

JAERI - M

85-210

再冠水解析コードREFLA-1D/MODE4  
(REFLA-1D局所出力効果モデル・燃料棒半径方向  
温度分布モデル組込み版)コード・マニュアル

1986年1月

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編集兼発行 日本原子力研究所  
印 刷 いばらき印刷株

再冠水解析コード REFLA-1D/MODE 4 (REFLA-1D 局所出力効果  
モデル・燃料棒半径方向温度分布モデル組込み版) コード・マニュアル

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(1985年12月6日受理)

REFLA-1D/MODE 3 コードに局所出力効果モデルおよび燃料棒半径方向温度分布モデルの組込みを行い、これらの効果を考慮した解析が可能な REFLA-1D/MODE 4 コードを作成した。作成したコードでは、炉心内の水平方向出力分布効果を考慮した局所燃料棒温度変化の計算および実燃料棒の模擬等が可能となった。

本報告書には、組込んだモデルの概要、モデル組込みにともなう修正内容および作成した REFLA-1D/MODE 4 コード使用上の情報が含まれている。

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\* 科学技術庁

User's manual of the REFLA-1D/MODE4 reflood  
thermo-hydrodynamic analysis code

— Incorporation of local power effect model and fuel  
temperature profile effect model into REFLA-1D —

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REFLA-1D/MODE4 code has been developed by incorporating local power effect model and fuel temperature profile effect model into REFLA-1D/MODE3 code. This code can calculate the temperature transient of local rod by considering radial power profile effect in core and simulate the thermal characteristics of the nuclear fuel rod.

This manual describes the outline of incorporated models, modification of the code with incorporating models and provides application information required to utilize the code.

Keywords; PWR, LOCA, Reflood, Computer Code, Quench, Thermo-hydrodynamics, Heat Transfer, Two-phase Flow, Local Power Effect Model, Fuel Temperature Profile Effect Model

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## 1. 序

原研では、加圧水型原子炉における大破断冷却材喪失事故時再冠水過程の熱水力挙動の解析を目的として、REFLA コードを開発している。<sup>(1),(2)</sup>

今回、REFLA-1D/MODE 3 コードに局所出力効果モデル<sup>(3)</sup> および燃料棒半径方向温度分布モデル<sup>(4)</sup> の組込みを行い、これらの効果を考慮した解析が可能なバージョン REFLA-1D/MODE 4 を作成した。

局所出力効果モデルの特徴は、水平方向に出力分布が存在するような炉心に対しても、水力挙動は平均出力棒に関して 1 次元的に取扱い、また、熱的挙動は平均出力棒、局所出力棒に関して 1 次元的に取扱うことによって、1 次元コードでも、水平方向出力分布効果を考慮した局所出力棒の被覆管温度変化を平均出力棒のそれと同時に解析できる点にある。

燃料棒半径方向温度分布モデルは Malang による HETRAP コード<sup>(5)</sup> の手法を元に開発したものであり、本モデルの特徴は燃料棒半径方向の材質の違いやギャップの存在等が考慮でき、実燃料の模擬も可能な点にある。

本報告書には、局所出力効果モデルおよび燃料棒半径方向温度分布モデルの概要、モデル組込みにともなう修正内容、および作成した REFLA-1D/MODE 4 コード使用上の情報が含まれている。

## 2. 局所出力効果モデルの組込み

### 2.1 局所出力効果モデルの概要

局所出力効果モデルは、原研で実施した CCTF 試験結果から得られた知見に基づいて、以下の様な仮定をしたモデルである。<sup>(3)</sup>

- (1) 炉心内水平方向に出力分布および温度分布が存在しても、蓄水挙動は水平方向に分布がなく、軸方向に 1 次元的に取扱うことができる。この蓄水挙動は、平均出力、平均温度の燃料棒（以下、平均燃料棒と呼ぶ）に対する計算で予測できる。

この仮定は、各高さで水と蒸気が水平方向に瞬時に混合することを意味しており、局所出力、局所温度の燃料棒（以下、局所燃料棒と呼ぶ）付近の蓄水挙動も平均燃料棒に対する蓄水挙動と同じとなる。

- (2) 局所燃料棒各高さの熱伝達率は、平均燃料棒の同じ高さにおける水力条件（ボイド率、蒸気流速、水流速、蒸気温度、水温度等）とその高さの局所燃料棒の熱的条件（被覆管表面温度、出力、クエンチ点からの距離等）から決定される。
- (3) クエンチ進行は水平方向に関して 1 次元的ではない。局所燃料棒のクエンチ進行は、平均燃料棒の水力条件と局所燃料棒の熱的条件から決定される。

局所燃料棒の出力が平均燃料棒の出力より大きい場合の両者の炉心内流動様式を図 2.1 に示す。上記(1), (3)の仮定より、クエンチ進行以外の流動様式は両者同一である。平均燃料棒と局所燃料棒のクエンチ進行の違いにより、流動様式は以下に示す 3 つのタイプに分類できる。

- 1) タイプ 1：平均燃料棒、局所燃料棒とともにクエンチ点の流体は飽和温度に達している場合  
両燃料棒とも、クエンチ点下方は液単相流領域（またはサブクール核沸騰領域）、飽和二相流領域からなり、クエンチ点上方は遷移流領域、液滴流領域、過熱蒸気流領域からなる。
- 2) タイプ 2：平均燃料棒クエンチ点の流体は飽和温度に達しているが局所燃料棒のそれは飽和温度以下の場合

平均燃料棒の流動様式はタイプ 1 と同じ。局所燃料棒の流動様式は、クエンチ点下方は液単相流領域（またはサブクール核沸騰領域）、クエンチ点上方はサブクール膜沸騰領域、遷移流領域、液滴流領域、過熱蒸気流領域からなる。

- 3) タイプ 3：平均燃料棒、局所燃料棒とともにクエンチ点の流体は飽和温度以下の場合  
両燃料棒とも、タイプ 2 の局所燃料棒と同じ流動様式。

局所出力効果モデルを適用した場合の炉心内熱水力計算手順の概略を図 2.2 に示す。

### 2.2 局所出力効果モデル組込みにともなう修正

REFLA-1D/MODE 3 への局所出力効果モデル組込みにともなう主なプログラム修正内容を以下に示す。

- 1) 局所出力効果モデル適用時には、平均燃料棒、局所燃料棒それぞれについて炉心内熱水力計算を行うので、サブルーチン REFLA 1 のクエンチ計算および炉心内熱水力計算部分をサブルーチン REFLAA として独立させた。
- 2) ICALL = 1 の時は平均燃料棒、ICALL = 2 の時は局所燃料棒の計算を行うようにした。
- 3) 局所燃料棒のクエンチ点以外の各領域の境界は、平均燃料棒計算で得られた境界点をサブルーチン REFLAA で設定するようにした。  
局所燃料棒のクエンチ点については、サブルーチン REFLAA で計算する。
- 4) 各領域の熱水力計算を行うサブルーチン SINGLF, SATTPF, TRNSRM, DISPRM および SPHTRM には、局所燃料棒に対しては熱伝達率計算のみ行うロジックを付加えた。局所出力効果モデル組込みにともなって修正された主なサブルーチンのフローチャートを図 2.3 ~ 2.8 に示す。なお、サブルーチン REFLA 1 については、燃料棒半径方向温度分布モデルも組んだ後のフローチャートを図 3.3 に示す。

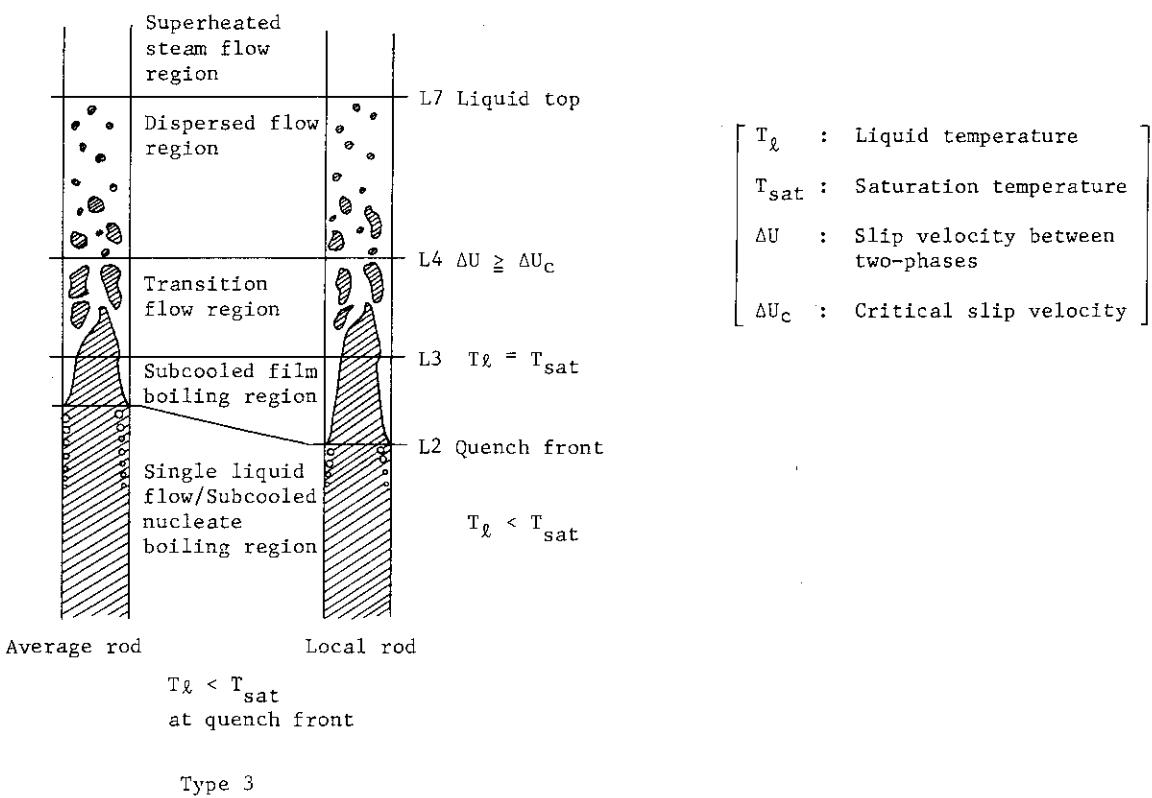
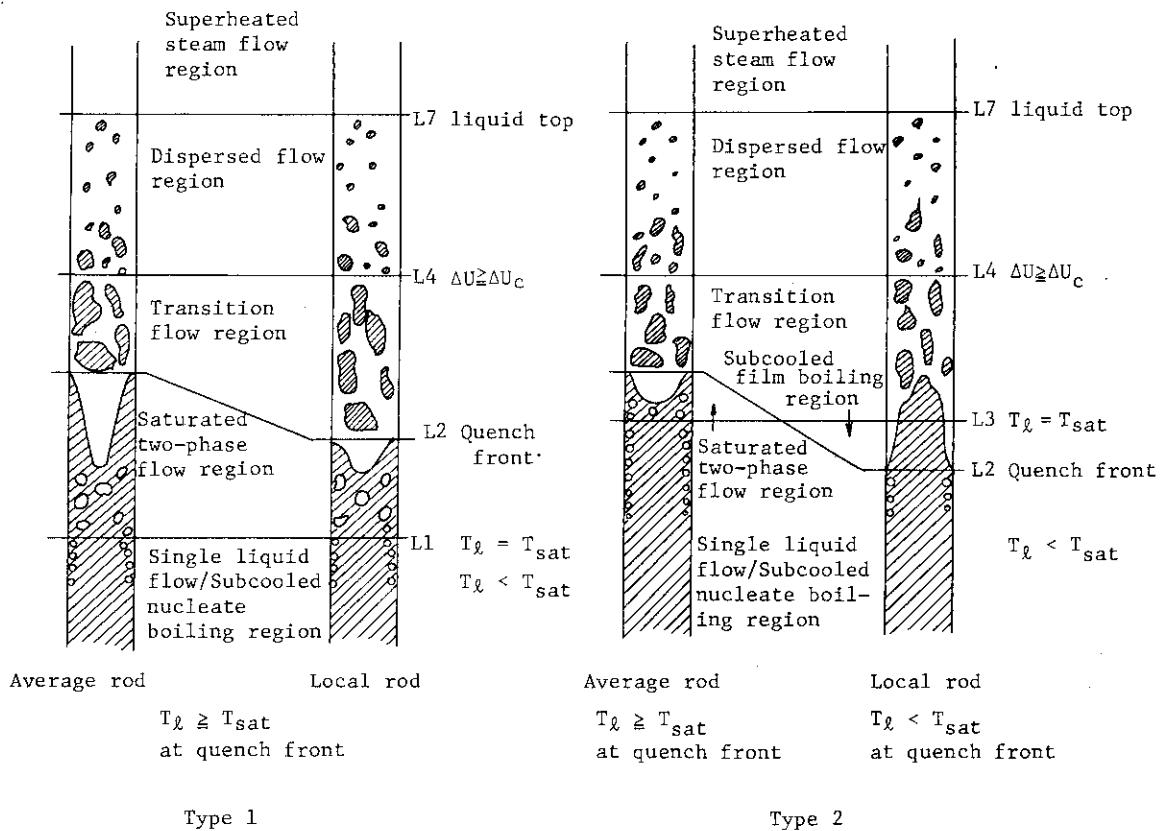


Fig. 2.1 Reflood flow model and definition of flow regime boundaries at average and local rod

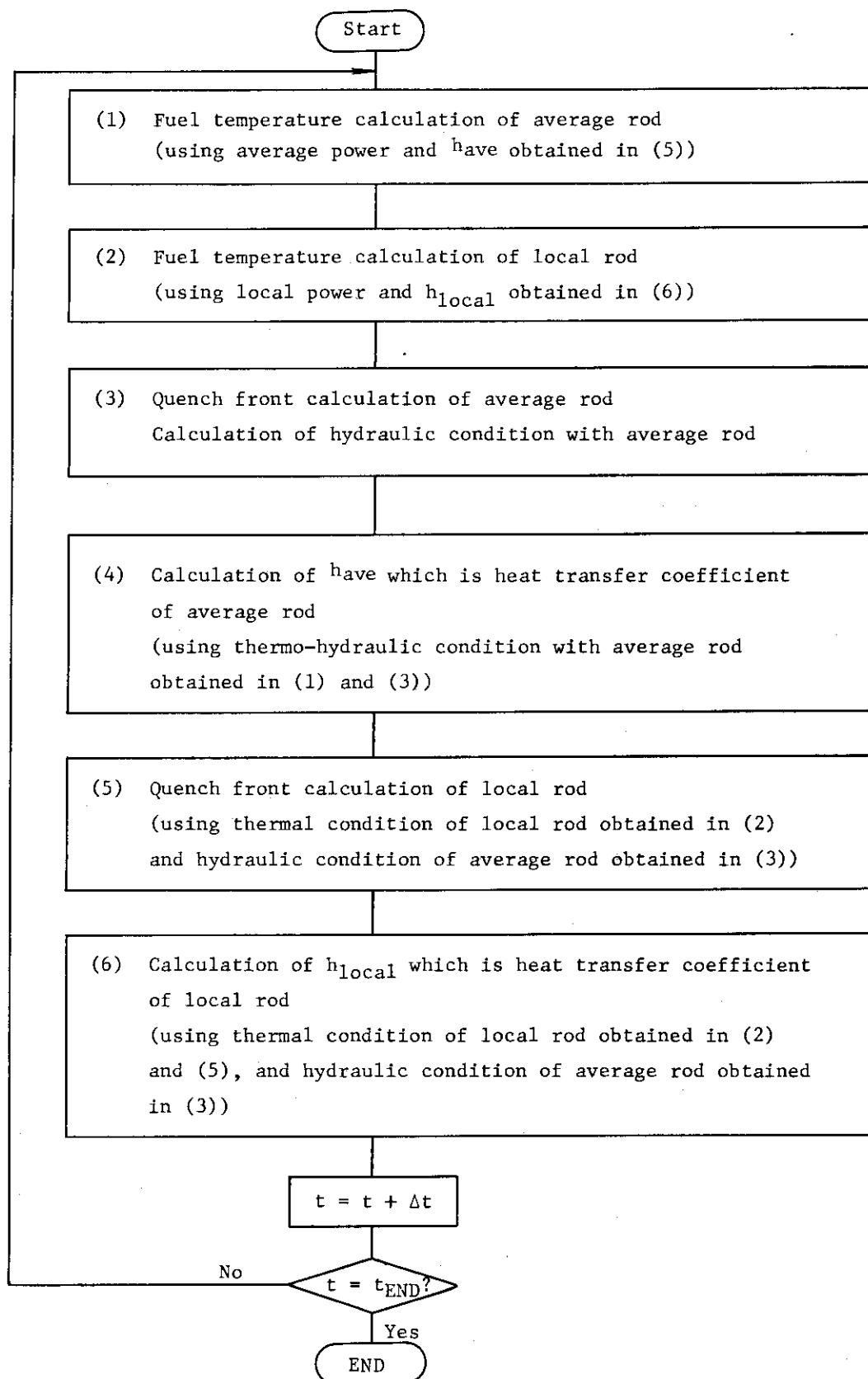


Fig. 2.2 Core thermo-hydraulic calculation procedure in case of using local power effect model

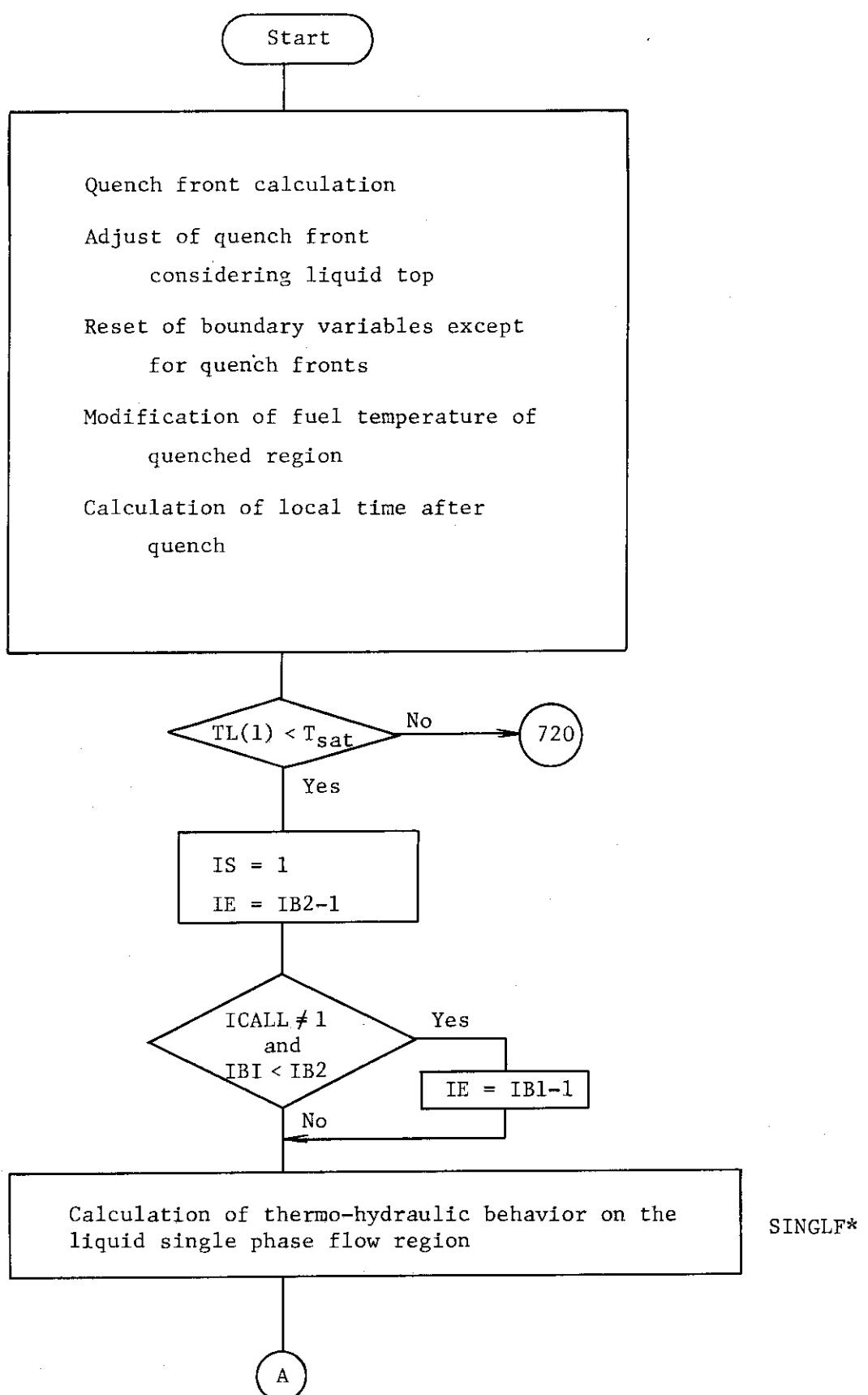


Fig. 2.3 Flow chart of subroutine REFLAA (1/5)

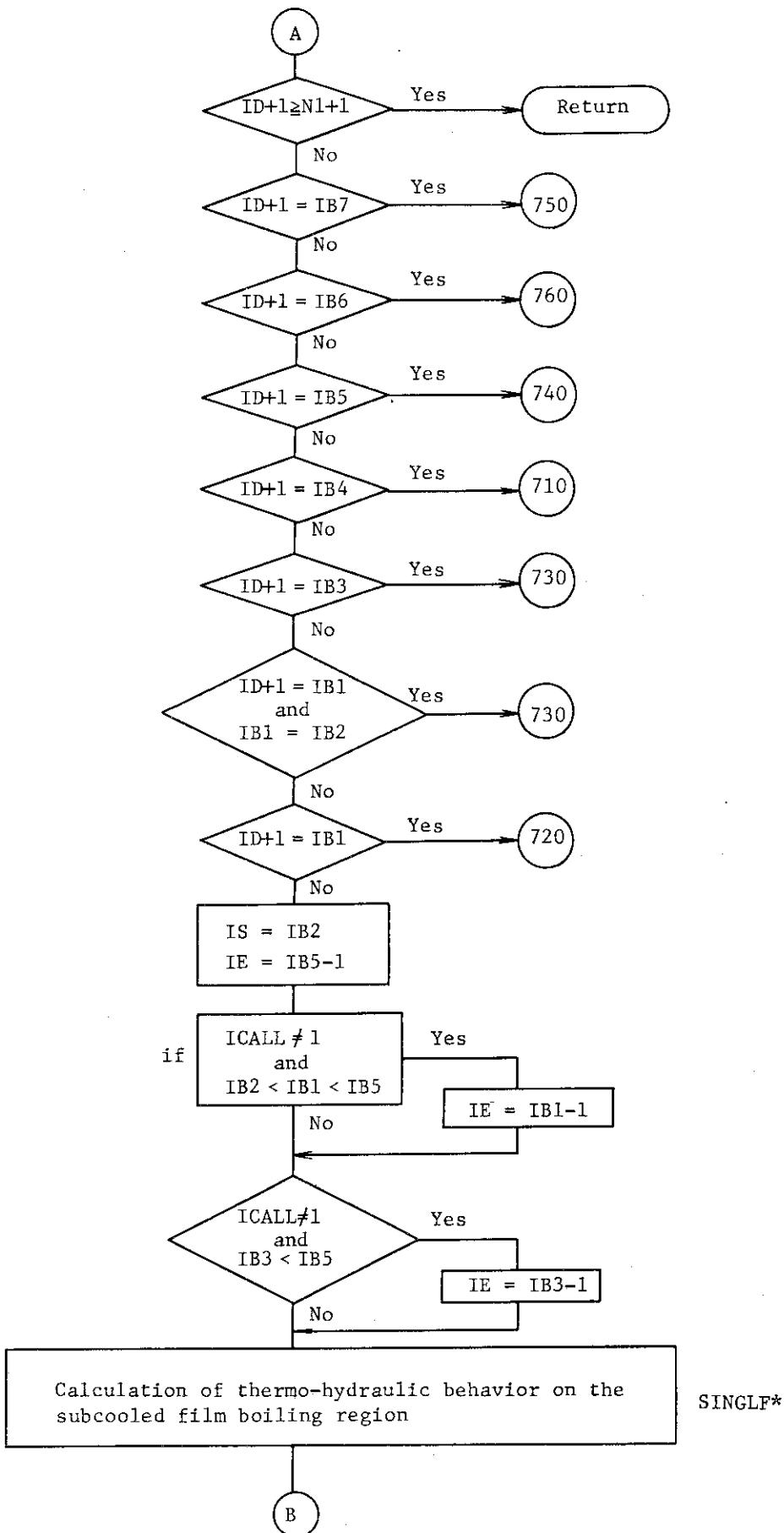


Fig. 2.3 Flow chart of subroutine REFLAA (2/5)

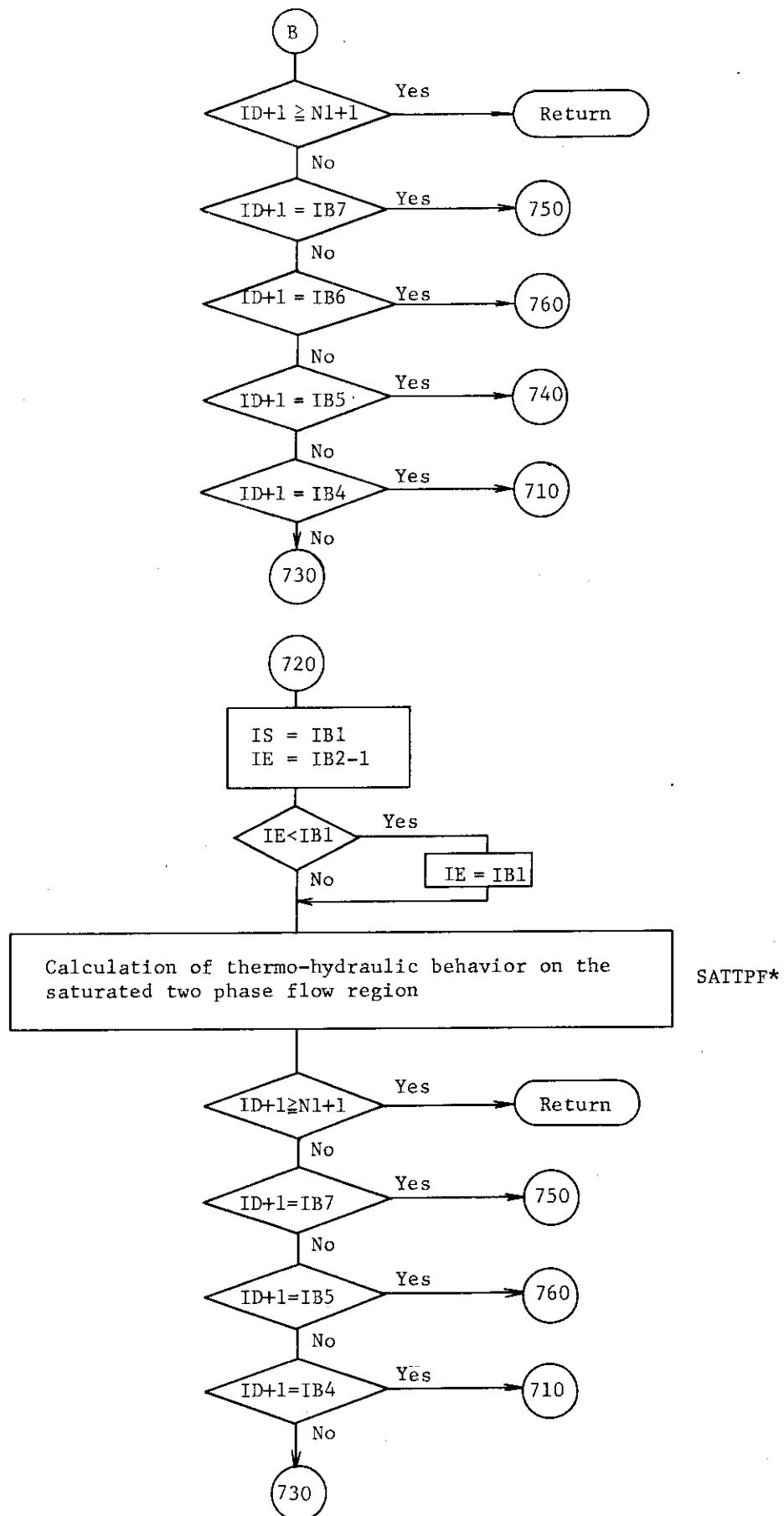


Fig. 2.3 Flow chart of subroutine REFLAA (3/5)

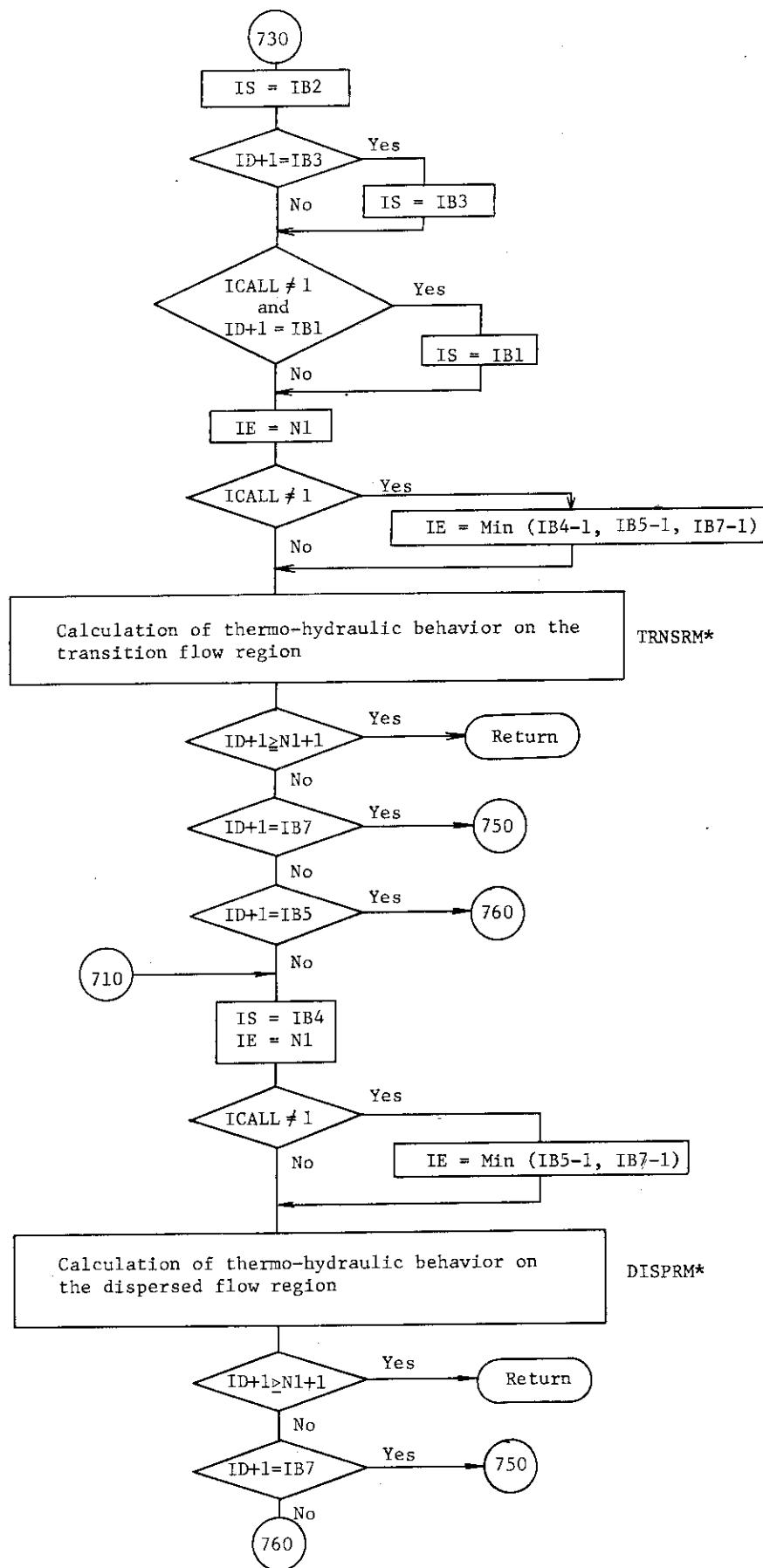


Fig. 2.3 Flow chart of subroutine REFLAA (4/5)

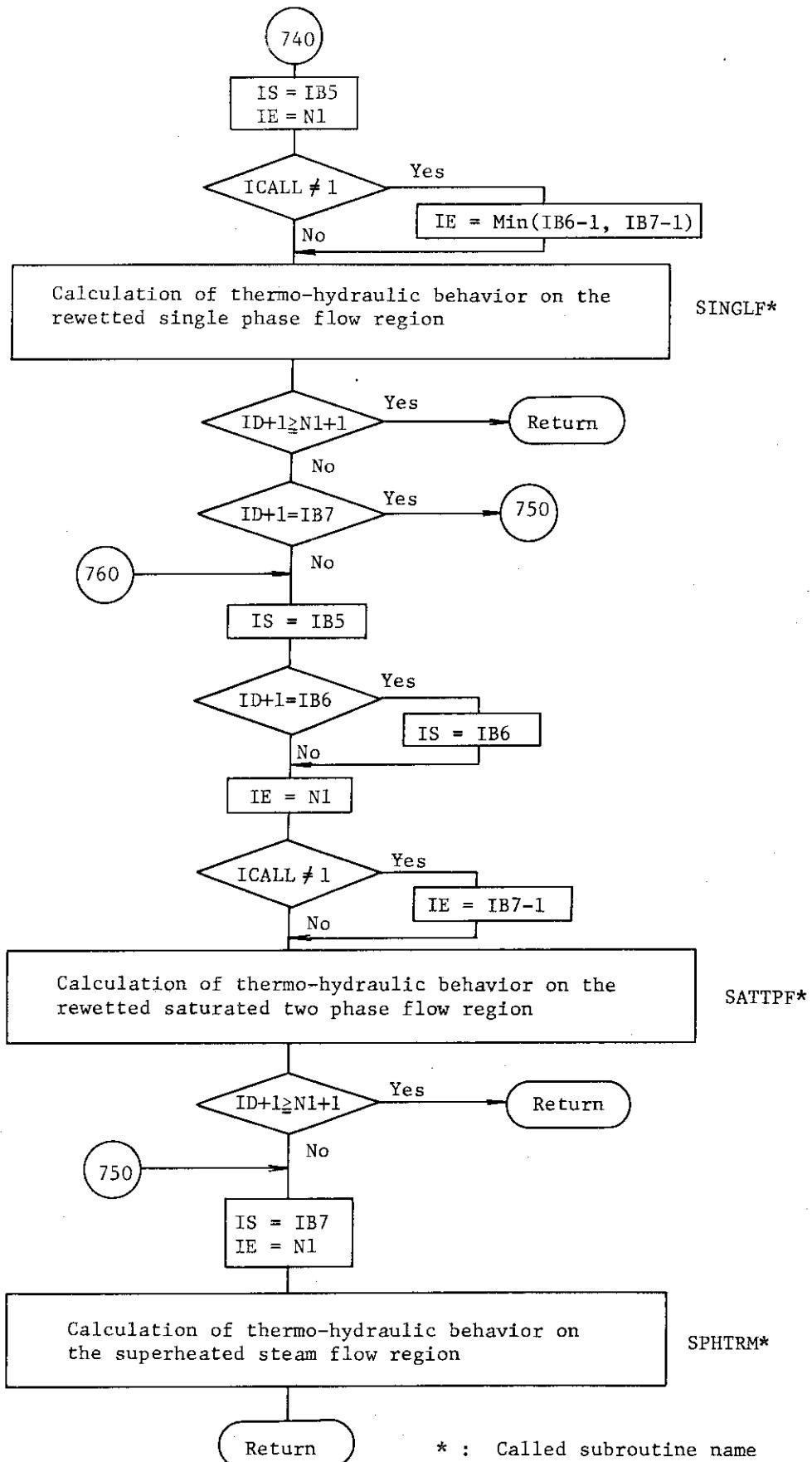


Fig. 2.3 Flow chart of subroutine REFLAA (5/5)

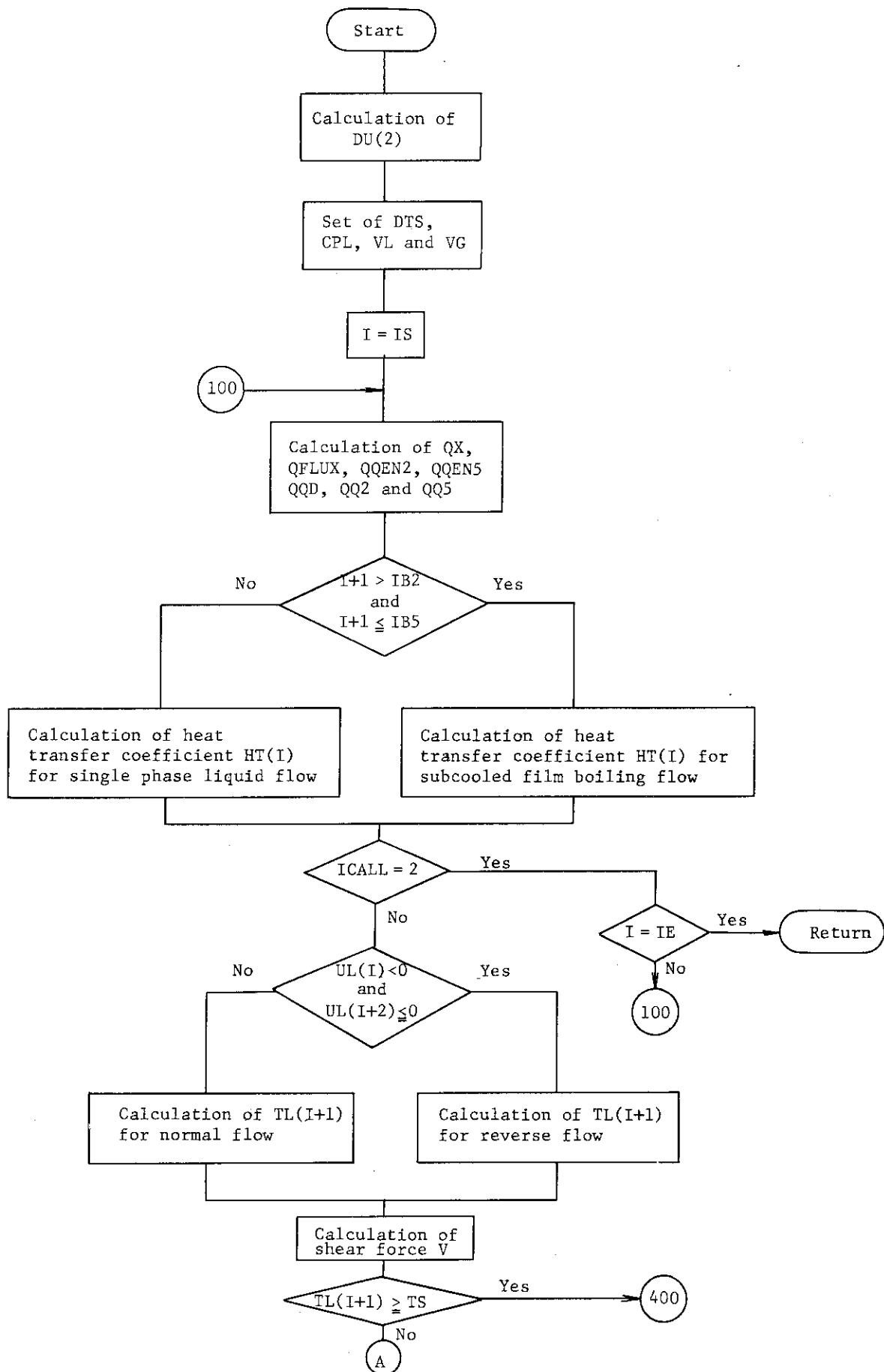


Fig. 2.4 Flow chart of subroutine SINGLF (1/4)

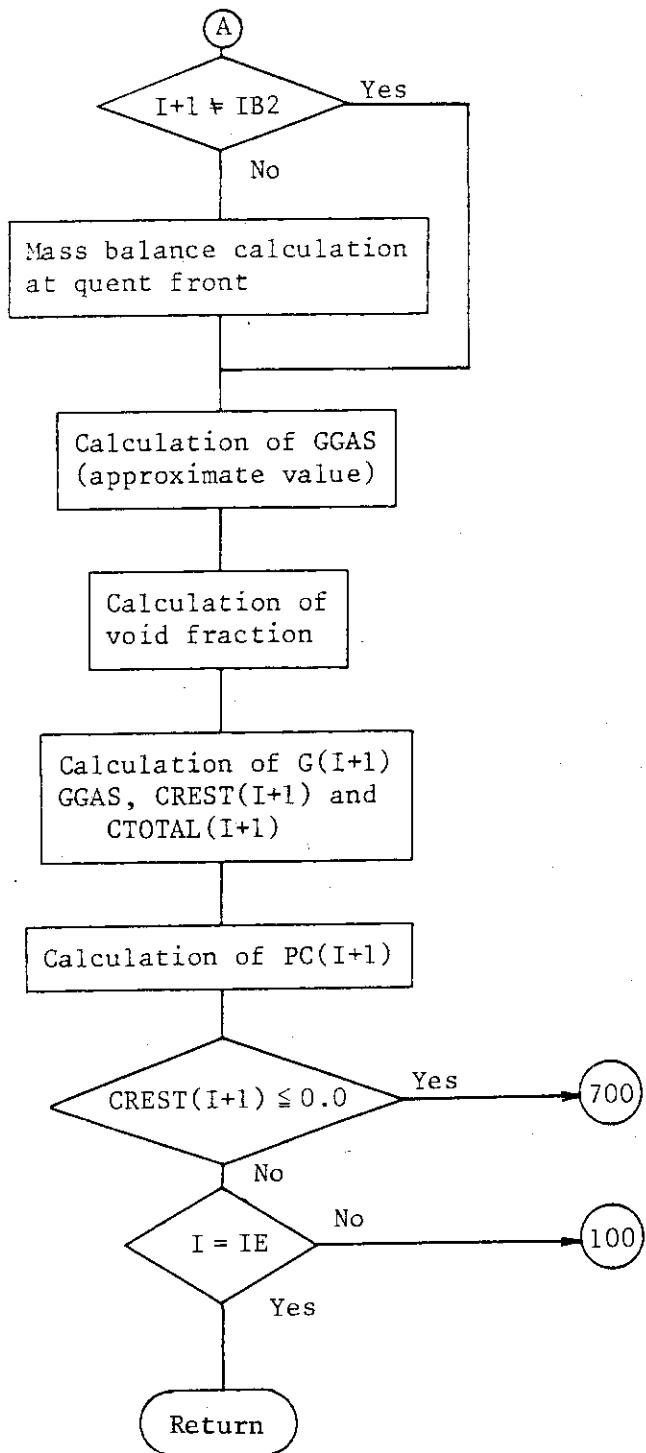


Fig. 2.4 Flow chart of subroutine SINGLF (2/4)

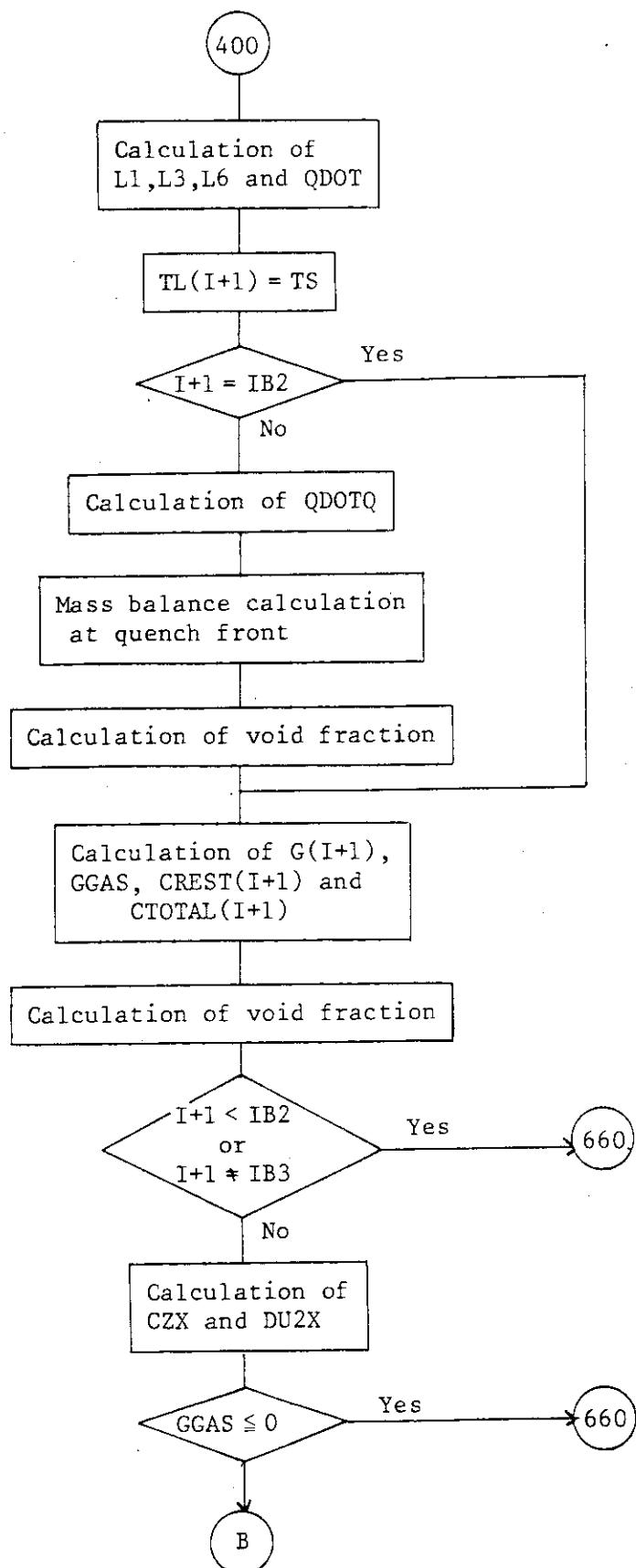


Fig. 2.4 Flow chart of subroutine SINGLF (3/4)

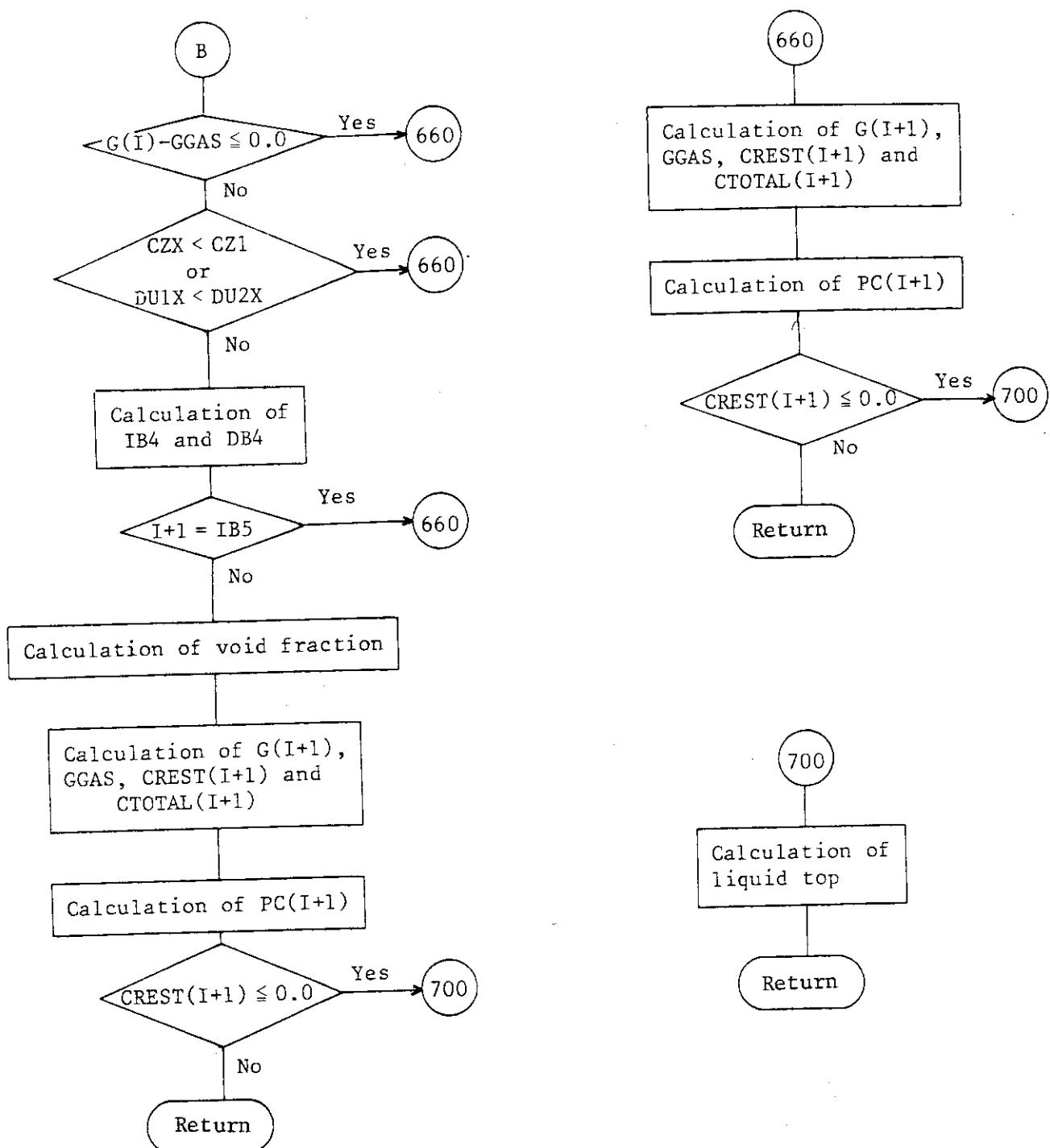


Fig. 2.4 Flow chart of subroutine SINGLEF (4/4)

