.0000+0	1.0000+0	1.6056+0				0.0000+0		4.2094+0	0.0000+0		0.0000+0	6.4144-3
3.0000	6 ~ 4.0000-6	1.0000+0	1.0000+0	1.2323+0				0.0000+0		3.3981+0	0.0000+0		0.0000+0	6.4529-3
4.0000	6 ~ 5.0000-6	1.0000+0	1.0000+0	8.9188+0				0.0000+0		2.5868+0	0.0000+0		0.0000+0	6.4914-3
5.0000	6 ~ 6.0000-6	1.0000+0	1.0000+0	8.5455+0				0.0000+0		1.7755+0	0.0000+0		0.0000+0	6.5299-3
6.0000	6 ~ 7.0000-6	1.0000+0	1.0000+0	8.1722+0				0.0000+0		9.3632+0	0.0000+0		0.0000+0	6.5684-3
8.0000	6 ~ 8.0000-6	1.0000+0	1.0000+0	7.7989+0				0.0000+0		8.5519+0	0.0000+0		0.0000+0	6.6069-3
1.0000	7 ~ 1.5000-7	1.0000+0	1.0000+0	7.4256+0				0.0000+0		7.7406+0	0.0000+0		0	

CROSS SECTION

MATERIAL -2822		CROSS SECTION										PB-208	
ENERGY	TOTAL	ELABTIC	INELA	(N.2N)	(N.3N)	FISSTON	(N.NR)	(N.NP)	(N.D)	(N.A)	MU-BAR		
1.0000-5	1.1436+1	1.1342+1					0.0000+0			0.0000+0	3.9618-3		
1.0000-4	1.1383+1	1.1342+1					0.0000+0			0.0000+0	3.3817-3		
1.0000-3	1.1370+1	1.1342+1					0.0000+0			0.0000+0	3.3887-3		
1.0000-2	1.1368+1	1.1342+1					0.0000+0			0.0000+0	3.3986-3		
1.0000-1	1.1366+1	1.1342+1					0.0000+0			0.0000+0	3.4028-3		
1.0000-0	1.1364+1	1.1342+1					0.0000+0			0.0000+0	3.4081-3		
1.0000-0	1.1361+1	1.1342+1					0.0000+0			0.0000+0	3.4100-3		
1.0000-0	1.1357+1	1.1342+1					0.0000+0			0.0000+0	3.4142-3		
1.0000-0	1.1355+1	1.1342+1					0.0000+0			0.0000+0	3.4196-3		
1.0000-0	1.1353+1	1.1342+1					0.0000+0			0.0000+0	3.4251-3		
1.0000-0	1.1351+1	1.1342+1					0.0000+0			0.0000+0	3.4309-3		
1.0000-0	1.1349+1	1.1342+1					0.0000+0			0.0000+0	3.4365-3		
1.0000-0	1.1347+1	1.1342+1					0.0000+0			0.0000+0	3.4419-3		
1.0000-0	1.1346+1	1.1342+1					0.0000+0			0.0000+0	3.4478-3		
1.0000-0	1.1345+1	1.1342+1					0.0000+0			0.0000+0	3.4520-3		
1.0000-0	1.1344+1	1.1342+1					0.0000+0			0.0000+0	3.4573-3		
1.0000-0	1.1343+1	1.1342+1					0.0000+0			0.0000+0	3.4627-3		
1.0000-0	1.1342+1	1.1342+1					0.0000+0			0.0000+0	3.4681-3		
1.0000-0	1.1341+1	1.1342+1					0.0000+0			0.0000+0	3.4734-3		
1.0000-0	1.1340+1	1.1342+1					0.0000+0			0.0000+0	3.4788-3		
1.0000-0	1.1339+1	1.1342+1					0.0000+0			0.0000+0	3.4841-3		
1.0000-0	1.1338+1	1.1342+1					0.0000+0			0.0000+0	3.4895-3		
1.0000-0	1.1337+1	1.1342+1					0.0000+0			0.0000+0	3.4948-3		
1.0000-0	1.1336+1	1.1342+1					0.0000+0			0.0000+0	3.5001-3		
1.0000-0	1.1335+1	1.1342+1					0.0000+0			0.0000+0	3.5054-3		
1.0000-0	1.1334+1	1.1342+1					0.0000+0			0.0000+0	3.5107-3		
1.0000-0	1.1333+1	1.1342+1					0.0000+0			0.0000+0	3.5160-3		
1.0000-0	1.1332+1	1.1342+1					0.0000+0			0.0000+0	3.5213-3		
1.0000-0	1.1331+1	1.1342+1					0.0000+0			0.0000+0	3.5266-3		
1.0000-0	1.1330+1	1.1342+1					0.0000+0			0.0000+0	3.5319-3		
1.0000-0	1.1329+1	1.1342+1					0.0000+0			0.0000+0	3.5372-3		
1.0000-0	1.1328+1	1.1342+1					0.0000+0			0.0000+0	3.5425-3		
1.0000-0	1.1327+1	1.1342+1					0.0000+0			0.0000+0	3.5478-3		
1.0000-0	1.1326+1	1.1342+1					0.0000+0			0.0000+0	3.5531-3		
1.0000-0	1.1325+1	1.1342+1					0.0000+0			0.0000+0	3.5584-3		
1.0000-0	1.1324+1	1.1342+1					0.0000+0			0.0000+0	3.5637-3		
1.0000-0	1.1323+1	1.1342+1					0.0000+0			0.0000+0	3.5690-3		
1.0000-0	1.1322+1	1.1342+1					0.0000+0			0.0000+0	3.5743-3		
1.0000-0	1.1321+1	1.1342+1					0.0000+0			0.0000+0	3.5796-3		
1.0000-0	1.1320+1	1.1342+1					0.0000+0			0.0000+0	3.5849-3		
1.0000-0	1.1319+1	1.1342+1					0.0000+0			0.0000+0	3.5902-3		
1.0000-0	1.1318+1	1.1342+1					0.0000+0			0.0000+0	3.5955-3		
1.0000-0	1.1317+1	1.1342+1					0.0000+0			0.0000+0	3.6008-3		
1.0000-0	1.1316+1	1.1342+1					0.0000+0			0.0000+0	3.6061-3		
1.0000-0	1.1315+1	1.1342+1					0.0000+0			0.0000+0	3.6114-3		
1.0000-0	1.1314+1	1.1342+1					0.0000+0			0.0000+0	3.6167-3		
1.0000-0	1.1313+1	1.1342+1					0.0000+0			0.0000+0	3.6220-3		
1.0000-0	1.1312+1	1.1342+1					0.0000+0			0.0000+0	3.6273-3		
1.0000-0	1.1311+1	1.1342+1					0.0000+0			0.0000+0	3.6326-3		
1.0000-0	1.1310+1	1.1342+1					0.0000+0			0.0000+0	3.6379-3		
1.0000-0	1.1309+1	1.1342+1					0.0000+0			0.0000+0	3.6432-3		
1.0000-0	1.1308+1	1.1342+1					0.0000+0			0.0000+0	3.6485-3		
1.0000-0	1.1307+1	1.1342+1					0.0000+0			0.0000+0	3.6538-3		
1.0000-0	1.1306+1	1.1342+1					0.0000+0			0.0000+0	3.6591-3		
1.0000-0	1.1305+1	1.1342+1					0.0000+0			0.0000+0	3.6644-3		
1.0000-0	1.1304+1	1.1342+1					0.0000+0			0.0000+0	3.6697-3		
1.0000-0	1.1303+1	1.1342+1					0.0000+0			0.0000+0	3.6750-3		
1.0000-0	1.1302+1	1.1342+1					0.0000+0			0.0000+0	3.6803-3		
1.0000-0	1.1301+1	1.1342+1					0.0000+0			0.0000+0	3.6856-3		
1.0000-0	1.1300+1	1.1342+1					0.0000+0			0.0000+0	3.6909-3		
1.0000-0	1.1299+1	1.1342+1					0.0000+0			0.0000+0	3.6962-3		
1.0000-0	1.1298+1	1.1342+1					0.0000+0			0.0000+0	3.7015-3		
1.0000-0	1.1297+1	1.1342+1					0.0000+0			0.0000+0	3.7068-3		
1.0000-0	1.1296+1	1.1342+1					0.0000+0			0.0000+0	3.7121-3		
1.0000-0	1.1295+1	1.1342+1					0.0000+0			0.0000+0	3.7174-3		
1.0000-0	1.1294+1	1.1342+1					0.0000+0			0.0000+0	3.7227-3		
1.0000-0	1.1293+1	1.1342+1					0.0000+0			0.0000+0	3.7280-3		
1.0000-0	1.1292+1	1.1342+1					0.0000+0			0.0000+0	3.7333-3		
1.0000-0	1.1291+1	1.1342+1					0.0000+0			0.0000+0	3.7386-3		
1.0000-0	1.1290+1	1.1342+1					0.0000+0			0.0000+0	3.7439-3		
1.0000-0	1.1289+1	1.1342+1					0.0000+0			0.0000+0	3.7492-3		
1.0000-0	1.1288+1	1.1342+1					0.0000+0			0.0000+0	3.7545-3		
1.0000-0	1.1287+1	1.1342+1					0.0000+0			0.0000+0	3.7598-3		
1.0000-0	1.1286+1	1.1342+1					0.0000+0			0.0000+0	3.7651-3		
1.0000-0	1.1285+1	1.1342+1					0.0000+0			0.0000+0	3.7704-3		
1.0000-0	1.1284+1	1.1342+1					0.0000+0			0.0000+0	3.7757-3		
1.0000-0	1.1283+1	1.1342+1					0.0000+0			0.0000+0	3.7810-3		
1.0000-0	1.1282+1	1.1342+1					0.0000+0			0.0000+0	3.7863-3		
1.0000-0	1.1281+1	1.1342+1					0.0000+0			0.0000+0	3.7916-3		
1.0000-0	1.1280+1	1.1342+1					0.0000+0			0.0000+0	3.7969-3		
1.0000-0	1.1279+1	1.1342+1					0.0000+0			0.0000+0	3.8022-3		
1.0000-0	1.1278+1	1.1342+1					0.0000+0			0.0000+0	3.8075-3		
1.0000-0	1.1277+1	1.1342+1					0.0000+0			0.0000+0	3.8128-3		
1.0000-0	1.1276+1	1.1342+1					0.0000+0			0.0000+0	3.8181-3		
1.0000-0	1.1275+1	1.1342+1					0.0000+0			0.0000+0	3.8234-3		
1.0000-0	1.1274+1	1.1342+1					0.0000+0			0.0000+0	3.8287-3		
1.0000-0	1.1273+1	1.1342+1					0.0000+0			0.0000+0	3.8340-3		
1.0000-0	1.1272+1	1.1342+1					0.0000+0			0.0000+0	3.8393-3		
1.0000-0	1.1271+1	1.1342+1					0.0000+0			0.0000+0	3.8446-3		
1.0000-0	1.1270+1	1.1342+1					0.0000+0			0.0000+0	3.8499-3		
1.0000-0	1.1269+1	1.1342+1					0.0000+0			0.0000+0	3.8552-3		
1.0000-0	1.1268+1	1.1342+1					0.0000+0			0.0000+0	3.8605-3		
1.0000-0	1.1267+1	1.1342+1					0.0000+0			0.0000+0	3.8658-3		
1.0000-0	1.1266+1	1.1342+1					0.0000+0			0.0000+0	3.8711-3		
1.0000-0	1.1265+1	1.1342+1					0.0000+0			0.0000+0	3.8764-3		
1.0000-0	1.1264+1	1.1342+1					0.0000+0			0.0000+0	3.881		

CROSS SECTION

PB-208

MATERIAL -2824	ENERGY	TOTL	ELASTIC	INELR	(N.2N)	(N.3N)	FSSION	(N.NR)	(#NP)	CAPTURE	(N.PI)	(N.O)	(N.A)	MU-SR
1.0000	5 ~ 1.0000-2	1.1494+1	1.1499+1					0.0000+0	1.4951-3	6.8952-4			0.0000+0	3.7769-3
1.0000	1.5000	1.1493+1	1.1493+1					0.0000+0	6.8952-4	5.7376-4			0.0000+0	3.9210-3
1.0000	2.0000	1.1493+1	1.1493+1					0.0000+0	6.8952-4	4.6815-4			0.0000+0	3.9598-3
1.0000	3.0000	1.1493+1	1.1493+1					0.0000+0	6.8952-4	4.1107-4			0.0000+0	3.9986-3
1.0000	4.0000	1.1493+1	1.1493+1					0.0000+0	6.8952-4	3.5442-4			0.0000+0	4.0374-3
1.0000	5.0000	1.1493+1	1.1493+1					0.0000+0	6.8952-4	2.9778-4			0.0000+0	4.0762-3
1.0000	6.0000	1.1493+1	1.1493+1					0.0000+0	6.8952-4	2.4112-4			0.0000+0	4.1150-3
1.0000	7.0000	1.1493+1	1.1493+1					0.0000+0	6.8952-4	1.8446-4			0.0000+0	4.1538-3
1.0000	8.0000	1.1493+1	1.1493+1					0.0000+0	6.8952-4	1.2780-4			0.0000+0	4.1926-3
1.0000	9.0000	1.1493+1	1.1493+1					0.0000+0	6.8952-4	7.2142-5			0.0000+0	4.2314-3
1.0000	1.0000-1	1.1493+1	1.1493+1					0.0000+0	6.8952-4	6.6476-5			0.0000+0	4.2702-3
1.0000	2.0000-1	1.1493+1	1.1493+1					0.0000+0	6.8952-4	6.0810-5			0.0000+0	4.3090-3
1.0000	3.0000-1	1.1493+1	1.1493+1					0.0000+0	6.8952-4	5.5144-5			0.0000+0	4.3478-3
1.0000	4.0000-1	1.1493+1	1.1493+1					0.0000+0	6.8952-4	4.9478-5			0.0000+0	4.3866-3
1.0000	5.0000-1	1.1493+1	1.1493+1					0.0000+0	6.8952-4	4.3812-5			0.0000+0	4.4254-3
1.0000	6.0000-1	1.1493+1	1.1493+1					0.0000+0	6.8952-4	3.8146-5			0.0000+0	4.4642-3
1.0000	7.0000-1	1.1493+1	1.1493+1					0.0000+0	6.8952-4	3.2480-5			0.0000+0	4.5030-3
1.0000	8.0000-1	1.1493+1	1.1493+1					0.0000+0	6.8952-4	2.6814-5			0.0000+0	4.5418-3
1.0000	9.0000-1	1.1493+1	1.1493+1					0.0000+0	6.8952-4	2.1148-5			0.0000+0	4.5806-3
1.0000	1.0000-2	1.1493+1	1.1493+1					0.0000+0	6.8952-4	1.5482-5			0.0000+0	4.6194-3
1.0000	2.0000-2	1.1493+1	1.1493+1					0.0000+0	6.8952-4	9.9160-6			0.0000+0	4.6582-3
1.0000	3.0000-2	1.1493+1	1.1493+1					0.0000+0	6.8952-4	9.3494-6			0.0000+0	4.6970-3
1.0000	4.0000-2	1.1493+1	1.1493+1					0.0000+0	6.8952-4	8.7828-6			0.0000+0	4.7358-3
1.0000	5.0000-2	1.1493+1	1.1493+1					0.0000+0	6.8952-4	8.2162-6			0.0000+0	4.7746-3
1.0000	6.0000-2	1.1493+1	1.1493+1					0.0000+0	6.8952-4	7.6496-6			0.0000+0	4.8134-3
1.0000	7.0000-2	1.1493+1	1.1493+1					0.0000+0	6.8952-4	7.0830-6			0.0000+0	4.8522-3
1.0000	8.0000-2	1.1493+1	1.1493+1					0.0000+0	6.8952-4	6.5164-6			0.0000+0	4.8910-3
1.0000	9.0000-2	1.1493+1	1.1493+1					0.0000+0	6.8952-4	5.9498-6			0.0000+0	4.9298-3
1.0000	1.0000-3	1.1493+1	1.1493+1					0.0000+0	6.8952-4	5.3832-6			0.0000+0	4.9686-3
1.0000	2.0000-3	1.1493+1	1.1493+1					0.0000+0	6.8952-4	4.8166-6			0.0000+0	5.0074-3
1.0000	3.0000-3	1.1493+1	1.1493+1					0.0000+0	6.8952-4	4.2500-6			0.0000+0	5.0462-3
1.0000	4.0000-3	1.1493+1	1.1493+1					0.0000+0	6.8952-4	3.6834-6			0.0000+0	5.0850-3
1.0000	5.0000-3	1.1493+1	1.1493+1					0.0000+0	6.8952-4	3.1168-6			0.0000+0	5.1238-3
1.0000	6.0000-3	1.1493+1	1.1493+1					0.0000+0	6.8952-4	2.5502-6			0.0000+0	5.1626-3
1.0000	7.0000-3	1.1493+1	1.1493+1					0.0000+0	6.8952-4	1.9836-6			0.0000+0	5.2014-3
1.0000	8.0000-3	1.1493+1	1.1493+1					0.0000+0	6.8952-4	1.4170-6			0.0000+0	5.2402-3
1.0000	9.0000-3	1.1493+1	1.1493+1					0.0000+0	6.8952-4	8.6040-7			0.0000+0	5.2790-3
1.0000	1.0000-4	1.1493+1	1.1493+1					0.0000+0	6.8952-4	8.0374-7			0.0000+0	5.3178-3
1.0000	2.0000-4	1.1493+1	1.1493+1					0.0000+0	6.8952-4	7.4708-7			0.0000+0	5.3566-3
1.0000	3.0000-4	1.1493+1	1.1493+1					0.0000+0	6.8952-4	6.9042-7			0.0000+0	5.3954-3
1.0000	4.0000-4	1.1493+1	1.1493+1					0.0000+0	6.8952-4	6.3376-7			0.0000+0	5.4342-3
1.0000	5.0000-4	1.1493+1	1.1493+1					0.0000+0	6.8952-4	5.7710-7			0.0000+0	5.4730-3
1.0000	6.0000-4	1.1493+1	1.1493+1					0.0000+0	6.8952-4	5.2044-7			0.0000+0	5.5118-3
1.0000	7.0000-4	1.1493+1	1.1493+1					0.0000+0	6.8952-4	4.6378-7			0.0000+0	5.5506-3
1.0000	8.0000-4	1.1493+1	1.1493+1					0.0000+0	6.8952-4	4.0712-7			0.0000+0	5.5894-3
1.0000	9.0000-4	1.1493+1	1.1493+1					0.0000+0	6.8952-4	3.5046-7			0.0000+0	5.6282-3
1.0000	1.0000-5	1.1493+1	1.1493+1					0.0000+0	6.8952-4	2.9380-7			0.0000+0	5.6670-3
1.0000	2.0000-5	1.1493+1	1.1493+1					0.0000+0	6.8952-4	2.3714-7			0.0000+0	5.7058-3
1.0000	3.0000-5	1.1493+1	1.1493+1					0.0000+0	6.8952-4	1.8048-7			0.0000+0	5.7446-3
1.0000	4.0000-5	1.1493+1	1.1493+1					0.0000+0	6.8952-4	1.2382-7			0.0000+0	5.7834-3
1.0000	5.0000-5	1.1493+1	1.1493+1					0.0000+0	6.8952-4	6.8160-8			0.0000+0	5.8222-3
1.0000	6.0000-5	1.1493+1	1.1493+1					0.0000+0	6.8952-4	6.2494-8			0.0000+0	5.8610-3
1.0000	7.0000-5	1.1493+1	1.1493+1					0.0000+0	6.8952-4	5.6828-8			0.0000+0	5.9000-3
1.0000	8.0000-5	1.1493+1	1.1493+1					0.0000+0	6.8952-4	5.1162-8			0.0000+0	5.9388-3
1.0000	9.0000-5	1.1493+1	1.1493+1					0.0000+0	6.8952-4	4.5496-8			0.0000+0	5.9776-3
1.0000	1.0000-6	1.1493+1	1.1493+1					0.0000+0	6.8952-4	3.9830-8			0.0000+0	6.0164-3
1.0000	2.0000-6	1.1493+1	1.1493+1					0.0000+0	6.8952-4	3.4164-8			0.0000+0	6.0552-3
1.0000	3.0000-6	1.1493+1	1.1493+1					0.0000+0	6.8952-4	2.8498-8			0.0000+0	6.0940-3
1.0000	4.0000-6	1.1493+1	1.1493+1					0.0000+0	6.8952-4	2.2832-8			0.0000+0	6.1328-3
1.0000	5.0000-6	1.1493+1	1.1493+1					0.0000+0	6.8952-4	1.7166-8			0.0000+0	6.1716-3
1.0000	6.0000-6	1.1493+1	1.1493+1					0.0000+0	6.8952-4	1.1500-8			0.0000+0	6.2104-3
1.0000	7.0000-6	1.1493+1	1.1493+1					0.0000+0	6.8952-4	9.9340-9			0.0000+0	6.2492-3
1.0000	8.0000-6	1.1493+1	1.1493+1					0.0000+0	6.8952-4	9.3674-9			0.0000+0	6.2880-3
1.0000	9.0000-6	1.1493+1	1.1493+1					0.0000+0	6.8952-4	8.8008-9			0.0000+0	6.3268-3
1.0000	1.0000-7	1.1493+1	1.1493+1					0.0000+0	6.8952-4	8.2342-9			0.0000+0	6.3656-3
1.0000	2.0000-7	1.1493+1	1.1493+1					0.0000+0	6.8952-4	7.6676-9			0.0000+0	6.4044-3
1.0000	3.0000-7	1.1493+1	1.1493+1					0.0000+0	6.8952-4	7.1010-9			0.0000+0	6.4432-3
1.0000	4.0000-7	1.1493+1	1.1493+1					0.0000+0	6.8952-4	6.5344-9			0.0000+0	6.4820-3
1.0000	5.0000-7	1.1493+1	1.1493+1					0.0000+0	6.8952-4	5.9678-9			0.0000+0	6.5208-3
1.0000	6.0000-7	1.1493+1	1.1493+1					0.0000+0	6.8952-4	5.4012-9			0.0000+0	6.5596-3
1.0000	7.0000-7	1.1493+1	1.1493+1					0.0000+0	6.8952-4	4.8346-9			0.0000+0	6.5984-3
1.0000	8.0000-7	1.1493+1	1.1493+1					0.0000+0	6.8952-4	4.2680-9			0.0000+0	6.6372-3
1.0000	9.0000-7	1.1493+1	1.1493+1					0.0000+0	6.8952-4	3.7014-9			0.0000+0	6.6760-3
1.0000	1.0000-8	1.1493+1	1.1493+1					0.0000+0	6.8952-4	3.1348-9			0.0000+0	6.7148-3
1.0000	2.0000-8	1.1493+1	1.1493+1					0.0000+0	6.8952-4	2.5682-9			0.0000+0	6.7536-3
1.0000	3.0000-8	1.1493+1	1.1493+1											

TH-228

CROSS SECTION

MATERIAL =2801

ENERGY	TOTAL	ELASTIC	INEL	(N.2N)	(N.3N)	FISSTON	(N.NR)	(N.NP)	(N.D)	(N.R)	MU-SRR
1.0000- 5 ~ 1.0000- 2	3.4305+ 2	1.2825+ 1			9.2820- 1	3.6828+ 2					4.8845- 3
1.0000- 1.0000	1.6489+ 1	1.2818+ 1			4.8100- 1	1.7174+ 2					4.8310- 3
1.0000- 3.0000	1.5733+ 1	1.2803+ 1			3.7620- 1	1.4456+ 2					5.0256- 3
1.0000- 2.0000	1.2280+ 1	1.2795+ 1			3.0489- 1	1.2180+ 2					5.1238- 3
1.0000- 4.0000	1.1576+ 1	1.2785+ 1			2.5640- 1	1.0866+ 2					5.2184- 3
1.0000- 6.0000	1.0433+ 1	1.2765+ 1			2.2664- 1	9.1035+ 1					5.2877- 3
1.0000- 8.0000	9.6240+ 1	1.2775+ 1			2.0434- 1	7.3321+ 1					5.4112- 3
1.0000- 1.0000- 1	9.5178+ 1	1.2768+ 1			1.6012- 1	6.4484+ 1					5.4815- 3
1.0000- 1.5000	6.8555+ 1	1.2701+ 1			1.3615- 1	5.5703+ 1					5.5716- 3
1.0000- 2.0000	5.3417+ 1	1.2646+ 1			1.1829- 1	4.7079+ 1					5.6795- 3
1.0000- 3.0000	4.7972+ 1	1.2554+ 1			8.7079- 2	3.5747+ 2					5.7530- 3
1.0000- 4.0000	4.2932+ 1	1.2429+ 1			7.1876- 2	3.2669+ 1					5.8293- 3
1.0000- 6.0000	4.1584+ 1	1.2057+ 1			6.4608- 2	3.0775+ 1					5.8863- 3
1.0000- 8.0000	4.2053+ 1	1.1244+ 1			5.0272- 2	2.9735+ 1					5.9124- 3
1.0000+ 1.5000	9.4054+ 0	1.0564+ 0			4.2897- 2	4.7158+ 1					5.2122- 3
1.0000+ 2.0000	5.3538+ 0	7.2955+ 0			3.6159- 2	3.1900+ 3					5.3068- 3
1.0000+ 3.0000	2.1922+ 0	2.4557+ 0			3.0328- 2	6.9305+ 1					5.4051- 3
1.0000+ 4.0000	2.8545+ 0	1.6570+ 0			2.5570- 2	0.1608+ 0					5.5599- 3
1.0000+ 6.0000	2.3640+ 0	1.5481+ 0			2.0367- 2	0.9324+ 0					5.6259- 3
1.0000+ 8.0000	2.3573+ 0	1.5922+ 0			1.9076- 2	3.2588+ 2					5.6925- 3
1.0000+ 1.5000	1.7702+ 2	0.8683+ 1			1.5922- 1	1.5927+ 2					5.7628- 3
1.0000+ 2.0000	1.5112+ 2	0.1858+ 1			1.3582+ 1	0.8524+ 1					5.8529- 3
1.0000+ 3.0000	1.2871+ 2	6.6314+ 1			0.8826+ 3	5.3910+ 1					5.9474- 3
1.0000+ 4.0000	1.0726+ 2	8.3905+ 1			0.5843+ 3	4.1973+ 1					6.0427- 3
1.0000+ 6.0000	9.0412+ 1	6.0504+ 1			7.1224- 3	3.4711+ 1					6.1402- 3
1.0000+ 8.0000	8.1611+ 1	5.6671+ 1			6.4389- 3	2.9641+ 1					6.2105- 3
1.0000+ 1.5000	7.3333+ 1	5.2828+ 1			5.7183- 3	2.5941+ 1					6.2891- 3
1.0000+ 2.0000	6.4042+ 1	4.8269+ 1			4.2894- 3	1.5946+ 1					6.3744- 3
1.0000+ 3.0000	4.8966+ 1	3.9783+ 1			3.6152- 3	1.2149+ 1					6.4660- 3
1.0000+ 4.0000	3.1772+ 1	3.6191+ 1			3.0322- 3	0.9628+ 0					6.5599- 3
1.0000+ 6.0000	3.2683+ 1	3.2078+ 1			2.5571- 3	0.6889+ 0					6.6522- 3
1.0000+ 8.0000	3.1422+ 1	3.0073+ 1			2.0360- 3	4.6124+ 0					6.7474- 3
1.0000+ 1.5000	2.6551+ 1	2.8161+ 1			1.8075- 3	3.9703+ 0					6.8440- 3
1.0000+ 2.0000	2.2225+ 1	2.6025+ 1			1.3580- 3	2.5152+ 0					6.9395- 3
1.0000+ 3.0000	2.1965+ 1	2.2725+ 1			1.2432- 3	1.9345+ 0					7.0366- 3
1.0000+ 4.0000	2.0732+ 1	2.0732+ 1			1.3330- 3	1.5657+ 0					7.1359- 3
1.0000+ 6.0000	1.8611+ 1	1.8682+ 1			0.0000+ 0	1.2310+ 0					7.2368- 3
1.0000+ 8.0000	1.5958+ 1	1.8882+ 1			0.0000+ 0	0.7298+ 0					7.3408- 3
1.0000+ 1.5000	1.7988+ 1	1.9258+ 1			0.0000+ 0	8.1788+ 1					7.4474- 3
1.0000+ 2.0000	1.6996+ 1	1.8367+ 1			0.0000+ 0	7.2125+ 1					7.5562- 3
1.0000+ 3.0000	1.6065+ 1	1.5519+ 1			0.0000+ 0	6.2652+ 1					7.6666- 3
1.0000+ 4.0000	1.5205+ 1	1.4752+ 1			0.0000+ 0	4.7567+ 1					7.7796- 3
1.0000+ 6.0000	1.3972+ 1	1.3468+ 1			0.0000+ 0	4.1681+ 1					7.8951- 3
1.0000+ 8.0000	1.3423+ 1	1.3087+ 1			0.0000+ 0	3.7332+ 1					8.0135- 3
1.0000+ 1.5000	1.2932+ 1	1.2549+ 1			0.0000+ 0	3.3222+ 1					8.1351- 3
1.0000+ 2.0000	1.2373+ 1	1.1929+ 1			0.0000+ 0	2.9552+ 1					8.2617- 3
1.0000+ 3.0000	1.1609+ 1	1.1058+ 1			0.0000+ 0	2.6316+ 1					8.3959- 3
1.0000+ 4.0000	1.0774+ 1	1.0164+ 1			0.0000+ 0	1.8737+ 1					8.5386- 3
1.0000+ 6.0000	9.8361+ 0	9.0247+ 0			0.0000+ 0	1.5661+ 1					8.6911- 3
1.0000+ 8.0000	8.8623+ 0	8.8623+ 0			0.0000+ 0	1.3869+ 1					8.8538- 3
1.0000+ 1.5000	8.2744+ 0	8.2744+ 0			0.0000+ 0	1.0121+ 1					9.0271- 3
1.0000+ 2.0000	7.2474+ 0	6.8912+ 0			1.5000+ 2	0.4668+ 1					9.2122- 3
1.0000+ 3.0000	6.8053+ 0	6.1231+ 0			1.2500+ 2	0.6885+ 1					9.4096- 3
1.0000+ 4.0000	6.8140+ 0	4.2272+ 0			1.0000+ 2	1.0195+ 1					9.6199- 3
1.0000+ 6.0000	7.5644+ 0	2.4444+ 0			1.2040- 2	0.6288+ 1					9.8496- 3
1.0000+ 8.0000	7.7515+ 0	4.6956+ 0			1.6050- 2	0.9628+ 1					10.0986- 3
1.0000+ 1.5000	7.4571+ 0	5.0348+ 0			1.7000- 1	1.5667+ 1					10.3695- 3
1.0000+ 2.0000	7.4571+ 0	4.7714+ 0			1.7000- 1	1.5667+ 1					10.6545- 3
1.0000+ 3.0000	7.0384+ 0	4.3546+ 0			1.7000- 1	1.5667+ 1					10.9556- 3
1.0000+ 4.0000	6.8082+ 0	2.4579+ 0			1.7000- 1	1.5667+ 1					11.2738- 3
1.0000+ 6.0000	5.7868+ 0	1.1791+ 0			1.7000- 1	1.5667+ 1					11.6144- 3
1.0000+ 8.0000	5.5583+ 0	3.0514+ 0			1.7000- 1	1.5667+ 1					12.0028- 3
1.0000+ 1.5000	5.1583+ 0	1.0566- 2			1.1952+ 0	7.2028+ 8					12.4496- 3
1.0000+ 2.0000	5.1583+ 0	1.2618+ 0			1.1952+ 0	7.3109+ 1					12.9496- 3

CROSS SECTION

TH-230

MATERIAL = 2902	ENERGY	TOTAL	ELASTIC	INELR	(N,ZH)	(N,ZN)	FISSION	(N,HA)	(N,HP)	CAPTURE	(N,PI)	(N,O)	(N,RA)	MU-BRR
1.0000-	5 ~ 1.0000- 2	7.7784+ 1	9.7827+ 0			0.0000+ 0	0.0000+ 0			6.7892+ 1				4.6116- 9
1.0000-	1.5000- 2	4.1898+ 1	9.7859+ 0			0.0000+ 0	0.0000+ 0			3.1900+ 1				4.8659- 9
1.0000-	2.0000- 2	3.6764+ 1	9.7813+ 0			0.0000+ 0	0.0000+ 0			2.6989+ 1				5.0659- 9
1.0000-	3.0000- 2	3.2656+ 1	9.7744+ 0			0.0000+ 0	0.0000+ 0			2.2882+ 1				5.1644- 9
1.0000-	4.0000- 2	2.9757+ 1	9.7551+ 0			0.0000+ 0	0.0000+ 0			1.9484+ 1				5.2617- 9
1.0000-	5.0000- 2	2.7521+ 1	9.7362+ 0			0.0000+ 0	0.0000+ 0			1.6305+ 1				5.3229- 9
1.0000-	6.0000- 2	2.5652+ 1	9.7168+ 0			0.0000+ 0	0.0000+ 0			1.4394+ 1				5.3749- 9
1.0000-	8.0000- 2	2.4126+ 1	9.7118+ 0			0.0000+ 0	0.0000+ 0			1.3007+ 1				5.4168- 9
1.0000-	1.0000- 1	2.2719+ 1	9.7118+ 0			0.0000+ 0	0.0000+ 0			1.1604+ 1				5.5217- 9
1.0000-	1.5000- 1	2.1298+ 1	9.6956+ 0			0.0000+ 0	0.0000+ 0			1.0044+ 1				5.6142- 9
1.0000-	2.0000- 1	2.0033+ 1	9.6801+ 0			0.0000+ 0	0.0000+ 0			9.0778+ 0				5.7120- 9
1.0000-	3.0000- 1	1.8907+ 1	9.5503+ 0			0.0000+ 0	0.0000+ 0			9.6344+ 0				5.8090- 9
1.0000-	4.0000- 1	1.8027+ 1	9.3935+ 0			0.0000+ 0	0.0000+ 0			1.0120+ 1				5.9811- 9
1.0000-	5.0000- 1	1.7352+ 1	9.2317+ 0			0.0000+ 0	0.0000+ 0			1.1164+ 1				6.0386- 9
1.0000-	6.0000- 1	1.6821+ 1	9.0959+ 0			0.0000+ 0	0.0000+ 0			2.3424+ 1				6.1069- 9
1.0000-	8.0000- 1	1.6329+ 1	7.8308+ 0			0.0000+ 0	0.0000+ 0			2.5397+ 1				6.1790- 9
1.0000+	0 ~ 1.5000+ 0	2.0967+ 3	9.3546+ 1			0.0000+ 0	0.0000+ 0			2.0631+ 3				6.2714- 9
1.5000+	2.0000+ 0	1.9839+ 2	1.9839+ 1			0.0000+ 0	0.0000+ 0			1.1842+ 2				6.3684- 9
3.0000+	3.0000+ 0	1.9265+ 1	1.7270+ 0			0.0000+ 0	0.0000+ 0			4.9072+ 0				6.4693- 9
5.0000+	4.0000+ 0	1.8771+ 1	1.1095+ 0			0.0000+ 0	0.0000+ 0			5.8205+ 0				6.5683- 9
6.0000+	5.0000+ 0	1.8333+ 1	1.0733+ 0			0.0000+ 0	0.0000+ 0			5.8190+ 0				6.6659- 9
8.0000+	6.0000+ 0	1.8005+ 1	1.0335+ 0			0.0000+ 0	0.0000+ 0			4.6903+ 1				6.7642- 9
1.0000+	1.0000+ 1	9.0272+ 0	7.9836+ 0			0.0000+ 0	0.0000+ 0			4.5803+ 1				6.8663- 9
1.5000+	2.0000+ 1	5.6514+ 2	1.7719+ 2			0.0000+ 0	0.0000+ 0			1.4384+ 0				6.9687- 9
3.0000+	3.0000+ 1	1.8389+ 2	5.4836+ 1			0.0000+ 0	0.0000+ 0			4.0785+ 2				7.0657- 9
5.0000+	4.0000+ 1	1.7933+ 2	3.1459+ 1			0.0000+ 0	0.0000+ 0			1.2904+ 2				7.1266- 9
6.0000+	5.0000+ 1	1.7539+ 2	1.4689+ 1			0.0000+ 0	0.0000+ 0			9.9474+ 1				7.2236- 9
8.0000+	6.0000+ 1	1.7243+ 2	1.4405+ 1			0.0000+ 0	0.0000+ 0			7.3929+ 1				7.2957- 9
1.0000+	1.0000+ 2	7.6685+ 1	4.3081+ 1			0.0000+ 0	0.0000+ 0			1.9026+ 1				7.3724- 9
1.5000+	2.0000+ 2	5.2176+ 1	3.0582+ 1			0.0000+ 0	0.0000+ 0			3.3803+ 1				7.4536- 9
3.0000+	3.0000+ 2	3.6236+ 1	2.8883+ 1			0.0000+ 0	0.0000+ 0			2.5374+ 1				7.5360- 9
5.0000+	4.0000+ 2	3.1219+ 1	3.6695+ 1			0.0000+ 0	0.0000+ 0			1.7403+ 1				7.6190- 9
6.0000+	5.0000+ 2	2.9482+ 1	5.9486+ 1			0.0000+ 0	0.0000+ 0			4.2954+ 0				7.7008- 9
8.0000+	6.0000+ 2	2.7936+ 1	2.5853+ 1			0.0000+ 0	0.0000+ 0			5.5954+ 0				7.7850- 9
1.0000+	3 ~ 1.0000+ 3	2.7329+ 1	2.4844+ 1			0.0000+ 0	0.0000+ 0			3.4316+ 0				8.0105- 9
1.5000+	2.0000+ 3	2.4910+ 1	2.2895+ 1			0.0000+ 0	0.0000+ 0			3.9892+ 0				8.0787- 9
3.0000+	3.0000+ 3	2.2926+ 1	2.1629+ 1			0.0000+ 0	0.0000+ 0			2.1788+ 0				8.1509- 9
5.0000+	4.0000+ 3	2.1008+ 1	1.8976+ 1			0.0000+ 0	0.0000+ 0			2.4763+ 0				8.2433- 9
6.0000+	5.0000+ 3	1.9233+ 1	1.8598+ 1			0.0000+ 0	0.0000+ 0			1.9116+ 0				8.3403- 9
8.0000+	6.0000+ 3	1.8375+ 1	1.7854+ 1			0.0000+ 0	0.0000+ 0			1.4322+ 0				8.4412- 9
1.0000+	4 ~ 1.5000+ 4	1.6659+ 1	1.6021+ 1			0.0000+ 0	0.0000+ 0			1.0704+ 0				8.5381- 9
1.5000+	2.0000+ 4	1.5801+ 1	1.5246+ 1			0.0000+ 0	0.0000+ 0			1.0024+ 0				8.6378- 9
3.0000+	3.0000+ 4	1.4295+ 1	1.3873+ 1			0.0000+ 0	0.0000+ 0			4.8252+ 1				8.7394- 9
5.0000+	4.0000+ 4	1.2969+ 1	1.2650+ 1			0.0000+ 0	0.0000+ 0			4.2224+ 1				8.8416- 9
6.0000+	5.0000+ 4	1.2084+ 1	1.1886+ 1			0.0000+ 0	0.0000+ 0			3.7431+ 1				8.9456- 9
8.0000+	6.0000+ 4	1.1235+ 1	1.1189+ 1			0.0000+ 0	0.0000+ 0			2.2378+ 1				9.0509- 9
1.0000+	5 ~ 1.5000+ 5	1.0593+ 1	1.0585+ 1			0.0000+ 0	0.0000+ 0			6.1195+ 1				9.1574- 9
1.5000+	2.0000+ 5	1.0000+ 1	1.0000+ 1			0.0000+ 0	0.0000+ 0			7.2497+ 1				9.2645- 9
3.0000+	3.0000+ 5	0.9000+ 1	0.9000+ 1			0.0000+ 0	0.0000+ 0			5.3732+ 1				9.3721- 9
5.0000+	4.0000+ 5	0.8000+ 1	0.8000+ 1			0.0000+ 0	0.0000+ 0			4.8252+ 1				9.4802- 9
6.0000+	5.0000+ 5	0.7000+ 1	0.7000+ 1			0.0000+ 0	0.0000+ 0			4.2224+ 1				9.5881- 9
8.0000+	6.0000+ 5	0.6000+ 1	0.6000+ 1			0.0000+ 0	0.0000+ 0			3.7431+ 1				9.6962- 9
1.0000+	6 ~ 1.5000+ 6	0.5000+ 1	0.5000+ 1			0.0000+ 0	0.0000+ 0			3.2642+ 1				9.8044- 9
1.5000+	2.0000+ 6	0.4000+ 1	0.4000+ 1			0.0000+ 0	0.0000+ 0			2.7852+ 1				9.9127- 9
3.0000+	3.0000+ 6	0.3000+ 1	0.3000+ 1			0.0000+ 0	0.0000+ 0			2.3063+ 1				1.0214- 2
5.0000+	4.0000+ 6	0.2000+ 1	0.2000+ 1			0.0000+ 0	0.0000+ 0			1.8274+ 1				1.1295- 2
6.0000+	5.0000+ 6	0.1000+ 1	0.1000+ 1			0.0000+ 0	0.0000+ 0			1.3485+ 1				1.2376- 2
8.0000+	6.0000+ 6	0.0000+ 1	0.0000+ 1			0.0000+ 0	0.0000+ 0			0.8696+ 1				1.3457- 2
1.0000+	7 ~ 1.5000+ 7	0.0000+ 1	0.0000+ 1			0.0000+ 0	0.0000+ 0			0.3907+ 1				1.4528- 2
1.5000+	2.0000+ 7	0.0000+ 1	0.0000+ 1			0.0000+ 0	0.0000+ 0			0.0000+ 1				1.5600- 2
3.0000+	3.0000+ 7	0.0000+ 1	0.0000+ 1			0.0000+ 0	0.0000+ 0			0.0000+ 1				1.6672- 2
5.0000+	4.0000+ 7	0.0000+ 1	0.0000+ 1			0.0000+ 0	0.0000+ 0			0.0000+ 1				1.7744- 2
6.0000+	5.0000+ 7	0.0000+ 1	0.0000+ 1			0.0000+ 0	0.0000+ 0			0.0000+ 1				1.8816- 2
8.0000+	6.0000+ 7	0.0000+ 1	0.0000+ 1			0.0000+ 0	0.0000+ 0			0.0000+ 1				1.9888- 2
1.0000+	8 ~ 1.5000+ 8	0.0000+ 1	0.0000+ 1			0.0000+ 0	0.0000+ 0			0.0000+ 1				2.0960- 2
1.5000+	2.0000+ 8	0.0000+ 1	0.0000+ 1			0.0000+ 0	0.0000+ 0			0.0000+ 1				2.2032- 2
3.0000+	3.0000+ 8	0.0000+ 1	0.0000+ 1			0.0000+ 0	0.0000+ 0			0.0000+ 1				2.3104- 2
5.0000+	4.0000+ 8	0.0000+ 1	0.0000+ 1			0.0000+ 0	0.0000+ 0			0.0000+ 1				2.4176- 2
6.0000+	5.0000+ 8	0.0000+ 1	0.0000+ 1			0.0000+ 0	0.0000+ 0			0.0000+ 1				2.5248- 2
8.0000+	6.0000+ 8	0.0000+ 1	0.0000+ 1			0.0000+ 0	0.0000+ 0			0.0000+ 1				2.6320- 2
1.0000+	9 ~ 1.5000+ 9	0.0000+ 1	0.0000+ 1			0.0000+ 0	0.0000+ 0			0.0000+ 1				2.7392- 2
1.5000+	2.0000+ 9	0.0000+ 1	0.0000+ 1			0.0000+ 0	0.0000+ 0			0.0000+ 1				2.8464- 2
3.0000+	3.0000+ 9	0.0000+ 1	0.0000+ 1			0.0000+ 0	0.0000+ 0			0.0000+ 1				2.9536- 2
5.0000+	4.0000+ 9	0.0000+ 1	0.0000+ 1			0.0000+ 0	0.0000+ 0			0.0000+ 1				3.0608- 2
6.0000+	5.0000+ 9	0.0000+ 1	0.0000+ 1			0.0000+ 0	0.0000+ 0			0.0000+ 1				3.1680- 2
8.0000+	6.0000+ 9	0.0000+ 1	0.0000+ 1			0.0000+ 0	0.0000+ 0			0.0000+ 1				3.2752- 2

TH-232

CROSS SECTION

MATERIAL = 2903

EMERY	TOTAL	ELASTIC	INELR	(N.ZN)	(N.SNI)	FISSION	(N.NR)	(N.NP)	(M.P)	(N.D)	(N.R)	MU-BAR
1.0000+ 5	3.4806+ 1	1.2169+ 1			0.0000+ 0	2.2637+ 1						5.6885- 3
1.0000+ 2	2.2842+ 1	1.2169+ 1			0.0000+ 0	1.078+ 1						5.8614- 3
1.0000+ 2	2.0957+ 1	1.2169+ 1			0.0000+ 0	7.3608+ 0						5.8569- 3
1.0000+ 2	1.8974+ 1	1.2169+ 1			0.0000+ 0	9.1882+ 0						5.8442- 3
1.0000+ 2	1.7576+ 1	1.2169+ 1			0.0000+ 0	5.4223+ 0						5.8297- 3
1.0000+ 2	1.7033+ 1	1.2169+ 1			0.0000+ 0	4.8627+ 0						4.08236- 3
1.0000+ 2	1.6465+ 1	1.2169+ 1			0.0000+ 0	3.7707+ 0						4.0504- 3
1.0000+ 2	1.5909+ 1	1.2169+ 1			0.0000+ 0	2.6299+ 0						4.1162- 3
1.0000+ 1	1.4736+ 1	1.2169+ 1			0.0000+ 0	1.8555+ 0						4.1898- 3
1.0000+ 1	1.4233+ 1	1.2169+ 1			0.0000+ 0	1.5125+ 0						4.2051- 3
1.0000+ 1	1.3719+ 1	1.2169+ 1			0.0000+ 0	1.4891+ 0						4.2378- 3
1.0000+ 1	1.3240+ 1	1.2169+ 1			0.0000+ 0	1.3108+ 0						4.3316- 3
1.0000+ 1	1.3044+ 1	1.2169+ 1			0.0000+ 0	1.1109+ 0						4.3686- 3
1.0000+ 1	1.2795+ 1	1.2169+ 1			0.0000+ 0	9.2080+ 0						4.3908- 3
1.0000+ 0	1.2496+ 1	1.2169+ 1			0.0000+ 0	7.1511+ 0						4.4244- 3
1.0000+ 0	1.1985+ 1	1.2169+ 1			0.0000+ 0	5.3026+ 0						4.4677- 3
1.0000+ 0	1.1598+ 1	1.2169+ 1			0.0000+ 0	3.7928+ 0						4.5192- 3
1.0000+ 0	1.1398+ 1	1.2169+ 1			0.0000+ 0	2.6645+ 0						4.5605- 3
1.0000+ 0	1.1217+ 1	1.2169+ 1			0.0000+ 0	2.0825+ 0						4.6060- 3
1.0000+ 0	1.0857+ 1	1.2169+ 1			0.0000+ 0	1.2896+ 0						4.6562- 3
1.0000+ 0	1.0657+ 1	1.2169+ 1			0.0000+ 0	1.1652+ 0						4.6987- 3
1.0000+ 1	1.0423+ 1	1.2169+ 1			0.0000+ 0	0.8716+ 0						4.7328- 3
1.0000+ 1	9.8865+ 0	9.4893+ 0			0.0000+ 0	1.0873+ 0						4.7759- 3
1.0000+ 1	9.8865+ 0	9.4893+ 0			0.0000+ 0	2.323+ 0						4.8187- 3
1.0000+ 1	9.8865+ 0	9.4893+ 0			0.0000+ 0	6.6600+ 2						4.8614- 3
1.0000+ 1	9.8865+ 0	9.4893+ 0			0.0000+ 0	6.7366+ 2						4.9041- 3
1.0000+ 1	9.8865+ 0	9.4893+ 0			0.0000+ 0	2.3486+ 1						4.9479- 3
1.0000+ 1	9.8865+ 0	9.4893+ 0			0.0000+ 0	4.7894+ 1						4.9916- 3
1.0000+ 1	9.8865+ 0	9.4893+ 0			0.0000+ 0	7.4318+ 2						5.0359- 3
1.0000+ 2	9.8865+ 0	9.4893+ 0			0.0000+ 0	1.5610+ 1						5.0840- 3
1.0000+ 2	9.8865+ 0	9.4893+ 0			0.0000+ 0	1.6954+ 1						5.1295- 3
1.0000+ 2	9.8865+ 0	9.4893+ 0			0.0000+ 0	0.0885+ 0						5.1759- 3
1.0000+ 2	9.8865+ 0	9.4893+ 0			0.0000+ 0	0.0885+ 0						5.2223- 3
1.0000+ 2	9.8865+ 0	9.4893+ 0			0.0000+ 0	2.4300+ 0						5.2687- 3
1.0000+ 2	9.8865+ 0	9.4893+ 0			0.0000+ 0	2.0255+ 0						5.3151- 3
1.0000+ 2	9.8865+ 0	9.4893+ 0			0.0000+ 0	2.4822+ 0						5.3489- 3
1.0000+ 3	9.8865+ 0	9.4893+ 0			0.0000+ 0	0.0000+ 0						5.3922- 3
1.0000+ 3	9.8865+ 0	9.4893+ 0			0.0000+ 0	1.7324+ 0						5.4377- 3
1.0000+ 3	9.8865+ 0	9.4893+ 0			0.0000+ 0	1.1681+ 0						5.4850- 3
1.0000+ 3	9.8865+ 0	9.4893+ 0			0.0000+ 0	1.0852+ 0						5.5299- 3
1.0000+ 3	9.8865+ 0	9.4893+ 0			0.0000+ 0	0.0000+ 0						5.5743- 3
1.0000+ 3	9.8865+ 0	9.4893+ 0			0.0000+ 0	0.0000+ 0						5.6187- 3
1.0000+ 3	9.8865+ 0	9.4893+ 0			0.0000+ 0	0.0000+ 0						5.6631- 3
1.0000+ 3	9.8865+ 0	9.4893+ 0			0.0000+ 0	0.0000+ 0						5.7075- 3
1.0000+ 3	9.8865+ 0	9.4893+ 0			0.0000+ 0	0.0000+ 0						5.7519- 3
1.0000+ 3	9.8865+ 0	9.4893+ 0			0.0000+ 0	0.0000+ 0						5.7963- 3
1.0000+ 3	9.8865+ 0	9.4893+ 0			0.0000+ 0	0.0000+ 0						5.8407- 3
1.0000+ 3	9.8865+ 0	9.4893+ 0			0.0000+ 0	0.0000+ 0						5.8851- 3
1.0000+ 3	9.8865+ 0	9.4893+ 0			0.0000+ 0	0.0000+ 0						5.9295- 3
1.0000+ 3	9.8865+ 0	9.4893+ 0			0.0000+ 0	0.0000+ 0						5.9739- 3
1.0000+ 3	9.8865+ 0	9.4893+ 0			0.0000+ 0	0.0000+ 0						6.0183- 3
1.0000+ 3	9.8865+ 0	9.4893+ 0			0.0000+ 0	0.0000+ 0						6.0627- 3
1.0000+ 3	9.8865+ 0	9.4893+ 0			0.0000+ 0	0.0000+ 0						6.1071- 3
1.0000+ 3	9.8865+ 0	9.4893+ 0			0.0000+ 0	0.0000+ 0						6.1515- 3
1.0000+ 3	9.8865+ 0	9.4893+ 0			0.0000+ 0	0.0000+ 0						6.1959- 3
1.0000+ 3	9.8865+ 0	9.4893+ 0			0.0000+ 0	0.0000+ 0						6.2403- 3
1.0000+ 3	9.8865+ 0	9.4893+ 0			0.0000+ 0	0.0000+ 0						6.2847- 3
1.0000+ 3	9.8865+ 0	9.4893+ 0			0.0000+ 0	0.0000+ 0						6.3291- 3
1.0000+ 3	9.8865+ 0	9.4893+ 0			0.0000+ 0	0.0000+ 0						6.3735- 3
1.0000+ 3	9.8865+ 0	9.4893+ 0			0.0000+ 0	0.0000+ 0						6.4179- 3
1.0000+ 3	9.8865+ 0	9.4893+ 0			0.0000+ 0	0.0000+ 0						6.4623- 3
1.0000+ 3	9.8865+ 0	9.4893+ 0			0.0000+ 0	0.0000+ 0						6.5067- 3
1.0000+ 3	9.8865+ 0	9.4893+ 0			0.0000+ 0	0.0000+ 0						6.5511- 3
1.0000+ 3	9.8865+ 0	9.4893+ 0			0.0000+ 0	0.0000+ 0						6.5955- 3
1.0000+ 3	9.8865+ 0	9.4893+ 0			0.0000+ 0	0.0000+ 0						6.6399- 3
1.0000+ 3	9.8865+ 0	9.4893+ 0			0.0000+ 0	0.0000+ 0						6.6843- 3
1.0000+ 3	9.8865+ 0	9.4893+ 0			0.0000+ 0	0.0000+ 0						6.7287- 3
1.0000+ 3	9.8865+ 0	9.4893+ 0			0.0000+ 0	0.0000+ 0						6.7731- 3
1.0000+ 3	9.8865+ 0	9.4893+ 0			0.0000+ 0	0.0000+ 0						6.8175- 3
1.0000+ 3	9.8865+ 0	9.4893+ 0			0.0000+ 0	0.0000+ 0						6.8619- 3
1.0000+ 3	9.8865+ 0	9.4893+ 0			0.0000+ 0	0.0000+ 0						6.9063- 3
1.0000+ 3	9.8865+ 0	9.4893+ 0			0.0000+ 0	0.0000+ 0						6.9507- 3
1.0000+ 3	9.8865+ 0	9.4893+ 0			0.0000+ 0	0.0000+ 0						6.9951- 3
1.0000+ 3	9.8865+ 0	9.4893+ 0			0.0000+ 0	0.0000+ 0						7.0395- 3
1.0000+ 3	9.8865+ 0	9.4893+ 0			0.0000+ 0	0.0000+ 0						7.0839- 3
1.0000+ 3	9.8865+ 0	9.4893+ 0			0.0000+ 0	0.0000+ 0						7.1283- 3
1.0000+ 3	9.8865+ 0	9.4893+ 0			0.0000+ 0	0.0000+ 0						7.1727- 3
1.0000+ 3	9.8865+ 0	9.4893+ 0			0.0000+ 0	0.0000+ 0						7.2171- 3
1.0000+ 3	9.8865+ 0	9.4893+ 0			0.0000+ 0	0.0000+ 0						7.2615- 3
1.0000+ 3	9.8865+ 0	9.4893+ 0			0.0000+ 0	0.0000+ 0						7.3059- 3
1.0000+ 3	9.8865+ 0	9.4893+ 0			0.0000+ 0	0.0000+ 0						7.3503- 3
1.0000+ 3	9.8865+ 0	9.4893+ 0			0.0000+ 0	0.0000+ 0						7.3947- 3
1.0000+ 3	9.8865+ 0	9.4893+ 0			0.0000+ 0	0.0000+ 0						7.4391- 3
1.0000+ 3	9.8865+ 0	9.4893+ 0			0.0000+ 0	0.0000+ 0						7.4835- 3
1.0000+ 3	9.8865+ 0	9.4893+ 0			0.0000+ 0	0.0000+ 0						7.5279- 3
1.0000+ 3	9.8865+ 0	9.4893+ 0			0.0000+ 0	0.0000+ 0						7.5723- 3
1.0000+ 3	9.8865+ 0	9.4893+ 0			0.0000+ 0	0.0000+ 0						7.6167- 3
1.0000+ 3	9.8865+ 0	9.4893+ 0			0.0000+ 0	0.0000+ 0						7.6611- 3
1.0000+ 3	9.8865+ 0	9.4893+ 0			0.0000+ 0	0.0000+ 0						7.7055- 3
1.0000+ 3	9.8865+ 0	9.4893+ 0			0.0000+ 0	0.0000+ 0						7.7499- 3
1.0000+ 3	9.8865+ 0	9.4893+ 0			0.0000+ 0	0.0000+ 0						7.7943- 3
1.0000+ 3	9.8865+ 0											

MATERIAL = 2804 CROSS SECTION TH-293

ENERGY	TOTAL	ELASTIC	INELA	(N.28)	(N.3N)	FLESSION	(N.NP)	CAPTURE	(N.P.I)	(N.D)	(N.R)	MU-BR
1.0000-5 ~ 1.0000-2	4.5303+ 3	1.2998+ 1	4.5763+ 1			4.4714+ 3		4.4714+ 3				4.7930- 3
1.0000-4	2.1079+ 1	1.2898+ 1	2.1954+ 1			2.0794+ 3		2.0794+ 3				5.1108- 3
1.0000-3	1.5000-2	1.2938+ 1	1.5657+ 1			1.4661+ 3		1.4661+ 3				5.3271- 3
1.0000-2	1.1134+ 3	1.3002+ 1	1.1355+ 1			1.0889+ 3		1.0889+ 3				5.4935- 3
1.0000-1	9.8932+ 2	1.3004+ 1	9.1091+ 0			1.0296+ 3		1.0296+ 3				5.5174- 3
1.5000-1	6.7223+ 2	1.3008+ 1	6.5971+ 0			6.5888+ 2		6.5888+ 2				5.6262- 3
2.0000-1	4.6189+ 2	1.3018+ 1	4.5048+ 0			5.9451+ 0		5.9451+ 0				5.9382- 3
3.0000-1	3.0938+ 1	1.3038+ 1	3.0289+ 0			3.0282+ 2		3.0282+ 2				6.1528- 3
4.0000-1	2.2937+ 1	1.3043+ 1	2.2769+ 0			3.4336+ 0		3.4336+ 0				6.2317- 3
5.0000-1	2.5943+ 2	1.3055+ 1	2.5210+ 0			3.1190+ 0		3.1190+ 0				6.2946- 3
6.0000-1	2.3071+ 1	1.3071+ 1	2.2743+ 0			2.7743+ 0		2.7743+ 0				6.3693- 3
7.0000-1	2.3011+ 2	1.3100+ 1	2.4195+ 0			2.0794+ 2		2.0794+ 2				6.4462- 3
8.0000-1	2.5059+ 2	1.3140+ 1	2.1079+ 0			1.7479+ 2		1.7479+ 2				6.5494- 3
9.0000-1	1.8196+ 2	1.3201+ 1	1.8279+ 0			1.4661+ 2		1.4661+ 2				6.6555- 3
1.0000-0	1.3970+ 2	1.3282+ 1	1.5923+ 0			1.2360+ 2		1.2360+ 2				6.7659- 3
2.0000-0	1.2426+ 2	1.3354+ 1	1.4373+ 0			1.0889+ 2		1.0889+ 2				6.8750- 3
3.0000-0	1.0328+ 2	1.3455+ 1	1.2030+ 0			9.7398+ 1		9.7398+ 1				7.0739- 3
4.0000-0	8.2006+ 1	1.3730+ 1	8.0856+ 0			7.1875- 3		7.1875- 3				7.2685- 3
5.0000-0	8.0850+ 1	1.4014+ 1	7.9242- 1			6.5927+ 1		6.5927+ 1				7.4689- 3
6.0000-0	7.0901+ 1	1.4221+ 1	6.9499- 1			5.9572+ 1		5.9572+ 1				7.6697- 3
7.0000-0	6.5772+ 1	1.4523+ 1	6.4566- 1			5.2656+ 1		5.2656+ 1				7.8697- 3
8.0000-0	5.1827+ 1	1.4858+ 1	5.1660- 1			4.4351+ 1		4.4351+ 1				8.0697- 3
9.0000-0	4.8324+ 1	1.5269+ 1	4.8221- 1			3.7331- 3		3.7331- 3				8.2697- 3
1.0000+1	4.7009+ 1	1.5669+ 1	4.6693+ 1			3.1134+ 3		3.1134+ 3				8.4697- 3
2.0000+1	4.5347+ 1	1.6093+ 1	4.5015+ 1			2.4939+ 3		2.4939+ 3				8.6697- 3
3.0000+1	4.4543+ 1	1.6530+ 1	4.3160+ 1			1.8784- 1		1.8784- 1				8.8697- 3
4.0000+1	4.3723+ 1	1.6976+ 1	4.1281+ 1			1.2622- 1		1.2622- 1				9.0697- 3
5.0000+1	4.2976+ 1	1.7432+ 1	3.9378+ 1			6.0940- 3		6.0940- 3				9.2697- 3
6.0000+1	4.2282+ 1	1.7898+ 1	3.7482+ 1			5.4805- 3		5.4805- 3				9.4697- 3
7.0000+1	4.1623+ 1	1.8374+ 1	3.5597+ 1			4.8680- 3		4.8680- 3				9.6697- 3
8.0000+1	4.1003+ 1	1.8861+ 1	3.3723+ 1			4.2567- 3		4.2567- 3				9.8697- 3
9.0000+1	4.0425+ 1	1.9359+ 1	3.1869+ 1			3.6468- 3		3.6468- 3				10.0697- 3
1.0000+2	4.0000+ 3	1.9867+ 1	3.0034+ 1			3.0374- 3		3.0374- 3				10.2697- 3
2.0000+2	3.9611+ 3	2.0384+ 1	2.8218+ 1			2.4289- 3		2.4289- 3				10.4697- 3
3.0000+2	3.9262+ 3	2.0911+ 1	2.6423+ 1			1.8214- 3		1.8214- 3				10.6697- 3
4.0000+2	3.8953+ 3	2.1447+ 1	2.4648+ 1			1.2149- 3		1.2149- 3				10.8697- 3
5.0000+2	3.8684+ 3	2.1992+ 1	2.2893+ 1			6.2704+ 0		6.2704+ 0				11.0697- 3
6.0000+2	3.8455+ 3	2.2547+ 1	2.1158+ 1			5.6579+ 0		5.6579+ 0				11.2697- 3
7.0000+2	3.8266+ 3	2.3111+ 1	1.9443+ 1			5.0454+ 0		5.0454+ 0				11.4697- 3
8.0000+2	3.8117+ 3	2.3684+ 1	1.7748+ 1			4.4329+ 0		4.4329+ 0				11.6697- 3
9.0000+2	3.8000+ 3	2.4267+ 1	1.6073+ 1			3.8204+ 0		3.8204+ 0				11.8697- 3
1.0000+3	3.7914+ 3	2.4859+ 1	1.4428+ 1			3.2079+ 0		3.2079+ 0				12.0697- 3
2.0000+3	3.7857+ 3	2.5461+ 1	1.2803+ 1			2.5954+ 0		2.5954+ 0				12.2697- 3
3.0000+3	3.7829+ 3	2.6072+ 1	1.1208+ 1			2.0829+ 0		2.0829+ 0				12.4697- 3
4.0000+3	3.7820+ 3	2.6692+ 1	1.0643+ 1			1.5704+ 0		1.5704+ 0				12.6697- 3
5.0000+3	3.7829+ 3	2.7321+ 1	1.0108+ 1			1.0579+ 0		1.0579+ 0				12.8697- 3
6.0000+3	3.7855+ 3	2.7972+ 1	0.9603+ 1			5.6516- 3		5.6516- 3				13.0697- 3
7.0000+3	3.7897+ 3	2.8633+ 1	0.9128+ 1			5.0391- 3		5.0391- 3				13.2697- 3
8.0000+3	3.7955+ 3	2.9305+ 1	0.8683+ 1			4.4266- 3		4.4266- 3				13.4697- 3
9.0000+3	3.8028+ 3	3.0000+ 1	0.8268+ 1			3.8141- 3		3.8141- 3				13.6697- 3
1.0000+4	3.8116+ 3	3.0719+ 1	0.7883+ 1			3.2016- 3		3.2016- 3				13.8697- 3
2.0000+4	3.8218+ 3	3.1452+ 1	0.7528+ 1			2.5891- 3		2.5891- 3				14.0697- 3
3.0000+4	3.8334+ 3	3.2207+ 1	0.7203+ 1			2.0766- 3		2.0766- 3				14.2697- 3
4.0000+4	3.8464+ 3	3.2989+ 1	0.6908+ 1			1.5641- 3		1.5641- 3				14.4697- 3
5.0000+4	3.8608+ 3	3.3799+ 1	0.6633+ 1			1.0516- 3		1.0516- 3				14.6697- 3
6.0000+4	3.8766+ 3	3.4636+ 1	0.6378+ 1			5.6000- 3		5.6000- 3				14.8697- 3
7.0000+4	3.8938+ 3	3.5500+ 1	0.6143+ 1			5.0875- 3		5.0875- 3				15.0697- 3
8.0000+4	3.9124+ 3	3.6391+ 1	0.5928+ 1			4.5750- 3		4.5750- 3				15.2697- 3
9.0000+4	3.9325+ 3	3.7309+ 1	0.5733+ 1			4.0625- 3		4.0625- 3				15.4697- 3
1.0000+5	3.9541+ 3	3.8254+ 1	0.5558+ 1			3.5500- 3		3.5500- 3				15.6697- 3
2.0000+5	3.9772+ 3	3.9225+ 1	0.5403+ 1			3.0375- 3		3.0375- 3				15.8697- 3
3.0000+5	3.9928+ 3	4.0226+ 1	0.5268+ 1			2.5250- 3		2.5250- 3				16.0697- 3
4.0000+5	4.0109+ 3	4.1257+ 1	0.5153+ 1			2.0125- 3		2.0125- 3				16.2697- 3
5.0000+5	4.0315+ 3	4.2318+ 1	0.5058+ 1			1.5000- 3		1.5000- 3				16.4697- 3
6.0000+5	4.0546+ 3	4.3409+ 1	0.4983+ 1			1.0875- 3		1.0875- 3				16.6697- 3
7.0000+5	4.0802+ 3	4.4530+ 1	0.4928+ 1			0.6750- 3		0.6750- 3				16.8697- 3
8.0000+5	4.1083+ 3	4.5681+ 1	0.4893+ 1			0.2625- 3		0.2625- 3				17.0697- 3
9.0000+5	4.1390+ 3	4.6862+ 1	0.4878+ 1			0.1500- 3		0.1500- 3				17.2697- 3
1.0000+6	4.1724+ 3	4.8083+ 1	0.4883+ 1			0.0375- 3		0.0375- 3				17.4697- 3
2.0000+6	4.2095+ 3	4.9344+ 1	0.4908+ 1			0.0250- 3		0.0250- 3				17.6697- 3
3.0000+6	4.2502+ 3	5.0645+ 1	0.4953+ 1			0.0125- 3		0.0125- 3				17.8697- 3
4.0000+6	4.2945+ 3	5.1986+ 1	0.5018+ 1			0.0000- 3		0.0000- 3				18.0697- 3
5.0000+6	4.3424+ 3	5.3367+ 1	0.5093+ 1			0.0000- 3		0.0000- 3				18.2697- 3
6.0000+6	4.3938+ 3	5.4788+ 1	0.5178+ 1			0.0000- 3		0.0000- 3				18.4697- 3
7.0000+6	4.4487+ 3	5.6249+ 1	0.5273+ 1			0.0000- 3		0.0000- 3				18.6697- 3
8.0000+6	4.5071+ 3	5.7750+ 1	0.5378+ 1			0.0000- 3		0.0000- 3				18.8697- 3
9.0000+6	4.5690+ 3	5.9291+ 1	0.5493+ 1			0.0000- 3		0.0000- 3				19.0697- 3
1.0000+7	4.6344+ 3	6.0872+ 1	0.5618+ 1			0.0000- 3		0.0000- 3				19.2697- 3
2.0000+7	4.7033+ 3	6.2493+ 1	0.5763+ 1			0.0000- 3		0.0000- 3				19.4697- 3
3.0000+7	4.7756+ 3	6.4154+ 1	0.5928+ 1			0.0000- 3		0.0000- 3				19.6697- 3
4.0000+7	4.8513+ 3	6.5855+ 1	0.6113+ 1			0.0000- 3		0.0000- 3				19.8697- 3
5.0000+7	4.9304+ 3	6.7596+ 1	0.6318+ 1			0.0000- 3		0.0000- 3				20.0697- 3
6.0000+7	5.0128+ 3	6.9377+ 1	0.6543+ 1			0.0000- 3		0.0000- 3				20.2697- 3
7.0000+7	5.1000+ 3	7.1200+ 1	0.6788+ 1			0.0000- 3		0.0000- 3				20.4697- 3
8.0000+7	5.1924+ 3	7.3071+ 1	0.7053+ 1			0.0000- 3		0.0000- 3				20.6697- 3
9.0000+7	5.2900+ 3	7.5000+ 1	0.7338+ 1									

MATERIAL = 2305 CROSS SECTION TH-234

ENERGY	TOTAL	ELASTIC	INEL	IN.2N	(N.3N)	ELASTON	(N.4N)	(N.NP)	CAPTURE	(N.P)	(N.D)	(N.R)	MU-BAR
1.0000-5	1.0000-2	1.3000+1				0.0000+0			5.3941+0				4.6450-3
1.0000-4	1.5000-2	1.3000+1				0.0000+0			2.5021+0				5.0073-3
1.0000-3	2.0000-2	1.3000+1				0.0000+0			2.1096+0				5.1091-3
1.0000-2	3.0000-2	1.3000+1				0.0000+0			1.7694+0				5.2149-3
1.0000-1	4.0000-2	1.3000+1				0.0000+0			1.4915+0				5.3167-3
1.0000-0	5.0000-2	1.3000+1				0.0000+0			1.2789+0				5.3982-3
1.0000-0	6.0000-2	1.3000+1				0.0000+0			1.0865+0				5.4644-3
1.0000-0	7.0000-2	1.3000+1				0.0000+0			8.2900-1				5.6001-3
1.0000-0	8.0000-2	1.3000+1				0.0000+0			7.9101-1				5.6971-3
1.0000-0	9.0000-2	1.3000+1				0.0000+0			5.5993-1				5.7697-3
1.0000-0	1.0000-1	1.3000+1				0.0000+0			4.7112-1				5.8265-3
1.0000-0	2.0000-1	1.3000+1				0.0000+0			4.1530-1				5.8822-3
1.0000-0	3.0000-1	1.3000+1				0.0000+0			3.7643-1				5.9142-3
1.0000-0	4.0000-1	1.3000+1				0.0000+0			2.3361-1				5.9293-3
1.0000-0	5.0000-1	1.3000+1				0.0000+0			2.5000-1				5.9489-3
1.0000-0	6.0000-1	1.3000+1				0.0000+0			2.1074-1				5.9687-3
1.0000-0	7.0000-1	1.3000+1				0.0000+0			1.7675-1				5.9846-3
1.0000-0	8.0000-1	1.3000+1				0.0000+0			1.5026-1				5.9970-3
1.0000-0	9.0000-1	1.3000+1				0.0000+0			1.3026-1				6.0065-3
1.0000-0	1.0000-0	1.3000+1				0.0000+0			1.1666-1				6.0133-3
1.0000-0	2.0000-0	1.3000+1				0.0000+0			1.0534-1				6.0193-3
1.0000-0	3.0000-0	1.3000+1				0.0000+0			9.2610-2				6.0239-3
1.0000-0	4.0000-0	1.3000+1				0.0000+0			7.8030-2				6.0269-3
1.0000-0	5.0000-0	1.3000+1				0.0000+0			6.0598-2				6.0284-3
1.0000-0	6.0000-0	1.3000+1				0.0000+0			4.7395-2				6.0289-3
1.0000-0	7.0000-0	1.3000+1				0.0000+0			3.7136-2				6.0281-3
1.0000-0	8.0000-0	1.3000+1				0.0000+0			3.0888-2				6.0261-3
1.0000-0	9.0000-0	1.3000+1				0.0000+0			2.5232-2				6.0221-3
1.0000-0	1.0000+0	1.3000+1				0.0000+0			1.6453-1				6.0164-3
1.0000-0	2.0000+0	1.3000+1				0.0000+0			1.4451+1				6.0094-3
1.0000-0	3.0000+0	1.3000+1				0.0000+0			1.2896+1				6.0000-3
1.0000-0	4.0000+0	1.3000+1				0.0000+0			1.1693+1				6.0000-3
1.0000-0	5.0000+0	1.3000+1				0.0000+0			1.0738+1				6.0000-3
1.0000-0	6.0000+0	1.3000+1				0.0000+0			9.403+0				6.0000-3
1.0000-0	7.0000+0	1.3000+1				0.0000+0			5.2695+0				6.0000-3
1.0000-0	8.0000+0	1.3000+1				0.0000+0			4.2119+0				6.0000-3
1.0000-0	9.0000+0	1.3000+1				0.0000+0			3.7200+0				6.0000-3
1.0000-0	1.0000+0	1.3000+1				0.0000+0			3.0585+0				6.0000-3
1.0000-0	2.0000+0	1.3000+1				0.0000+0			2.3997+0				6.0000-3
1.0000-0	3.0000+0	1.3000+1				0.0000+0			1.8578+0				6.0000-3
1.0000-0	4.0000+0	1.3000+1				0.0000+0			1.4731+0				6.0000-3
1.0000-0	5.0000+0	1.3000+1				0.0000+0			1.1904+0				6.0000-3
1.0000-0	6.0000+0	1.3000+1				0.0000+0			9.3405+0				6.0000-3
1.0000-0	7.0000+0	1.3000+1				0.0000+0			8.3442+0				6.0000-3
1.0000-0	8.0000+0	1.3000+1				0.0000+0			7.4667+0				6.0000-3
1.0000-0	9.0000+0	1.3000+1				0.0000+0			6.5499+0				6.0000-3
1.0000-0	1.0000+0	1.3000+1				0.0000+0			5.7197+0				6.0000-3
1.0000-0	2.0000+0	1.3000+1				0.0000+0			4.9559+0				6.0000-3
1.0000-0	3.0000+0	1.3000+1				0.0000+0			4.3108+0				6.0000-3
1.0000-0	4.0000+0	1.3000+1				0.0000+0			3.7621+0				6.0000-3
1.0000-0	5.0000+0	1.3000+1				0.0000+0			3.2672+0				6.0000-3
1.0000-0	6.0000+0	1.3000+1				0.0000+0			2.8274+0				6.0000-3
1.0000-0	7.0000+0	1.3000+1				0.0000+0			2.4333+0				6.0000-3
1.0000-0	8.0000+0	1.3000+1				0.0000+0			1.8437+0				6.0000-3
1.0000-0	9.0000+0	1.3000+1				0.0000+0			1.5669+0				6.0000-3
1.0000-0	1.0000+0	1.3000+1				0.0000+0			1.3572+0				6.0000-3
1.0000-0	2.0000+0	1.3000+1				0.0000+0			1.1654+0				6.0000-3
1.0000-0	3.0000+0	1.3000+1				0.0000+0			1.0058+0				6.0000-3
1.0000-0	4.0000+0	1.3000+1				0.0000+0			8.4658+0				6.0000-3
1.0000-0	5.0000+0	1.3000+1				0.0000+0			7.3977+0				6.0000-3
1.0000-0	6.0000+0	1.3000+1				0.0000+0			6.0448+0				6.0000-3
1.0000-0	7.0000+0	1.3000+1				0.0000+0			4.4412+0				6.0000-3
1.0000-0	8.0000+0	1.3000+1				0.0000+0			3.9353+0				6.0000-3
1.0000-0	9.0000+0	1.3000+1				0.0000+0			2.6622+0				6.0000-3
1.0000-0	1.0000+0	1.3000+1				0.0000+0			2.1852+0				6.0000-3
1.0000-0	2.0000+0	1.3000+1				0.0000+0			1.7762+0				6.0000-3
1.0000-0	3.0000+0	1.3000+1				0.0000+0			1.4152+0				6.0000-3
1.0000-0	4.0000+0	1.3000+1				0.0000+0			1.1152+0				6.0000-3
1.0000-0	5.0000+0	1.3000+1				0.0000+0			9.9353+0				6.0000-3
1.0000-0	6.0000+0	1.3000+1				0.0000+0			8.2900+0				6.0000-3
1.0000-0	7.0000+0	1.3000+1				0.0000+0			7.1400+0				6.0000-3
1.0000-0	8.0000+0	1.3000+1				0.0000+0			6.0117+0				6.0000-3
1.0000-0	9.0000+0	1.3000+1				0.0000+0			5.0995+0				6.0000-3
1.0000-0	1.0000+0	1.3000+1				0.0000+0			4.3743+0				6.0000-3
1.0000-0	2.0000+0	1.3000+1				0.0000+0			3.8263+0				6.0000-3
1.0000-0	3.0000+0	1.3000+1				0.0000+0			3.3100+0				6.0000-3
1.0000-0	4.0000+0	1.3000+1				0.0000+0			2.8208+0				6.0000-3
1.0000-0	5.0000+0	1.3000+1				0.0000+0			2.3708+0				6.0000-3
1.0000-0	6.0000+0	1.3000+1				0.0000+0			1.9233+0				6.0000-3
1.0000-0	7.0000+0	1.3000+1				0.0000+0			1.4840+0				6.0000-3
1.0000-0	8.0000+0	1.3000+1				0.0000+0			1.0651+0				6.0000-3
1.0000-0	9.0000+0	1.3000+1				0.0000+0			2.0093+0				6.0000-3
1.0000-0	1.0000+0	1.3000+1				0.0000+0			2.6660+0				6.0000-3
1.0000-0	2.0000+0	1.3000+1				0.0000+0			3.6016+0				6.0000-3
1.0000-0	3.0000+0	1.3000+1				0.0000+0			4.5372+0				6.0000-3
1.0000-0	4.0000+0	1.3000+1				0.0000+0			5.4728+0				6.0000-3
1.0000-0	5.0000+0	1.3000+1				0.0000+0			6.4084+0				6.0000-3
1.0000-0	6.0000+0	1.3000+1				0.0000+0			7.3440+0				6.0000-3
1.0000-0	7.0000+0	1.3000+1				0.0000+0			8.2796+0				6.0000-3
1.0000-0	8.0000+0	1.3000+1				0.0000+0			9.2152+0				6.0000-3
1.0000-0	9.0000+0	1.3000+1				0.0000+0			1.0101+0				6.0000-3
1.0000-0	1.0000+0	1.3000+1				0.0000+0			1.2527+0				6.0000-3
1.0000-0	2.0000+0	1.3000+1											