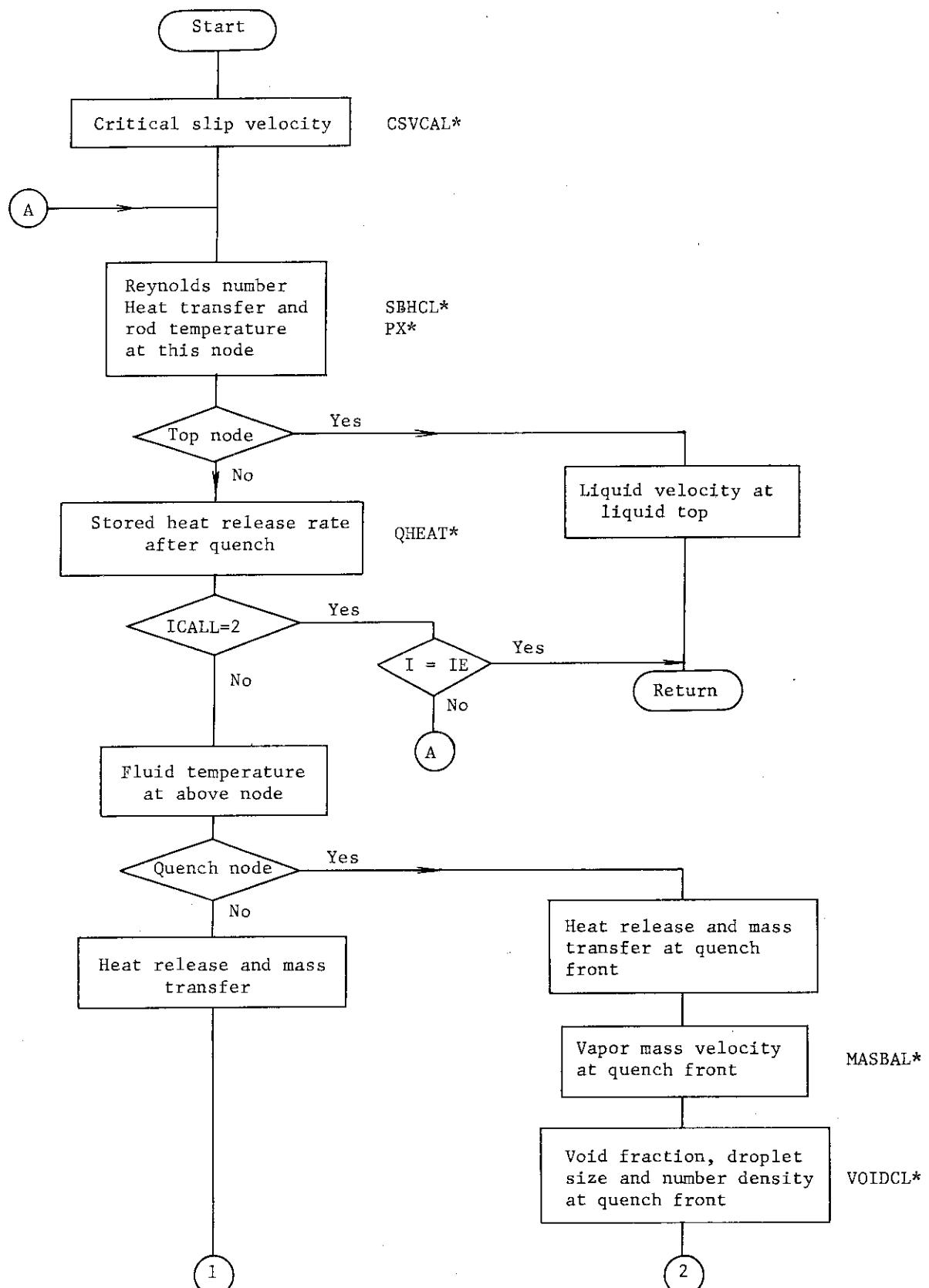


Fig. 2.5 Flow chart of subroutine SATTPF (1/3)

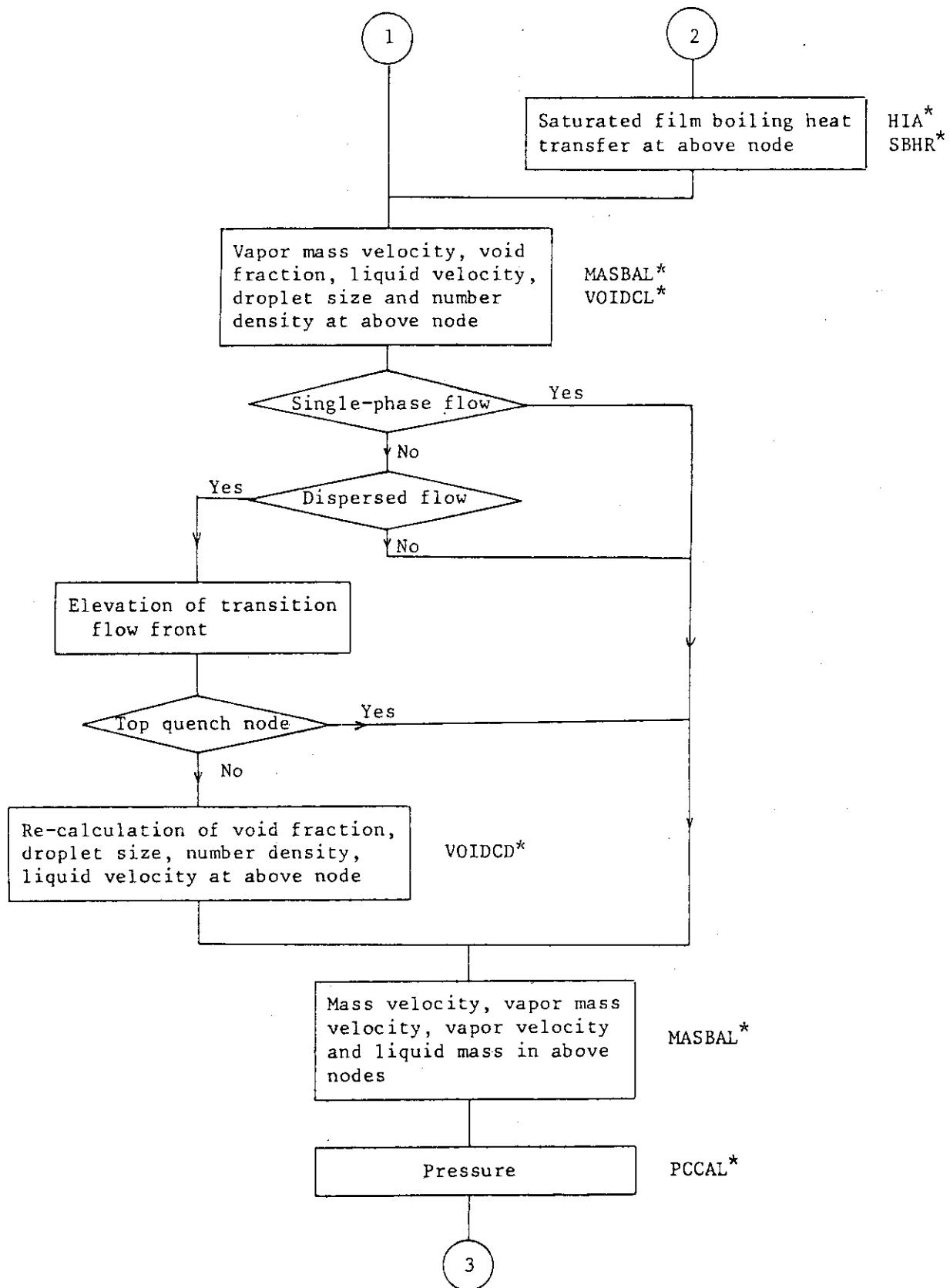
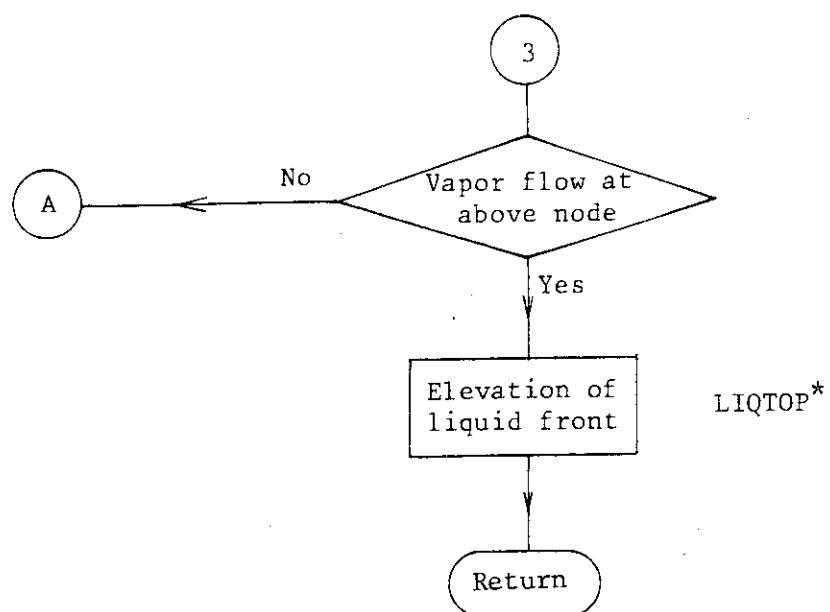


Fig. 2.5 Flow chart of subroutine SATTPF (2/3)



\* : called subroutine name

Fig. 2.5 Flow chart of subroutine SATTPF (3/3)

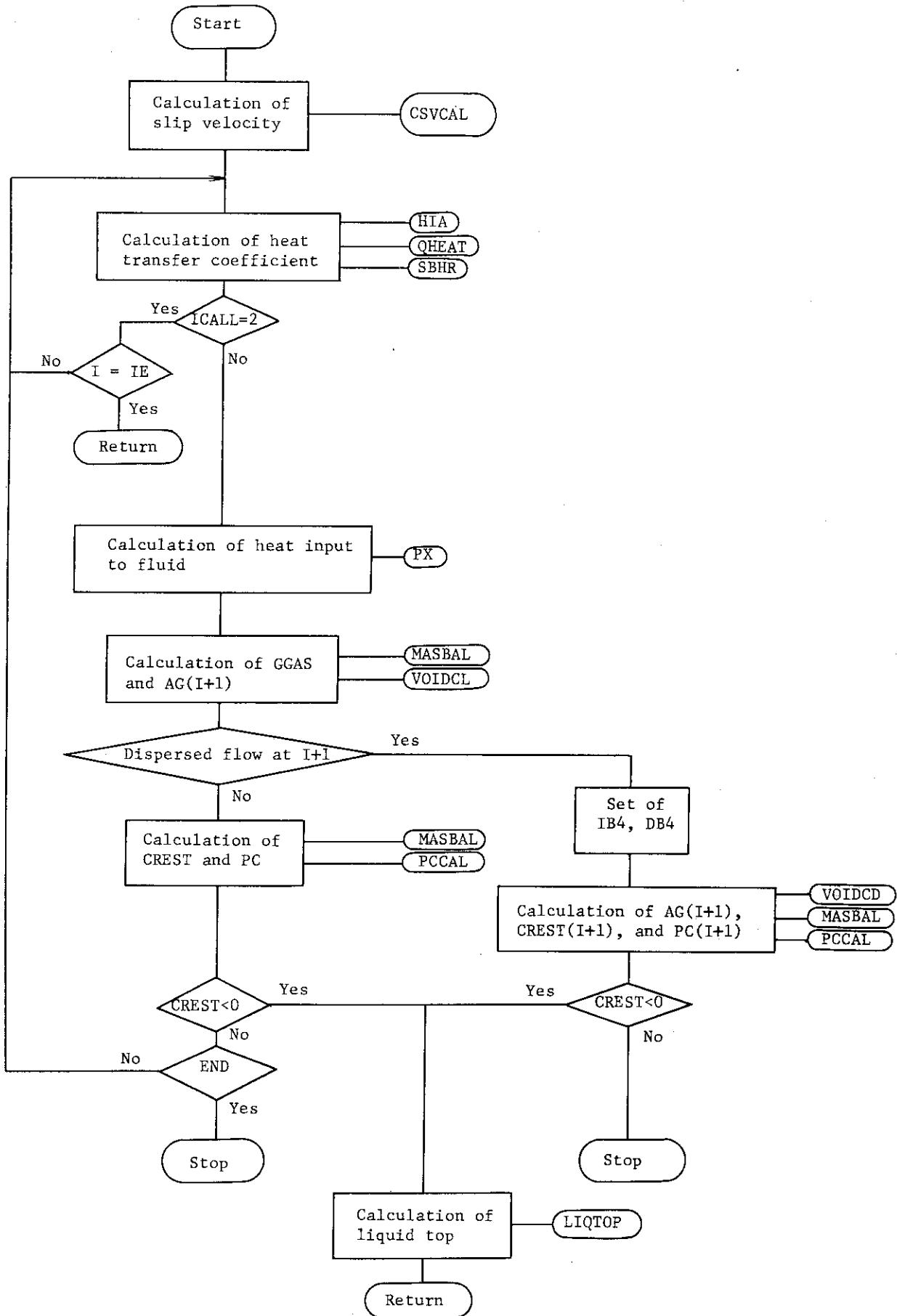


Fig. 2.6 Flow chart of subroutine TRNSRM

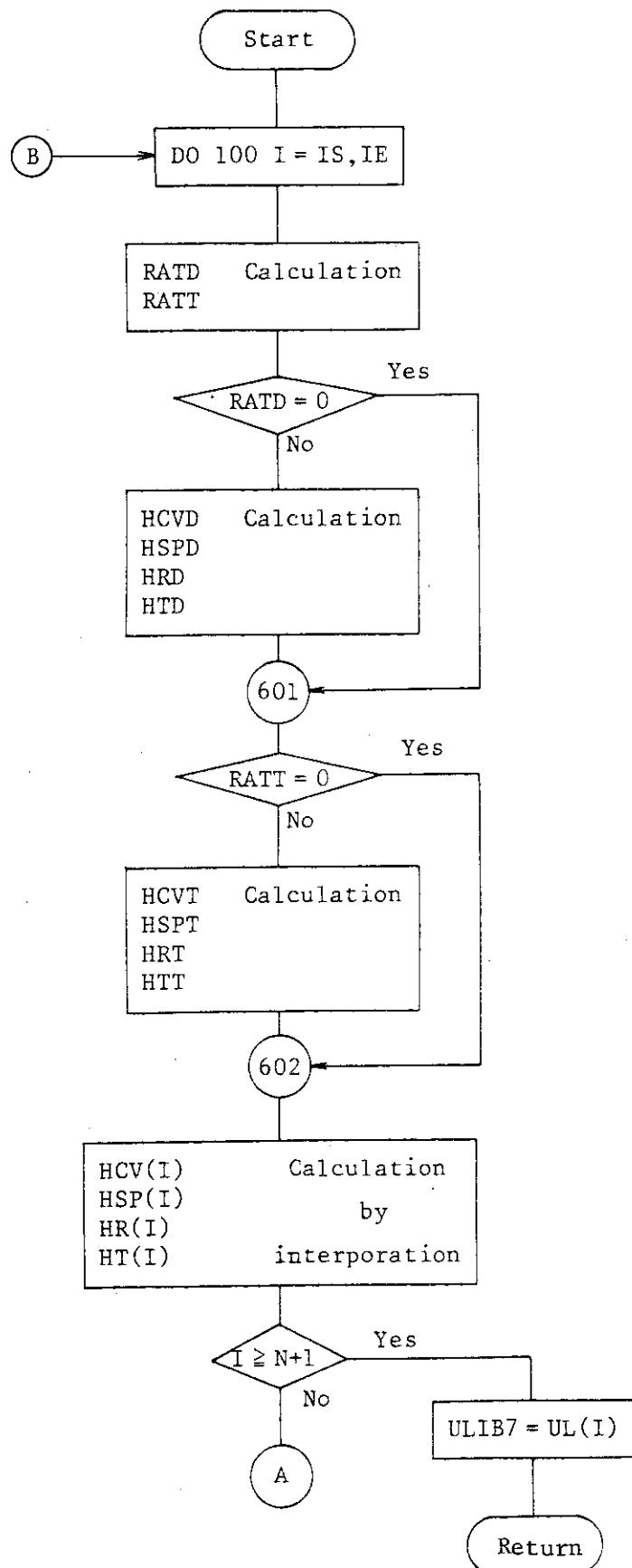


Fig. 2.7 Flow chart of subroutine DISPRM (1/2)

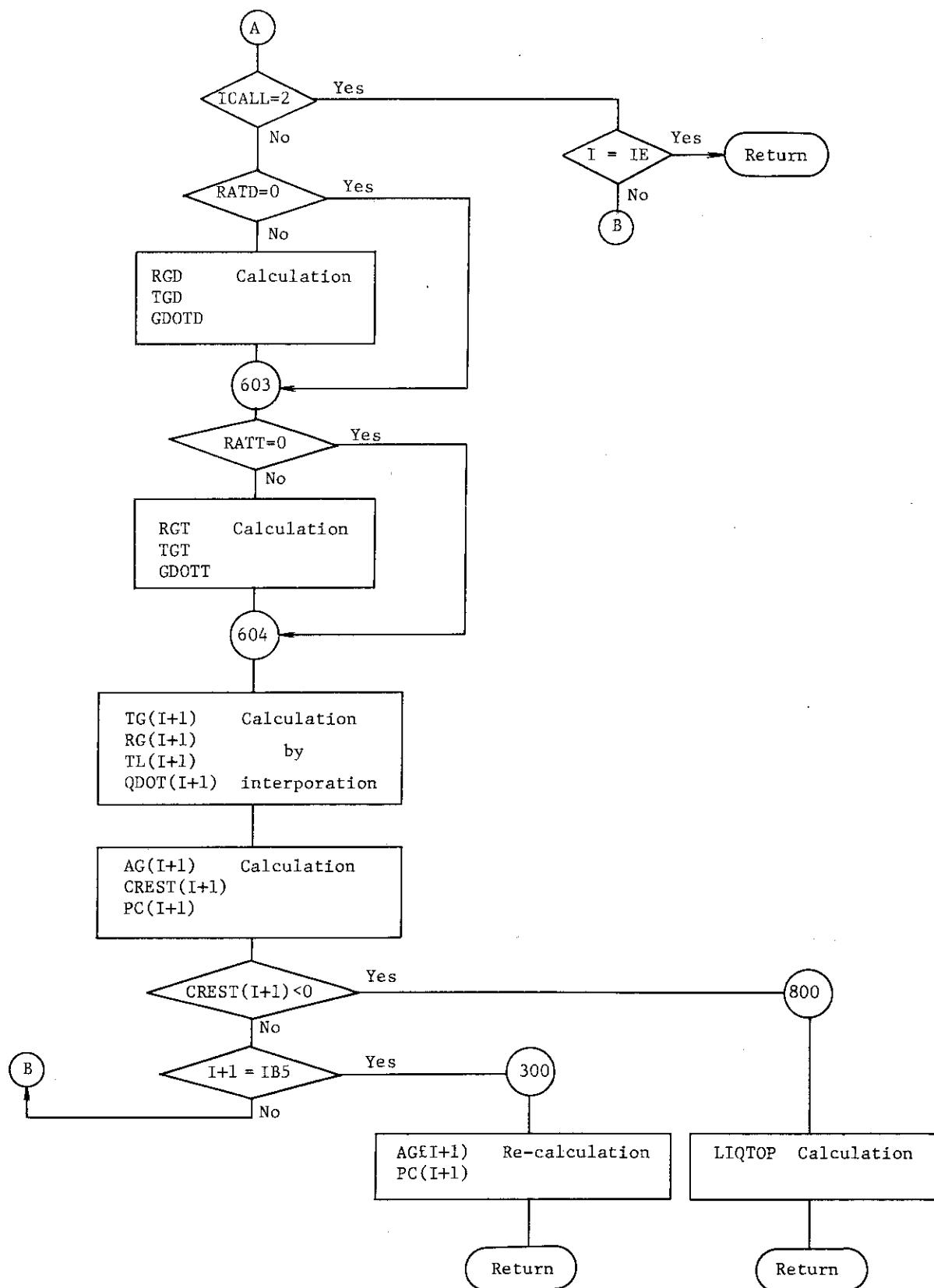


Fig. 2.7 Flow chart of subroutine DISPRM (2/2)

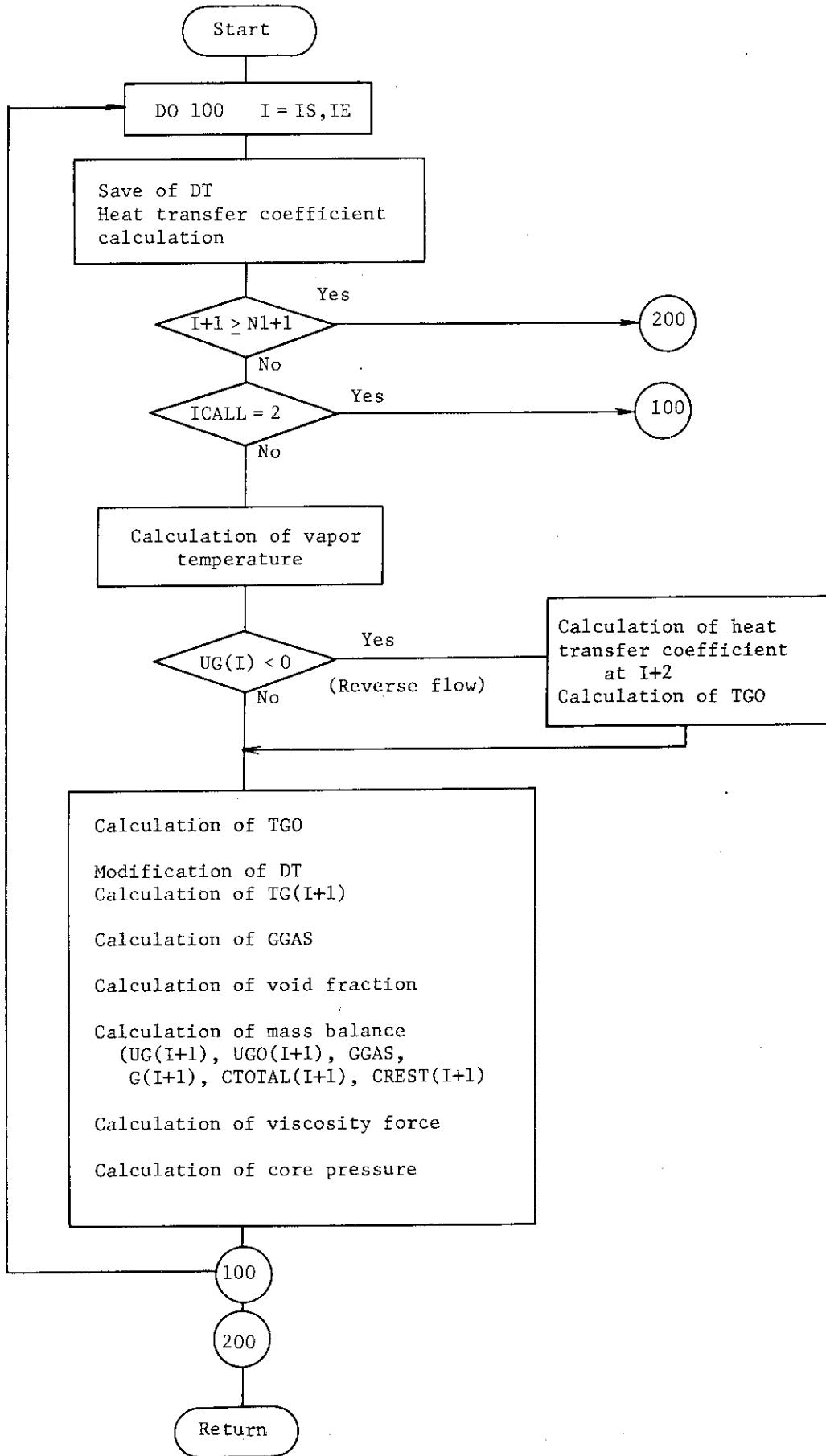


Fig. 2.8 Flow chart of subroutine SPHTRM

### 3. 燃料棒半径方向温度分布モデルの組込み

#### 3.1 燃料棒半径方向温度分布計算コード HETRAP との結合

REFLA-1D/MODE 3 コードの燃料棒モデルでは、燃料棒半径方向の温度分布は平坦で、燃料棒内部の温度は被覆管表面温度で代表されていた。<sup>(1)</sup>そこで、燃料棒半径方向に温度分布をもたせる機能を追加するために、燃料棒半径方向温度分布計算コード HE TRAP<sup>(5)</sup>を REFLA-1D/MODE 3 コードと結合した。

なお、燃料棒半径方向温度分布計算を行うのはクエンチ点上方についてのみであり、クエンチ点以下では、従来どおり燃料棒半径方向に温度分布はなく、燃料棒内部の温度は Jens & Lottes の式で計算された被覆管表面温度に代表される。

図 3.1 に燃料棒半径方向温度分布モデル適用時の燃料棒温度計算の概略を示す。

#### 3.2 クエンチによる燃料棒から流体への熱放出計算の修正

REFLA-1D/MODE 3 コードでは、クエンチによる燃料棒から流体への熱放出は次のような取扱いをしている。図 3.2(a) に示すように、燃料棒内の熱伝導による熱放出の時間遅れを考慮して、クエンチした部分の蓄熱量のうち  $A_{st}$  の割合のみ瞬時放出し、残りの  $1 - A_{st}$  なる割合のものは時定数  $\tau$  で徐々に放出されると仮定している。単位時間、単位長さ当たりの瞬時放熱量  $Q_{QF}$ 、減衰放熱量  $Q_{QD}$  は以下の式で計算される。

$$Q_{QF_i} = F_{Q_i} \cdot A_{st} \cdot (T_q - T_{w_i}^{old}) \cdot \Delta Z_q / (\Delta t \cdot \Delta Z) \quad (1)$$

$$F_{Q_i} = S_F \cdot \{ (C_p \rho)_i^{old} + (C_p \rho)_i^{new} \} / 2 \quad (2)$$

$$Q_{QD_i} = \frac{1 - A_{st}}{\tau} \cdot F_{R_i} \cdot \exp(-t_{q_i} / \tau) \quad (3)$$

$$F_{R_i} = S_F \cdot \{ T_{w_i}^{old} \cdot (C_p \rho)_i^{old} - T_{w_i}^{new} \cdot (C_p \rho)_i^{new} \} \quad (4)$$

$T_q$  : クエンチ温度

$T_w$  : 被覆管表面温度

$\Delta Z_q$  : 1 time step 当りのクエンチ進行距離

$\Delta t$  : time step 幅

$\Delta Z$  : 軸方向ノード間距離

$S_F$  : 燃料棒断面積

$\rho$  : 燃料棒密度

$C_p$  : 比熱

$t_q$  : クエンチ後の時間 $i$  : 軸方向ノード番号

old : 旧時刻

new : 新時刻

燃料棒半径方向温度分布モデルの組込みに伴い、このモデル適用時のクエンチによる燃料棒から流体への熱放出の取扱いは次のように変更した。図 3.2 (b) に示すように、被覆管部分の蓄積熱は瞬時に流体へ放出し、燃料ペレット部分の蓄積熱は時定数  $\tau$  で徐々に流体へ放出されるようにした。単位時間、単位長さ当たりの瞬時放熱量  $Q_{QF}$ 、減衰放熱量  $Q_{QD}$  は以下の式で計算される。

$$Q_{QF_i} = F_{Q_i} \cdot (T_q - T_{w_i}^{old}) \cdot \Delta Z_q / (\Delta t \cdot \Delta Z) \quad (5)$$

$$F_{Q_i} = \frac{1}{2} \left\{ \sum_j^{clad} (C_p \rho S)_j^{old} + \sum_j^{clad} (C_p \rho S)_j^{new} \right\} \quad (6)$$

$$Q_{QD_i} = \frac{F_{R_i}}{\tau} \exp(-t_{q_i} / \tau) \quad (7)$$

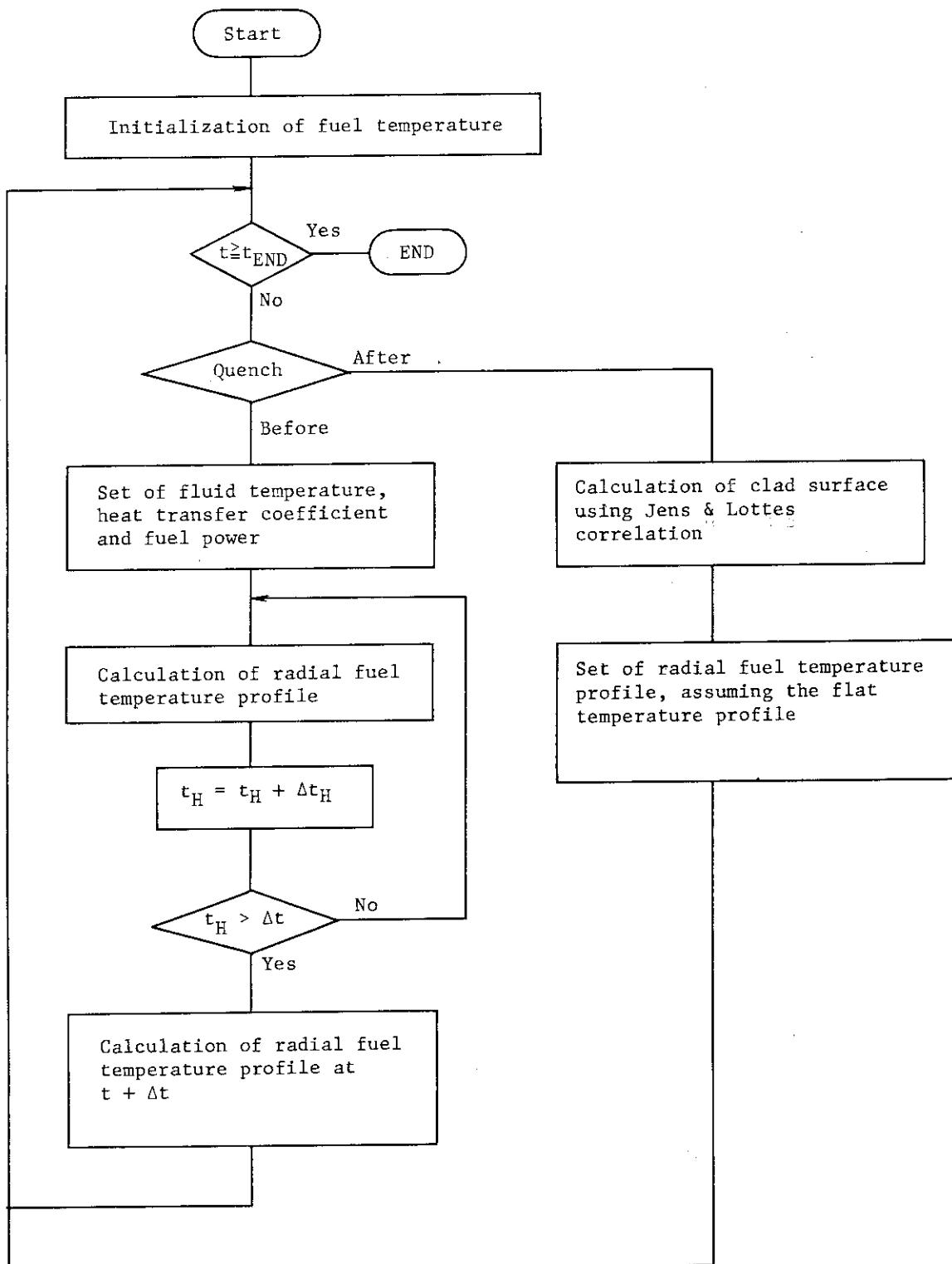
$$F_{R_i} = \sum_j^{pellet} T_{pj}^{old} \cdot (C_p \rho S)_j^{old} - \sum_j^{pellet} T_{pj}^{new} \cdot (C_p \rho S)_j^{new} \quad (8)$$

 $\sum_j^{clad}$  : 被覆管部分の和

 $\sum_j^{pellet}$  : 燃料ペレット部分の和
 $j$  : 燃料棒半径方向ノード番号 $T_p$  : 燃料ペレット温度

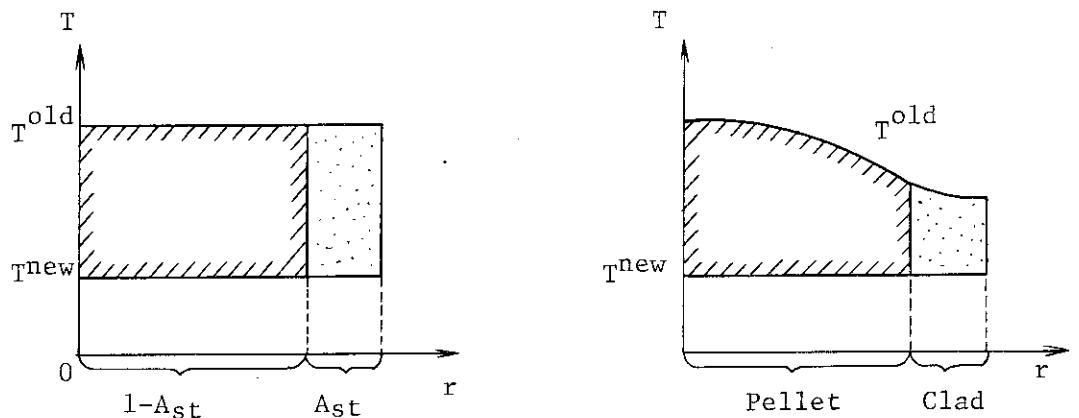
### 3.3 モデル組込み後の炉心内熱水力計算の概略

REFLA-1D/MODE 3 コードに、局所出力効果モデルおよび燃料棒半径方向温度分布モデルを組込んで作成した REFLA-1D/MODE 4 コードの炉心熱水力計算部分（サブルーチン REFLA1）の概略フローチャートを図 3.3 に示す。



$t_H$  : Time used in HETRAP  
 $t$  : Time used in REFLA  
 $t_{END}$  : Termination time of calculation  
 $\Delta t_H$  : Time step size used in HETRAP  
 $\Delta t$  : Time step size used in REFLA

Fig. 3.1 Fuel temperature calculation procedure in case of using fuel temperature profile effect model



(a) In case of using previous radial fuel temperature model (one point model)

(b) In case of using present fuel temperature profile effect model

: Instantaneous stored energy release

: Gradual stored energy release

$T^{\text{old}}$  : Radial fuel temperature profile before quenching

$T^{\text{new}}$  : Radial fuel temperature profile after quenching

Fig. 3.2 Calculation method of stored energy release rate due to quenching

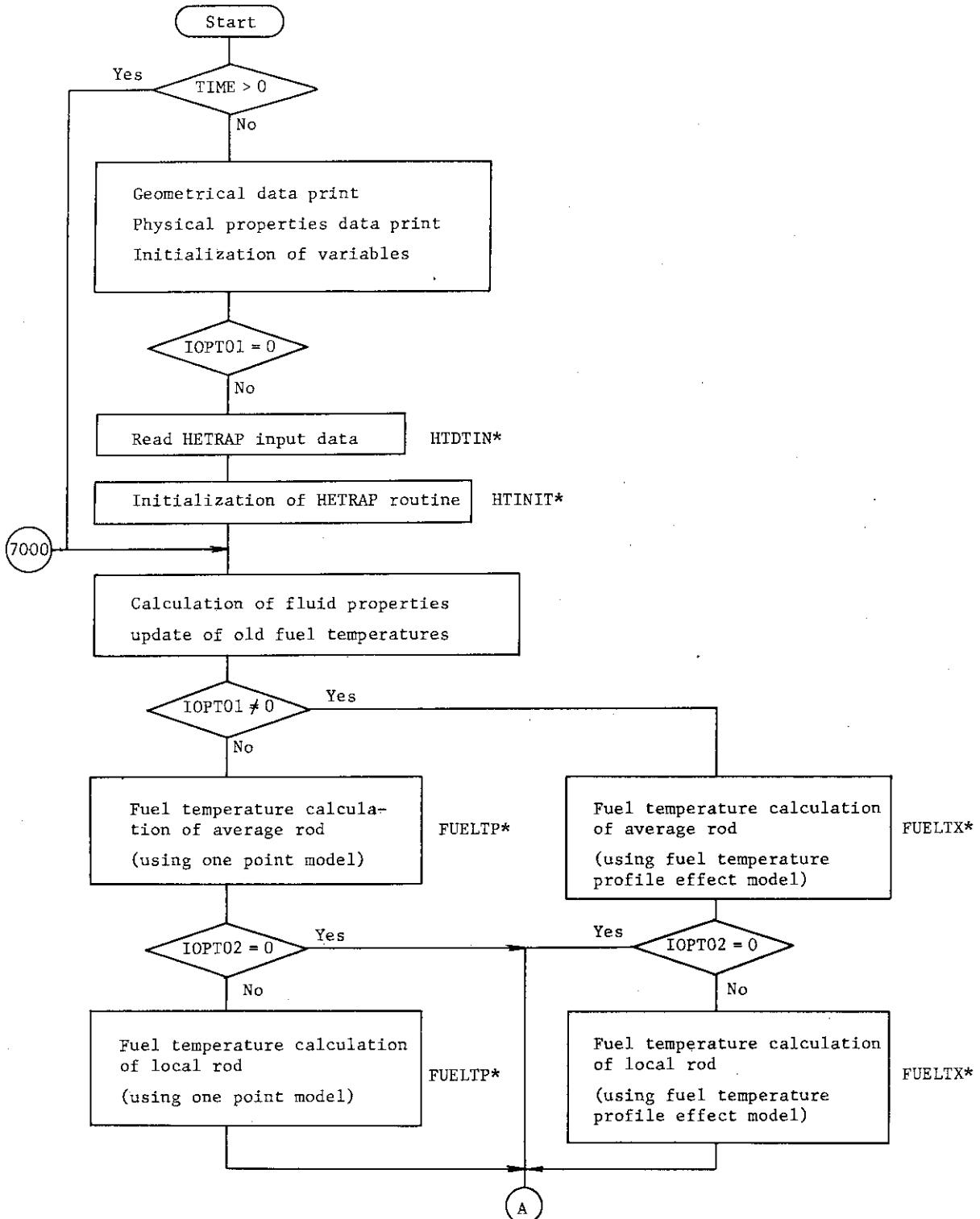


Fig. 3.3 Core thermo-hydraulic calculation procedure in REFLA-1D/MODE4  
(Flow chart of subroutine REFLA1) (1/2)

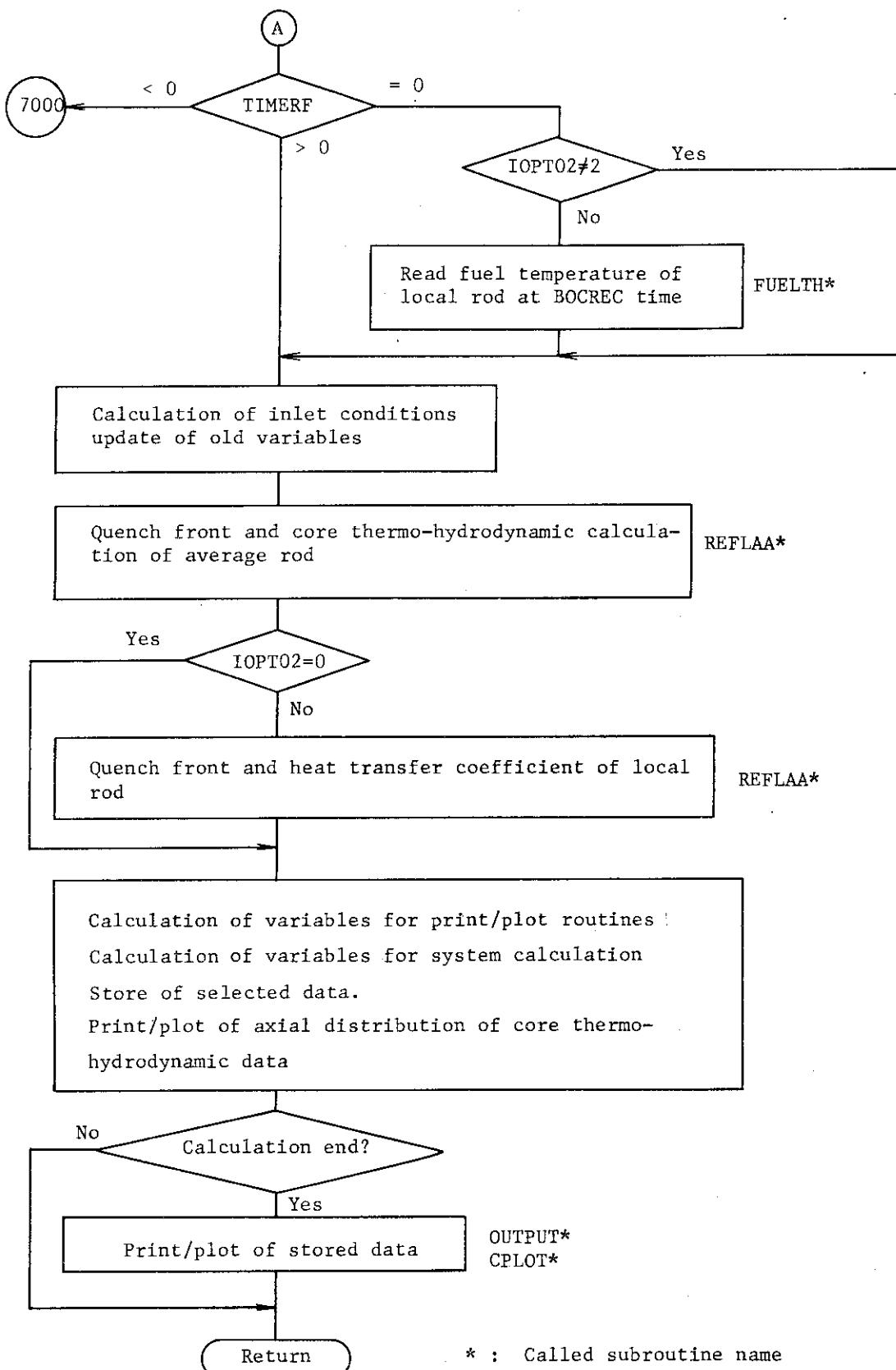


Fig. 3.3 Core thermo-hydraulic calculation procedure in REFLA-1D/MODE4  
(Flow chart of subroutine REFLA1) (2/2)

## 4. REFLA-1D/MODE4コード使用上の情報

### 4.1 REFLA 入力データ

表 4.1 に燃料棒半径方向温度分布計算用入力データを除く REFLA-1D/MODE 4 の入力データ (REFLA 入力データ) 形式を示す。REFLA-1D/MODE 3 から追加・修正された入力データについて以下に説明する。その他の入力データについては参考文献(1)の REFLA-1D/MODE 3 コードマニュアルを参照のこと。

#### 4.1.1 REFLA 入力データの変更点

##### (1) Card No. 2 の追加 (Format (2I 3))

- 1) IOPT01 =  $\begin{cases} 0 : \text{燃料棒半径方向 1 点近似計算} \\ 1 : \text{燃料棒半径方向温度分布計算} \end{cases}$
- 2) IOPT02 =  $\begin{cases} 0 : \text{平均燃料棒のみ計算} \\ 1 : \text{局所燃料棒も同時に計算} \\ \quad \left( \begin{array}{l} \text{現在局所燃料棒初期温度の入力データはなく、平均燃料棒} \\ \text{初期温度 TW(I)と同じ値が設定される。} \\ \text{再冠水開始時局所燃料棒温度分布は、平均燃料棒同様に、} \\ \text{平均燃料棒中心高さの温度が TEMP 2 に到達するまで、断熱} \\ \text{昇温計算して決定される。} \end{array} \right) \\ 2 : \text{局所燃料棒も同時に計算} \\ \quad \left( \begin{array}{l} \text{再冠水開始時局所燃料棒被覆管表面温度は TBOC(I),} \\ I = 1, 5 \text{ から内挿して与える。} \end{array} \right) \end{cases}$

##### (2) Card No. 5 の変更 (Format (G 12.5, F 6.3, 5F 6.1))

- 1) NPLOT =  $\begin{cases} 0 : \text{プロット出力なし} \\ 1 : \text{すべての出力を行う} \\ 2 : \text{時間履歴データのプリント出力なし} \end{cases}$   
(従来どおり必ず必要)
- 2) NPR : 局所燃料棒の平均燃料棒に対する出力比  
(IOPT02 = 1 または 2 のとき必要)
- 3) TBOC(I), I = 1, 5 : 再冠水開始時の局所燃料棒被覆管表面温度 (°C)  
I は IAXMOD に依存してサブルーチン ITELE で決定  
される高さ 1 ~ 5 に対応 (参考文献(1)の Table 4.4 参照)  
(IOPT02 = 2 のときのみ必要)

##### (3) Card No. 18, 19 の追加 (Format (2A 4))

炉心入口境界条件を入力で与えて炉心内熱水力計算をする場合 (Z = 4.0) に必要なデータ

(炉心入口流速, 炉心入口水温, 炉心入口圧力) および計算結果と実験結果の比較図を作成するのに必要な実験データを標準ファイルから読込むための入力データを追加した。

## Card No. 18 (2 A 4)

- 1) IRUN : 実験 Run №
- 2) CORS : 実験名 (ブランクの時は "CCTF" が自動入力される)

## Card No. 19 (2 A 4)

- 1) ITAG 1(I) } 実験データの Tag-ID
- 2) ITAG 2(I) }

Card No. 19\_1 から 19\_30 に入力する実験データを表 4.2 に示す。

なお、比較図を作成するのに必要なクエンチ進行データは、Card No. 19 で指定した被覆管表面温度データと同じ平均燃料棒および局所燃料棒のクエンチ進行データがサブルーチン QPLOT で温度情報ファイルから自動的に読込まれる。

## (4) CCON, ICON の追加

追加したCCON, ICON およびそれぞれのデフォルト値を以下に示す。

CCON (41) = 4.0 : クエンチ後の燃料棒から流体への減衰熱放出時定数 (sec)

ICON (4) = 1 : クエンチ相関式圧力依存性オプション

= 0 : 圧力依存性なし (ステンレス被覆管)

= 1 : 圧力依存性あり (ステンレス被覆管)

= 2 : 圧力依存性あり (ジルカロイ被覆管)

ICON (14) = 4 : 燃料棒半径方向温度

格納データ数 ( $\leq 4$ )

ICON (15) = 1 : 時間履歴データのプリント出力間隔

(\*DTS × ICON(11) × ICON(15)" 秒毎に出力)

ICON (16) = 1 : 1ページに出力するプロット図の数

## 4.2 燃料棒半径方向温度分布計算用入力データ (HETRAP 入力データ)

表 4.3 に燃料棒半径方向温度分布モデル適用時に必要な HETRAP 入力データ形式を示す。さらに、表 4.4 に HETRAP 入力データ変数の説明を示す。

現在、局所燃料棒半径方向初期温度分布の入力データではなく、平均燃料棒の半径方向初期温度分布の入力値と同値が設定される。

また、再冠水開始時の局所燃料棒半径方向温度分布を与える入力データも現在ない。

## 4.3 計算結果格納データ

REFLA-1D/MODE 4 コードにおける計算結果格納データを表 4.5 に示す。REFLA-1D/MODE 3 コードの格納データ<sup>(1)</sup>に対して若干の修正および配列名 ADDG および DATTF の格納データが追加されている。

#### 4.4 プリント出力データ

プリント出力データは以下に示す4項目とデバッグ出力からなる。REFLA-1D/MODE 4コードでは、REFLA-1D/MODE 3コードから炉心データと時間履歴データに新たな出力データが追加されている。

(1) 入力データ、物性値等の出力

- 1) 入力カードリスト
- 2) 入力データリスト
- 3) 形状データ
- 4) 物理定数および物性値
- 5) 燃料棒の初期状態

(2) 炉心データ（表4.6参照）

- 1) 炉心データ "Inlet and outlet condition"
- 2) 局所燃料棒の情報 (IOPT02 ≠ 0 のとき出力)
- 3) 平均燃料棒半径方向温度分布 (IOPT01 = 1 のとき出力)
- 4) 局所燃料棒半径方向温度分布 (IOPT01 = 1かつ IOPT02 ≠ 0 のとき出力)

2)～4)は新しく追加されたプリント出力データである。

炉心データは DTS × ICON (12) 秒毎にプリント出力される。

(3) システムデータ（表4.7参照）

システムデータは DTS × 40 秒毎にプリント出力される。

(4) 時間履歴データ（表4.8参照）

- 1) コントロールデータ
  - 2) 平均燃料棒被覆管表面温度
  - 3) 局所燃料棒被覆管表面温度 (IOPT02 ≠ 0 のとき出力)
  - 4) 平均燃料棒クエンチデータおよびキャリーオーバー率
  - 5) 局所燃料棒クエンチデータ (IOPT02 ≠ 0 のとき出力)
  - 6) 平均燃料棒熱伝達率
  - 7) 局所燃料棒熱伝達率 (IOPT02 ≠ 0 のとき出力)
  - 8) ポイド率
  - 9) 炉心内流動各領域の境界
  - 10) 炉心出口状態
  - 11) 平均燃料棒半径方向温度分布 (IOPT01 = 1 のとき出力)
  - 12) 局所燃料棒半径方向温度分布 (IOPT01 = 1かつ IOPT02 ≠ 0 のとき出力)
- 3), 5), 7) および 10)～12) は新しく追加されたプリント出力データである。
- 時間履歴データは、上記(1)～(3)のプリント出力完了後に、DTS × ICON (11) × ICON (15) 秒毎の値がプリント出力される。

#### 4.5 プロット出力データ

プロット出力データは以下に示す3項目からなる。表4.9～表4.11に各項目のプロット出力データを示す。

- (1) 実験データの図（表4.9参照）
- (2) 計算結果の図（表4.10参照）
- (3) 実験データと計算結果の比較図（表4.11参照）

#### 4.6 J C L

作成したREFLA-1D/MODE4コード実行のJCL例を表4.12に示す。

Table 4.1 REFLA input data format

| Column<br>Card No. |   | 1 ~ 12                                    | 13 ~ 24 | 25 ~ 36 | 37 ~ 48 | 49 ~ 60 | 61 ~ 72        |
|--------------------|---|---|---------|---------|---------|---------|----------------|
| 1                  |   | TITLE(1) ~ TITLE (18) (18A4)              |         |         |         |         |                |
| 2                  |   | IOPT01, IOPT02 (2I3)                      |         |         |         |         |                |
| 3                  | QMAX0   | DTS                                       | AXMOD   | TLIN    | PIN     | POUT    |                |
| 4                  | TIME3   | AZ1                                       | AZ2     | DTC     |         | Z       |                |
| 5                  | NPLOT   | NPR, TBOC(1) ~ TBOC(5) (G12.5,F6.3,5F6.1) |         |         |         |         |                |
| 6                  | N   |   | DIA     | PITCH   | CLENG   |         | $^{69}$ IDECAY |
| 7                  | WEC   |   |         |         |         |         |                |
| 8                  |   |   |         | DF      | CF      |         |                |
| 9                  |   | CNHEAT                                    | CSAVE   |         |         |         |                |
| 10                 |   |   |         |         |         |         |                |
| 11                 |   | TEMP2                                     |         |         |         |         |                |
| 12                 |   |   |         |         |         |         |                |
| 13                 |   |   |         |         |         |         |                |
| 14                 | TIME5   | TEMP5                                     |         |         |         |         |                |
| 15_1~15_N+1        | TW(1) ~ TW(N+1) (12F6.1)                          |   |         |         |         |         |                |
| 16                 | ITHCON  |   |         |         |         |         |                |
| 17_1~17_ITHCON     | NCCON(1), CCCON(1) ~ NCCON(ITHCON), CCCON(ITHCON) |   |         |         |         |         |                |
| 18                 |   | IRUN, CORS (2A4)                          |         |         |         |         |                |
| 19_1               |   | ITAG1(1), ITAG2(1) (2A4)                  |         |         |         |         |                |
| {                  |   | {   |         |         |         |         |                |
| 19_30              |   | ITAG1(30), ITAG2(30) (2A4)                |         |         |         |         |                |

\* Format of input

N : I 12  
 IDECAY : I 4  
 ITHCON : I 3  
 NCCON(I) : I 6  
 Others : G 12.5

Table 4.2 Description of REFLA input card No.19

| Card No. | Unit                | Description of Tag-ID  |
|----------|---------------------|--|
| 19-1     | K                   | Clad surface temperature at the 1st elevation<br>of average rod        |
| }        |                     | }  |
| 19-5     | K                   | 5th  |
| 19-6     | MPa                 | Differential pressure of intact loop                                   |
| 19-7     | MPa                 | Differential pressure of downcomer                                     |
| 19-8     | MPa                 | Differential pressure of broken loop                                   |
| 19-9     | MPa                 | Differential pressure of core  |
| 19-10    | -                   | Average void fraction between bottom and the 1st<br>elevation of core  |
| 19-11    |                     | the 1st and the 2nd  |
| }        |                     | }  |
| 19-15    | -                   | the 5th and the 6th  |
| 19-16    | m/s                 | Core inlet water velocity  |
| 19-17    | K                   | Core inlet water temperature   |
| 19-18    | MPa                 | Differential pressure between core inlet and<br>bottom of PV           |
| 19-19    | MPa                 | Pressure at bottom of PV   |
| 19-20    | -                   | Dummy  |
| 19-21    | K                   | Clad surface temperature at 1st elevation<br>of local rod              |
| }        |                     | }  |
| 19-25    | K                   | 5th  |
| 19-26    | W/m <sup>2</sup> •K | Total heat transfer coefficient at the 1st<br>elevation of average rod |
| 19-30    | W/m <sup>2</sup> •K | 5th  |

Table 4.3 HETRAP input data format

| Column<br>Card No. | 1 ~ 12                        | 13 ~ 24      | 25~36       | 37~48       | 49~60         | 61~72         |
|--------------------|-------------------------------|--------------|-------------|-------------|---------------|---------------|
| 1                  | NDZMAX                        |              |             |             |               |               |
| 2                  | NDZ1                          | NDZ2         |             |             |               |               |
| 3                  | NR1(NDZ1)                     |              |             |             |               |               |
| 4-1                | R(1,NDZ1)                     | PF(1,NDZ1)   | H(1,NDZ1)   | E(1,NDZ1)   | IWC(1,NDZ1)   | IWP(1,NDZ1)   |
|                    |                               | {            |             |             |               |               |
| 4-NR1              | R(NR1,NDZ1)                   | PF(NR1,NDZ1) | H(NR1,NDZ1) | E(NR1,NDZ1) | IWC(NR1,NDZ1) | IWP(NR1,NDZ1) |
| 5                  | DTA                           |              |             |             |               |               |
| 6                  | NTZMAX                        |              |             |             |               |               |
| 7                  | NTZ1                          | NTZ2         |             |             |               |               |
| 8                  | TN(1,NTZ1,1) ~ TN(NR1,NTZ1,1) |              |             |             |               |               |

}\*1

}\*2

## ◦ Format of input

NDZMAX, NDZ1, NDZ2, NR1(NDZ1), NTZMAX, NTZ1, NTZ2 : I12

Others : F12.0

## ◦ Note 1:

\*1 Repeat NDZMAX times from Card No.2 to No.4

\*2 Repeat NTZMAX times from Card No.7 to No.8

## ◦ Note 2:

- 1) Initial values of NR1, R, PF, H, E, IWC and IWP from level NDZ1+1 to NDZ2 are equal to the input values at level NDZ1.
- 2) Initial value of TN from level NTZ1+1 to NTZ2 is equal to the input value at level NTZ1.

Table 4.4 Description of HETRAP input variables

| Variable     | Unit                  | Description  |
|--------------|-----------------------|--|
| NDZMAX       | —                     | Number of axial divisions of fuel rod                                  |
| NDZ1         | —                     | Bottom node of axial division of fuel rod                              |
| NDZ2         | —                     | Top node of axial division of fuel rod                                 |
| NR1(NDZ1)    | —                     | Number of radial nodes at level NDZ1                                   |
| R(J,NDZ1)    | cm                    | Distance from center of fuel rod at radial node J and level NDZ1       |
| PF(J,NDZ1)   | —                     | Power factor at radial node J and level NDZ1                           |
| H(J,NDZ1)    | W/cm <sup>2</sup> ·°C | Heat transfer coefficient between radial node J and J-1 at level NDZ1  |
| E(J,NNZ1)    | —                     | Emissivity between radial node J and J-1 at level NDZ1                 |
| IWC(J,NDZ1)  | —                     | Material number <sup>(*)1</sup> at radial node J-1 and level NDZ1      |
| IWP(J,NDZ1)  | —                     | Material number <sup>(*)1</sup> at radial node J and level NDZ1        |
| DTA          | s                     | Time step of HETRAP routine  |
| NTZMAX       | —                     | Number of axial divisions to input initial temperature of fuel rod     |
| NTZ1         | —                     | Bottom node of axial division to input initial temperature of fuel rod |
| NTZ2         | —                     | Top node of axial division to input initial temperature of fuel rod    |
| TN(J,NTZ1,1) | °C                    | Initial temperature at radial node J and level NTZ1 of fuel rod        |

Note :

\*1

| No. | Material                       |
|-----|--------------------------------|
| 1   | Zircaloy-4                     |
| 2   | UO <sub>2</sub>                |
| 3   | BN                             |
| 4   | MgO                            |
| 5   | Stainless Steel 316            |
| 6   | Inconel 800                    |
| 7   | Inconel 600                    |
| 8   | Stainless Steel 347            |
| 9   | Al <sub>2</sub> O <sub>3</sub> |
| 10  | NCH-1                          |

Table 4.5 Description of stored output data (1/4)

## (1) DATX (J, NPPINT)

| J  | Description   | Unit                 |
|----|---|----------------------|
| 1  | Time after reflood  | s                    |
| 2  | Peak liner power of average rod                                     | kW/m                 |
| 3  | Reflooding flow velocity  | cm/s                 |
| 4  | System pressure   | kg/cm <sup>2</sup> a |
| 5  | Clad surface temperature at the 1st elevation of average rod        | °C                   |
| {  | }   | }                    |
| 10 | 6th   | °C                   |
| 11 | Total heat transfer coefficient at the 1st elevation of average rod | W/m <sup>2</sup> ·K  |
| {  | }   | }                    |
| 16 | 6th   | W/m <sup>2</sup> K   |
| 17 | Average void fraction between bottom and the 1st elevation of core  | -                    |
| 18 | the 1st and the 2nd   | -                    |
| {  | }   | }                    |
| 22 | the 5th and the 6th   | -                    |
| 23 | Gas phase temperature at the 1st elevation of core                  | °C                   |
| {  | }   | }                    |
| 28 | 6th   | °C                   |
| 29 | Coolant subcooling at quench point of average rod                   | °C                   |
| 30 | Quench velocity of average rod                                      | cm/s                 |
| 31 | Entrainment carryover fraction                                      | -                    |
| 32 | Apparent water level  | m                    |
| 33 | L1 : bulk boiling point   | m                    |
| 34 | L2 : quench point of average rod                                    | m                    |
| 35 | L3 : start point of transition flow                                 | m                    |
| 36 | L4 : start point of dispersed flow                                  | m                    |
| 37 | L5 : start point of rewetted region                                 | m                    |

Table 4.5 Description of stored output data (2/4)

| J  | Description  | Unit                 |
|----|--|----------------------|
| 38 | L7 : start point of superheated steam flow<br>(liquid top) | m                    |
| 39 | Differential pressure head of core                         | m Aq.                |
| 40 | Clad surface temperature at level 46 of local rod          | °C                   |
| 41 | Differential pressure head between lower and upper plenum  | m Aq.                |
| 42 | L6 : start point of bulk boiling in rewetted region        | m                    |
| 43 | Lower quench temperature of average rod                    | °C                   |
| 44 | LP2 : quench point of local rod                            | m                    |
| 45 | Total heat transfer coefficient at level 46 of local rod   | W/m <sup>2</sup> ·K  |
| 46 | Upper quench node  | -                    |
| 47 | Differential pressure head in downcomer                    | m Aq.                |
| 48 | Differential pressure head across loop                     | m Aq.                |
| 49 | Mass flux of gas at the outlet of core                     | kg/m <sup>2</sup> ·h |
| 50 | Mass flux of liquid at the outlet of core                  | kg/m <sup>2</sup> ·h |

## (2) ADDG (J, NPRINT)

| J  | Description   | Unit                |
|----|---|---------------------|
| 1  | Core outlet liquid mass flow rate                                 | kg/s                |
| 2  | Core outlet vapor mass flow rate                                  | kg/s                |
| 3  | Carryover fraction  | -                   |
| 4  | Clad surface temperature at the 1st elevation of local rod        | °C                  |
| {  |   | }                   |
| 9  | 6th   | °C                  |
| 10 | Peak linear power density of local rod                            | kW/m                |
| 11 | Lower quench temperature of local rod                             | °C                  |
| 12 | Total heat transfer coefficient at the 1st elevation of local rod | W/m <sup>2</sup> ·K |
| {  |   | }                   |
| 17 | 6th   | W/m <sup>2</sup> ·K |
| 18 | Coolant subcooling at quench point of local rod                   | °C                  |
| 19 | Quench velocity of local rod                                      | cm/s                |

Table 4.5 Description of stored output data (3/4)

## (3) DATTF (J, NPRINT)

| J  | Description  | Unit |
|----|--|------|
| 1  | Average rod temperature at the 1st radial point of the 1st elevation | °C   |
| {  |  | }    |
| 4  | 4th  | °C   |
| 5  | Average rod temperature at the 1st radial point of the 2nd elevation | °C   |
| {  |  | }    |
| 8  | 4th  | °C   |
| 9  | Average rod temperature at the 1st radial point of the 3rd elevation | °C   |
| {  |  | }    |
| 12 | 4th  | °C   |
| 13 | Average rod temperature at the 1st radial point of the 4th elevation | °C   |
| {  |  | }    |
| 16 | 4th  | °C   |
| 17 | Average rod temperature at the 1st radial point of the 5th elevation | °C   |
| {  |  | }    |
| 20 | 4th  | °C   |

Table 4.5 Description of stored output data (4/4)

| J  | Description  | Unit |
|----|--|------|
| 21 | Local rod temperature at the 1st radial point of the 1st elevation | °C   |
| {  | }  | }    |
| 24 | 4th  | °C   |
| 25 | Local rod temperature at the 1st radial point of the 2nd elevation | °C   |
| {  | }  | }    |
| 28 | 4th  | °C   |
| 29 | Local rod temperature at the 1st radial point of the 3rd elevation | °C   |
| {  | }  | }    |
| 32 | 4th  | °C   |
| 33 | Local rod temperature at the 1st radial point of the 4th elevation | °C   |
| {  | }  | }    |
| 36 | 4th  | °C   |
| 37 | Local rod temperature at the 1st radial point of the 5th elevation | °C   |
| {  | }  | }    |
| 40 | 4th  | °C   |

Table 4.6 Description of core state data (1/3)

## (1) Inlet and outlet condition

| Data      | Description  | Unit                              |
|-----------|--|-----------------------------------|
| TQN2      | Quench temperature of bottom quench point of average rod | °C                                |
| ZB2       | Position of bottom quench point of average rod           | m                                 |
| TQN5      | Quench temperature of top quench point of average rod    | °C                                |
| ZB5       | Position of top quench point of average rod              | m                                 |
| DD(IB4)   | Droplet diameter at level IB4 (*1)                       | mm                                |
| DD(N1)    | Droplet diameter at outlet of core                       | mm                                |
| DP        | Differential pressure head in core                       | m Aq.                             |
| CRATIO    | Entrainment carryover fraction                           | -                                 |
| P         | Pressure at core inlet                                   | kg/m <sup>2</sup>                 |
| RL        | Density of liquid  | kg·h <sup>2</sup> /m <sup>4</sup> |
| RGST      | Density of gas at saturation temperature                 | kg·h <sup>2</sup> /m <sup>4</sup> |
| I         | Number of level  | -                                 |
| IP        | Index of flow pattern at level I of average rod (*2)     | -                                 |
| AG(I)     | Void fraction at level I                                 | -                                 |
| AGINF(I)  | Void fraction for transition flow at level I             | -                                 |
| AGDISP(I) | Void fraction for dispersed flow at level I              | -                                 |
| TW(I)     | Clad surface temperature at level I of average rod       | °C                                |
| TL/TG(I)  | Fluid temperature at level I                             | °C                                |
| PC(I)     | Pressure at level I                                      | kg/m <sup>2</sup>                 |
| HT(I)     | Heat transfer coefficient at level I of average rod      | kcal/m <sup>2</sup> ·h·°C         |
| HR(I)     | Radiative heat flux at level I of average rod (*3)       | kcal/m <sup>3</sup> ·h            |
| HCV(I)    | Convective heat flux at level I of average rod (*3)      | kcal/m <sup>3</sup> ·h            |
| G(I)      | Mass flux at level I                                     | kg·h/m <sup>3</sup>               |
| GG(I)     | Mass flux of gas at level I                              | kg·h/m <sup>3</sup>               |
| GL(I)     | Mass flux of liquid at level I                           | kg·h/m <sup>3</sup>               |

Table 4.6 Description of core state data (2/3)

(2) Local rod information (print out if IOPT02 ≠ 0)

| Data    | Description  | Unit                      |
|---------|--|---------------------------|
| TPN2    | Quench temperature of bottom quench point of local rod | °C                        |
| ZP2     | Position of bottom quench point of local rod           | m                         |
| I       | Number of level  | -                         |
| IPP     | Index of flow pattern at level I of local rod (*2)     | -                         |
| TWP(I)  | Clad surface temperature at level I of local rod       | °C                        |
| HTP(I)  | Heat transfer coefficient at level I of local rod      | kcal/m <sup>2</sup> ·h·°C |
| HRP(I)  | Radiative heat flux at level I of local rod (*3)       | kcal/m <sup>3</sup> ·h    |
| HCVP(I) | Convective heat flux at level I of local rod (*3)      | kcal/m <sup>3</sup> ·h    |

Note :

\*1

IB4 is the level just above the initiation point of dispersed flow.

\*2

Indices of flow pattern are defined as follows :

| Index | Flow regime  |
|-------|--|
| 1     | Single phase liquid flow or Subcooled nucleate boiling |
| 2     | Subcooled film boiling flow                            |
| 3     | Saturated two-phase flow                               |
| 4     | Transition flow  |
| 5     | Dispersed flow   |
| 6     | Single phase flow in rewetted region                   |
| 7     | Saturated two-phase flow rewetted region               |
| 8     | Superheated steam flow                                 |

\*3

This is multiplied heat flux by ( $\frac{CL}{SO}$ ).

Where, CL : wetted perimeter [m]

SO : cross section of flow area [m<sup>2</sup>]

Table 4.6 Description of core state data (3/3)

(3) Radial temperature distribution of average rod (print out if IOPT01 = 1)

| Data      | Description   | Unit |
|-----------|---|------|
| I         | Number of level                                     | -    |
| TF(1, I)  | Average rod temperature at radial node 1 of level I | °C   |
| }         |   | }    |
| TF(12, I) | at radial node 12 of level I                        | °C   |

(4) Radial temperature distribution of local rod (print out if IOPT01 = 1  
and IOPT02 ≠ 0)

| Data      | Description                                       | Unit |
|-----------|---|------|
| I         | Number of level                                   | -    |
| TFP(1,I)  | Local rod temperature at radial node 1 of level I | °C   |
| }         |   | }    |
| TFP(12,I) | at radial node 12 of level I                      | °C   |

Table 4.7 Description of system state data

| Data   | Description   | Unit                  |
|--------|---|-----------------------|
| USUP   | Supplied ECC water flow rate <sup>(*1)</sup>                                      | cm/s                  |
| ULIN   | Liquid velocity at core inlet <sup>(*1)</sup>                                     | cm/s                  |
| UDUP   | Liquid top velocity in downcomer <sup>(*1,2)</sup>                                | cm/s                  |
| UCUP   | Liquid top velocity in core <sup>(*1,2)</sup>                                     | cm/s                  |
| UGOUT  | Gas velocity at core outlet <sup>(*1)</sup>                                       | cm/s                  |
| ULOUT  | Liquid velocity at core outlet <sup>(*1)</sup>                                    | cm/s                  |
| UGLÖP  | Gas velocity in loop <sup>(*1,2)</sup>  | cm/s                  |
| CRF    | Carryover fraction  | —                     |
| DPDN   | Differential pressure between bottom of downcomer and containment <sup>(*2)</sup> | m Aq. <sup>(*3)</sup> |
| DPCR   | Differential pressure between upper and lower plenum <sup>(*2)</sup>              | m Aq.                 |
| DPLÖP  | Differential pressure between upper plenum and containment <sup>(*2)</sup>        | m Aq.                 |
| AMCOIN | Time-integrated mass flux at core inlet <sup>(*4)</sup>                           | kg/m <sup>2</sup>     |
| AMCOR  | Accumulated water in core calculated in REFLA1 <sup>(*4)</sup>                    | kg/m <sup>2</sup>     |
| AMGS   | Time-integrated mass flux of gas at core outlet <sup>(*4)</sup>                   | kg/m <sup>2</sup>     |
| AMLS   | Time-integrated mass flux of liquid at core outlet <sup>(*4)</sup>                | kg/m <sup>2</sup>     |
| MERROR | Error of mass balance <sup>(*4)</sup> (= AMCOIN-AMCOR-AMGS-AMLS)                  | kg/m <sup>2</sup>     |

Note:

<sup>\*1</sup>

This value is converted into core water state value. Namely, the mass flux is divided by core flow area and core water density.

<sup>\*2</sup>

This value is meaningless unless Z = 2.0.

<sup>\*3</sup>

1 m Aq. = 0.1 kg/cm<sup>2</sup>

<sup>\*4</sup>

This value is divided by core flow area.

Table 4.8 Description of time history data (1/5)

## (1) Control data

| Item     | Description   | Unit                 |
|----------|---|----------------------|
| MAXPOWER | Maximum linear power density of average rod                       | kW/m                 |
| FLOWRATE | Liquid velocity at core inlet                                     | cm/s                 |
| PRESSURE | Pressure at core inlet  | kg/cm <sup>2</sup>   |
| DPCORE   | Differential pressure between upper and lower plenum              | m Aq.                |
| DPDOWN   | Differential pressure between bottom of downcomer and containment | m Aq.                |
| DPLoop   | Differential pressure between upper plenum and containment        | m Aq.                |
| WGOUT    | Mass flux of gas at core outlet                                   | kg/m <sup>2</sup> ·h |

## (2) Temperature profile of average rod

| Item | Description   | Unit                |
|------|---|---------------------|
| TW1  | Clad surface temperature at elevation 1 of average rod  | °C                  |
| TW2  | Clad surface temperature at elevation 2 of average rod  | °C                  |
| TW3  | Clad surface temperature at elevation 3 of average rod  | °C                  |
| TW4  | Clad surface temperature at elevation 4 of average rod  | °C                  |
| TW5  | Clad surface temperature at elevation 5 of average rod  | °C                  |
| TW6  | Clad surface temperature at elevation 6 of average rod  | °C                  |
| HT3  | Heat transfer coefficient at elevation 3 of average rod | W/m <sup>2</sup> ·K |

## (3) Temperature profile of local rod (print out if IOPT02 ≠ 0)

| Item | Description   | Unit                |
|------|---|---------------------|
| TWP1 | Clad surface temperature at elevation 1 of local rod  | °C                  |
| TWP2 | Clad surface temperature at elevation 2 of local rod  | °C                  |
| TWP3 | Clad surface temperature at elevation 3 of local rod  | °C                  |
| TWP4 | Clad surface temperature at elevation 4 of local rod  | °C                  |
| TWP5 | Clad surface temperature at elevation 5 of local rod  | °C                  |
| TWP6 | Clad surface temperature at elevation 6 of local rod  | °C                  |
| HTP3 | Heat transfer coefficient at elevation 3 of local rod | W/m <sup>2</sup> ·K |

Table 4.8 Description of time history data (2/5)

(4) Quench data of average rod and entrainment carryover ratio

| Item     | Description   | Unit                |
|----------|---|---------------------|
| LC.SUBCL | Subcooling of liquid at node just above quench point of average rod | °C                  |
| QUENCHVL | Quench velocity of average rod                                      | cm/s                |
| QUENCHPT | Position of quench point of average rod                             | m                   |
| CARRYOVR | Entrainment carryover fraction                                      | -                   |
| QUENCHTP | Quench temperature of average rod                                   | °C                  |
| TW3      | Clad surface temperature at elevation 3 of average rod              | °C                  |
| HT3      | Heat transfer coefficient at elevation 3 of average rod             | W/m <sup>2</sup> ·K |

(5) Quench data of local rod (print out if IOPT02 ≠ 0)

| Item     | Description   | Unit                |
|----------|---|---------------------|
| LC.SUBCL | Subcooling of liquid at node just above quench point of local rod | °C                  |
| QUENCHVL | Quench velocity of local rod                                      | cm/s                |
| QUENCHPT | Position of quench point of local rod                             | m                   |
| QUENCHTP | Quench temperature of local rod                                   | °C                  |
| MAXPOWER | Maximum linear power density of local rod                         | kW/m                |
| TWP3     | Clad surface temperature at elevation 3 of local rod              | °C                  |
| HTP3     | Heat transfer coefficient at elevation 3 of local rod             | W/m <sup>2</sup> ·K |

(6) Heat transfer coefficient of average rod

| Item  | Description   | Unit                |
|-------|---|---------------------|
| HT1   | Heat transfer coefficient at elevation 1 of average rod | W/m <sup>2</sup> ·K |
| HT2   | Heat transfer coefficient at elevation 2 of average rod | W/m <sup>2</sup> ·K |
| HT3   | Heat transfer coefficient at elevation 3 of average rod | W/m <sup>2</sup> ·K |
| HT4   | Heat transfer coefficient at elevation 4 of average rod | W/m <sup>2</sup> ·K |
| HT5   | Heat transfer coefficient at elevation 5 of average rod | W/m <sup>2</sup> ·K |
| HT6   | Heat transfer coefficient at elevation 6 of average rod | W/m <sup>2</sup> ·K |
| VOID3 | Average void fraction between elevation 2 and 3 of core | -                   |

Table 4.8 Description of time history data (3/5)

(7) Heat transfer coefficient of local rod (print out if IOPT02 ≠ 0)

| Item  | Description   | Unit                |
|-------|---|---------------------|
| HTP1  | Heat transfer coefficient at elevation 1 of local rod   | W/m <sup>2</sup> ·K |
| HTP2  | Heat transfer coefficient at elevation 2 of local rod   | W/m <sup>2</sup> ·K |
| HTP3  | Heat transfer coefficient at elevation 3 of local rod   | W/m <sup>2</sup> ·K |
| HTP4  | Heat transfer coefficient at elevation 4 of local rod   | W/m <sup>2</sup> ·K |
| HTP5  | Heat transfer coefficient at elevation 5 of local rod   | W/m <sup>2</sup> ·K |
| HTP6  | Heat transfer coefficient at elevation 6 of local rod   | W/m <sup>2</sup> ·K |
| VOID3 | Average void fraction between elevation 2 and 3 of core | -                   |

(8) Void fraction

| Item     | Description  | Unit |
|----------|--|------|
| VOID1    | Average void fraction between bottom and the 1st elevation of core | -    |
| VOID2    | the 1st and the 2nd  | -    |
| VOID3    | the 2nd and the 3rd  | -    |
| VOID4    | the 3rd and the 4th  | -    |
| VOID5    | the 4th and the 5th  | -    |
| VOID6    | the 5th and the 6th  | -    |
| MAXPOWER | Maximum linear power density of average rod                        | kW/m |

Table 4.8 Description of time history data (4/5)

(12) Radial temperature distribution of local rod (print out IOPT01 = 1  
and IOPT02 ≠ 0)

| Item       | Description   | Unit |
|------------|---|------|
| AXIAL NODE | Axial node number   | -    |
| TFP(R.1)   | Local rod temperature at the 1st radial point of the defined axial node | °C   |
| TFP(R.2)   | Local rod temperature at the 2nd radial point of the defined axial node | °C   |
| TFP(R.3)   | Local rod temperature at the 3rd radial point of the defined axial node | °C   |
| TFP(R.4)   | Local rod temperature at the 4th radial point of the defined axial node | °C   |

Table 4.8 Description of time history data (5/5)

## (9) Movement of boundaries

| Item     | Description                        | Unit  |
|----------|------------------------------------|-------|
| LIQ.BOLL | Position of L1                     | m     |
| QUENCHPT | Position of L2                     | m     |
| SATURATE | Position of L3                     | m     |
| TRA-DISP | Position of L4                     | m     |
| REWETTED | Position of L5                     | m     |
| LIQ.LEV  | Position of L7                     | m     |
| PRESHEAD | Differential pressure head in core | m Aq. |

## (10) Core outlet condition

| Item       | Description                       | Unit |
|------------|-----------------------------------|------|
| GLOUT/G(1) | Core outlet liquid mass flow rate | kg/s |
| G(NL)/G(1) | Core outlet vapor mass flow rate  | kg/s |
| MDOT/G(1)  | Carryover fraction                | -    |

## (11) Radial temperature distribution of average rod (print out if IOPT01 = 1)

| Item       | Description   | Unit |
|------------|---|------|
| AXIAL NODE | Axial node number   | -    |
| TF(R.1)    | Average rod temperature at the 1st radial point of the defined axial node | °C   |
| TF(R.2)    | Average rod temperature at the 2nd radial point of the defined axial node | °C   |
| TF(R.3)    | Average rod temperature at the 3rd radial point of the defined axial node | °C   |
| TF(R.4)    | Average rod temperature at the 4th radial point of the defined axial node | °C   |

Table 4.9 Description of plotted measured data

| No. | Item                                   | Description  |
|-----|--|--|
| 1   | UL1/5+6<br>PC1-PCN1<br>DPDWN<br>DPLOOP | Core inlet liquid velocity (cm/s) ÷ 5 + 6<br>Differential pressure between upper and lower plenum<br>Differential pressure between bottom of downcomer and containment<br>Differential pressure between upper plenum and containment |
| 2   | TW(EL.1)<br>{<br>TW(EL.5)              | Clad surface temperature at the 1st elevation of average rod<br>}<br>5th   |
| 3   | TWP(EL1)<br>{<br>TWP(EL5)              | Clad surface temperature at the 1st elevation of local rod<br>}<br>5th   |
| 4   | AG(EL.1)<br>AG(EL.2)<br>{<br>AG(EL.6)  | Average void fraction between bottom and the 1st elevation of core<br>the 1st and the 2nd<br>}<br>the 5th and the 6th  |

Table 4.10 Description of plotted calculational data (1/4)

| No.   | Item   | Description   |
|---|--|---|
| 1   | 0 SEC<br>X <sub>1</sub> SEC<br>}<br>X <sub>N</sub> SEC | Axial clad surface temperature profile of average rod at 0 sec<br>x <sub>1</sub> sec <sup>(*1)</sup><br>}<br>x <sub>N</sub> sec <sup>(*1)</sup> |
| No. 2 is plotted if IOPT02 ≠ 0  |  |   |
| 2   | 0 SEC<br>X <sub>1</sub> SEC<br>}<br>X <sub>N</sub> SEC | Axial clad surface temperature profile local rod at 0 sec<br>x <sub>1</sub> sec <sup>(*1)</sup><br>}<br>x <sub>N</sub> sec <sup>(*1)</sup>      |
| 3 UL1/5+6 Core inlet liquid velocity (cm/s) : 5 + 6<br>PC1-PCN1 Differential pressure between upper and lower plenum<br>DPDWN Differential pressure between bottom of downcomer and containment |  |   |
| 4   | TW(EL.1)<br>}<br>TW(EL.6)                              | Clad surface temperature at the 1st elevation of average rod<br>}<br>6th<br>(Y-axis : 0 ~ 1200 °C)  |
| 5   | TW(EL.1)<br>}<br>TW(EL.6)                              | Clad surface temperature at the 1st elevation of average rod<br>}<br>6th<br>(Y-axis : 0 ~ 2000 °C)  |
| No. 6 and 7 are plotted if IOPT02 ≠ 0   |  |   |
| 6   | TWP(EL1)<br>}<br>TWP(EL5)                              | Clad surface temperature at the 1st elevation of local rod<br>}<br>5th  |
| 7   | TWP(46)  | Clad surface temperature at level 46 of local rod   |
| 8   | TQN2   | Quench temperature of average rod   |
| No. 9 is plotted if IOPT02 ≠ 0  |  |   |
| 9   | TPN2   | Quench temperature of local rod   |

Table 4.10 Description of plotted calculational data (2/4)

| No.                                    | Item   | Description  |
|--|--|--|
| 10                                     | HT(EL.1)<br>}  | Heat transfer coefficient at the 1st elevation of average rod<br>}<br>HT(EL.6)   |
|  |  | 6th  |
| No. 11 is plotted if IOPT02 ≠ 0        |  |  |
| 11                                     | HTP(EL1)<br>}  | Heat transfer coefficient at the 1st elevation of local rod<br>}<br>HTP(EL5)   |
| 12                                     | AG(EL.1)<br>AG(EL.2)<br>}                              | Average void fraction between bottom and the 1st elevation of core<br>the 1st and the 2nd<br>}<br>AG(EL.6)   |
| 13                                     | L1<br>L2<br>L3<br>L4<br>L5<br>L7                       | Position of L1<br>Position of L2<br>Position of L3<br>Position of L4<br>Position of L5<br>Position of L7   |
| No. 14 is plotted if IOPT02 ≠ 0        |  |  |
| 14                                     | LP2  | Position of bottom quench point of local rod   |
| 15                                     | GLOUT/G1<br>GN1/G1<br>MCDOT/G1                         | Core outlet liquid mass flow rate (kg/s)<br>Core outlet vapor mass flow rate (kg/s)<br>Carryover fraction  |
| No. 16 to 20 are plotted if IOPT01 = 1 |  |  |
| 16                                     | 0 SEC<br>X <sub>1</sub> SEC<br>}<br>X <sub>N</sub> SEC | Radial temperature profile of the 1st elevation of average rod at<br>0 sec<br>X <sub>1</sub> sec <sup>(*1)</sup><br>}<br>X <sub>N</sub> sec <sup>(*1)</sup><br>} |

Table 4.10 Description of plotted calculational data (3/4)

| No.   | Item   | Description   |
|---|--|---|
| 20  | 0 SEC<br>X <sub>1</sub> SEC<br>}<br>X <sub>N</sub> SEC | Radial temperature profile of the 5th elevation of average rod at<br>0 sec<br>X <sub>1</sub> sec <sup>(*1)</sup><br>}<br>X <sub>N</sub> sec <sup>(*1)</sup> |
| No. 21 to 25 are plotted if IOPT01 = 1 and IOPT02 ≠ 0 |  |   |
| 21  | 0 SEC<br>X <sub>1</sub> SEC<br>}<br>X <sub>N</sub> SEC | Radial temperature profile of the 1st elevation of local rod at<br>0 sec<br>X <sub>1</sub> sec <sup>(*1)</sup><br>}<br>X <sub>N</sub> sec <sup>(*1)</sup>   |
| {   |  |   |
| 25  | 0 SEC<br>X <sub>1</sub> SEC<br>}<br>X <sub>N</sub> SEC | Radial temperature profile of the 5th elevation of local rod at<br>0 sec<br>X <sub>1</sub> sec <sup>(*1)</sup><br>}<br>X <sub>N</sub> sec <sup>(*1)</sup>   |
| No. 26 to 30 are plotted if IOPT01 = 1                |  |   |
| 26  | TF(1,1)<br>}<br>TF(4,1)                                | Average rod temperature at the 1st radial point of the 1st elevation<br>}<br>4th  |
| {   |  |   |
| 30  | TF(1,5)<br>}<br>TF(4,5)                                | Average rod temperature at the 1st radial point of the 5th elevation<br>}<br>4th  |

Table 4.10 Description of plotted calculational data (4/4)

| No.   | Item                      | Description  |
|---|---------------------------|--|
| No. 31 to 35 are plotted if IOPT01 = 1 and IOPT02 ≠ 0 |                           |  |
| 31  | TFP(1,1)<br>}<br>TFP(4,1) | Local rod temperature at the 1st radial point of the 1st elevation<br>}<br>4th |
|   |                           |  |
| 35  | TPF(1,5)<br>}<br>TPF(4,5) | Local rod temperature at the 1st radial point of the 5th elevation<br>}<br>4th |

Note :

\*1

$$X_i = i \times DTS \times ICON(12)$$

Maximum number of the profile can be plotted is 9.

Table 4.11 Description of plotted data comparison between measured and calculated

| No.                            | Item                                  | Description  |
|--------------------------------|---------------------------------------|--|
| 1                              | UL1/5+6<br>PC1-PCN1<br>DPDWN          | Core inlet liquid velocity (cm/s) ÷ 5 + 6<br>Differential pressure between lower and upper plenum<br>Differential pressure between bottom of downcomer and containment |
| 2                              | TW(EL.1)<br>}<br>TW(EL.6)             | Clad surface temperature at the 1st elevation of average rod<br>}<br>6th<br>(Y-axis : 0 ~ 1200 °C)   |
| 3                              | TW(EL.1)<br>}<br>TW(EL.6)             | Clad surface temperature at the 1st elevation of average rod<br>}<br>6th<br>(Y-axis : 0 ~ 2000 °C)   |
| No. 4 is plotted if IOPT02 ≠ 0 |                                       |  |
| 4                              | TWP(EL1)<br>}<br>TWP(EL5)             | Clad surface temperature at the 1st elevation of local rod<br>}<br>5th   |
| 5                              | HT(EL.1)<br>}<br>HT(EL.6)             | Heat transfer coefficient at the 1st elevation of average rod<br>}<br>6th  |
| 6                              | AG(EL.1)<br>AG(EL.2)<br>}<br>AG(EL.6) | Average void fraction between bottom and the 1st elevation of core<br>the 1st and the 2nd<br>}<br>the 5th and the 6th  |
| 7                              | L2                                    | Position of bottom quench point of average rod   |
| No. 8 is plotted if IOPT02 ≠ 0 |                                       |  |
| 8                              | LP2                                   | Position of bottom quench point of local rod   |

Note :

Calculational data is plotted by line.

Measurement data is plotted by dotted line.

Table 4.12 JCL for REFLA-1D/MODE4 calculation (1/3)

## (1) In case of using radial fuel temperature one point model

```

//JCLG JOB
//JCLG EXEC JCLG
//SYSIN DD DATA,DLM='++'
// JUSER 00919089,TS.HOJO,0957.01
    T.5 W.3 I.4 C.4 GRP SRP
    OPTP PASSWORD=
/*JOBPARM K=0
//***** *****
//*   RUN J9089.REFLAPS.FORT   ***
//***** *****
//FR1 EXEC FORT77,SO='J9089.REFLAPS',A='ELM(*),NOS,LANGLVL(66)',..... 1)
//    Q='.FORT',DISP=MOD
//SYSPRINT DD DUMMY
//FR2 EXEC FORT77,SO='J2156.SYSTEM0',A='ELM(*),NOS,LANGLVL(66)',..... 2)
//    Q='.FORT',DISP=MOD
//SYSPRINT DD DUMMY
//FR3 EXEC FORT77,SO='J1207.UPLOT2',
//    A='ELM(GETTAG,GETTB,PUTDAT),NOS,LANGLVL(66)',Q='.FORT',DISP=MOD.. 3)
//SYSPRINT DD DUMMY
//FR4 EXEC FORT77,SO='J3105.SSPLOT',
//    A='ELM(*),NOS,LANGLVL(66)',Q='.FORT',DISP=MOD .. .... 4)
//SYSPRINT DD DUMMY
//LIK EXEC LKED77,GRLIB=PNL
//SYSPRINT DD DUMMY
//REFLA EXEC GO
//NLP EXPAND GRNLP,SYSPUT=N
//FT09F001 DD SYSOUT=*,DCB=(RECFM=FA,BLKSIZE=133)
//FT10F001 DD DSN=J3349.CC1J038.DATA,DISP=SHR,LABEL=(,,IN) ..... 5)
//FT20F001 DD DSN=J3349.CCTMJ038.DATA,DISP=SHR,LABEL=(,,IN)..... 6)
//DATA EXPAND DISKTO,DDN=SYSIN,DSN=J9089.REFLAPS,Q='DATA(C1R38B17)... 7)
++
//
```

- 1) Data set name for storing MAIN and core thermo-hydrodynamic calculation routine
- 2) Data set name for storing system calculation routine
- 3) Data set name for storing plot calculation routine 1
- 4) Data set name for storing plot calculation routine 2
- 5) Data set name for storing measured data 1 to use boundary condition determination and data comparison
- 6) Data set name for storing measured data 2 to use data comparison
- 7) Data set name for storing REFLA input data

Table 4.12 JCL for REFLA-1D/MODE4 calculation (2/3)

- (2) In case of using fuel temperature profile effect model  
(IOPT01=1 and IOPT02=0)

```

//JCLG JOB
//JCLG EXEC JCLG
//SYSIN DD DATA,DLM='++'
// JUSER 00919089,TS.HOJO,0957.01
    T.8 W.3 I.4 C.4 GRP SRP NGT
    OOPTP PASSWORD=
/*JOBPARM K=0
//***** *****
//* RUN J9089.REFLAPS.FORT ***
//***** *****
//FR1 EXEC FORT77,SO='J9089.REFLAPS',A='ELM(*),NOS,LANGLVL(66)',..... 1)
//   Q='.FORT',DISP=MOD
//SYSPRINT DD DUMMY
//FR2 EXEC FORT77,SO='J2156.SYSTEM0',A='ELM(*),NOS,LANGLVL(66)',..... 2)
//   Q='.FORT',DISP=MOD
//SYSPRINT DD DUMMY
//FR3 EXEC FORT77,SO='J1207.UPLOT2',
//   A='ELM(GETTAG,GETTB,PUTDAT),NOS,LANGLVL(66)',Q='.FORT',DISP=MOD ... 3)
//SYSPRINT DD DUMMY
//FR4 EXEC FORT77,SO='J3105.SSPL0T',
//   A='ELM(*),NOS,LANGLVL(66)',Q='.FORT',DISP=MOD ..... 4)
//SYSPRINT DD DUMMY
//LIK EXEC LKED77,GRLIB=PNL
//SYSPRINT DD DUMMY
//REFLA EXEC GO
//NLP EXPAND GRNLP,SYSOUT=N
//FT09F001 DD SYSOUT=*,DCB=(RECFM=FA,BLKSIZE=133) ..... 5)
//FT10F001 DD DSN=J3349.CC1J038.DATA,DISP=SHR,LABEL=(,,IN) ..... 6)
//FT20F001 DD DSN=J3349.CCTMJ038.DATA,DISP=SHR,LABEL=(,,IN) ..... 8)
//FT55F001 DD DSN=J9089.REFLAPS.DATA(HETCCTF),DISP=SHR ..... 7)
//DATA EXPAND DISKTO,DDN=SYSIN,DSN=J9089.REFLAPS,Q='DATA(REFEMI)'.... 7)
++
/

```

1)

{ Same as (1)

7)

8) Data set name for storing HETRAP input data

Table 4.12 JCL for REFLA-1D/MODE4 calculation (3/3)

- (3) In case of using local power effect model and fuel temperature profile effect model (OPPT01=1 and ITPT02=1)

```

//JCLG JOB
//JCLG EXEC JCLG
//SYSIN DD DATA,DLM='++'
// JUSER 00919089,TS.HOJO,0957.01
    T.9 W.5 I.4 C.4 GRP SRP NGT
    OPTP PASSWORD=
/*JOBPARM K=0
//***** *****
// * RUN J9089.REFLAPS.FORT   ***
//***** *****
//FR1 EXEC FORT77,SO='J9089.REFLAPS',A='ELM(*),NOS,LANGLVL(66)',..... 1)
//   Q='.FORT',DISP=MOD
//SYSPRINT DD DUMMY
//FR2 EXEC FORT77,SO='J2156.SYSTEM0',A='ELM(*),NOS,LANGLVL(66)',..... 2)
//   Q='.FORT',DISP=MOD
//SYSPRINT DD DUMMY
//FR3 EXEC FORT77,SO='J1207.UPLOT2',
//   A='ELM(GETTAG,GETTB,PUTDAT),NOS,LANGLVL(66)',Q='.FORT',DISP=MOD..... 3)
//SYSPRINT DD DUMMY
//FR4 EXEC FORT77,SO='J3105.SS PLOT',
//   A='ELM(*),NOS,LANGLVL(66)',Q='.FORT',DISP=MOD ..... 4)
//SYSPRINT DD DUMMY
//LIK EXEC LKED77,GRLIB=PNL
//SYSPRINT DD DUMMY
//REFLA EXEC GO
//NLP EXPAND GRNLP,SYSOUT=N
//GDFILE DD SYSOUT=N,OUTLIM=80000,DEST=LOCAL
//FT09F001 DD SYSOUT=*,DCB=(RECFM=FA,BLKSIZE=133)
//FT10F001 DD DSN=J3349.CC1J038.DATA,DISP=SHR,LABEL=(,,IN)..... 5)
//FT20F001 DD DSN=J3349.CCTMJ038.DATA,DISP=SHR,LABEL=(,,IN)..... 6)
//FT55F001 DD DSN=J9089.REFLAPS.DATA(HETCCTF),DISP=SHR ..... 8)
//DATA EXPAND DISKTO,DDN=SYSIN,DSN=J9089.REFLAPS,Q='DATA(RZFUELPS)' .... 7)
+*
//
```

1)

? Same as (2)

8)

## 5. サンプル計算

作成した REFLA-1D/MODE 4 コードによるサンプル計算を示す。対象とした試験は CCTF 試験 C 1-19 (Run 38)<sup>(6)</sup> で、局所燃料棒としてはバンドル 17 の Y-rod を選定した。なお、この燃料棒の半径方向ピーキング係数は 1.10 である。

### 5.1 CCTF 試験 C 1-19 の試験条件

CCTF 試験 C 1-19 の試験条件を表 5.1 に示す。

### 5.2 入力データ

CCTF 試験 C 1-19 計算用入力データを表 5.2 に示す。

### 5.3 プリント出力およびプロット出力

CCTF 試験 C 1-19 計算結果のプリント出力およびプロット出力を付録 C に示す。

Table 5.1 Summary of test conditions for CCTF test Cl-19 (Run 38)

1. TEST TYPE : EVALUATION MODEL TEST
2. TEST NUMBER : RUN 038                            3. DATE : March 18, 1981
4. POWER : A: TOTAL: 9.28 MW; B:LINEAR: 1.39 KW/M
5. RELATIVE RADIAL POWER SHAPE :
 

|           |              |              |              |
|-----------|--------------|--------------|--------------|
| A: ZONE:  | A            | B            | C            |
| B: RATIO: | <u>1.299</u> | <u>1.092</u> | <u>0.841</u> |
6. AXIAL POWER SHAPE : CHOPPED COSINE
7. PRESSURE (KG/CM<sup>2</sup>A) :
 

|                               |             |                |             |
|-------------------------------|-------------|----------------|-------------|
| A: SYSTEM:                    | <u>2.03</u> | B: CONTAINMENT | <u>2.03</u> |
| C: STEAM GENERATOR SECONDARY: | <u>53.2</u> |                |             |
8. TEMPERATURE (DEG.C) :
 

|                                       |             |                              |            |
|---------------------------------------|-------------|------------------------------|------------|
| A: DOWNCOMER WALL                     | <u>169</u>  | B: VESSEL INTERNALS          | <u>115</u> |
| C: PRIMARY PIPING WALL                | <u>123</u>  | D: LOWER PELNUM LIQUID       | <u>114</u> |
| E: ECC LIQUID                         | <u>38.1</u> | F: STEAM GENERATOR SECONDARY | <u>263</u> |
| G: CORE TEMPERATURE AT ECC INITIATION | <u>844</u>  |                              |            |
9. ECC INJECTION TYPE: C
 

|              |                  |                            |
|--------------|------------------|----------------------------|
| A: COLD LEG, | B: LOWER PLENUM, | C: LOWER PLENUM + COLD LEG |
|--------------|------------------|----------------------------|
10. PUMP K-FACTOR : ~ 15
11. ECC FLOW RATES AND DURATION :
 

|                                    |                              |          |             |           |             |         |
|------------------------------------|------------------------------|----------|-------------|-----------|-------------|---------|
| A: ACCUMULATOR                     | <u>372 M<sup>3</sup>/HR</u>  | FROM     | <u>0</u>    | TO        | <u>25.5</u> | SECONDS |
| B: LPCI                            | <u>40.5 M<sup>3</sup>/HR</u> | FROM     | <u>25.5</u> | TO        | <u>737</u>  | SECONDS |
| C: ECC INJECTION TO LOWER PLENUM : | FROM                         | <u>0</u> | TO          | <u>14</u> | SECONDS     |         |

(VALVE OPENING AND CLOSING TIMES ARE INCLUDED IN THE INJECTION DURATION)
12. INITIAL WATER LEVEL IN LOWER PLENUM : 0.89 M.
13. POWER CONTROL : ANS x 1.2 + ACTINIDE ( 30 SEC AFTER SCRAM)
14. EXPECTED BOCREC TIME FROM ECC INITIATION 9 SEC
15. EXPECTED PEAK TEMPERATURE AT BOCREC 870 C

Table 5.2 Input data for CCTF test C1-19 (Run 38) (1/2)

## (1) REFLA input data

```

** REFLAPS RUN ( IOPT = 1,1 ) **      CCTF CORE-I ( RUN 38 , BUNDLE 17 )
1   1
    2.086      0.25      7.0      100.      2.000      2.000
    100.0      8.0       8.0       0.1
    1 1.10  375.6 621.3 760.0 672.2 493.3
    90          10.7      14.3      3.66
    .1           0.25
                  10.8      2000.0     0.41318

720.0

1000.0
480.0      1500.0
120.0

5
2      .10     22      2.0     211      2.0     215     20.0
212  400.0

38
TE18Z11
TE18Z12
TE18Z13
TE18Z14
TE18Z15
DPLLOOP1
DPDOWN5
DPLLOOP4
DPCOREA
LT07RQ5V
LT06RQ5V
LT05RQ5V
LT04RQ5V
LT03RQ5V
LT02RQ5V
ULCRI1
TACRIN
LT01RQ5
PTOORNO
TE32X13
TE17Y11
TE17Y12
TE17Y13
TE17Y14
TE17Y15
HTE18Z11
HTE18Z12
HTE18Z13
HTE18Z14
HTE18Z15

```

Table 5.2 Input data for CCTF test Cl-19 (Run 38) (2/2)