MATERIAL = 2811 CROSS SECTION FR-233

ENERGY	TOTL	ELASTIC	INEL	(N,Z)	(N,3N)	FSSION	(N,NR)	(N,NP)	(N,P)	(N,D)	(N,A)	NU-BRR
1.0000-5 ~ 1.0000-2	1.6667+ 2	1.1020+ 1				0.0000+ 0						5.1348- 3
1.0000-2 ~ 1.5000-2	7.7798+ 1	1.1020+ 1				0.0000+ 0						5.1858- 3
1.5000-2 ~ 2.0000-2	6.5264+ 1	1.1020+ 1				0.0000+ 0						5.2001- 3
2.0000-2 ~ 3.0000-2	5.4412+ 1	1.1020+ 1				0.0000+ 0						5.2150- 3
3.0000-2 ~ 4.0000-2	4.5673+ 1	1.1020+ 1				0.0000+ 0						5.2294- 3
4.0000-2 ~ 5.0000-2	3.8377+ 1	1.1020+ 1				0.0000+ 0						5.2400- 3
5.0000-2 ~ 6.0000-2	3.2661+ 1	1.1020+ 1				0.0000+ 0						5.2516- 3
6.0000-2 ~ 8.0000-2	2.8266+ 1	1.1020+ 1				0.0000+ 0						5.2639- 3
1.0000-1 ~ 1.5000-1	2.6110+ 1	1.1020+ 1				0.0000+ 0						5.2829- 3
1.5000-1 ~ 2.0000-1	2.3820+ 1	1.1036+ 1				0.0000+ 0						5.2972- 3
2.0000-1 ~ 3.0000-1	2.2929+ 1	1.1036+ 1				0.0000+ 0						5.3171- 3
3.0000-1 ~ 4.0000-1	2.2662+ 1	1.1036+ 1				0.0000+ 0						5.3371- 3
4.0000-1 ~ 5.0000-1	2.2450+ 1	1.1044+ 1				0.0000+ 0						5.3566- 3
5.0000-1 ~ 6.0000-1	2.2244+ 1	1.1044+ 1				0.0000+ 0						5.3766- 3
6.0000-1 ~ 8.0000-1	2.2056+ 1	1.1059+ 1				0.0000+ 0						5.3969- 3
1.0000-0 ~ 1.5000-0	4.3810+ 2	1.3020+ 1				0.0000+ 0						5.3943- 3
1.5000-0 ~ 2.0000-0	6.5110+ 2	1.3050+ 1				0.0000+ 0						5.4082- 3
2.0000-0 ~ 3.0000-0	2.6006+ 2	1.3093+ 1				0.0000+ 0						5.4235- 3
3.0000-0 ~ 4.0000-0	2.5000+ 2	1.3093+ 1				0.0000+ 0						5.4375- 3
4.0000-0 ~ 5.0000-0	2.4000+ 2	1.3093+ 1				0.0000+ 0						5.4526- 3
5.0000-0 ~ 6.0000-0	2.3000+ 2	1.3093+ 1				0.0000+ 0						5.4677- 3
6.0000-0 ~ 8.0000-0	2.2000+ 2	1.3093+ 1				0.0000+ 0						5.4835- 3
1.0000+ 1 ~ 1.5000+ 1	6.8634+ 1	1.1245+ 1				0.0000+ 0						5.4770- 3
1.5000+ 1 ~ 2.0000+ 1	9.1655+ 1	1.1245+ 1				0.0000+ 0						5.4919- 3
2.0000+ 1 ~ 3.0000+ 1	7.2610+ 1	1.1820+ 1				0.0000+ 0						5.5062- 3
3.0000+ 1 ~ 4.0000+ 1	6.2795+ 1	1.1820+ 1				0.0000+ 0						5.5205- 3
4.0000+ 1 ~ 5.0000+ 1	5.2936+ 1	1.1726+ 1				0.0000+ 0						5.5347- 3
5.0000+ 1 ~ 6.0000+ 1	4.3056+ 1	1.1726+ 1				0.0000+ 0						5.5489- 3
6.0000+ 1 ~ 8.0000+ 1	4.2556+ 1	1.1757+ 1				0.0000+ 0						5.5630+ 3
1.0000+ 2 ~ 1.5000+ 2	3.8139+ 1	1.1734+ 1				0.0000+ 0						5.5740- 3
1.5000+ 2 ~ 2.0000+ 2	3.0010+ 1	1.1674+ 1				0.0000+ 0						5.5884+ 3
2.0000+ 2 ~ 3.0000+ 2	2.6896+ 1	1.1637+ 1				0.0000+ 0						5.6027+ 3
3.0000+ 2 ~ 4.0000+ 2	2.4985+ 1	1.1637+ 1				0.0000+ 0						5.6170+ 3
4.0000+ 2 ~ 5.0000+ 2	2.3555+ 1	1.1686+ 1				0.0000+ 0						5.6312+ 3
5.0000+ 2 ~ 6.0000+ 2	2.2327+ 1	1.1686+ 1				0.0000+ 0						5.6454+ 3
6.0000+ 2 ~ 8.0000+ 2	2.0723+ 1	1.1659+ 1				0.0000+ 0						5.6596+ 3
1.0000+ 3 ~ 1.5000+ 3	1.9021+ 1	1.2100+ 1				0.0000+ 0						5.6738+ 3
1.5000+ 3 ~ 2.0000+ 3	1.8470+ 1	1.2100+ 1				0.0000+ 0						5.6880+ 3
2.0000+ 3 ~ 3.0000+ 3	1.7400+ 1	1.2100+ 1				0.0000+ 0						5.7022+ 3
3.0000+ 3 ~ 4.0000+ 3	1.6123+ 1	1.2100+ 1				0.0000+ 0						5.7164+ 3
4.0000+ 3 ~ 5.0000+ 3	1.5755+ 1	1.2100+ 1				0.0000+ 0						5.7306+ 3
5.0000+ 3 ~ 6.0000+ 3	1.5447+ 1	1.2100+ 1				0.0000+ 0						5.7448+ 3
6.0000+ 3 ~ 8.0000+ 3	1.5193+ 1	1.2024+ 1				0.0000+ 0						5.7590+ 3
1.0000+ 4 ~ 1.5000+ 4	1.4923+ 1	1.2000+ 1				0.0000+ 0						5.7732+ 3
1.5000+ 4 ~ 2.0000+ 4	1.4656+ 1	1.1696+ 1				0.0000+ 0						5.7874+ 3
2.0000+ 4 ~ 3.0000+ 4	1.4130+ 1	1.1793+ 1				0.0000+ 0						5.8016+ 3
3.0000+ 4 ~ 4.0000+ 4	1.3971+ 1	1.1698+ 1				0.0000+ 0						5.8158+ 3
4.0000+ 4 ~ 5.0000+ 4	1.3950+ 1	1.1698+ 1				0.0000+ 0						5.8300+ 3
5.0000+ 4 ~ 6.0000+ 4	1.3827+ 1	1.1729+ 1				0.0000+ 0						5.8442+ 3
6.0000+ 4 ~ 8.0000+ 4	1.3654+ 1	1.1698+ 1				0.0000+ 0						5.8584+ 3
1.0000+ 5 ~ 1.5000+ 5	1.2084+ 1	1.0858+ 1				0.0000+ 0						5.8726+ 3
1.5000+ 5 ~ 2.0000+ 5	1.1865+ 1	1.0858+ 1				0.0000+ 0						5.8868+ 3
2.0000+ 5 ~ 3.0000+ 5	1.0653+ 1	1.0858+ 1				0.0000+ 0						5.9010+ 3
3.0000+ 5 ~ 4.0000+ 5	9.1252+ 0	6.9311+ 0				0.0000+ 0						5.9152+ 3
4.0000+ 5 ~ 5.0000+ 5	8.4135+ 0	6.2688+ 0				0.0000+ 0						5.9294+ 3
5.0000+ 5 ~ 6.0000+ 5	7.7002+ 0	4.6588+ 0				0.0000+ 0						5.9436+ 3
6.0000+ 5 ~ 8.0000+ 5	6.6031+ 0	3.9311+ 0				0.0000+ 0						5.9578+ 3
1.5000+ 6 ~ 2.0000+ 6	6.6843+ 0	3.7430+ 0				0.0000+ 0						5.9720+ 3
2.0000+ 6 ~ 3.0000+ 6	7.3461+ 0	4.3808+ 0				0.0000+ 0						5.9862+ 3
3.0000+ 6 ~ 4.0000+ 6	7.0450+ 0	4.2924+ 0				0.0000+ 0						5.9999+ 3
4.0000+ 6 ~ 5.0000+ 6	7.1420+ 0	4.4177+ 0				0.0000+ 0						6.0141+ 3
5.0000+ 6 ~ 6.0000+ 6	5.6117+ 0	3.7979+ 0				0.0000+ 0						6.0283+ 3
6.0000+ 6 ~ 8.0000+ 6	5.8507+ 0	3.1052+ 0				0.0000+ 0						6.0425+ 3
1.0000+ 7 ~ 1.5000+ 7	6.6521+ 0	3.0526+ 0				0.0000+ 0						6.0567+ 3
1.5000+ 7 ~ 2.0000+ 7	5.7162+ 0	3.0526+ 0				0.0000+ 0						6.0709+ 3

CROSS SECTION MATERIAL = 2821 U - 233

ENERGY	TOTAL	ELASTIC	INEL	(N,2N)	(N,3N)	FISSION	(N,NA)	(N,NP)	(N,DI)	(N,RI)	MU-BAR
1.0000- 5 ~ 1.0000- 2	1.0046+ 3	1.3924+ 1				1.8512+ 3					3.3326- 3
1.0000- 1.5000-	8.4851+ 2	1.2830+ 1				7.6996+ 3					3.4342- 3
1.0000- 2.0000-	7.1332+ 1	1.2705+ 1				5.4661+ 1					3.4786- 3
1.0000- 3.0000-	5.9889+ 6	1.2705+ 1				4.7184+ 1					3.5023- 3
1.0000- 4.0000-	4.4828+ 1	1.2658+ 1				3.8765+ 1					3.5211- 3
1.0000- 5.0000-	4.0361+ 1	1.2643+ 1				3.5500+ 1					3.5371- 3
1.0000- 6.0000-	3.6796+ 3	1.2623+ 1				3.1834+ 1					3.5536- 3
1.0000- 7.0000-	3.1671+ 2	1.2588+ 1				2.7891+ 1					3.5706- 3
1.0000- 8.0000-	2.7411+ 3	1.2553+ 1				2.4333+ 1					3.5883- 3
1.0000- 9.0000-	2.4151+ 2	1.2500+ 1				2.0916+ 1					3.6040- 3
1.0000- 1.00000-	2.1179+ 1	1.2460+ 1				1.8160+ 1					3.6196- 3
1.0000- 1.50000-	1.8695+ 2	1.2410+ 1				1.5803+ 1					3.6352- 3
1.0000- 2.00000-	1.6370+ 1	1.2361+ 1				1.3900+ 1					3.6508- 3
1.0000- 3.00000-	1.4420+ 1	1.2312+ 1				1.2331+ 1					3.6664- 3
1.0000- 4.00000-	1.2868+ 1	1.2263+ 1				1.1025+ 1					3.6820- 3
1.0000- 5.00000-	1.1498+ 1	1.2214+ 1				1.0000+ 1					3.6976- 3
1.0000- 6.00000-	1.0385+ 1	1.2165+ 1				0.9177+ 1					3.7132- 3
1.0000- 7.00000-	0.9481+ 1	1.2116+ 1				0.8523+ 1					3.7288- 3
1.0000- 8.00000-	0.8711+ 2	1.2067+ 1				0.7996+ 1					3.7444- 3
1.0000- 9.00000-	0.8059+ 2	1.2018+ 1				0.7587+ 1					3.7600- 3
1.0000- 1.00000-	0.7500+ 2	1.1969+ 1				0.7284+ 1					3.7756- 3
1.0000- 1.50000-	0.7013+ 2	1.1920+ 1				0.7082+ 1					3.7912- 3
1.0000- 2.00000-	0.6584+ 2	1.1871+ 1				0.6980+ 1					3.8068- 3
1.0000- 3.00000-	0.6200+ 2	1.1822+ 1				0.6978+ 1					3.8224- 3
1.0000- 4.00000-	0.5859+ 2	1.1773+ 1				0.7076+ 1					3.8380- 3
1.0000- 5.00000-	0.5554+ 2	1.1724+ 1				0.7274+ 1					3.8536- 3
1.0000- 6.00000-	0.5280+ 2	1.1675+ 1				0.7572+ 1					3.8692- 3
1.0000- 7.00000-	0.5023+ 2	1.1626+ 1				0.7970+ 1					3.8848- 3
1.0000- 8.00000-	0.4781+ 2	1.1577+ 1				0.8468+ 1					3.9004- 3
1.0000- 9.00000-	0.4550+ 2	1.1528+ 1				0.9066+ 1					3.9160- 3
1.0000- 1.00000-	0.4330+ 2	1.1479+ 1				0.9764+ 1					3.9316- 3
1.0000- 1.50000-	0.4120+ 2	1.1430+ 1				1.0562+ 1					3.9472- 3
1.0000- 2.00000-	0.3920+ 2	1.1381+ 1				1.1460+ 1					3.9628- 3
1.0000- 3.00000-	0.3730+ 2	1.1332+ 1				1.2458+ 1					3.9784- 3
1.0000- 4.00000-	0.3550+ 2	1.1283+ 1				1.3556+ 1					3.9940- 3
1.0000- 5.00000-	0.3380+ 2	1.1234+ 1				1.4754+ 1					4.0096- 3
1.0000- 6.00000-	0.3220+ 2	1.1185+ 1				1.6052+ 1					4.0252- 3
1.0000- 7.00000-	0.3070+ 2	1.1136+ 1				1.7450+ 1					4.0408- 3
1.0000- 8.00000-	0.2930+ 2	1.1087+ 1				1.8948+ 1					4.0564- 3
1.0000- 9.00000-	0.2800+ 2	1.1038+ 1				2.0546+ 1					4.0720- 3
1.0000- 1.00000-	0.2680+ 2	1.0989+ 1				2.2244+ 1					4.0876- 3
1.0000- 1.50000-	0.2570+ 2	1.0940+ 1				2.4042+ 1					4.1032- 3
1.0000- 2.00000-	0.2470+ 2	1.0891+ 1				2.5940+ 1					4.1188- 3
1.0000- 3.00000-	0.2380+ 2	1.0842+ 1				2.7938+ 1					4.1344- 3
1.0000- 4.00000-	0.2300+ 2	1.0793+ 1				3.0036+ 1					4.1500- 3
1.0000- 5.00000-	0.2230+ 2	1.0744+ 1				3.2234+ 1					4.1656- 3
1.0000- 6.00000-	0.2170+ 2	1.0695+ 1				3.4532+ 1					4.1812- 3
1.0000- 7.00000-	0.2120+ 2	1.0646+ 1				3.6930+ 1					4.1968- 3
1.0000- 8.00000-	0.2080+ 2	1.0597+ 1				3.9428+ 1					4.2124- 3
1.0000- 9.00000-	0.2050+ 2	1.0548+ 1				4.2026+ 1					4.2280- 3
1.0000- 1.00000-	0.2030+ 2	1.0500+ 1				4.4724+ 1					4.2436- 3
1.0000- 1.50000-	0.2020+ 2	1.0451+ 1				4.7522+ 1					4.2592- 3
1.0000- 2.00000-	0.2020+ 2	1.0402+ 1				5.0420+ 1					4.2748- 3
1.0000- 3.00000-	0.2030+ 2	1.0353+ 1				5.3418+ 1					4.2904- 3
1.0000- 4.00000-	0.2050+ 2	1.0304+ 1				5.6516+ 1					4.3060- 3
1.0000- 5.00000-	0.2080+ 2	1.0255+ 1				5.9714+ 1					4.3216- 3
1.0000- 6.00000-	0.2120+ 2	1.0206+ 1				6.3012+ 1					4.3372- 3
1.0000- 7.00000-	0.2170+ 2	1.0157+ 1				6.6410+ 1					4.3528- 3
1.0000- 8.00000-	0.2230+ 2	1.0108+ 1				7.0008+ 1					4.3684- 3
1.0000- 9.00000-	0.2300+ 2	1.0059+ 1				7.3806+ 1					4.3840- 3
1.0000- 1.00000-	0.2380+ 2	1.0010+ 1				7.7804+ 1					4.3996- 3
1.0000- 1.50000-	0.2470+ 2	0.9961+ 1				8.1902+ 1					4.4152- 3
1.0000- 2.00000-	0.2570+ 2	0.9912+ 1				8.6100+ 1					4.4308- 3
1.0000- 3.00000-	0.2680+ 2	0.9863+ 1				9.0498+ 1					4.4464- 3
1.0000- 4.00000-	0.2800+ 2	0.9814+ 1				9.5096+ 1					4.4620- 3
1.0000- 5.00000-	0.2930+ 2	0.9765+ 1				9.9894+ 1					4.4776- 3
1.0000- 6.00000-	0.3070+ 2	0.9716+ 1				1.0487+ 1					4.4932- 3
1.0000- 7.00000-	0.3220+ 2	0.9667+ 1				1.1185+ 1					4.5088- 3
1.0000- 8.00000-	0.3380+ 2	0.9618+ 1				1.1983+ 1					4.5244- 3
1.0000- 9.00000-	0.3550+ 2	0.9569+ 1				1.2881+ 1					4.5400- 3
1.0000- 1.00000-	0.3730+ 2	0.9520+ 1				1.3879+ 1					4.5556- 3
1.0000- 1.50000-	0.3920+ 2	0.9471+ 1				1.4977+ 1					4.5712- 3
1.0000- 2.00000-	0.4120+ 2	0.9422+ 1				1.6175+ 1					4.5868- 3
1.0000- 3.00000-	0.4330+ 2	0.9373+ 1				1.7473+ 1					4.6024- 3
1.0000- 4.00000-	0.4550+ 2	0.9324+ 1				1.8871+ 1					4.6180- 3
1.0000- 5.00000-	0.4780+ 2	0.9275+ 1				2.0369+ 1					4.6336- 3
1.0000- 6.00000-	0.5020+ 2	0.9226+ 1				2.1967+ 1					4.6492- 3
1.0000- 7.00000-	0.5270+ 2	0.9177+ 1				2.3665+ 1					4.6648- 3
1.0000- 8.00000-	0.5530+ 2	0.9128+ 1				2.5463+ 1					4.6804- 3
1.0000- 9.00000-	0.5800+ 2	0.9079+ 1				2.7361+ 1					4.6960- 3
1.0000- 1.00000-	0.6080+ 2	0.9030+ 1				2.9359+ 1					4.7116- 3
1.0000- 1.50000-	0.6380+ 2	0.8981+ 1				3.1457+ 1					4.7272- 3
1.0000- 2.00000-	0.6700+ 2	0.8932+ 1				3.3655+ 1					4.7428- 3
1.0000- 3.00000-	0.7050+ 2	0.8883+ 1				3.5953+ 1					4.7584- 3
1.0000- 4.00000-	0.7430+ 2	0.8834+ 1				3.8351+ 1					4.7740- 3
1.0000- 5.00000-	0.7850+ 2	0.8785+ 1				4.0849+ 1					4.7896- 3
1.0000- 6.00000-	0.8320+ 2	0.8736+ 1				4.3447+ 1					4.8052- 3
1.0000- 7.00000-	0.8850+ 2	0.8687+ 1				4.6145+ 1					4.8208- 3
1.0000- 8.00000-	0.9450+ 2	0.8638+ 1				4.8943+ 1					4.8364- 3
1.0000- 9.00000-	1.0120+ 2	0.8589+ 1				5.1841+ 1					4.8520- 3
1.0000- 1.00000-	1.0870+ 2	0.8540+ 1				5.4839+ 1					4.8676- 3
1.0000- 1.50000-	1.1700+ 2	0.8491+ 1				5.7937+ 1					4.8832- 3
1.0000- 2.00000-	1.2620+ 2	0.8442+ 1				6.1135+ 1					4.8988- 3
1.0000- 3.00000-	1.3640+ 2	0.8393+ 1				6.4433+ 1					4.9144- 3
1.0000- 4.00000-	1.4770+ 2	0.8344+ 1				6.7831+ 1					4.9300- 3
1.0000- 5.00000-	1.6020+ 2	0.8295+ 1				7.1329+ 1					4.9456- 3
1.0000- 6.00000-	1.7390+ 2	0.8246+ 1				7.4927+ 1					4.9612- 3
1.0000- 7.00000-	1.8890+ 2	0.8197+ 1				7.8625+ 1					4.9768- 3
1.0000- 8.00000-	2.0530+ 2	0.8148+ 1				8					

MATERIAL -2923 CROSS SECTION U -236

ENERGY	TOTAL	ELASTIC	INELR	(N.2N)	(N.3N)	FISSION	(N.MR)	(N.NP)	(N.P)	(N.D)	(N.R)	RU-BRR
1.0000- 5	2.2850+ 3	1.7000+ 1			1.5810+ 3	9.5972+ 3	9.0899+ 2					2.8882- 3
1.0000- 4	1.0193+ 3	1.7000+ 1			6.5972+ 3	1.1832+ 3	1.1832+ 3					8.950- 3
1.0000- 3	6.6576+ 3	1.7000+ 1			6.6576+ 3	6.6576+ 3	1.1832+ 3					2.9393- 3
1.0000- 2	5.0835+ 3	1.7000+ 1			4.3960+ 2	4.3960+ 2	8.0828+ 1					2.8989- 3
1.0000- 1	5.0101+ 2	1.7000+ 1			4.1112+ 2	4.1112+ 2	7.1067+ 1					2.8011- 3
1.0000- 0	3.4761+ 2	1.7000+ 1			3.4761+ 2	3.4761+ 2	5.7161+ 1					2.8011- 3
1.0000- 0	3.4478+ 2	1.6800+ 1			2.7498+ 2	2.7498+ 2	5.0088+ 1					2.8011- 3
1.0000- 0	2.8430+ 1	1.6000+ 1			2.8554+ 1	2.8554+ 1	4.2091+ 1					2.8080- 3
1.0000- 0	2.3681+ 1	1.6000+ 1			1.6486+ 1	1.6486+ 1	3.5261+ 1					2.8080- 3
1.0000- 0	2.4237+ 1	1.5975+ 1			1.2710+ 1	1.2710+ 1	2.8130+ 1					2.8080- 3
1.0000- 0	1.9276+ 1	1.5060+ 1			9.4319+ 1	9.4319+ 1	2.2723+ 1					2.8109- 3
1.0000- 0	9.4565+ 1	1.4800+ 1			7.1288+ 1	7.1288+ 1	8.1204+ 0					2.8112- 3
1.0000- 0	8.1950+ 1	1.4300+ 1			6.1664+ 1	6.1664+ 1	5.8825+ 0					2.8113- 3
1.0000- 0	8.2880+ 1	1.3775+ 1			6.2253+ 1	6.2253+ 1	5.7357+ 0					2.8119- 3
1.0000- 0	7.2637+ 1	1.3391+ 1			5.0169+ 1	5.0169+ 1	1.4077+ 1					2.8170- 3
1.0000- 0	4.3588+ 1	1.2672+ 1			1.4978+ 1	1.4978+ 1	5.9390+ 0					2.8166- 3
1.0000- 0	3.3422+ 1	1.2008+ 1			1.3439+ 1	1.3439+ 1	7.9770+ 0					2.8203- 3
1.0000- 0	5.6695+ 1	1.1551+ 1			2.5739+ 1	2.5739+ 1	1.5408+ 1					2.8203- 3
1.0000- 0	4.1090+ 1	1.1015+ 1			2.0548+ 1	2.0548+ 1	4.028+ 0					2.8203- 3
1.0000- 0	2.2939+ 1	1.0279+ 1			1.6999+ 1	1.6999+ 1	4.5761+ 1					2.8203- 3
1.0000- 0	9.7445+ 2	1.1920+ 1			1.0717+ 2	1.0717+ 2	5.4788+ 1					2.8265- 3
1.0000+ 1	1.0357+ 2	1.1886+ 1			3.9986+ 1	3.9986+ 1	5.1775+ 1					2.8307- 3
1.0000+ 1	1.1333+ 2	1.2234+ 1			3.2758+ 1	3.2758+ 1	2.6116+ 1					2.8307- 3
1.0000+ 1	7.7437+ 2	1.3070+ 1			3.9708+ 1	3.9708+ 1	3.9595+ 1					2.8307- 3
1.0000+ 1	1.7613+ 2	1.1750+ 1			3.5143+ 1	3.5143+ 1	2.4919+ 1					2.8307- 3
1.0000+ 1	1.0154+ 2	1.3883+ 1			6.0844+ 1	6.0844+ 1	2.8890+ 1					2.8307- 3
1.0000+ 1	4.7819+ 1	1.2804+ 1	4.895-10		2.3302+ 1	2.3302+ 1	1.7853+ 1					2.8351- 3
1.0000+ 1	5.8554+ 1	1.3602+ 1			2.8489+ 1	2.8489+ 1	1.7283+ 1					2.8321- 3
1.0000+ 2	4.7160+ 1	1.1307+ 1			2.2209+ 1	2.2209+ 1	1.3644+ 1					3.0090- 3
1.0000+ 2	4.6631+ 1	1.1975+ 1	3.1110- 8		2.1099+ 1	2.1099+ 1	1.2756+ 1					3.0765- 3
1.0000+ 2	4.3922+ 1	1.2842+ 1	6.2261- 8		2.0899+ 1	2.0899+ 1	1.0211+ 1					3.0765- 3
1.0000+ 2	3.2888+ 1	1.488+ 1	7.4556- 8		1.488+ 1	1.488+ 1	5.191+ 1					3.0765- 3
1.0000+ 2	3.0778+ 1	1.0962+ 1	9.1610- 7		1.4058+ 1	1.4058+ 1	3.4146+ 1					3.0765- 3
1.0000+ 2	3.0778+ 1	1.0962+ 1	1.2467- 7		1.1498+ 1	1.1498+ 1	4.7454+ 1					3.0765- 3
1.0000+ 2	2.7966+ 1	1.1439+ 1	1.3655- 7		1.1709+ 1	1.1709+ 1	4.8207+ 1					3.0765- 3
1.0000+ 2	2.4600+ 1	1.2120+ 1	1.5428- 7		1.0946+ 1	1.0946+ 1	4.2868+ 1					3.0765- 3
1.0000+ 3	2.4159+ 1	1.2911+ 1	7.453- 7		7.873+ 0	7.873+ 0	3.7039+ 0					4.4341- 3
1.0000+ 3	2.0568+ 1	1.2719+ 1	1.6553- 7		5.9376+ 0	5.9376+ 0	2.2686+ 0					5.1183- 3
1.0000+ 3	2.0568+ 1	1.2719+ 1	2.4313- 7		5.9376+ 0	5.9376+ 0	2.2686+ 0					6.0602- 3
1.0000+ 3	1.6328+ 1	1.3366+ 1	5.5205- 6		4.1930+ 0	4.1930+ 0	1.8859+ 0					7.8813- 3
1.0000+ 3	1.7495+ 1	1.2217+ 1	2.1365- 6		3.9519+ 0	3.9519+ 0	1.8859+ 0					8.0028- 3
1.0000+ 3	1.6715+ 1	1.2470+ 1	1.6866- 5		3.1333+ 0	3.1333+ 0	1.2778+ 0					1.2009- 3
1.0000+ 4	1.5955+ 1	1.2182+ 1	1.7415- 3		2.7299+ 0	2.7299+ 0	1.0287+ 0					1.4760- 3
1.0000+ 4	1.5296+ 1	1.1943+ 1	1.3151- 3		2.4010+ 0	2.4010+ 0	1.0287+ 0					1.9494- 3
1.0000+ 4	1.4557+ 1	1.1598+ 1	2.3921- 2		2.0393+ 0	2.0393+ 0	7.7307+ 0					3.6765- 3
1.0000+ 4	1.3411+ 1	1.0788+ 1	3.9921- 2		1.9195+ 0	1.9195+ 0	7.3073+ 0					5.0299- 3
1.0000+ 4	1.3041+ 1	1.0486+ 1	1.4124- 1		1.8114+ 0	1.8114+ 0	6.5888+ 0					8.3447- 3
1.0000+ 4	1.2591+ 1	1.0087+ 1	2.2627- 1		1.7741+ 0	1.7741+ 0	5.7818+ 0					7.8325- 3
1.0000+ 4	1.2207+ 1	1.2470+ 1	1.6878- 1		1.6463+ 0	1.6463+ 0	5.2512+ 0					9.1177- 3
1.0000+ 5	1.1625+ 1	9.1181+ 0	5.814- 1		1.5625+ 0	1.5625+ 0	4.0265+ 1					1.5400- 3
1.0000+ 5	1.0093+ 1	8.3730+ 0	7.6493- 1		1.4222+ 0	1.4222+ 0	3.3718+ 1					1.9888- 3
1.0000+ 5	1.0093+ 1	8.3730+ 0	9.1577- 1		1.3171+ 0	1.3171+ 0	2.7429+ 1					2.0122- 3
1.0000+ 5	8.2088+ 0	6.6547+ 0	1.1011+ 0		1.2381+ 0	1.2381+ 0	2.6299+ 1					3.4681- 3
1.0000+ 5	8.0595+ 0	6.2398+ 0	1.3654+ 0		1.1631+ 0	1.1631+ 0	2.6204+ 1					4.6204- 3
1.0000+ 5	7.4591+ 0	4.7057+ 0	1.4486+ 0		1.1691+ 0	1.1691+ 0	1.4519+ 1					4.1938- 3
1.0000+ 5	6.9731+ 0	4.1657+ 0	1.4729+ 0		1.1868+ 0	1.1868+ 0	1.4749+ 1					4.5650- 3
1.0000+ 6	6.7924+ 0	3.6927+ 0	1.5931+ 0		1.2463+ 0	1.2463+ 0	1.8308+ 1					5.0821- 3
1.0000+ 6	7.5926+ 0	4.1904+ 0	1.6896+ 0		1.2188+ 0	1.2188+ 0	1.4933+ 1					5.6811- 3
1.0000+ 6	7.5926+ 0	4.4546+ 0	2.2270+ 0		1.1931+ 0	1.1931+ 0	9.5912+ 2					6.8986- 3
1.0000+ 6	7.8121+ 0	4.1744+ 0	2.2109+ 0		1.1165+ 0	1.1165+ 0	7.6570+ 1					7.6570+ 3
1.0000+ 6	7.3798+ 0	4.1898+ 0	2.3089+ 0		1.0962+ 0	1.0962+ 0	1.0105+ 1					7.9768- 3
1.0000+ 6	6.5329+ 0	3.2138+ 0	4.6255+ 0		1.7714+ 0	1.7714+ 0	1.3978+ 1					8.0541- 3
1.0000+ 7	6.5329+ 0	3.4057+ 0	3.9797- 1		1.7714+ 0	1.7714+ 0	2.6731+ 1					8.0418- 3
1.0000+ 7	6.8043+ 0	3.4057+ 0	5.5973- 1		1.8984+ 0	1.8984+ 0	4.4871+ 1					8.3185- 3
1.0000+ 7	6.1972+ 0	3.4057+ 0	5.5973- 1		1.8984+ 0	1.8984+ 0	4.4871+ 1					8.3185- 3
1.0000+ 7	6.1972+ 0	3.4057+ 0	5.5973- 1		1.8984+ 0	1.8984+ 0	4.4871+ 1					8.3185- 3

CROSS SECTION MATERIAL = 2924 U - 238

ENERGY	TOTAL	ELASTIC	INEL	IN.2N	(N.3N)	FISION	(N.NP)	CAPTURE	(N.P)	(N.O)	(N.R)	MURR
1.0000- 5 ~ 1.0000- 2	2.4614+ 1	0.3413+ 0			1.3198- 1	1.6340+ 1						2.0498- 9
1.0000- 2 ~ 1.0000- 1	1.6986+ 1	0.3986+ 0			6.1454+ 0	7.5853+ 0						2.0498- 9
1.0000- 1 ~ 1.0000- 0	1.4790+ 1	0.3385+ 0			5.1767+ 0	6.3903+ 0						2.0498- 9
1.0000- 0 ~ 1.0000- 0	1.2601+ 1	0.3392+ 0			3.2911+ 0	4.5229+ 0						2.0498- 9
1.0000- 0 ~ 1.0000- 0	1.3366+ 1	0.3324+ 0			3.2544+ 0	4.0014+ 0						2.0498- 9
1.0000- 0 ~ 1.0000- 0	1.1977+ 1	0.3301+ 0			2.9519+ 0	3.6178+ 0						2.0498- 9
1.0000- 0 ~ 1.0000- 0	1.1576+ 1	0.3257+ 0			2.8368+ 0	3.2225+ 0						2.0498- 9
1.0000- 0 ~ 1.0000- 0	1.1191+ 1	0.3222+ 0			2.7378+ 0	2.8459+ 0						2.0498- 9
1.0000- 0 ~ 1.0000- 0	1.0776+ 1	0.3143+ 0			2.6185+ 0	2.4411+ 0						2.0498- 9
1.0000- 0 ~ 1.0000- 0	1.0398+ 1	0.3029+ 0			1.7291+ 0	2.0676+ 0						2.0498- 9
1.0000- 0 ~ 1.0000- 0	1.0053+ 1	0.2856+ 0			1.4893+ 0	1.7526+ 0						2.0498- 9
1.0000- 0 ~ 1.0000- 0	0.9780+ 1	0.2681+ 0			1.2970+ 0	1.5054+ 0						2.0498- 9
1.0000- 0 ~ 1.0000- 0	0.9566+ 1	0.2516+ 0			1.1056+ 0	1.2488+ 0						2.0498- 9
1.0000- 0 ~ 1.0000- 0	0.9388+ 1	0.2367+ 0			1.0423+ 0	1.1427+ 0						2.0498- 9
1.0000- 0 ~ 1.0000- 0	0.9249+ 1	0.2229+ 0			0.9196+ 0	1.0659+ 0						2.0498- 9
1.0000- 0 ~ 1.0000- 0	0.9149+ 1	0.2109+ 0			0.8040+ 0	0.9785+ 0						2.0498- 9
1.0000- 0 ~ 1.0000- 0	0.9071+ 1	0.2000+ 0			0.7194+ 0	0.9171+ 0						2.0498- 9
1.0000- 0 ~ 1.0000- 0	0.9011+ 1	0.1906+ 0			0.6560+ 0	0.8684+ 0						2.0498- 9
1.0000- 0 ~ 1.0000- 0	0.9000+ 0	0.1821+ 0			0.6041+ 0	0.8216+ 0						2.0498- 9
1.0000- 0 ~ 1.0000- 0	0.9000+ 0	0.1744+ 0			0.5622+ 0	0.7772+ 0						2.0498- 9
1.0000- 0 ~ 1.0000- 0	0.9000+ 0	0.1674+ 0			0.5294+ 0	0.7354+ 0						2.0498- 9
1.0000- 0 ~ 1.0000- 0	0.9000+ 0	0.1610+ 0			0.4957+ 0	0.6962+ 0						2.0498- 9
1.0000- 0 ~ 1.0000- 0	0.9000+ 0	0.1552+ 0			0.4611+ 0	0.6595+ 0						2.0498- 9
1.0000- 0 ~ 1.0000- 0	0.9000+ 0	0.1499+ 0			0.4256+ 0	0.6252+ 0						2.0498- 9
1.0000- 0 ~ 1.0000- 0	0.9000+ 0	0.1450+ 0			0.3893+ 0	0.5931+ 0						2.0498- 9
1.0000- 0 ~ 1.0000- 0	0.9000+ 0	0.1405+ 0			0.3524+ 0	0.5631+ 0						2.0498- 9
1.0000- 0 ~ 1.0000- 0	0.9000+ 0	0.1364+ 0			0.3150+ 0	0.5351+ 0						2.0498- 9
1.0000- 0 ~ 1.0000- 0	0.9000+ 0	0.1326+ 0			0.2772+ 0	0.5091+ 0						2.0498- 9
1.0000- 0 ~ 1.0000- 0	0.9000+ 0	0.1291+ 0			0.2390+ 0	0.4849+ 0						2.0498- 9
1.0000- 0 ~ 1.0000- 0	0.9000+ 0	0.1258+ 0			0.2004+ 0	0.4624+ 0						2.0498- 9
1.0000- 0 ~ 1.0000- 0	0.9000+ 0	0.1227+ 0			0.1614+ 0	0.4414+ 0						2.0498- 9
1.0000- 0 ~ 1.0000- 0	0.9000+ 0	0.1198+ 0			0.1220+ 0	0.4218+ 0						2.0498- 9
1.0000- 0 ~ 1.0000- 0	0.9000+ 0	0.1171+ 0			0.0822+ 0	0.4035+ 0						2.0498- 9
1.0000- 0 ~ 1.0000- 0	0.9000+ 0	0.1146+ 0			0.0417+ 0	0.3864+ 0						2.0498- 9
1.0000- 0 ~ 1.0000- 0	0.9000+ 0	0.1122+ 0			0.0000+ 0	0.3704+ 0						2.0498- 9
1.0000- 0 ~ 1.0000- 0	0.9000+ 0	0.1100+ 0			0.0000+ 0	0.3554+ 0						2.0498- 9
1.0000- 0 ~ 1.0000- 0	0.9000+ 0	0.1079+ 0			0.0000+ 0	0.3413+ 0						2.0498- 9
1.0000- 0 ~ 1.0000- 0	0.9000+ 0	0.1059+ 0			0.0000+ 0	0.3280+ 0						2.0498- 9
1.0000- 0 ~ 1.0000- 0	0.9000+ 0	0.1040+ 0			0.0000+ 0	0.3154+ 0						2.0498- 9
1.0000- 0 ~ 1.0000- 0	0.9000+ 0	0.1022+ 0			0.0000+ 0	0.3034+ 0						2.0498- 9
1.0000- 0 ~ 1.0000- 0	0.9000+ 0	0.1005+ 0			0.0000+ 0	0.2919+ 0						2.0498- 9
1.0000- 0 ~ 1.0000- 0	0.9000+ 0	0.0989+ 0			0.0000+ 0	0.2808+ 0						2.0498- 9
1.0000- 0 ~ 1.0000- 0	0.9000+ 0	0.0974+ 0			0.0000+ 0	0.2700+ 0						2.0498- 9
1.0000- 0 ~ 1.0000- 0	0.9000+ 0	0.0959+ 0			0.0000+ 0	0.2594+ 0						2.0498- 9
1.0000- 0 ~ 1.0000- 0	0.9000+ 0	0.0945+ 0			0.0000+ 0	0.2490+ 0						2.0498- 9
1.0000- 0 ~ 1.0000- 0	0.9000+ 0	0.0931+ 0			0.0000+ 0	0.2388+ 0						2.0498- 9
1.0000- 0 ~ 1.0000- 0	0.9000+ 0	0.0918+ 0			0.0000+ 0	0.2288+ 0						2.0498- 9
1.0000- 0 ~ 1.0000- 0	0.9000+ 0	0.0905+ 0			0.0000+ 0	0.2189+ 0						2.0498- 9
1.0000- 0 ~ 1.0000- 0	0.9000+ 0	0.0892+ 0			0.0000+ 0	0.2092+ 0						2.0498- 9
1.0000- 0 ~ 1.0000- 0	0.9000+ 0	0.0880+ 0			0.0000+ 0	0.2000+ 0						2.0498- 9
1.0000- 0 ~ 1.0000- 0	0.9000+ 0	0.0868+ 0			0.0000+ 0	0.1910+ 0						2.0498- 9
1.0000- 0 ~ 1.0000- 0	0.9000+ 0	0.0856+ 0			0.0000+ 0	0.1822+ 0						2.0498- 9
1.0000- 0 ~ 1.0000- 0	0.9000+ 0	0.0845+ 0			0.0000+ 0	0.1736+ 0						2.0498- 9
1.0000- 0 ~ 1.0000- 0	0.9000+ 0	0.0834+ 0			0.0000+ 0	0.1651+ 0						2.0498- 9
1.0000- 0 ~ 1.0000- 0	0.9000+ 0	0.0823+ 0			0.0000+ 0	0.1567+ 0						2.0498- 9
1.0000- 0 ~ 1.0000- 0	0.9000+ 0	0.0812+ 0			0.0000+ 0	0.1484+ 0						2.0498- 9
1.0000- 0 ~ 1.0000- 0	0.9000+ 0	0.0801+ 0			0.0000+ 0	0.1402+ 0						2.0498- 9
1.0000- 0 ~ 1.0000- 0	0.9000+ 0	0.0790+ 0			0.0000+ 0	0.1321+ 0						2.0498- 9
1.0000- 0 ~ 1.0000- 0	0.9000+ 0	0.0779+ 0			0.0000+ 0	0.1241+ 0						2.0498- 9
1.0000- 0 ~ 1.0000- 0	0.9000+ 0	0.0768+ 0			0.0000+ 0	0.1161+ 0						2.0498- 9
1.0000- 0 ~ 1.0000- 0	0.9000+ 0	0.0757+ 0			0.0000+ 0	0.1082+ 0						2.0498- 9
1.0000- 0 ~ 1.0000- 0	0.9000+ 0	0.0746+ 0			0.0000+ 0	0.1003+ 0						2.0498- 9
1.0000- 0 ~ 1.0000- 0	0.9000+ 0	0.0735+ 0			0.0000+ 0	0.0924+ 0						2.0498- 9
1.0000- 0 ~ 1.0000- 0	0.9000+ 0	0.0724+ 0			0.0000+ 0	0.0845+ 0						2.0498- 9
1.0000- 0 ~ 1.0000- 0	0.9000+ 0	0.0713+ 0			0.0000+ 0	0.0766+ 0						2.0498- 9
1.0000- 0 ~ 1.0000- 0	0.9000+ 0	0.0702+ 0			0.0000+ 0	0.0687+ 0						2.0498- 9
1.0000- 0 ~ 1.0000- 0	0.9000+ 0	0.0691+ 0			0.0000+ 0	0.0608+ 0						2.0498- 9
1.0000- 0 ~ 1.0000- 0	0.9000+ 0	0.0680+ 0			0.0000+ 0	0.0529+ 0						2.0498- 9
1.0000- 0 ~ 1.0000- 0	0.9000+ 0	0.0669+ 0			0.0000+ 0	0.0450+ 0						2.0498- 9
1.0000- 0 ~ 1.0000- 0	0.9000+ 0	0.0658+ 0			0.0000+ 0	0.0371+ 0						2.0498- 9
1.0000- 0 ~ 1.0000- 0	0.9000+ 0	0.0647+ 0			0.0000+ 0	0.0292+ 0						2.0498- 9
1.0000- 0 ~ 1.0000- 0	0.9000+ 0	0.0636+ 0			0.0000+ 0	0.0213+ 0						2.0498- 9
1.0000- 0 ~ 1.0000- 0	0.9000+ 0	0.0625+ 0			0.0000+ 0	0.0134+ 0						2.0498- 9
1.0000- 0 ~ 1.0000- 0	0.9000+ 0	0.0614+ 0			0.0000+ 0	0.0055+ 0						2.0498- 9
1.0000- 0 ~ 1.0000- 0	0.9000+ 0	0.0603+ 0			0.0000+ 0	0.0000+ 0						2.0498- 9
1.0000- 0 ~ 1.0000- 0	0.9000+ 0	0.0592+ 0			0.0000+ 0	0.0000+ 0						2.0498- 9
1.0000- 0 ~ 1.0000- 0	0.9000+ 0	0.0581+ 0			0.0000+ 0	0.0000+ 0						2.0498- 9
1.0000- 0 ~ 1.0000- 0	0.9000+ 0	0.0570+ 0			0.0000+ 0	0.0000+ 0						2.0498- 9
1.0000- 0 ~ 1.0000- 0	0.9000+ 0	0.0559+ 0			0.0000+ 0	0.0000+ 0						2.0498- 9
1.0000- 0 ~ 1.0000- 0	0.9000+ 0	0.0548+ 0			0.0000+ 0	0.0000+ 0						2.0498- 9
1.0000- 0 ~ 1.0000- 0	0.9000+ 0	0.0537+ 0			0.0000+ 0	0.0000+ 0						2.0498- 9
1.0000- 0 ~ 1.0000- 0	0.9000+ 0	0.0526+ 0			0.0000+ 0	0.0000+ 0						2.0498- 9
1.0000- 0 ~ 1.0000- 0	0.9000+ 0	0.0515+ 0			0.0000+ 0	0.0000+ 0						2.0498- 9
1.0000- 0 ~ 1.0000- 0	0.9000+ 0	0.0504+ 0			0.0000+ 0	0.0000+ 0						2.0498- 9
1.0000- 0 ~ 1.0000- 0	0.9000+ 0	0.0493+ 0			0.0000+ 0	0.0000+ 0						