## (2) HETRAP input data

|         |        |        |        |      |      |
|---------|--------|--------|--------|------|------|
| 3       |        |        |        |      |      |
| 1       | 33     |        |        |      |      |
| 12      |        |        |        |      |      |
| 5.35D-1 | 0.0D00 | 0.0D00 | 0.0D00 | 0    | 7    |
| 5.10D-1 |        |        |        | 7    | 7    |
| 4.75D-1 |        |        |        | 7    | 7    |
| 4.35D-1 |        |        |        | 7    | 7    |
| 4.00D-1 |        |        |        | 4    | 4    |
| 3.65D-1 |        |        |        | 4    | 4    |
| 3.30D-1 | 1.0D00 |        |        | 4    | 10   |
| 2.70D-1 | 1.0D00 |        |        | 10   | 10   |
| 2.25D-1 |        |        |        | 9    | 9    |
| 1.75D-1 |        |        |        | 9    | 9    |
| 1.00D-1 |        |        |        | 9    | 9    |
| 0.00D00 |        |        |        | 9    | 9    |
| 34      | 58     |        |        |      |      |
| 12      |        |        |        |      |      |
| 5.35D-1 | 0.0D00 | 0.0D00 | 0.0D00 | 0    | 7    |
| 5.10D-1 |        |        |        | 7    | 7    |
| 4.75D-1 |        |        |        | 7    | 7    |
| 4.35D-1 |        |        |        | 7    | 7    |
| 4.00D-1 |        |        |        | 3    | 3    |
| 3.65D-1 |        |        |        | 3    | 3    |
| 3.30D-1 | 1.0D00 |        |        | 3    | 10   |
| 2.70D-1 | 1.0D00 |        |        | 10   | 10   |
| 2.25D-1 |        |        |        | 9    | 9    |
| 1.75D-1 |        |        |        | 9    | 9    |
| 1.00D-1 |        |        |        | 9    | 9    |
| 0.00D00 |        |        |        | 9    | 9    |
| 59      | 91     |        |        |      |      |
| 12      |        |        |        |      |      |
| 5.35D-1 | 0.0D00 | 0.0D00 | 0.0D00 | 0    | 7    |
| 5.10D-1 |        |        |        | 7    | 7    |
| 4.75D-1 |        |        |        | 7    | 7    |
| 4.35D-1 |        |        |        | 7    | 7    |
| 4.00D-1 |        |        |        | 4    | 4    |
| 3.65D-1 |        |        |        | 4    | 4    |
| 3.30D-1 | 1.0D00 |        |        | 4    | 10   |
| 2.70D-1 | 1.0D00 |        |        | 10   | 10   |
| 2.25D-1 |        |        |        | 9    | 9    |
| 1.75D-1 |        |        |        | 9    | 9    |
| 1.00D-1 |        |        |        | 9    | 9    |
| 0.00D00 |        |        |        | 9    | 9    |
| 0.02    |        |        |        |      |      |
| 1       |        |        |        |      |      |
| 1       | 91     |        |        |      |      |
| 120.    | 120.   | 120.   | 120.   | 120. | 120. |
| 120.    | 120.   | 120.   | 120.   | 120. | 120. |

## 6. ま　と　め

REFLA-1D/MODE 3 コードは、強制注水時ならびに FLECHT-SET Phase A のようなシステムにおけるダウンカマからの重力差による注水時の再冠水過程炉心内熱水力挙動の解析が可能なコードである。このコードに、局所出力効果モデルおよび燃料棒半径方向温度分布モデルの組込みを行い、これらの効果を考慮した解析が可能な REFLA-1D/MODE 4 を作成した。

作成したコードでは、水平方向出力分布効果を考慮した局所燃料棒温度変化の計算および実燃料棒の模擬等が可能となった。

今後の改良としては、多ループシステムモデル、グリッドスペーサモデル等の組込みを予定している。

### 謝　　辞

終りに、本報告書をまとめるに当たり御指導をいただいた佐藤一男、平野見明、斯波正誼、の各氏に感謝の意を表します。

また、本プログラムを開発する際に、有益な討論と助力を賜わりました安全工学第2研究室の各位に深謝致します。

## 6. ま　と　め

REFLA-1D/MODE 3 コードは、強制注水時ならびに FLECHT-SET Phase A のようなシステムにおけるダウンカマからの重力差による注水時の再冠水過程炉心内熱水力挙動の解析が可能なコードである。このコードに、局所出力効果モデルおよび燃料棒半径方向温度分布モデルの組込みを行い、これらの効果を考慮した解析が可能な REFLA-1D/MODE 4 を作成した。

作成したコードでは、水平方向出力分布効果を考慮した局所燃料棒温度変化の計算および実燃料棒の模擬等が可能となった。

今後の改良としては、多ループシステムモデル、グリッドスペーサモデル等の組込みを予定している。

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## 付録 A 燃料棒半径方向温度分布モデル組込みにともなう追加・修正

**common block および sub program**

## A. 1 追加 Common block

| COMMON/GUIDE / |               |       |                      |      |
|----------------|---------------|-------|----------------------|------|
| No.            | Variable Name | Type  | Content.             | Unit |
| 1              | TMIN          | R * 8 | 未使用                  |      |
| 2              | TMAX          | "     | "                    |      |
| 3              | TSTART        | "     | "                    |      |
| 4              | DTA           | "     | HETRAP 最小 time step巾 | sec  |
| 5              | DTWRIT        | "     | 未使用                  |      |
| 6              | KROD          | I * 4 | "                    |      |

| COMMON/HETRAP/ |                |       |  |   |
|----------------|----------------|-------|--|---|
| No.            | Variable Name  | Type  | Content.   | Unit                                    |
| 1              | DT             | R * 8 | 未使用  |   |
| 2              | DTMAX (20)     | "     | R 方向 node 間 $\Delta t$ max   | sec                                     |
| 3              | DTM            | "     | $\Delta t$ (HETRAP)  | "                                       |
| 4              | DUMMY          | "     | 未使用  |   |
| 5              | F (20)         | "     | "  |   |
| 6              | HCAP (20)      | "     | $\rho C_p V$   | $\frac{W \cdot sec}{cm \cdot ^\circ C}$ |
| 7              | HGAP           | "     | 未使用  |   |
| 8              | HVER (20)      | "     | $(\text{熱抵抗})^{-1}$  | $W/cm^\circ C$                          |
| 9              | STOR           | "     | 未使用  |   |
| 10             | QVO            | "     | $Q / \sum P_t \cdot V$ <small>Q : rod 発熱量<br/>P : Power factor</small> | $W/cm^2$                                |
| 11             | QVOL           | "     | 未使用  |   |
| 12             | RMQ            | "     | $(r_{i-1}^2 - r_i^2) / 2 \cdot \log(r_{i-1}/r_i)$                      | $cm^2$                                  |
| 13             | TIME           | "     | 未使用  |   |
| 14             | S (20, 91)     | "     | 前 node 半径  | cm                                      |
| 15             | T (20, 91)     | "     | 燃料棒温度 <small>OLD</small>   | $^\circ C$                              |
| 16             | TN (20, 91, 2) | "     | <small>NEW</small>   | $^\circ C$                              |
| 17             | V (20, 91)     | "     | R 方向 mesh 体積   | $cm^3/cm$                               |
| 18             | VER (20, 91)   | "     | $\log(r_{i-1}/r_i)$  | -                                       |
| 19             | IFCAN          | I * 4 | 未使用  |   |
| 20             | IFCEN          | "     | "  |   |
| 21             | IGAP           | "     | "  |   |
| 22             | IFCURR         | "     | "  |   |
| 23             | IFH            | "     | "  |   |
| 24             | IFQ            | "     | "  |   |
| 25             | IFT            | "     | "  |   |
| 26             | IFALL          | "     | node 間熱伝導計算用オプション  |   |
| 27             | IFP            | "     | 未使用  |   |
| 28             | IZ             | "     |  |   |

| COMMON/OPTION/ |               |       |                    |      |
|----------------|---------------|-------|--------------------|------|
| No.            | Variable Name | Type  | Content            | Unit |
| 1              | IOPT 01       | I * 4 | 燃料棒半径方向温度分布計算オプション |      |
| 2              | IOPT 02       | "     | 局所出力効果モデル使用オプション   |      |

| COMMON/RHINTR/ |               |       |                    |      |
|----------------|---------------|-------|--------------------|------|
| No.            | Variable Name | Type  | Content            | Unit |
| 1              | NZ 1          | I * 4 | Z 軸方向分割点数          |      |
| 2              | NR 1 (91)     | "     | R 方向 "             |      |
| 3              | NCLAD (2, 91) | "     | R 方向 clad 部 node 点 |      |
| 4              | NPLET (2, 91) | "     | " pellet 部 "       |      |

| COMMON/ROD/ |               |       |               |        |
|-------------|---------------|-------|---------------|--------|
| No.         | Variable Name | Type  | Content       | Unit   |
| 1           | R (20, 91)    | R * 8 | node 点 R 座標   | cm     |
| 2           | PF (20, 91)   | "     | power factor  | -      |
| 3           | H (20, 91)    | "     | node 間熱伝達率    | W/cm°C |
| 4           | E (20, 91)    | "     | " 輻射率         | -      |
| 5           | IWC (20, 91)  | I * 4 | 前 node 物質 No. | -      |
| 6           | IWP (20, 91)  | "     | 現 "           | -      |

## A.2.1 修正 sub program

## (1) Subroutine REFLA 1

(修正内容)

本文中の図 3.3 に示したフローチャート参照

## (2) Subroutine REFLAA

(修正内容)

燃料棒半径方向温度分布モデル使用時のクエンチによる燃料棒から流体への熱放出計算部分の修正。

修正部分のフローチャートを図 A.1 に示す。

## (3) Subroutine DISPRM, SATTPF, SINGLF, TRNSRM

(修正内容)

クエンチによる燃料棒から流体への熱放出量計算部分の修正

## 1) 瞬時熱放出量

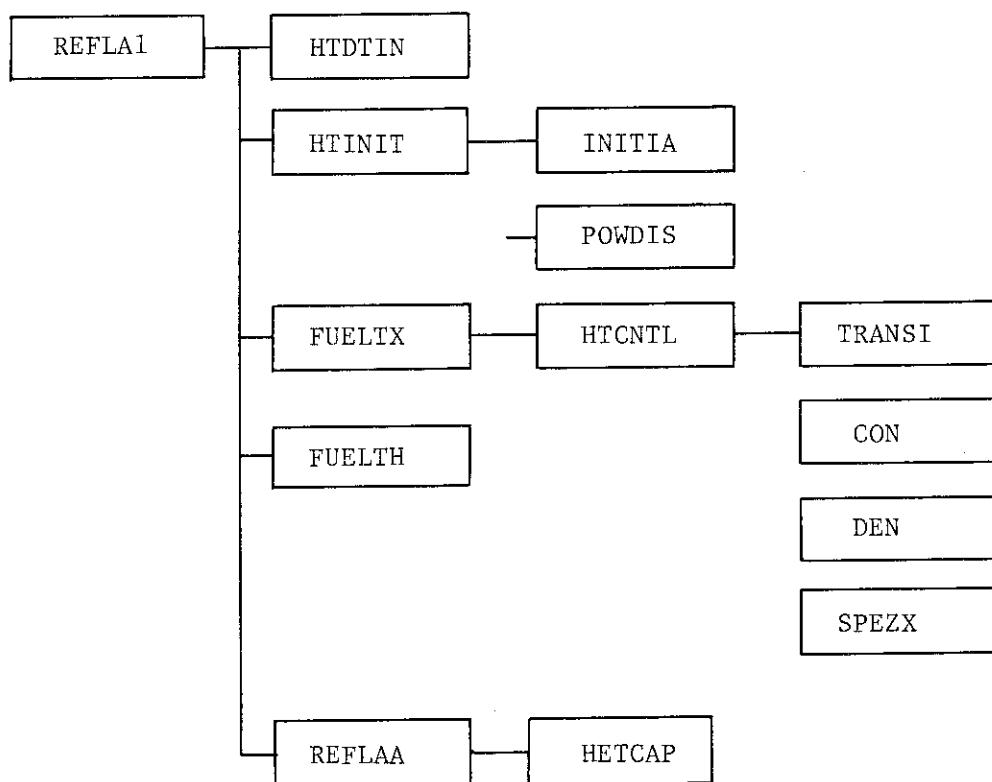
$$\left\{ \begin{array}{l} FCPRV = FCPQ(I) * ASTORE \quad (\text{半径方向 1 点近似計算}) \\ FCPRV = FCPQ(I) \quad (\text{半径方定温度分布計算}) \end{array} \right.$$

## 2) 減衰熱放出量

$$\left\{ \begin{array}{l} Q_{QD} = (1.0 - ASTORE) / QTAW * FCPR(I) \\ \quad * EXP(-QTIME(I)/QTAW) \quad (\text{半径方向 1 点近似計算}) \\ Q_{QD} = 1.0 / QTAW * FCPR(I) * EXP(-QTIME(I)/QTAW) \\ \quad (\text{半径方向温度分布計算}) \end{array} \right.$$

## A.2 追加修正 Sub program

燃料棒半径方向温度分布モデルの組込みにともなって追加修正した Sub program の構造を以下に示す。



| Module Description Sheet |   |              | Page |
|--------------------------|---|--------------|------|
| Module name              | HTINIT  | Project name |      |
| Module type              | Subroutine  | Coder        |      |
| Module number            |   | Date         |      |
| Called by                | REFLA1  |              |      |
| Calls                    | POWDIS, INITIA  |              |      |
| Argument                 | <u>無し</u>   |              |      |
| 呼び出し形式                   | CALL HTINIT   |              |      |
| 機能及び処理                   | <ul style="list-style-type: none"> <li>• HETRAP routine initialize</li> </ul> |              |      |

## A. 2.2 追加 Sub program

| Module Description Sheet |                                      | Page         | / |
|--------------------------|--------------------------------------|--------------|---|
| Module name              | HTDTIN                               | Project name |   |
| Module type              | Subroutine                           | Coder        |   |
| Module number            |                                      | Date         |   |
| Called by                | REFLA1                               |              |   |
| <u>Argument</u>          | 無し                                   |              |   |
| <u>呼び出し形式</u>            | CALL HTDTIN                          |              |   |
| <u>機能及び処理</u>            | 燃料体温度場計算 routine (HETRAP) 入力データの読み込み |              |   |
| <u>入力データ</u>             |                                      |              |   |
| 1° NDZ MAX               | : Z 軸方向パラメタ場設定数 (一様の時は 1)            |              |   |
| 2° NDZ 1, NDZ 2          | : Z 軸方向パラメタ設定 node 点 no.             |              |   |
| 3° NR 1                  | : R 方向 node 点数                       |              |   |
| 4° R                     | : R 方向 node 点 R 座標値                  |              |   |
| 5° PF                    | : Dower factor                       |              |   |
| 6° H                     | : 热伝達率                               |              |   |
| 7° E                     | : 輻射率                                |              |   |
| 8° INC                   | : 前 node 物質 no                       |              |   |
| 9° IWP                   | : 現 node "                           |              |   |
| 10° DTA                  | : HETRAP $\Delta t$                  |              |   |
| 11° NTZ MAZ              | : Z 軸方向初期温度分布設定数                     |              |   |
| 12° NTZ 1, NTZ 2         | : Z 軸方向パラメタ設定 node 点 no.             |              |   |
| 13° TN                   | : 初期温度分布                             |              |   |

| Module Description Sheet      |                 |              | Page | / |
|-------------------------------|-----------------|--------------|------|---|
| Module name                   | POWDIS          | Project name |      |   |
| Module type                   | Subroutine      | Coder        |      |   |
| Module number                 |                 | Date         |      |   |
| Called by                     | HTINIT          |              |      |   |
| Calls                         |                 |              |      |   |
| <u>Argument</u>               |                 |              |      |   |
| V                             | : R 方向 Mesh 体積  |              |      |   |
| PF                            | : Power factor  |              |      |   |
| NGES                          | : R 方向 mesh 分割数 |              |      |   |
| <u>呼び出し形式</u>                 |                 |              |      |   |
| CALL POWDIS(V, PF, NGES)      |                 |              |      |   |
| <u>機能及び処理</u>                 |                 |              |      |   |
| R 方向 Power factor の normalize |                 |              |      |   |

| Module Description Sheet |   |              | Page | / |
|--------------------------|---|--------------|------|---|
| Module name              | INITIA  | Project name |      |   |
| Module type              | Subroutine  | Coder        |      |   |
| Module number            |   | Date         |      |   |
| Called by                | HTINIT  |              |      |   |
| Calls                    |   |              |      |   |
| <u>Argument</u>          |   |              |      |   |
| J                        | : Z 軸方向 node 点 no.                                |              |      |   |
| <u>呼び出し形式</u>            |   |              |      |   |
| CALL INITIA(J)           |   |              |      |   |
| <u>機能及び処理</u>            |   |              |      |   |
| HETRAP routine 初期値設定     |   |              |      |   |
| VER(i,j)                 | : $\log(r_{i-1}/r_i)$                             |              |      |   |
| RMQ(i,j)                 | : $(r_{i-1}^2 - r_i^2)/2 \cdot \log(r_{i-1}/r_i)$ |              |      |   |
| V(i,j)                   | : Mesh 体積   |              |      |   |
| IFALL <sub>ij</sub>      | : node 間熱伝導計算用 flag                               |              |      |   |
| NCLAD <sub>j</sub>       | : clad 部分 node 点 no.                              |              |      |   |
| NPLET <sub>j</sub>       | : pellet 部分 node 点 no.                            |              |      |   |

| Module Description Sheet     |            |              | Page / |
|------------------------------|------------|--------------|--------|
| Module name                  | FUELTX     | Project name |        |
| Module type                  | Subroutine | Coder        |        |
| Module number                |            | Date         |        |
| Called by                    | REFLA1     |              |        |
| Calls                        | PX, HTCNTL |              |        |
| <u>Argument</u>              |            |              |        |
| DTX : REFLA time step巾 (sec) |            |              |        |
| <u>呼び出し形式</u>                |            |              |        |
| CALL FUELTX (DTX)            |            |              |        |
| <u>機能及び処理</u>                |            |              |        |
| 燃料棒温度分布の設定                   |            |              |        |
| 図 A.2 にフローチャートを示す。           |            |              |        |

| Module Description Sheet   |            |              | Page / |
|--|------------|--------------|--------|
| Module name  | HTCNTL     | Project name |        |
| Module type  | Subroutine | Coder        |        |
| Module number  |            | Date         |        |
| Called by  | FUELTX     |              |        |
| Calls  | TRANSI     |              |        |
| <u>Argument</u>  |            |              |        |
| QMAX <sub>j</sub> : rod 出力 (kcal/m·h)                              |            |              |        |
| TCOOL <sub>j</sub> : Coolant 温度 (°C)                               |            |              |        |
| HCOOL <sub>j</sub> : 热伝達率 (kcal/m <sup>2</sup> ·h·°C)              |            |              |        |
| TFIN : REFLA time step巾 (sec)                                      |            |              |        |
| TFUEL <sub>ij</sub> : 燃料棒温度分布 (°C)                                 |            |              |        |
| <u>呼び出し形式</u>  |            |              |        |
| CALL HTCNTL (QMAX, TCOOL, HCOOL, TFIN, TFUEL)                      |            |              |        |
| <u>機能及び処理</u>  |            |              |        |
| 燃料棒温度分布計算 routine "TRANSI" を制御し, "REFLA" の次期 time step の温度分布を設定する。 |            |              |        |
| 図 A.3 にフローチャートを示す。   |            |              |        |

| Module Description Sheet                               |                               |              | Page |
|--|-------------------------------|--------------|------|
| Module name  | TRANSI                        | Project name |      |
| Module type  | Subroutine                    | Coder        |      |
| Module number  |                               | Date         |      |
| Called by  | HTCNTL                        |              |      |
| Calls  | DEN CON SPEZX                 |              |      |
| <u>Argument</u>  |                               |              |      |
| J  | Z 軸方向 node no.                | ( IN )       |      |
| RODPOW   | rod 出力 (W/cm)                 | ( " )        |      |
| TCOOL  | coolant 温度 (°C)               | ( " )        |      |
| HCOOL  | 熱伝達率 (W/cm <sup>2</sup> · °C) | ( " )        |      |
| DTFUEL <sub>i</sub>                                    | 燃料棒温度変化量 (°C/sec)             | ( out )      |      |
| DTIME  | time step 巾 (sec)             | ( out )      |      |
| <u>呼び出し形式</u>  |                               |              |      |
| CALL TRANSI ( J, PODPOW, TCOOL, HCOOL, DTFUEL, DTIME ) |                               |              |      |
| <u>機能及び処理</u>  |                               |              |      |
| Rod 出力, Coolant 温度及び熱伝達率から, 燃料棒における $\dot{T}$ を計算する。   |                               |              |      |
| 図 A.4 にフローチャートを示す。                                     |                               |              |      |

| Module Description Sheet                |                |              | Page |
|---|----------------|--------------|------|
| Module name                             | SPEZX          | Project name |      |
| Module type                             | Function       | Coder        |      |
| Module number                           |                | Date         |      |
| Called by                               | TRANSI, HETCAP |              |      |
| Calls                                   |                |              |      |
| <u>Argument</u>                         |                |              |      |
| I W                                     | 物質 no.         |              |      |
| TW                                      | 温度 (°C)        |              |      |
| <u>呼び出し形式</u>                           |                |              |      |
| A = SPEZX( IW, TW )                     |                |              |      |
| <u>機能及び処理</u>                           |                |              |      |
| 物質 no. IW, 温度 TWにおける比熱 (W·sec/g·°C) を計算 |                |              |      |

| Module Description Sheet                        |                                |              | Page / |  |  |  |
|---|--------------------------------|--------------|--------|--|--|--|
| Module name                                     | DEN                            | Project name |        |  |  |  |
| Module type                                     | Function                       | Coder        |        |  |  |  |
| Module number                                   |                                | Date         |        |  |  |  |
| Called by                                       | TRANSI , HETCAP                |              |        |  |  |  |
| <u>Argument</u>                                 |                                |              |        |  |  |  |
| IW : 物質 no.                                     |                                |              |        |  |  |  |
| TW : 溫度 (°C)                                    |                                |              |        |  |  |  |
| <u>呼び出し形式</u>                                   |                                |              |        |  |  |  |
| A = DEN ( IW, TW)                               |                                |              |        |  |  |  |
| <u>機能及び処理</u>                                   |                                |              |        |  |  |  |
| 物質 no. IW, 溫度 TWにおける密度 (g/cm <sup>3</sup> ) を計算 |                                |              |        |  |  |  |
| I W   | 物質                             |              |        |  |  |  |
| 1   | Zircaloy - 4                   |              |        |  |  |  |
| 2   | UO <sub>2</sub>                |              |        |  |  |  |
| 3   | BN                             |              |        |  |  |  |
| 4   | MgO                            |              |        |  |  |  |
| 5   | Stainless Steel 316            |              |        |  |  |  |
| 6   | Inconel 800                    |              |        |  |  |  |
| 7   | Inconel 600                    |              |        |  |  |  |
| 8   | Stainless Steel 347            |              |        |  |  |  |
| 9   | Al <sub>2</sub> O <sub>3</sub> |              |        |  |  |  |
| 10  | NCH - 1                        |              |        |  |  |  |

| Module Description Sheet                             |          |              | Page |  |  |  |
|--|----------|--------------|------|--|--|--|
| Module name  | CON      | Project name |      |  |  |  |
| Module type  | Function | Coder        |      |  |  |  |
| Module number  |          | Date         |      |  |  |  |
| Called by  | TRANSI   |              |      |  |  |  |
| <u>Argument</u>                                      |          |              |      |  |  |  |
| IW : 物質 no.  |          |              |      |  |  |  |
| TP 1 : 溫度 $T_1$ (°C)                                 |          |              |      |  |  |  |
| TP 2 : " $T_2$                                       |          |              |      |  |  |  |
| <u>呼び出し形式</u>  |          |              |      |  |  |  |
| A = CON ( IW, TP 1, TP 2 )                           |          |              |      |  |  |  |
| <u>機能及び処理</u>  |          |              |      |  |  |  |
| 物質 no. IW, 溫度 $T_1$ , $T_2$ 間の熱伝導率 (W/cm · °C) を求める。 |          |              |      |  |  |  |

| Module Description Sheet                                 |             |              | Page |  |  |  |
|--|-------------|--------------|------|--|--|--|
| Module name  | HETCAP      | Project name |      |  |  |  |
| Module type  | Subroutine  | Coder        |      |  |  |  |
| Module number  |             | Date         |      |  |  |  |
| Called by  | REFLAA      |              |      |  |  |  |
| Calls  | DEN, SPEZZX |              |      |  |  |  |
| <u>Argument</u>  |             |              |      |  |  |  |
| J : Z 軸方向 nod no. (IN)                                   |             |              |      |  |  |  |
| TFUEL : R 方向温度分布 (IN)                                    |             |              |      |  |  |  |
| FCF : $\rho C_p V$ (out)                                 |             |              |      |  |  |  |
| <u>呼び出し形式</u>  |             |              |      |  |  |  |
| CALL HETCAP ( J, TFUEL, FCF )                            |             |              |      |  |  |  |
| <u>機能及び処理</u>  |             |              |      |  |  |  |
| 燃料棒 R 方向温度分布から、各 node 点における $\rho C_p V$ (kcal/m) を計算する。 |             |              |      |  |  |  |

## subroutine FUELTH

再冠水開始時の Local Rod 軸方向被覆管表面温度実験データ TBOC(I), I = 1, 5 と再冠水開始時 Ave. Rod 軸方向被覆管表面温度分布の計算値 TW(J), J = 1, 91 を用いて、再冠水開始時 Local Rod 軸方向被覆管表面温度 TWP(J), J = 1, 91 を内挿する Subroutine.

## TWP(J) の計算式

$$\left\{ \begin{array}{l} \text{① } A(J) = AI(1) : (J \leq II(1)) \\ \text{② } A(J) = AI(K) \times \frac{J - II(K-1)}{II(K) - II(K-1)} + AI(K-1) \times \frac{II(K) - J}{II(K) - II(K-1)} \\ \quad : (II(K-1) < J \leq II(K), K = 2, 5) \\ \text{③ } A(J) = AI(5) : (J > II(5)) \end{array} \right. \quad TWP(J) = \frac{TBOC(I) - T_{sat}}{TW(II(I)) - T_{sat}} \quad (I = 1, 5)$$

TWP(J) : ノード J の Local Rod 被覆管表面温度

TW(J) : " Ave. Rod "

$T_{sat}$  : 鮎和温度

TBOC(I) : 測定点 I の再冠水開始時 Local Rod 被覆管表面温度

II(I) : 測定点 I に対応する軸方向のノード番号

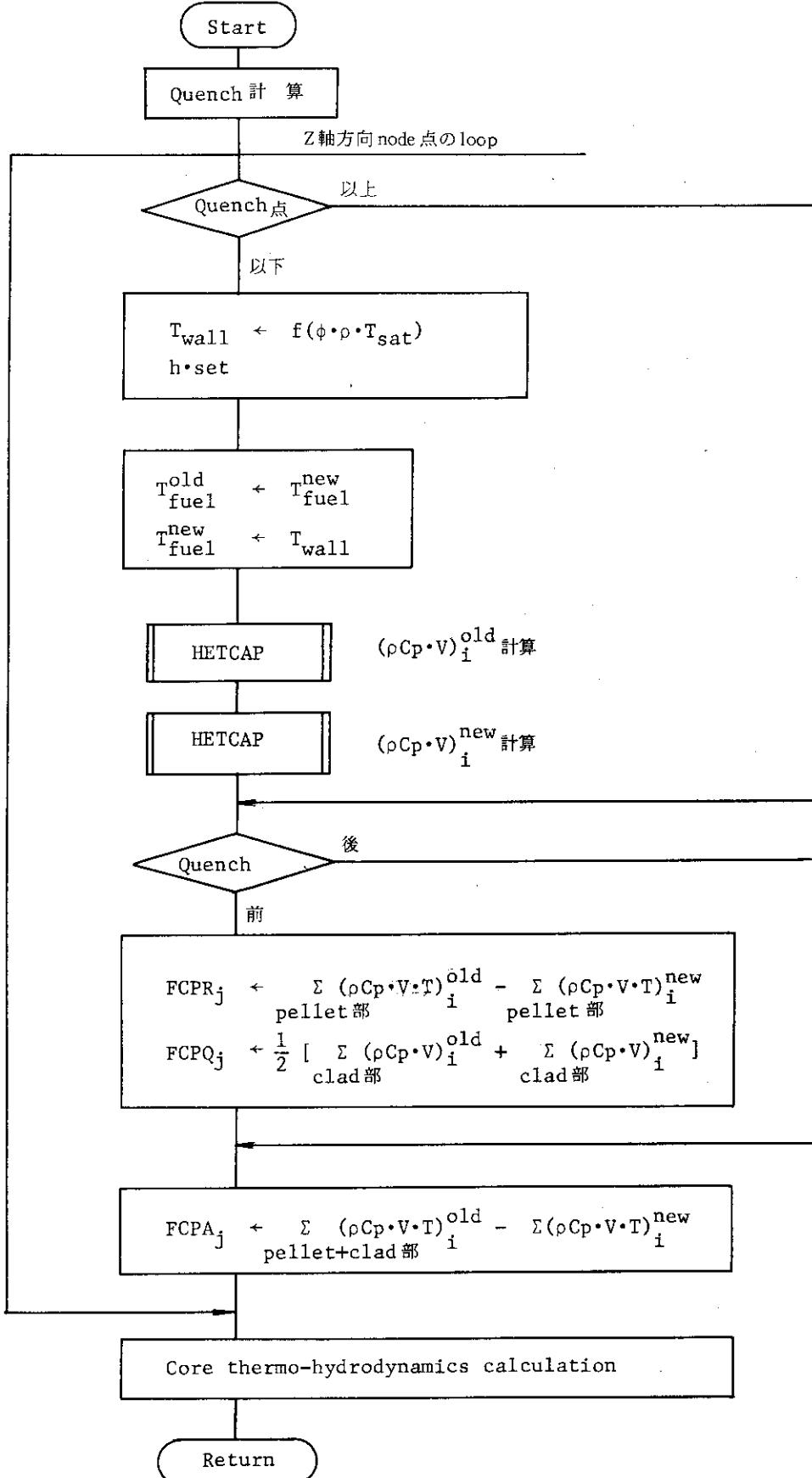


Fig. A.1 Revised part of flow chart of subroutine REFLAA with incorporating fuel temperature profile effect model

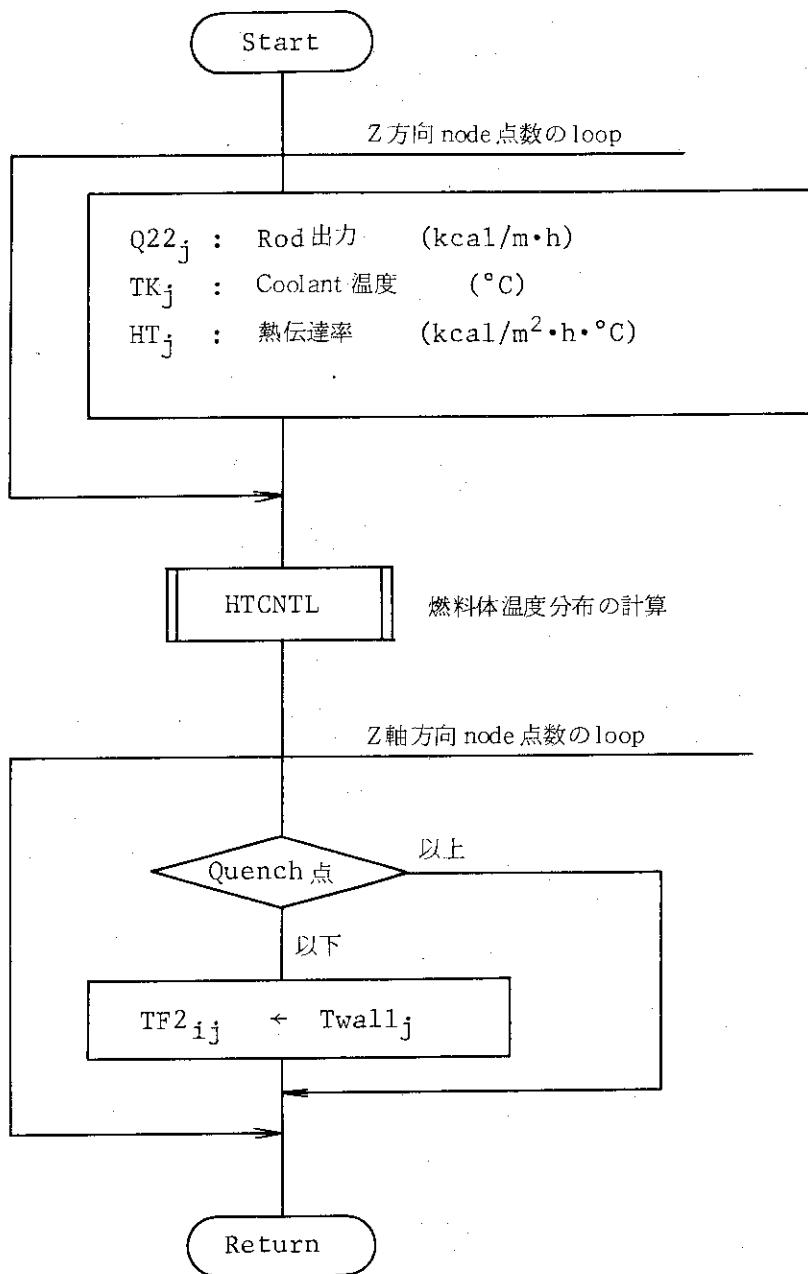


Fig. A.2 Flow chart of subroutine FUELTX

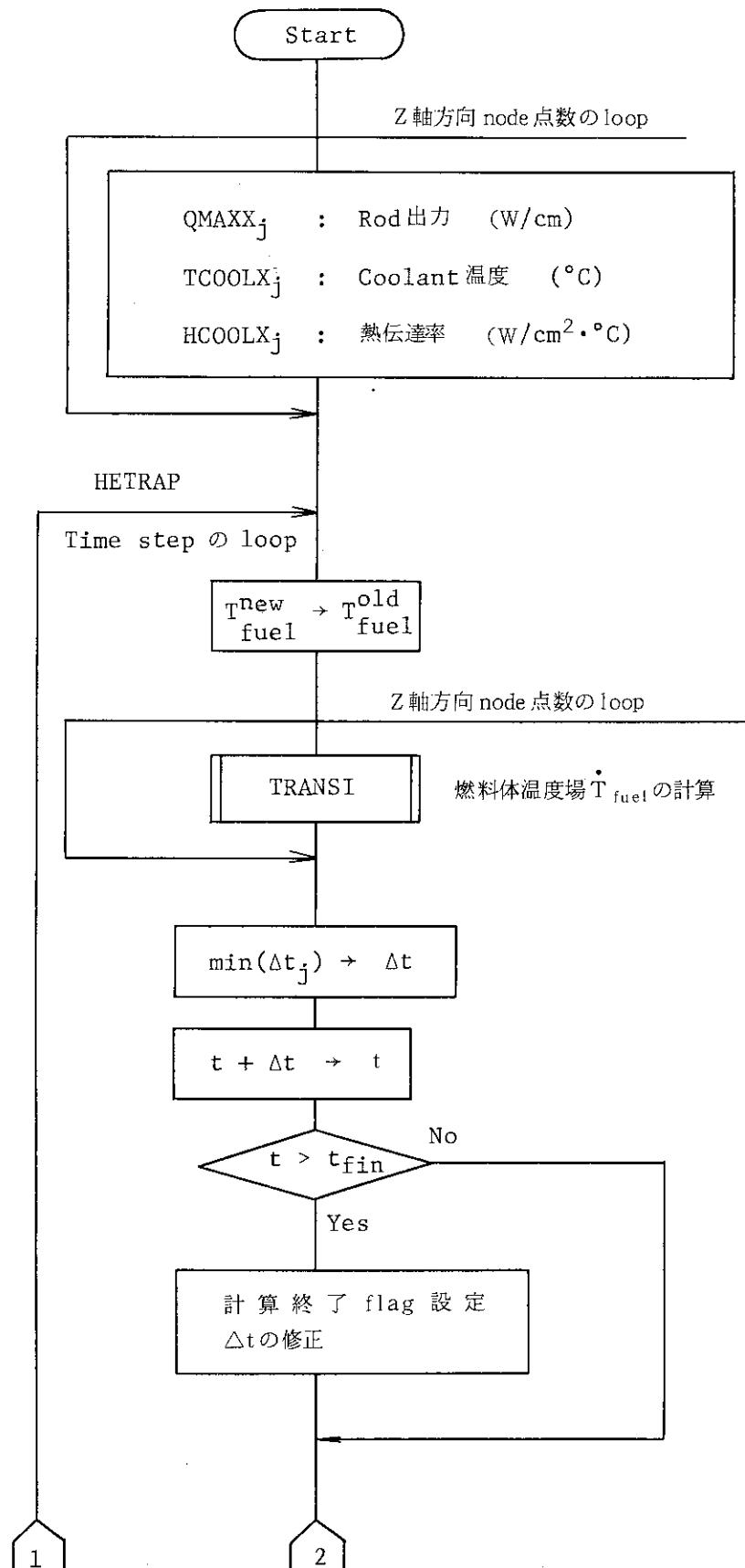


Fig. A.3 Flow chart of subroutine HTCTRL (1/2)

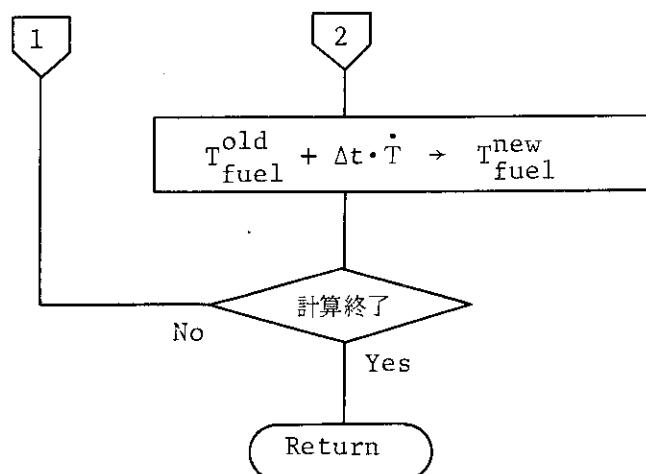


Fig. A.3 Flow chart of subroutine HTCTRL (2/2)

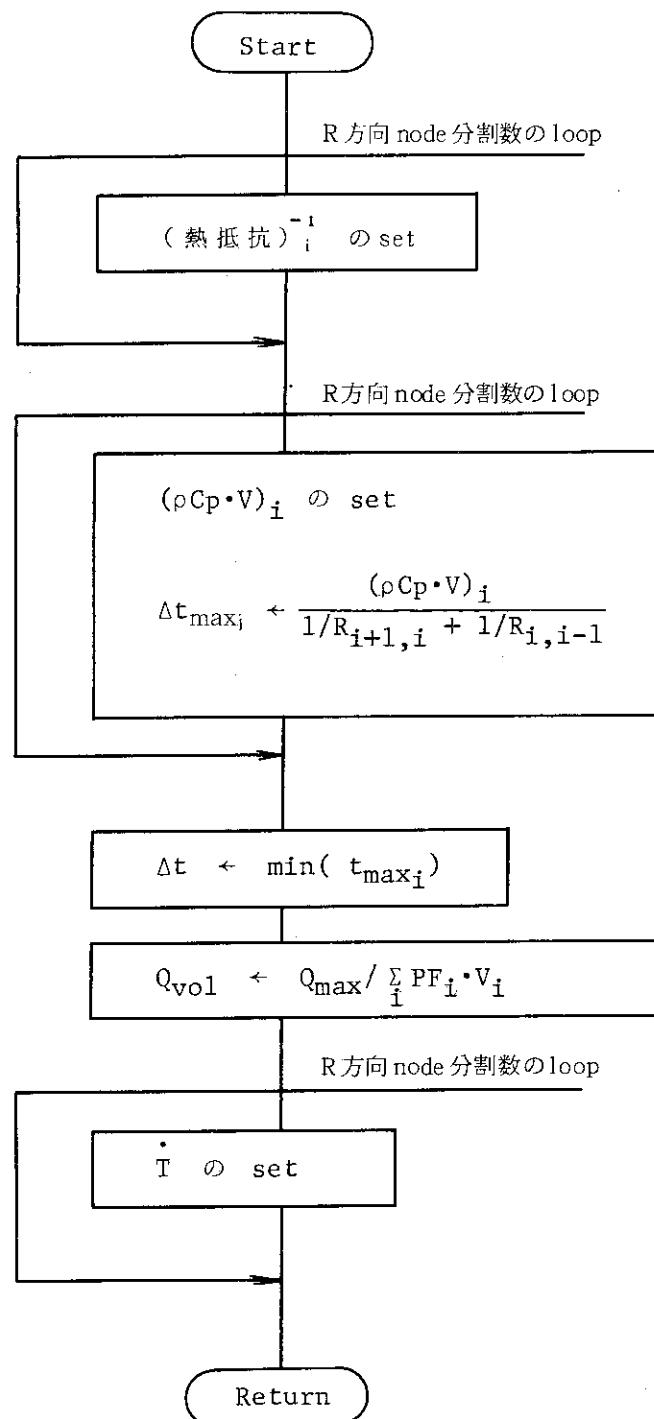


Fig. A.4 Flow chart of subroutine TRANSI

## 付録 B REFLA コードのバグの修正

REFLA-1D/MODE 4 コードの作成は、まず REFLA-1D/MODE 3 コードに局所出力効果モデルを組込んだ中間バージョンを作成し、これに、燃料棒半径方向温度分布モデルを組込む手順で行った。この中間バージョンから REFLA-1D/MODE 4 コードを作成する作業中にいくつかのバグを発見し、その修正を行ったので、以下に概略修正内容を記す。

### B.1 Froth Level (L4) 決定に関する修正

REFLA コードでは、

$$\Delta U_F \geq \Delta U_{\min}$$

$$\left( \begin{array}{l} \Delta U_F = U_{go} - \frac{U_{go}}{1-0.98} \\ \Delta U_{\min} = a \times \Delta U_{\text{crit}}, \quad a = 0.1 \end{array} \right)$$

となると Dispersed Flow Regime になり、 $\Delta U_F = \Delta U_{\min}$  の位置を Froth Level (L4) とする。計算手順は概略右フローチャートのとおり。

局所出力効果モデルを組んだ中間バージョンでは、Froth level 以下で Flow Pattern の変化が生じたとき（例えば、飽和二相流から遷移流へ）、下の regime で計算された  $\Delta U_F^{i+1}(t)$  が、上の regime を計算する subroutine へ引渡されていなかったので、 $\Delta U_F^{i+1}(t)$  を引数として引渡すように修正した。

また、

$$\Delta U_F \leq 0 \text{ のとき } \Delta U_F = 0$$

とする Logic もつけ加えた。

### B.2 Local Rod クエンチ計算の修正

#### 1) Local Rod クエンチ点直下の液体温度

TLPN 2 を正しく与えるように修正

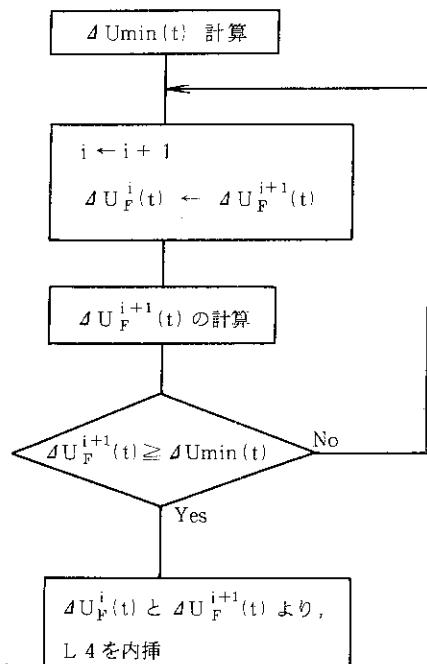
(修正前) : IF (IB02 GT 1) TLPN 2=TL (IB02-1)

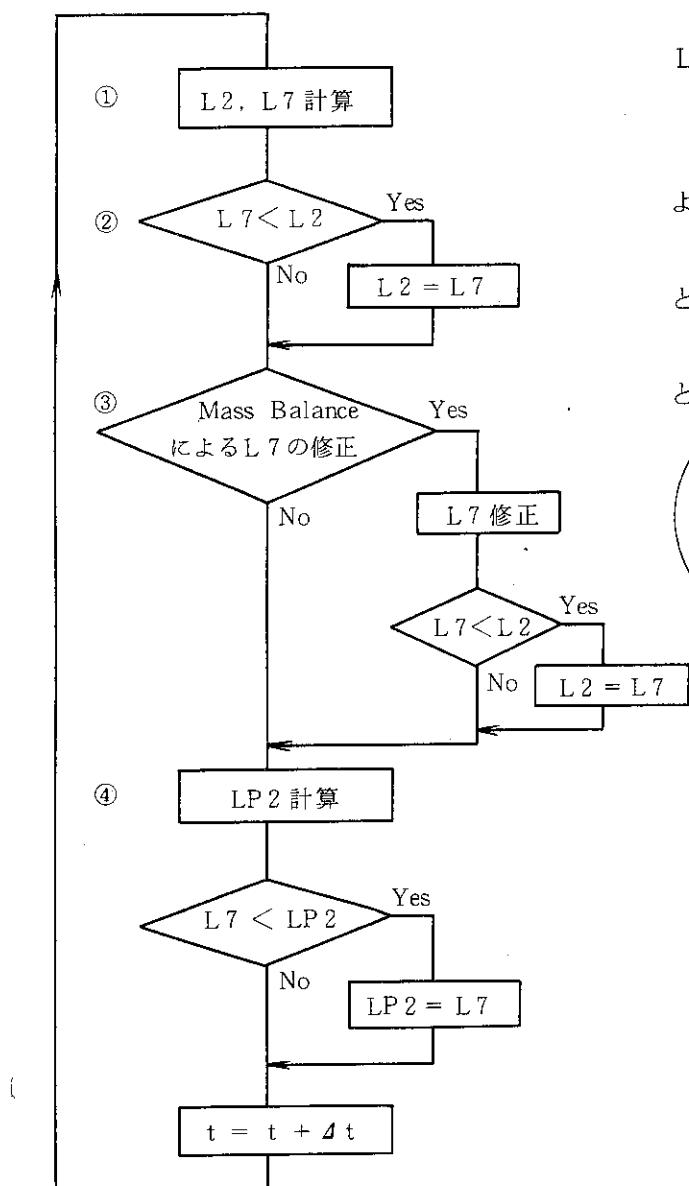
↓

(修正後) : IF (IP02 LE 1) TLPN 2=TL (1)

IF (IP02 GT 1) TLPN 2=TL (IP02-1)

2) "Liquid Top を考慮したクエンチ点の修正" を次ページフローチャートのように修正した。また、この Logic だと、 $t = 0$  のとき  $LP2 \neq 0$  となってしまうので、 $t = 0$  のとき  $LP2 = 0$  となるような修正も付加えた。



$(t > 0)$ 

左の Logic のままだと、 $t = 0$  のとき  
 $LP2 \neq 0$  となる理由を以下に示す。

$t = 0$  のとき、①で

$$L2 > 0, L7 = 0$$

よって、②で  $L2 = L7 = 0$  となる。

しかし、③で  $L7 > 0$ 、④で  $LP2 > 0$  となるので、

$$t = 0 \text{ のとき } LP2 \neq 0$$

となってしまう。

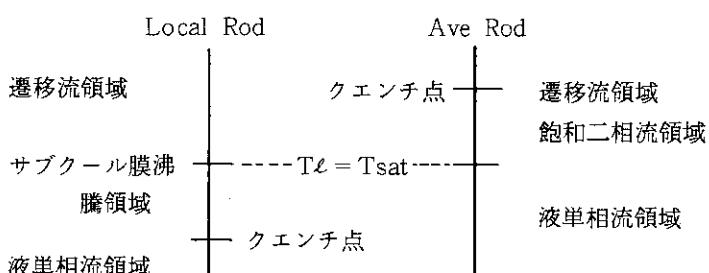
③で  $L7 > 0$  となる理由は、現在未調査。正確には  $t = 0$  の  $L7 = 0$  とすることによって、 $LP2 = 0$  とするべきか？

### B.3 Local Rod クエンチ点上方の Flow Pattern 判定文の修正

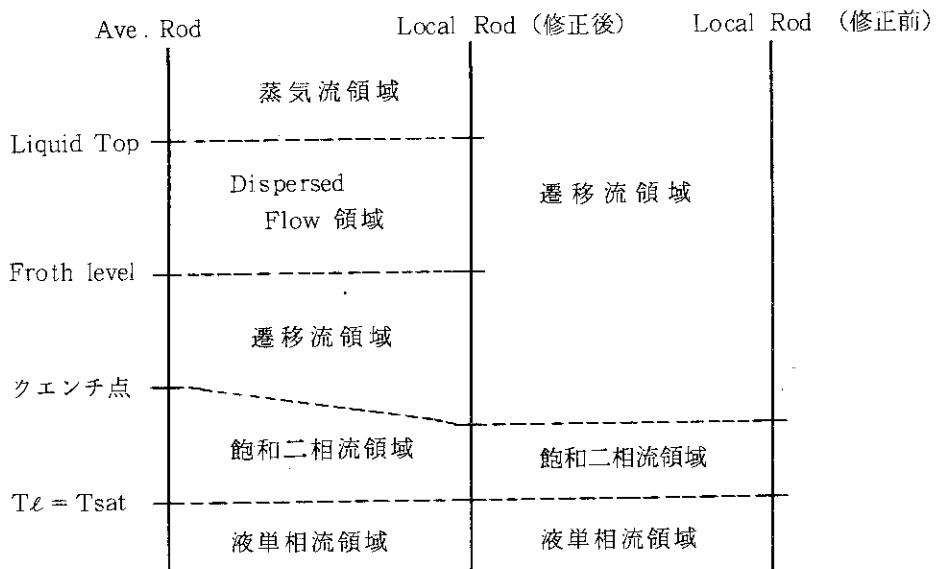
REFLA-1D/MODE 4 コードでは、"Local Rod の Flow Pattern は、クエンチ進行以外は Ave. Rod のそれと基本的には同じである。

ただし、右図のように、  
Local Rod でのみサブクール膜沸騰領域が存在するような場合も考慮する。"  
としている。

しかし、局所出力効果モデルを組んだ中間バージョンの Local Rod 計算では、クエンチ点（サブクール膜沸騰領域が存在する場合には飽和点）直上のノードの Flow Regime が炉心上端まで広がっているような計算をしていた。（次ページの図の Local Rod (修正前) 参照）



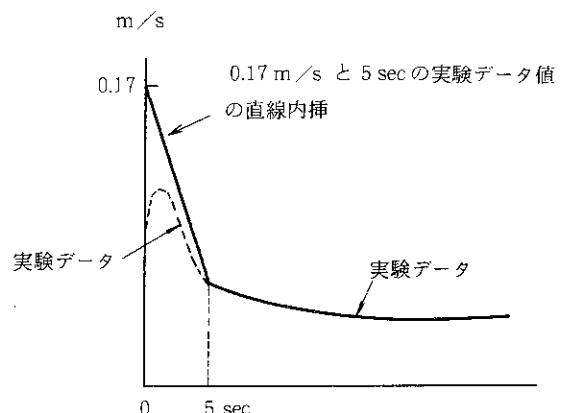
そこで、クエンチ点（サブクール膜沸騰領域が存在する場合は飽和点）上方でも、上記定義のとおり、Ave. Rod と同じ Flow Pattern になるように修正した。（下図の Local Rod (修正後) 参照）