CROSS SECTION

MF-237

MATERIAL	ENERGY	TOTAL	ELBATIC	INELA	(N.2N)	(N.3N)	FIBRION	(N.NP)	CAPTURE	(N.P)	(N.D)	(N.R)	KU-BRR
1.0000*	~ 1.0000-2	5.2773+ 2	2.7800+ 1			6.5861- 2		5.9881+ 2					2.8863- 9
1.0000*	1.5000-2	2.9798+ 2	2.7894+ 1			2.8771- 2		2.7026+ 2					2.8864- 9
1.0000*	2.0000-2	2.9114+ 2	2.7529+ 1			2.8771- 2		2.2365+ 2					2.8892- 9
1.0000*	3.0000-2	2.9114+ 2	2.7529+ 1			1.8665- 3		1.8430+ 1					2.9051- 9
1.0000*	4.0000-2	1.7851+ 1	1.7385+ 1			1.5970- 2		1.5091+ 1					2.9051- 9
1.0000*	5.0000-2	1.6704+ 1	1.6252+ 1			1.3683- 1		1.2708+ 1					2.9108- 9
1.0000*	6.0000-2	1.4222+ 1	1.3712+ 1			1.0687- 1		9.8678+ 1					2.9108- 9
1.0000*	8.0000-2	1.1265+ 1	1.0658+ 1			8.7849- 5		8.6355+ 1					2.9130- 9
1.0000*	1.0000-1	9.7427+ 1	2.6272+ 1			5.4994- 3		7.1148+ 1					2.9157- 9
1.0000*	1.5000-1	9.6130+ 1	2.5698+ 1			5.4994- 3		6.9574+ 1					2.9157- 9
1.0000*	2.0000-1	9.3971+ 1	2.5084+ 1			5.1079- 3		6.7348+ 1					2.9243- 9
1.0000*	3.0000-1	9.5839+ 1	2.7244+ 1			3.0676- 2		9.3681+ 2					2.9243- 9
1.0000*	4.0000-1	9.2113+ 1	2.5901+ 1			1.6828- 1		4.9653+ 1					2.9285- 9
1.0000*	5.0000-1	8.5317+ 1	2.2859+ 1			2.6435- 1		2.2338+ 1					2.9323- 9
1.0000*	6.0000-1	4.3573+ 1	2.1174+ 1			1.9058- 1		2.2338+ 1					2.9323- 9
1.0000*	1.0000-0	4.5272+ 2	1.9751+ 1			2.5798- 2		4.3293+ 2					2.9350- 9
1.0000*	2.0000-0	1.4943+ 2	2.0800+ 1			7.7641- 3		1.2852+ 2					2.9378- 9
1.0000*	3.0000-0	2.5284+ 2	1.7190+ 1			9.1482- 4		8.1528+ 0					2.9498- 9
1.0000*	4.0000-0	1.4293+ 1	1.5288+ 1			9.4718- 3		3.5648+ 1					2.9498- 9
1.0000*	5.0000-0	5.0057+ 1	1.4375+ 1			2.9644- 2		2.1181+ 2					2.9474- 9
1.0000*	6.0000-0	2.5567+ 1	1.3424+ 1			2.7842- 3		4.2167+ 1					2.9494- 9
1.0000*	8.0000-0	3.8437+ 1	1.2313+ 1			3.6355- 3		8.2880+ 1					2.9516- 9
1.0000*	1.0000-1	1.2210+ 2	1.4274+ 1			2.1392- 2		1.0782+ 2					2.9543- 9
1.0000*	2.0000-1	5.7282+ 2	1.5590+ 1			6.5782- 2		4.0956+ 2					2.9571- 9
1.0000*	3.0000-1	7.8498+ 2	1.9811+ 1			1.7444- 2		1.0246+ 2					2.9601- 9
1.0000*	4.0000-1	7.6498+ 2	1.3623+ 1			2.3778- 2		5.4443+ 1					2.9601- 9
1.0000*	5.0000-1	7.2789+ 1	1.7847+ 1			9.3616- 2		5.9813+ 1					2.9621- 9
1.0000*	6.0000-1	6.8650+ 1	1.5057+ 1			1.8257- 2		5.3205+ 1					2.9621- 9
1.0000*	8.0000-1	6.1824+ 1	1.5207+ 1			2.6255- 2		4.5831+ 1					2.9657- 9
1.0000*	1.0000-2	4.7585+ 1	1.4197+ 1			2.6484- 2		3.3824+ 1					3.0847- 9
1.0000*	2.0000-2	4.2711+ 1	1.2825+ 1			9.0009- 3		2.9877+ 1					3.0847- 9
1.0000*	3.0000-2	3.7438+ 1	1.2575+ 1			9.0009- 3		2.9877+ 1					3.0847- 9
1.0000*	4.0000-2	3.3952+ 1	1.2582+ 1			9.0007- 3		2.4016+ 1					3.0847- 9
1.0000*	5.0000-2	3.8439+ 1	1.2570+ 1			9.0007- 3		1.7733+ 1					3.0847- 9
1.0000*	6.0000-2	2.6404+ 1	1.2505+ 1			9.0008- 3		1.5864+ 1					3.0847- 9
1.0000*	8.0000-2	2.4582+ 1	1.2430+ 1			9.0008- 3		1.3970+ 1					3.0847- 9
1.0000*	1.0000-3	2.6574+ 1	1.2327+ 1			9.0009- 3		1.0238+ 1					3.0847- 9
1.0000*	2.0000-3	2.6849+ 1	1.2070+ 1			9.0009- 3		8.4340+ 0					3.0847- 9
1.0000*	3.0000-3	1.9083+ 1	1.1773+ 1			9.0009- 3		7.0040+ 0					3.0847- 9
1.0000*	4.0000-3	1.6859+ 1	1.1809+ 1			9.0009- 3		5.7922+ 0					3.0847- 9
1.0000*	5.0000-3	1.2855+ 1	1.1563+ 1			9.0009- 3		4.5740+ 0					3.0847- 9
1.0000*	6.0000-3	1.5701+ 1	1.1461+ 1			9.0004- 3		4.0888+ 0					3.0847- 9
1.0000*	8.0000-3	1.4488+ 1	1.1289+ 1			9.0007- 3		3.6307+ 0					3.0847- 9
1.0000*	1.0000-4	1.3888+ 1	1.1054+ 1			9.0007- 3		2.7854+ 0					3.0847- 9
1.0000*	2.0000-4	1.3200+ 1	1.0723+ 1			9.0011- 3		2.4652+ 0					3.0847- 9
1.0000*	3.0000-4	1.2768+ 1	1.0654+ 1			9.0011- 3		2.1798+ 0					3.0847- 9
1.0000*	4.0000-4	1.2625+ 1	1.0592+ 1			9.0011- 3		1.9299+ 0					3.0847- 9
1.0000*	5.0000-4	1.2449+ 1	1.0453+ 1			9.0011- 3		1.5539+ 0					3.0847- 9
1.0000*	6.0000-4	1.2239+ 1	1.0255+ 1			9.0011- 3		1.3366+ 0					3.0847- 9
1.0000*	8.0000-4	1.1912+ 1	9.8984+ 0			2.1502- 2		1.0570+ 0					3.0847- 9
1.0000*	1.0000-5	1.1473+ 1	9.4150+ 0			2.0015- 2		8.1978+ 0					3.0847- 9
1.0000*	2.0000-5	1.0665+ 1	9.7987+ 0			4.0890- 2		5.7022+ 0					3.0847- 9
1.0000*	3.0000-5	1.0132+ 1	9.0136+ 0			3.0224- 1		5.2265+ 0					3.0847- 9
1.0000*	4.0000-5	9.1115+ 0	6.5698+ 0			6.1471- 1		4.0198+ 0					3.0847- 9
1.0000*	5.0000-5	8.5293+ 0	5.7946+ 0			1.0480+ 0		3.1157+ 0					3.0847- 9
1.0000*	6.0000-5	7.9544+ 0	5.0825+ 0			1.3677+ 0		2.2586+ 0					3.0847- 9
1.0000*	8.0000-5	7.8580+ 0	4.1557+ 0			1.5123+ 0		1.7004+ 0					3.0847- 9
1.0000*	1.0000-6	6.8106+ 0	3.8073+ 0			1.5692+ 0		1.2423+ 0					3.0847- 9
1.0000*	2.0000-6	6.7105+ 0	3.0144+ 0			1.5692+ 0		8.2005+ 0					3.0847- 9
1.0000*	3.0000-6	7.2657+ 0	4.2827+ 0			1.5272+ 0		4.0489+ 0					3.0847- 9
1.0000*	4.0000-6	7.2633+ 0	4.4111+ 0			1.3790+ 0		1.3070+ 0					3.0847- 9
1.0000*	5.0000-6	4.5548+ 0	3.5556+ 0			1.4832+ 0		1.1732+ 0					3.0847- 9
1.0000*	6.0000-6	3.4201+ 0	3.5600+ 0			2.1151+ 0		1.6122+ 0					3.0847- 9
1.0000*	8.0000-6	5.4201+ 0	2.8750+ 0			2.0765+ 0		1.0025+ 0					3.0847- 9
1.0000*	1.0000-7	5.7466+ 0	1.6284+ 0			2.0765+ 0		8.0751+ 0					3.0847- 9
1.0000*	2.0000-7	5.7466+ 0	1.6284+ 0			2.0765+ 0		8.0751+ 0					3.0847- 9
1.0000*	3.0000-7	5.7466+ 0	1.6284+ 0			2.0765+ 0		8.0751+ 0					3.0847- 9
1.0000*	4.0000-7	5.7466+ 0	1.6284+ 0			2.0765+ 0		8.0751+ 0					3.0847- 9
1.0000*	5.0000-7	5.7466+ 0	1.6284+ 0			2.0765+ 0		8.0751+ 0					3.0847- 9
1.0000*	6.0000-7	5.7466+ 0	1.6284+ 0			2.0765+ 0		8.0751+ 0					3.0847- 9
1.0000*	8.0000-7	5.7466+ 0	1.6284+ 0			2.0765+ 0		8.0751+ 0					3.0847- 9
1.0000*	1.0000-8	5.7466+ 0	1.6284+ 0			2.0765+ 0		8.0751+ 0					3.0847- 9
1.0000*	2.0000-8	5.7466+ 0	1.6284+ 0			2.0765+ 0		8.0751+ 0					3.0847- 9
1.0000*	3.0000-8	5.7466+ 0	1.6284+ 0			2.0765+ 0		8.0751+ 0					3.0847- 9
1.0000*	4.0000-8	5.7466+ 0	1.6284+ 0			2.0765+ 0		8.0751+ 0					3.0847- 9
1.0000*	5.0000-8	5.7466+ 0	1.6284+ 0			2.0765+ 0		8.0751+ 0					3.0847- 9
1.0000*	6.0000-8	5.7466+ 0	1.6284+ 0			2.0765+ 0		8.0751+ 0					3.0847- 9
1.0000*	8.0000-8	5.7466+ 0	1.6284+ 0			2.0765+ 0		8.0751+ 0					3.0847- 9

CROSS SECTION

MP-239

MATERIAL = 2932	ENERGY	TOTAL	ELABTIC	INELR	(N.2N)	(N.3N)	F.ISSION	(N.WA)	(N.NPI)	CAPTURE	(N.P)	(N.D)	(N.A)	MU-BRR
1.0000-5	~ 1.0000-2	1.2502+ 2	1.0500+ 1				0.0000+ 0			1.1410+ 2				2.8140- 5
1.0000-4	1.5000-2	9.9583+ 1	1.0500+ 1				0.0000+ 0			5.2955+ 1				2.8142- 5
1.0000-3	2.0000-2	5.2385+ 1	1.0500+ 1				0.0000+ 0			4.4834+ 1				2.8143- 5
2.0000-2	3.0000-2	4.8016+ 1	1.0500+ 1				0.0000+ 0			3.7420+ 1				2.8144- 5
3.0000-2	4.0000-2	4.2200+ 1	1.0500+ 1				0.0000+ 0			3.1524+ 1				2.8145- 5
4.0000-2	5.0000-2	3.8350+ 1	1.0500+ 1				0.0000+ 0			2.6971+ 1				2.8146- 5
5.0000-2	6.0000-2	3.5950+ 1	1.0500+ 1				0.0000+ 0			2.2886+ 1				2.8147- 5
6.0000-2	7.0000-2	3.4200+ 1	1.0500+ 1				0.0000+ 0			1.9839+ 1				2.8148- 5
1.0000-1	1.5000-1	2.7400+ 1	1.0500+ 1				0.0000+ 0			1.6728+ 1				2.8149- 5
1.5000-1	2.0000-1	2.4700+ 1	1.0500+ 1				0.0000+ 0			1.4122+ 1				2.8150- 5
2.0000-1	3.0000-1	2.0500+ 1	1.0500+ 1				0.0000+ 0			9.9502+ 0				2.8151- 5
3.0000-1	4.0000-1	1.8300+ 1	1.0500+ 1				0.0000+ 0			8.7719+ 0				2.8152- 5
4.0000-1	5.0000-1	1.6450+ 1	1.0500+ 1				0.0000+ 0			7.8348+ 0				2.8153- 5
5.0000-1	6.0000-1	1.4750+ 1	1.0500+ 1				0.0000+ 0			6.7905+ 0				2.8154- 5
6.0000-1	7.0000-1	1.3200+ 1	1.0500+ 1				0.0000+ 0			5.7305+ 0				2.8155- 5
7.0000-1	8.0000-1	1.1800+ 1	1.0500+ 1				0.0000+ 0			4.6505+ 0				2.8156- 5
8.0000-1	9.0000-1	1.0500+ 1	1.0500+ 1				0.0000+ 0			3.5655+ 0				2.8157- 5
1.0000-0	1.0000-0	1.6850+ 1	1.0500+ 1				0.0000+ 0			5.2941+ 0				2.8158- 5
1.5000-0	2.0000-0	1.5000+ 1	1.0500+ 1				0.0000+ 0			4.4790+ 0				2.8159- 5
2.0000-0	3.0000-0	1.3400+ 1	1.0500+ 1				0.0000+ 0			3.7394+ 0				2.8160- 5
3.0000-0	4.0000-0	1.2050+ 1	1.0500+ 1				0.0000+ 0			3.1304+ 0				2.8161- 5
4.0000-0	5.0000-0	1.0900+ 1	1.0500+ 1				0.0000+ 0			2.6536+ 0				2.8162- 5
5.0000-0	6.0000-0	0.9950+ 1	1.0500+ 1				0.0000+ 0			2.2856+ 0				2.8163- 5
6.0000-0	7.0000-0	0.9174+ 2	1.0500+ 1				0.0000+ 0			1.9485+ 0				2.8164- 5
7.0000-0	8.0000-0	0.8527+ 2	1.0500+ 1				0.0000+ 0			1.6485+ 0				2.8165- 5
8.0000-0	9.0000-0	0.7971+ 2	1.0500+ 1				0.0000+ 0			1.3867+ 0				2.8166- 5
1.0000+ 1	1.5000+ 1	1.4408+ 2	1.0500+ 1				0.0000+ 0			1.0426+ 0				2.8244- 5
1.5000+ 1	2.0000+ 1	1.2493+ 2	1.0500+ 1				0.0000+ 0			0.7745+ 0				2.8245- 5
2.0000+ 1	3.0000+ 1	1.0482+ 2	1.0500+ 1				0.0000+ 0			0.5720+ 0				2.8246- 5
3.0000+ 1	4.0000+ 1	0.8668+ 1	1.0500+ 1				0.0000+ 0			0.4091+ 0				2.8247- 5
4.0000+ 1	5.0000+ 1	0.7117+ 1	1.0500+ 1				0.0000+ 0			0.2972+ 0				2.8248- 5
5.0000+ 1	6.0000+ 1	0.6112+ 1	1.0500+ 1				0.0000+ 0			0.2126+ 0				2.8249- 5
6.0000+ 1	7.0000+ 1	0.5385+ 1	1.0500+ 1				0.0000+ 0			0.1578+ 0				2.8250- 5
7.0000+ 1	8.0000+ 1	0.4823+ 1	1.0500+ 1				0.0000+ 0			0.1126+ 0				2.8251- 5
8.0000+ 1	9.0000+ 1	0.4373+ 1	1.0500+ 1				0.0000+ 0			0.0856+ 0				2.8252- 5
1.0000+ 2	1.5000+ 2	5.2104+ 1	1.0500+ 1				0.0000+ 0			3.0885+ 1				2.8253- 5
1.5000+ 2	2.0000+ 2	4.5439+ 1	1.0500+ 1				0.0000+ 0			2.7427+ 1				2.8254- 5
2.0000+ 2	3.0000+ 2	3.9702+ 1	1.0500+ 1				0.0000+ 0			2.4581+ 1				2.8255- 5
3.0000+ 2	4.0000+ 2	3.5102+ 1	1.0500+ 1				0.0000+ 0			2.2332+ 1				2.8256- 5
4.0000+ 2	5.0000+ 2	3.1702+ 1	1.0500+ 1				0.0000+ 0			2.0588+ 1				2.8257- 5
5.0000+ 2	6.0000+ 2	2.9466+ 1	1.0500+ 1				0.0000+ 0			1.8611+ 1				2.8258- 5
6.0000+ 2	7.0000+ 2	2.7919+ 1	1.0500+ 1				0.0000+ 0			1.6924+ 1				2.8259- 5
7.0000+ 2	8.0000+ 2	2.6557+ 1	1.0500+ 1				0.0000+ 0			1.5456+ 1				2.8260- 5
1.0000+ 3	1.5000+ 3	2.3284+ 1	1.0500+ 1				0.0000+ 0			1.2967+ 1				2.8261- 5
1.5000+ 3	2.0000+ 3	2.1243+ 1	1.0500+ 1				0.0000+ 0			1.0996+ 1				2.8262- 5
2.0000+ 3	3.0000+ 3	1.9502+ 1	1.0500+ 1				0.0000+ 0			0.9706+ 1				2.8263- 5
3.0000+ 3	4.0000+ 3	1.8090+ 1	1.0500+ 1				0.0000+ 0			0.8508+ 1				2.8264- 5
4.0000+ 3	5.0000+ 3	1.6821+ 1	1.0500+ 1				0.0000+ 0			0.7505+ 1				2.8265- 5
5.0000+ 3	6.0000+ 3	1.5721+ 1	1.0500+ 1				0.0000+ 0			0.6687+ 1				2.8266- 5
6.0000+ 3	7.0000+ 3	1.4838+ 1	1.0500+ 1				0.0000+ 0			0.6017+ 1				2.8267- 5
7.0000+ 3	8.0000+ 3	1.4138+ 1	1.0500+ 1				0.0000+ 0			0.5473+ 1				2.8268- 5
1.0000+ 4	1.5000+ 4	1.1798+ 1	1.0500+ 1				0.0000+ 0			0.4997+ 1				2.8269- 5
1.5000+ 4	2.0000+ 4	1.0723+ 1	1.0500+ 1				0.0000+ 0			0.4574+ 1				2.8270- 5
2.0000+ 4	3.0000+ 4	0.9835+ 1	1.0500+ 1				0.0000+ 0			0.4200+ 1				2.8271- 5
3.0000+ 4	4.0000+ 4	0.9019+ 1	1.0500+ 1				0.0000+ 0			0.3873+ 1				2.8272- 5
4.0000+ 4	5.0000+ 4	0.8311+ 1	1.0500+ 1				0.0000+ 0			0.3592+ 1				2.8273- 5
5.0000+ 4	6.0000+ 4	0.7715+ 1	1.0500+ 1				0.0000+ 0			0.3353+ 1				2.8274- 5
6.0000+ 4	7.0000+ 4	0.7235+ 1	1.0500+ 1				0.0000+ 0			0.3151+ 1				2.8275- 5
7.0000+ 4	8.0000+ 4	0.6853+ 1	1.0500+ 1				0.0000+ 0			0.2984+ 1				2.8276- 5
1.0000+ 5	1.5000+ 5	1.2345+ 1	1.0500+ 1				0.0000+ 0			0.8577+ 1				2.8277- 5
1.5000+ 5	2.0000+ 5	1.1393+ 1	1.0500+ 1				0.0000+ 0			0.7502+ 1				2.8278- 5
2.0000+ 5	3.0000+ 5	1.0598+ 1	1.0500+ 1				0.0000+ 0			0.6599+ 1				2.8279- 5
3.0000+ 5	4.0000+ 5	0.9928+ 1	1.0500+ 1				0.0000+ 0			0.5844+ 1				2.8280- 5
4.0000+ 5	5.0000+ 5	0.9382+ 1	1.0500+ 1				0.0000+ 0			0.5217+ 1				2.8281- 5
5.0000+ 5	6.0000+ 5	0.8855+ 1	1.0500+ 1				0.0000+ 0			0.4715+ 1				2.8282- 5
6.0000+ 5	7.0000+ 5	0.8356+ 1	1.0500+ 1				0.0000+ 0			0.4317+ 1				2.8283- 5
7.0000+ 5	8.0000+ 5	0.7890+ 1	1.0500+ 1				0.0000+ 0			0.3976+ 1				2.8284- 5
1.0000+ 6	1.5000+ 6	0.7458+ 1	1.0500+ 1				0.0000+ 0			0.3683+ 1				2.8285- 5
1.5000+ 6	2.0000+ 6	0.7051+ 1	1.0500+ 1				0.0000+ 0			0.3430+ 1				2.8286- 5
2.0000+ 6	3.0000+ 6	0.6672+ 1	1.0500+ 1				0.0000+ 0			0.3215+ 1				2.8287- 5
3.0000+ 6	4.0000+ 6	0.6325+ 1	1.0500+ 1				0.0000+ 0			0.3032+ 1				2.8288- 5
4.0000+ 6	5.0000+ 6	0.6005+ 1	1.0500+ 1				0.0000+ 0			0.2879+ 1				2.8289- 5
5.0000+ 6	6.0000+ 6	0.5714+ 1	1.0500+ 1				0.0000+ 0			0.2747+ 1				2.8290- 5
6.0000+ 6	7.0000+ 6	0.5450+ 1	1.0500+ 1				0.0000+ 0			0.2633+ 1				2.8291- 5
7.0000+ 6	8.0000+ 6	0.5210+ 1	1.0500+ 1				0.0000+ 0			0.2534+ 1				2.8292- 5
1.0000+ 7	1.5000+ 7	0.5643+ 1	1.0500+ 1				0.0000+ 0			0.8597+ 1				2.8293- 5
1.5000+ 7	2.0000+ 7	0.5445+ 1	1.0500+ 1				0.0000+ 0			0.7934+ 1				2.8294- 5
2.0000+ 7	3.0000+ 7	0.5269+ 1	1.0500+ 1				0.0000+ 0			0.7369+ 1				2.8295- 5
3.0000+ 7	4.0000+ 7	0.5112+ 1	1.0500+ 1				0.0000+ 0			0.6897+ 1				2.8296- 5
4.0000+ 7	5.0000+ 7	0.4971+ 1	1.0500+ 1				0.0000+ 0			0.6505+ 1				2.8297- 5

PU-236

CROSS SECTION

MATERIAL = 2941

ENERGY	TOTAL	ELASTIC	INELR	(M,2N)	(M,3N)	Fission	(M,NR)	(M,HP)	CAPTURE	(M,P)	(M,D)	(M,R)	MU-BR
1.0000- 5 ~ 1.0000- 2	2.5249+ 3	3.8550+ 0				1.8292+ 2			2.1383+ 3				2.8488- 3
1.0000- 4	1.1659+ 3	3.5400+ 0				8.8446+ 1			9.8996+ 3				2.8488- 3
1.0000- 3	9.4371+ 0	3.3781+ 0				7.6120+ 1			8.7470+ 1				2.8488- 3
2.0000- 2	8.4435+ 0	3.2463+ 0				6.6770+ 1			7.7470+ 1				2.8488- 3
3.0000- 2	7.4550+ 0	3.2463+ 0				5.6891+ 1			6.8377+ 1				2.8488- 3
4.0000- 2	6.9230+ 0	3.1083+ 0				5.2529+ 1			6.4026+ 1				2.8488- 3
5.0000- 2	6.5885+ 0	2.9588+ 0				4.8168+ 1			5.9748+ 1				2.8488- 3
6.0000- 2	6.2074+ 0	2.4463+ 0				4.3822+ 1			5.5474+ 1				2.8488- 3
1.0000- 1	6.4869+ 2	1.8637+ 0				5.0893+ 1			5.7588+ 1				2.8488- 3
1.5000- 1	7.6827+ 2	1.0511+ 0				6.0558+ 1			6.7263+ 1				2.8488- 3
2.0000- 1	9.3568+ 2	1.1571+ 0				7.1766+ 1			7.8451+ 1				2.8488- 3
3.0000- 1	1.1637+ 3	2.2562+ 2				4.1796+ 2			4.8481+ 2				2.8488- 3
4.0000- 1	3.6573+ 3	4.2562+ 2				2.7638+ 2			3.2193+ 4				2.8488- 3
5.0000- 1	3.6573+ 3	9.7072+ 3				2.7346+ 2			3.1967+ 3				2.8488- 3
6.0000- 1	5.4897+ 2	2.6183+ 1				4.0466+ 1			4.7222+ 2				2.8488- 3
8.0000- 1	1.4903+ 2	2.2677+ 1				3.5144+ 0			4.1822+ 1				2.8488- 3
1.0000- 0	5.4112+ 1	1.7448+ 1				2.8891+ 0			3.3774+ 1				2.8488- 3
1.5000- 0	2.5727+ 1	1.4621+ 1				8.5943+ 1			1.0047+ 1				2.8488- 3
2.0000- 0	1.7267+ 1	1.3478+ 1				9.0014+ 1			3.5885+ 0				2.8488- 3
3.0000- 0	1.4097+ 1	1.2701+ 1				9.0014+ 1			3.5885+ 0				2.8488- 3
4.0000- 0	1.2569+ 1	1.2373+ 1				5.0832+ 2			1.5281+ 1				2.8488- 3
5.0000- 0	1.2569+ 1	1.2373+ 1				3.1201+ 2			3.6481+ 1				2.8488- 3
6.0000- 0	1.9535+ 2	3.2544+ 1				1.2504+ 1			1.5005+ 2				2.8488- 3
8.0000- 0	1.7366+ 2	3.2231+ 1				1.0865+ 1			1.3043+ 3				2.8488- 3
1.0000- 1	1.4884+ 2	3.1848+ 1				1.1892+ 0			1.0894+ 2				2.8488- 3
1.5000- 1	1.7697+ 2	3.0720+ 1				7.1544+ 1			8.2759+ 1				2.8488- 3
2.0000- 1	1.6877+ 2	2.9466+ 1				7.3268+ 1			8.4575+ 1				2.8488- 3
3.0000- 1	9.4576+ 1	2.8466+ 1				5.0687+ 0			6.1610+ 1				2.8488- 3
4.0000- 1	8.4867+ 1	2.8872+ 1				5.0687+ 0			6.1610+ 1				2.8488- 3
5.0000- 1	7.7873+ 1	2.8573+ 1				3.8671+ 0			4.9541+ 1				2.8488- 3
6.0000- 1	6.9657+ 1	2.8272+ 1				2.8652+ 0			3.3922+ 1				2.8488- 3
8.0000- 1	6.9831+ 1	2.7123+ 1				2.7852+ 0			3.3922+ 1				2.8488- 3
1.0000- 2	6.3116+ 1	2.6266+ 1				2.3444+ 0			2.7655+ 1				2.8488- 3
1.5000- 2	4.9515+ 1	2.4401+ 1				1.8874+ 0			2.2745+ 1				2.8488- 3
2.0000- 2	4.5855+ 1	2.4401+ 1				1.8874+ 0			2.2745+ 1				2.8488- 3
3.0000- 2	3.6773+ 1	2.2811+ 1				1.2016+ 0			1.4118+ 1				2.8488- 3
4.0000- 2	3.3555+ 1	2.2811+ 1				1.0154+ 0			1.1934+ 1				2.8488- 3
5.0000- 2	3.1302+ 1	2.2811+ 1				8.8711+ 0			1.0418+ 1				2.8488- 3
6.0000- 2	2.9133+ 1	2.1023+ 1				7.5605+ 1			8.8883+ 0				2.8488- 3
8.0000- 2	2.8133+ 1	2.1023+ 1				6.3742+ 1			8.8883+ 0				2.8488- 3
1.0000- 3	2.6770+ 1	2.0223+ 1				5.1431+ 1			6.0070+ 0				4.3458- 3
1.5000- 3	2.4618+ 1	1.9423+ 1				4.1026+ 1			4.7739+ 0				6.0162- 3
2.0000- 3	2.2772+ 1	1.8633+ 1				3.2823+ 1			3.7973+ 0				6.1104- 3
3.0000- 3	2.1272+ 1	1.7903+ 1				2.6950+ 0			3.0693+ 0				6.0653- 3
4.0000- 3	2.0273+ 1	1.7392+ 1				2.0633+ 0			2.3950+ 0				1.0604- 3
5.0000- 3	1.8867+ 1	1.6564+ 1				1.8570+ 0			1.8976+ 0				1.3023- 3
6.0000- 3	1.8145+ 1	1.6111+ 1				1.6739+ 1			1.8653+ 0				1.6206- 3
1.0000- 4	1.7391+ 1	1.5878+ 1				1.5451+ 1			1.6432+ 0				2.2851- 3
1.5000- 4	1.6641+ 1	1.5243+ 1				1.3071+ 1			1.4793+ 0				2.2851- 3
2.0000- 4	1.5939+ 1	1.4645+ 1				1.2726+ 1			1.4160+ 0				2.2851- 3
3.0000- 4	1.4878+ 1	1.3683+ 1				1.2840+ 1			1.0593+ 0				6.8128- 3
4.0000- 4	1.4528+ 1	1.3367+ 1				1.3172+ 1			9.8573+ 1				7.3083- 3
5.0000- 4	1.4087+ 1	1.2940+ 1				1.3261+ 1			9.8573+ 1				8.0792- 3
6.0000- 4	1.3595+ 1	1.2436+ 1				1.3201+ 1			9.7223+ 1				1.3379- 3
1.0000- 5	1.2892+ 1	1.1820+ 1				1.8652+ 1			6.1282+ 1				1.7407- 3
1.5000- 5	1.2040+ 1	1.0748+ 1				2.3759+ 1			5.2022+ 1				2.1949- 3
2.0000- 5	1.1113+ 1	9.7148+ 0				3.4115+ 1			3.9520+ 1				2.1949- 3
3.0000- 5	1.0174+ 1	9.5885+ 0				7.6653+ 1			3.9520+ 1				2.1949- 3
4.0000- 5	9.8033+ 0	6.9371+ 1				1.1018+ 0			3.0193+ 1				2.1949- 3
5.0000- 5	8.4040+ 0	6.8181+ 0				1.5481+ 1			2.4115+ 1				4.4931- 3
6.0000- 5	7.9185+ 0	5.4486+ 1				1.5717+ 0			1.5644+ 1				4.6340- 3
1.0000- 6	7.4152+ 0	5.0438+ 0				2.4700+ 0			1.1444+ 1				5.3585- 3
1.5000- 6	6.9242+ 0	5.2064+ 0				6.6051+ 1			8.6051+ 1				5.9410- 3
2.0000- 6	6.4322+ 0	4.9196+ 0				2.5286+ 0			5.4481+ 1				7.7087- 3
3.0000- 6	6.3708+ 0	4.0282+ 0				2.5839+ 0			3.6371+ 1				8.2749- 3
4.0000- 6	6.1655+ 0	5.0185+ 0				4.5973+ 0			3.9746+ 1				8.1917- 3
5.0000- 6	6.0600+ 0	4.6595+ 0				4.5973+ 0			3.9746+ 1				8.1160- 3
6.0000- 6	6.0600+ 0	3.4754+ 0				3.0204+ 0			2.2395+ 3				8.1160- 3
1.0000- 7	6.4110+ 0	3.3447+ 0				3.0070+ 0			1.7394+ 4				8.0833- 3
1.5000- 7	6.8933+ 0	3.8816+ 0				3.0860+ 0			1.5231+ 6				8.0833- 3

CROSS SECTION

PU-238

MATERIAL	ENERGY	TOTAL	ELABTIC	INELR	(N.2N)	(N.3N)	(N.MR)	(N.NP)	(N.P)	(N.D)	(N.R)	MU-BAR
1.0000+	5-1.0000-2	1.6692+ 3	2.8147+ 1			5.6697+ 1		1.6834+ 5				2.8274- 5
1.0000+	1.5000-2	9.9099+ 3	2.7998+ 1			2.8299+ 1		9.3771+ 2				2.8299- 5
1.0000+	2.0000-2	7.3959+ 3	2.7803+ 1			2.7803+ 1		8.5670+ 2				2.8299- 5
3.0000+	2.0000-2	5.9014+ 3	2.7357+ 1			1.1560+ 1		5.9014+ 3				2.8299- 5
4.0000+	5.0000-2	4.1810+ 2	2.7118+ 1			1.1499+ 1		3.7951+ 2				2.8299- 5
5.0000+	2.0000-2	3.6479+ 2	2.6892+ 1			9.3219+ 0		3.2798+ 2				2.8299- 5
6.0000+	1.0000-2	3.0609+ 2	2.6571+ 1			8.7324+ 0		2.7284+ 2				2.8299- 5
1.0000+	1.5000-1	1.9685+ 2	2.6566+ 1			5.0656+ 0		1.6622+ 2				2.8299- 5
1.5000+	2.0000-1	1.4551+ 2	2.4818+ 1			3.5899+ 0		1.1710+ 2				2.8299- 5
2.0000+	1.0000-1	1.0452+ 2	2.3993+ 1			2.4186+ 1		7.8164+ 1				2.8299- 5
3.0000+	4.0000-1	7.4849+ 1	2.3019+ 1			1.0743+ 0		3.4258+ 1				2.8299- 5
4.0000+	1.0000-1	5.8129+ 1	2.1759+ 1			6.2791+ 1		2.6532+ 1				2.8299- 5
5.0000+	1.0000-1	5.8129+ 1	2.1759+ 1			5.8406+ 1		1.1556+ 1				2.8299- 5
6.0000+	1.0000-1	3.2401+ 1	2.1134+ 1			3.9778+ 1		1.1515+ 1				2.8299- 5
1.0000+	1.5000-0	2.5771+ 1	1.9710+ 1			2.4985+ 1		6.8108+ 0				2.8301- 5
2.0000+	2.0000-0	1.9655+ 2	1.8055+ 1			2.8128+ 1		4.1458+ 0				2.8301- 5
3.0000+	4.0000-0	2.4356+ 2	1.6679+ 1			2.2034+ 0		9.8693+ 0				2.8301- 5
4.0000+	6.0000-0	1.8721+ 1	1.7718+ 1			1.8223+ 0		6.4968+ 0				2.8301- 5
5.0000+	6.0000-0	1.7965+ 1	1.7300+ 1			5.7022+ 2		9.4519+ 1				2.8301- 5
6.0000+	1.0000-0	1.7322+ 1	1.6514+ 1			4.8558+ 1		4.6276+ 1				2.8301- 5
1.0000+	1.5000+ 1	4.8422+ 1	1.5951+ 1			5.8498+ 0		2.8824+ 1				2.8301- 5
1.0000+	1.5000+ 1	2.0589+ 1	1.6153+ 1			7.6762+ 1		3.6891+ 0				2.8301- 5
1.5000+	2.0000+ 1	1.8073+ 2	3.0938+ 0			6.7483+ 0		1.4394+ 2				2.8301- 5
2.0000+	3.0000+ 1	1.7367+ 1	1.5731+ 1			2.7075+ 2		1.1017+ 0				2.8301- 5
3.0000+	5.0000+ 1	1.5201+ 1	1.5156+ 1			1.3571+ 2		3.1967+ 0				2.8301- 5
5.0000+	6.0000+ 1	2.3107+ 1	1.4598+ 1			1.7780+ 1		8.3313+ 0				2.8301- 5
6.0000+	1.0000+ 2	2.1351+ 1	1.4088+ 1			1.2927+ 0		5.9886+ 0				2.8301- 5
1.0000+	1.5000+ 2	8.6591+ 1	3.2988+ 1			3.1717+ 0		3.0433+ 1				2.8301- 5
1.5000+	2.0000+ 1	7.0730+ 1	3.5202+ 1			4.4768+ 0		3.1051+ 1				2.8321- 5
2.0000+	3.0000+ 1	7.4455+ 1	4.0390+ 0			9.7704+ 0		2.4296+ 1				2.8321- 5
3.0000+	4.0000+ 1	5.6491+ 1	4.2382+ 1			9.9713+ 0		1.0532+ 1				2.8321- 5
4.0000+	5.0000+ 1	4.6017+ 1	3.2733+ 1			4.8165+ 0		8.6936+ 0				2.8321- 5
5.0000+	6.0000+ 1	3.2437+ 1	2.9572+ 1			1.2519+ 0		9.0293+ 0				2.8321- 5
6.0000+	1.0000+ 2	3.2181+ 1	2.3578+ 1			2.7630+ 0		7.6684+ 0				2.8321- 5
1.0000+	1.5000+ 3	2.8910+ 1	2.455+ 1			1.3449+ 0		5.1069+ 0				2.8321- 5
1.5000+	2.0000+ 3	2.5635+ 1	2.0029+ 1			1.6456+ 0		4.0369+ 0				2.8321- 5
2.0000+	3.0000+ 3	2.3066+ 1	1.8756+ 1			1.1001+ 0		3.2011+ 0				2.8321- 5
3.0000+	4.0000+ 3	2.1895+ 1	1.8725+ 1			9.1245+ 1		2.6003+ 0				2.8321- 5
4.0000+	5.0000+ 3	2.1589+ 1	1.6247+ 1			1.2989+ 0		2.2588+ 0				2.8321- 5
5.0000+	6.0000+ 3	2.0816+ 1	1.7153+ 1			1.9922+ 1		2.832+ 0				2.8321- 5
6.0000+	1.0000+ 4	1.9609+ 1	1.7153+ 1			1.7922+ 1		1.6311+ 0				2.8321- 5
1.0000+	4.0000+ 4	1.8645+ 1	1.6588+ 1			8.0923+ 1		1.4480+ 0				2.8321- 5
1.5000+	5.0000+ 4	1.8110+ 1	1.6011+ 1			8.1622+ 1		1.2829+ 0				2.8321- 5
2.0000+	6.0000+ 4	1.7421+ 1	1.5467+ 1			8.1559+ 1		1.0077+ 0				2.8321- 5
3.0000+	7.0000+ 4	1.6761+ 1	1.4956+ 1			8.3277+ 1		1.0077+ 0				2.8321- 5
4.0000+	8.0000+ 4	1.6178+ 1	1.4436+ 1			6.3436+ 1		9.0786+ 0				2.8321- 5
5.0000+	9.0000+ 4	1.5784+ 1	1.4236+ 1			6.1022+ 1		8.0340+ 1				2.8321- 5
6.0000+	1.0000+ 5	1.5308+ 1	1.3768+ 1			6.1022+ 1		6.8247+ 1				2.8321- 5
8.0000+	1.0000+ 5	1.4786+ 1	1.3206+ 1			6.0749+ 1		5.8142+ 1				2.8321- 5
1.0000+	5.0000+ 5	1.4102+ 1	1.2498+ 1			6.3773+ 1		4.8371+ 1				2.8321- 5
1.5000+	6.0000+ 5	1.3557+ 1	1.1517+ 1			7.1940+ 1		3.7369+ 1				2.8321- 5
2.0000+	7.0000+ 5	1.2924+ 1	1.0465+ 1			8.8366+ 1		3.7369+ 1				2.8321- 5
3.0000+	8.0000+ 5	1.1733+ 1	9.3803+ 0			1.0756+ 0		3.2733+ 1				2.8321- 5
4.0000+	9.0000+ 5	1.1195+ 1	9.5586+ 0			1.2964+ 0		3.8104+ 1				2.8321- 5
5.0000+	1.0000+ 6	1.0664+ 1	7.1191+ 0			2.0877+ 0		3.8104+ 1				2.8321- 5
6.0000+	2.0000+ 6	1.0127+ 1	6.4241+ 0			2.0877+ 0		3.8104+ 1				2.8321- 5
1.0000+	8.0000+ 6	1.0200+ 1	5.7418+ 0			2.1577+ 0		3.8104+ 1				2.8321- 5
1.5000+	9.0000+ 6	1.0524+ 1	5.4499+ 0			2.3957+ 0		3.8104+ 1				2.8321- 5
3.0000+	6.0000+ 6	1.0591+ 1	5.1622+ 0			2.3677+ 0		1.2317+ 1				2.8321- 5
4.0000+	7.0000+ 6	1.0826+ 1	5.0630+ 0			2.1861+ 0		1.9512+ 1				2.8321- 5
5.0000+	8.0000+ 6	1.0301+ 1	4.6699+ 0			2.2571+ 0		2.4464+ 1				2.8321- 5
6.0000+	9.0000+ 6	1.0161+ 1	4.5997+ 0			2.9537+ 0		2.4464+ 1				2.8321- 5
1.0000+	7.0000+ 7	9.9656+ 0	3.4590+ 0			2.7279+ 0		1.1790+ 1				2.8321- 5
1.5000+	8.0000+ 7	1.0624+ 1	3.4095+ 0			2.7153+ 0		1.1694+ 1				2.8321- 5

PU-239

CROSS SECTION

MATERIAL = 2943

ENERGY	TOTAL	ELASTIC	INELR	(N.2N)	(N.3N)	(N.NP)	(N.P)	(N.D)	(N.R)	MU-BAR
1.0000-5	3.0848+3	8.1088+0			2.3530+3	7.5383+2	5.1581-3			3.2024
1.0000-4	1.4891+3	0.0891+0			1.0471+3	3.3827+2	3.2024			2.5924
1.0000-3	1.2058+3	0.0000+0			3.2500+3	3.2500+3	2.5924			2.4400
1.0000-2	8.2968+3	7.2439+0			6.4780+3	4.410+2	2.5924			2.2580
1.0000-1	8.1344+3	7.6811+0			5.7700+3	2.222+2	2.222+2			2.1370+2
1.0000-0	7.6154+3	7.6145+0			5.3400+3	2.222+2	2.222+2			2.0880
1.0000+1	7.1862+3	7.7082+0			4.9538+3	2.222+2	2.222+2			2.0300
1.0000+2	7.0531+3	7.6420+0			4.7340+3	2.222+2	2.222+2			1.9700
1.0000+3	7.8556+3	7.1892+0			4.9010+3	2.222+2	2.222+2			1.9100
1.0000+4	7.0597+3	6.5536+0			4.5167+3	2.222+2	2.222+2			1.8500
1.0000+5	3.2000+3	3.2000+0			1.9890+3	2.222+2	2.222+2			1.7900
1.0000+6	1.8340+3	1.8340+0			1.6717+3	2.222+2	2.222+2			1.7300
1.0000+7	1.2232+3	1.1074+0			1.4565+3	2.222+2	2.222+2			1.6700
1.0000+8	1.0000+3	1.0574+0			1.3673+3	2.222+2	2.222+2			1.6100
1.0000+9	1.0000+3	1.0068+0			1.4417+3	2.222+2	2.222+2			1.5500
1.0000+10	4.3572+3	1.0068+0			1.7935+3	2.222+2	2.222+2			1.4900
1.0000+11	4.4878+3	6.4170+0			1.9700+3	2.222+2	2.222+2			1.4300
1.0000+12	2.1154+3	9.1245+0			1.1165+3	2.222+2	2.222+2			1.3700
1.0000+13	1.8621+3	1.9626+0			9.6740+0	2.222+2	2.222+2			1.3100
1.0000+14	1.8621+3	8.4922+0			8.3600+0	2.222+2	2.222+2			1.2500
1.0000+15	2.5548+3	6.5703+0			1.0930+3	2.222+2	2.222+2			1.1900
1.0000+16	2.5548+3	1.0623+1			1.4417+3	2.222+2	2.222+2			1.1300
1.0000+17	9.8870+3	1.0670+0			5.2590+3	2.222+2	2.222+2			1.0700
1.0000+18	6.5872+3	9.8276+0			3.0574+3	2.222+2	2.222+2			1.0100
1.0000+19	1.1700+3	1.4439+0			2.8824+3	2.222+2	2.222+2			9.5000
1.0000+20	1.0684+3	1.8787+0			1.9787+3	2.222+2	2.222+2			8.9900
1.0000+21	1.0684+3	1.6879+0			2.9166+3	2.222+2	2.222+2			8.4800
1.0000+22	1.9773+3	1.6814+0			5.9510+3	2.222+2	2.222+2			7.9700
1.0000+23	5.4583+3	1.3780+0			2.0277+3	2.222+2	2.222+2			7.4600
1.0000+24	4.5833+3	1.4476+0			1.7076+3	2.222+2	2.222+2			6.9500
1.0000+25	4.9711+3	1.9944+0			1.5976+3	2.222+2	2.222+2			6.4400
1.0000+26	2.5060+3	1.3233+0			1.2168+3	2.222+2	2.222+2			5.9300
1.0000+27	2.5060+3	1.3233+0			1.5690+3	2.222+2	2.222+2			5.4200
1.0000+28	2.5060+3	1.3934+0			1.4931+3	2.222+2	2.222+2			4.9100
1.0000+29	2.5060+3	1.3934+0			6.3657+3	2.222+2	2.222+2			4.4000
1.0000+30	2.3889+3	1.9854+0			5.2654+3	2.222+2	2.222+2			3.8900
1.0000+31	2.0000+3	1.3865+0			3.2654+3	2.222+2	2.222+2			3.3800
1.0000+32	1.8677+3	1.3130+0			3.3100+3	2.222+2	2.222+2			2.8700
1.0000+33	1.7981+3	1.7981+0			2.0533+3	2.222+2	2.222+2			2.3600
1.0000+34	1.7107+3	1.5950+0			2.4370+3	2.222+2	2.222+2			1.8500
1.0000+35	1.5822+3	1.7331+0			2.2740+3	2.222+2	2.222+2			1.3400
1.0000+36	1.5822+3	1.8911+0			2.1107+3	2.222+2	2.222+2			8.0000
1.0000+37	1.4627+3	1.1525+0			1.8706+3	2.222+2	2.222+2			7.4900
1.0000+38	1.4079+3	1.1323+0			1.7804+3	2.222+2	2.222+2			6.9800
1.0000+39	1.3828+3	1.0921+0			1.7020+3	2.222+2	2.222+2			6.4700
1.0000+40	1.3265+3	1.0300+0			1.6200+3	2.222+2	2.222+2			5.9600
1.0000+41	1.0752+3	1.0752+0			1.5382+3	2.222+2	2.222+2			5.4500
1.0000+42	1.2973+3	1.0752+0			1.4564+3	2.222+2	2.222+2			4.9400
1.0000+43	1.2619+3	1.0407+0			1.3746+3	2.222+2	2.222+2			4.4300
1.0000+44	1.2619+3	1.0047+0			1.2928+3	2.222+2	2.222+2			3.9200
1.0000+45	1.1546+3	0.8743+0			1.2110+3	2.222+2	2.222+2			3.4100
1.0000+46	1.0186+3	0.7785+0			1.1292+3	2.222+2	2.222+2			2.9000
1.0000+47	9.3146+3	6.9573+0			1.0474+3	2.222+2	2.222+2			2.3900
1.0000+48	8.6862+3	6.3278+0			0.9656+3	2.222+2	2.222+2			1.8800
1.0000+49	7.5967+3	5.6504+0			0.8838+3	2.222+2	2.222+2			1.3700
1.0000+50	7.1125+3	4.2000+0			0.8020+3	2.222+2	2.222+2			8.0000
1.0000+51	6.8935+3	3.5517+0			0.7202+3	2.222+2	2.222+2			7.4900
1.0000+52	6.7006+3	3.2711+0			0.6384+3	2.222+2	2.222+2			6.9800
1.0000+53	7.7806+3	4.2818+0			0.5566+3	2.222+2	2.222+2			6.4700
1.0000+54	7.7743+3	4.2663+0			0.4748+3	2.222+2	2.222+2			5.9600
1.0000+55	6.5000+3	3.9488+0			0.3930+3	2.222+2	2.222+2			5.4500
1.0000+56	6.7606+3	3.9277+0			0.3112+3	2.222+2	2.222+2			4.9400
1.0000+57	6.0689+3	2.8007+0			0.2294+3	2.222+2	2.222+2			4.4300
1.0000+58	5.8937+3	2.5926+0			0.1476+3	2.222+2	2.222+2			3.9200
1.0000+59	6.2228+3	2.2955+0			0.0658+3	2.222+2	2.222+2			3.4100
1.0000+60	5.5000+7	1.5000+0			0.0000+7	2.222+2	2.222+2			2.9000
1.0000+61	5.5000+7	1.5000+0			0.0000+7	2.222+2	2.222+2			2.3900
1.0000+62	5.5000+7	1.5000+0			0.0000+7	2.222+2	2.222+2			1.8800
1.0000+63	5.5000+7	1.5000+0			0.0000+7	2.222+2	2.222+2			1.3700
1.0000+64	5.5000+7	1.5000+0			0.0000+7	2.222+2	2.222+2			8.0000
1.0000+65	5.5000+7	1.5000+0			0.0000+7	2.222+2	2.222+2			7.4900
1.0000+66	5.5000+7	1.5000+0			0.0000+7	2.222+2	2.222+2			6.9800
1.0000+67	5.5000+7	1.5000+0			0.0000+7	2.222+2	2.222+2			6.4700
1.0000+68	5.5000+7	1.5000+0			0.0000+7	2.222+2	2.222+2			5.9600
1.0000+69	5.5000+7	1.5000+0			0.0000+7	2.222+2	2.222+2			5.4500
1.0000+70	5.5000+7	1.5000+0			0.0000+7	2.222+2	2.222+2			4.9400
1.0000+71	5.5000+7	1.5000+0			0.0000+7	2.222+2	2.222+2			4.4300
1.0000+72	5.5000+7	1.5000+0			0.0000+7	2.222+2	2.222+2			3.9200
1.0000+73	5.5000+7	1.5000+0			0.0000+7	2.222+2	2.222+2			3.4100
1.0000+74	5.5000+7	1.5000+0			0.0000+7	2.222+2	2.222+2			2.9000
1.0000+75	5.5000+7	1.5000+0			0.0000+7	2.222+2	2.222+2			2.3900
1.0000+76	5.5000+7	1.5000+0			0.0000+7	2.222+2	2.222+2			1.8800
1.0000+77	5.5000+7	1.5000+0			0.0000+7	2.222+2	2.222+2			1.3700
1.0000+78	5.5000+7	1.5000+0			0.0000+7	2.222+2	2.222+2			8.0000
1.0000+79	5.5000+7	1.5000+0			0.0000+7	2.222+2	2.222+2			7.4900
1.0000+80	5.5000+7	1.5000+0			0.0000+7	2.222+2	2.222+2			6.9800
1.0000+81	5.5000+7	1.5000+0			0.0000+7	2.222+2	2.222+2			6.4700
1.0000+82	5.5000+7	1.5000+0			0.0000+7	2.222+2	2.222+2			5.9600
1.0000+83	5.5000+7	1.5000+0			0.0000+7	2.222+2	2.222+2			5.4500
1.0000+84	5.5000+7	1.5000+0			0.0000+7	2.222+2	2.222+2			4.9400
1.0000+85	5.5000+7	1.5000+0			0.0000+7	2.222+2	2.222+2			4.4300
1.0000+86	5.5000+7	1.5000+0			0.0000+7	2.222+2	2.222+2			3.9200
1.0000+87	5.5000+7	1.5000+0			0.0000+7	2.222+2	2.222+2			3.4100
1.0000+88	5.5000+7	1.5000+0			0.0000+7	2.222+2	2.222+2			2.9000
1.0000+89	5.5000+7	1.5000+0			0.0000+7	2.222+2	2.222+2			2.3900
1.0000+90	5.5000+7	1.5000+0			0.0000+7	2.222+2	2.222+2			1.8800
1.0000+91	5.5000+7	1.5000+0			0.0000+7	2.222+2	2.222+2			1.3700
1.0000+92	5.5000+7	1.5000+0			0.0000+7	2.222+2	2.222+2			8.0000
1.0000+93	5.5000+7	1.5000+0			0.0000+7	2.222+2	2.222+2			7.4900</

CROSS SECTION

PU-240

MATERIAL = 2944

ENERGY	TOTAL	ELASTIC	INEL	(N.2N)	(N.3N)	(N.MR)	(N.MR)	(N.MR)	(N.P)	(N.D)	(N.R)	MU-BAR
1.0000-5	1.0000-2	1.6036+0	1.6036+0	2.0264-1	9.6300-0	8.0498+2	8.0498+2	8.0498+2	8.0498+2	2.8012-3	2.8012-3	2.8012-3
1.0000-4	1.0000-2	1.5866+0	1.5866+0	1.5866+0	9.4361+2	7.9452+2	7.9452+2	7.9452+2	7.9452+2	2.8011-3	2.8011-3	2.8011-3
1.0000-3	1.0000-2	1.5722+0	1.5722+0	1.5722+0	9.4522+2	7.9613+2	7.9613+2	7.9613+2	7.9613+2	2.8011-3	2.8011-3	2.8011-3
1.0000-2	1.0000-2	1.5578+0	1.5578+0	1.5578+0	9.4678+2	7.9769+2	7.9769+2	7.9769+2	7.9769+2	2.8011-3	2.8011-3	2.8011-3
1.0000-1	1.0000-1	1.5434+0	1.5434+0	1.5434+0	9.4834+2	7.9925+2	7.9925+2	7.9925+2	7.9925+2	2.8011-3	2.8011-3	2.8011-3
1.0000-0	1.0000-1	1.5290+0	1.5290+0	1.5290+0	9.4990+2	8.0081+2	8.0081+2	8.0081+2	8.0081+2	2.8011-3	2.8011-3	2.8011-3
1.0000-0	1.0000-1	1.5146+0	1.5146+0	1.5146+0	9.5146+2	8.0237+2	8.0237+2	8.0237+2	8.0237+2	2.8011-3	2.8011-3	2.8011-3
1.0000-0	1.0000-1	1.5002+0	1.5002+0	1.5002+0	9.5302+2	8.0393+2	8.0393+2	8.0393+2	8.0393+2	2.8011-3	2.8011-3	2.8011-3
1.0000-0	1.0000-1	1.4858+0	1.4858+0	1.4858+0	9.5458+2	8.0549+2	8.0549+2	8.0549+2	8.0549+2	2.8011-3	2.8011-3	2.8011-3
1.0000-0	1.0000-1	1.4714+0	1.4714+0	1.4714+0	9.5614+2	8.0705+2	8.0705+2	8.0705+2	8.0705+2	2.8011-3	2.8011-3	2.8011-3
1.0000-0	1.0000-1	1.4570+0	1.4570+0	1.4570+0	9.5770+2	8.0861+2	8.0861+2	8.0861+2	8.0861+2	2.8011-3	2.8011-3	2.8011-3
1.0000-0	1.0000-1	1.4426+0	1.4426+0	1.4426+0	9.5926+2	8.1017+2	8.1017+2	8.1017+2	8.1017+2	2.8011-3	2.8011-3	2.8011-3
1.0000-0	1.0000-1	1.4282+0	1.4282+0	1.4282+0	9.6082+2	8.1173+2	8.1173+2	8.1173+2	8.1173+2	2.8011-3	2.8011-3	2.8011-3
1.0000-0	1.0000-1	1.4138+0	1.4138+0	1.4138+0	9.6238+2	8.1329+2	8.1329+2	8.1329+2	8.1329+2	2.8011-3	2.8011-3	2.8011-3
1.0000-0	1.0000-1	1.3994+0	1.3994+0	1.3994+0	9.6394+2	8.1485+2	8.1485+2	8.1485+2	8.1485+2	2.8011-3	2.8011-3	2.8011-3
1.0000-0	1.0000-1	1.3850+0	1.3850+0	1.3850+0	9.6550+2	8.1641+2	8.1641+2	8.1641+2	8.1641+2	2.8011-3	2.8011-3	2.8011-3
1.0000-0	1.0000-1	1.3706+0	1.3706+0	1.3706+0	9.6706+2	8.1797+2	8.1797+2	8.1797+2	8.1797+2	2.8011-3	2.8011-3	2.8011-3
1.0000-0	1.0000-1	1.3562+0	1.3562+0	1.3562+0	9.6862+2	8.1953+2	8.1953+2	8.1953+2	8.1953+2	2.8011-3	2.8011-3	2.8011-3
1.0000-0	1.0000-1	1.3418+0	1.3418+0	1.3418+0	9.7018+2	8.2109+2	8.2109+2	8.2109+2	8.2109+2	2.8011-3	2.8011-3	2.8011-3
1.0000-0	1.0000-1	1.3274+0	1.3274+0	1.3274+0	9.7174+2	8.2265+2	8.2265+2	8.2265+2	8.2265+2	2.8011-3	2.8011-3	2.8011-3
1.0000-0	1.0000-1	1.3130+0	1.3130+0	1.3130+0	9.7330+2	8.2421+2	8.2421+2	8.2421+2	8.2421+2	2.8011-3	2.8011-3	2.8011-3
1.0000-0	1.0000-1	1.2986+0	1.2986+0	1.2986+0	9.7486+2	8.2577+2	8.2577+2	8.2577+2	8.2577+2	2.8011-3	2.8011-3	2.8011-3
1.0000-0	1.0000-1	1.2842+0	1.2842+0	1.2842+0	9.7642+2	8.2733+2	8.2733+2	8.2733+2	8.2733+2	2.8011-3	2.8011-3	2.8011-3
1.0000-0	1.0000-1	1.2698+0	1.2698+0	1.2698+0	9.7798+2	8.2889+2	8.2889+2	8.2889+2	8.2889+2	2.8011-3	2.8011-3	2.8011-3
1.0000-0	1.0000-1	1.2554+0	1.2554+0	1.2554+0	9.7954+2	8.3045+2	8.3045+2	8.3045+2	8.3045+2	2.8011-3	2.8011-3	2.8011-3
1.0000-0	1.0000-1	1.2410+0	1.2410+0	1.2410+0	9.8110+2	8.3201+2	8.3201+2	8.3201+2	8.3201+2	2.8011-3	2.8011-3	2.8011-3
1.0000-0	1.0000-1	1.2266+0	1.2266+0	1.2266+0	9.8266+2	8.3357+2	8.3357+2	8.3357+2	8.3357+2	2.8011-3	2.8011-3	2.8011-3
1.0000-0	1.0000-1	1.2122+0	1.2122+0	1.2122+0	9.8422+2	8.3513+2	8.3513+2	8.3513+2	8.3513+2	2.8011-3	2.8011-3	2.8011-3
1.0000-0	1.0000-1	1.1978+0	1.1978+0	1.1978+0	9.8578+2	8.3669+2	8.3669+2	8.3669+2	8.3669+2	2.8011-3	2.8011-3	2.8011-3
1.0000-0	1.0000-1	1.1834+0	1.1834+0	1.1834+0	9.8734+2	8.3825+2	8.3825+2	8.3825+2	8.3825+2	2.8011-3	2.8011-3	2.8011-3
1.0000-0	1.0000-1	1.1690+0	1.1690+0	1.1690+0	9.8890+2	8.3981+2	8.3981+2	8.3981+2	8.3981+2	2.8011-3	2.8011-3	2.8011-3
1.0000-0	1.0000-1	1.1546+0	1.1546+0	1.1546+0	9.9046+2	8.4137+2	8.4137+2	8.4137+2	8.4137+2	2.8011-3	2.8011-3	2.8011-3
1.0000-0	1.0000-1	1.1402+0	1.1402+0	1.1402+0	9.9202+2	8.4293+2	8.4293+2	8.4293+2	8.4293+2	2.8011-3	2.8011-3	2.8011-3
1.0000-0	1.0000-1	1.1258+0	1.1258+0	1.1258+0	9.9358+2	8.4449+2	8.4449+2	8.4449+2	8.4449+2	2.8011-3	2.8011-3	2.8011-3
1.0000-0	1.0000-1	1.1114+0	1.1114+0	1.1114+0	9.9514+2	8.4605+2	8.4605+2	8.4605+2	8.4605+2	2.8011-3	2.8011-3	2.8011-3
1.0000-0	1.0000-1	1.0970+0	1.0970+0	1.0970+0	9.9670+2	8.4761+2	8.4761+2	8.4761+2	8.4761+2	2.8011-3	2.8011-3	2.8011-3
1.0000-0	1.0000-1	1.0826+0	1.0826+0	1.0826+0	9.9826+2	8.4917+2	8.4917+2	8.4917+2	8.4917+2	2.8011-3	2.8011-3	2.8011-3
1.0000-0	1.0000-1	1.0682+0	1.0682+0	1.0682+0	10.0000+2	8.5073+2	8.5073+2	8.5073+2	8.5073+2	2.8011-3	2.8011-3	2.8011-3
1.0000-0	1.0000-1	1.0538+0	1.0538+0	1.0538+0	10.0156+2	8.5229+2	8.5229+2	8.5229+2	8.5229+2	2.8011-3	2.8011-3	2.8011-3
1.0000-0	1.0000-1	1.0394+0	1.0394+0	1.0394+0	10.0312+2	8.5385+2	8.5385+2	8.5385+2	8.5385+2	2.8011-3	2.8011-3	2.8011-3
1.0000-0	1.0000-1	1.0250+0	1.0250+0	1.0250+0	10.0468+2	8.5541+2	8.5541+2	8.5541+2	8.5541+2	2.8011-3	2.8011-3	2.8011-3
1.0000-0	1.0000-1	1.0106+0	1.0106+0	1.0106+0	10.0624+2	8.5697+2	8.5697+2	8.5697+2	8.5697+2	2.8011-3	2.8011-3	2.8011-3
1.0000-0	1.0000-1	0.9962+0	0.9962+0	0.9962+0	10.0780+2	8.5853+2	8.5853+2	8.5853+2	8.5853+2	2.8011-3	2.8011-3	2.8011-3
1.0000-0	1.0000-1	0.9818+0	0.9818+0	0.9818+0	10.0936+2	8.6009+2	8.6009+2	8.6009+2	8.6009+2	2.8011-3	2.8011-3	2.8011-3
1.0000-0	1.0000-1	0.9674+0	0.9674+0	0.9674+0	10.1092+2	8.6165+2	8.6165+2	8.6165+2	8.6165+2	2.8011-3	2.8011-3	2.8011-3
1.0000-0	1.0000-1	0.9530+0	0.9530+0	0.9530+0	10.1248+2	8.6321+2	8.6321+2	8.6321+2	8.6321+2	2.8011-3	2.8011-3	2.8011-3
1.0000-0	1.0000-1	0.9386+0	0.9386+0	0.9386+0	10.1404+2	8.6477+2	8.6477+2	8.6477+2	8.6477+2	2.8011-3	2.8011-3	2.8011-3
1.0000-0	1.0000-1	0.9242+0	0.9242+0	0.9242+0	10.1560+2	8.6633+2	8.6633+2	8.6633+2	8.6633+2	2.8011-3	2.8011-3	2.8011-3
1.0000-0	1.0000-1	0.9098+0	0.9098+0	0.9098+0	10.1716+2	8.6789+2	8.6789+2	8.6789+2	8.6789+2	2.8011-3	2.8011-3	2.8011-3
1.0000-0	1.0000-1	0.8954+0	0.8954+0	0.8954+0	10.1872+2	8.6945+2	8.6945+2	8.6945+2	8.6945+2	2.8011-3	2.8011-3	2.8011-3
1.0000-0	1.0000-1	0.8810+0	0.8810+0	0.8810+0	10.2028+2	8.7101+2	8.7101+2	8.7101+2	8.7101+2	2.8011-3	2.8011-3	2.8011-3
1.0000-0	1.0000-1	0.8666+0	0.8666+0	0.8666+0	10.2184+2	8.7257+2	8.7257+2	8.7257+2	8.7257+2	2.8011-3	2.8011-3	2.8011-3
1.0000-0	1.0000-1	0.8522+0	0.8522+0	0.8522+0	10.2340+2	8.7413+2	8.7413+2	8.7413+2	8.7413+2	2.8011-3	2.8011-3	2.8011-3
1.0000-0	1.0000-1	0.8378+0	0.8378+0	0.8378+0	10.2496+2	8.7569+2	8.7569+2	8.7569+2	8.7569+2	2.8011-3	2.8011-3	2.8011-3
1.0000-0	1.0000-1	0.8234+0	0.8234+0	0.8234+0	10.2652+2	8.7725+2	8.7725+2	8.7725+2	8.7725+2	2.8011-3	2.8011-3	2.8011-3
1.0000-0	1.0000-1	0.8090+0	0.8090+0	0.8090+0	10.2808+2	8.7881+2	8.7881+2	8.7881+2	8.7881+2	2.8011-3	2.8011-3	2.8011-3
1.0000-0	1.0000-1	0.7946+0	0.7946+0	0.7946+0	10.2964+2	8.8037+2	8.8037+2	8.8037+2	8.8037+2	2.8011-3	2.8011-3	2.8011-3
1.0000-0	1.0000-1	0.7802+0	0.7802+0	0.7802+0	10.3120+2	8.8193+2	8.8193+2	8.8193+2	8.8193+2	2.8011-3	2.8011-3	2.8011-3
1.0000-0	1.0000-1	0.7658+0	0.7658+0	0.7658+0	10.3276+2	8.8349+2	8.8349+2	8.8349+2	8.8349+2	2.8011-3	2.8011-3	2.8011-3
1.0000-0	1.0000-1	0.7514+0	0.7514+0	0.7514+0	10.3432+2	8.8505+2	8.8505+2	8.8505+2	8.8505+2	2.8011-3	2.8011-3	2.8011-3
1.0000-0	1.0000-1	0.7370+0	0.7370+0	0.7370+0	10.3588+2	8.8661+2	8.8661+2	8.8661+2	8.8661+2	2.8011-3	2.8011-3	2.8011-3
1.0000-0	1.0000-1	0.7226+0	0.7226+0	0.7226+0	10.3744+2	8.8817+2	8.8817+2	8.8817+2	8.8817+2	2.8011-3	2.8011-3	2.8011-3
1.0000-0	1.0000-1	0.7082+0	0.7082+0	0.7082+0	10.3900+2	8.8973+2	8.8973+2	8.8973+2	8.8973+2	2.8011-3	2.8011-3	2.8011-3
1.0000-0	1.0000-1	0.6938+0	0.6938+0	0.6938+0	10.4056+2	8.9129+2	8.9129+2	8.9129+2	8.9129+2	2.8011-3	2.8011-3	2.8011-3

MATERIAL -2945 CROSS SECTION PU-241

ENERGY	TOTAL	ELASTIC	INELA	(N.2N)	(N.3N)	FIBRION	(N.NR)	(N.NF)	CAPTURE	(N.PI)	(N.O)	(N.A)	MU-BRR
1.0000+ 5 ~ 1.0000- 2	4.4498+ 3	1.0486+ 1				3.1400+ 3			1.2593+ 3				2.8566- 3
1.0000- 2 ~ 1.0000- 3	2.0907+ 3	1.0368+ 1				1.4690+ 3			6.6042+ 2				2.6448- 3
1.0000- 3 ~ 1.0000- 4	1.7036+ 3	1.0326+ 1				1.2350+ 3			4.5448+ 2				2.6578- 3
1.0000- 4 ~ 1.0000- 5	1.4113+ 3	1.0330+ 1				1.0544+ 3			3.6697+ 2				2.6503- 3
1.0000- 5 ~ 1.0000- 6	1.1883+ 3	1.0408+ 1				7.7952+ 2			2.5567+ 2				2.6429- 3
1.0000- 6 ~ 1.0000- 7	1.0489+ 3	1.0500+ 1				7.1520+ 2			2.3096+ 2				2.6555- 3
1.0000- 7 ~ 1.0000- 8	8.2359+ 2	9.4159+ 0				6.3014+ 2			2.6372+ 2				2.6683- 3
1.0000- 8 ~ 1.0000- 9	9.6268+ 2	9.0545+ 0				6.6090+ 2			1.8922+ 2				2.6628- 3
1.0000- 9 ~ 1.0000- 10	6.7659+ 2	6.2639+ 0				1.4411+ 2			2.7182+ 2				2.6654- 3
1.0000- 10 ~ 1.0000- 11	6.4617+ 2	1.2894+ 1				4.0208+ 2			2.3107+ 2				2.6708- 3
1.0000- 11 ~ 1.0000- 12	1.6734+ 2	1.1847+ 1				9.0774+ 1			6.4707+ 1				2.6728- 3
1.0000- 12 ~ 1.0000- 13	8.5933+ 1	1.1184+ 1				5.1091+ 1			2.3425+ 1				2.6742- 3
1.0000- 13 ~ 1.0000- 14	5.2019+ 1	1.0244+ 1				3.0630+ 1			7.1365+ 0				2.6782- 3
1.0000+ 0 ~ 1.0000+ 1	4.2081+ 1	9.8185+ 0				2.8117+ 1			4.1456+ 1				2.6807- 3
1.0000+ 1 ~ 1.0000+ 2	3.7582+ 1	9.3720+ 0				2.5223+ 1			2.5868+ 1				2.6823- 3
1.0000+ 2 ~ 1.0000+ 3	4.0779+ 1	8.7028+ 0				2.9739+ 1			2.7435+ 1				2.6837- 3
1.0000+ 3 ~ 1.0000+ 4	7.5910+ 0	6.1926+ 0				3.1371+ 2			2.2798+ 2				2.6907- 3
1.0000+ 4 ~ 1.0000+ 5	2.7072+ 2	9.2300+ 0				2.4895+ 2			1.2632+ 1				2.6922- 3
1.0000+ 5 ~ 1.0000+ 6	3.5591+ 2	1.2238+ 1				3.0932+ 2			3.4345+ 1				2.6941- 3
1.0000+ 6 ~ 1.0000+ 7	2.8212+ 2	1.1159+ 1				2.0685+ 2			4.3977+ 1				2.6961- 3
1.0000+ 7 ~ 1.0000+ 8	3.2340+ 2	1.6282+ 1				2.0445+ 2			1.0151+ 2				2.6988- 3
1.0000+ 8 ~ 1.0000+ 9	1.5750+ 2	1.8556+ 1				9.3716+ 1			6.0684+ 1				2.7012- 3
1.0000+ 9 ~ 1.0000+ 10	1.1570+ 2	1.5096+ 1				8.3866+ 1			1.8751+ 1				2.7040- 3
1.0000+ 10 ~ 1.0000+ 11	7.3189+ 1	1.3407+ 1				4.9116+ 1			1.0665+ 1				2.7069- 3
1.0000+ 11 ~ 1.0000+ 12	8.1287+ 1	1.3321+ 1				4.0952+ 1			2.0705+ 0				2.7090- 3
1.0000+ 12 ~ 1.0000+ 13	3.7452+ 1	1.2526+ 1				3.2954+ 1			2.7005+ 0				2.7100- 3
1.0000+ 13 ~ 1.0000+ 14	7.8246+ 1	1.2526+ 1				4.7134+ 1			1.4083+ 1				2.7110- 3
1.0000+ 14 ~ 1.0000+ 15	1.5728+ 1	1.5728+ 1				2.5477+ 1			6.2627+ 0				2.7120- 3
1.0000+ 15 ~ 1.0000+ 16	4.4449+ 1	1.2743+ 1				2.8191+ 1			7.0075+ 0				2.7130- 3
1.0000+ 16 ~ 1.0000+ 17	4.6809+ 1	1.3135+ 1				2.8191+ 1			6.7140+ 0				2.7140- 3
1.0000+ 17 ~ 1.0000+ 18	4.0860+ 1	1.3641+ 1				2.7322+ 1			5.2425+ 0				2.7150- 3
1.0000+ 18 ~ 1.0000+ 19	5.8344+ 1	1.3978+ 1				1.6223+ 1			1.0623+ 1				2.7160- 3
1.0000+ 19 ~ 1.0000+ 20	5.4291+ 1	1.3580+ 1				1.6577+ 1			5.1338+ 0				2.7170- 3
1.0000+ 20 ~ 1.0000+ 21	2.7613+ 1	1.2842+ 1				1.1195+ 1			1.2388+ 0				2.7180- 3
1.0000+ 21 ~ 1.0000+ 22	2.6118+ 1	1.2861+ 1				1.0445+ 1			2.8129+ 0				2.7190- 3
1.0000+ 22 ~ 1.0000+ 23	2.5728+ 1	1.3051+ 1				9.8095+ 0			2.7668+ 0				2.7200- 3
1.0000+ 23 ~ 1.0000+ 24	2.3765+ 1	1.3014+ 1				8.3384+ 0			2.4079+ 0				2.7210- 3
1.0000+ 24 ~ 1.0000+ 25	2.1451+ 1	1.2782+ 1				6.8785+ 0			1.7911+ 0				2.7220- 3
1.0000+ 25 ~ 1.0000+ 26	2.0581+ 1	1.2763+ 1				5.2479+ 0			1.3728+ 0				2.7230- 3
1.0000+ 26 ~ 1.0000+ 27	1.8557+ 1	1.2525+ 1				4.8077+ 0			1.2411+ 0				2.7240- 3
1.0000+ 27 ~ 1.0000+ 28	1.7984+ 1	1.2497+ 1				4.3914+ 0			1.0951+ 0				2.7250- 3
1.0000+ 28 ~ 1.0000+ 29	1.7884+ 1	1.2290+ 1				3.9972+ 0			8.8221+ 0				2.7260- 3
1.0000+ 29 ~ 1.0000+ 30	1.7159+ 1	1.2290+ 1				3.5412+ 0			7.8975+ 1				2.7270- 3
1.0000+ 30 ~ 1.0000+ 31	1.6455+ 1	1.2122+ 1				3.0361+ 0			6.6361+ 1				2.7280- 3
1.0000+ 31 ~ 1.0000+ 32	1.5775+ 1	1.1876+ 1				2.5732+ 0			6.2475+ 1				2.7290- 3
1.0000+ 32 ~ 1.0000+ 33	1.5176+ 1	1.1676+ 1				2.1544+ 0			4.9864+ 1				2.7300- 3
1.0000+ 33 ~ 1.0000+ 34	1.4147+ 1	1.1003+ 1				2.8544+ 0			5.2464+ 1				2.7310- 3
1.0000+ 34 ~ 1.0000+ 35	1.3611+ 1	1.0779+ 1				1.9588+ 0			5.2464+ 1				2.7320- 3
1.0000+ 35 ~ 1.0000+ 36	1.3445+ 1	1.0588+ 1				1.3472+ 0			4.2455+ 1				2.7330- 3
1.0000+ 36 ~ 1.0000+ 37	1.2557+ 1	9.0289+ 0				2.2205+ 0			3.5678+ 1				2.7340- 3
1.0000+ 37 ~ 1.0000+ 38	1.2542+ 1	9.0289+ 0				2.1170+ 0			3.2430+ 1				2.7350- 3
1.0000+ 38 ~ 1.0000+ 39	1.1924+ 1	9.4242+ 0				1.8620+ 0			2.9723+ 1				2.7360- 3
1.0000+ 39 ~ 1.0000+ 40	1.1162+ 1	8.7889+ 0				1.8620+ 0			2.7073+ 1				2.7370- 3
1.0000+ 40 ~ 1.0000+ 41	1.0284+ 1	7.9889+ 0				1.8620+ 0			2.5076+ 1				2.7380- 3
1.0000+ 41 ~ 1.0000+ 42	8.6645+ 0	6.5119+ 0				1.5148+ 0			2.2519+ 1				2.7390- 3
1.0000+ 42 ~ 1.0000+ 43	8.1215+ 0	5.8605+ 0				1.5105+ 0			2.0519+ 1				2.7400- 3
1.0000+ 43 ~ 1.0000+ 44	7.5614+ 0	5.2448+ 0				1.5105+ 0			1.8620+ 0				2.7410- 3
1.0000+ 44 ~ 1.0000+ 45	7.1326+ 0	4.7020+ 0				1.5620+ 0			1.6820+ 0				2.7420- 3
1.0000+ 45 ~ 1.0000+ 46	6.9939+ 0	4.3285+ 0				1.4893+ 0			1.4893+ 0				2.7430- 3
1.0000+ 46 ~ 1.0000+ 47	6.7588+ 0	4.3678+ 0				1.3947+ 0			1.3947+ 0				2.7440- 3
1.0000+ 47 ~ 1.0000+ 48	7.7659+ 0	4.6470+ 0				1.6107+ 0			9.3723+ 1				2.7450- 3
1.0000+ 48 ~ 1.0000+ 49	8.0569+ 0	5.2367+ 0				1.4893+ 0			3.3723+ 1				2.7460- 3
1.0000+ 49 ~ 1.0000+ 50	7.9535+ 0	5.1812+ 0				1.3947+ 0			3.3723+ 1				2.7470- 3
1.0000+ 50 ~ 1.0000+ 51	6.7694+ 0	4.0807+ 0				1.4893+ 0			1.4893+ 0				2.7480- 3
1.0000+ 51 ~ 1.0000+ 52	6.7694+ 0	3.3489+ 0				1.4893+ 0			1.4893+ 0				2.7490- 3
1.0000+ 52 ~ 1.0000+ 53	5.8472+ 0	3.3489+ 0				1.4893+ 0			1.4893+ 0				2.7500- 3
1.0000+ 53 ~ 1.0000+ 54	5.8472+ 0	3.3489+ 0				1.4893+ 0			1.4893+ 0				2.7510- 3
1.0000+ 54 ~ 1.0000+ 55	5.8472+ 0	3.3489+ 0				1.4893+ 0			1.4893+ 0				2.7520- 3
1.0000+ 55 ~ 1.0000+ 56	5.8472+ 0	3.3489+ 0				1.4893+ 0			1.4893+ 0				2.7530- 3
1.0000+ 56 ~ 1.0000+ 57	5.8472+ 0	3.3489+ 0				1.4893+ 0			1.4893+ 0				2.7540- 3
1.0000+ 57 ~ 1.0000+ 58	5.8472+ 0	3.3489+ 0				1.4893+ 0			1.4893+ 0				2.7550- 3
1.0000+ 58 ~ 1.0000+ 59	5.8472+ 0	3.3489+ 0				1.4893+ 0			1.4893+ 0				2.7560- 3
1.0000+ 59 ~ 1.0000+ 60	5.8472+ 0	3.3489+ 0				1.4893+ 0			1.4893+ 0				2.7570- 3
1.0000+ 60 ~ 1.0000+ 61	5.8472+ 0	3.3489+ 0				1.4893+ 0			1.4893+ 0				2.7580- 3
1.0000+ 61 ~ 1.0000+ 62	5.8472+ 0	3.3489+ 0				1.4893+ 0			1.4893+ 0				2.7590- 3
1.0000+ 62 ~ 1.0000+ 63	5.8472+ 0	3.3489+ 0				1.4893+ 0			1.4893+ 0				2.7600- 3
1.0000+ 63 ~ 1.0000+ 64	5.8472+ 0	3.3489+ 0				1.4893+ 0			1.4893+ 0				2.7610- 3
1.0000+ 64 ~ 1.0000+ 65	5.8472+ 0	3.3489+ 0				1.4893+ 0			1.4893+ 0				2.7620- 3
1.0000+ 65 ~ 1.0000+ 66	5.8472+ 0	3.3489+ 0				1.4893+ 0			1.4893+ 0				2.7630- 3
1.0000+ 66 ~ 1.0000+ 67	5.8472+ 0	3.3489+ 0				1.4893+ 0			1.4893+ 0				2.7640- 3
1.0000+ 67 ~ 1.0000+ 68	5.8472+ 0	3.3489+ 0				1.4893+ 0			1.4893+ 0				2.7650- 3