#### B.4 炉心入口流量の修正

局所出力効果モデルを組込んだ中間バージョンでは、CCTF 炉心計算をする場合、炉心入口流量は右下図の実線のように与えられていた。

REFLA-1D/MODE 4 コードでは、0~5 sec も実験データ値（点線部分）を用いるように修正した。



#### B.5 Jens & Lottes の式の係数の修正

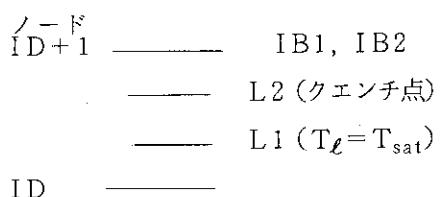
液单相流領域および飽和二相流領域の被覆管表面温度は Jens & Lottes の式から求められるが、式の係数が違っていたので下記のように訂正した。

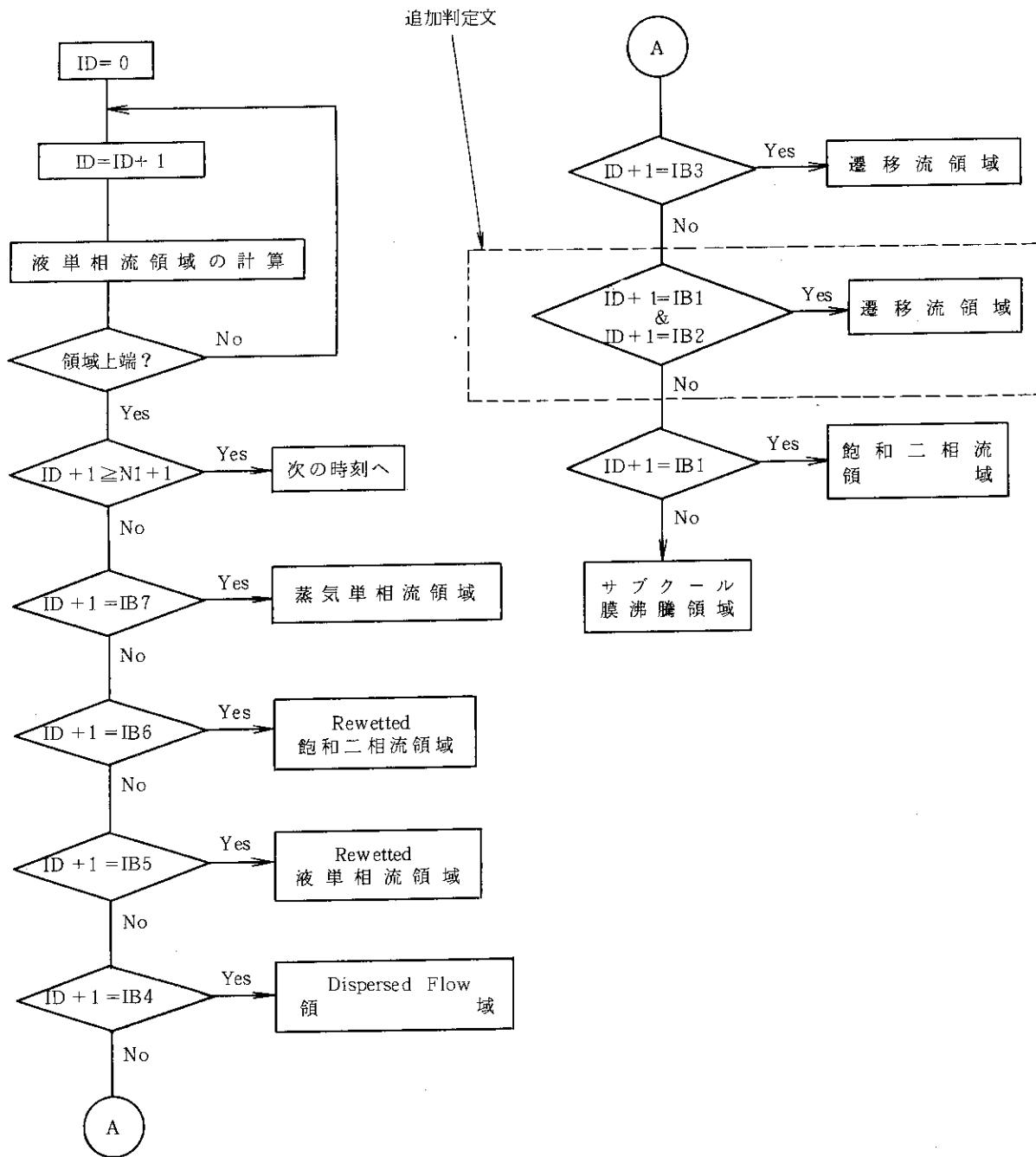
$$T_w = \left[ \frac{QFLUX}{2.197 \times \exp(6.321 \times 10^{-6} \cdot P)} \right]^{0.25} + T_{sat}$$

#### B.6 Flow Pattern 判定文の追加

右図のような場合、ノード ID+1 は遷移流領域になるべきだが、今まででは飽和二相流領域となっていた。

これを、正しい Logic になるように判定文を追加した。





## B.7 CCTF Core-II 用 Flow area の修正

CCTF Core-II の計算する場合、Flow area が違っていたので、正しい Flow area を用いるように修正した。

(修正前) IF (IAXMOD. EQ. 7) SO = 1.244 \* SO

↓

(修正後) IF (IAXMOD. EQ. 7, OR, IAXMOD. EQ. 11) SO = 1.244 \* SO

## 付録C サンプル試験結果 - 1

```

J E S   J O B   L O G -- S Y S T E M   S Y S C -- N O D E   S U N

11.59.56 JOB 1400 .M2:SEND ' 1400 F9089406   JOB ACCEPTED      ',USER=(J9089),LOGON
02.04.19 JOB 1400 KDS700011 J9089  LAST ACCESS AT 16:28:01 ON 85.311
02.04.19 JOB 1400 JDJ3731 F9089406 STARTED - INIT 4 - CLASS H - SYS SYSC
02.04.19 JOB 1400 ACT1400   JOB (F9089406) START. TIME=02:04:19
02.05.09 JOB 1400 ACT1401 CODE=0004 STEP (FORT77) END. PGM JZKDFORT
02.05.17 JOB 1400 ACT1401 CODE=0000 STEP (FORT77) END. PGM JZKDFORT
02.05.23 JOB 1400 ACT1401 CODE=0000 STEP (FORT77) END. PGM JZKDFORT
02.05.34 JOB 1400 ACT1401 CODE=0000 STEP (FORT77) END. PGM JZKDFORT
02.06.19 JOB 1400 ACT1401 CODE=0000 STEP (LINK) END. PGM JGAL
04.42.01 JOB 1400 ACT1402 CODE=0000 STEP (RUN) END. PGM =TEMPNAME
04.42.01 JOB 1400 ACT1402 CODE=0000 JOB (F9089406) END. TIME=04:42:01 << TS.MOJO  >>
04.42.01 JOB 1400 JEM3951 F9089406 ENDED

----- JES JOB STATISTICS -----

08 NOV 85 JOB EXECUTION DATE

60 CARDS READ

3,901 SYSOUT PRINT RECORDS

0 SYSOUT PUNCH RECORDS

157.70 MINUTES EXECUTION TIME

E20 V10L20 <<< JCL STATEMENTS LIST >>> DATE 11/07/85 TIME 11:59
1 //F9089406 JOB ('009190890957.01      ',          JOB 1400
// 'TS.JHOJ  'CLASS=H,PRTY=00,TIME=(0045,00),
// MSGCLASS=0,MSGLEVEL<2,0,1>
// USER=J9089, GROUP=G0957, PASSWORD=
***JOBPARM S=ANY,R=9089,L=0012,C=0000000
***** LIST OF PRIVATE PROC
***** LIST OF USER JCL
***JOBPARM K=0          0007000
*** RUE J9089.REFLAPS.FORT  00080000
***          00090001
00100000
2 //FRI EXEC FORT77,
// SD='J9089.REFLAPS',
// A='ELM(*)',NOS,LANGLVL(66),
// Q=!,PORT,
// DISP=MOD
6 //SYSPRINT DD DUMMY          00160004
10 //FR2 EXEC FORT77,
// SD='J2156.SYSTEM0',
// A='ELM(*)',NOS,LANGLVL(66),
// Q=!,PORT,
// DISP=MOD
14 //SYSPRINT DD DUMMY          00190004
18 //FR3 EXEC FORT77,
// SD='J1207.UPLDT2',
// A='ELMGETTAG,GETTB,PUTDAT',NOS,LANGLVL(66),
// Q=!,PORT,
// DISP=MOD
22 //SYSPRINT DD DUMMY          00220004
26 //FR4 EXEC FORT77,
// SD='J3105.SSPLOT',
// A='ELM(*)',NOS,LANGLVL(66),
// Q=!,PORT,
// DISP=MOD
30 //SYSPRINT DD DUMMY          00250004
34 //FLIK EXEC LKE077,
// GRLIB=PNL
45 //SYSPRINT DD DUMMY          00270001
51 //REFLAP EXEC GO
59 //NLPE EXPAND GRNLPE,
// SYSOUT#
62 //GDFILE DD SYSOUT=N,OUTLIM=80000,DEST=LOCAL          00300000
63 //FT01FO01 DD SYSOUT=*,DCB=(RECFM=FA,BLKSIZE=133)  00310000
64 //FT10FO01 DD DSN=J3349.CC1J038.DATA,DISP=SHR,LABEL=(,,IN) 00320002
65 //FT20FO01 DD DSN=J3349.CCTMJD8.DATA,DISP=SHR,LABEL=(,,IN) 00330002
66 //FT55FO01 DD DSN=J9089.REFLAPS.DATA(HETCCTF),DISP=SHR 00340000
67 //DATA EXPAND DISK0,
// DSN=SYSIN,
// DSN='J9089,REFLAPS',
// Q=!.DATA(RZFUELPS)
//



<<< SYSTEM MESSAGES LIST >>>

51 JDJ6861 DDNAME REFERRED TO ON DDNAME KEYWORD IN PRIOR STEP WAS NOT RESOLVED
KDS700011 J9089  LAST ACCESS AT 16:28:01 ON 85.311
JDJ1421 F9089406 FORT77 FRI - STEP WAS EXECUTED - COND CODE 0004
JDJ3731 STEP/FORT77 / START 85312.0204
JDJ3741 STEP/FORT77 / STDP 85312.0205 CPU    OMIN 00.00SEC SRB    OMIN 00.08SEC VIRT  1024K
ACT0611   SYSTEM  (< SYSC M-380 ) EXCP   572TIMES
JDJ1421 F9089406 FORT77 FR2 - STEP WAS EXECUTED - COND CODE 0000
JDJ3731 STEP/FORT77 / START 85312.0205
JDJ3741 STEP/FORT77 / STDP 85312.0205 CPU    OMIN 00.31SEC SRB    OMIN 00.01SEC VIRT  1024K
ACT0611   SYSTEM  (< SYSC M-380 ) EXCP   60TIMES
JDJ1421 F9089406 FORT77 FR3 - STEP WAS EXECUTED - COND CODE 0000
JDJ3731 STEP/FORT77 / START 85312.0205
JDJ3741 STEP/FORT77 / STDP 85312.0205 CPU    OMIN 00.34SEC SRB    OMIN 00.01SEC VIRT  1024K
ACT0611   SYSTEM  (< SYSC M-380 ) EXCP   227TIMES
JDJ1421 F9089406 FORT77 FR4 - STEP WAS EXECUTED - COND CODE 0000
JDJ3731 STEP/FORT77 / START 85312.0205
JDJ3741 STEP/FORT77 / STDP 85312.0205 CPU    OMIN 00.97SEC SRB    OMIN 00.02SEC VIRT  1024K
ACT0611   SYSTEM  (< SYSC M-380 ) EXCP   145TIMES
JDJ1421 F9089406 LINK LINK STEP WAS EXECUTED - COND CODE 0000
JDJ3731 STEP/LINK  / START 85312.0205
JDJ3741 STEP/LINK  / STDP 85312.0206 CPU    OMIN 02.04SEC SRB    OMIN 00.16SEC VIRT  512K
ACT0611   SYSTEM  (< SYSC M-380 ) EXCP   1456TIMES
JDJ1421 F9089406 RUN REFLA - STEP WAS EXECUTED - COND CODE 0000
JDJ3731 STEP/RUN  / START 85312.0206
** WRN **

-----
```

JOJ3741 STEP/RUN / STOP 85312.0442 CPU 36MIN 34.23SEC SRB 0MIN 00.89SEC VIRT 3324K  
 ACT0611 SYSTEM ( SYSC M-380 ) EXCP 385TIMES  
 JDJ3751 JOB/F9089406/ START 85312.0204  
 JDJ3761 JOB/F9089406/ STOP 85312.0442 CPU 36MIN 45.89SEC SRB 0MIN 01.17SEC  
 \*\*\*\*  
 \*\*\* USER NAME <<TS.HOJO >> SECTION NO << G0957 >> \*\*\*  
 \*\*\*  
 \*\*\* JOB NUMBER ... 1400 RUNNING DATE ... 1985/11/07 \*\*\*  
 \*\*\* JOB NAME ... F9089406 USER-ID ... J9089 \*\*\*  
 \*\*\* JOB CLASS ... H JOB PRIORITY ... 00 \*\*\*  
 \*\*\* TOTAL JOB STEPS ... 6 COMPLETION CODE ... 0004 \*\*\*  
 \*\*\*  
 \*\*\* CPU TIME ... OH36M45S89 I I/O ACCESS FILES ACCESS \*\*\*  
 \*\*\* SRB TIME ... OH 0M 1517 I DISK ... 29 2646 \*\*\*  
 \*\*\* JOB START DATE ... 1985/11/08 I TAPE ... 0 0 \*\*\*  
 \*\*\* TIME ... 2H 4M19S75 I TOTAL ..... 3670 \*\*\*  
 \*\*\* JOB END DATE ... 1985/11/08 I VIO PAGE IN ... 300 \*\*\*  
 \*\*\* TIME ... 4H42M 1S19 I VIO PAGE OUT ... 301 \*\*\*  
 \*\*\* ELAPSED TIME ... 2H37M41S44 I \*\*\*  
 \*\*\*  
 \*\*\* PAGE IN ... 30 STORAGE REQ'D(MAX) ... 4160 KB \*\*\*  
 \*\*\* PAGE OUT ... 125 STORAGE USED (MAX) ... 3324 KB \*\*\*  
 \*\*\*  
 \*\*\* ROOM-LIMIT-CPU ROOM-USED-CPU USER-LIMIT-CPU USER-USED-CPU \*\*\*  
 \*\*\* XH XM XSXX XH XM XSXX XH XM XSXX XH XM XSXX \*\*\*  
 \*\*\*

\* \* \* \* INPUT CARDS LIST \* \* \* \*  
 NO. ....1....2....3....4....5....6....7....8....9....10....11....12 ....13..  
 1 (\*\* REFLAPS RUN ( IOPT = 1,1 ) \*\* CCTF CORE-I ( RUN 38 , BUNDLE 17 ) >00010000  
 2 ( 1 1 >00020002  
 3 ( 2.086 0.25 7.0 100. 2.000 2.000100030000  
 4 ( 100.0 8.0 8.0 0.1 4.0 >00040000  
 5 ( 1 1.10 375.6 621.3 760.0 672.2 493.3 >00050004  
 6 ( 90 10.7 14.3 3.66 >00060000  
 7 ( .1 0.25 >00070000  
 8 ( 10.8 2000.0 0.41318 >00080000  
 9 ( >00090000  
 10 ( >00100000  
 11 ( 720.0 >00110000  
 12 ( >00120000  
 13 ( 1000.0 >00130000  
 14 ( 480.0 1500.0 >00140006  
 15 ( 120.0 >00150000  
 16 ( >00160000  
 17 ( >00170000  
 18 ( >00180000  
 19 ( >00190000  
 20 ( >00200000  
 NO. ....1....2....3....4....5....6....7....8....9....10....11....12 ....13..  
 21 ( >00210000  
 22 ( >00220000  
 23 ( 5 >00230006  
 24 ( 2 10 22 2.0 211 2.0 215 20.0 >00240006  
 25 ( 212 400.0 >00241006  
 26 ( 38 >00250000  
 27 ( TE18Z11 >00260000  
 28 ( TE18Z12 >00270000  
 29 ( TE18Z13 >00280000  
 30 ( TE18Z14 >00290000  
 31 ( TE18Z15 >00300000  
 32 ( DPLLOOP1 >00310000  
 33 ( DPDOWN5 >00320000  
 34 ( DPLLOOP4 >00330000  
 35 ( DPCOREA >00340000  
 36 ( LT07RQ5V >00350000  
 37 ( LT06RQ5V >00360000  
 38 ( LT05RQ5V >00370000  
 39 ( LT04RQ5V >00380000  
 40 ( LT03RQ5V >00390000

| NO. | .....1.....2.....3.....4.....5.....6.....7.....8.....9....10....11....12 ....13.. |
|-----|---|
| 41  | (LTO2RQ5V )00400000   |
| 42  | (ULCR11 )00410000   |
| 43  | (TACRIN )00420000   |
| 44  | (LTO1RQS )00430000  |
| 45  | (PTOORNO )00440000  |
| 46  | (TE52X13 )00450000  |
| 47  | (TE17Y11 )00460000  |
| 48  | (TE17Y12 )00470000  |
| 49  | (TE17Y13 )00480000  |
| 50  | (TE17Y14 )00490000  |
| 51  | (TE17Y15 )00500000  |
| 52  | (HTE18Z11 )00510006   |
| 53  | (HTE18Z12 )00520006   |
| 54  | (HTE18Z13 )00530006   |
| 55  | (HTE18Z14 )00540006   |
| 56  | (HTE18Z15 )00550006   |

---

```
** REFLAPS RUN ( IDPT = 1.1 ) **      CCTF CORE-I ( RUN 38 , BUNDLE 17 )

IDPT01 =           1
IDPT02 =           1

QMAX0 =   2.086      DTS =   0.2500      AXMOD =    7.000
TLIN =   100.0       PIN =   2.000       POUT =    2.000
TIME3 =   100.0       AZ1 =   8.000       A22 =    8.000
DTC =   0.1000       AK3 =   0.0          Z =    4.000

NPLOT =           1
RPF =   1.1000

NRSTRT =          0
DTRST =   0.0
CPEND =   0.0

N =             90
IFBMOD =          0
DIA =   10.700
PITCH =  14.300
CLENG =  3.6600

RUN1 =        RUN2 =        RUN3 =        IRUN =        0

WEC =   0.10000
WEC1 =   0.0
YYY =   0.0
TPRINT =  0.25000
VOL =   0.0
SW3 =   0.0

NS =           0
RC =   0.0
CKF =   10.800
DF =   2000.0
CF =   0.41318

IAXMOD =         7  ( CCTF CORE I AXIAL POWER PROFILE )
IDECAY =         1  ( ANS*1.2 + ACTINIDES*1.1 ( 30 S AFTER SCRAM )

CNHEAT =   0.0
CSAVE =   0.0

TIME1= 0.0      TEMP1= 0.0      QMAX1= 0.0      ULIN1= 0.0      PSYS1= 0.0      TLIN1= 0.0
TIME2= 0.0      XXXX2= 720.00    QMAX2= 0.0      ULIN2= 0.0      PSYS2= 0.0      TLIN2= 0.0
TEMP2= 720.00    TEMP4= 0.0      QMAX4= 0.0      ULIN3= 0.0      PSYS4= 0.0      TLIN4= 0.0
TIME3= 480.00    TEMP5= 1500.0    QMAX5= 0.0      ULIN5= 0.0      PSYS5= 0.0      TLIN5= 0.0
```

## \*\*\* INITIAL CONDITION FOR AXIAL TEMPERATURE DISTRIBUTION (DEGC) \*\*\*

| I  | TW(I)  |
|----|--------|----|--------|----|--------|----|--------|----|--------|
| 1  | 120.00 | 2  | 120.00 | 3  | 120.00 | 4  | 120.00 | 5  | 120.00 |
| 6  | 120.00 | 7  | 120.00 | 8  | 120.00 | 9  | 120.00 | 10 | 120.00 |
| 11 | 120.00 | 12 | 120.00 | 13 | 120.00 | 14 | 120.00 | 15 | 120.00 |
| 16 | 120.00 | 17 | 120.00 | 18 | 120.00 | 19 | 120.00 | 20 | 120.00 |
| 21 | 120.00 | 22 | 120.00 | 23 | 120.00 | 24 | 120.00 | 25 | 120.00 |
| 26 | 120.00 | 27 | 120.00 | 28 | 120.00 | 29 | 120.00 | 30 | 120.00 |
| 31 | 120.00 | 32 | 120.00 | 33 | 120.00 | 34 | 120.00 | 35 | 120.00 |
| 36 | 120.00 | 37 | 120.00 | 38 | 120.00 | 39 | 120.00 | 40 | 120.00 |
| 41 | 120.00 | 42 | 120.00 | 43 | 120.00 | 44 | 120.00 | 45 | 120.00 |
| 46 | 120.00 | 47 | 120.00 | 48 | 120.00 | 49 | 120.00 | 50 | 120.00 |
| 51 | 120.00 | 52 | 120.00 | 53 | 120.00 | 54 | 120.00 | 55 | 120.00 |
| 56 | 120.00 | 57 | 120.00 | 58 | 120.00 | 59 | 120.00 | 60 | 120.00 |
| 61 | 120.00 | 62 | 120.00 | 63 | 120.00 | 64 | 120.00 | 65 | 120.00 |
| 66 | 120.00 | 67 | 120.00 | 68 | 120.00 | 69 | 120.00 | 70 | 120.00 |
| 71 | 120.00 | 72 | 120.00 | 73 | 120.00 | 74 | 120.00 | 75 | 120.00 |
| 76 | 120.00 | 77 | 120.00 | 78 | 120.00 | 79 | 120.00 | 80 | 120.00 |
| 81 | 120.00 | 82 | 120.00 | 83 | 120.00 | 84 | 120.00 | 85 | 120.00 |
| 86 | 120.00 | 87 | 120.00 | 88 | 120.00 | 89 | 120.00 | 90 | 120.00 |
| 91 | 120.00 |    |        |    |        |    |        |    |        |

## \*\*\* LIST OF CONTROL VARIABLES CCON AND ICON \*\*\*

```

CCON( 1)= 0.10000
CCON( 2)= 0.10000
CCON(21)= 0.30000
CCON(22)= 2.00000
CCON(23)= 0.30000
CCON(24)= 0.0
CCON(25)= 0.10000
CCON(26)= 1.10000
CCON(27)= 0.60000
CCON(28)= 0.00070
CCON(29)= -1.00000
CCON(30)= 0.0
CCON(31)= 0.0
CCON(32)= 0.0
CCON(33)= 15.80000
CCON(34)= 15.80000
CCON(40)= 0.0
CCON(41)= 4.00000

ICON( 1)= 0
ICON( 2)= 0
ICON( 3)= 0
ICON( 4)= 1
ICON(11)= 2
ICON(12)= 400
ICON(13)= 5
ICON(14)= 4
ICON(15)= 20
ICON(16)= 1

```

```

READ IRUN=38
READ ITAG1-ITAG
1  TE18Z11
2  TE18Z12
3  TE18Z13
4  TE18Z14
5  TE18Z15
6  DPLLOOP1
7  DPDOWN5
8  DPLLOOP4
9  DPCQREA
10 LT07R05V
11 LT06R05V
12 LT05R05V
13 LT04R05V
14 LT03R05V
15 LT02R05V
16 ULCRII
17 TACRIN
18 LT01R05
19 PTOORNO
20 TE32X13
21 TE17Y11
22 TE17Y12
23 TE17Y13
24 TE17Y14
25 TE17Y15
26 HTE18Z11
27 HTE18Z12
28 HTE18Z13
29 HTE18Z14
30 HTE18Z15

```

## \*\*\* RETURN CODE OF GETTAG IS GOOD \*\*\*

| TIME(SEC) | ULIN(M/SEC) | TLIN(K) | DPIN(MPA)   | PLP(MPA) | PIN(MPA) |
|-----------|-------------|---------|-------------|----------|----------|
| 0.0       | 0.49933E-01 | 394.97  | 0.18546E-01 | 0.22285  | 0.20430  |
| 25.000    | 0.37087E-01 | 386.29  | 0.20254E-01 | 0.30011  | 0.27986  |
| 50.000    | 0.28992E-01 | 376.49  | 0.19831E-01 | 0.31887  | 0.29904  |
| 75.000    | 0.24247E-01 | 372.45  | 0.19848E-01 | 0.30864  | 0.28879  |
| 100.000   | 0.23612E-01 | 371.87  | 0.19875E-01 | 0.30114  | 0.28127  |
| 125.000   | 0.20695E-01 | 373.97  | 0.19781E-01 | 0.29607  | 0.27629  |
| 150.000   | 0.24470E-01 | 376.72  | 0.19782E-01 | 0.29084  | 0.27106  |
| 175.000   | 0.16926E-01 | 381.18  | 0.19699E-01 | 0.28981  | 0.27011  |
| 200.000   | 0.20809E-01 | 384.75  | 0.19845E-01 | 0.29210  | 0.27225  |
| 225.000   | 0.15255E-01 | 388.09  | 0.19534E-01 | 0.28710  | 0.26756  |
| 250.000   | 0.27787E-01 | 389.89  | 0.19563E-01 | 0.28592  | 0.26636  |
| 275.000   | 0.23357E-01 | 391.72  | 0.19594E-01 | 0.29004  | 0.27044  |
| 300.000   | 0.23922E-01 | 393.14  | 0.19658E-01 | 0.29195  | 0.27229  |
| 325.000   | 0.20098E-01 | 395.22  | 0.19714E-01 | 0.29349  | 0.27378  |
| 350.000   | 0.24508E-01 | 396.00  | 0.19523E-01 | 0.29269  | 0.27316  |
| 375.000   | 0.22926E-01 | 397.05  | 0.19568E-01 | 0.28967  | 0.27010  |
| 400.000   | 0.26380E-01 | 397.98  | 0.19560E-01 | 0.29033  | 0.27077  |
| 425.000   | 0.20979E-01 | 398.26  | 0.19413E-01 | 0.28548  | 0.26607  |
| 450.000   | 0.20083E-01 | 397.85  | 0.19757E-01 | 0.28305  | 0.26329  |
| 475.000   | 0.10219E-01 | 398.44  | 0.19800E-01 | 0.28055  | 0.26074  |

ITMAX= 996

| ***** SYSTEM PARAMETERS ***** |                    |
|-------------------------------|--------------------|
| CORE FLOW AREA                | 0.2500000 ( M**2 ) |
| DOWNCOMER FLOW AREA           | 0.1970000 ( M**2 ) |
| FLOW AREA OF CO-DO CONNECTED  | 0.7905000 ( M**2 ) |
| LOOP FLOW AREA                | 0.0757000 ( M**2 ) |
| UPPER PLenum Volum            | 1.8950005 ( M**3 ) |
| CORE HEATED LENGTH            | 3.660 ( M )        |
| DOWNCOMER LENGTH              | 4.849 ( M )        |
| LENGTH OF CO-DO CONNECTED     | 2.100 ( M )        |
| INLET RESISTANCE COEFFICIENT  | 20.000 ( - )       |
| IN-CORE RESISTANCE COE.       | 20.000 ( - )       |
| IN-DOWNCOMER RESISTANCE COE.  | 10.000 ( - )       |
| LOOP RESISTANCE COEFFICIENT.  | 25.000 ( - )       |

## FLOW CHANNEL GEOMETRY

|                  |         |       |
|------------------|---------|-------|
| PIN DIA          | 10.7000 | MM    |
| PITCH            | 14.3000 | MM    |
| CROSS SECTION    | 1.42925 | CM**2 |
| WETTED PERIMETER | 33.6150 | MM    |
| EQUIVALENT DIA   | 13.6332 | MM    |
| CORE LENGTH      | 3660.00 | MM    |
| AXIAL INCREMENT  | 40.6667 | MM    |

## CONSTANTS + PHYSICAL PROPERTIES

|                  |              |          |
|------------------|--------------|----------|
| PAI              | 3.14159      | -        |
| GRAVITATIONAL AC | 0.127100E+09 | M/H**2   |
| STEFAN BOLTZ.CON | 0.488000E-07 | KC/M2K4H |
| SATURATION TEMP. | 120.733      | DEG.C    |
| DENSITY OF WATER | 0.741522E-05 | KG*H2/M4 |
| DENSITY OF VAPOR | 0.906317E-08 | KG*H2/M4 |
| LATENT HEAT      | 525.345      | KCAL/KG  |
| VISCOSITY OF WAT | 0.886757E-03 | KG*H/M2  |
| VISCOSITY OF VAP | 0.414661E-01 | KG*H/M2  |
| PRANDTL NO. WAT  | 1.43304      | -        |
| PRANDTL NO. VAP  | 1.11073      | -        |
| HEAT CONDUCT WAT | 0.588963     | KCAL/MHC |
| HEAT CONDUCT VAP | 0.223696E-01 | KCAL/MHC |
| SPECIFIC HT WAT  | 1.00000      | KCAL/KG  |
| SPECIFIC HT VAP  | 0.500000     | KCAL/KG  |
| SURFACE TENS WAT | 0.553352E-02 | KG/M     |

JAERI-M 85-210

CASE NUMBER = 1  
INITIAL CONDITION

| DISTANCE | NMPOWER  | INIT.TW | INIT.TG |
|----------|----------|---------|---------|
| ( MM )   | ( - )    | ( DC )  | ( DC )  |
| 0.0      | 0.184000 | 120.000 | 120.000 |
| 40.667   | 0.184000 | 120.000 | 120.000 |
| 81.333   | 0.184000 | 120.000 | 120.000 |
| 122.000  | 0.184000 | 120.000 | 120.000 |
| 162.667  | 0.184000 | 120.000 | 120.000 |
| 203.333  | 0.184000 | 120.000 | 120.000 |
| 244.000  | 0.184000 | 120.000 | 120.000 |
| 284.667  | 0.381000 | 120.000 | 120.000 |
| 325.333  | 0.381000 | 120.000 | 120.000 |
| 366.000  | 0.381000 | 120.000 | 120.000 |
| 406.667  | 0.381000 | 120.000 | 120.000 |
| 447.333  | 0.381000 | 120.000 | 120.000 |
| 488.000  | 0.381000 | 120.000 | 120.000 |
| 528.667  | 0.546000 | 120.000 | 120.000 |
| 569.333  | 0.546000 | 120.000 | 120.000 |
| 610.000  | 0.546000 | 120.000 | 120.000 |
| 650.667  | 0.546000 | 120.000 | 120.000 |
| 691.333  | 0.546000 | 120.000 | 120.000 |
| 732.000  | 0.678000 | 120.000 | 120.000 |
| 772.667  | 0.678000 | 120.000 | 120.000 |
| 813.333  | 0.678000 | 120.000 | 120.000 |
| 854.000  | 0.678000 | 120.000 | 120.000 |
| 894.667  | 0.678000 | 120.000 | 120.000 |
| 935.333  | 0.788000 | 120.000 | 120.000 |
| 976.000  | 0.788000 | 120.000 | 120.000 |
| 1016.67  | 0.788000 | 120.000 | 120.000 |
| 1057.33  | 0.788000 | 120.000 | 120.000 |
| 1098.00  | 0.788000 | 120.000 | 120.000 |
| 1138.67  | 0.879000 | 120.000 | 120.000 |
| 1179.33  | 0.879000 | 120.000 | 120.000 |
| 1220.00  | 0.879000 | 120.000 | 120.000 |
| 1260.67  | 0.879000 | 120.000 | 120.000 |
| 1301.33  | 0.879000 | 120.000 | 120.000 |
| 1342.00  | 0.946000 | 120.000 | 120.000 |
| 1382.67  | 0.946000 | 120.000 | 120.000 |
| 1423.33  | 0.946000 | 120.000 | 120.000 |
| 1464.00  | 0.946000 | 120.000 | 120.000 |
| 1504.67  | 0.946000 | 120.000 | 120.000 |
| 1545.33  | 0.986000 | 120.000 | 120.000 |
| 1586.00  | 0.986000 | 120.000 | 120.000 |
| 1626.67  | 0.986000 | 120.000 | 120.000 |
| 1667.33  | 0.986000 | 120.000 | 120.000 |
| 1708.00  | 0.986000 | 120.000 | 120.000 |
| 1748.67  | 1.000000 | 120.000 | 120.000 |
| 1789.33  | 1.000000 | 120.000 | 120.000 |
| 1830.00  | 1.000000 | 120.000 | 120.000 |
| 1870.67  | 1.000000 | 120.000 | 120.000 |
| 1911.33  | 1.000000 | 120.000 | 120.000 |
| 1952.00  | 0.986000 | 120.000 | 120.000 |
| 1992.67  | 0.986000 | 120.000 | 120.000 |

INITIAL CONDITION (CONTINUED)

| DISTANCE | NMPOWER  | INIT.TW | INIT.TG |
|----------|----------|---------|---------|
| ( MM )   | ( - )    | ( DC )  | ( DC )  |
| 2033.33  | 0.986000 | 120.000 | 120.000 |
| 2074.00  | 0.986000 | 120.000 | 120.000 |
| 2114.67  | 0.986000 | 120.000 | 120.000 |
| 2155.33  | 0.946000 | 120.000 | 120.000 |
| 2196.00  | 0.946000 | 120.000 | 120.000 |
| 2236.67  | 0.946000 | 120.000 | 120.000 |
| 2277.33  | 0.946000 | 120.000 | 120.000 |
| 2318.00  | 0.946000 | 120.000 | 120.000 |
| 2358.67  | 0.879000 | 120.000 | 120.000 |
| 2399.33  | 0.879000 | 120.000 | 120.000 |
| 2440.00  | 0.879000 | 120.000 | 120.000 |
| 2480.67  | 0.879000 | 120.000 | 120.000 |
| 2521.33  | 0.879000 | 120.000 | 120.000 |
| 2562.00  | 0.788000 | 120.000 | 120.000 |
| 2602.67  | 0.788000 | 120.000 | 120.000 |
| 2643.33  | 0.788000 | 120.000 | 120.000 |
| 2684.00  | 0.788000 | 120.000 | 120.000 |
| 2724.67  | 0.788000 | 120.000 | 120.000 |
| 2765.33  | 0.678000 | 120.000 | 120.000 |
| 2806.00  | 0.678000 | 120.000 | 120.000 |
| 2846.67  | 0.678000 | 120.000 | 120.000 |
| 2887.33  | 0.678000 | 120.000 | 120.000 |
| 2928.00  | 0.678000 | 120.000 | 120.000 |
| 2968.67  | 0.546000 | 120.000 | 120.000 |
| 3009.33  | 0.546000 | 120.000 | 120.000 |
| 3050.00  | 0.546000 | 120.000 | 120.000 |
| 3090.67  | 0.546000 | 120.000 | 120.000 |
| 3131.33  | 0.546000 | 120.000 | 120.000 |
| 3172.00  | 0.381000 | 120.000 | 120.000 |
| 3212.67  | 0.381000 | 120.000 | 120.000 |
| 3253.33  | 0.381000 | 120.000 | 120.000 |
| 3294.00  | 0.381000 | 120.000 | 120.000 |
| 3334.67  | 0.381000 | 120.000 | 120.000 |
| 3375.33  | 0.381000 | 120.000 | 120.000 |
| 3416.00  | 0.184000 | 120.000 | 120.000 |
| 3456.67  | 0.184000 | 120.000 | 120.000 |
| 3497.33  | 0.184000 | 120.000 | 120.000 |
| 3538.00  | 0.184000 | 120.000 | 120.000 |
| 3578.67  | 0.184000 | 120.000 | 120.000 |
| 3619.33  | 0.184000 | 120.000 | 120.000 |
| 3660.00  | 0.184000 | 120.000 | 120.000 |

## JAERI-M 85-210

\*\*\* PARAMETER LIST FOR CALCULATION OF TEMPERATURE FIELD OF FUEL ROD

Z-NODE FROM 1 TO 33

| I  | R      | PF     | H   | E   | IWC | IWP |
|----|--------|--------|-----|-----|-----|-----|
| 1  | 0.5350 | 0.0    | 0.0 | 0.0 | 0   | 7   |
| 2  | 0.5100 | 0.0    | 0.0 | 0.0 | 7   | 7   |
| 3  | 0.4750 | 0.0    | 0.0 | 0.0 | 7   | 7   |
| 4  | 0.4350 | 0.0    | 0.0 | 0.0 | 4   | 4   |
| 5  | 0.4000 | 0.0    | 0.0 | 0.0 | 4   | 4   |
| 6  | 0.3650 | 0.0    | 0.0 | 0.0 | 4   | 10  |
| 7  | 0.3300 | 1.0000 | 0.0 | 0.0 | 10  | 10  |
| 8  | 0.2700 | 1.0000 | 0.0 | 0.0 | 9   | 9   |
| 9  | 0.2250 | 0.0    | 0.0 | 0.0 | 9   | 9   |
| 10 | 0.1750 | 0.0    | 0.0 | 0.0 | 9   | 9   |
| 11 | 0.1000 | 0.0    | 0.0 | 0.0 | 9   | 9   |
| 12 | 0.0    | 0.0    | 0.0 | 0.0 | 9   | 9   |

Z-NODE FROM 34 TO 58

| I  | R      | PF     | H   | E   | IWC | IWP |
|----|--------|--------|-----|-----|-----|-----|
| 1  | 0.5350 | 0.0    | 0.0 | 0.0 | 0   | 7   |
| 2  | 0.5100 | 0.0    | 0.0 | 0.0 | 7   | 7   |
| 3  | 0.4750 | 0.0    | 0.0 | 0.0 | 7   | 7   |
| 4  | 0.4350 | 0.0    | 0.0 | 0.0 | 3   | 3   |
| 5  | 0.4000 | 0.0    | 0.0 | 0.0 | 3   | 3   |
| 6  | 0.3650 | 0.0    | 0.0 | 0.0 | 3   | 10  |
| 7  | 0.3300 | 1.0000 | 0.0 | 0.0 | 10  | 10  |
| 8  | 0.2700 | 1.0000 | 0.0 | 0.0 | 9   | 9   |
| 9  | 0.2250 | 0.0    | 0.0 | 0.0 | 9   | 9   |
| 10 | 0.1750 | 0.0    | 0.0 | 0.0 | 9   | 9   |
| 11 | 0.1000 | 0.0    | 0.0 | 0.0 | 9   | 9   |
| 12 | 0.0    | 0.0    | 0.0 | 0.0 | 9   | 9   |

Z-NODE FROM 59 TO 91

| I  | R      | PF     | H   | E   | IWC | IWP |
|----|--------|--------|-----|-----|-----|-----|
| 1  | 0.5350 | 0.0    | 0.0 | 0.0 | 0   | 7   |
| 2  | 0.5100 | 0.0    | 0.0 | 0.0 | 7   | 7   |
| 3  | 0.4750 | 0.0    | 0.0 | 0.0 | 7   | 7   |
| 4  | 0.4350 | 0.0    | 0.0 | 0.0 | 4   | 4   |
| 5  | 0.4000 | 0.0    | 0.0 | 0.0 | 4   | 4   |
| 6  | 0.3650 | 0.0    | 0.0 | 0.0 | 4   | 10  |
| 7  | 0.3300 | 1.0000 | 0.0 | 0.0 | 10  | 10  |
| 8  | 0.2700 | 1.0000 | 0.0 | 0.0 | 9   | 9   |
| 9  | 0.2250 | 0.0    | 0.0 | 0.0 | 9   | 9   |
| 10 | 0.1750 | 0.0    | 0.0 | 0.0 | 9   | 9   |
| 11 | 0.1000 | 0.0    | 0.0 | 0.0 | 9   | 9   |
| 12 | 0.0    | 0.0    | 0.0 | 0.0 | 9   | 9   |

DTA = 2.0000D-02

\*\*\* INITIAL TEMPERATURE FIELD OF FUEL ROD

Z-NODE FROM 1 TO 91

| 1              | 2              | 3        | 4        | 5        | 6        | 7        | 8        | 9        | 10       |
|----------------|----------------|----------|----------|----------|----------|----------|----------|----------|----------|
| 120.0000       | 120.0000       | 120.0000 | 120.0000 | 120.0000 | 120.0000 | 120.0000 | 120.0000 | 120.0000 | 120.0000 |
| 11<br>120.0000 | 12<br>120.0000 |          |          |          |          |          |          |          |          |









|    |        |        |        |        |        |        |        |        |        |        |        |        |
|----|--------|--------|--------|--------|--------|--------|--------|--------|--------|--------|--------|--------|
| 57 | 741.56 | 741.56 | 741.76 | 742.19 | 743.53 | 745.41 | 747.88 | 748.29 | 745.96 | 744.21 | 742.42 | 741.56 |
| 58 | 741.56 | 741.56 | 741.76 | 742.19 | 743.53 | 745.41 | 747.88 | 748.29 | 745.96 | 744.21 | 742.42 | 741.56 |
| 59 | 670.76 | 670.76 | 670.94 | 671.34 | 679.84 | 692.01 | 708.22 | 708.60 | 706.52 | 704.97 | 703.36 | 702.60 |
| 60 | 670.76 | 670.76 | 670.94 | 671.34 | 679.84 | 692.01 | 708.22 | 708.60 | 706.52 | 704.97 | 703.36 | 702.60 |
| 61 | 670.76 | 670.76 | 670.94 | 671.34 | 679.84 | 692.01 | 708.22 | 708.60 | 706.52 | 704.97 | 703.36 | 702.60 |
| 62 | 670.76 | 670.76 | 670.94 | 671.34 | 679.84 | 692.01 | 708.22 | 708.60 | 706.52 | 704.97 | 703.36 | 702.60 |
| 63 | 670.76 | 670.76 | 670.94 | 671.34 | 679.84 | 692.01 | 708.22 | 708.60 | 706.52 | 704.97 | 703.36 | 702.60 |
| 64 | 619.09 | 619.09 | 619.25 | 619.61 | 627.13 | 637.92 | 652.30 | 652.67 | 650.92 | 649.61 | 648.26 | 647.61 |
| 65 | 619.09 | 619.09 | 619.25 | 619.61 | 627.13 | 637.92 | 652.30 | 652.67 | 650.92 | 649.61 | 648.26 | 647.61 |
| 66 | 619.09 | 619.09 | 619.25 | 619.61 | 627.13 | 637.92 | 652.30 | 652.67 | 650.92 | 649.61 | 648.26 | 647.61 |
| 67 | 619.09 | 619.09 | 619.25 | 619.61 | 627.13 | 637.92 | 652.30 | 652.67 | 650.92 | 649.61 | 648.26 | 647.61 |
| 68 | 619.09 | 619.09 | 619.25 | 619.61 | 627.13 | 637.92 | 652.30 | 652.67 | 650.92 | 649.61 | 648.26 | 647.61 |
| 69 | 555.17 | 555.17 | 555.31 | 555.64 | 562.00 | 571.16 | 583.39 | 583.73 | 582.37 | 581.34 | 580.29 | 579.79 |
| 70 | 555.17 | 555.17 | 555.31 | 555.64 | 562.00 | 571.16 | 583.39 | 583.73 | 582.37 | 581.34 | 580.29 | 579.79 |
| 71 | 555.17 | 555.17 | 555.31 | 555.64 | 562.00 | 571.16 | 583.39 | 583.73 | 582.37 | 581.34 | 580.29 | 579.79 |
| 72 | 555.17 | 555.17 | 555.31 | 555.64 | 562.00 | 571.16 | 583.39 | 583.73 | 582.37 | 581.34 | 580.29 | 579.79 |
| 73 | 555.17 | 555.17 | 555.31 | 555.64 | 562.00 | 571.16 | 583.39 | 583.73 | 582.37 | 581.34 | 580.29 | 579.79 |
| 74 | 476.49 | 476.49 | 476.61 | 476.88 | 481.87 | 489.09 | 498.74 | 499.04 | 498.12 | 497.43 | 496.73 | 496.39 |
| 75 | 476.49 | 476.49 | 476.61 | 476.88 | 481.87 | 489.09 | 498.74 | 499.04 | 498.12 | 497.43 | 496.73 | 496.39 |
| 76 | 476.49 | 476.49 | 476.61 | 476.88 | 481.87 | 489.09 | 498.74 | 499.04 | 498.12 | 497.43 | 496.73 | 496.39 |
| 77 | 476.49 | 476.49 | 476.61 | 476.88 | 481.87 | 489.09 | 498.74 | 499.04 | 498.12 | 497.43 | 496.73 | 496.39 |
| 78 | 476.49 | 476.49 | 476.61 | 476.88 | 481.87 | 489.09 | 498.74 | 499.04 | 498.12 | 497.43 | 496.73 | 496.39 |
| 79 | 375.05 | 375.05 | 375.14 | 375.34 | 378.67 | 383.49 | 389.94 | 390.17 | 389.66 | 389.27 | 388.88 | 388.69 |
| 80 | 375.05 | 375.05 | 375.14 | 375.34 | 378.67 | 383.49 | 389.94 | 390.17 | 389.66 | 389.27 | 388.88 | 388.69 |
| 81 | 375.05 | 375.05 | 375.14 | 375.34 | 378.67 | 383.49 | 389.94 | 390.17 | 389.66 | 389.27 | 388.88 | 388.69 |
| 82 | 375.05 | 375.05 | 375.14 | 375.34 | 378.67 | 383.49 | 389.94 | 390.17 | 389.66 | 389.27 | 388.88 | 388.69 |
| 83 | 375.05 | 375.05 | 375.14 | 375.34 | 378.67 | 383.49 | 389.94 | 390.17 | 389.66 | 389.27 | 388.88 | 388.69 |
| 84 | 375.05 | 375.05 | 375.14 | 375.34 | 378.67 | 383.49 | 389.94 | 390.17 | 389.66 | 389.27 | 388.88 | 388.69 |
| 85 | 247.73 | 247.73 | 247.77 | 247.88 | 249.40 | 251.59 | 254.52 | 254.67 | 254.50 | 254.37 | 254.24 | 254.18 |
| 86 | 247.73 | 247.73 | 247.77 | 247.88 | 249.40 | 251.59 | 254.52 | 254.67 | 254.50 | 254.37 | 254.24 | 254.18 |
| 87 | 247.73 | 247.73 | 247.77 | 247.88 | 249.40 | 251.59 | 254.52 | 254.67 | 254.50 | 254.37 | 254.24 | 254.18 |
| 88 | 247.73 | 247.73 | 247.77 | 247.88 | 249.40 | 251.59 | 254.52 | 254.67 | 254.50 | 254.37 | 254.24 | 254.18 |
| 89 | 247.73 | 247.73 | 247.77 | 247.88 | 249.40 | 251.59 | 254.52 | 254.67 | 254.50 | 254.37 | 254.24 | 254.18 |
| 90 | 247.73 | 247.73 | 247.77 | 247.88 | 249.40 | 251.59 | 254.52 | 254.67 | 254.50 | 254.37 | 254.24 | 254.18 |
| 91 | 247.73 | 247.73 | 247.77 | 247.88 | 249.40 | 251.59 | 254.52 | 254.67 | 254.50 | 254.37 | 254.24 | 254.18 |

NAME(1)= 0

| TIME DMASS G(1) G(N1) GGAS 0.25000 -0.41772E-05 0.13329E-02 0.37220E-04 0.37220E-04                               |  |       |       |       |       |       |       |       |      |       |       |        |        |        |       |        |
|---|--|-------|-------|-------|-------|-------|-------|-------|------|-------|-------|--------|--------|--------|-------|--------|
| TIME  | USUP   | ULIN  | UDUP  | UCUP  | UGOUT | ULOUT | UGLOP | CRF   | DPDN | DPCR  | DPLOP | AMCOIN | AMCOR  | AMGS   | AMLS  | MERROR |
| <----> <---> <--- ( CM/SEC ) AT CORE WATER STATE -----> <--- ( M.AQ ) -----> <--- ( KG/M**2 ) AT CORE FLOW -----> |  |       |       |       |       |       |       |       |      |       |       |        |        |        |       |        |
| 10.00   | 4.788  | 4.788 | 3.526 | 4.474 | 1.305 | 0.981 | 0.0   | 0.206 | 0.0  | 4.52  | 0.0   | 526.5  | 406.8  | 89.3   | 32.1  | 1.3    |
|   | TIMES DMASS G(1) G(N1) GGAS 20.000 0.27707E-06 0.97705E-03 0.22939E-03 0.22939E-03   |       |       |       |       |       |       |       |      |       |       |        |        |        |       |        |
| 20.00   | 3.693  | 3.693 | 3.526 | 4.474 | 0.859 | 0.0   | 0.0   | 0.0   | 0.0  | 8.11  | 0.0   | 918.5  | 632.1  | 192.0  | 93.4  | 4.1    |
|   | TIMES DMASS G(1) G(N1) GGAS 40.000 -0.16391E-06 0.77644E-03 0.43591E-03 0.33853E-03  |       |       |       |       |       |       |       |      |       |       |        |        |        |       |        |
| 30.00   | 3.638  | 3.638 | 3.526 | 4.474 | 1.128 | 0.744 | 0.0   | 0.207 | 0.0  | 8.78  | 0.0   | 1267.2 | 804.9  | 300.1  | 158.1 | 7.2    |
|   | TIMES DMASS G(1) G(N1) GGAS 60.000 0.34721E-07 0.75513E-03 0.54341E-03 0.41395E-03   |       |       |       |       |       |       |       |      |       |       |        |        |        |       |        |
| 40.00   | 2.941  | 2.941 | 3.526 | 4.474 | 1.268 | 0.365 | 0.0   | 0.125 | 0.0  | 9.92  | 0.0   | 1566.9 | 939.1  | 411.0  | 209.6 | 10.3   |
|   | TIMES DMASS G(1) G(N1) GGAS 80.000 0.14890E-06 0.62036E-03 0.55609E-03 0.41564E-03   |       |       |       |       |       |       |       |      |       |       |        |        |        |       |        |
| 50.00   | 2.899  | 2.899 | 3.526 | 4.474 | 1.410 | 0.481 | 0.0   | 0.168 | 0.0  | 10.25 | 0.0   | 1841.3 | 1043.7 | 539.4  | 248.0 | 13.4   |
|   | TIMES DMASS G(1) G(N1) GGAS 100.000 -0.22002E-07 0.62454E-03 0.55675E-03 0.41433E-03 |       |       |       |       |       |       |       |      |       |       |        |        |        |       |        |
| 60.00   | 2.860  | 2.860 | 3.526 | 4.474 | 1.551 | 0.485 | 0.0   | 0.171 | 0.0  | 9.98  | 0.0   | 2111.4 | 1124.7 | 680.1  | 293.3 | 16.3   |
|   | TIMES DMASS G(1) G(N1) GGAS 80.000 0.14890E-06 0.62036E-03 0.55609E-03 0.41564E-03   |       |       |       |       |       |       |       |      |       |       |        |        |        |       |        |
| 70.00   | 2.638  | 2.638 | 3.526 | 4.474 | 1.606 | 0.643 | 0.0   | 0.246 | 0.0  | 9.41  | 0.0   | 2376.0 | 1178.6 | 828.5  | 352.8 | 19.1   |
|   | TIMES DMASS G(1) G(N1) GGAS 100.000 -0.22002E-07 0.62454E-03 0.55675E-03 0.41433E-03 |       |       |       |       |       |       |       |      |       |       |        |        |        |       |        |
| 80.00   | 2.347  | 2.347 | 3.526 | 4.474 | 1.557 | 0.504 | 0.0   | 0.217 | 0.0  | 8.99  | 0.0   | 2607.1 | 1202.2 | 982.0  | 404.6 | 21.5   |
|   | TIMES DMASS G(1) G(N1) GGAS 100.000 -0.22002E-07 0.62454E-03 0.55675E-03 0.41433E-03 |       |       |       |       |       |       |       |      |       |       |        |        |        |       |        |
| 90.00   | 2.280  | 2.280 | 3.526 | 4.474 | 1.542 | 0.493 | 0.0   | 0.218 | 0.0  | 8.61  | 0.0   | 2826.4 | 1226.6 | 1128.9 | 450.4 | 23.6   |





|    |        |        |        |        |        |        |        |        |        |        |        |        |
|----|--------|--------|--------|--------|--------|--------|--------|--------|--------|--------|--------|--------|
| 57 | 757.89 | 758.46 | 759.31 | 760.34 | 762.95 | 765.77 | 768.84 | 769.89 | 770.05 | 770.16 | 770.28 | 770.34 |
| 58 | 760.73 | 761.30 | 762.14 | 763.17 | 765.76 | 768.57 | 771.63 | 772.68 | 772.82 | 772.93 | 773.04 | 773.09 |
| 59 | 711.83 | 712.35 | 713.11 | 714.05 | 730.75 | 748.98 | 769.07 | 770.01 | 770.06 | 770.10 | 770.14 | 770.16 |
| 60 | 709.66 | 710.17 | 710.92 | 711.85 | 728.37 | 746.43 | 766.36 | 767.29 | 767.32 | 767.33 | 767.35 | 767.36 |
| 61 | 711.25 | 711.76 | 712.51 | 713.43 | 729.87 | 747.86 | 767.72 | 768.65 | 768.66 | 768.67 | 768.68 | 768.68 |
| 62 | 713.28 | 713.78 | 714.52 | 715.44 | 731.82 | 749.75 | 769.56 | 770.48 | 770.48 | 770.48 | 770.48 | 770.48 |
| 63 | 715.43 | 715.93 | 716.67 | 717.58 | 733.90 | 751.78 | 771.55 | 772.46 | 772.45 | 772.44 | 772.43 | 772.43 |
| 64 | 670.01 | 670.46 | 671.13 | 671.96 | 686.39 | 702.21 | 719.70 | 720.55 | 720.53 | 720.52 | 720.51 | 720.50 |
| 65 | 668.13 | 668.57 | 669.23 | 670.05 | 684.35 | 700.04 | 717.42 | 718.26 | 718.20 | 718.17 | 718.15 | 718.15 |
| 66 | 669.48 | 669.92 | 670.58 | 671.40 | 685.64 | 701.28 | 718.61 | 719.44 | 719.40 | 719.36 | 719.32 | 719.31 |
| 67 | 671.04 | 671.48 | 672.14 | 672.95 | 687.14 | 702.73 | 720.02 | 720.85 | 720.80 | 720.76 | 720.71 | 720.69 |
| 68 | 672.72 | 673.15 | 673.81 | 674.62 | 688.76 | 704.31 | 721.56 | 722.39 | 722.32 | 722.28 | 722.23 | 722.20 |
| 69 | 613.58 | 613.97 | 614.54 | 615.25 | 627.26 | 640.46 | 655.09 | 655.84 | 655.79 | 655.75 | 655.71 | 655.69 |
| 70 | 609.95 | 610.33 | 610.89 | 611.59 | 623.46 | 636.53 | 651.05 | 651.79 | 651.72 | 651.67 | 651.62 | 651.59 |
| 71 | 610.24 | 610.62 | 611.18 | 611.88 | 623.69 | 636.70 | 651.17 | 651.91 | 651.84 | 651.78 | 651.71 | 651.69 |
| 72 | 611.19 | 611.53 | 612.08 | 612.78 | 624.55 | 637.52 | 651.96 | 652.69 | 652.61 | 652.54 | 652.48 | 652.45 |
| 73 | 612.29 | 612.66 | 613.21 | 613.91 | 625.63 | 638.58 | 652.98 | 653.71 | 653.62 | 653.55 | 653.48 | 653.45 |
| 74 | 535.74 | 536.05 | 536.51 | 537.10 | 546.42 | 556.69 | 568.11 | 568.75 | 568.70 | 568.65 | 568.61 | 568.58 |
| 75 | 529.77 | 530.08 | 530.54 | 531.11 | 540.28 | 550.42 | 561.72 | 562.35 | 562.28 | 562.23 | 562.17 | 562.14 |
| 76 | 529.68 | 529.98 | 530.43 | 531.01 | 540.14 | 550.24 | 561.50 | 562.13 | 562.05 | 561.99 | 561.93 | 561.90 |
| 77 | 530.58 | 530.88 | 531.31 | 531.88 | 540.99 | 551.07 | 562.31 | 562.94 | 562.86 | 562.79 | 562.73 | 562.70 |
| 78 | 531.36 | 531.66 | 532.11 | 532.68 | 541.76 | 551.82 | 563.04 | 563.67 | 563.58 | 563.52 | 563.45 | 563.42 |
| 79 | 427.59 | 427.82 | 428.16 | 428.59 | 434.80 | 441.65 | 449.28 | 449.78 | 449.75 | 449.72 | 449.70 | 449.68 |
| 80 | 419.21 | 419.44 | 419.77 | 420.19 | 426.25 | 432.96 | 440.46 | 440.96 | 440.91 | 440.87 | 440.84 | 440.82 |
| 81 | 418.54 | 418.76 | 419.09 | 419.51 | 425.54 | 432.22 | 439.69 | 440.18 | 440.13 | 440.09 | 440.06 | 440.04 |
| 82 | 418.85 | 419.07 | 419.40 | 419.82 | 425.83 | 432.50 | 439.96 | 440.45 | 440.40 | 440.36 | 440.32 | 440.30 |
| 83 | 419.42 | 419.64 | 419.97 | 420.39 | 426.39 | 433.04 | 440.49 | 440.98 | 440.92 | 440.88 | 440.84 | 440.82 |
| 84 | 420.00 | 420.22 | 420.54 | 420.96 | 426.94 | 433.59 | 441.03 | 441.51 | 441.46 | 441.42 | 441.38 | 441.36 |
| 85 | 284.02 | 284.14 | 284.32 | 284.54 | 287.31 | 290.36 | 293.76 | 294.04 | 294.03 | 294.02 | 294.01 | 294.01 |
| 86 | 275.52 | 275.63 | 275.80 | 276.02 | 278.68 | 281.63 | 284.93 | 285.21 | 285.19 | 285.18 | 285.16 | 285.15 |
| 87 | 275.01 | 275.12 | 275.29 | 275.50 | 278.14 | 281.08 | 284.37 | 284.65 | 284.63 | 284.61 | 284.60 | 284.59 |
| 88 | 275.16 | 275.27 | 275.44 | 275.65 | 278.29 | 281.22 | 284.51 | 284.79 | 284.77 | 284.75 | 284.74 | 284.73 |
| 89 | 275.42 | 275.53 | 275.70 | 275.91 | 278.54 | 281.47 | 284.76 | 285.03 | 285.01 | 285.00 | 284.98 | 284.97 |
| 90 | 275.82 | 275.93 | 276.09 | 276.31 | 278.94 | 281.86 | 285.15 | 285.42 | 285.40 | 285.38 | 285.37 | 285.36 |
| 91 | 276.04 | 276.15 | 276.32 | 276.53 | 279.15 | 282.08 | 285.36 | 285.63 | 285.61 | 285.59 | 285.58 | 285.57 |

| FUEL TEMPERATURE | ( TIME = 100.00 ( SEC ) )  |
|------------------|--|
| J                | TFPC(1,J) TFPC(2,J) TFPC(3,J) TFPC(4,J) TFPC(5,J) TFPC(6,J) TFPC(7,J) TFPC(8,J) TFPC(9,J) TFPC(10,J) TFPC(11,J) TFPC(12,J) |
| 1                | 138.66   |
| 2                | 138.66   |
| 3                | 138.66   |
| 4                | 138.66   |
| 5                | 138.66   |
| 6                | 138.66   |
| 7                | 138.66   |
| 8                | 140.17   |
| 9                | 140.17   |
| 10               | 140.17   |
| 11               | 140.17   |
| 12               | 140.17   |
| 13               | 140.17   |
| 14               | 141.02   |
| 15               | 141.02   |
| 16               | 141.02   |
| 17               | 141.02   |
| 18               | 141.02   |
| 19               | 141.56   |
| 20               | 141.56   |
| 21               | 141.56   |
| 22               | 141.56   |
| 23               | 141.56   |
| 24               | 141.96   |
| 25               | 141.96   |
| 26               | 480.25   |
| 27               | 507.31   |
| 28               | 526.96   |
| 29               | 582.94   |
| 30               | 597.09   |
| 31               | 609.75   |
| 32               | 620.95   |
| 33               | 631.25   |
| 34               | 683.30   |
| 35               | 691.74   |
| 36               | 699.37   |
| 37               | 706.40   |
| 38               | 712.50   |
| 39               | 737.27   |
| 40               | 744.02   |
| 41               | 751.35   |
| 42               | 758.46   |
| 43               | 765.94   |
| 44               | 779.75   |
| 45               | 786.55   |
| 46               | 791.57   |
| 47               | 797.25   |
| 48               | 801.40   |
| 49               | 798.46   |
| 50               | 802.10   |
| 51               | 806.16   |
| 52               | 810.11   |
| 53               | 813.92   |
| 54               | 797.00   |
| 55               | 799.07   |
| 56               | 802.00   |

|    |        |        |        |        |        |        |        |        |        |        |        |        |
|----|--------|--------|--------|--------|--------|--------|--------|--------|--------|--------|--------|--------|
| 57 | 804.97 | 805.59 | 806.51 | 807.62 | 810.46 | 813.54 | 816.89 | 818.01 | 818.19 | 818.32 | 818.45 | 818.52 |
| 58 | 807.87 | 808.49 | 809.40 | 810.51 | 813.34 | 816.40 | 819.74 | 820.86 | 821.02 | 821.14 | 821.27 | 821.32 |
| 59 | 756.51 | 757.07 | 757.89 | 758.91 | 777.42 | 797.65 | 819.91 | 820.91 | 820.96 | 821.00 | 821.05 | 821.07 |
| 60 | 754.59 | 755.14 | 755.95 | 756.96 | 775.28 | 795.33 | 817.43 | 818.42 | 818.45 | 818.47 | 818.48 | 818.49 |
| 61 | 756.29 | 756.83 | 757.64 | 758.64 | 776.88 | 796.85 | 818.89 | 819.87 | 819.88 | 819.89 | 819.89 | 819.89 |
| 62 | 758.38 | 758.92 | 759.73 | 760.72 | 778.89 | 798.80 | 820.77 | 821.75 | 821.74 | 821.74 | 821.74 | 821.73 |
| 63 | 760.59 | 761.13 | 761.93 | 762.91 | 781.02 | 800.88 | 822.79 | 823.76 | 823.74 | 823.73 | 823.72 | 823.71 |
| 64 | 712.25 | 712.74 | 713.47 | 714.36 | 730.34 | 747.87 | 767.26 | 768.16 | 768.13 | 768.11 | 768.09 | 768.08 |
| 65 | 710.56 | 711.04 | 711.75 | 712.64 | 728.48 | 745.87 | 765.15 | 766.04 | 765.99 | 765.95 | 765.91 | 765.89 |
| 66 | 711.98 | 712.46 | 713.17 | 714.05 | 729.83 | 747.17 | 766.39 | 767.27 | 767.22 | 767.17 | 767.12 | 767.10 |
| 67 | 713.60 | 714.07 | 714.78 | 715.66 | 731.38 | 748.67 | 767.85 | 768.72 | 768.66 | 768.60 | 768.55 | 768.52 |
| 68 | 715.31 | 715.79 | 716.49 | 717.37 | 733.03 | 750.28 | 769.42 | 770.29 | 770.21 | 770.15 | 770.09 | 770.06 |
| 69 | 652.19 | 652.60 | 653.22 | 653.98 | 667.24 | 681.84 | 698.03 | 698.82 | 698.75 | 698.70 | 698.65 | 698.62 |
| 70 | 648.70 | 649.10 | 649.71 | 650.47 | 663.59 | 678.04 | 694.11 | 694.90 | 694.81 | 694.74 | 694.67 | 694.64 |
| 71 | 649.07 | 649.47 | 650.08 | 650.83 | 663.89 | 678.28 | 694.30 | 695.09 | 694.99 | 694.91 | 694.84 | 694.80 |
| 72 | 650.04 | 650.44 | 651.04 | 651.79 | 664.80 | 679.15 | 695.13 | 695.91 | 695.81 | 695.73 | 695.64 | 695.60 |
| 73 | 651.22 | 651.62 | 652.22 | 652.97 | 665.93 | 680.25 | 696.19 | 696.86 | 696.77 | 696.68 | 696.64 | 696.64 |
| 74 | 569.13 | 569.46 | 569.96 | 570.59 | 580.86 | 592.20 | 604.83 | 605.50 | 605.43 | 605.37 | 605.31 | 605.28 |
| 75 | 563.20 | 563.53 | 564.02 | 564.64 | 574.75 | 585.95 | 598.44 | 599.11 | 599.01 | 598.94 | 598.86 | 598.83 |
| 76 | 563.17 | 563.50 | 563.99 | 564.60 | 574.68 | 585.83 | 598.29 | 599.85 | 598.77 | 598.69 | 598.65 | 598.65 |
| 77 | 564.07 | 564.40 | 564.89 | 565.50 | 575.55 | 586.68 | 599.11 | 599.78 | 599.67 | 599.59 | 599.50 | 599.46 |
| 78 | 564.90 | 565.23 | 565.71 | 566.32 | 576.34 | 587.45 | 599.86 | 600.52 | 600.41 | 600.33 | 600.24 | 600.20 |
| 79 | 452.89 | 453.14 | 453.51 | 453.97 | 460.81 | 468.39 | 476.84 | 477.37 | 477.32 | 477.28 | 477.25 | 477.23 |
| 80 | 444.06 | 444.30 | 444.66 | 445.11 | 451.79 | 459.21 | 467.51 | 468.03 | 467.97 | 467.93 | 467.88 | 467.86 |
| 81 | 443.44 | 443.67 | 444.03 | 444.48 | 451.13 | 458.51 | 466.79 | 467.31 | 467.24 | 467.19 | 467.14 | 467.12 |
| 82 | 443.78 | 444.01 | 444.37 | 444.82 | 451.45 | 458.82 | 467.08 | 467.59 | 467.53 | 467.48 | 467.43 | 467.40 |
| 83 | 444.36 | 444.60 | 444.95 | 445.40 | 452.01 | 459.37 | 467.62 | 468.14 | 468.07 | 468.02 | 467.96 | 467.94 |
| 84 | 444.95 | 445.18 | 445.54 | 445.98 | 452.58 | 459.93 | 468.17 | 468.68 | 468.61 | 468.56 | 468.51 | 468.48 |
| 85 | 298.24 | 298.37 | 298.56 | 298.80 | 301.86 | 305.24 | 309.00 | 309.30 | 309.29 | 309.28 | 309.27 | 309.26 |
| 86 | 288.51 | 288.64 | 288.82 | 289.05 | 291.98 | 295.24 | 298.89 | 299.18 | 299.16 | 299.15 | 299.13 | 299.12 |
| 87 | 288.02 | 288.14 | 288.32 | 288.55 | 291.47 | 294.71 | 298.35 | 298.64 | 298.52 | 298.60 | 298.58 | 298.58 |
| 88 | 288.19 | 288.31 | 288.49 | 288.72 | 291.63 | 294.86 | 298.50 | 298.79 | 298.77 | 298.75 | 298.73 | 298.72 |
| 89 | 288.43 | 288.55 | 288.74 | 288.97 | 291.87 | 295.10 | 298.73 | 299.03 | 299.00 | 298.98 | 298.96 | 298.95 |
| 90 | 288.83 | 288.95 | 289.14 | 289.37 | 292.26 | 295.50 | 299.12 | 299.42 | 299.39 | 299.37 | 299.35 | 299.35 |
| 91 | 289.06 | 289.18 | 289.36 | 289.59 | 292.48 | 295.71 | 299.33 | 299.62 | 299.60 | 299.58 | 299.56 | 299.55 |

NAME(1) = 100

| TIME  | USUP                        | ULIN  | UDUP                                 | UCUP                 | UGOUT  | ULOUT                                | UGLOP                | CRF         | DPDN                 | DPCR                 | DPLOP       | AMCOIN               | AMCOR                | AMGS   | AMLS                 | MERROR               |  |
|---|-----------------------------|-------|--------------------------------------|----------------------|--------|--------------------------------------|----------------------|-------------|----------------------|----------------------|-------------|----------------------|----------------------|--------|----------------------|----------------------|--|
|   |                             |       |                                      |                      |        |                                      |                      |             |                      |                      |             |                      |                      |        |                      |                      |  |
| <---- ( CM/SEC ) AT CORE WATER STATE -----> | <--- ( M.AQ ) ----->        |       | <--- ( KG/M**2 ) AT CORE FLOW -----> | <--- ( M.AQ ) -----> |        | <--- ( KG/M**2 ) AT CORE FLOW -----> | <--- ( M.AQ ) -----> |             | <--- ( M.AQ ) -----> | <--- ( M.AQ ) -----> |             | <--- ( M.AQ ) -----> | <--- ( M.AQ ) -----> |        | <--- ( M.AQ ) -----> | <--- ( M.AQ ) -----> |  |
| 100.00                                      | 2.361                       | 2.361 | 3.526                                | 4.474                | 1.552  | 0.533                                | 0.0                  | 0.228       | 0.0                  | 8.33                 | 0.0         | 3045.5               | 1253.5               | 1274.8 | 494.7                | 25.6                 |  |
| 110.00                                      | 2.259                       | 2.259 | 3.526                                | 4.474                | 1.553  | 0.487                                | 0.0                  | 0.218       | 0.0                  | 8.07                 | 0.0         | 3261.1               | 1277.0               | 1419.3 | 540.3                | 27.6                 |  |
|   | TIMES DMASS G(1) G(N1) GGAS |       |                                      |                      | 120.00 |                                      | 0.23050E-07          | 0.62503E-03 | 0.55428E-03          |                      | 0.39045E-03 |                      |                      |        |                      |                      |  |
| 120.00                                      | 2.362                       | 2.362 | 3.526                                | 4.474                | 1.663  | 0.614                                | 0.0                  | 0.262       | 0.0                  | 7.79                 | 0.0         | 3482.3               | 1302.0               | 1560.7 | 593.3                | 29.5                 |  |
| 130.00                                      | 1.944                       | 1.944 | 3.526                                | 4.474                | 1.476  | 0.487                                | 0.0                  | 0.253       | 0.0                  | 7.69                 | 0.0         | 3680.3               | 1307.7               | 1701.5 | 642.9                | 31.2                 |  |
|   | TIMES DMASS G(1) G(N1) GGAS |       |                                      |                      | 140.00 |                                      | -0.86380E-07         | 0.60407E-03 | 0.54102E-03          |                      | 0.38018E-03 |                      |                      |        |                      |                      |  |
| 140.00                                      | 2.281                       | 2.281 | 3.526                                | 4.474                | 1.424  | 0.602                                | 0.0                  | 0.266       | 0.0                  | 7.38                 | 0.0         | 3878.0               | 1314.7               | 1839.9 | 693.7                | 32.8                 |  |
|   | TIMES DMASS G(1) G(N1) GGAS |       |                                      |                      | 180.00 |                                      | -0.12049E-07         | 0.57422E-03 | 0.53438E-03          |                      | 0.37029E-03 |                      |                      |        |                      |                      |  |
| 150.00                                      | 2.467                       | 2.467 | 3.526                                | 4.474                | 1.394  | 0.688                                | 0.0                  | 0.281       | 0.0                  | 7.22                 | 0.0         | 4104.8               | 1340.8               | 1974.6 | 757.8                | 34.6                 |  |
|   | TIMES DMASS G(1) G(N1) GGAS |       |                                      |                      | 160.00 |                                      | 0.55879E-08          | 0.52825E-03 | 0.55884E-03          |                      | 0.39482E-03 |                      |                      |        |                      |                      |  |
| 160.00                                      | 1.995                       | 1.995 | 3.526                                | 4.474                | 1.479  | 0.614                                | 0.0                  | 0.311       | 0.0                  | 7.24                 | 0.0         | 4311.4               | 1347.8               | 2112.2 | 818.2                | 36.2                 |  |
| 170.00                                      | 1.876                       | 1.876 | 3.526                                | 4.474                | 1.426  | 0.350                                | 0.0                  | 0.188       | 0.0                  | 7.16                 | 0.0         | 4500.8               | 1346.2               | 2247.5 | 872.3                | 37.7                 |  |
|   | TIMES DMASS G(1) G(N1) GGAS |       |                                      |                      | 200.00 |                                      | 0.11224E-05          | 0.55099E-03 | 0.35608E-03          |                      | 0.35608E-03 |                      |                      |        |                      |                      |  |
| 180.00                                      | 2.168                       | 2.168 | 3.526                                | 4.474                | 1.387  | 0.615                                | 0.0                  | 0.286       | 0.0                  | 7.06                 | 0.0         | 4670.5               | 1332.5               | 2379.9 | 922.2                | 39.0                 |  |
| 190.00                                      | 1.852                       | 1.852 | 3.526                                | 4.474                | 1.427  | 0.575                                | 0.0                  | 0.313       | 0.0                  | 7.33                 | 0.0         | 4889.2               | 1361.7               | 2508.6 | 981.2                | 40.7                 |  |
|   | TIMES DMASS G(1) G(N1) GGAS |       |                                      |                      | 200.00 |                                      | -0.68452E-07         | 0.55099E-03 | 0.12187E-03          |                      | 0.35734E-03 |                      |                      |        |                      |                      |  |
|   | TIMES DMASS G(1) G(N1) GGAS |       |                                      |                      | 200.00 |                                      | 0.11224E-05          | 0.55099E-03 | 0.35608E-03          |                      | 0.35608E-03 |                      |                      |        |                      |                      |  |







|    |        |        |        |        |        |        |        |        |        |        |        |        |
|----|--------|--------|--------|--------|--------|--------|--------|--------|--------|--------|--------|--------|
| 57 | 751.14 | 751.72 | 752.56 | 753.61 | 756.24 | 759.09 | 762.19 | 763.29 | 763.60 | 763.85 | 764.12 | 764.24 |
| 58 | 756.31 | 756.87 | 757.21 | 758.73 | 761.33 | 764.16 | 767.24 | 768.32 | 768.62 | 768.86 | 769.12 | 769.24 |
| 59 | 721.98 | 722.51 | 723.29 | 724.27 | 741.81 | 760.88 | 781.68 | 782.68 | 782.97 | 783.18 | 783.40 | 783.51 |
| 60 | 724.00 | 724.54 | 725.33 | 726.31 | 745.85 | 762.86 | 783.40 | 784.59 | 784.86 | 785.06 | 785.27 | 785.37 |
| 61 | 727.56 | 728.11 | 728.91 | 729.89 | 747.47 | 766.48 | 787.20 | 788.19 | 788.45 | 788.65 | 788.85 | 788.95 |
| 62 | 731.28 | 731.83 | 732.64 | 733.62 | 751.22 | 770.23 | 790.94 | 791.92 | 792.18 | 792.38 | 792.58 | 792.67 |
| 63 | 735.04 | 735.59 | 736.40 | 737.38 | 754.98 | 773.98 | 794.69 | 795.67 | 795.93 | 796.12 | 796.31 | 796.41 |
| 64 | 690.32 | 690.83 | 691.56 | 692.45 | 708.06 | 724.91 | 743.26 | 744.17 | 744.39 | 744.55 | 744.71 | 744.79 |
| 65 | 691.78 | 692.28 | 693.01 | 693.90 | 709.46 | 726.25 | 744.55 | 745.46 | 745.67 | 745.82 | 745.97 | 746.05 |
| 66 | 694.75 | 695.24 | 695.99 | 696.88 | 712.42 | 729.20 | 747.49 | 748.39 | 748.59 | 748.74 | 748.89 | 748.97 |
| 67 | 697.80 | 698.31 | 699.04 | 699.93 | 715.46 | 732.22 | 750.49 | 751.39 | 751.59 | 751.73 | 751.88 | 751.96 |
| 68 | 700.88 | 701.38 | 702.11 | 703.00 | 718.52 | 735.26 | 753.53 | 754.42 | 754.61 | 754.75 | 754.90 | 754.97 |
| 69 | 640.18 | 640.62 | 641.27 | 642.05 | 655.23 | 669.44 | 684.93 | 685.74 | 685.90 | 686.01 | 686.13 | 686.18 |
| 70 | 640.06 | 640.51 | 641.15 | 641.92 | 655.04 | 669.19 | 684.62 | 685.43 | 685.57 | 685.68 | 685.78 | 685.84 |
| 71 | 642.02 | 642.46 | 643.10 | 643.88 | 656.97 | 671.09 | 686.50 | 687.30 | 687.44 | 687.54 | 687.65 | 687.70 |
| 72 | 644.26 | 644.70 | 645.34 | 646.11 | 659.19 | 673.29 | 688.69 | 689.49 | 689.62 | 689.72 | 689.82 | 689.87 |
| 73 | 644.59 | 647.03 | 647.67 | 648.44 | 661.50 | 675.58 | 690.99 | 691.77 | 691.90 | 691.99 | 692.09 | 692.14 |
| 74 | 564.76 | 565.13 | 565.67 | 566.31 | 576.65 | 587.80 | 599.98 | 600.68 | 600.77 | 600.85 | 600.92 | 600.96 |
| 75 | 562.61 | 562.98 | 563.51 | 564.15 | 574.42 | 585.49 | 597.59 | 598.29 | 598.38 | 598.44 | 598.51 | 598.54 |
| 76 | 563.86 | 564.23 | 564.76 | 565.40 | 575.64 | 586.69 | 598.78 | 599.47 | 599.55 | 599.62 | 599.68 | 599.71 |
| 77 | 565.60 | 565.97 | 566.50 | 567.14 | 577.37 | 588.42 | 600.49 | 601.18 | 601.26 | 601.32 | 601.39 | 601.42 |
| 78 | 567.31 | 567.67 | 568.20 | 568.84 | 579.06 | 590.09 | 602.16 | 602.84 | 602.92 | 602.98 | 603.04 | 603.07 |
| 79 | 451.48 | 451.75 | 452.14 | 452.62 | 459.53 | 467.00 | 475.16 | 475.71 | 475.76 | 475.79 | 475.83 | 475.85 |
| 80 | 446.76 | 447.03 | 447.43 | 447.90 | 454.73 | 462.10 | 470.18 | 470.72 | 470.76 | 470.79 | 470.83 | 470.84 |
| 81 | 447.18 | 447.45 | 447.84 | 448.31 | 455.12 | 462.48 | 470.55 | 471.09 | 471.12 | 471.15 | 471.18 | 471.20 |
| 82 | 448.17 | 448.44 | 448.83 | 449.30 | 456.11 | 463.46 | 471.51 | 472.05 | 472.09 | 472.11 | 472.14 | 472.16 |
| 83 | 449.30 | 449.57 | 449.96 | 450.43 | 457.23 | 464.57 | 472.62 | 473.16 | 473.19 | 473.22 | 473.25 | 473.26 |
| 84 | 450.42 | 450.69 | 451.08 | 451.55 | 458.34 | 465.68 | 473.72 | 474.26 | 474.29 | 474.32 | 474.35 | 474.36 |
| 85 | 297.08 | 297.22 | 297.43 | 297.67 | 300.76 | 304.09 | 307.72 | 308.04 | 308.05 | 308.07 | 308.08 | 308.09 |
| 86 | 291.19 | 291.34 | 291.54 | 291.79 | 294.82 | 298.08 | 301.65 | 301.96 | 301.98 | 301.99 | 302.00 |        |
| 87 | 291.20 | 291.34 | 291.55 | 291.79 | 294.81 | 298.07 | 301.64 | 301.95 | 301.96 | 301.97 | 301.97 | 301.98 |
| 88 | 291.61 | 291.76 | 291.96 | 292.21 | 295.22 | 298.48 | 302.04 | 302.35 | 302.36 | 302.37 | 302.38 | 302.38 |
| 89 | 292.08 | 292.22 | 292.42 | 292.67 | 295.68 | 298.94 | 302.50 | 302.81 | 302.82 | 302.82 | 302.83 | 302.84 |
| 90 | 292.62 | 292.77 | 292.97 | 293.22 | 296.23 | 299.48 | 303.04 | 303.35 | 303.36 | 303.37 | 303.37 | 303.38 |
| 91 | 293.07 | 293.21 | 293.42 | 293.66 | 296.67 | 299.92 | 303.47 | 303.78 | 303.79 | 303.80 | 303.81 | 303.81 |

NAME(1) = 200

| TIME | USUP   | ULIN       | UDUP    | UCUP  | UGOUT | ULOUT  | UGLDP  | CRF   | DPDN     | DPCR   | DPLDP | AMCOIN      | AMCOR   | AMGS | AMLS | MERROR |
|------|--------|------------|---------|-------|-------|--------|--------|-------|----------|--------|-------|-------------|---------|------|------|--------|
|      | <----> | ( CM/SEC ) | AT CORE | WATER | STATE | -----> | -----> | <---> | ( M.AQ ) | -----> | <---> | ( KG/M**2 ) | AT CORE | FLOW | -->  |        |

|        |                        |       |       |       |       |        |              |             |      |              |     |        |             |        |        |      |
|--------|------------------------|-------|-------|-------|-------|--------|--------------|-------------|------|--------------|-----|--------|-------------|--------|--------|------|
| 200.00 | 2.081                  | 2.081 | 3.526 | 4.474 | 1.334 | 0.0    | 0.0          | 0.0         | 7.35 | 0.0          | 0.0 | 5087.9 | 1364.8      | 2638.9 | 1045.1 | 42.3 |
| 210.00 | 2.492                  | 2.492 | 3.526 | 4.474 | 1.378 | 0.874  | 0.0          | 0.353       | 6.99 | 0.0          | 0.0 | 5286.9 | 1364.8      | 2765.9 | 1115.5 | 43.8 |
|        | TIMES DMASS G(1) G(N1) | GGAS  |       |       |       | 220.00 | -0.30035E-07 | 0.61049E-03 |      | 0.569972E-03 |     |        | 0.37319E-03 |        |        |      |
| 220.00 | 2.304                  | 2.304 | 3.526 | 4.474 | 1.398 | 0.737  | 0.0          | 0.322       | 6.90 | 0.0          | 0.0 | 5518.2 | 1384.7      | 2893.8 | 1197.3 | 45.5 |
| 230.00 | 1.655                  | 1.655 | 3.526 | 4.474 | 1.318 | 0.925  | 0.0          | 0.563       | 6.57 | 0.0          | 0.0 | 5681.5 | 1342.3      | 3024.1 | 1271.5 | 46.7 |
|        | TIMES DMASS G(1) G(N1) | GGAS  |       |       |       | 237.50 | 0.11500E-05  | 0.33702E-03 |      | 0.33730E-03  |     |        | 0.33730E-03 |        |        |      |
|        | TIMES DMASS G(1) G(N1) | GGAS  |       |       |       | 240.00 | -0.74026E-07 | 0.58841E-03 |      | 0.47446E-03  |     |        | 0.36618E-03 |        |        |      |
| 240.00 | 1.466                  | 1.466 | 3.526 | 4.474 | 1.372 | 0.406  | 0.0          | 0.279       | 6.81 | 0.0          | 0.0 | 5820.8 | 1304.1      | 3151.6 | 1520.5 | 47.8 |

| TIME | USUP   | ULIN       | UDUP    | UCUP  | UGOUT | ULOUT  | UGLDP  | CRF   | DPDN     | DPCR   | DPLDP | AMCOIN      | AMCOR   | AMGS | AMLS | MERROR |
|------|--------|------------|---------|-------|-------|--------|--------|-------|----------|--------|-------|-------------|---------|------|------|--------|
|      | <----> | ( CM/SEC ) | AT CORE | WATER | STATE | -----> | -----> | <---> | ( M.AQ ) | -----> | <---> | ( KG/M**2 ) | AT CORE | FLOW | -->  |        |

|        |                        |       |       |       |       |        |              |             |      |             |     |        |             |        |        |      |
|--------|------------------------|-------|-------|-------|-------|--------|--------------|-------------|------|-------------|-----|--------|-------------|--------|--------|------|
| 250.00 | 2.779                  | 2.779 | 3.526 | 4.474 | 1.235 | 0.999  | 0.0          | 0.362       | 6.72 | 0.0         | 0.0 | 6040.8 | 1340.3      | 3270.1 | 1384.0 | 49.4 |
|        | TIMES DMASS G(1) G(N1) | GGAS  |       |       |       | 253.50 | 0.12412E-05  | 0.74043E-03 |      | 0.33782E-03 |     |        | 0.33782E-03 |        |        |      |
|        | TIMES DMASS G(1) G(N1) | GGAS  |       |       |       | 257.00 | 0.89291E-06  | 0.66501E-03 |      | 0.33486E-03 |     |        | 0.33486E-03 |        |        |      |
|        | TIMES DMASS G(1) G(N1) | GGAS  |       |       |       | 260.00 | -0.78115E-07 | 0.47326E-03 |      | 0.51904E-03 |     |        | 0.36345E-03 |        |        |      |

|        |                        |       |       |       |       |        |              |             |      |             |     |        |             |        |        |      |
|--------|------------------------|-------|-------|-------|-------|--------|--------------|-------------|------|-------------|-----|--------|-------------|--------|--------|------|
| 260.00 | 1.787                  | 1.787 | 3.526 | 4.474 | 1.362 | 0.583  | 0.0          | 0.329       | 6.98 | 0.0         | 0.0 | 6284.9 | 1382.5      | 3390.8 | 1463.5 | 51.2 |
| 270.00 | 1.965                  | 1.965 | 3.526 | 4.474 | 1.253 | 0.439  | 0.0          | 0.225       | 7.01 | 0.0         | 0.0 | 6417.4 | 1329.4      | 3515.0 | 1523.9 | 52.2 |
|        | TIMES DMASS G(1) G(N1) | GGAS  |       |       |       | 280.00 | -0.75870E-09 | 0.54224E-03 |      | 0.51326E-03 |     |        | 0.34203E-03 |        |        |      |
| 280.00 | 2.048                  | 2.048 | 3.526 | 4.474 | 1.281 | 0.641  | 0.0          | 0.316       | 7.33 | 0.0         | 0.0 | 6625.4 | 1362.3      | 3633.3 | 1579.0 | 53.8 |
| 290.00 | 1.792                  | 1.792 | 3.526 | 4.474 | 1.339 | 0.828  | 0.0          | 0.477       | 7.36 | 0.0         | 0.0 | 6808.8 | 1364.0      | 3734.5 | 1638.1 | 55.3 |
|        | TIMES DMASS G(1) G(N1) | GGAS  |       |       |       | 300.00 | -0.10201E-07 | 0.63344E-03 |      | 0.50768E-03 |     |        | 0.33608E-03 |        |        |      |

















## AXIAL NODE OF STORED OUTPUT DATA

```

EL.1 = 10
EL.2 = 26
EL.3 = 46
EL.4 = 61
EL.5 = 76
EL.6 = 91

```

## RADIAL NODE OF STORED OUTPUT DATA

| ( EL.1 ) | ( EL.2 ) | ( EL.3 ) | ( EL.4 ) | ( EL.5 ) |
|----------|----------|----------|----------|----------|
| R.1 = 1  |
| R.2 = 4  |
| R.3 = 8  |
| R.4 = 12 |

## CONTROL DATA

| TIME<br>( SEC ) | MAXPOWER<br>( KW/M ) | FLOWRATE<br>( CM/SEC ) | PRESSURE<br>( KG/CM**2 ) | DPCORE<br>( M.AG ) | DPDOWN<br>( M.AG ) | DPLoop<br>( M.AG ) | WGOUT<br>( KG/M**2H ) |
|-----------------|----------------------|------------------------|--------------------------|--------------------|--------------------|--------------------|-----------------------|
| 0.0             | 2.08600              | 4.99329                | 2.08391                  | 0.102166E-01       | 0.0                | 0.0                | 16993.4               |
| 10.0000         | 1.98895              | 4.78839                | 2.50962                  | 0.466525           | 0.0                | 0.0                | 44272.5               |
| 20.0000         | 1.91494              | 3.69299                | 2.84814                  | 0.704347           | 0.0                | 0.0                | 29155.7               |
| 30.0000         | 1.85665              | 3.63752                | 2.91181                  | 0.878486           | 0.0                | 0.0                | 38285.9               |
| 40.0000         | 1.80883              | 2.94053                | 3.01862                  | 1.02528            | 0.0                | 0.0                | 43027.2               |
| 50.0000         | 1.76844              | 2.89917                | 3.05021                  | 1.13974            | 0.0                | 0.0                | 47840.0               |
| 60.0000         | 1.73359              | 2.85997                | 3.02457                  | 1.22442            | 0.0                | 0.0                | 52612.7               |
| 70.0000         | 1.70300              | 2.63786                | 2.97036                  | 1.28675            | 0.0                | 0.0                | 54477.4               |
| 80.0000         | 1.67581              | 2.34710                | 2.93148                  | 1.30543            | 0.0                | 0.0                | 52828.2               |
| 90.0000         | 1.65136              | 2.28025                | 2.89584                  | 1.33659            | 0.0                | 0.0                | 52305.1               |
| 100.000         | 1.62919              | 2.36118                | 2.86890                  | 1.36392            | 0.0                | 0.0                | 52661.4               |
| 110.000         | 1.60891              | 2.25877                | 2.84414                  | 1.38711            | 0.0                | 0.0                | 52708.0               |
| 120.000         | 1.59026              | 2.36160                | 2.81784                  | 1.41061            | 0.0                | 0.0                | 49625.9               |
| 130.000         | 1.58954              | 1.94354                | 2.80903                  | 1.41613            | 0.0                | 0.0                | 50095.9               |
| 140.000         | 1.56443              | 2.28139                | 2.77930                  | 1.42189            | 0.0                | 0.0                | 48320.9               |
| 150.000         | 1.54112              | 2.46702                | 2.76482                  | 1.44852            | 0.0                | 0.0                | 47301.0               |
| 160.000         | 1.51939              | 1.99474                | 2.76603                  | 1.46119            | 0.0                | 0.0                | 50181.4               |
| 170.000         | 1.49907              | 1.87581                | 2.75903                  | 1.45798            | 0.0                | 0.0                | 48373.7               |
| 180.000         | 1.48000              | 2.16789                | 2.74955                  | 1.44226            | 0.0                | 0.0                | 47064.1               |
| 190.000         | 1.46204              | 1.85236                | 2.77495                  | 1.47458            | 0.0                | 0.0                | 48424.6               |
| 200.000         | 1.44508              | 2.08087                | 2.77697                  | 1.47387            | 0.0                | 0.0                | 45257.6               |
| 210.000         | 1.42903              | 2.49175                | 2.74231                  | 1.47560            | 0.0                | 0.0                | 46737.5               |
| 220.000         | 1.41380              | 2.30439                | 2.73403                  | 1.49710            | 0.0                | 0.0                | 47433.1               |
| 230.000         | 1.39932              | 1.45511                | 2.70269                  | 1.45015            | 0.0                | 0.0                | 44733.7               |
| 240.000         | 1.38553              | 1.46600                | 2.72592                  | 1.40968            | 0.0                | 0.0                | 46538.9               |
| 250.000         | 1.37236              | 2.77866                | 2.71684                  | 1.44734            | 0.0                | 0.0                | 42568.6               |
| 260.000         | 1.35977              | 1.78657                | 2.74197                  | 1.49381            | 0.0                | 0.0                | 46195.1               |
| 270.000         | 1.34771              | 1.96456                | 2.74498                  | 1.43484            | 0.0                | 0.0                | 42520.5               |
| 280.000         | 1.33615              | 2.04776                | 2.77432                  | 1.47136            | 0.0                | 0.0                | 43471.8               |
| 290.000         | 1.32505              | 1.75190                | 2.77775                  | 1.47425            | 0.0                | 0.0                | 45426.1               |
| 300.000         | 1.31438              | 2.39224                | 2.77738                  | 1.48109            | 0.0                | 0.0                | 42715.2               |
| 310.000         | 1.30410              | 1.87374                | 2.78466                  | 1.49760            | 0.0                | 0.0                | 45181.4               |
| 320.000         | 1.29419              | 2.29387                | 2.79733                  | 1.50356            | 0.0                | 0.0                | 42665.8               |
| 330.000         | 1.28463              | 1.75907                | 2.78928                  | 1.49772            | 0.0                | 0.0                | 43131.4               |
| 340.000         | 1.27539              | 1.46232                | 2.76847                  | 1.46143            | 0.0                | 0.0                | 43537.0               |
| 350.000         | 1.26647              | 2.45847                | 2.78884                  | 1.47911            | 0.0                | 0.0                | 40311.0               |
| 360.000         | 1.25783              | 2.55294                | 2.76722                  | 1.51067            | 0.0                | 0.0                | 41411.5               |
| 370.000         | 1.24946              | 1.39747                | 2.76105                  | 1.50931            | 0.0                | 0.0                | 42040.9               |
| 380.000         | 1.24135              | 2.90837                | 2.75584                  | 1.51468            | 0.0                | 0.0                | 39404.1               |
| 390.000         | 1.23348              | 1.01908                | 2.76377                  | 1.49051            | 0.0                | 0.0                | 41447.6               |
| 400.000         | 1.22584              | 2.51261                | 2.76193                  | 1.47249            | 0.0                | 0.0                | 38695.5               |
| 410.000         | 1.21842              | 2.31441                | 2.75001                  | 1.53219            | 0.0                | 0.0                | 39343.8               |
| 420.000         | 1.21121              | 2.43051                | 2.73477                  | 1.53165            | 0.0                | 0.0                | 40547.2               |
| 430.000         | 1.20419              | 1.04214                | 2.72030                  | 1.50629            | 0.0                | 0.0                | 40730.0               |
| 440.000         | 1.19736              | 3.12032                | 2.70096                  | 1.51083            | 0.0                | 0.0                | 38875.9               |
| 450.000         | 1.19071              | 1.96570                | 2.68236                  | 1.53445            | 0.0                | 0.0                | 40063.7               |
| 460.000         | 1.18422              | 2.48170                | 2.66165                  | 1.51619            | 0.0                | 0.0                | 39424.6               |
| 470.000         | 1.17790              | 1.83941                | 2.65444                  | 1.54076            | 0.0                | 0.0                | 39718.7               |
| 480.000         | 1.17174              | 1.31158                | 2.65870                  | 1.41972            | 0.0                | 0.0                | 33161.7               |







## JAERI - M 85 - 210

## VOID FRACTION

| TIME     | VOID1         | VOID2     | VOID3    | VOID4    | VOID5    | VOID6    | MAXPOWER |
|----------|---------------|-----------|----------|----------|----------|----------|----------|
| ( SEC )  | ( - )         | ( - )     | ( - )    | ( - )    | ( - )    | ( - )    | ( KW/M ) |
| 0.0      | 0.999090      | 0.998655  | 0.998424 | 0.996725 | 0.994809 | 0.995550 | 2.08600  |
| 10.0000  | 0.330503      | 0.955601  | 0.963727 | 0.975090 | 1.00000  | 1.00000  | 1.98895  |
| 20.0000  | 0.914582E-01  | 0.791882  | 0.988366 | 0.989052 | 0.991060 | 0.993515 | 1.91494  |
| 30.0000  | 0.154999E-01  | 0.712957  | 0.934411 | 0.952859 | 0.966614 | 0.977318 | 1.85665  |
| 40.0000  | 0.0           | 0.622965  | 0.883602 | 0.917515 | 0.939730 | 0.955708 | 1.80883  |
| 50.0000  | 0.0           | 0.518333  | 0.839653 | 0.896643 | 0.929625 | 0.947600 | 1.76844  |
| 60.0000  | 0.0           | 0.437136  | 0.801243 | 0.889393 | 0.923837 | 0.941389 | 1.73359  |
| 70.0000  | 0.0           | 0.369351  | 0.783371 | 0.884878 | 0.917380 | 0.935759 | 1.70300  |
| 80.0000  | 0.0           | 0.333743  | 0.774261 | 0.893736 | 0.921933 | 0.936399 | 1.67581  |
| 90.0000  | 0.0           | 0.296940  | 0.757632 | 0.890227 | 0.923167 | 0.941022 | 1.65134  |
| 100.0000 | 0.0           | 0.269877  | 0.745112 | 0.887539 | 0.921497 | 0.940156 | 1.62919  |
| 110.0000 | 0.0           | 0.248900  | 0.733573 | 0.885276 | 0.919806 | 0.938617 | 1.60891  |
| 120.0000 | 0.0           | 0.231773  | 0.722704 | 0.880891 | 0.916541 | 0.935744 | 1.59026  |
| 130.0000 | 0.0           | 0.226714  | 0.709713 | 0.883843 | 0.921765 | 0.936573 | 1.58954  |
| 140.0000 | 0.0           | 0.231807  | 0.702013 | 0.880157 | 0.918641 | 0.936595 | 1.56443  |
| 150.0000 | 0.0           | 0.227780  | 0.684304 | 0.871650 | 0.911299 | 0.930469 | 1.54112  |
| 160.0000 | 0.0           | 0.228399  | 0.660855 | 0.871114 | 0.913818 | 0.930051 | 1.51939  |
| 170.0000 | 0.0           | 0.249440  | 0.647042 | 0.866941 | 0.913798 | 0.932809 | 1.49907  |
| 180.0000 | 0.0           | 0.273066  | 0.635687 | 0.867442 | 0.922573 | 0.937028 | 1.48000  |
| 190.0000 | 0.0           | 0.253505  | 0.619200 | 0.859819 | 0.916679 | 0.935385 | 1.46204  |
| 200.0000 | 0.0           | 0.259851  | 0.606580 | 0.865816 | 0.916253 | 0.935474 | 1.44508  |
| 210.0000 | 0.172496E-03  | 0.291820  | 0.603625 | 0.854279 | 0.905687 | 0.924394 | 1.42903  |
| 220.0000 | 0.208020E-03  | 0.290520  | 0.594106 | 0.845413 | 0.898703 | 0.917685 | 1.41380  |
| 230.0000 | 0.133132E-01  | 0.523153  | 0.595830 | 0.849316 | 0.913287 | 0.927810 | 1.39932  |
| 240.0000 | 0.239425E-01  | 0.3353852 | 0.595254 | 0.856614 | 0.933288 | 0.944097 | 1.38553  |
| 250.0000 | 0.187415E-01  | 0.327175  | 0.582688 | 0.845588 | 0.917989 | 0.935136 | 1.37236  |
| 260.0000 | 0.900269E-02  | 0.311112  | 0.567707 | 0.835963 | 0.904284 | 0.923059 | 1.35977  |
| 270.0000 | 0.318514E-01  | 0.339052  | 0.572847 | 0.834978 | 0.933615 | 0.935450 | 1.34771  |
| 280.0000 | 0.221606E-01  | 0.326924  | 0.559446 | 0.828414 | 0.918858 | 0.932126 | 1.33615  |
| 290.0000 | 0.292041E-01  | 0.332687  | 0.561935 | 0.818023 | 0.912820 | 0.928527 | 1.32505  |
| 300.0000 | 0.304276E-01  | 0.333313  | 0.560348 | 0.807796 | 0.910396 | 0.929706 | 1.31438  |
| 310.0000 | 0.314681E-01  | 0.333098  | 0.559098 | 0.797121 | 0.901414 | 0.922726 | 1.30410  |
| 320.0000 | 0.319126E-01  | 0.331409  | 0.556010 | 0.788238 | 0.905914 | 0.921659 | 1.29419  |
| 330.0000 | 0.438841E-01  | 0.340523  | 0.559786 | 0.780428 | 0.900511 | 0.919481 | 1.28463  |
| 340.0000 | 0.567454E-01  | 0.349812  | 0.565258 | 0.777621 | 0.921023 | 0.933745 | 1.27539  |
| 350.0000 | 0.561590E-01  | 0.346685  | 0.560604 | 0.767617 | 0.911747 | 0.932409 | 1.26647  |
| 360.0000 | 0.503923E-01  | 0.342372  | 0.557743 | 0.758300 | 0.896441 | 0.918248 | 1.25783  |
| 370.0000 | 0.562960E-01  | 0.346474  | 0.559433 | 0.751866 | 0.897168 | 0.914488 | 1.24946  |
| 380.0000 | 0.567308E-01  | 0.340001  | 0.555679 | 0.743369 | 0.899324 | 0.917821 | 1.24135  |
| 390.0000 | 0.633136E-01  | 0.349329  | 0.560055 | 0.740845 | 0.914752 | 0.928237 | 1.23348  |
| 400.0000 | 0.8133389E-01 | 0.357466  | 0.562476 | 0.736543 | 0.911590 | 0.936663 | 1.22584  |
| 410.0000 | 0.5978798E-01 | 0.344149  | 0.553394 | 0.724610 | 0.890258 | 0.915807 | 1.21842  |
| 420.0000 | 0.6964864E-01 | 0.349723  | 0.556180 | 0.721065 | 0.883458 | 0.909187 | 1.21121  |
| 430.0000 | 0.779483E-01  | 0.355364  | 0.560129 | 0.720530 | 0.901447 | 0.915254 | 1.20419  |
| 440.0000 | 0.830648E-01  | 0.354936  | 0.557458 | 0.716933 | 0.890903 | 0.919927 | 1.19736  |
| 450.0000 | 0.762450E-01  | 0.350958  | 0.556987 | 0.719225 | 0.888826 | 0.892261 | 1.19071  |
| 460.0000 | 0.926341E-01  | 0.358750  | 0.559420 | 0.718575 | 0.873202 | 0.911865 | 1.18422  |
| 470.0000 | 0.839286E-01  | 0.353544  | 0.555128 | 0.714057 | 0.863116 | 0.904389 | 1.17790  |
| 480.0000 | 0.106538      | 0.363129  | 0.561337 | 0.720398 | 0.921089 | 1.000000 | 1.17174  |