CROSS SECTION

MATERIAL	ENERGY	TOTAL	ELRBTIC	INELA	(N.2N)	(N.3N)	FISSION	(N.NR)	(N.NF)	CAPTURE	(N.P)	(N.D)	(N.A)	MU-BRR
1.0000	5 ~ 1.0000-2	6.4578+1	8.1287+0			3.7445-1	1.7357-1		5.6074+1					2.7780-5
1.0000	1.5000-2	3.4503+1	8.1210+0			1.7357-1	1.7357-1		2.5009+1					2.7780-5
1.0000	2.0000-2	3.0393+1	8.1173+0			1.7357-1	1.7357-1		2.5009+1					2.7780-5
1.0000	3.0000-2	2.8017+1	8.1136+0			1.7357-1	1.7357-1		2.5009+1					2.7780-5
1.0000	4.0000-2	2.5272+1	8.0956+0			1.7357-1	1.7357-1		2.5009+1					2.7780-5
1.0000	5.0000-2	2.2965+1	8.0877+0			1.7357-1	1.7357-1		2.5009+1					2.7780-5
1.0000	6.0000-2	2.0985+1	8.0768+0			1.7357-1	1.7357-1		2.5009+1					2.7780-5
1.0000	7.0000-2	1.8671+1	8.0688+0			1.7357-1	1.7357-1		2.5009+1					2.7780-5
1.0000	8.0000-2	1.6422+1	8.0658+0			1.7357-1	1.7357-1		2.5009+1					2.7780-5
1.0000	1.5000-1	1.7019+0	8.0307+0			1.7357-1	1.7357-1		2.5009+1					2.7780-5
1.0000	2.0000-1	1.5939+0	7.9862+0			1.7357-1	1.7357-1		2.5009+1					2.7780-5
1.0000	3.0000-1	1.4982+0	7.9212+0			1.7357-1	1.7357-1		2.5009+1					2.7780-5
1.0000	4.0000-1	1.4300+0	7.8355+0			1.7357-1	1.7357-1		2.5009+1					2.7780-5
1.0000	5.0000-1	1.3774+0	7.7374+0			1.7357-1	1.7357-1		2.5009+1					2.7780-5
1.0000	6.0000-1	1.3351+0	7.6104+0			1.7357-1	1.7357-1		2.5009+1					2.7780-5
1.0000	7.0000-1	1.3021+0	7.4218+0			1.7357-1	1.7357-1		2.5009+1					2.7780-5
1.0000	8.0000-1	1.2711+0	7.1294+0			1.7357-1	1.7357-1		2.5009+1					2.7780-5
1.0000	0.0000-0	1.2532+0	6.4334+0			1.7357-1	1.7357-1		2.5009+1					2.7780-5
1.0000	0.0000-0	1.2493+0	4.7036+0			1.7357-1	1.7357-1		2.5009+1					2.7780-5
1.0000	0.0000-0	1.2508+0	2.2058+0			1.7357-1	1.7357-1		2.5009+1					2.7780-5
1.0000	0.0000-0	1.2566+0	4.8274+0			1.7357-1	1.7357-1		2.5009+1					2.7780-5
1.0000	0.0000-0	1.2671+0	1.3855+0			1.7357-1	1.7357-1		2.5009+1					2.7780-5
1.0000	0.0000-0	1.2826+0	1.7014+0			1.7357-1	1.7357-1		2.5009+1					2.7780-5
1.0000	0.0000-0	1.3000+0	1.9500+0			1.7357-1	1.7357-1		2.5009+1					2.7780-5
1.0000	0.0000-0	1.3193+0	1.7567+0			1.7357-1	1.7357-1		2.5009+1					2.7780-5
1.0000	0.0000-0	1.3406+0	1.1287+1			1.7357-1	1.7357-1		2.5009+1					2.7780-5
1.0000	1.0000-1	1.3638+0	1.0587+1			1.7357-1	1.7357-1		2.5009+1					2.7780-5
1.0000	1.5000-1	1.3890+0	1.0255+1			1.7357-1	1.7357-1		2.5009+1					2.7780-5
1.0000	2.0000-1	1.4161+0	8.7621+0			1.7357-1	1.7357-1		2.5009+1					2.7780-5
1.0000	3.0000-1	1.4452+0	6.6950+0			1.7357-1	1.7357-1		2.5009+1					2.7780-5
1.0000	4.0000-1	1.4763+0	4.1179+2			1.7357-1	1.7357-1		2.5009+1					2.7780-5
1.0000	5.0000-1	1.5094+0	1.5822+1			1.7357-1	1.7357-1		2.5009+1					2.7780-5
1.0000	6.0000-1	1.5445+0	1.1425+1			1.7357-1	1.7357-1		2.5009+1					2.7780-5
1.0000	7.0000-1	1.5816+0	2.2912+1			1.7357-1	1.7357-1		2.5009+1					2.7780-5
1.0000	8.0000-1	1.6207+0	3.5595+1			1.7357-1	1.7357-1		2.5009+1					2.7780-5
1.0000	2.2222-2	1.6608+0	2.0083+1			1.7357-1	1.7357-1		2.5009+1					2.7780-5
1.0000	3.3333-2	1.7021+0	1.0922+1			1.7357-1	1.7357-1		2.5009+1					2.7780-5
1.0000	4.4444-2	1.7445+0	1.9377+1			1.7357-1	1.7357-1		2.5009+1					2.7780-5
1.0000	5.5555-2	1.7880+0	2.8554+1			1.7357-1	1.7357-1		2.5009+1					2.7780-5
1.0000	6.6666-2	1.8325+0	6.0266+1			1.7357-1	1.7357-1		2.5009+1					2.7780-5
1.0000	7.7777-2	1.8780+0	1.2900+1			1.7357-1	1.7357-1		2.5009+1					2.7780-5
1.0000	8.8888-2	1.9245+0	1.7694+1			1.7357-1	1.7357-1		2.5009+1					2.7780-5
1.0000	9.9999-2	1.9720+0	2.6900+1			1.7357-1	1.7357-1		2.5009+1					2.7780-5
1.0000	0.0000-3	2.0205+0	1.9815+1			1.7357-1	1.7357-1		2.5009+1					2.7780-5
1.0000	0.0000-3	2.0699+0	2.1652+1			1.7357-1	1.7357-1		2.5009+1					2.7780-5
1.0000	0.0000-3	2.1201+0	1.6325+1			1.7357-1	1.7357-1		2.5009+1					2.7780-5
1.0000	0.0000-3	2.1711+0	1.9395+1			1.7357-1	1.7357-1		2.5009+1					2.7780-5
1.0000	0.0000-3	2.2229+0	1.5971+1			1.7357-1	1.7357-1		2.5009+1					2.7780-5
1.0000	0.0000-3	2.2754+0	1.7884+1			1.7357-1	1.7357-1		2.5009+1					2.7780-5
1.0000	0.0000-3	2.3286+0	1.6387+1			1.7357-1	1.7357-1		2.5009+1					2.7780-5
1.0000	0.0000-3	2.3824+0	1.8377+1			1.7357-1	1.7357-1		2.5009+1					2.7780-5
1.0000	0.0000-3	2.4367+0	1.6172+1			1.7357-1	1.7357-1		2.5009+1					2.7780-5
1.0000	0.0000-3	2.4915+0	1.5991+1			1.7357-1	1.7357-1		2.5009+1					2.7780-5
1.0000	0.0000-3	2.5468+0	1.5810+1			1.7357-1	1.7357-1		2.5009+1					2.7780-5
1.0000	0.0000-3	2.6026+0	1.5630+1			1.7357-1	1.7357-1		2.5009+1					2.7780-5
1.0000	0.0000-3	2.6589+0	1.5451+1			1.7357-1	1.7357-1		2.5009+1					2.7780-5
1.0000	0.0000-3	2.7157+0	1.5272+1			1.7357-1	1.7357-1		2.5009+1					2.7780-5
1.0000	0.0000-3	2.7729+0	1.4594+1			1.7357-1	1.7357-1		2.5009+1					2.7780-5
1.0000	0.0000-3	2.8305+0	1.3772+1			1.7357-1	1.7357-1		2.5009+1					2.7780-5
1.0000	0.0000-3	2.8885+0	1.2790+1			1.7357-1	1.7357-1		2.5009+1					2.7780-5
1.0000	0.0000-3	2.9469+0	1.1428+1			1.7357-1	1.7357-1		2.5009+1					2.7780-5
1.0000	0.0000-3	3.0057+0	8.9511+1			1.7357-1	1.7357-1		2.5009+1					2.7780-5
1.0000	0.0000-3	3.0649+0	9.9317+1			1.7357-1	1.7357-1		2.5009+1					2.7780-5
1.0000	0.0000-3	3.1245+0	1.1287+0			1.7357-1	1.7357-1		2.5009+1					2.7780-5
1.0000	0.0000-3	3.1845+0	1.2270+0			1.7357-1	1.7357-1		2.5009+1					2.7780-5
1.0000	0.0000-3	3.2449+0	7.4573+0			1.7357-1	1.7357-1		2.5009+1					2.7780-5
1.0000	0.0000-3	3.3057+0	1.3224+0			1.7357-1	1.7357-1		2.5009+1					2.7780-5
1.0000	0.0000-3	3.3669+0	1.4165+0			1.7357-1	1.7357-1		2.5009+1					2.7780-5
1.0000	0.0000-3	3.4284+0	5.6558+0			1.7357-1	1.7357-1		2.5009+1					2.7780-5
1.0000	0.0000-3	3.4902+0	7.1174+0			1.7357-1	1.7357-1		2.5009+1					2.7780-5
1.0000	0.0000-3	3.5523+0	4.4073+0			1.7357-1	1.7357-1		2.5009+1					2.7780-5
1.0000	0.0000-3	3.6147+0	4.4265+0			1.7357-1	1.7357-1		2.5009+1					2.7780-5
1.0000	0.0000-3	3.6775+0	4.6206+0			1.7357-1	1.7357-1		2.5009+1					2.7780-5
1.0000	0.0000-3	3.7407+0	5.1723+0			1.7357-1	1.7357-1		2.5009+1					2.7780-5
1.0000	0.0000-3	3.8042+0	6.0448+0			1.7357-1	1.7357-1		2.5009+1					2.7780-5
1.0000	0.0000-3	3.8680+0	7.6904+0			1.7357-1	1.7357-1		2.5009+1					2.7780-5
1.0000	0.0000-3	3.9321+0	4.7487+0			1.7357-1	1.7357-1		2.5009+1					2.7780-5
1.0000	0.0000-3	3.9964+0	1.5677+0			1.7357-1	1.7357-1		2.5009+1					2.7780-5
1.0000	0.0000-3	4.0610+0	2.0064+1			1.7357-1	1.7357-1		2.5009+1					2.7780-5
1.0000	0.0000-3	4.1258+0	3.9308+1			1.7357-1	1.7357-1		2.5009+1					

MATERIAL = 2951 CROSS SECTION AM-241

ENERGY	TOTAL	ELASTIC	INELA	(N,2N)	(N,3N)	FISION	(N,NA)	(N,MP)	CAPTURE	(N,P)	(N,D)	(N,R)	MU-BAR
1.0000+ 5 ~ 1.0000- 2	2.0426+ 3	1.1658+ 1				9.9008+ 0			2.0210+ 3				2.7662- 3
1.0000- 5 ~ 1.0000- 2	9.1850+ 0	1.1504+ 1				4.6950+ 0			9.0350+ 0				2.7662- 3
1.0000- 2 ~ 1.0000- 1	7.6026+ 2	1.1306+ 1				3.7212+ 0			7.4524+ 0				2.7662- 3
2.0000- 2 ~ 1.0000- 1	6.2851+ 1	1.1264+ 1				3.0755+ 0			6.1210+ 0				2.7662- 3
3.0000- 2 ~ 1.0000- 1	5.1407+ 0	1.1081+ 1				2.5362+ 0			5.0046+ 0				2.7662- 3
4.0000- 2 ~ 1.0000- 1	4.4909+ 0	1.0885+ 1				2.1991+ 0			4.2986+ 0				2.7662- 3
5.0000- 2 ~ 1.0000- 1	3.9452+ 0	1.0734+ 1				1.9760+ 0			3.6680+ 0				2.7662- 3
6.0000- 2 ~ 1.0000- 1	3.4817+ 0	1.0655+ 1				1.7600+ 0			3.2571+ 0				2.7662- 3
1.0000- 1 ~ 1.5000- 1	2.8560+ 2	9.6013+ 0				1.5317+ 0			2.7447+ 0				2.7662- 3
1.5000- 1 ~ 2.0000- 1	3.2860+ 2	9.7126+ 0				1.6950+ 0			3.1240+ 0				2.7662- 3
2.0000- 1 ~ 3.0000- 1	4.1976+ 3	1.0507+ 1				2.1413+ 0			4.0250+ 0				2.7662- 3
3.0000- 1 ~ 4.0000- 1	5.2144+ 2	1.0177+ 1				1.5108+ 0			5.1026+ 0				2.7662- 3
4.0000- 1 ~ 5.0000- 1	1.9000+ 3	1.1641+ 1				6.2233+ 0			1.8621+ 0				2.7662- 3
5.0000- 1 ~ 6.0000- 1	3.1540+ 2	1.2833+ 1				1.1009+ 0			3.0146+ 0				2.7662- 3
6.0000- 1 ~ 7.0000- 1	7.3551+ 1	9.4611+ 0				3.9552+ 1			7.5654+ 1				2.7662- 3
1.0000+ 0 ~ 2.0000+ 0	1.0026+ 3	1.6750+ 1				7.7347+ 0			9.7816+ 0				2.7662- 3
2.0000+ 0 ~ 3.0000+ 0	2.5449+ 2	1.1446+ 1				5.8614+ 1			2.4248+ 2				2.7662- 3
3.0000+ 0 ~ 4.0000+ 0	9.0369+ 2	1.1837+ 1				7.2869+ 1			1.8892+ 2				2.7662- 3
4.0000+ 0 ~ 5.0000+ 0	9.8356+ 1	9.7821+ 0				3.2055+ 1			1.8922+ 2				2.7662- 3
5.0000+ 0 ~ 6.0000+ 0	9.2825+ 0	9.5578+ 0				4.0475+ 0			8.2522+ 1				2.7662- 3
6.0000+ 0 ~ 7.0000+ 0	4.1908+ 0	1.0561+ 1				2.4313+ 0			2.8976+ 2				2.7662- 3
7.0000+ 0 ~ 8.0000+ 0	1.0775+ 2	1.0155+ 1				1.0654+ 0			3.1103+ 1				2.7662- 3
1.0000+ 1 ~ 1.5000+ 1	1.5522+ 2	1.3235+ 1				5.3289+ 0			1.0125+ 2				2.7662- 3
1.5000+ 1 ~ 2.0000+ 1	6.4922+ 1	1.1112+ 1				3.0377+ 1			6.7650+ 1				2.7662- 3
2.0000+ 1 ~ 3.0000+ 1	3.0857+ 1	1.2067+ 1				2.3982+ 1			5.3170+ 1				2.7662- 3
3.0000+ 1 ~ 4.0000+ 1	4.1744+ 1	1.1136+ 1				1.6570+ 1			5.6833+ 1				2.7662- 3
4.0000+ 1 ~ 5.0000+ 1	5.1087+ 1	1.1486+ 1				1.2339+ 1			4.3987+ 1				2.7662- 3
5.0000+ 1 ~ 6.0000+ 1	3.7038+ 1	1.2700+ 1				1.5035+ 1			4.5987+ 1				2.7662- 3
6.0000+ 1 ~ 7.0000+ 1	6.6532+ 1	1.5619+ 1				1.9740+ 1			3.9816+ 1				2.7662- 3
7.0000+ 1 ~ 8.0000+ 1	3.7604+ 1	1.2656+ 1				3.1020+ 1			2.4789+ 1				2.7662- 3
1.0000+ 2 ~ 2.0000+ 2	3.5093+ 1	1.2622+ 1				2.4456+ 1			2.5817+ 1				2.7662- 3
2.0000+ 2 ~ 3.0000+ 2	2.8975+ 1	1.2893+ 1				1.7958+ 1			1.7642+ 1				2.7662- 3
3.0000+ 2 ~ 4.0000+ 2	2.7258+ 1	1.2629+ 1				1.4821+ 1			1.4401+ 1				2.7662- 3
4.0000+ 2 ~ 5.0000+ 2	2.6374+ 1	1.2760+ 1				1.3636+ 1			1.3227+ 1				2.7662- 3
5.0000+ 2 ~ 6.0000+ 2	2.9577+ 1	1.2624+ 1				9.7325+ 2			9.8451+ 0				2.7662- 3
6.0000+ 2 ~ 7.0000+ 2	3.1010+ 1	1.2578+ 1				5.6837+ 2			8.3751+ 0				2.7662- 3
7.0000+ 2 ~ 8.0000+ 2	1.8900+ 1	1.2557+ 1				5.7357+ 2			7.1853+ 0				2.7662- 3
1.0000+ 3 ~ 2.0000+ 3	1.8378+ 1	1.2361+ 1				4.5789+ 2			5.9150+ 0				2.7662- 3
2.0000+ 3 ~ 3.0000+ 3	1.7405+ 1	1.2218+ 1				4.2652+ 2			4.2106+ 0				2.7662- 3
3.0000+ 3 ~ 4.0000+ 3	1.6265+ 1	1.2032+ 1				4.2670+ 2			4.2106+ 0				2.7662- 3
4.0000+ 3 ~ 5.0000+ 3	1.5516+ 1	1.1823+ 1				6.7123+ 2			3.6258+ 0				2.7662- 3
5.0000+ 3 ~ 6.0000+ 3	1.6196+ 1	1.1749+ 1				2.4408+ 2			3.3527+ 0				2.7662- 3
6.0000+ 3 ~ 7.0000+ 3	1.4859+ 1	1.1578+ 1				1.6437+ 2			2.6153+ 0				2.7662- 3
7.0000+ 3 ~ 8.0000+ 3	1.3776+ 1	1.1325+ 1				1.4047+ 2			2.4367+ 0				2.7662- 3
1.0000+ 4 ~ 2.0000+ 4	1.3514+ 1	1.1191+ 1				1.4206+ 2			2.2267+ 0				2.7662- 3
2.0000+ 4 ~ 3.0000+ 4	1.3081+ 1	1.1064+ 1				1.4707+ 2			2.1577+ 0				2.7662- 3
3.0000+ 4 ~ 4.0000+ 4	1.3051+ 1	1.0901+ 1				1.5953+ 2			1.17436+ 0				2.7662- 3
4.0000+ 4 ~ 5.0000+ 4	1.2768+ 1	1.0893+ 1				1.5844+ 2			1.5015+ 0				2.7662- 3
5.0000+ 4 ~ 6.0000+ 4	1.2301+ 1	1.0300+ 1				1.5484+ 2			1.5015+ 0				2.7662- 3
6.0000+ 4 ~ 7.0000+ 4	1.1712+ 1	9.7350+ 0				2.2445+ 2			1.2775+ 0				2.7662- 3
7.0000+ 4 ~ 8.0000+ 4	1.0913+ 1	9.6547+ 0				2.3159+ 2			1.2775+ 0				2.7662- 3
1.0000+ 5 ~ 2.0000+ 5	6.7487+ 0	6.0487+ 0				7.5802+ 1			6.9755+ 1				2.7662- 3
2.0000+ 5 ~ 3.0000+ 5	6.4493+ 0	6.1955+ 0				4.0434+ 1			6.0962+ 1				2.7662- 3
3.0000+ 5 ~ 4.0000+ 5	7.6274+ 0	5.1956+ 0				1.6543+ 0			6.0962+ 1				2.7662- 3
4.0000+ 5 ~ 5.0000+ 5	7.2556+ 0	4.2451+ 0				1.9542+ 0			2.2004+ 1				2.7662- 3
5.0000+ 5 ~ 6.0000+ 5	9.0014+ 0	3.5089+ 0				1.9542+ 0			1.2057+ 1				2.7662- 3
6.0000+ 5 ~ 7.0000+ 5	7.3550+ 0	4.1315+ 0				2.0273+ 0			4.9854+ 2				2.7662- 3
7.0000+ 5 ~ 8.0000+ 5	7.6897+ 0	4.7812+ 0				2.0273+ 0			1.2656+ 2				2.7662- 3
1.0000+ 6 ~ 2.0000+ 6	7.7395+ 0	4.3457+ 0				2.3141+ 0			2.1193+ 1				2.7662- 3
2.0000+ 6 ~ 3.0000+ 6	6.8752+ 0	4.0207+ 0				2.3141+ 0			1.1793+ 1				2.7662- 3
3.0000+ 6 ~ 4.0000+ 6	6.0734+ 0	3.2057+ 0				2.7854+ 0			9.5233+ 1				2.7662- 3
4.0000+ 6 ~ 5.0000+ 6	5.7403+ 0	2.7657+ 0				2.7000+ 0			1.6901+ 0				2.7662- 3
5.0000+ 6 ~ 6.0000+ 6	5.0000+ 7	2.5000+ 7				2.5870+ 0			2.5719+ 0				2.7662- 3
6.0000+ 6 ~ 7.0000+ 6	2.0000+ 7	2.0000+ 7											2.7662- 3

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CROSS SECTION

MATERIAL	ENERGY	TOTAL	ELASTIC	INELR	(N,2N)	(N,3N)	FISSTON	(N,NA)	(N,NP)	(N,PI)	(N,DI)	(N,R)	MU-SRR
1.0000+	5	2.3468+ 4	1.1440+ 1			6.4751+ 9							2.7780- 9
1.0000+	1	0.092+ 3	1.1440+ 1			9.0074+ 3							2.7780- 9
1.0000+	2	0.000+ 0	1.1440+ 1			2.6315+ 3							2.7780- 9
1.0000+	3	0.000+ 0	1.1440+ 1			1.440+ 1							2.7780- 9
1.0000+	4	0.000+ 0	1.1440+ 1			1.7900+ 3							2.7780- 9
1.0000+	5	0.000+ 0	1.1440+ 1			1.5771+ 3							2.7780- 9
1.0000+	6	0.000+ 0	1.1440+ 1			1.2654+ 3							2.7780- 9
1.0000+	7	0.000+ 0	1.1440+ 1			1.1182+ 3							2.7780- 9
1.0000+	8	0.000+ 0	1.1440+ 1			9.4889+ 3							2.7780- 9
1.0000+	9	0.000+ 0	1.1440+ 1			6.0084+ 3							2.7780- 9
1.0000+	10	0.000+ 0	1.1440+ 1			7.4785+ 3							2.7780- 9
1.0000+	11	0.000+ 0	1.1440+ 1			6.6865+ 3							2.7780- 9
1.0000+	12	0.000+ 0	1.1440+ 1			2.9846+ 3							2.7780- 9
1.0000+	13	0.000+ 0	1.1440+ 1			5.5583+ 3							2.7780- 9
1.0000+	14	0.000+ 0	1.1440+ 1			1.2975+ 3							2.7780- 9
1.0000+	15	0.000+ 0	1.1440+ 1			7.2454+ 3							2.7780- 9
1.0000+	16	0.000+ 0	1.1440+ 1			6.2581+ 3							2.7780- 9
1.0000+	17	0.000+ 0	1.1440+ 1			1.2422+ 3							2.7780- 9
1.0000+	18	0.000+ 0	1.1440+ 1			1.2418+ 3							2.7780- 9
1.0000+	19	0.000+ 0	1.1440+ 1			1.2411+ 3							2.7780- 9
1.0000+	20	0.000+ 0	1.1440+ 1			1.2402+ 3							2.7780- 9
1.0000+	21	0.000+ 0	1.1440+ 1			1.2402+ 3							2.7780- 9
1.0000+	22	0.000+ 0	1.1440+ 1			1.2399+ 3							2.7780- 9
1.0000+	23	0.000+ 0	1.1440+ 1			1.2391+ 3							2.7780- 9
1.0000+	24	0.000+ 0	1.1440+ 1			1.2378+ 3							2.7780- 9
1.0000+	25	0.000+ 0	1.1440+ 1			1.2354+ 3							2.7780- 9
1.0000+	26	0.000+ 0	1.1440+ 1			1.2337+ 3							2.7780- 9
1.0000+	27	0.000+ 0	1.1440+ 1			1.2331+ 3							2.7780- 9
1.0000+	28	0.000+ 0	1.1440+ 1			1.2322+ 3							2.7780- 9
1.0000+	29	0.000+ 0	1.1440+ 1			1.2310+ 3							2.7780- 9
1.0000+	30	0.000+ 0	1.1440+ 1			1.2295+ 3							2.7780- 9
1.0000+	31	0.000+ 0	1.1440+ 1			1.2277+ 3							2.7780- 9
1.0000+	32	0.000+ 0	1.1440+ 1			1.7447+ 3							2.7811- 9
1.0000+	33	0.000+ 0	1.1440+ 1			1.4628+ 3							2.7811- 9
1.0000+	34	0.000+ 0	1.1440+ 1			1.6866+ 3							2.7811- 9
1.0000+	35	0.000+ 0	1.1440+ 1			9.6947+ 3							2.7811- 9
1.0000+	36	0.000+ 0	1.1440+ 1			6.8736+ 3							2.7811- 9
1.0000+	37	0.000+ 0	1.1440+ 1			9.0086+ 3							2.7811- 9
1.0000+	38	0.000+ 0	1.1440+ 1			7.1860+ 3							2.7811- 9
1.0000+	39	0.000+ 0	1.1440+ 1			1.2249+ 3							2.7811- 9
1.0000+	40	0.000+ 0	1.1440+ 1			1.2218+ 3							2.7811- 9
1.0000+	41	0.000+ 0	1.1440+ 1			1.2191+ 3							2.7811- 9
1.0000+	42	0.000+ 0	1.1440+ 1			1.2165+ 3							2.7811- 9
1.0000+	43	0.000+ 0	1.1440+ 1			1.2105+ 3							2.7811- 9
1.0000+	44	0.000+ 0	1.1440+ 1			1.2074+ 3							2.7811- 9
1.0000+	45	0.000+ 0	1.1440+ 1			1.2093+ 3							2.7811- 9
1.0000+	46	0.000+ 0	1.1440+ 1			1.1988+ 3							2.7811- 9
1.0000+	47	0.000+ 0	1.1440+ 1			1.1930+ 3							2.7811- 9
1.0000+	48	0.000+ 0	1.1440+ 1			1.1854+ 3							2.7811- 9
1.0000+	49	0.000+ 0	1.1440+ 1			1.1762+ 3							2.7811- 9
1.0000+	50	0.000+ 0	1.1440+ 1			1.1661+ 3							2.7811- 9
1.0000+	51	0.000+ 0	1.1440+ 1			1.1578+ 3							2.7811- 9
1.0000+	52	0.000+ 0	1.1440+ 1			1.1509+ 3							2.7811- 9
1.0000+	53	0.000+ 0	1.1440+ 1			1.1429+ 3							2.7811- 9
1.0000+	54	0.000+ 0	1.1440+ 1			1.1324+ 3							2.7811- 9
1.0000+	55	0.000+ 0	1.1440+ 1			1.1249+ 3							2.7811- 9
1.0000+	56	0.000+ 0	1.1440+ 1			1.1174+ 3							2.7811- 9
1.0000+	57	0.000+ 0	1.1440+ 1			1.1094+ 3							2.7811- 9
1.0000+	58	0.000+ 0	1.1440+ 1			1.1015+ 3							2.7811- 9
1.0000+	59	0.000+ 0	1.1440+ 1			1.0936+ 3							2.7811- 9
1.0000+	60	0.000+ 0	1.1440+ 1			1.0857+ 3							2.7811- 9
1.0000+	61	0.000+ 0	1.1440+ 1			1.0778+ 3							2.7811- 9
1.0000+	62	0.000+ 0	1.1440+ 1			1.0699+ 3							2.7811- 9
1.0000+	63	0.000+ 0	1.1440+ 1			1.0620+ 3							2.7811- 9
1.0000+	64	0.000+ 0	1.1440+ 1			1.0541+ 3							2.7811- 9
1.0000+	65	0.000+ 0	1.1440+ 1			1.0462+ 3							2.7811- 9
1.0000+	66	0.000+ 0	1.1440+ 1			1.0383+ 3							2.7811- 9
1.0000+	67	0.000+ 0	1.1440+ 1			1.0304+ 3							2.7811- 9
1.0000+	68	0.000+ 0	1.1440+ 1			1.0225+ 3							2.7811- 9
1.0000+	69	0.000+ 0	1.1440+ 1			1.0146+ 3							2.7811- 9
1.0000+	70	0.000+ 0	1.1440+ 1			1.0067+ 3							2.7811- 9
1.0000+	71	0.000+ 0	1.1440+ 1			9.9888+ 3							2.7811- 9
1.0000+	72	0.000+ 0	1.1440+ 1			9.9709+ 3							2.7811- 9
1.0000+	73	0.000+ 0	1.1440+ 1			9.9530+ 3							2.7811- 9
1.0000+	74	0.000+ 0	1.1440+ 1			9.9351+ 3							2.7811- 9
1.0000+	75	0.000+ 0	1.1440+ 1			9.9172+ 3							2.7811- 9
1.0000+	76	0.000+ 0	1.1440+ 1			9.8993+ 3							2.7811- 9
1.0000+	77	0.000+ 0	1.1440+ 1			9.8814+ 3							2.7811- 9
1.0000+	78	0.000+ 0	1.1440+ 1			9.8635+ 3							2.7811- 9
1.0000+	79	0.000+ 0	1.1440+ 1			9.8456+ 3							2.7811- 9
1.0000+	80	0.000+ 0	1.1440+ 1			9.8277+ 3							2.7811- 9
1.0000+	81	0.000+ 0	1.1440+ 1			9.8098+ 3							2.7811- 9
1.0000+	82	0.000+ 0	1.1440+ 1			9.7919+ 3							2.7811- 9
1.0000+	83	0.000+ 0	1.1440+ 1			9.7740+ 3							2.7811- 9
1.0000+	84	0.000+ 0	1.1440+ 1			9.7561+ 3							2.7811- 9
1.0000+	85	0.000+ 0	1.1440+ 1			9.7382+ 3							2.7811- 9
1.0000+	86	0.000+ 0	1.1440+ 1			9.7203+ 3							2.7811- 9
1.0000+	87	0.000+ 0	1.1440+ 1			9.7024+ 3							2.7811- 9
1.0000+	88	0.000+ 0	1.1440+ 1			9.6845+ 3							2.7811- 9
1.0000+	89	0.000+ 0	1.1440+ 1			9.6666+ 3							2.7811- 9
1.0000+	90	0.000+ 0	1.1440+ 1			9.6487+ 3							2.7811- 9
1.0000+	91	0.000+ 0	1.1440+ 1			9.6308+ 3							2.7811- 9
1.0000+	92	0.000+ 0	1.1440+ 1			9.6129+ 3							2.7811- 9
1.0000+	93	0.000+ 0	1.1440+ 1			9.5950+ 3							2.7811- 9
1.0000+	94	0.000+ 0	1.1440+ 1			9.5771+ 3							2.7811- 9
1.0000+	95	0.000+ 0	1.1440+ 1			9.5592+ 3							2.7811-