## MOVEMENT OF BOUNDARIES

| TIME     | LIQ.BOIL | QUENCHPT | SATURATE | TRA-DISP | REWETTED | LIQ. LEV | PRESHEAD     |
|----------|----------|----------|----------|----------|----------|----------|--------------|
| ( SEC )  | ( M )    | ( M )    | ( M )    | ( M )    | ( M )    | ( M )    | ( M )        |
| 0.0      | 0.0      | 0.0      | 3.66000  | 0.0      | 3.66000  | 0.0      | 0.102166E-01 |
| 10.0000  | 0.297866 | 0.336203 | 0.297866 | 0.370771 | 3.66000  | 3.66000  | 0.466525     |
| 20.0000  | 0.426777 | 0.519774 | 0.426777 | 0.988649 | 3.66000  | 0.988649 | 0.704347     |
| 30.0000  | 0.527369 | 0.588678 | 0.527369 | 0.675232 | 3.66000  | 3.66000  | 0.878486     |
| 40.0000  | 0.603304 | 0.675155 | 0.603304 | 0.694182 | 3.66000  | 3.66000  | 1.02528      |
| 50.0000  | 0.649228 | 0.742334 | 0.649228 | 0.795650 | 3.66000  | 3.66000  | 1.13974      |
| 60.0000  | 0.690321 | 0.803475 | 0.690321 | 0.852774 | 3.66000  | 3.66000  | 1.22442      |
| 70.0000  | 0.726067 | 0.869567 | 0.726067 | 0.870402 | 3.66000  | 3.66000  | 1.28475      |
| 80.0000  | 0.722833 | 0.930238 | 0.722833 | 0.932456 | 3.66000  | 3.66000  | 1.30543      |
| 90.0000  | 0.711033 | 0.980380 | 0.711033 | 0.980380 | 3.66000  | 3.66000  | 1.33659      |
| 100.0000 | 0.720355 | 1.02893  | 0.720355 | 1.02893  | 3.66000  | 3.66000  | 1.36392      |
| 110.0000 | 0.725228 | 1.07814  | 0.725228 | 1.07814  | 3.66000  | 3.66000  | 1.38711      |
| 120.0000 | 0.727990 | 1.12632  | 0.727990 | 1.12632  | 3.66000  | 3.66000  | 1.41061      |
| 130.0000 | 0.714894 | 1.16854  | 0.714894 | 1.16854  | 3.66000  | 3.66000  | 1.41613      |
| 140.0000 | 0.685642 | 1.21296  | 0.685642 | 1.21296  | 3.66000  | 3.66000  | 1.42189      |
| 150.0000 | 0.691151 | 1.25853  | 0.691151 | 1.25853  | 3.66000  | 3.66000  | 1.44852      |
| 160.0000 | 0.687574 | 1.30521  | 0.687574 | 1.30521  | 3.66000  | 3.66000  | 1.46119      |
| 170.0000 | 0.649453 | 1.34746  | 0.649453 | 1.34746  | 3.66000  | 3.66000  | 1.45798      |
| 180.0000 | 0.607601 | 1.38799  | 0.607601 | 1.38799  | 3.66000  | 3.66000  | 1.44226      |
| 190.0000 | 0.635359 | 1.42990  | 0.635359 | 1.42990  | 3.66000  | 3.66000  | 1.47458      |
| 200.0000 | 0.624301 | 1.47293  | 0.624301 | -3.62465 | 3.66000  | 3.62465  | 1.47387      |
| 210.0000 | 0.568652 | 1.51627  | 0.568652 | 1.51627  | 3.66000  | 3.66000  | 1.47560      |
| 220.0000 | 0.568801 | 1.55734  | 0.568801 | 1.55734  | 3.66000  | 3.66000  | 1.49710      |
| 230.0000 | 0.483419 | 1.59798  | 0.483419 | 1.59798  | 3.66000  | 3.66000  | 1.45015      |
| 240.0000 | 0.437197 | 1.63880  | 0.437197 | 1.63880  | 3.66000  | 3.66000  | 1.40968      |
| 250.0000 | 0.459856 | 1.67957  | 0.459856 | 1.67957  | 3.66000  | 3.66000  | 1.44734      |
| 260.0000 | 0.507572 | 1.72031  | 0.507572 | 1.72031  | 3.66000  | 3.66000  | 1.49381      |
| 270.0000 | 0.406624 | 1.76034  | 0.406624 | 1.76034  | 3.66000  | 3.66000  | 1.43484      |
| 280.0000 | 0.441978 | 1.80017  | 0.441978 | 1.80017  | 3.66000  | 3.66000  | 1.47136      |
| 290.0000 | 0.406669 | 1.84014  | 0.406669 | 1.84014  | 3.66000  | 3.66000  | 1.47425      |
| 300.0000 | 0.406680 | 1.87992  | 0.406680 | 1.87992  | 3.66000  | 3.66000  | 1.48109      |
| 310.0000 | 0.404566 | 1.91958  | 0.404566 | 1.91958  | 3.66000  | 3.66000  | 1.49780      |
| 320.0000 | 0.403131 | 1.96015  | 0.403131 | 1.96015  | 3.66000  | 3.66000  | 1.50356      |
| 330.0000 | 0.363570 | 2.00054  | 0.363570 | 2.00054  | 3.66000  | 3.66000  | 1.49772      |
| 340.0000 | 0.322771 | 2.04041  | 0.322771 | 2.04041  | 3.66000  | 3.66000  | 1.46143      |
| 350.0000 | 0.323265 | 2.07992  | 0.323265 | 2.07992  | 3.66000  | 3.66000  | 1.47791      |
| 360.0000 | 0.344572 | 2.11884  | 0.344572 | 2.11884  | 3.66000  | 3.66000  | 1.51047      |
| 370.0000 | 0.322792 | 2.15896  | 0.322792 | 2.15896  | 3.66000  | 3.66000  | 1.50931      |
| 380.0000 | 0.319748 | 2.19991  | 0.319748 | 2.19991  | 3.66000  | 3.66000  | 1.51468      |
| 390.0000 | 0.296531 | 2.24039  | 0.296531 | 2.24039  | 3.66000  | 3.66000  | 1.49051      |
| 400.0000 | 0.229774 | 2.28021  | 0.229774 | 2.28021  | 3.66000  | 3.66000  | 1.47249      |
| 410.0000 | 0.311057 | 2.31940  | 0.311057 | 2.31940  | 3.66000  | 3.66000  | 1.53219      |
| 420.0000 | 0.278113 | 2.36118  | 0.278113 | 2.36118  | 3.66000  | 3.66000  | 1.53165      |
| 430.0000 | 0.237797 | 2.40537  | 0.237797 | 2.40537  | 3.66000  | 3.66000  | 1.50629      |
| 440.0000 | 0.215141 | 2.44800  | 0.215141 | 2.44800  | 3.66000  | 3.66000  | 1.51083      |
| 450.0000 | 0.225467 | 2.48933  | 0.225467 | 2.48933  | 3.66000  | 3.66000  | 1.53445      |
| 460.0000 | 0.173184 | 2.53004  | 0.173184 | 2.53004  | 3        |          |              |

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## MASS BALANCE IN CORE

| TIME(S)   | GLOUT/G(1) | G(N1)/G(1) | MDOT/G(1) |
|-----------|------------|------------|-----------|
| 0.0       | 0.0        | 11.22730   | 1.00000   |
| 10.00000  | 2.40379    | 13.19746   | 0.52019   |
| 20.00000  | 0.0        | 12.10569   | 0.76694   |
| 30.00000  | 1.82382    | 12.76509   | 0.48009   |
| 40.00000  | 0.89384    | 13.10752   | 0.43882   |
| 50.00000  | 1.17749    | 13.45511   | 0.34047   |
| 60.00000  | 1.18839    | 13.79980   | 0.28033   |
| 70.00000  | 1.57634    | 13.53448   | 0.13876   |
| 80.00000  | 1.23414    | 13.81537   | 0.11303   |
| 90.00000  | 1.20748    | 13.77759   | 0.09969   |
| 100.00000 | 1.30730    | 13.80332   | 0.10860   |
| 110.00000 | 1.19429    | 13.80668   | 0.08854   |
| 120.00000 | 1.50389    | 13.58409   | 0.11316   |
| 130.00000 | 1.19288    | 13.61804   | -0.01855  |
| 140.00000 | 1.47638    | 13.48984   | 0.10422   |
| 150.00000 | 1.68472    | 13.41618   | 0.14941   |
| 160.00000 | 1.50564    | 13.62421   | -0.05791  |
| 170.00000 | 0.85856    | 13.49366   | 0.04580   |
| 180.00000 | 1.50623    | 13.39907   | 0.06941   |
| 190.00000 | 1.40933    | 13.49733   | -0.09012  |
| 200.00000 | 0.0        | 13.26860   | 0.35171   |
| 210.00000 | 2.14158    | 13.37549   | 0.08959   |
| 220.00000 | 1.80579    | 13.42572   | 0.06651   |
| 230.00000 | 2.28588    | 13.23077   | -0.36524  |
| 240.00000 | 0.99409    | 13.36114   | -0.22133  |
| 250.00000 | 2.44764    | 13.07439   | 0.18292   |
| 260.00000 | 1.42822    | 13.33631   | -0.09655  |
| 270.00000 | 1.07644    | 13.07092   | 0.13166   |
| 280.00000 | 1.57180    | 13.13963   | 0.05346   |
| 290.00000 | 2.03017    | 13.28077   | -0.24728  |
| 300.00000 | 1.57522    | 13.08498   | 0.19855   |
| 310.00000 | 1.62682    | 13.26310   | -0.07388  |
| 320.00000 | 1.97499    | 13.08142   | 0.09288   |
| 330.00000 | 1.18542    | 13.11504   | -0.00606  |
| 340.00000 | 1.22884    | 13.14434   | -0.23070  |
| 350.00000 | 2.12320    | 12.91135   | 0.15745   |
| 360.00000 | 1.95993    | 12.99083   | 0.20224   |
| 370.00000 | 1.40848    | 13.03629   | -0.30821  |
| 380.00000 | 3.04785    | 12.84585   | 0.16658   |
| 390.00000 | 1.52095    | 12.99344   | -0.82156  |
| 400.00000 | 1.67259    | 12.79467   | 0.26861   |
| 410.00000 | 2.15587    | 12.84149   | 0.11208   |
| 420.00000 | 2.46130    | 12.92841   | 0.08824   |
| 430.00000 | 2.00368    | 12.94161   | -0.95123  |
| 440.00000 | 2.94877    | 12.80770   | 0.24163   |
| 450.00000 | 4.14524    | 12.89349   | -0.47154  |
| 460.00000 | 2.38103    | 12.84733   | 0.13447   |
| 470.00000 | 2.95458    | 12.86857   | -0.30079  |
| 480.00000 | 0.90211    | 12.39501   | -0.03301  |

## TEMPERATURE FIELD OF FUEL ROD ( AXIAL NODE = 10 )

| TIME    | TF(R.1) | TF(R.2) | TF(R.3) | TF(R.4) |
|---------|---------|---------|---------|---------|
| ( SEC ) | ( DC )  | ( DC )  | ( DC )  | ( DC )  |
| 0.0     | 353.218 | 353.483 | 366.851 | 365.598 |
| 10.000  | 342.993 | 345.604 | 379.465 | 379.840 |
| 20.000  | 140.044 | 140.044 | 140.044 | 140.044 |
| 30.000  | 140.809 | 140.809 | 140.809 | 140.809 |
| 40.000  | 142.091 | 142.091 | 142.091 | 142.091 |
| 50.000  | 142.353 | 142.353 | 142.353 | 142.353 |
| 60.000  | 142.054 | 142.054 | 142.054 | 142.054 |
| 70.000  | 141.383 | 141.383 | 141.383 | 141.383 |
| 80.000  | 140.837 | 140.837 | 140.837 | 140.837 |
| 90.000  | 140.337 | 140.337 | 140.337 | 140.337 |
| 100.000 | 139.954 | 139.954 | 139.954 | 139.954 |
| 110.000 | 139.601 | 139.601 | 139.601 | 139.601 |
| 120.000 | 139.230 | 139.230 | 139.230 | 139.230 |
| 130.000 | 139.114 | 139.114 | 139.114 | 139.114 |
| 140.000 | 138.689 | 138.689 | 138.689 | 138.689 |
| 150.000 | 138.466 | 138.466 | 138.466 | 138.466 |
| 160.000 | 138.451 | 138.451 | 138.451 | 138.451 |
| 170.000 | 138.330 | 138.330 | 138.330 | 138.330 |
| 180.000 | 138.178 | 138.178 | 138.178 | 138.178 |
| 190.000 | 138.485 | 138.485 | 138.485 | 138.485 |
| 200.000 | 138.487 | 138.487 | 138.487 | 138.487 |
| 210.000 | 138.008 | 138.008 | 138.008 | 138.008 |
| 220.000 | 137.876 | 137.876 | 137.876 | 137.876 |
| 230.000 | 137.443 | 137.443 | 137.443 | 137.443 |
| 240.000 | 137.727 | 137.727 | 137.727 | 137.727 |
| 250.000 | 137.587 | 137.587 | 137.587 | 137.587 |
| 260.000 | 137.898 | 137.898 | 137.898 | 137.898 |
| 270.000 | 137.919 | 137.919 | 137.919 | 137.919 |
| 280.000 | 138.286 | 138.286 | 138.286 | 138.286 |
| 290.000 | 138.313 | 138.313 | 138.313 | 138.313 |
| 300.000 | 138.292 | 138.292 | 138.292 | 138.292 |
| 310.000 | 138.371 | 138.371 | 138.371 | 138.371 |
| 320.000 | 138.521 | 138.521 | 138.521 | 138.521 |
| 330.000 | 138.400 | 138.400 | 138.400 | 138.400 |
| 340.000 | 138.374 | 138.374 | 138.374 | 138.374 |
| 350.000 | 138.365 | 138.365 | 138.365 | 138.365 |
| 360.000 | 138.067 | 138.067 | 138.067 | 138.067 |
| 370.000 | 137.972 | 137.972 | 137.972 | 137.972 |
| 380.000 | 137.890 | 137.890 | 137.890 | 137.890 |
| 390.000 | 137.981 | 137.981 | 137.981 | 137.981 |
| 400.000 | 137.944 | 137.944 | 137.944 | 137.944 |
| 410.000 | 137.775 | 137.775 | 137.775 | 137.775 |
| 420.000 | 137.563 | 137.563 | 137.563 | 137.563 |
| 430.000 | 137.361 | 137.361 | 137.361 | 137.361 |
| 440.000 | 137.095 | 137.095 | 137.095 | 137.095 |
| 450.000 | 136.840 | 136.840 | 136.840 | 136.840 |
| 460.000 | 136.557 | 136.557 | 136.557 | 136.557 |
| 470.000 | 136.451 | 136.451 | 136.451 | 136.451 |
| 480.000 | 136.496 | 136.496 | 136.496 | 136.496 |

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| TEMPERATURE FIELD OF FUEL ROD |         | ( AXIAL NODE = 26 ) |         |         |  |
|-------------------------------|---------|---------------------|---------|---------|--|
| TIME                          | TF(R.1) | TF(R.2)             | TF(R.3) | TF(R.4) |  |
| ( SEC )                       | ( °C )  | ( °C )              | ( °C )  | ( °C )  |  |
| 0.0                           | 577.643 | 578.130             | 607.953 | 603.570 |  |
| 10.000                        | 589.376 | 591.143             | 637.666 | 635.746 |  |
| 20.000                        | 599.285 | 601.141             | 649.919 | 648.760 |  |
| 30.000                        | 601.574 | 603.733             | 656.138 | 655.712 |  |
| 40.000                        | 600.682 | 603.003             | 657.364 | 657.435 |  |
| 50.000                        | 587.210 | 590.229             | 652.504 | 653.746 |  |
| 60.000                        | 563.668 | 566.976             | 634.281 | 636.578 |  |
| 70.000                        | 537.830 | 541.328             | 610.304 | 612.974 |  |
| 80.000                        | 507.896 | 511.621             | 582.290 | 585.224 |  |
| 90.000                        | 471.242 | 475.592             | 549.295 | 552.545 |  |
| 100.000                       | 141.709 | 141.709             | 141.709 | 141.709 |  |
| 110.000                       | 141.352 | 141.352             | 141.352 | 141.352 |  |
| 120.000                       | 140.977 | 140.977             | 140.977 | 140.977 |  |
| 130.000                       | 140.860 | 140.860             | 140.860 | 140.860 |  |
| 140.000                       | 140.429 | 140.429             | 140.429 | 140.429 |  |
| 150.000                       | 140.200 | 140.200             | 140.200 | 140.200 |  |
| 160.000                       | 140.179 | 140.179             | 140.179 | 140.179 |  |
| 170.000                       | 140.052 | 140.052             | 140.052 | 140.052 |  |
| 180.000                       | 139.895 | 139.895             | 139.895 | 139.895 |  |
| 190.000                       | 140.196 | 140.196             | 140.196 | 140.196 |  |
| 200.000                       | 140.193 | 140.193             | 140.193 | 140.193 |  |
| 210.000                       | 139.710 | 139.710             | 139.710 | 139.710 |  |
| 220.000                       | 139.574 | 139.574             | 139.574 | 139.574 |  |
| 230.000                       | 139.138 | 139.138             | 139.138 | 139.138 |  |
| 240.000                       | 139.417 | 139.417             | 139.417 | 139.417 |  |
| 250.000                       | 139.273 | 139.273             | 139.273 | 139.273 |  |
| 260.000                       | 139.579 | 139.579             | 139.579 | 139.579 |  |
| 270.000                       | 139.596 | 139.596             | 139.596 | 139.596 |  |
| 280.000                       | 139.959 | 139.959             | 139.959 | 139.959 |  |
| 290.000                       | 139.983 | 139.983             | 139.983 | 139.983 |  |
| 300.000                       | 139.958 | 139.958             | 139.958 | 139.958 |  |
| 310.000                       | 140.033 | 140.033             | 140.033 | 140.033 |  |
| 320.000                       | 140.180 | 140.180             | 140.180 | 140.180 |  |
| 330.000                       | 140.056 | 140.056             | 140.056 | 140.056 |  |
| 340.000                       | 140.028 | 140.028             | 140.028 | 140.028 |  |
| 350.000                       | 140.015 | 140.015             | 140.015 | 140.015 |  |
| 360.000                       | 139.715 | 139.715             | 139.715 | 139.715 |  |
| 370.000                       | 139.617 | 139.617             | 139.617 | 139.617 |  |
| 380.000                       | 139.533 | 139.533             | 139.533 | 139.533 |  |
| 390.000                       | 139.621 | 139.621             | 139.621 | 139.621 |  |
| 400.000                       | 139.582 | 139.582             | 139.582 | 139.582 |  |
| 410.000                       | 139.411 | 139.411             | 139.411 | 139.411 |  |
| 420.000                       | 139.196 | 139.196             | 139.196 | 139.196 |  |
| 430.000                       | 138.992 | 138.992             | 138.992 | 138.992 |  |
| 440.000                       | 138.725 | 138.725             | 138.725 | 138.725 |  |
| 450.000                       | 138.468 | 138.468             | 138.468 | 138.468 |  |
| 460.000                       | 138.183 | 138.183             | 138.183 | 138.183 |  |
| 470.000                       | 138.075 | 138.075             | 138.075 | 138.075 |  |
| 480.000                       | 138.118 | 138.118             | 138.118 | 138.118 |  |
| TEMPERATURE FIELD OF FUEL ROD |         | ( AXIAL NODE = 46 ) |         |         |  |
| TIME                          | TF(R.1) | TF(R.2)             | TF(R.3) | TF(R.4) |  |
| ( SEC )                       | ( °C )  | ( °C )              | ( °C )  | ( °C )  |  |
| 0.0                           | 720.308 | 720.911             | 726.786 | 720.470 |  |
| 10.000                        | 746.272 | 750.013             | 760.387 | 757.834 |  |
| 20.000                        | 764.020 | 766.068             | 775.340 | 773.259 |  |
| 30.000                        | 773.771 | 776.109             | 785.935 | 784.673 |  |
| 40.000                        | 779.475 | 781.973             | 792.124 | 791.554 |  |
| 50.000                        | 779.130 | 781.887             | 792.613 | 792.863 |  |
| 60.000                        | 772.889 | 775.825             | 787.010 | 788.043 |  |
| 70.000                        | 765.642 | 748.516             | 779.476 | 780.434 |  |
| 80.000                        | 759.287 | 762.039             | 772.661 | 773.453 |  |
| 90.000                        | 752.498 | 755.521             | 765.993 | 766.875 |  |
| 100.000                       | 744.296 | 747.172             | 757.960 | 759.054 |  |
| 110.000                       | 735.091 | 737.992             | 748.850 | 750.152 |  |
| 120.000                       | 725.450 | 728.303             | 739.010 | 740.255 |  |
| 130.000                       | 715.554 | 718.441             | 729.233 | 730.519 |  |
| 140.000                       | 704.872 | 707.729             | 718.400 | 719.681 |  |
| 150.000                       | 693.870 | 696.723             | 707.330 | 708.627 |  |
| 160.000                       | 681.951 | 684.861             | 695.511 | 696.869 |  |
| 170.000                       | 669.415 | 672.355             | 682.970 | 684.360 |  |
| 180.000                       | 656.253 | 659.198             | 669.865 | 671.335 |  |
| 190.000                       | 642.698 | 645.543             | 656.267 | 657.735 |  |
| 200.000                       | 628.160 | 631.139             | 641.845 | 643.418 |  |
| 210.000                       | 612.970 | 615.972             | 626.720 | 628.373 |  |
| 220.000                       | 597.896 | 600.884             | 611.563 | 613.173 |  |
| 230.000                       | 581.468 | 584.492             | 595.262 | 596.955 |  |
| 240.000                       | 564.586 | 567.627             | 578.428 | 580.083 |  |
| 250.000                       | 546.916 | 550.012             | 560.936 | 562.607 |  |
| 260.000                       | 527.385 | 530.591             | 541.787 | 543.566 |  |
| 270.000                       | 504.949 | 508.324             | 519.943 | 521.895 |  |
| 280.000                       | 476.685 | 480.484             | 493.145 | 495.568 |  |
| 290.000                       | 440.600 | 140.600             | 140.600 | 140.600 |  |
| 300.000                       | 140.573 | 140.573             | 140.573 | 140.573 |  |
| 310.000                       | 140.648 | 140.648             | 140.648 | 140.648 |  |
| 320.000                       | 140.793 | 140.793             | 140.793 | 140.793 |  |
| 330.000                       | 140.668 | 140.668             | 140.668 | 140.668 |  |
| 340.000                       | 140.639 | 140.639             | 140.639 | 140.639 |  |
| 350.000                       | 140.625 | 140.625             | 140.625 | 140.625 |  |
| 360.000                       | 140.324 | 140.324             | 140.324 | 140.324 |  |
| 370.000                       | 140.225 | 140.225             | 140.225 | 140.225 |  |
| 380.000                       | 140.140 | 140.140             | 140.140 | 140.140 |  |
| 390.000                       | 140.227 | 140.227             | 140.227 | 140.227 |  |
| 400.000                       | 140.187 | 140.187             | 140.187 | 140.187 |  |
| 410.000                       | 140.015 | 140.015             | 140.015 | 140.015 |  |
| 420.000                       | 139.800 | 139.800             | 139.800 | 139.800 |  |
| 430.000                       | 139.595 | 139.595             | 139.595 | 139.595 |  |
| 440.000                       | 139.327 | 139.327             | 139.327 | 139.327 |  |
| 450.000                       | 139.069 | 139.069             | 139.069 | 139.069 |  |
| 460.000                       | 138.784 | 138.784             | 138.784 | 138.784 |  |
| 470.000                       | 138.675 | 138.675             | 138.675 | 138.675 |  |
| 480.000                       | 138.718 | 138.718             | 138.718 | 138.718 |  |

| TEMPERATURE FIELD OF FUEL ROD |         | ( AXIAL NODE = 61 ) |         |         |  |
|-------------------------------|---------|---------------------|---------|---------|--|
| TIME                          | TF(R.1) | TF(R.2)             | TF(R.3) | TF(R.4) |  |
| ( SEC )                       | ( DC )  | ( DC )              | ( DC )  | ( DC )  |  |
| 0.0                           | 625.444 | 625.977             | 659.538 | 654.369 |  |
| 10.000                        | 651.751 | 654.133             | 698.675 | 694.970 |  |
| 20.000                        | 672.065 | 673.671             | 722.298 | 719.844 |  |
| 30.000                        | 690.369 | 692.148             | 741.848 | 739.704 |  |
| 40.000                        | 698.048 | 700.069             | 753.984 | 752.792 |  |
| 50.000                        | 703.001 | 705.120             | 760.603 | 759.904 |  |
| 60.000                        | 706.354 | 708.511             | 764.584 | 764.181 |  |
| 70.000                        | 707.934 | 710.144             | 766.598 | 766.413 |  |
| 80.000                        | 709.889 | 712.035             | 767.620 | 767.482 |  |
| 90.000                        | 711.109 | 713.276             | 768.526 | 768.437 |  |
| 100.000                       | 711.253 | 713.430             | 768.648 | 768.678 |  |
| 110.000                       | 710.566 | 712.750             | 767.891 | 768.028 |  |
| 120.000                       | 708.803 | 711.018             | 766.327 | 766.591 |  |
| 130.000                       | 707.570 | 709.741             | 764.647 | 764.885 |  |
| 140.000                       | 705.712 | 707.912             | 762.599 | 762.911 |  |
| 150.000                       | 702.337 | 704.573             | 759.461 | 759.935 |  |
| 160.000                       | 698.620 | 700.833             | 755.273 | 755.822 |  |
| 170.000                       | 695.095 | 697.307             | 751.116 | 751.658 |  |
| 180.000                       | 692.590 | 694.737             | 747.202 | 747.638 |  |
| 190.000                       | 688.144 | 690.327             | 743.095 | 743.678 |  |
| 200.000                       | 683.158 | 685.317             | 738.004 | 738.683 |  |
| 210.000                       | 679.233 | 681.415             | 733.313 | 733.918 |  |
| 220.000                       | 672.580 | 674.825             | 727.416 | 728.218 |  |
| 230.000                       | 667.137 | 669.295             | 720.744 | 721.484 |  |
| 240.000                       | 663.966 | 666.008             | 715.529 | 716.057 |  |
| 250.000                       | 660.382 | 662.470             | 711.685 | 712.179 |  |
| 260.000                       | 652.886 | 655.102             | 706.029 | 706.849 |  |
| 270.000                       | 648.302 | 650.374             | 699.433 | 700.100 |  |
| 280.000                       | 642.447 | 644.584             | 693.777 | 694.470 |  |
| 290.000                       | 634.733 | 636.907             | 686.793 | 687.670 |  |
| 300.000                       | 627.871 | 630.021             | 679.253 | 680.101 |  |
| 310.000                       | 619.434 | 621.672             | 671.396 | 672.339 |  |
| 320.000                       | 612.420 | 614.582             | 663.287 | 664.153 |  |
| 330.000                       | 603.303 | 605.523             | 654.802 | 655.799 |  |
| 340.000                       | 594.438 | 596.675             | 645.628 | 646.608 |  |
| 350.000                       | 585.812 | 588.010             | 636.372 | 637.335 |  |
| 360.000                       | 575.672 | 577.945             | 626.869 | 627.945 |  |
| 370.000                       | 564.075 | 566.421             | 615.913 | 617.114 |  |
| 380.000                       | 551.885 | 554.272             | 603.984 | 605.246 |  |
| 390.000                       | 538.144 | 540.587             | 590.808 | 592.175 |  |
| 400.000                       | 524.318 | 526.795             | 576.938 | 578.301 |  |
| 410.000                       | 508.382 | 510.961             | 561.910 | 563.375 |  |
| 420.000                       | 489.937 | 492.658             | 544.825 | 546.434 |  |
| 430.000                       | 465.992 | 469.042             | 524.306 | 526.252 |  |
| 440.000                       | 138.997 | 138.997             | 138.997 | 138.997 |  |
| 450.000                       | 138.739 | 138.739             | 138.739 | 138.739 |  |
| 460.000                       | 138.454 | 138.454             | 138.454 | 138.454 |  |
| 470.000                       | 138.346 | 138.346             | 138.346 | 138.346 |  |
| 480.000                       | 138.389 | 138.389             | 138.389 | 138.389 |  |
| TEMPERATURE FIELD OF FUEL ROD |         | ( AXIAL NODE = 76 ) |         |         |  |
| TIME                          | TF(R.1) | TF(R.2)             | TF(R.3) | TF(R.4) |  |
| ( SEC )                       | ( DC )  | ( DC )              | ( DC )  | ( DC )  |  |
| 0.0                           | 446.371 | 446.731             | 466.626 | 464.360 |  |
| 10.000                        | 467.189 | 468.358             | 493.145 | 491.417 |  |
| 20.000                        | 482.780 | 483.788             | 511.450 | 510.203 |  |
| 30.000                        | 498.286 | 499.355             | 527.181 | 526.011 |  |
| 40.000                        | 505.042 | 506.343             | 537.363 | 536.693 |  |
| 50.000                        | 510.917 | 512.242             | 543.703 | 543.177 |  |
| 60.000                        | 515.514 | 516.846             | 548.709 | 548.333 |  |
| 70.000                        | 518.798 | 520.179             | 552.284 | 551.993 |  |
| 80.000                        | 523.310 | 524.603             | 555.669 | 555.338 |  |
| 90.000                        | 526.977 | 528.304             | 559.249 | 558.931 |  |
| 100.000                       | 529.675 | 531.006             | 562.132 | 561.901 |  |
| 110.000                       | 531.828 | 533.153             | 564.242 | 564.065 |  |
| 120.000                       | 532.531 | 533.913             | 565.579 | 565.519 |  |
| 130.000                       | 534.342 | 535.666             | 566.746 | 566.625 |  |
| 140.000                       | 534.973 | 536.346             | 567.607 | 567.553 |  |
| 150.000                       | 533.864 | 535.282             | 567.174 | 567.272 |  |
| 160.000                       | 533.690 | 535.051             | 568.192 | 566.265 |  |
| 170.000                       | 533.141 | 534.528             | 565.572 | 565.654 |  |
| 180.000                       | 532.781 | 534.150             | 564.782 | 564.869 |  |
| 190.000                       | 531.144 | 532.494             | 563.065 | 563.219 |  |
| 200.000                       | 528.787 | 530.213             | 561.044 | 561.260 |  |
| 210.000                       | 525.934 | 527.357             | 558.306 | 558.580 |  |
| 220.000                       | 522.448 | 523.879             | 554.905 | 555.232 |  |
| 230.000                       | 520.155 | 521.556             | 551.676 | 551.926 |  |
| 240.000                       | 519.321 | 520.594             | 549.430 | 549.577 |  |
| 250.000                       | 516.614 | 517.990             | 547.543 | 547.774 |  |
| 260.000                       | 512.830 | 514.221             | 544.117 | 544.443 |  |
| 270.000                       | 510.548 | 511.896             | 540.888 | 541.123 |  |
| 280.000                       | 507.512 | 508.881             | 538.024 | 538.303 |  |
| 290.000                       | 504.007 | 505.358             | 534.438 | 534.756 |  |
| 300.000                       | 500.700 | 502.075             | 530.993 | 531.297 |  |
| 310.000                       | 496.487 | 497.865             | 526.971 | 527.334 |  |
| 320.000                       | 492.402 | 493.795             | 522.728 | 523.088 |  |
| 330.000                       | 488.037 | 489.428             | 518.242 | 518.614 |  |
| 340.000                       | 485.001 | 486.309             | 514.135 | 514.429 |  |
| 350.000                       | 482.076 | 483.403             | 510.989 | 511.256 |  |
| 360.000                       | 477.346 | 478.729             | 506.964 | 507.330 |  |
| 370.000                       | 472.394 | 473.781             | 502.020 | 502.418 |  |
| 380.000                       | 468.965 | 470.307             | 497.649 | 497.959 |  |
| 390.000                       | 464.521 | 465.824             | 493.140 | 493.497 |  |
| 400.000                       | 462.584 | 463.868             | 489.930 | 490.141 |  |
| 410.000                       | 458.119 | 459.479             | 486.539 | 486.865 |  |
| 420.000                       | 452.297 | 453.698             | 481.367 | 481.794 |  |
| 430.000                       | 446.989 | 448.356             | 475.651 | 476.063 |  |
| 440.000                       | 443.781 | 445.094             | 471.227 | 471.519 |  |
| 450.000                       | 438.181 | 439.561             | 466.523 | 466.925 |  |
| 460.000                       | 433.963 | 435.307             | 461.541 | 461.879 |  |
| 470.000                       | 428.417 | 429.808             | 456.452 | 456.848 |  |
| 480.000                       | 435.212 | 435.835             | 454.110 | 453.674 |  |

| TEMPERATURE FIELD OF FUEL ROD |          | < AXIAL NODE = 10 > |          |          |  |
|-------------------------------|----------|---------------------|----------|----------|--|
| TIME                          | TFP(R.1) | TFP(R.2)            | TFP(R.3) | TFP(R.4) |  |
| ( SEC )                       | ( DC )   | ( DC )              | ( DC )   | ( DC )   |  |
| 0.0                           | 375.052  | 375.340             | 390.175  | 388.486  |  |
| 10.000                        | 368.015  | 370.448             | 404.930  | 405.116  |  |
| 20.000                        | 140.266  | 140.266             | 140.266  | 140.266  |  |
| 30.000                        | 141.028  | 141.028             | 141.028  | 141.028  |  |
| 40.000                        | 142.309  | 142.309             | 142.309  | 142.309  |  |
| 50.000                        | 142.569  | 142.569             | 142.569  | 142.569  |  |
| 60.000                        | 142.270  | 142.270             | 142.270  | 142.270  |  |
| 70.000                        | 141.597  | 141.597             | 141.597  | 141.597  |  |
| 80.000                        | 141.051  | 141.051             | 141.051  | 141.051  |  |
| 90.000                        | 140.550  | 140.550             | 140.550  | 140.550  |  |
| 100.000                       | 140.166  | 140.166             | 140.166  | 140.166  |  |
| 110.000                       | 139.813  | 139.813             | 139.813  | 139.813  |  |
| 120.000                       | 139.442  | 139.442             | 139.442  | 139.442  |  |
| 130.000                       | 139.325  | 139.325             | 139.325  | 139.325  |  |
| 140.000                       | 138.900  | 138.900             | 138.900  | 138.900  |  |
| 150.000                       | 138.676  | 138.676             | 138.676  | 138.676  |  |
| 160.000                       | 138.660  | 138.660             | 138.660  | 138.660  |  |
| 170.000                       | 138.539  | 138.539             | 138.539  | 138.539  |  |
| 180.000                       | 138.386  | 138.386             | 138.386  | 138.386  |  |
| 190.000                       | 138.692  | 138.692             | 138.692  | 138.692  |  |
| 200.000                       | 138.693  | 138.693             | 138.693  | 138.693  |  |
| 210.000                       | 138.214  | 138.214             | 138.214  | 138.214  |  |
| 220.000                       | 138.082  | 138.082             | 138.082  | 138.082  |  |
| 230.000                       | 137.648  | 137.648             | 137.648  | 137.648  |  |
| 240.000                       | 137.931  | 137.931             | 137.931  | 137.931  |  |
| 250.000                       | 137.792  | 137.792             | 137.792  | 137.792  |  |
| 260.000                       | 138.101  | 138.101             | 138.101  | 138.101  |  |
| 270.000                       | 138.122  | 138.122             | 138.122  | 138.122  |  |
| 280.000                       | 138.488  | 138.488             | 138.488  | 138.488  |  |
| 290.000                       | 138.515  | 138.515             | 138.515  | 138.515  |  |
| 300.000                       | 138.493  | 138.493             | 138.493  | 138.493  |  |
| 310.000                       | 138.572  | 138.572             | 138.572  | 138.572  |  |
| 320.000                       | 138.722  | 138.722             | 138.722  | 138.722  |  |
| 330.000                       | 138.600  | 138.600             | 138.600  | 138.600  |  |
| 340.000                       | 138.574  | 138.574             | 138.574  | 138.574  |  |
| 350.000                       | 138.564  | 138.564             | 138.564  | 138.564  |  |
| 360.000                       | 138.266  | 138.266             | 138.266  | 138.266  |  |
| 370.000                       | 138.171  | 138.171             | 138.171  | 138.171  |  |
| 380.000                       | 138.089  | 138.089             | 138.089  | 138.089  |  |
| 390.000                       | 138.180  | 138.180             | 138.180  | 138.180  |  |
| 400.000                       | 138.142  | 138.142             | 138.142  | 138.142  |  |
| 410.000                       | 137.973  | 137.973             | 137.973  | 137.973  |  |
| 420.000                       | 137.761  | 137.761             | 137.761  | 137.761  |  |
| 430.000                       | 137.558  | 137.558             | 137.558  | 137.558  |  |
| 440.000                       | 137.293  | 137.293             | 137.293  | 137.293  |  |
| 450.000                       | 137.037  | 137.037             | 137.037  | 137.037  |  |
| 460.000                       | 136.753  | 136.753             | 136.753  | 136.753  |  |
| 470.000                       | 136.648  | 136.648             | 136.648  | 136.648  |  |
| 480.000                       | 136.693  | 136.693             | 136.693  | 136.693  |  |
| TEMPERATURE FIELD OF FUEL ROD |          | < AXIAL NODE = 26 > |          |          |  |
| TIME                          | TFP(R.1) | TFP(R.2)            | TFP(R.3) | TFP(R.4) |  |
| ( SEC )                       | ( DC )   | ( DC )              | ( DC )   | ( DC )   |  |
| 0.0                           | 619.087  | 619.614             | 652.669  | 647.610  |  |
| 10.000                        | 630.117  | 632.087             | 684.421  | 682.283  |  |
| 20.000                        | 640.378  | 642.409             | 696.842  | 695.554  |  |
| 30.000                        | 641.152  | 643.551             | 702.578  | 702.221  |  |
| 40.000                        | 639.756  | 642.292             | 702.976  | 703.130  |  |
| 50.000                        | 626.601  | 629.789             | 697.785  | 699.081  |  |
| 60.000                        | 603.154  | 606.618             | 679.725  | 682.158  |  |
| 70.000                        | 578.663  | 582.061             | 656.241  | 658.997  |  |
| 80.000                        | 551.541  | 555.275             | 629.958  | 632.889  |  |
| 90.000                        | 520.403  | 524.356             | 600.457  | 603.664  |  |
| 100.000                       | 480.253  | 484.862             | 566.053  | 569.718  |  |
| 110.000                       | 141.606  | 141.606             | 141.606  | 141.606  |  |
| 120.000                       | 141.230  | 141.230             | 141.230  | 141.230  |  |
| 130.000                       | 141.114  | 141.114             | 141.114  | 141.114  |  |
| 140.000                       | 140.682  | 140.682             | 140.682  | 140.682  |  |
| 150.000                       | 140.452  | 140.452             | 140.452  | 140.452  |  |
| 160.000                       | 140.430  | 140.430             | 140.430  | 140.430  |  |
| 170.000                       | 140.302  | 140.302             | 140.302  | 140.302  |  |
| 180.000                       | 140.144  | 140.144             | 140.144  | 140.144  |  |
| 190.000                       | 140.445  | 140.445             | 140.445  | 140.445  |  |
| 200.000                       | 140.441  | 140.441             | 140.441  | 140.441  |  |
| 210.000                       | 139.957  | 139.957             | 139.957  | 139.957  |  |
| 220.000                       | 139.821  | 139.821             | 139.821  | 139.821  |  |
| 230.000                       | 139.384  | 139.384             | 139.384  | 139.384  |  |
| 240.000                       | 139.662  | 139.662             | 139.662  | 139.662  |  |
| 250.000                       | 139.518  | 139.518             | 139.518  | 139.518  |  |
| 260.000                       | 139.823  | 139.823             | 139.823  | 139.823  |  |
| 270.000                       | 139.840  | 139.840             | 139.840  | 139.840  |  |
| 280.000                       | 140.202  | 140.202             | 140.202  | 140.202  |  |
| 290.000                       | 140.225  | 140.225             | 140.225  | 140.225  |  |
| 300.000                       | 140.200  | 140.200             | 140.200  | 140.200  |  |
| 310.000                       | 140.275  | 140.275             | 140.275  | 140.275  |  |
| 320.000                       | 140.421  | 140.421             | 140.421  | 140.421  |  |
| 330.000                       | 140.297  | 140.297             | 140.297  | 140.297  |  |
| 340.000                       | 140.268  | 140.268             | 140.268  | 140.268  |  |
| 350.000                       | 140.255  | 140.255             | 140.255  | 140.255  |  |
| 360.000                       | 139.954  | 139.954             | 139.954  | 139.954  |  |
| 370.000                       | 139.856  | 139.856             | 139.856  | 139.856  |  |
| 380.000                       | 139.772  | 139.772             | 139.772  | 139.772  |  |
| 390.000                       | 139.859  | 139.859             | 139.859  | 139.859  |  |
| 400.000                       | 139.820  | 139.820             | 139.820  | 139.820  |  |
| 410.000                       | 139.648  | 139.648             | 139.648  | 139.648  |  |
| 420.000                       | 139.434  | 139.434             | 139.434  | 139.434  |  |
| 430.000                       | 139.229  | 139.229             | 139.229  | 139.229  |  |
| 440.000                       | 138.962  | 138.962             | 138.962  | 138.962  |  |
| 450.000                       | 138.704  | 138.704             | 138.704  | 138.704  |  |
| 460.000                       | 138.419  | 138.419             | 138.419  | 138.419  |  |
| 470.000                       | 138.311  | 138.311             | 138.311  | 138.311  |  |
| 480.000                       | 138.354  | 138.354             | 138.354  | 138.354  |  |

| TEMPERATURE FIELD OF FUEL ROD |          | ( AXIAL NODE = 46 ) |          |          |  |
|-------------------------------|----------|---------------------|----------|----------|--|
| TIME                          | TFP(R.1) | TFP(R.2)            | TFP(R.3) | TFP(R.4) |  |
| ( SEC )                       | ( DC )   | ( DC )              | ( DC )   | ( DC )   |  |
| 0.0                           | 772.306  | 772.963             | 779.384  | 772.030  |  |
| 10.000                        | 797.395  | 801.545             | 813.134  | 810.483  |  |
| 20.000                        | 814.870  | 817.140             | 827.422  | 825.189  |  |
| 30.000                        | 823.632  | 826.202             | 837.090  | 835.808  |  |
| 40.000                        | 829.193  | 831.894             | 845.041  | 842.442  |  |
| 50.000                        | 828.643  | 831.614             | 843.353  | 843.657  |  |
| 60.000                        | 821.807  | 824.970             | 837.187  | 838.381  |  |
| 70.000                        | 814.049  | 817.143             | 829.080  | 830.171  |  |
| 80.000                        | 807.380  | 810.345             | 821.897  | 822.789  |  |
| 90.000                        | 800.205  | 803.251             | 814.848  | 815.851  |  |
| 100.000                       | 791.567  | 794.668             | 806.367  | 807.604  |  |
| 110.000                       | 781.898  | 785.023             | 796.784  | 798.257  |  |
| 120.000                       | 771.839  | 774.911             | 786.505  | 787.908  |  |
| 130.000                       | 761.497  | 764.606             | 776.293  | 777.743  |  |
| 140.000                       | 750.384  | 753.457             | 765.002  | 766.434  |  |
| 150.000                       | 739.026  | 742.090             | 753.555  | 754.995  |  |
| 160.000                       | 726.809  | 729.926             | 741.417  | 742.908  |  |
| 170.000                       | 714.012  | 717.138             | 728.606  | 730.127  |  |
| 180.000                       | 700.560  | 703.710             | 715.203  | 716.809  |  |
| 190.000                       | 686.806  | 689.947             | 701.374  | 702.960  |  |
| 200.000                       | 672.206  | 675.372             | 686.855  | 688.536  |  |
| 210.000                       | 657.129  | 660.307             | 671.801  | 673.545  |  |
| 220.000                       | 642.360  | 645.514             | 656.911  | 658.590  |  |
| 230.000                       | 626.441  | 629.613             | 641.047  | 642.802  |  |
| 240.000                       | 610.456  | 613.616             | 624.992  | 626.702  |  |
| 250.000                       | 594.230  | 597.410             | 608.796  | 610.508  |  |
| 260.000                       | 576.954  | 580.192             | 591.710  | 593.484  |  |
| 270.000                       | 558.306  | 561.611             | 573.296  | 575.114  |  |
| 280.000                       | 537.790  | 541.214             | 553.191  | 555.117  |  |
| 290.000                       | 512.746  | 516.555             | 529.491  | 531.906  |  |
| 300.000                       | 477.886  | 482.250             | 496.571  | 499.596  |  |
| 310.000                       | 440.904  | 440.904             | 440.904  | 440.904  |  |
| 320.000                       | 414.049  | 414.049             | 414.049  | 414.049  |  |
| 330.000                       | 400.923  | 400.923             | 400.923  | 400.923  |  |
| 340.000                       | 400.893  | 400.893             | 400.893  | 400.893  |  |
| 350.000                       | 400.879  | 400.879             | 400.879  | 400.879  |  |
| 360.000                       | 400.578  | 400.578             | 400.578  | 400.578  |  |
| 370.000                       | 400.479  | 400.479             | 400.479  | 400.479  |  |
| 380.000                       | 400.393  | 400.393             | 400.393  | 400.393  |  |
| 390.000                       | 400.480  | 400.480             | 400.480  | 400.480  |  |
| 400.000                       | 400.439  | 400.439             | 400.439  | 400.439  |  |
| 410.000                       | 400.267  | 400.267             | 400.267  | 400.267  |  |
| 420.000                       | 400.052  | 400.052             | 400.052  | 400.052  |  |
| 430.000                       | 399.847  | 399.847             | 399.847  | 399.847  |  |
| 440.000                       | 399.578  | 399.578             | 399.578  | 399.578  |  |
| 450.000                       | 399.320  | 399.320             | 399.320  | 399.320  |  |
| 460.000                       | 399.034  | 399.034             | 399.034  | 399.034  |  |
| 470.000                       | 388.926  | 388.926             | 388.926  | 388.926  |  |
| 480.000                       | 388.967  | 388.967             | 388.967  | 388.967  |  |
| TEMPERATURE FIELD OF FUEL ROD |          | ( AXIAL NODE = 61 ) |          |          |  |
| TIME                          | TFP(R.1) | TFP(R.2)            | TFP(R.3) | TFP(R.4) |  |
| ( SEC )                       | ( DC )   | ( DC )              | ( DC )   | ( DC )   |  |
| 0.0                           | 670.762  | 671.341             | 708.602  | 702.596  |  |
| 10.000                        | 694.813  | 697.592             | 749.255  | 745.240  |  |
| 20.000                        | 715.412  | 717.215             | 772.420  | 769.771  |  |
| 30.000                        | 732.944  | 734.932             | 791.348  | 789.071  |  |
| 40.000                        | 741.406  | 743.598             | 803.628  | 802.274  |  |
| 50.000                        | 746.975  | 749.266             | 810.794  | 809.962  |  |
| 60.000                        | 750.657  | 752.990             | 815.181  | 814.697  |  |
| 70.000                        | 752.462  | 754.851             | 817.443  | 817.214  |  |
| 80.000                        | 754.656  | 756.977             | 818.628  | 818.459  |  |
| 90.000                        | 756.049  | 758.392             | 819.471  | 819.559  |  |
| 100.000                       | 756.288  | 758.642             | 819.869  | 819.893  |  |
| 110.000                       | 755.628  | 757.990             | 819.131  | 819.278  |  |
| 120.000                       | 753.846  | 756.240             | 817.540  | 817.830  |  |
| 130.000                       | 752.582  | 754.929             | 815.829  | 816.096  |  |
| 140.000                       | 750.715  | 753.091             | 813.714  | 814.060  |  |
| 150.000                       | 747.217  | 749.632             | 810.460  | 810.992  |  |
| 160.000                       | 743.379  | 745.767             | 806.085  | 806.705  |  |
| 170.000                       | 739.787  | 742.174             | 801.768  | 802.377  |  |
| 180.000                       | 737.284  | 739.600             | 797.715  | 798.202  |  |
| 190.000                       | 732.696  | 735.048             | 793.458  | 794.112  |  |
| 200.000                       | 727.563  | 729.892             | 788.186  | 788.947  |  |
| 210.000                       | 723.537  | 725.887             | 783.315  | 783.993  |  |
| 220.000                       | 716.649  | 719.065             | 777.201  | 778.100  |  |
| 230.000                       | 711.142  | 713.465             | 770.311  | 771.133  |  |
| 240.000                       | 708.154  | 710.345             | 765.021  | 765.593  |  |
| 250.000                       | 704.474  | 706.725             | 761.162  | 761.705  |  |
| 260.000                       | 696.778  | 699.154             | 755.337  | 756.242  |  |
| 270.000                       | 692.346  | 694.571             | 748.676  | 749.395  |  |
| 280.000                       | 686.468  | 688.779             | 743.014  | 743.766  |  |
| 290.000                       | 678.749  | 681.072             | 735.978  | 736.929  |  |
| 300.000                       | 671.934  | 674.236             | 728.425  | 729.341  |  |
| 310.000                       | 663.481  | 665.868             | 720.532  | 721.551  |  |
| 320.000                       | 656.609  | 658.916             | 712.448  | 713.375  |  |
| 330.000                       | 647.604  | 649.966             | 704.019  | 705.081  |  |
| 340.000                       | 639.031  | 641.400             | 694.993  | 696.025  |  |
| 350.000                       | 630.696  | 633.024             | 685.974  | 686.984  |  |
| 360.000                       | 620.859  | 623.254             | 676.708  | 677.832  |  |
| 370.000                       | 609.755  | 612.210             | 666.108  | 667.351  |  |
| 380.000                       | 598.449  | 600.923             | 654.797  | 656.069  |  |
| 390.000                       | 585.841  | 588.553             | 642.538  | 643.910  |  |
| 400.000                       | 573.601  | 576.123             | 629.931  | 631.286  |  |
| 410.000                       | 559.879  | 562.466             | 616.659  | 618.102  |  |
| 420.000                       | 545.054  | 547.696             | 602.193  | 603.722  |  |
| 430.000                       | 529.046  | 531.752             | 586.666  | 588.261  |  |
| 440.000                       | 510.501  | 513.483             | 570.064  | 571.771  |  |
| 450.000                       | 483.429  | 486.692             | 547.259  | 549.524  |  |
| 460.000                       | 462.758  | 467.156             | 516.847  | 519.952  |  |
| 470.000                       | 438.588  | 438.588             | 438.588  | 438.588  |  |
| 480.000                       | 438.631  | 438.631             | 438.631  | 438.631  |  |