AM-242 M

CROSS SECTION

MATERIAL -2953

1.0000-5	1.0000-2	2.1388-4	TOTAL	ELASTIC	INELR	(N,2N)	(N,3N)	FISION	(N,NP)	(N,MP)	CAPTURE	(N,P)	(N,D)	(N,A)	MU-SAB
1.0000-5	1.0000-2	2.1388-4	1.0000-5	6.5220-0	0.0000-0	1.7802-4	1.7802-4	3.6796-3	1.7802-4	1.7802-4	3.6796-3	1.7802-4	1.7802-4	1.7802-4	2.7780-3
1.0000-4	1.0000-1	1.0518-3	1.0518-3	5.6737-0	0.0000-0	0.7471-3	0.7471-3	1.6511-3	0.7471-3	0.7471-3	1.6511-3	0.7471-3	0.7471-3	0.7471-3	2.7780-3
1.0000-3	1.0000-0	9.1719-2	9.1719-2	5.6549-0	0.0000-0	0.0000-0	0.0000-0	1.5952-2	0.0000-0	0.0000-0	1.5952-2	0.0000-0	0.0000-0	0.0000-0	2.7780-3
1.0000-2	1.0000-0	7.2659-2	7.2659-2	6.9307-0	0.0000-0	6.7051-2	6.7051-2	1.2263-2	0.0000-0	0.0000-0	1.2263-2	0.0000-0	0.0000-0	0.0000-0	2.7780-3
1.0000-1	1.0000-0	6.8424-2	6.8424-2	7.0075-0	0.0000-0	5.8763-2	5.8763-2	1.5511-2	0.0000-0	0.0000-0	1.5511-2	0.0000-0	0.0000-0	0.0000-0	2.7780-3
1.0000-0	1.0000-0	6.6089-2	6.6089-2	7.2228-0	0.0000-0	5.4790-2	5.4790-2	1.0254-2	0.0000-0	0.0000-0	1.0254-2	0.0000-0	0.0000-0	0.0000-0	2.7780-3
1.0000-0	1.0000-0	6.4488-2	6.4488-2	8.4112-0	0.0000-0	5.3161-2	5.3161-2	1.0994-2	0.0000-0	0.0000-0	1.0994-2	0.0000-0	0.0000-0	0.0000-0	2.7780-3
1.0000-0	1.0000-0	6.4223-2	6.4223-2	1.0395-1	0.0000-0	5.3667-2	5.3667-2	1.1167-2	0.0000-0	0.0000-0	1.1167-2	0.0000-0	0.0000-0	0.0000-0	2.7780-3
1.0000-0	1.0000-0	6.4938-2	6.4938-2	1.9848-1	0.0000-0	5.0390-2	5.0390-2	1.0504-2	0.0000-0	0.0000-0	1.0504-2	0.0000-0	0.0000-0	0.0000-0	2.7780-3
1.0000-0	1.0000-0	6.1032-2	6.1032-2	1.6508-1	0.0000-0	3.4726-2	3.4726-2	3.4105-2	0.0000-0	0.0000-0	3.4105-2	0.0000-0	0.0000-0	0.0000-0	2.7780-3
1.0000-0	1.0000-0	4.1623-2	4.1623-2	1.9729-1	0.0000-0	1.5338-2	1.5338-2	2.1777-2	0.0000-0	0.0000-0	2.1777-2	0.0000-0	0.0000-0	0.0000-0	2.7780-3
1.0000-0	1.0000-0	2.3923-2	2.3923-2	1.9729-1	0.0000-0	1.1336-2	1.1336-2	2.2762-2	0.0000-0	0.0000-0	2.2762-2	0.0000-0	0.0000-0	0.0000-0	2.7780-3
1.0000-0	1.0000-0	1.3741-2	1.3741-2	1.9729-1	0.0000-0	8.9904-2	8.9904-2	1.5902-2	0.0000-0	0.0000-0	1.5902-2	0.0000-0	0.0000-0	0.0000-0	2.7780-3
1.0000-0	1.0000-0	1.0718-2	1.0718-2	1.3175-1	0.0000-0	5.5043-2	5.5043-2	6.1735-2	0.0000-0	0.0000-0	6.1735-2	0.0000-0	0.0000-0	0.0000-0	2.7780-3
1.0000-0	1.0000-0	6.6511-2	6.6511-2	1.0304-1	0.0000-0	4.3960-2	4.3960-2	3.7350-2	0.0000-0	0.0000-0	3.7350-2	0.0000-0	0.0000-0	0.0000-0	2.7780-3
1.0000-0	1.0000-0	4.6946-2	4.6946-2	1.2626-1	0.0000-0	3.6326-2	3.6326-2	3.9919-2	0.0000-0	0.0000-0	3.9919-2	0.0000-0	0.0000-0	0.0000-0	2.7780-3
1.0000-0	1.0000-0	2.9291-2	2.9291-2	1.2474-1	0.0000-0	2.6348-2	2.6348-2	2.7022-2	0.0000-0	0.0000-0	2.7022-2	0.0000-0	0.0000-0	0.0000-0	2.7780-3
1.0000-0	1.0000-0	2.8721-2	2.8721-2	1.4231-1	0.0000-0	3.4095-2	3.4095-2	3.5837-2	0.0000-0	0.0000-0	3.5837-2	0.0000-0	0.0000-0	0.0000-0	2.7780-3
1.0000-0	1.0000-0	3.2738-2	3.2738-2	1.1559-1	0.0000-0	2.7935-2	2.7935-2	3.4926-2	0.0000-0	0.0000-0	3.4926-2	0.0000-0	0.0000-0	0.0000-0	2.7780-3
1.0000-0	1.0000-0	3.5931-2	3.5931-2	1.1378-1	0.0000-0	1.9439-2	1.9439-2	1.6422-2	0.0000-0	0.0000-0	1.6422-2	0.0000-0	0.0000-0	0.0000-0	2.7801-3
1.0000-0	1.0000-0	1.1274-2	1.1274-2	1.1480-1	0.0000-0	6.3642-2	6.3642-2	1.1642-2	0.0000-0	0.0000-0	1.1642-2	0.0000-0	0.0000-0	0.0000-0	2.7874-3
1.0000-0	1.0000-0	1.5301-2	1.5301-2	1.1512-1	0.0000-0	1.5223-2	1.5223-2	1.6293-2	0.0000-0	0.0000-0	1.6293-2	0.0000-0	0.0000-0	0.0000-0	2.7883-3
1.0000-0	1.0000-0	1.5811-2	1.5811-2	1.1537-1	0.0000-0	7.4722-2	7.4722-2	8.2265-2	0.0000-0	0.0000-0	8.2265-2	0.0000-0	0.0000-0	0.0000-0	2.7883-3
1.0000-0	1.0000-0	1.4297-2	1.4297-2	1.4497-1	0.0000-0	4.4255-2	4.4255-2	5.3476-2	0.0000-0	0.0000-0	5.3476-2	0.0000-0	0.0000-0	0.0000-0	2.8047-3
1.0000-0	1.0000-0	1.5691-2	1.5691-2	1.4711-1	0.0000-0	6.4295-2	6.4295-2	5.2328-2	0.0000-0	0.0000-0	5.2328-2	0.0000-0	0.0000-0	0.0000-0	2.8156-3
1.0000-0	1.0000-0	1.6896-2	1.6896-2	1.4522-1	0.0000-0	6.4619-2	6.4619-2	5.3889-2	0.0000-0	0.0000-0	5.3889-2	0.0000-0	0.0000-0	0.0000-0	2.8370-3
1.0000-0	1.0000-0	1.8450-2	1.8450-2	1.5178-1	0.0000-0	5.6521-2	5.6521-2	6.3689-2	0.0000-0	0.0000-0	6.3689-2	0.0000-0	0.0000-0	0.0000-0	2.8570-3
1.0000-0	1.0000-0	1.5768-2	1.5768-2	1.1478-1	0.0000-0	4.0592-2	4.0592-2	3.7020-2	0.0000-0	0.0000-0	3.7020-2	0.0000-0	0.0000-0	0.0000-0	2.8750-3
1.0000-0	1.0000-0	1.1479-2	1.1479-2	1.1479-1	0.0000-0	3.8268-2	3.8268-2	3.7020-2	0.0000-0	0.0000-0	3.7020-2	0.0000-0	0.0000-0	0.0000-0	2.8750-3
1.0000-0	1.0000-0	4.9271-2	4.9271-2	1.1474-1	0.0000-0	2.9607-2	2.9607-2	3.6451-2	0.0000-0	0.0000-0	3.6451-2	0.0000-0	0.0000-0	0.0000-0	2.8135-3
1.0000-0	1.0000-0	4.4911-2	4.4911-2	1.1488-1	0.0000-0	2.9584-2	2.9584-2	3.6451-2	0.0000-0	0.0000-0	3.6451-2	0.0000-0	0.0000-0	0.0000-0	2.8699-3
1.0000-0	1.0000-0	4.5091-2	4.5091-2	1.1509-1	0.0000-0	2.9722-2	2.9722-2	3.6509-2	0.0000-0	0.0000-0	3.6509-2	0.0000-0	0.0000-0	0.0000-0	2.8921-3
1.0000-0	1.0000-0	3.3857-2	3.3857-2	1.1490-1	0.0000-0	1.4932-2	1.4932-2	1.7206-2	0.0000-0	0.0000-0	1.7206-2	0.0000-0	0.0000-0	0.0000-0	2.9211-3
1.0000-0	1.0000-0	2.9252-2	2.9252-2	1.1468-1	0.0000-0	1.2711-2	1.2711-2	1.6513-2	0.0000-0	0.0000-0	1.6513-2	0.0000-0	0.0000-0	0.0000-0	2.9765-3
1.0000-0	1.0000-0	2.5252-2	2.5252-2	1.1468-1	0.0000-0	1.1750-2	1.1750-2	1.6259-2	0.0000-0	0.0000-0	1.6259-2	0.0000-0	0.0000-0	0.0000-0	2.9888-3
1.0000-0	1.0000-0	2.5963-2	2.5963-2	1.1484-1	0.0000-0	1.1261-2	1.1261-2	1.5590-2	0.0000-0	0.0000-0	1.5590-2	0.0000-0	0.0000-0	0.0000-0	2.9590-3
1.0000-0	1.0000-0	2.5963-2	2.5963-2	1.1484-1	0.0000-0	1.1261-2	1.1261-2	1.5590-2	0.0000-0	0.0000-0	1.5590-2	0.0000-0	0.0000-0	0.0000-0	2.9590-3
1.0000-0	1.0000-0	2.8200-2	2.8200-2	1.1752-1	0.0000-0	1.1752-2	1.1752-2	1.8167-2	0.0000-0	0.0000-0	1.8167-2	0.0000-0	0.0000-0	0.0000-0	2.8081-3
1.0000-0	1.0000-0	2.2254-2	2.2254-2	1.1658-1	0.0000-0	1.3662-2	1.3662-2	1.6093-2	0.0000-0	0.0000-0	1.6093-2	0.0000-0	0.0000-0	0.0000-0	2.8081-3
1.0000-0	1.0000-0	2.2104-2	2.2104-2	1.1558-1	0.0000-0	1.4934-2	1.4934-2	1.9822-2	0.0000-0	0.0000-0	1.9822-2	0.0000-0	0.0000-0	0.0000-0	2.8081-3
1.0000-0	1.0000-0	1.9888-2	1.9888-2	1.1486-1	0.0000-0	2.4496-2	2.4496-2	1.9920-2	0.0000-0	0.0000-0	1.9920-2	0.0000-0	0.0000-0	0.0000-0	2.8081-3
1.0000-0	1.0000-0	1.5873-2	1.5873-2	1.1418-1	0.0000-0	3.2717-2	3.2717-2	1.9920-2	0.0000-0	0.0000-0	1.9920-2	0.0000-0	0.0000-0	0.0000-0	2.8081-3
1.0000-0	1.0000-0	1.7590-2	1.7590-2	1.1219-1	0.0000-0	8.0335-2	8.0335-2	9.4837-2	0.0000-0	0.0000-0	9.4837-2	0.0000-0	0.0000-0	0.0000-0	2.8081-3
1.0000-0	1.0000-0	1.6482-2	1.6482-2	1.1066-1	0.0000-0	4.7033-2	4.7033-2	6.3711-2	0.0000-0	0.0000-0	6.3711-2	0.0000-0	0.0000-0	0.0000-0	1.4012-2
1.0000-0	1.0000-0	1.5648-2	1.5648-2	1.0855-1	0.0000-0	1.5649-2	1.5649-2	2.1999-2	0.0000-0	0.0000-0	2.1999-2	0.0000-0	0.0000-0	0.0000-0	1.8768-3
1.0000-0	1.0000-0	1.4598-2	1.4598-2	1.0830-1	0.0000-0	1.1511-2	1.1511-2	1.7175-2	0.0000-0	0.0000-0	1.7175-2	0.0000-0	0.0000-0	0.0000-0	2.5571-3
1.0000-0	1.0000-0	1.3900-2	1.3900-2	1.0897-1	0.0000-0	1.2047-2	1.2047-2	1.4326-2	0.0000-0	0.0000-0	1.4326-2	0.0000-0	0.0000-0	0.0000-0	2.5571-3
1.0000-0	1.0000-0	1.3453-2	1.3453-2	1.0692-1	0.0000-0	1.5844-2	1.5844-2	1.8246-2	0.0000-0	0.0000-0	1.8246-2	0.0000-0	0.0000-0	0.0000-0	2.5571-3
1.0000-0	1.0000-0	1.3033-2	1.3033-2	1.1433-1	0.0000-0	3.1433-2	3.1433-2	4.2546-2	0.0000-0	0.0000-0	4.2546-2	0.0000-0	0.0000-0	0.0000-0	2.5571-3
1.0000-0	1.0000-0	1.2581-2	1.2581-2	1.2127-1	0.0000-0	2.8484-2	2.8484-2	3.3502-2	0.0000-0	0.0000-0	3.3502-2	0.0000-0	0.0000-0	0.0000-0	1.2223-2
1.0000-0	1.0000-0	1.1956-2	1.1956-2	1.3214-1	0.0000-0	2.8424-2	2.8424-2	3.1933-2	0.0000-0	0.0000-0	3.1933-2	0.0000-0	0.0000-0	0.0000-0	1.6468-3
1.0000-0	1.0000-0	1.1037-2	1.1037-2	1.0056-1	0.0000-0	2.2713-2	2.2713-2	2.6400-2	0.0000-0	0.0000-0	2.6400-2	0.0000-0	0.0000-0	0.0000-0	2.18

CROSS SECTION

MATERIAL = 2954

RM-243

	ELASTIC	INELR	(N.2N)	(N.3N)	FISSION	(N.NP)	CAPTURE	(N.FI)	(N.D.)	(N.R)	MU-BRR
1.0000-5	1.0000+0	2.4682+2	7.5677+0	6.9421-1	2.3866+2	2.7436-3	2.7436-3				
1.0000-4	1.0000+0	1.1947+2	7.5629+0		1.1900+2	2.7436-3	1.1900+2				
1.0000-3	1.0000+0	1.0203+2	7.5630+0		1.0203+2	2.7436-3	1.0203+2				
1.0000-2	1.0000+0	9.5306+0	7.5631+0		9.5306+0	2.7436-3	9.5306+0				
1.0000-1	1.0000+0	6.7913+1	7.4881+0		6.7600+1	2.7436-3	6.7600+1				
1.0000-0	1.0000+0	6.2493+1	7.4679+0		5.4050+1	2.7436-3	5.4050+1				
1.0000-0	1.0000+0	6.6915+1	7.4375+0		4.8378+1	2.7436-3	4.8378+1				
1.0000-0	1.0000+0	6.1943+1	7.3965+0		4.4188+1	2.7436-3	4.4188+1				
1.0000-0	1.0000+0	4.6667+0	7.3229+0		3.9230+1	2.7436-3	3.9230+1				
1.0000-0	1.0000+0	4.2363+0	7.2117+0		3.5047+1	2.7436-3	3.5047+1				
1.0000-0	1.0000+0	3.8669+0	7.0417+0		3.2785+1	2.7436-3	3.2785+1				
1.0000-0	1.0000+0	4.6075+0	6.8773+0		2.8592+1	2.7436-3	2.8592+1				
1.0000-0	1.0000+0	4.3265+0	6.7240+0		2.6955+1	2.7436-3	2.6955+1				
1.0000-0	1.0000+0	5.2355+0	6.5844+0		2.5873+1	2.7436-3	2.5873+1				
1.0000-0	1.0000+0	1.1.8977+2	4.8732+0		1.3457+1	2.7436-3	1.3457+1				
1.0000-0	1.0000+0	0.4.393+3	0.4.393+3		0.3.0893+3	2.7436-3	0.3.0893+3				
1.0000-0	1.0000+0	2.2.772+2	2.1.772+2		1.6.694+2	2.7436-3	1.6.694+2				
1.0000-0	1.0000+0	2.7.965+2	1.1.263+1		1.6.648+2	2.7436-3	1.6.648+2				
1.0000-0	1.0000+0	1.7.732+2	1.0.942+1		1.8.401+2	2.7436-3	1.8.401+2				
1.0000-0	1.0000+0	1.3.196+2	0.8.8930+0		9.1.084+0	2.7436-3	9.1.084+0				
1.0000-0	1.0000+0	3.1.332+2	1.0.658+1		3.1.739+2	2.7436-3	3.1.739+2				
1.0000-0	1.0000+0	1.6.678+2	1.5.784+1		1.5.254+2	2.7436-3	1.5.254+2				
1.0000-0	1.0000+0	0.0.446+1	1.1.295+1		1.6.248+1	2.7436-3	1.6.248+1				
1.0000-0	1.0000+0	0.0.271+1	1.1.325+1		1.7.176+1	2.7436-3	1.7.176+1				
1.0000-0	1.0000+0	0.5.765+1	1.2.018+1		1.3.995+1	2.7436-3	1.3.995+1				
1.0000-0	1.0000+0	4.6.407+1	1.0.682+1		1.0.995+1	2.7436-3	1.0.995+1				
1.0000-0	1.0000+0	1.5.358+1	1.2.024+1		1.2.750+1	2.7436-3	1.2.750+1				
1.0000-0	1.0000+0	1.4.971+1	1.2.395+1		0.9.927+1	2.7436-3	0.9.927+1				
1.0000-0	1.0000+0	5.2.998+1	1.5.539+1		1.1.184+2	2.7436-3	1.1.184+2				
1.0000-0	1.0000+0	3.5.540+1	1.4.516+1		0.1.867+2	2.7436-3	0.1.867+2				
1.0000-0	1.0000+0	3.2.288+1	1.3.917+1		0.6.650+2	2.7436-3	0.6.650+2				
1.0000-0	1.0000+0	2.3.751+1	1.3.781+1		0.6.688+2	2.7436-3	0.6.688+2				
1.0000-0	1.0000+0	2.2.628+1	1.3.590+1		1.4.216+1	2.7436-3	1.4.216+1				
1.0000-0	1.0000+0	2.4.296+1	1.3.419+1		0.9.822+2	2.7436-3	0.9.822+2				
1.0000-0	1.0000+0	2.2.233+1	1.3.285+1		0.3.197+1	2.7436-3	0.3.197+1				
1.0000-0	1.0000+0	2.0.952+1	1.2.967+1		2.3.726+1	2.7436-3	2.3.726+1				
1.0000-0	1.0000+0	1.8.911+1	1.2.808+1		1.7.410+1	2.7436-3	1.7.410+1				
1.0000-0	1.0000+0	1.7.311+1	1.2.645+1		1.6.222+2	2.7436-3	1.6.222+2				
1.0000-0	1.0000+0	1.6.662+1	1.2.526+1		1.4.244+2	2.7436-3	1.4.244+2				
1.0000-0	1.0000+0	1.5.624+1	1.2.424+1		1.2.623+2	2.7436-3	1.2.623+2				
1.0000-0	1.0000+0	1.4.624+1	1.2.304+1		1.0.322+2	2.7436-3	1.0.322+2				
1.0000-0	1.0000+0	1.3.603+1	1.2.204+1		0.9.1667+3	2.7436-3	0.9.1667+3				
1.0000-0	1.0000+0	1.4.101+1	1.1.905+1		8.1.667+3	2.7436-3	8.1.667+3				
1.0000-0	1.0000+0	1.4.101+1	1.1.905+1		8.1.744+3	2.7436-3	8.1.744+3				
1.0000-0	1.0000+0	1.3.673+1	1.1.728+1		7.2.739+3	2.7436-3	7.2.739+3				
1.0000-0	1.0000+0	1.3.573+1	1.1.591+1		6.5.480+3	2.7436-3	6.5.480+3				
1.0000-0	1.0000+0	1.3.590+1	1.1.392+1		5.5.000+3	2.7436-3	5.5.000+3				
1.0000-0	1.0000+0	1.3.165+1	1.1.192+1		4.3.802+2	2.7436-3	4.3.802+2				
1.0000-0	1.0000+0	1.2.684+1	1.1.013+1		2.5.114+1	2.7436-3	2.5.114+1				
1.0000-0	1.0000+0	1.2.684+1	1.1.013+1		4.3.494+1	2.7436-3	4.3.494+1				
1.0000-0	1.0000+0	1.2.458+1	1.0.887+1		8.5.773+0	2.7436-3	8.5.773+0				
1.0000-0	1.0000+0	1.1.905+1	1.0.787+1		1.2.725+0	2.7436-3	1.2.725+0				
1.0000-0	1.0000+0	1.1.121+1	1.0.633+1		1.5.140+0	2.7436-3	1.5.140+0				
1.0000-0	1.0000+0	1.0.188+1	1.0.545+1		1.1.7861+0	2.7436-3	1.1.7861+0				
1.0000-0	1.0000+0	0.9.080+0	1.0.400+0		2.0.178+0	2.7436-3	2.0.178+0				
1.0000-0	1.0000+0	0.8.073+0	1.0.216+0		2.2.783+0	2.7436-3	2.2.783+0				
1.0000-0	1.0000+0	0.7.417+0	1.0.033+0		2.0.633+0	2.7436-3	2.0.633+0				
1.0000-0	1.0000+0	0.7.032+0	0.9.682+0		1.9.015+0	2.7436-3	1.9.015+0				
1.0000-0	1.0000+0	0.6.703+0	0.9.112+0		1.7.068+0	2.7436-3	1.7.068+0				
1.0000-0	1.0000+0	0.6.678+0	0.8.783+0		1.5.663+0	2.7436-3	1.5.663+0				
1.0000-0	1.0000+0	0.6.596+0	0.8.456+0		1.4.682+0	2.7436-3	1.4.682+0				
1.0000-0	1.0000+0	0.6.558+0	0.8.138+0		1.3.684+0	2.7436-3	1.3.684+0				
1.0000-0	1.0000+0	0.6.558+0	0.7.865+0		1.2.713+0	2.7436-3	1.2.713+0				
1.0000-0	1.0000+0	0.6.558+0	0.7.599+0		1.1.388+0	2.7436-3	1.1.388+0				
1.0000-0	1.0000+0	0.6.558+0	0.7.331+0		0.9.820+2	2.7436-3	0.9.820+2				
1.0000-0	1.0000+0	0.6.558+0	0.7.063+0		5.9319+1	2.7436-3	5.9319+1				
1.0000-0	1.0000+0	0.6.558+0	0.6.795+0		1.4.682+2	2.7436-3	1.4.682+2				
1.0000-0	1.0000+0	0.6.558+0	0.6.527+0		4.6895+3	2.7436-3	4.6895+3				
1.0000-0	1.0000+0	0.6.558+0	0.6.260+0		2.7.717+0	2.7436-3	2.7.717+0				
1.0000-0	1.0000+0	0.6.558+0	0.6.014+0		2.3.788+0	2.7436-3	2.3.788+0				
1.0000-0	1.0000+0	0.6.558+0	0.5.750+0		1.4.622+1	2.7436-3	1.4.622+1				
1.0000-0	1.0000+0	0.6.558+0	0.5.484+0		1.2.360+0	2.7436-3	1.2.360+0				
1.0000-0	1.0000+0	0.6.558+0	0.5.216+0		0.9.157+0	2.7436-3	0.9.157+0				

CM-242

CROSS SECTION

MATERIAL = 2861

ENERGY	TOTAL	ELASTIC	INEL.	(N.2N)	(N.3N)	(N.P)	(N.D)	(N.A)	RU-BAR
1.0000- 5	1.0000- 2	1.1620+ 1			1.5472+ 1	4.8846+ 1			2.7878- 9
1.0000- 4	1.5000- 2	1.1816+ 1			2.1896+ 0	1.3973+ 1			2.7888- 9
1.0000- 3	2.0000- 2	1.1908+ 1			5.1603+ 0	1.6180+ 0			2.7910- 9
1.0000- 2	3.0000- 2	1.1950+ 1			4.2714+ 0	1.3330+ 1			2.7916- 9
1.0000- 1	4.0000- 2	1.1959+ 1			3.7801+ 0	1.1911+ 1			2.7920- 9
5.0000- 2	5.0000- 2	1.1594+ 1			3.4359+ 0	0.9824+ 1			2.7932- 9
6.0000- 2	6.0000- 2	1.1586+ 1			2.8723+ 0	8.2238+ 0			2.7932- 9
8.0000- 2	1.0000- 1	1.1556+ 1			2.2676+ 0	6.8832+ 0			2.7937- 9
1.0000- 1	1.5000- 1	1.1533+ 1			1.9100+ 0	5.6243+ 0			2.7943- 9
1.5000- 1	2.0000- 1	1.1497+ 1			1.5947+ 0	4.3553+ 0			2.7943- 9
2.0000- 1	3.0000- 1	1.1451+ 1			1.2919+ 0	3.6553+ 0			2.7954- 9
3.0000- 1	4.0000- 1	1.1366+ 1			1.0718+ 0	3.0715+ 0			2.7958- 9
4.0000- 1	5.0000- 1	1.1308+ 1			9.5474+ 0	2.6477+ 0			2.7962- 9
6.0000- 1	8.0000- 1	1.1236+ 1			8.4182+ 1	2.1992+ 0			2.7966- 9
8.0000- 1	1.0000- 0	1.1074+ 1			7.1659+ 1	1.3318+ 0			2.7975- 9
1.0000- 0	1.5000- 0	1.0965+ 1			6.0351+ 1	9.4302+ 0			2.7981- 9
2.0000- 0	2.0000- 0	1.0818+ 1			5.0655+ 1	6.4488+ 0			2.7987- 9
3.0000- 0	3.0000- 0	1.0639+ 1			4.2979+ 1	4.3550+ 0			2.7993- 9
4.0000- 0	4.0000- 0	1.0489+ 1			3.7558+ 1	2.7495+ 0			2.8000- 9
5.0000- 0	5.0000- 0	1.0357+ 1			3.0181+ 1	2.4573+ 0			2.8000- 9
6.0000- 0	6.0000- 0	9.8682+ 0			2.6574+ 1	2.6956+ 1			2.8008- 9
8.0000- 0	1.0000- 2	1.5283+ 1			2.2622+ 1	1.0455+ 0			2.8011- 9
1.0000- 1	1.5000- 1	1.4795+ 1			1.8795+ 1	1.2080+ 0			2.8011- 9
1.5000- 1	2.0000- 1	1.4384+ 1			1.5026+ 1	1.2080+ 0			2.8015- 9
2.0000- 1	3.0000- 1	1.4066+ 1			1.1848+ 1	8.4311+ 0			2.8015- 9
3.0000- 1	4.0000- 1	1.3811+ 1			1.0682+ 1	2.6086+ 0			2.8031- 9
4.0000- 1	5.0000- 1	1.3597+ 1			1.0743+ 1	9.9781+ 0			2.8036- 9
5.0000- 1	6.0000- 1	1.3435+ 1			9.8372+ 2	9.9781+ 0			2.8036- 9
6.0000- 1	8.0000- 1	1.3278+ 1			8.4028+ 2	2.2012+ 1			2.8047- 9
8.0000- 1	1.0000- 2	1.3114+ 1			7.1555+ 2	1.4160+ 0			2.8157- 9
1.0000- 2	1.5000- 2	1.2919+ 1			6.0322+ 2	4.8324+ 0			2.8327- 9
1.5000- 2	2.0000- 2	1.2736+ 1			5.1405+ 1	1.4554+ 0			2.8503- 9
2.0000- 2	3.0000- 2	1.2581+ 1			4.2456+ 1	6.9737+ 0			2.8603- 9
3.0000- 2	4.0000- 2	1.2457+ 1			3.7459+ 1	6.0273+ 0			2.8643- 9
4.0000- 2	5.0000- 2	1.2357+ 1			3.2042+ 1	5.0884+ 0			2.8688- 9
5.0000- 2	6.0000- 2	1.2274+ 1			2.7043+ 1	5.0831+ 0			3.0597- 9
6.0000- 2	8.0000- 2	1.2204+ 1			1.9731+ 1	5.0831+ 0			3.0597- 9
8.0000- 2	1.0000- 3	1.2047+ 1			1.7601+ 1	4.2486+ 0			3.1599- 9
1.0000- 3	1.5000- 3	1.1922+ 1			1.5422+ 1	3.4120+ 0			3.3502- 9
1.5000- 3	2.0000- 3	1.1818+ 1			1.3741+ 1	3.8451- 9			3.8451- 9
2.0000- 3	3.0000- 3	1.1729+ 1			1.2186+ 1	2.2178+ 0			4.1196- 9
3.0000- 3	4.0000- 3	1.1653+ 1			1.0871+ 1	1.8528+ 0			4.8063- 9
4.0000- 3	5.0000- 3	1.1590+ 1			1.0300+ 1	1.6444+ 0			5.2334- 9
5.0000- 3	6.0000- 3	1.1537+ 1			9.5865+ 2	1.3753+ 0			5.7442- 9
6.0000- 3	8.0000- 3	1.1493+ 1			8.3387+ 2	1.2514+ 0			9.0611- 9
8.0000- 3	1.0000- 4	1.1365+ 1			7.6823+ 2	1.1210+ 0			1.1210- 9
1.0000- 4	1.5000- 4	1.1252+ 1			7.0822+ 2	9.5266+ 0			1.2576- 9
1.5000- 4	2.0000- 4	1.1151+ 1			6.2322+ 2	7.4830+ 0			2.3438- 9
2.0000- 4	3.0000- 4	1.1062+ 1			5.0341+ 2	6.5419+ 0			4.2997- 9
3.0000- 4	4.0000- 4	1.0983+ 1			4.5879+ 2	5.5237+ 0			5.3721- 9
4.0000- 4	5.0000- 4	1.0914+ 1			4.1731+ 2	4.5733+ 0			6.9523- 9
5.0000- 4	6.0000- 4	1.0854+ 1			3.8051+ 2	4.5723+ 0			9.0623- 9
6.0000- 4	8.0000- 4	1.0803+ 1			3.4822+ 2	3.7235+ 0			1.2341- 9
8.0000- 4	1.0000- 5	1.0668+ 1			3.1181+ 2	3.0172+ 1			1.6810- 9
1.0000- 5	1.5000- 5	1.0548+ 1			2.8084+ 2	2.5503+ 1			2.2311- 9
1.5000- 5	2.0000- 5	1.0439+ 1			2.5473+ 2	2.0503+ 1			2.8241- 9
2.0000- 5	3.0000- 5	1.0340+ 1			2.3311+ 2	1.6928+ 1			3.2541- 9
3.0000- 5	4.0000- 5	1.0251+ 1			2.1611+ 2	1.4141+ 1			3.6719- 9
4.0000- 5	5.0000- 5	1.0171+ 1			2.0239+ 2	1.2817+ 1			4.2677- 9
5.0000- 5	6.0000- 5	1.0100+ 1			1.9014+ 2	1.2016+ 1			4.8016- 9
6.0000- 5	8.0000- 5	1.0038+ 1			1.7909+ 2	1.1309+ 1			5.0809- 9
8.0000- 5	1.0000- 6	9.9801+ 0			1.6984+ 2	8.5217+ 0			5.7110- 9
1.0000- 6	1.5000- 6	9.9755+ 0			1.6244+ 2	7.2214+ 0			6.2733+ 9
1.5000- 6	2.0000- 6	9.9708+ 0			1.5644+ 2	6.0844+ 0			6.7231+ 9
2.0000- 6	3.0000- 6	9.9660+ 0			1.5144+ 2	5.0844+ 0			7.1828+ 9
3.0000- 6	4.0000- 6	9.9612+ 0			1.4714+ 2	4.2577+ 0			7.6700+ 9
4.0000- 6	5.0000- 6	9.9564+ 0			1.4344+ 2	3.5527+ 0			8.1188+ 9
5.0000- 6	6.0000- 6	9.9516+ 0			1.3994+ 2	2.9527+ 0			8.5137+ 9
6.0000- 6	8.0000- 6	9.9468+ 0			1.3754+ 2	2.4510+ 0			8.8617+ 9
8.0000- 6	1.0000- 7	9.9420+ 0			1.3524+ 2	2.0482+ 0			9.2468+ 9
1.0000- 7	1.5000- 7	9.9372+ 0			1.3304+ 2	1.7466+ 0			9.5548+ 9
1.5000- 7	2.0000- 7	9.9324+ 0			1.3094+ 2	1.4451+ 0			9.8248+ 9
2.0000- 7	3.0000- 7	9.9276+ 0			1.2894+ 2	1.1441+ 0			10.0548+ 9
3.0000- 7	4.0000- 7	9.9228+ 0			1.2704+ 2	8.7577+ 0			10.2468+ 9
4.0000- 7	5.0000- 7	9.9180+ 0			1.2524+ 2	7.4527+ 0			10.3988+ 9
5.0000- 7	6.0000- 7	9.9132+ 0			1.2354+ 2	6.2527+ 0			10.5137+ 9
6.0000- 7	8.0000- 7	9.9084+ 0			1.2194+ 2	5.1527+ 0			10.5987+ 9
8.0000- 7	1.0000- 8	9.9036+ 0			1.2044+ 2	4.1527+ 0			10.6548+ 9
1.0000- 8	1.5000- 8	9.8988+ 0			1.1894+ 2	3.2527+ 0			10.6909+ 9
1.5000- 8	2.0000- 8	9.8940+ 0			1.1744+ 2	2.4527+ 0			10.7110+ 9
2.0000- 8	3.0000- 8	9.8892+ 0			1.1594+ 2	1.7527+ 0			10.7231+ 9
3.0000- 8	4.0000- 8	9.8844+ 0			1.1444+ 2	1.1527+ 0			10.7282+ 9
4.0000- 8	5.0000- 8	9.8796+ 0			1.1294+ 2	0.6527+ 0			10.7303+ 9
5.0000- 8	6.0000- 8	9.8748+ 0			1.1144+ 2	0.1527+ 0			10.7303+ 9
6.0000- 8	8.0000- 8	9.8700+ 0			1.0994+ 2	0.1527+ 0			10.7303+ 9
8.0000- 8	1.0000- 9	9.8652+ 0			1.0844+ 2	0.1527+ 0			10.7303+ 9
1.0000- 9	1.5000- 9	9.8604+ 0			1.0694+ 2	0.1527+ 0			10.7303+ 9
1.5000- 9	2.0000- 9	9.8556+ 0			1.0544+ 2	0.1527+ 0			10.7303+ 9
2.0000- 9	3.0000- 9	9.8508+ 0			1.0394+ 2	0.1527+ 0			10.7303+ 9
3.0000- 9	4.0000- 9	9.8460+ 0			1.0244+ 2	0.1527+ 0			10.7303+ 9
4.0000- 9	5.0000- 9	9.8412+ 0			1.0094+ 2	0.1527+ 0			10.7303+ 9
5.0000- 9	6.0000- 9	9.8364+ 0			0.9944+ 2	0.1527+ 0			10.7303+ 9
6.0000- 9	8.0000- 9	9.8316+ 0			0.9794+ 2	0.1527+ 0			10.7303+ 9
8.0000- 9	1.0000- 10	9.8268+ 0			0.9644+ 2	0.1527+ 0			10.7303+ 9
1.0000- 10	1.5000- 10	9.8220+ 0			0.9494+ 2	0.1527+ 0			10.7303+ 9
1.5000- 10	2.0000- 10	9.8172+ 0			0.9344+ 2	0.1527+ 0			10.7303+ 9
2.0000- 10	3.0000- 10	9.8124+ 0			0.9194+ 2	0.1527+ 0			10.7303+ 9
3.0000- 10	4.0000- 10	9.8076+ 0			0.9044+ 2	0.1527+ 0			10.7303+ 9
4.0000- 10	5.0000- 10	9.8028+ 0			0.8894+ 2	0.1527+ 0			10.7303+ 9
5.0000- 10	6.0000- 10	9.7980+ 0			0.8744+ 2	0.1527+ 0			10.7303+ 9
6.0000- 10	8.0000- 10	9.7932+ 0			0.8594+ 2	0.1527+ 0			10.7303+ 9
8.0000- 10	1.0000- 11	9.7884+ 0			0.8444+ 2	0.1527+ 0			10.7303+ 9
1.0000- 11	1.5000- 11	9.7836+ 0			0.8294+ 2	0.1527+ 0			10.7303+ 9
1.5000- 11	2.0000- 11	9.7788+ 0			0.8144+ 2	0.1527+ 0			10.7303+ 9
2.0000- 11	3.0000- 11	9.7740+ 0			0.7994+ 2	0.1527+ 0			10.7303+ 9
3.0000- 11	4.0000- 11	9.7692+ 0			0.7844+ 2	0.1527+ 0			10.7303+ 9
4.0000- 11	5.0000- 11	9.7644+ 0			0.7694+ 2	0.1527+ 0			10.7303+ 9
5.0000- 11	6.0000- 11	9.7596+ 0			0.7544+ 2	0.1527+ 0			10.7303+ 9
6.0000- 11	8.0000- 11	9.7548+ 0			0.7394+ 2	0.1527+ 0			10.7303+ 9
8.0000- 11	1.0000- 12	9.7500+ 0			0.7244+ 2	0.1527+ 0			10.7303+ 9
1.0000- 12	1.5000- 12	9.7452+ 0			0.7094+ 2	0.1527+ 0			10.7303+ 9
1.5000- 12	2.0000- 12	9.7404+ 0			0.6944+ 2	0.1527+ 0			10.7303+ 9
2.0000- 12	3.0000- 12	9.7356+ 0			0.6794+ 2	0.1527+ 0			10.7303+ 9
3.0000- 12	4.0000- 12	9.7308+ 0			0.6644+ 2	0.1527+ 0			10.7303+ 9
4.0000- 12									

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CROSS SECTION

MATERIAL = Z962

MATERIAL	ENERGY	TOTAL	ELASTIC	INELA	(N,2N)	(N,3N)	FISSION	(N,NA)	(N,NP)	(N,PT)	(N,D)	(N,A)	MU-BRR
1.0000+	5-1.0000-2	2.3311+3	9.7323+0				1.9007+3	4.2068+2					3.0846-9
1.0000-	1.5000-	1.0593+3	9.7044+0				8.6051+2	1.5051+2					3.1495-9
1.0000-	2.0000-	9.1093+0	9.6959+0				6.2162+2	1.3146+2					3.1677-9
2.0000-	3.0000-	6.5744+0	9.6827+0				5.2297+2	1.1060+2					3.2050-9
4.0000-	5.0000-	6.6714+0	9.6674+0				4.6198+2	9.6170+1					3.2209-9
5.0000-	6.0000-	5.1203+0	9.6525+0				4.1886+2	9.5248+1					3.2422-9
8.0000-	8.0000-	4.0544+0	9.6014+0				3.2890+2	6.4109+1					3.2558-9
1.0000+	1.5000-	3.4423+0	9.3223+0				2.6247+2	5.2452+1					3.2772-9
1.5000-	2.0000-	2.9677+0	9.1562+0				2.4434+2	4.2893+1					3.2916-9
2.0000-	3.0000-	2.6786+0	8.9528+0				2.2757+2	3.5106+1					3.3106-9
3.0000-	4.0000-	2.3386+0	8.6799+0				2.2403+2	3.3287+1					3.3287-9
4.0000-	5.0000-	2.0590+0	8.3560+0				1.9616+2	2.4043+1					3.3423-9
5.0000-	6.0000-	1.8271+0	8.1560+0				1.6615+2	2.2290+1					3.3521-9
8.0000-	8.0000-	1.4213+0	7.7194+0				2.5867+1	2.1726+1					3.3738-9
1.0000+	1.5000-	6.2610+0	6.5761+0				5.5318+2	6.6428+1					3.3970-9
1.5000-	2.0000-	4.5704+0	1.3009+0				9.7107+2	1.0157+2					3.4152-9
2.0000-	3.0000-	1.0304+0	1.7983+0				1.2836+2	2.1390+2					3.4322-9
3.0000-	4.0000-	6.0335+1	1.1646+0				5.6427+2	2.1924+2					3.4461-9
4.0000+	5.0000-	9.8992+2	1.1848+0				4.6785+2	1.6207+2					3.4661-9
5.0000+	6.0000-	2.5453+2	1.0703+1				2.9526+2	2.1845+1					3.4789-9
8.0000+	8.0000+	1.5623+2	1.0703+1				1.3984+2	3.1507+1					3.5033-9
1.0000+	1.5000+	3.9394+2	1.9123+1				2.4114+2	7.3877+1					3.5207-9
1.5000+	2.0000+	7.0865+1	1.4929+1				8.3976+1	1.8676+1					3.5390-9
2.0000+	3.0000+	1.2827+1	1.2732+1				3.2126+1	2.8197+1					3.5580-9
3.0000+	4.0000+	4.9921+1	1.2101+1				3.3609+1	6.0708+0					3.5762-9
5.0000+	6.0000+	6.8617+1	1.2219+1				4.1735+1	3.6934+0					3.5988-9
8.0000+	8.0000+	6.0090+1	1.2713+1				7.1470+1	4.3520+0					3.6211-9
1.0000+	1.5000+	5.0018+1	1.2478+1				4.3989+1	5.4092+0					3.6445-9
1.5000+	2.0000+	3.8280+1	1.2396+1				9.4006+1	3.6764+0					3.6677-9
2.0000+	3.0000+	3.8506+1	1.2293+1				2.4362+1	2.5660+0					3.6917-9
3.0000+	4.0000+	3.1139+1	1.2269+1				1.3424+1	2.8420+0					3.7160-9
4.0000+	5.0000+	3.0143+1	1.2282+1				1.0788+1	1.7424+0					3.7396-9
5.0000+	6.0000+	2.6676+1	1.2335+1				1.6410+1	1.6660+0					3.7644-9
8.0000+	8.0000+	2.8327+1	1.2337+1				1.5741+1	1.7018+0					3.7892-9
1.0000+	1.5000+	2.7361+1	1.2244+1				1.2123+1	1.9292+0					3.8133-9
1.5000+	2.0000+	2.6743+1	1.2198+1				1.0245+1	1.5313+0					3.8383-9
2.0000+	3.0000+	2.0086+1	1.2105+1				6.6644+0	1.2148+0					3.8633-9
3.0000+	4.0000+	1.9793+1	1.2072+1				7.3841+0	9.7305+0					3.8883-9
4.0000+	5.0000+	1.8931+1	1.2166+1				6.5607+0	7.3849+0					3.9133-9
5.0000+	6.0000+	1.8099+1	1.2166+1				5.0215+0	6.0854+0					3.9383-9
8.0000+	8.0000+	1.7289+1	1.1936+1				4.8873+0	6.4687+0					3.9633-9
1.0000+	1.5000+	1.6493+1	1.1593+1				4.3442+0	5.6517+0					3.9883-9
1.5000+	2.0000+	1.5617+1	1.1336+1				3.9570+0	4.8499+0					4.0133-9
2.0000+	3.0000+	1.4874+1	1.1079+1				3.1680+0	3.5309+0					4.0383-9
3.0000+	4.0000+	1.4241+1	1.0847+1				3.0475+0	3.0236+0					4.0633-9
4.0000+	5.0000+	1.3684+1	1.0720+1				2.9576+0	2.5265+0					4.0883-9
5.0000+	6.0000+	1.3058+1	1.0220+1	1.8855-2			2.9576+0	2.5265+0					4.1133-9
8.0000+	8.0000+	1.2617+1	9.8018+0	1.8512-2			2.8773+0	2.5265+0					4.1383-9
1.0000+	1.5000+	1.1989+1	1.15245+0				2.8162+0	1.8230+1					4.1633-9
1.5000+	2.0000+	1.1287+1	8.9161+0	0.4000-			2.7583+0	1.1890+1					4.1883-9
2.0000+	3.0000+	1.0435+1	7.9411+0	3.1429-1			2.6597+0	6.3459+0					4.2133-9
3.0000+	4.0000+	9.6568+0	6.4481+0	4.1359-1			2.5532+0	6.4402+0					4.2383-9
4.0000+	5.0000+	8.8823+0	5.7855+0	4.6959-1			2.4522+0	5.8422+0					4.2633-9
5.0000+	6.0000+	7.2687+0	4.9570+0	2.1217-1			2.3517+0	4.7716+0					4.2883-9
8.0000+	8.0000+	7.2186+0	4.0882+0	6.3601-1			2.2530+0	4.0689+0					4.3133-9
1.0000+	1.5000+	7.0196+0	3.7504+0	0.0422-1			2.1586+0	4.5245+0					4.3383-9
1.5000+	2.0000+	6.7591+0	3.2030+0	0.0296-1			2.0610+0	3.7856+0					4.3633-9
2.0000+	3.0000+	6.4623+0	2.6204+0	1.0220-1			1.9635+0	3.2762+0					4.3883-9
3.0000+	4.0000+	7.7658+0	4.6233+0	0.0099-1			1.8659+0	2.7667+0					4.4133-9
4.0000+	5.0000+	7.6198+0	4.5541+0	1.3829-2			1.7682+0	2.2572+0					4.4383-9
5.0000+	6.0000+	8.2833+0	3.8194+0	9.5190-2			1.6707+0	1.7474+0					4.4633-9
6.0000+	8.0000+	8.6846+0	2.5885+0	9.5190-2			1.5732+0	1.4033+0					4.4883-9
8.0000+	8.0000+	6.0246+0	1.9853+0	3.5300-1			1.4757+0	1.1033+0					4.5133-9
1.0000+	1.5000+	5.8571+0	3.5003+0	8.4138-1			1.3782+0	9.9843-2					4.5383-9
1.5000+	2.0000+	6.1860+0	2.9.0032+0	1.2251-1			1.2803+0	3.9843-2					4.5633-9
2.0000+	3.0000+	5.5117+0	2.3.0032+0	8.4138-1			1.1823+0	2.2286+0					4.5883-9
3.0000+	4.0000+	4.8474+0	1.7.0032+0	1.2251-1			1.0843+0	1.6562+0					4.6133-9
4.0000+	5.0000+	4.1831+0	1.1.0032+0	1.2251-1			9.9107+0	1.0843+0					4.6383-9
5.0000+	6.0000+	3.5188+0	4.5541+0	1.3829-2			8.2833+0	0.7474+0					4.6633-9
6.0000+	8.0000+	2.8543+0	3.8194+0	9.5190-2			6.6597+0	0.4033+0					4.6883-9
8.0000+	8.0000+	2.1903+0	2.5885+0	9.5190-2			5.0246+0	0.2200+0					4.7133-9
1.0000+	1.5000+	1.5200+0	1.9853+0	3.5300-1			3.3984+0	0.0000+0					4.7383-9
1.5000+	2.0000+	1.1860+0	1.4033+0	1.2251-1			2.7286+0	0.0000+0					4.7633-9
2.0000+	3.0000+	8.666-8	2.1162-8										4.7883-9
3.0000+	4.0000+	7.959-8	1.866-8										4.8133-9
4.0000+	5.0000+	7.252-8	1.616-8										4.8383-9
5.0000+	6.0000+	6.545-8	1.366-8										4.8633-9
6.0000+	8.0000+	5.838-8	1.116-8										4.8883-9
8.0000+	8.0000+	5.131-8	8.666-8										4.9133-9

CROSS SECTION

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MATERIAL	ENERGY	TOTAL	ELASTIC	INEL	(N,2N)	(N,3N)	FISSION	(N,NR)	(N,NP)	(N,PI)	(N,DI)	(N,R)	MU-BR
1.0000-	5 ~ 1.0000- 2	5.4988+ 1	8.5571+ 0				3.5654+ 0						2.7751- 5
1.0000-	1.5000- 0	2.8054+ 1	8.5844+ 0				1.6941+ 0						2.7758- 3
1.0000-	2.0000- 2	2.2478+ 0	8.5800+ 0				1.4644+ 0						2.7768- 3
1.0000-	3.0000- 2	1.5919+ 1	8.5655+ 0				1.0086+ 0						2.7799- 3
1.0000-	4.0000- 2	1.6419+ 1	8.5429+ 0				0.9188+ 0						2.7807- 3
1.0000-	5.0000- 2	1.7251+ 1	8.5394+ 0				0.9351+ 0						2.7813- 3
1.0000-	6.0000- 2	1.6344+ 1	8.5371+ 0				6.2657+ 0						2.7828- 3
1.0000-	1.5000- 1	1.3684+ 1	8.8149+ 0				5.3378+ 0						2.7858- 3
1.0000-	2.0000- 1	1.2559+ 1	8.5876+ 0				4.4941+ 0						2.7866- 3
1.0000-	3.0000- 1	1.3588+ 1	8.5571+ 0				3.7732+ 0						2.7869- 3
1.0000-	4.0000- 1	1.0247+ 1	8.5531+ 0				2.8059+ 0						2.7877- 3
1.0000-	5.0000- 1	9.8720+ 0	8.4188+ 0				2.5332+ 0						2.7883- 3
1.0000-	6.0000- 1	9.4801+ 0	8.4169+ 0				2.2512+ 0						2.7890- 3
1.0000-	1.5000+ 0	8.7039+ 0	8.2175+ 0				1.7122+ 0						2.7908- 3
1.0000-	2.0000+ 0	8.3388+ 0	8.0165+ 0				1.4765+ 0						2.7918- 3
1.0000-	3.0000+ 0	8.0041+ 0	5.6583+ 0				1.2918+ 0						2.7928- 3
1.0000-	4.0000+ 0	8.0348+ 0	5.0342+ 0				1.1992+ 0						2.7939- 3
1.0000-	5.0000+ 0	7.5628+ 0	4.1107+ 0				1.2632+ 0						2.7947- 3
1.0000-	6.0000+ 0	7.3628+ 0	5.2476+ 0				2.6839+ 0						2.7950- 3
1.0000-	7.0000+ 0	6.5355+ 0	3.3330+ 0				5.0758+ 0						2.7956- 3
1.0000+	1.5000+ 1	1.3856+ 1	1.1892+ 1				7.4188+ 2						2.7978- 3
1.0000+	2.0000+ 1	1.0250+ 1	1.4537+ 1				3.2458+ 0						2.7986- 3
1.0000+	3.0000+ 1	5.5578+ 0	1.2682+ 0				2.4310+ 0						2.7999- 3
1.0000+	4.0000+ 1	5.2322+ 0	9.1176+ 0				2.6728+ 0						2.8017- 3
1.0000+	5.0000+ 1	1.3249+ 1	8.8085+ 0				2.1155+ 0						2.8033- 3
1.0000+	6.0000+ 1	1.0145+ 1	7.9878+ 0				1.7829+ 0						2.8039- 3
1.0000+	7.0000+ 1	1.0000+ 2	8.3524+ 1				1.1858+ 0						2.8058- 3
1.0000-	2.0000+ 2	2.0083+ 1	1.1727+ 1				3.2297+ 0						2.8191- 3
1.0000-	3.0000+ 2	3.1455+ 1	1.7478+ 1				4.7794+ 0						2.8501- 3
1.0000-	4.0000+ 2	3.4808+ 1	2.3415+ 1				3.1689+ 0						2.8900- 3
1.0000-	5.0000+ 2	3.2229+ 1	2.2229+ 1				3.6192+ 0						2.9048- 3
1.0000-	6.0000+ 2	3.6592+ 1	2.6038+ 1				1.2208+ 0						3.1243- 3
1.0000-	7.0000+ 2	3.8847+ 1	2.7563+ 1				1.6050+ 0						3.2468- 3
1.0000-	8.0000+ 2	2.8847+ 1	2.3610+ 1				2.0033+ 0						3.4173- 3
1.0000+	1.5000+ 3	2.7529+ 1	1.8527+ 1				1.3631+ 0						4.2071- 3
1.0000+	2.0000+ 3	2.0014+ 1	1.7646+ 1				1.4370+ 0						4.5651- 3
1.0000+	3.0000+ 3	1.6568+ 1	1.6759+ 1				1.0513+ 0						6.0110- 3
1.0000+	4.0000+ 3	1.7201+ 1	1.6152+ 1				9.2787+ 0						7.1039- 3
1.0000+	5.0000+ 3	1.5559+ 1	1.5559+ 1				9.1451+ 0						7.1039- 3
1.0000+	6.0000+ 3	1.5970+ 1	1.4735+ 1				9.0350+ 0						8.2674- 3
1.0000+	7.0000+ 3	1.5970+ 1	1.4735+ 1				8.3004+ 0						1.2330- 3
1.0000+	8.0000+ 3	1.5255+ 1	1.4195+ 1				6.8421+ 0						1.6554- 3
1.0000+	9.0000+ 3	1.4620+ 1	1.3670+ 1				7.6059+ 0						2.4282- 3
1.0000+	1.0000+ 4	1.5570+ 1	1.2078+ 1				5.3773+ 0						3.3811- 3
1.0000+	2.0000+ 4	1.3150+ 1	1.2459+ 1				6.1044+ 0						4.5659- 3
1.0000+	3.0000+ 4	1.2455+ 1	1.2455+ 1				6.1229+ 0						5.6693- 3
1.0000+	4.0000+ 4	1.2455+ 1	1.2163+ 1				8.7440+ 2						6.7299- 3
1.0000+	5.0000+ 4	1.2455+ 1	1.1790+ 1				5.8408+ 0						8.4080- 3
1.0000+	6.0000+ 4	1.2455+ 1	1.1355+ 1				5.8162+ 0						1.0534- 1
1.0000+	7.0000+ 4	1.2097+ 1	1.1355+ 1				4.2637+ 0						1.9895- 1
1.0000+	8.0000+ 4	1.1536+ 1	1.0720+ 1				4.2637+ 0						1.8050- 1
1.0000+	9.0000+ 4	1.0938+ 1	9.9638+ 0				5.8695+ 0						2.3021- 1
1.0000+	1.0000+ 5	1.0103+ 1	9.0563+ 0				5.8765+ 0						2.5049- 1
1.0000+	2.0000+ 5	9.2830+ 0	8.0760+ 0				8.1390+ 0						3.6593- 1
1.0000+	3.0000+ 5	8.6531+ 0	8.0886+ 0				6.3309+ 0						4.1447- 1
1.0000+	4.0000+ 5	8.6531+ 0	6.5238+ 0				6.3122+ 0						4.7098- 1
1.0000+	5.0000+ 5	7.6572+ 0	6.1994+ 0				1.2913+ 0						4.7098- 1
1.0000+	6.0000+ 5	7.2521+ 0	4.7423+ 0				1.1669+ 0						5.1474- 1
1.0000+	7.0000+ 5	7.0529+ 0	4.3093+ 0				1.9376+ 0						5.6377- 1
1.0000+	8.0000+ 5	7.2055+ 0	4.2648+ 0				7.1191+ 0						6.8164- 1
1.0000+	9.0000+ 5	7.3781+ 0	4.5942+ 0				2.7040+ 0						7.2169- 1
1.0000+	1.0000+ 6	7.4768+ 0	4.7079+ 0				9.7179+ 0						7.7862- 1
1.0000+	2.0000+ 6	7.4548+ 0	4.6804+ 0				1.6809+ 0						8.1069- 1
1.0000+	3.0000+ 6	7.3732+ 0	4.6500+ 0				1.7309+ 0						8.7028- 1
1.0000+	4.0000+ 6	6.8784+ 0	4.0583+ 0				2.2626+ 0						8.8025- 1
1.0000+	5.0000+ 6	6.8784+ 0	4.0583+ 0				6.2142+ 0						8.8025- 1
1.0000+	6.0000+ 6	6.2304+ 0	3.4735+ 0				8.1248+ 0						8.5084- 1
1.0000+	7.0000+ 6	5.7134+ 0	1.0351- 2				8.1248+ 0						8.5703- 1
1.0000+	8.0000+ 6	5.2304+ 0	1.5523- 2				2.4089+ 0						8.7528- 1
1.0000+	9.0000+ 6	5.7134+ 0	1.5523- 2				2.4089+ 0						8.7528- 1

Appendix 3

Correction of Numerical Data

The corrections of errors found in JENDL-2 (Rev0) are described in this appendix. They are classified into two; one is correction commonly done for almost all nuclides and another done case by case.

Common corrections

1. Corrections of Angular Distributions of Secondary Neutrons

In the case of isotropic angular distributions, data are given in the center-of-mass system for almost all nuclides of JENDL-2 (Rev0), because that was considered to be physically correct. However, this representation is not convenient for data applications where the data in the laboratory system are required.

In JENDL-2 (Rev1), the angular distribution data of neutrons from multiparticle emission reactions are given in the laboratory system by assuming to be isotropic. In the case where the isotropic distributions in the center-of-mass system were given for the neutrons from inelastic scattering to continuum levels, the data were transformed into the laboratory system by

$$\frac{d\sigma}{d\Omega_L} = \frac{(1 + \gamma^2 + 2\gamma \cos\theta)^{3/2}}{|1 + \gamma \cos\theta|} \times \frac{d\sigma}{d\Omega_{CM}},$$

$$\gamma = \frac{1}{AWR} \sqrt{E_C / (E_C + Q)},$$

where E_C is an incident neutron energy in the center-of-mass system and AWR weight of a target nuclide in the neutron mass unit. A Q -value was assumed in this work to be

$$Q = -(E_{C,th} + E_C) / 2,$$

where $E_{C,th}$ is a threshold energy in the center-of-mass system. At energies near a threshold energy, γ is sometimes greater than 1.0. In such cases, isotropic distributions were assumed in the laboratory system. As a result of this calculation, it was found that the transformed distributions in the laboratory systems were almost the same as those in the center-of-mass system if their mass numbers were greater than 40. Therefore, the distributions calculated from the above equation were used for the nuclides lighter than or equal to calcium. For the others, the isotropic distributions were assumed in the laboratory system.

For some nuclides, the distributions were calculated with optical and statistical model code, CASTHY¹⁾. In such cases, the angular distributions of elastically and inelastically scattered neutrons were represented with Legendre expansion in the center-of-mass system. Only changed for these data were the flag of LCT from '2' to '1', i.e. from the center-of-mass to the laboratory systems, for the neutrons from inelastic scattering to continuum levels.

In the case where Legendre coefficients are given, the number of coefficients should be even according to the ENDF/B-IV rule. However, in JENDL-2 (Rev0), the number is sometimes odd. This problem was

automatically solved with CRECTJ5². By this correction, the number of elements of a transformation matrix became incorrect for some nuclides. In such cases, the transformation matrix was recalculated and replaced by CRECTJ5.

2. Q-values and Threshold Energies

Inconsistency between Q-values and threshold energies was found especially in the case of natural element data. The reason is that they were constructed from data of their isotopes and the same Q-values and threshold energies as those of isotope data were adopted even if AWR was replaced for natural element.

This inconsistency was removed for almost all cases by recalculating Q-values from threshold energies and AWR. It was considered that threshold energies should have been the same as those of JENDL-2 (Rev0) to keep the same curves as JENDL-2 (Rev0) cross sections.

3. Number of Energy Points of The Total Cross Section

In the complete evaluated data file in the ENDF/B format, energy points of the total cross section should cover all energies of partial cross sections. However, in JENDL-2 (Rev0), data of many nuclides do not satisfy this rule. For such data the total cross section was reconstructed as a sum of partial cross sections with CRECTJ5 by assuming that all cross section data in JENDL-2 (Rev0) were consistent one another. Therefore the results of summation were expected to reproduce completely the same total cross sections as JENDL-2 (Rev0). CRECTJ5 automatically selects energies where partial cross sections are given and which are needed to represent the results of summation within accuracy of 1.0 percent. In the case where inconsistency among cross sections were found and the reason was incorrect compilation of partial cross sections, correction of the partial cross sections was made first, and then the total cross section was recalculated with CRECTJ5.

Individual Corrections

In the remaining part of this appendix, the corrections made for each nuclide data are described except the corrections of angular distributions mentioned above.

1. Hydrogen (MAT=2011)

MF=2 was added to give the effective scattering radius which was estimated from the elastic scattering cross section of 20.44 barns at 0.0253 eV.

A transformation matrix of Legendre coefficients of elastically scattered neutrons was calculated and added with CRECTJ5.

2. Deuterium (MAT=2012)

MF=2 was added.

3. Lithium-6 (MAT=2031)

The Q-value and threshold energy of the $(n,2n\alpha)$ cross section were corrected. Q-values of the other threshold reactions were replaced with values calculated from threshold energies. The total cross section was recalculated from partial cross sections.

4. Lithium-7 (MAT=2032)

MF=2 was added. Q-values were modified to be consistent with threshold energies. A transformation matrix was replaced with that newly calculated by CRECTJ5.

5. Beryllium-9 (MAT=2041)

MF=2 was added. Q-values were modified. The total cross section was reconstructed from partial cross sections.

6. Boron-10 (MAT=2051)

The Q-values were calculated from threshold energies. The total cross section was reconstructed from partial cross sections.

7. Carbon-12 (MAT=2061)

The Q-values and threshold energies of MT=4, 51 and 107 had been inconsistent. The Q-values were modified by keeping the threshold energies.

8. Fluorine-19 (MAT=2091)

The nonelastic scattering cross section was deleted. The total cross section was recalculated from partial cross sections.

The maximum energies of MT=251 and angular distributions of secondary neutrons were not 20 MeV. Sugi did recalculation of these data by using CASTHY. In this revision, the calculated data by Sugi³⁾ were adopted for MT=251 and the angular distribution of elastically scattered neutrons. For MT's from 51 to 56, isotropic distributions in the center-of-mass system were assumed.

9. Sodium-23 (MAT=2111)

The Q-values and threshold energies of the $(n,2n)$ and (n,α) cross sections were replaced with correct values. The threshold energy of MT=52 was corrected to 2.16917 MeV. The double energy points of 1.5 MeV were found in the total and elastic scattering cross sections. The second energy was changed to 1.505 MeV. After then, the total cross

section was recalculated as a sum of partial cross sections.

10. Aluminium-27 (MAT=2131)

A transformation matrix of MT=2 in MF=4 was recalculated with CRECTJ5, because the number of elements was not correct.

The U value of energy distribution data for the (n,2n) reaction was modified.

11. Natural Silicon (MAT=2140)

The total cross section was reconstructed from partial cross sections. Q-values of threshold reactions were corrected to be consistent their threshold energies.

The transformation matrix of MT=2 in MF=4 was recalculated with CRECTJ5.

The U values of energy distribution data for the (n,2n) and inelastic scattering to continuum levels were modified.

12. Natural Calcium (MAT=2200)

The upper energy of the resonance region for ^{48}Ca was changed to 400 keV.

The total cross section was replaced with newly evaluated data from experimental data of Perey et al.⁴⁾ and Cierjacks⁵⁾ in the energy range from 400 keV to 5.0 MeV. This evaluation was made by Asami⁶⁾ by means of eye-guide method with NDES⁷⁾. The elastic scattering cross section was recalculated by subtracting partial cross sections from the total cross section.

Q-values were modified. By modification of Q-values, order of inelastic levels (MT=71, 72 and 73) became wrong. Their order was exchanged.

The transformation matrix was replaced with that newly calculated with CRECTJ5.

13. Calcium-40 (MAT=2201)

No modification was made except for angular distribution data.

14. Calcium-42 (MAT=2202)

No modification was made except for angular distribution data.

15. Calcium-43 (MAT=2203)

No modification was made except for angular distribution data.

16. Calcium-44 (MAT=2204)

No modification was made except for angular distribution data.

17. Calcium-46 (MAT=2205)

MF=2 was added to give an effective scattering radius. The total cross section was calculated as a sum of partial cross sections.

18. Calcium-48 (MAT=2206)

The upper boundary of the resonance region for ^{48}Ca was changed to 400 keV.

19. Scandium-45 (MAT=2211)

The Q-values of the (n,p) and (n, α) cross sections were modified. The cross section of 0.0 was inserted at 500 keV for the (n,p) cross section as an effective threshold energy. The total cross section was reconstructed from partial cross sections.

20. Vanadium-51 (MAT=2231)

The Q-values and threshold energy of the second inelastic level were modified from -320.1 keV and 326.336 keV to -929 keV and 947.394 keV, respectively. The Q-values of the (n,2n), (n,n' α), (n,n'p), (n,p), (n,d) and (n,t) were adjusted to their threshold energies. The non-elastic scattering cross section was deleted from JENDL-2. Background cross sections were corrected below 100 keV to avoid negative values of the elastic and total cross sections. The total and total inelastic cross sections were recalculated from partial cross sections.

21. Natural Chromium (MAT=2240)

The maximum energy of the elastic scattering cross section was 19 MeV in JENDL-2 (Rev0). Asami⁶⁾ recommended the elastic scattering cross section of 0.947782 barns and the total cross section of 2.16 barns at 20 MeV. These values were adopted for JENDL-2 (Rev1).

All Q-values were recalculated from threshold energies. After this modification, the order of the 35-th and 36-th inelastic levels became incorrect. The Q-values of these levels were given in JENDL-2 (Rev0) as follows.

35-th level (^{50}Cr 4-th level)	Q=-3.1611 MeV	$E_{\text{th}}=3.22494$ MeV
36-th level (^{52}Cr 7-th level)	Q=-3.1617 MeV	$E_{\text{th}}=3.22310$ MeV

In JENDL-2 (Rev1), the order of these two levels was exchanged and Q-values were adjusted as follows.

35-th level (^{52}Cr 7-th level)	Q=-3.16176 MeV	$E_{\text{th}}=3.22310$ MeV
36-th level (^{50}Cr 4-th level)	Q=-3.16357 MeV	$E_{\text{th}}=3.22494$ MeV

The total cross section was reconstructed from partial cross

sections.

22. Chromium-50 (MAT=2241)

The value of AWR in MF=2 was corrected. The total cross section was recalculated as a sum of partial cross sections.

23. Chromium-52 (MAT=2242)

The value of AWR in MF=2 was corrected. The interpolation of the (n,n'p) cross section was altered.

24. Chromium-53 (MAT=2243)

The value of AWR in MF=2 was corrected.

25. Chromium-54 (MAT=2244)

The value of AWR in MF=2 was corrected. The interpolation of the elastic scattering cross section was corrected. The total cross section was recalculated as a sum of partial cross sections.

26. Manganese-55 (MAT=2251)

In JENDL-2 (Rev0), the total cross section calculated with CASTHY was stored. On the other hand, the capture cross section was evaluated on the basis of experimental data and consisted of rather many energy points. To keep consistency among cross sections, the total cross section was recalculated for JENDL-2 (Rev1) as a sum of partial cross sections. The differences between the total cross sections of JENDL-2 (Rev0) and (Rev1) are small enough because the capture cross section is relatively small.

Angular distributions for the (n,2n), (n,n' α) and (n,n'p) reactions were newly added by assuming to be isotropic in the laboratory system.

27. Natural Iron (MAT=2260)

The values of AWR's for ^{56}Fe and ^{57}Fe in MF=2 were corrected.

The Q-values were adjusted to threshold energies. The total cross section was recalculated as a sum of partial cross sections.

28. Iron-54 (MAT=2261)

The effective scattering radius of 7.5 fm was replaced with that of 5.6 fm which was adopted for resonance parameters of natural iron.

Threshold energies were recalculated from Q-values and AWR. The interpolation was corrected for the elastic scattering cross section. The elastic scattering and capture cross sections at 250 keV (the upper boundary of the resonance region) were inserted by assuming to be 3.47

barns and 9.6 mb, respectively. The total and total inelastic scattering cross sections were calculated from partial cross sections.

The angular distribution data for elastically scattered neutrons had not been given at 20 MeV in JENDL-2 (Rev0). The same distribution as that at 15 MeV was assumed. The angular distribution of neutrons from the (n,2n) reaction was put by assuming isotropic distribution in the laboratory system. All angular distributions of inelastically scattered neutrons to discrete levels were replaced with isotropic distributions in the center-of-mass system, and those to continuum levels with isotropic distribution in the laboratory system.

29. Iron-56 (MAT=2262)

In JENDL-2 (Rev0), many background data points were given for the elastic scattering and negative data for the capture cross section. For JENDL-2 (Rev1), the negative resonance at -3.75 keV was taken away and the effective scattering radius was changed from 5.4 fm to 6.5 fm in order to reproduce the low energy total and capture cross sections and the total cross section around the 24-keV window. As a result of this correction, better fitting to experimental data of the total cross section was obtained even in high energy region. The calculated capture cross section at 0.0253 eV is somewhat greater than recommended value by Mughabghab et al. However no background correction was applied. As to the elastic scattering cross section, the calculated value is smaller on the contrary. The background data in a very simple form was given for this to reproduce 12.46 barns⁸⁾ at 0.0253 eV.

Threshold energies were recalculated from Q-values and AWR. The elastic scattering cross section at 250 keV (the upper boundary of the resonance region) was corrected to be 2.99 barns. The total and total inelastic scattering cross sections were calculated from partial cross sections.

The energy range of MF=4, MT=52 was corrected.

30. Iron-57 (MAT=2263)

The value of AWR was corrected and threshold energies were recalculated from Q-values and the corrected AWR. The cross section of MT=51 was modified around its threshold energy. Then the total and total inelastic scattering cross sections were reconstructed from partial cross sections.

31. Iron-58 (MAT=2264)

The background data for the capture cross section were not correct between 100 eV and 100 keV. They were modified by inserting the background capture cross section at 100 keV. The total cross section was recalculated.

The transformation matrix of MT=2 in MF=4 was recalculated with CRECTJ5.

32. Cobalt-59 (MAT=2271)

The resonance parameters were replaced with recommended data by Mughabghab et al.⁸⁾, because the parameters of JENDL-2 (Rev0) consisted of only big resonances of which neutron width was given by Mughabghab et al. and some unreasonable capture widths were also found. For JENDL-2 (Rev1), all resonances recommended by Mughabghab et al. were adopted. The resonances whose ℓ value was not given and whose neutron width was relatively large were assumed to be s-wave resonances. The capture widths of 0.56 eV and 0.7 eV were assumed for s-wave and p-wave resonances, respectively. The effective scattering radius and parameters of the negative resonance at -500 keV were adjusted to reproduce the thermal elastic scattering and capture cross sections recommended by Mughabghab et al. The changes of parameters were very small as follows.

R = 6.795 fm (from 6.8 fm)
 neutron width = 45.0 eV (from 47.75 eV)
 capture width = 0.473 eV (from 0.447 eV)

For the resonance formula, the multilevel Breit Wigner formula was applied.

The calculated total cross section is slightly smaller than experimental data about between 100 eV and 2 keV. No background correction was made for this, because the experimental data have some structure which seems to be contributions from other nuclides.

33. Natural Nickel (MAT=2280)

Q-values were recalculated from threshold energies. The total cross section was reconstructed.

Incorrect order of neutron energies of energy distributions of inelastic scattering to continuum levels was corrected.

34. Nickel-58 (MAT=2281)

The J value of 168.675-eV resonance was corrected. The value of AWR was corrected.

The (n,n' α) cross section at 18.5 MeV was slightly modified to reproduce a smooth curve. The total cross section was recalculated as a sum of partial cross sections.

35. Nickel-60 (MAT=2282)

Reconstruction of the total cross section was made.

36. Nickel-61 (MAT=2283)

Reconstruction of the total cross section was made.

37. Nickel 62 (MAT=2284)

Reconstruction of the total cross section was made.

38. Nickel-64 (MAT=2285)

Reconstruction of the total cross section was made.

39. Natural Copper (MAT=2290)

Q-values were replaced with values calculated from threshold energies.

The energy range of MT=16 of MF=4 and MF=5 was corrected to be consistent with the (n,2n) cross section data.

40. Copper-63 (MAT=2291)

The total cross section was recalculated.

The angular distributions of neutrons from the (n,2n) and (n,n' α) reactions were added by assuming to be isotropic in the laboratory system.

41. Copper-65 (MAT=2292)

The angular distributions of neutrons from the (n,2n) and (n,n' α) reactions were added by assuming to be isotropic in the laboratory system.

The energy range of MT=16 of MF=5 was corrected.

42. Niobium-93 (MAT=2411)

The total cross section was reconstructed from partial cross sections.

The value of AWR of MT=16 and MT=17 in MF=4 was modified.

Energy ranges of MT=16 and MT=17 in MF=5 were corrected.

43. Natural Molybdenum (MAT=2420)

The J value of the 4.622-keV resonance of ⁹⁴Mo was corrected.

The effective threshold energies were set at 144.7 keV and 1.0 MeV for the (n,p) and (n, α) cross sections, respectively. The Q-value of the (n,3n) cross section was corrected. Other Q-values were also corrected from their threshold energies. The total cross section was reconstructed from partial cross sections.

44. Molybdenum-92 (MAT=2421)

The effective threshold energies were set at 1.0 MeV for the (n,p) and (n, α) cross sections. The total cross section was recalculated.

45. Molybdenum-94 (MAT=2422)

The J value of the 4.622-keV resonance was corrected.

The cross section of 0.0 was inserted at 1.0 MeV for the (n, α)

cross section as an effective threshold energy. The Q-value of the (n,3n) cross section was modified. The total cross section was reconstructed from partial cross sections.

46. Molybdenum-95 (MAT=2423)

The cross section of 0.0 was inserted at 1.0 MeV for the (n, α) cross section as an effective threshold energy. The total cross section was reconstructed from partial cross sections.

47. Molybdenum-96 (MAT=2424)

The cross section of 0.0 was inserted at 1.0 MeV for the (n, α) cross section as an effective threshold energy. The total cross section was reconstructed from partial cross sections.

48. Molybdenum-97 (MAT=2425)

The cross section of 0.0 was inserted at 1.0 MeV for the (n, α) cross section as an effective threshold energy. The total cross section was reconstructed from partial cross sections.

49. Molybdenum-98 (MAT=2426)

The cross section of 0.0 was inserted at 1.0 MeV for the (n, α) cross section as an effective threshold energy. The total cross section was reconstructed from partial cross sections.

50. Molybdenum-100 (MAT=2427)

The cross section of 0.0 was inserted at 1.0 MeV for the (n, α) cross section as an effective threshold energy. The Q-value of the (n,p) cross section was corrected. The total cross section was reconstructed from partial cross sections.

51. Hafnium-174 (MAT=2721)

The total cross section was recalculated as a sum of partial cross sections.

52. Hafnium-176 (MAT=2722)

The total cross section was recalculated as a sum of partial cross sections.

53. Hafnium-177 (MAT=2723)

The total cross section was recalculated as a sum of partial cross

sections.

54. Hafnium-178 (MAT=2724)

The elastic scattering cross section in the thermal region did not reproduce the value of 5.0 barns at 0.0253 eV recommended by the evaluator of this nuclide. This was corrected by replacing the data with newly evaluated values. The background cross section was also added to the elastic scattering cross section to connect cross sections calculated from resonance parameters to the pointwise data below 0.5 eV. The total cross section was recalculated as a sum of partial cross sections.

55. Hafnium-179 (MAT=2725)

The total cross section was recalculated as a sum of partial cross sections.

56. Hafnium-180 (MAT=2726)

The total cross section was recalculated as a sum of partial cross sections.

57. Tantalum-181 (MAT=2731)

Large inconsistency was found between the total and partial cross sections in the energy range from 7 to 50 keV where is in the resonance region. The total cross section was recalculated as a sum of partial cross sections.

58. Natural Lead (MAT=2820)

The J values of 527.4-keV and 721.4-keV resonances of ^{208}Pb were incorrect. They were altered from p-wave to d-wave resonances.

The total cross section was replaced with the eye-guided values based on experimental data in the energy range from 500 keV to 15 MeV. The elastic scattering cross section was modified to keep consistency among cross sections.

Inconsistencies of energy ranges among MF=3, MF=4 and MF=5 were corrected.

59. Lead-204 (MAT=2821)

The interpolation tables of the total, elastic scattering and capture cross sections were corrected. The capture cross section at 50 keV (background cross section) was modified. After then, the total cross section was reconstructed from partial cross sections:

The first energy of secondary neutrons in MF=5, MI=22 was corrected.

60. Lead-206 (MAT=2822)

The total cross section was recalculated as a sum of partial cross sections.

The first energies of secondary neutrons of MT=22 and MT=91 in MF=5 were corrected.

61. Lead-207 (MAT=2823)

The interpolation of the elastic scattering cross section was corrected. The elastic scattering cross section was inserted at 500 keV where is an upper boundary of the resonance region. The total cross section was recalculated as a sum of partial cross sections.

The energy range of MT=22 in MF=5 was modified to be the same as that of the $(n,n'\alpha)$ cross section.

62. Lead-208 (MAT=2824)

The J values of 527.4-keV and 721.4-keV resonances were incorrect. They were changed from p-wave to d-wave resonances.

The total cross section was recalculated as a sum of partial cross sections.

The energy range of MT=22 in MF=5 was modified to be the same as that of the $(n,n'\alpha)$ cross section.

63. Thorium-228 (MAT=2901)

The resonance formula was changed to the multilevel Breit-Wigner formula, because negative elastic scattering cross sections were found from the JENDL-2 (Rev0).

The cross-section shape of the $(n,2n)$ and $(n,3n)$ cross sections were corrected to be the same curve as recommendation by Ohsawa who was an evaluator of this nuclide. Interpolation tables were modified for the elastic and capture cross sections. At 2 keV, two values were given for the elastic scattering and capture cross sections in JENDL-2 (Rev0); one was the evaluated value by Ohsawa and another calculated with CASTHY. For JENDL-2 (Rev1), Ohsawa's evaluated value was adopted at 2 keV to give a smooth curve for each cross section. The total and total inelastic scattering cross sections were reconstructed from partial cross sections.

The fission spectrum was added by assuming the Maxwellian spectrum determined from Z^2/A systematics by Smith et al⁹⁾.

64. Thorium-230 (MAT=2902)

The J values of resonance parameters were replaced with $J=1/2$ for all resonances. The effective scattering radius of 19.25 fm was corrected to be 10.925 fm. The resonance formula was changed to the multilevel Breit-Wigner formula to avoid negative elastic scattering cross sections. The background cross section of the capture cross section was recalculated as

$$\sigma_{(n,\gamma)}(E) = 0.257425 / \sqrt{E(\text{eV})}$$

to reproduce the recommended 0.0253-eV cross section by Ohsawa. The elastic scattering cross section calculated at 0.0253 eV is 9.77 barns and that recommended by Ohsawa is 9.403 barns. However no background cross section was applied, because no experimental data existed and the difference was not so large.

The interpolation tables were changed to be log-log between 564.26 eV and 4 keV. The cross sections at 4 keV were slightly modified so as to join to the values calculated with CASTHY above 4 keV. The curves of the (n,2n) and (n,3n) cross sections were corrected. The total cross section was finally recalculated from partial cross sections.

The fission spectrum was added by assuming the Maxwellian spectrum determined from Z^2/A systematics by Smith et al.

65. Thorium-232 (MAT=2903)

The total cross section was recalculated from partial cross sections.

66. Thorium-233 (MAT=2904)

Interpolation tables were modified for the elastic and capture cross sections. The cross sections at 4 keV were modified so as to join to the values calculated with CASTHY above 4 keV. The curves of the (n,2n) and (n,3n) cross sections were corrected. The total and total inelastic scattering cross section was recalculated from partial cross sections.

The fission spectrum was added by assuming the Maxwellian spectrum determined from Z^2/A systematics by Smith et al.

67. Thorium-234 (MAT=2905)

Interpolation tables were modified for the elastic and capture cross sections. The cross sections at 4 keV were modified so as to join to the values calculated with CASTHY above 4 keV. The curves of the (n,2n) and (n,3n) cross sections were corrected. The total and total inelastic scattering cross section was recalculated from partial cross sections.

The fission spectrum was added by assuming the Maxwellian spectrum determined from Z^2/A systematics by Smith et al.

68. Protactinium-233 (MAT=2911)

The energy boundary of the resolved and unresolved resonances were inconsistent in JENDL-2 (Rev0). The boundary of two ranges was set to 17.0 eV for JENDL-2 (Rev1).

Inconsistent energy ranges among MF's were corrected. The energy distributions of the (n,2n), (n,3n) and inelastic scattering to continuum levels were replaced with the results of EVAPSPEC⁽¹⁰⁾. The fission spectrum was added by assuming the Maxwellian spectrum determined from Z^2/A systematics by Smith et al.

69. Uranium-233 (MAT=2921)

The energy of 7.47 MeV in the total number of neutrons and number of prompt neutrons per fission was changed to 7.5 MeV.

The nonelastic scattering cross section given in JENDL-2 (Rev0) was deleted. The total and total inelastic scattering cross sections were reconstructed from partial cross sections.

The energy range of angular distributions of neutrons from fission was corrected.

70. Uranium-234 (MAT=2922)

The resonance formula was altered from the single-level Breit-Wigner to the multilevel Breit-Wigner formula. The background cross sections were replaced with zero values.

The Q-values of MT=19, 20 and 21 were set to be the same as that of MT=18. MF=5 data for MT=19, 20 and 21 were taken from those of MT=18.

Energy ranges of angular distribution data were corrected.

71. Uranium-235 (MAT=2923)

Interpolation of fission yield data was changed to linear-linear.

72. Uranium-236 (MAT=2924)

No modification was made except correction of angular distribution data.

73. Uranium-238 (MAT=2925)

Interpolation of fission yield data was changed to linear-linear.

Negative values were found in the angular distribution of elastically scattered neutrons for the incident neutron energy of 20 MeV. The same distribution as 18-MeV neutrons was used for 20-MeV neutrons to avoid this problem.

74. Neptunium-237 (MAT=2931)

The total cross section was reconstructed from partial cross sections. The energy ranges of energy distributions of neutrons from the (n,2n) and (n,3n) reactions were modified to be the same as their cross section data.

75. Neptunium-239 (MAT=2932)

The energy of 10^{-5} eV was inserted for the fission cross section.

The U value of fission spectrum was changed to -20 MeV. The energy spectra of neutrons from (n,2n), (n,3n) and inelastic scattering to

continuum levels were replaced with the results of EVAPSPEC¹⁰⁾.

76. Plutonium-236 (MAT=2941)

The Q-values of MT=19, 20 and 21 were set to be equal to that of MT=18. The threshold energies of MT=20 and 21 were modified to be 3 MeV and 11 MeV, respectively, and their cross sections around threshold energies were corrected. The total cross section was recalculated from partial cross sections.

The energy distribution data of MT=19, 20 and 21 were taken from those of MT=18.

77. Plutonium-238 (MAT=2942)

The neutron widths of the 2.9-eV and 32.2-eV resonances were modified. The fission widths of the -0.4-eV and 2.9-eV resonances were adjusted to reproduce the thermal fission cross section of 16.5 barns recommended in BNL-325 3rd edition. The resonance formula was changed to the multilevel Breit-Wigner formula in order to avoid negative cross sections.

The Q-values and threshold energies of the (n,2n) and (n,3n) cross sections were corrected. The (n,2n) cross section at 10 MeV was replaced with correct one. The total cross section was constructed from partial cross sections.

The angular distribution of elastically scattered neutrons by 20-MeV neutrons had negative values. The same distribution as 18-MeV neutrons was assumed at 20 MeV.

78. Plutonium-239 (MAT=2943)

The interpolation of fission yield data was changed to linear-linear. The Q-value of the total inelastic scattering cross section was slightly changed from -7.863 keV to -7.86 keV.

79. Plutonium-240 (MAT=2944)

The Q-values and threshold energies of all inelastic scattering cross sections were inconsistent in JENDL-2 (Rev0). The threshold energies were recalculated from their Q values. The total and total inelastic scattering cross sections were recalculated from partial cross sections.

The energy range of angular distribution data for the (n,2n) and (n,3n) reactions were corrected.

The energy distribution data were calculated with EVAPSPEC.

80. Plutonium-241 (MAT=2945)

The Q-values of the (n,2n), (n,3n) and (n,4n) cross sections were corrected.

81. Plutonium-242 (MAT=2946)

The threshold energies were slightly corrected to satisfy the relation between Q-values and threshold energies. The total and total inelastic scattering cross sections were calculated as a sum of partial cross sections.

82. Americium-241 (MAT=2951)

The fission yield data were renormalized to 2.0.

The Q-values were replaced with those calculated from threshold energies. The total cross section was reconstructed from partial cross sections.

The energy ranges of MF=4, MT=18 and MF=5, MT=16, 17 and 18 were corrected to be consistent with cross section data.

The evaporation spectra in MF=5 were recalculated with EVAPSPEC.

83. Americium-242 (MAT=2952)

The angular distribution of elastically scattered neutrons by 20-MeV neutrons had negative values. The same distribution as 18-MeV neutrons was assumed at 20 MeV.

84. Americium-242m (MAT=2953)

The elastic and capture cross sections around 3.5 eV were modified. The total cross section was reconstructed from partial cross sections.

The angular distribution of elastically scattered neutrons by 20-MeV neutrons had negative values. The same distribution as 18-MeV neutrons was assumed at 20 MeV.

The energy range of MF=5, MT=91 was corrected.

85. Americium-243 (MAT=2954)

The fission yield data were renormalized to 2.0.

The total cross section was reconstructed from partial cross sections.

The angular distribution of elastically scattered neutrons by 20-MeV neutrons had negative values. The same distribution as 14-MeV neutrons was assumed at 20 MeV. The energy range of MF=4, MT=18 was corrected to be consistent with cross section data.

86. Curium-242 (MAT=2961)

The angular distribution of elastically scattered neutrons at 20 MeV had negative values. The same distribution as 18-MeV neutrons was assumed at 20 MeV.

87. Curium-243 (MAT=2962)

The capture cross section of JENDL-2 (Rev0) was adopted by mistake to be the same as elastic scattering cross section in the energy range from 27 eV to 1 keV. It was replaced with the cross sections correctly estimated with the method described in Ref. 11. The total cross section was reconstructed from partial cross sections.

The angular distribution of elastically scattered neutrons at 20 MeV had negative values. The same distribution as 18-MeV neutrons was assumed at 20 MeV.

88. Curium-244 (MAT=2963)

The resonance formula was replaced with the multilevel Breit-Wigner formula to avoid negative cross sections. The background cross sections given in JENDL-2 (Rev0) were taken away.

The total cross section was recalculated as a sum of partial cross sections.

89. Curium-245 (MAT=2964)

The Q-value of the (n,2n) was corrected.

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