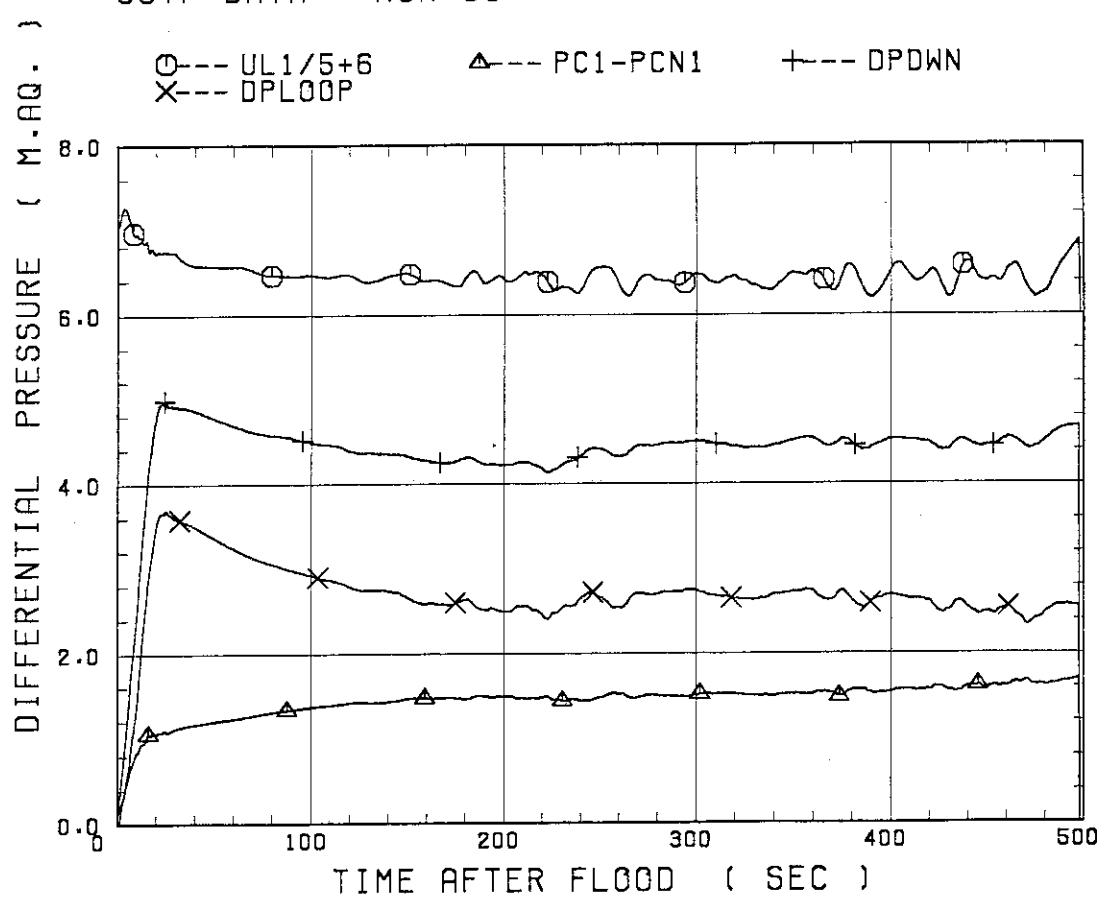
| TEMPERATURE FIELD OF FUEL ROD |          | < AXIAL NODE = 76 > |          |          |  |
|-------------------------------|----------|---------------------|----------|----------|--|
| TIME                          | TFP(R.1) | TFP(R.2)            | TFP(R.3) | TFP(R.4) |  |
| ( SEC )                       | ( DC )   | ( DC )              | ( DC )   | ( DC )   |  |
| 0.0                           | 476.489  | 476.878             | 499.039  | 496.385  |  |
| 10.000                        | 496.157  | 497.612             | 526.735  | 524.860  |  |
| 20.000                        | 512.231  | 513.366             | 544.829  | 543.466  |  |
| 30.000                        | 527.414  | 528.623             | 560.288  | 559.021  |  |
| 40.000                        | 534.903  | 536.290             | 570.713  | 569.936  |  |
| 50.000                        | 541.633  | 543.058             | 577.740  | 577.090  |  |
| 60.000                        | 546.868  | 548.298             | 583.424  | 582.953  |  |
| 70.000                        | 550.877  | 552.161             | 587.558  | 587.185  |  |
| 80.000                        | 555.839  | 557.227             | 591.486  | 591.066  |  |
| 90.000                        | 560.037  | 561.463             | 595.605  | 595.202  |  |
| 100.000                       | 563.174  | 564.604             | 598.953  | 598.654  |  |
| 110.000                       | 565.707  | 567.131             | 601.452  | 601.219  |  |
| 120.000                       | 566.653  | 568.137             | 603.105  | 603.011  |  |
| 130.000                       | 568.789  | 570.213             | 604.556  | 604.395  |  |
| 140.000                       | 569.640  | 571.117             | 605.457  | 605.373  |  |
| 150.000                       | 568.578  | 570.104             | 605.353  | 605.453  |  |
| 160.000                       | 568.575  | 570.038             | 604.451  | 604.521  |  |
| 170.000                       | 568.150  | 569.642             | 603.949  | 604.029  |  |
| 180.000                       | 567.910  | 569.382             | 603.249  | 603.338  |  |
| 190.000                       | 566.266  | 567.717             | 601.513  | 601.684  |  |
| 200.000                       | 563.857  | 565.395             | 599.470  | 599.712  |  |
| 210.000                       | 560.924  | 562.454             | 596.654  | 596.966  |  |
| 220.000                       | 557.313  | 558.851             | 593.129  | 593.505  |  |
| 230.000                       | 555.021  | 556.530             | 589.804  | 590.087  |  |
| 240.000                       | 554.331  | 555.698             | 587.544  | 587.704  |  |
| 250.000                       | 551.360  | 552.848             | 585.599  | 585.870  |  |
| 260.000                       | 547.417  | 548.911             | 581.940  | 582.317  |  |
| 270.000                       | 545.151  | 546.604             | 578.638  | 578.900  |  |
| 280.000                       | 542.032  | 543.503             | 575.698  | 576.016  |  |
| 290.000                       | 538.475  | 539.923             | 572.000  | 572.360  |  |
| 300.000                       | 535.094  | 536.573             | 568.493  | 568.835  |  |
| 310.000                       | 530.742  | 532.220             | 564.326  | 564.739  |  |
| 320.000                       | 526.572  | 528.066             | 559.966  | 560.371  |  |
| 330.000                       | 522.092  | 523.584             | 555.354  | 555.771  |  |
| 340.000                       | 519.102  | 520.500             | 551.168  | 551.495  |  |
| 350.000                       | 516.037  | 517.469             | 547.997  | 548.302  |  |
| 360.000                       | 511.087  | 512.572             | 543.772  | 544.188  |  |
| 370.000                       | 506.019  | 507.503             | 538.678  | 539.123  |  |
| 380.000                       | 502.437  | 503.884             | 534.224  | 534.580  |  |
| 390.000                       | 498.021  | 499.409             | 529.566  | 529.957  |  |
| 400.000                       | 496.040  | 497.403             | 526.387  | 526.624  |  |
| 410.000                       | 491.296  | 492.753             | 522.790  | 523.162  |  |
| 420.000                       | 485.457  | 486.950             | 517.516  | 517.983  |  |
| 430.000                       | 480.135  | 481.587             | 511.746  | 512.198  |  |
| 440.000                       | 476.937  | 478.346             | 507.355  | 507.677  |  |
| 450.000                       | 471.347  | 472.807             | 502.575  | 503.011  |  |
| 460.000                       | 467.156  | 468.588             | 497.608  | 497.974  |  |
| 470.000                       | 461.643  | 463.117             | 492.518  | 492.945  |  |
| 480.000                       | 467.656  | 468.436             | 489.983  | 489.591  |  |

\*\*\*\*\* CPOINT START NPRINT= 961 \*\*\*\*\*

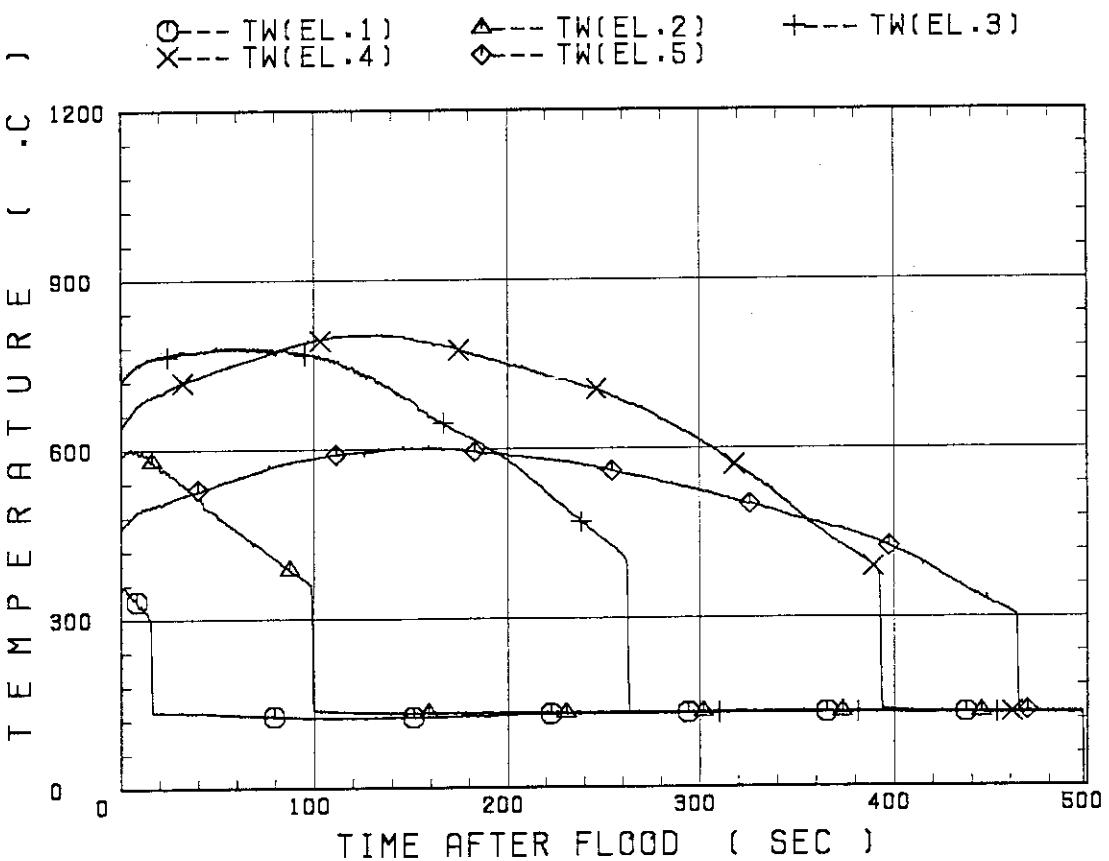
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TE18Z11
TE18Z12
TE18Z13
TE18Z14
TE18Z15
TE17Y11
TE17Y12
TE17Y13
TE17Y14
TE17Y15
ITAG = TE17Y13 IELV = 3 ELV = 1.8300
ITAG = TE17Y14 IELV = 4 ELV = 2.4400
ITAG = TE18Z13 IELV = 3 ELV = 1.8300
ITAG = TE18Z14 IELV = 4 ELV = 2.4400
ITAG = TE17Y11 IELV = 1 ELV = 0.3800
ITAG = TE17Y12 IELV = 2 ELV = 1.0150
ITAG = TE17Y15 IELV = 5 ELV = 3.0500
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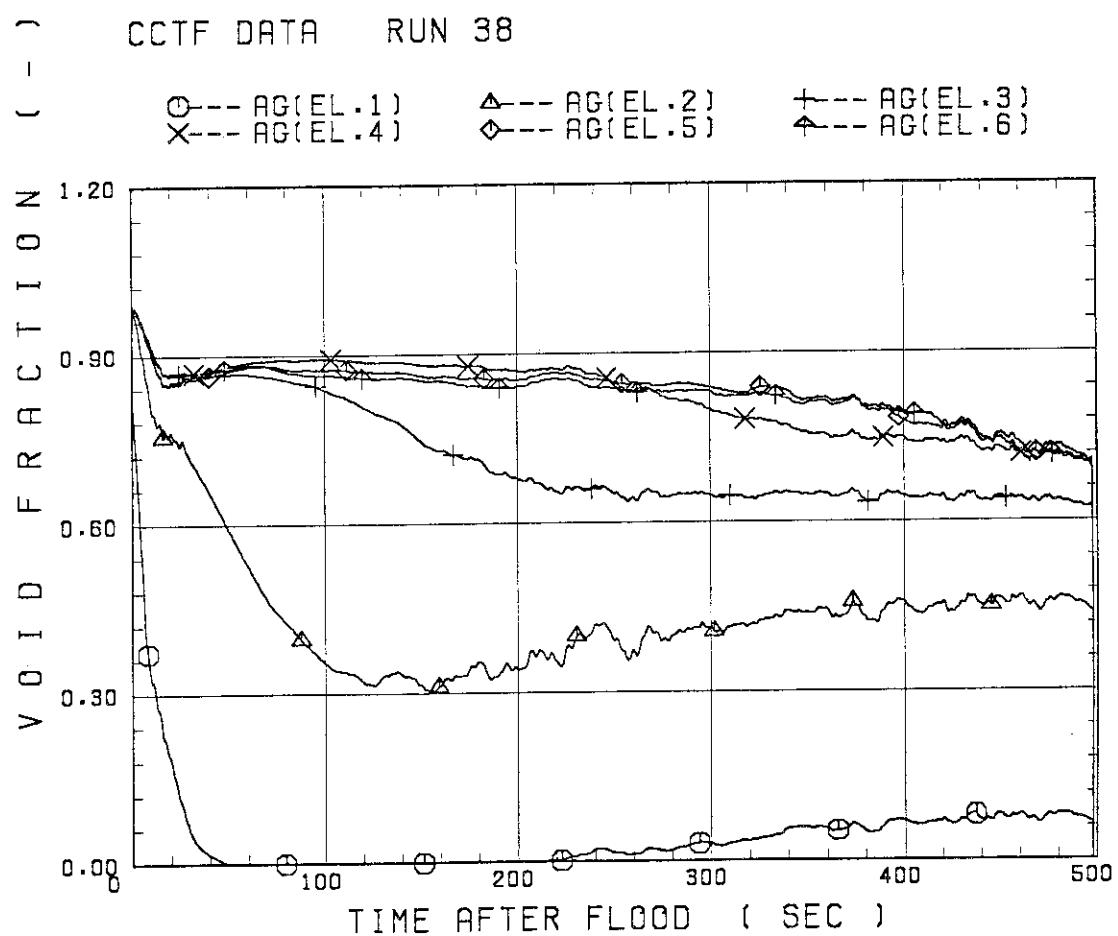
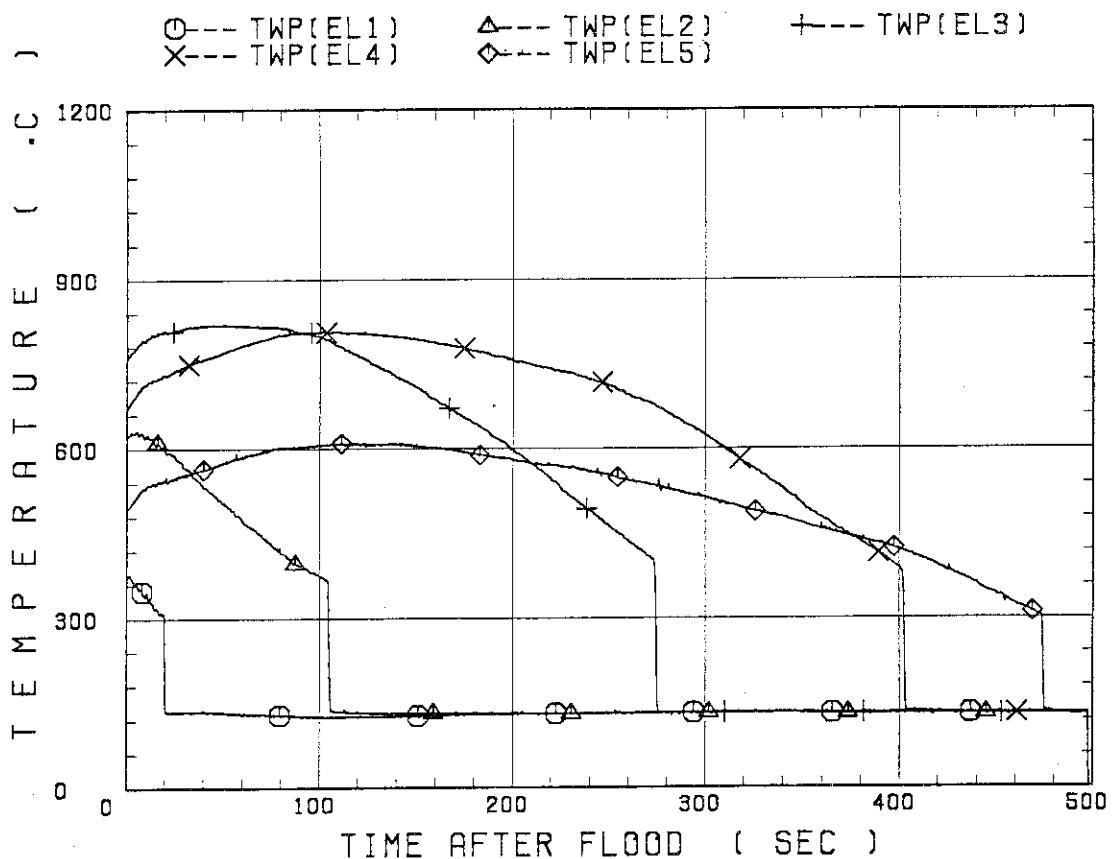
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CCTF DATA RUN 38

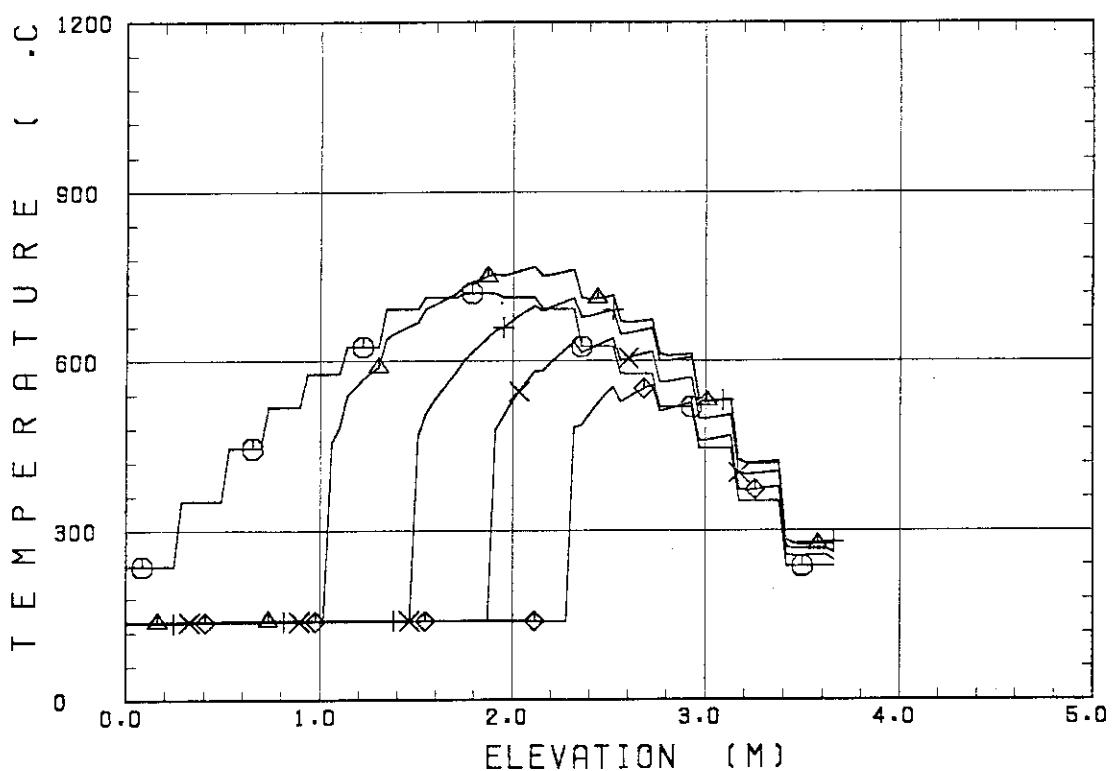


JAERI - M 85 - 210  
CCTF DATA RUN 38



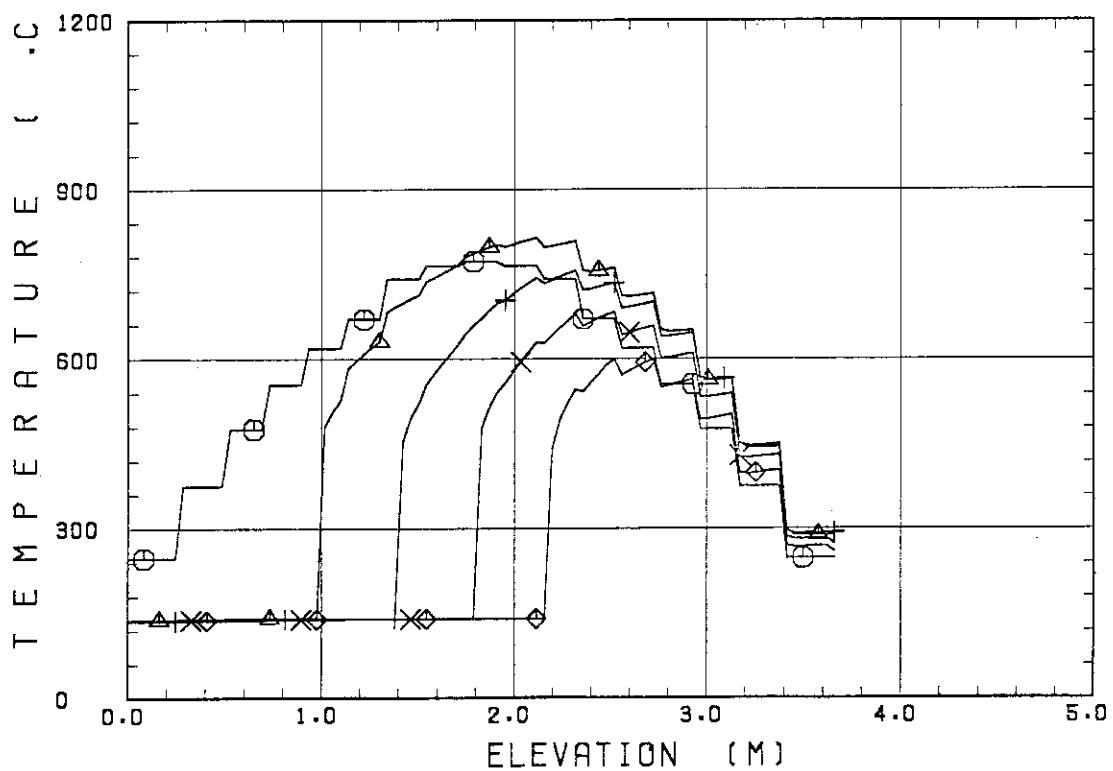
\*\* REFLAPS RUN ( IOPT = 1,1 ) \*\*  
 CCTF CORE-I ( RUN 38 , BUNDLE 17 )

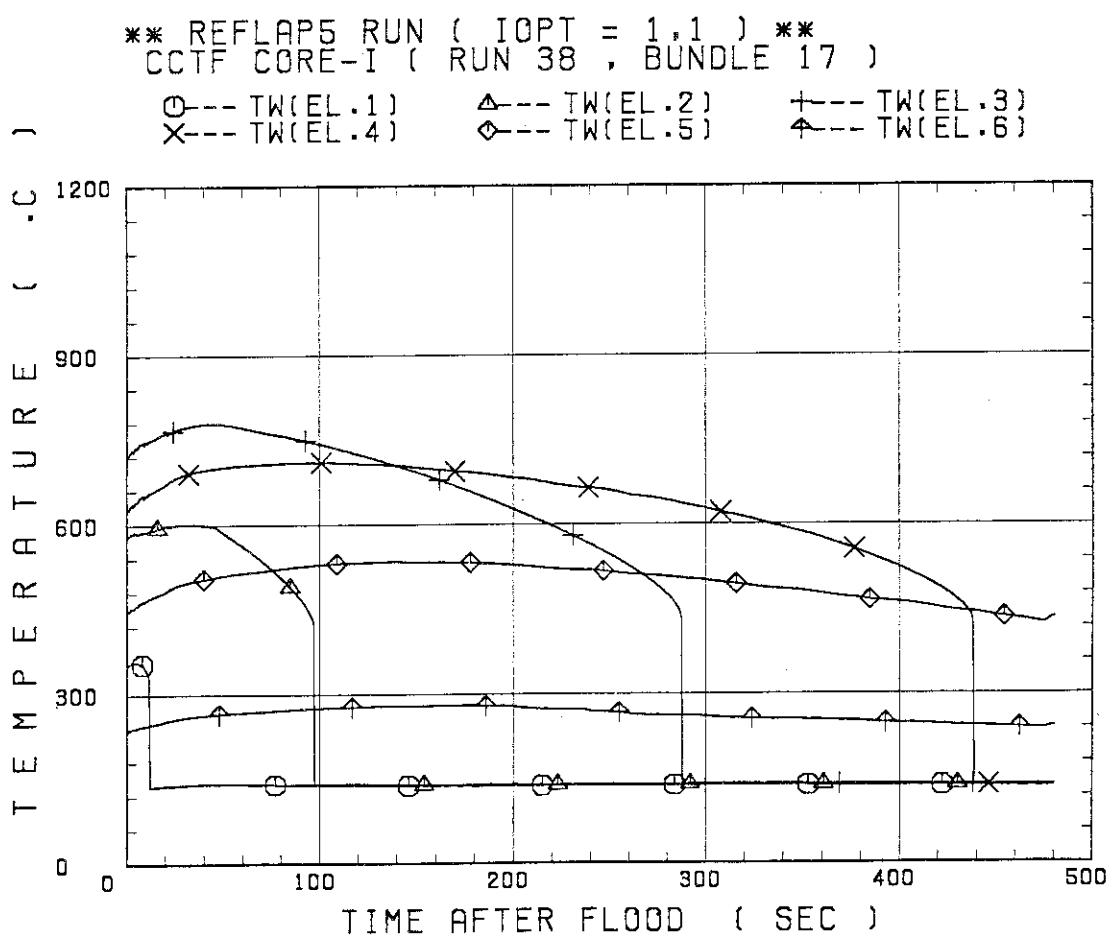
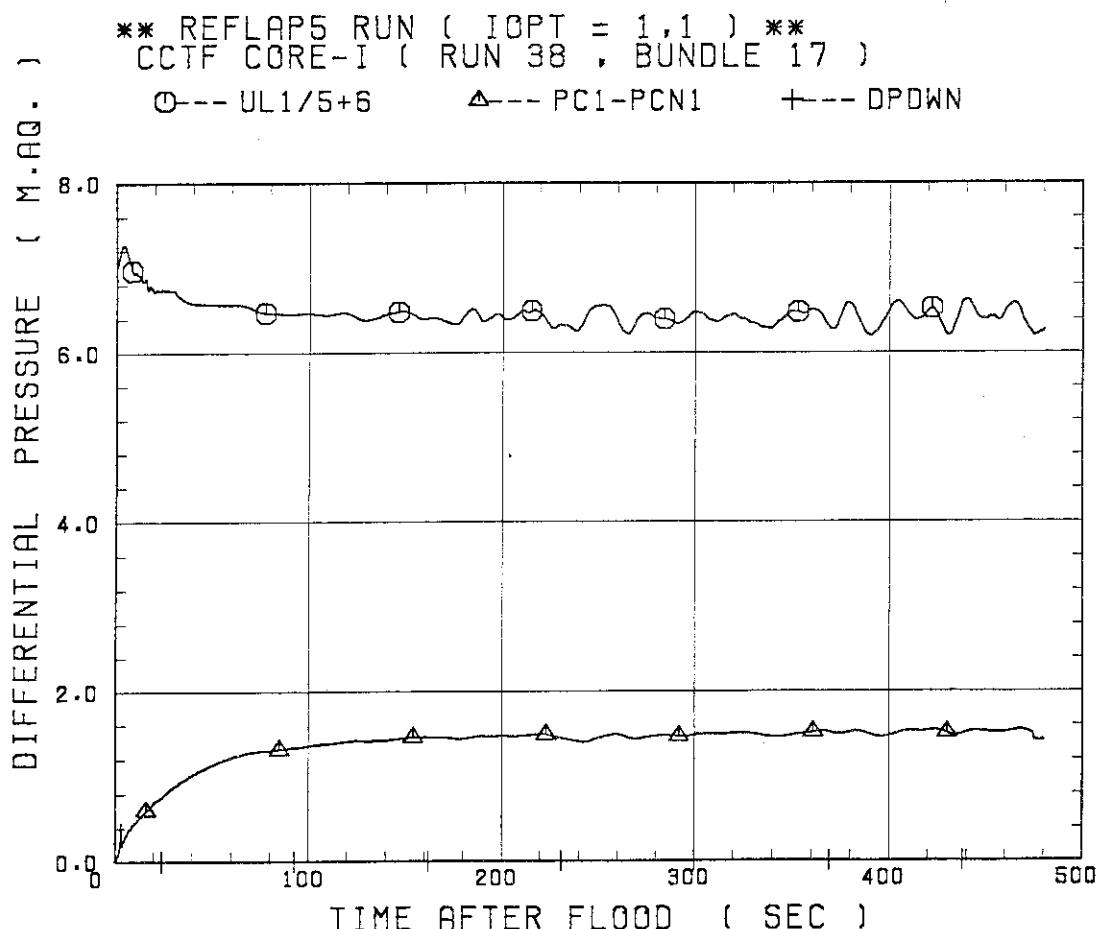
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 X--- 300 SEC      ◆--- 400 SEC



\*\* REFLAPS RUN ( IOPT = 1,1 ) \*\*  
 CCTF CORE-I ( RUN 38 , BUNDLE 17 )

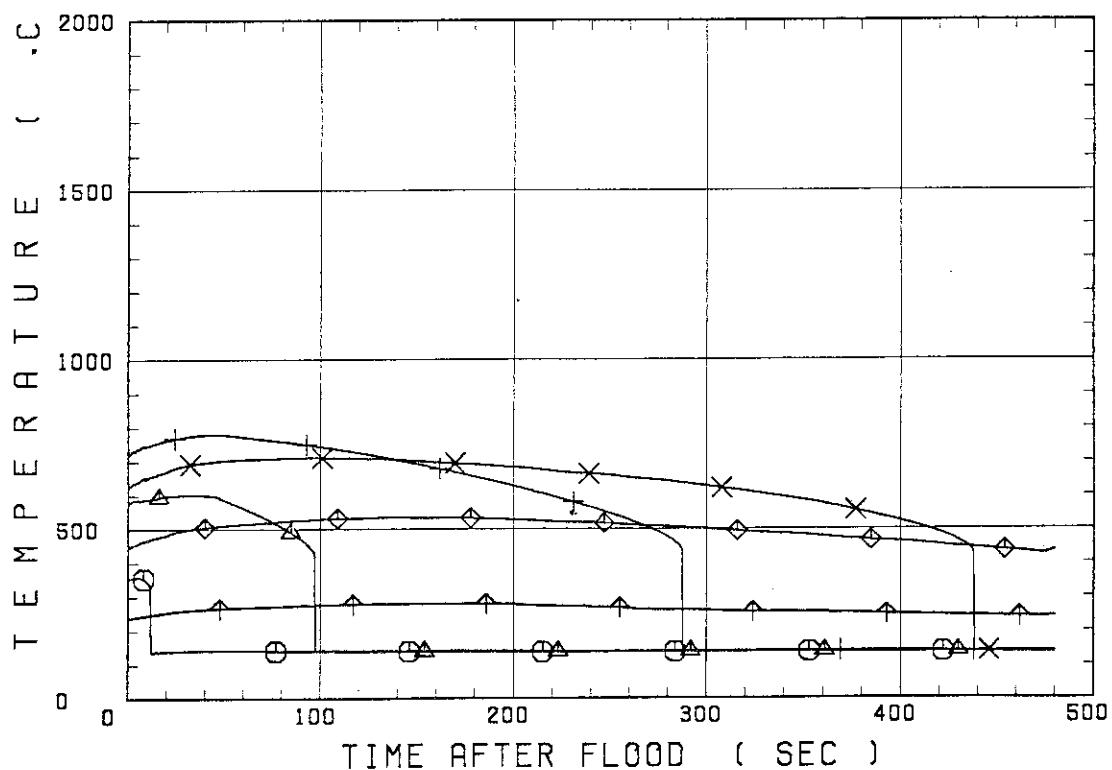
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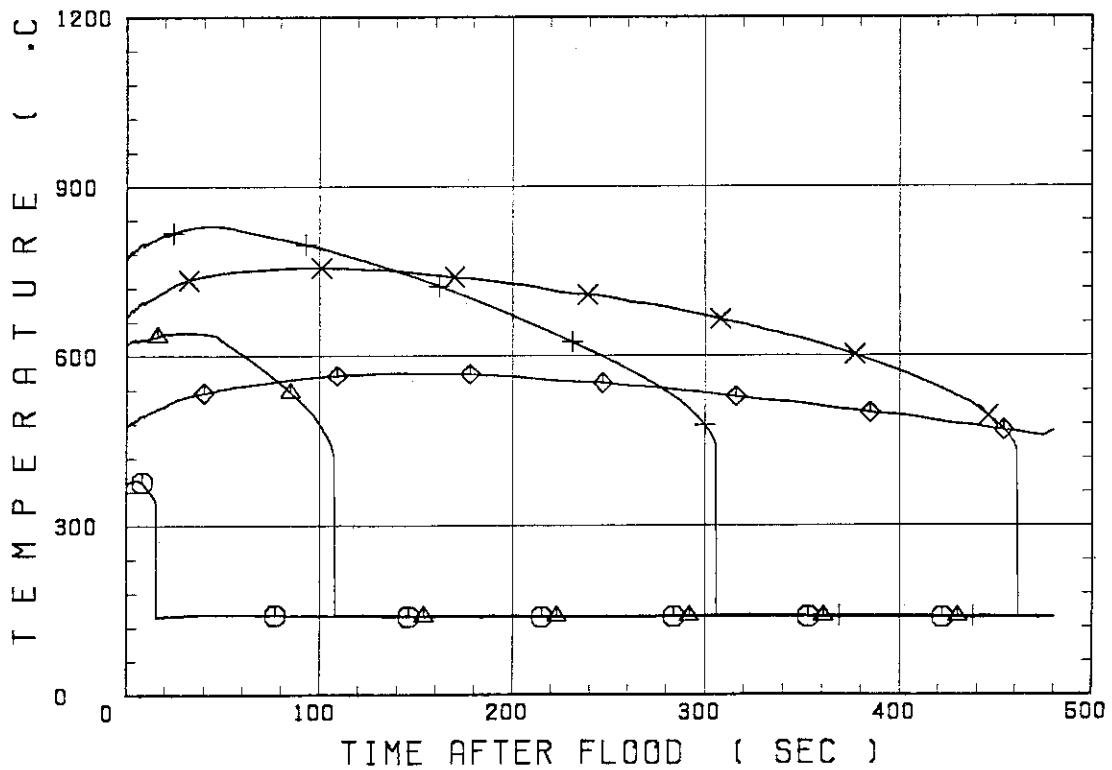
\*\* REFLAP5 RUN ( IOPT = 1,1 ) \*\*  
 CCTF CORE-I ( RUN 38 , BUNDLE 17 )

( O--- TW(EL.1) )    ( △--- TW(EL.2) )    ( +--- TW(EL.3) )  
 ( X--- TW(EL.4) )    ( ◇--- TW(EL.5) )    ( ↑--- TW(EL.6) )



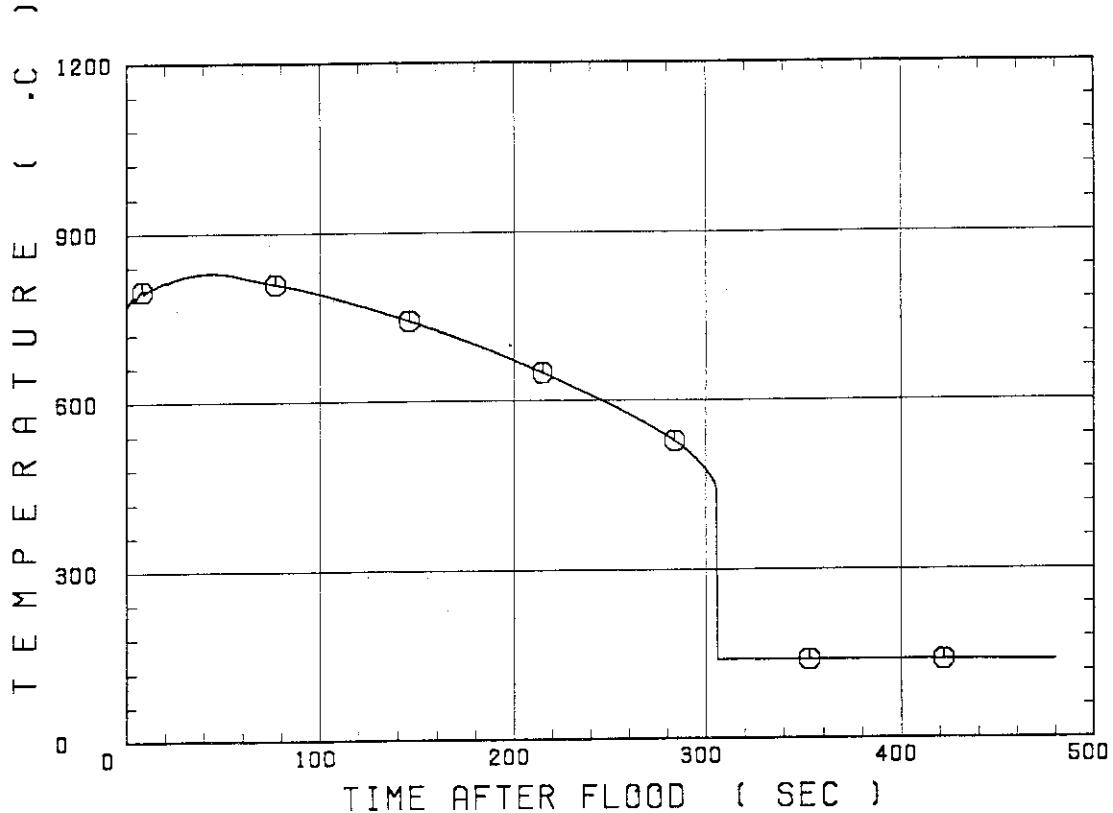
\*\* REFLAP5 RUN ( IOPT = 1,1 ) \*\*  
 CCTF CORE-I ( RUN 38 , BUNDLE 17 )

( O--- TWP(EL1) )    ( △--- TWP(EL2) )    ( +--- TWP(EL3) )  
 ( X--- TWP(EL4) )    ( ◇--- TWP(EL5) )



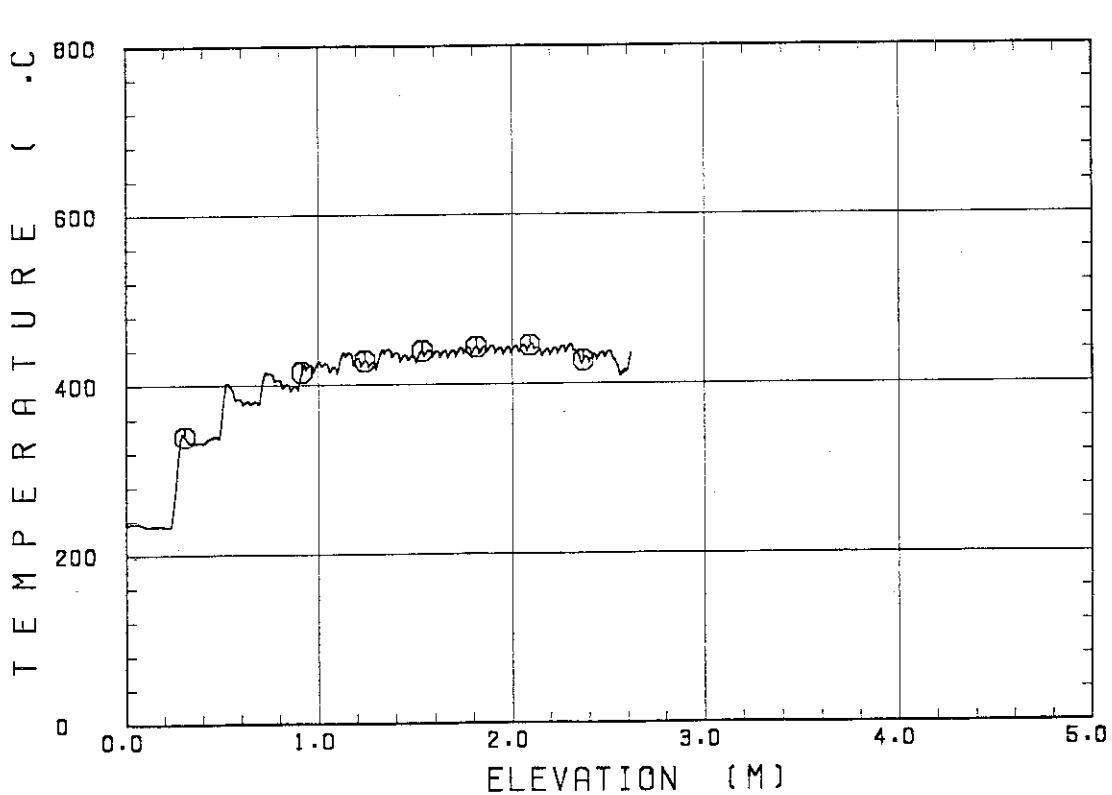
\*\* REFLAP5 RUN ( IOPT = 1,1 ) \*\*  
CCTF CORE-I ( RUN 38 , BUNDLE 17 )

○--- TWP(46)



\*\* REFLAP5 RUN ( IOPT = 1,1 ) \*\*  
CCTF CORE-I ( RUN 38 , BUNDLE 17 )

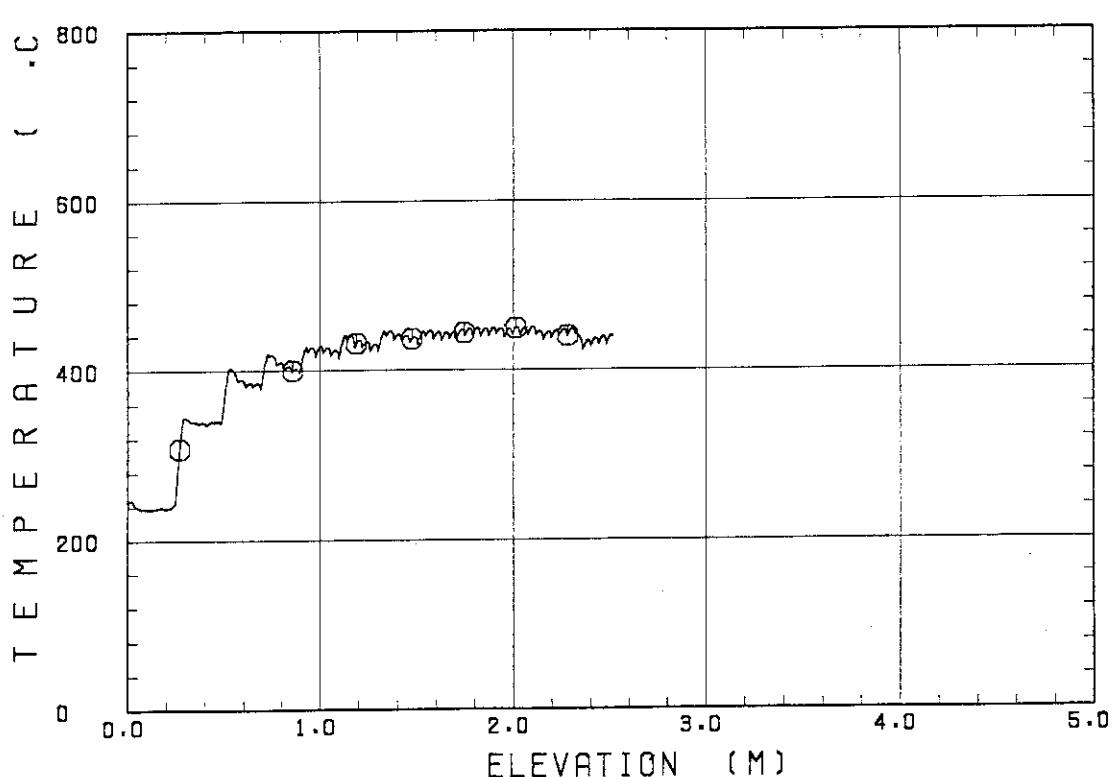
○--- TQN2



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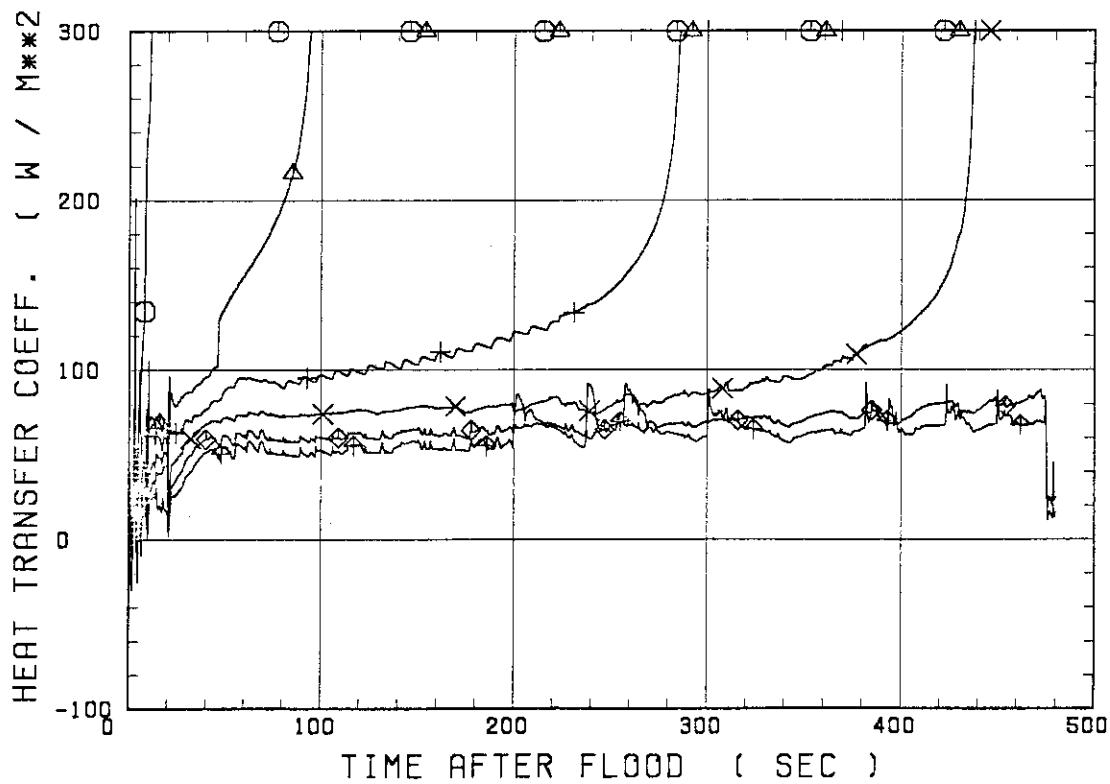
\*\* REFLAPS RUN ( IOPT = 1,1 ) \*\*  
CCTF CORE-I ( RUN 38 , BUNDLE 17 )

O---TPN2



\*\* REFLAPS RUN ( IOPT = 1,1 ) \*\*  
CCTF CORE-I ( RUN 38 , BUNDLE 17 )

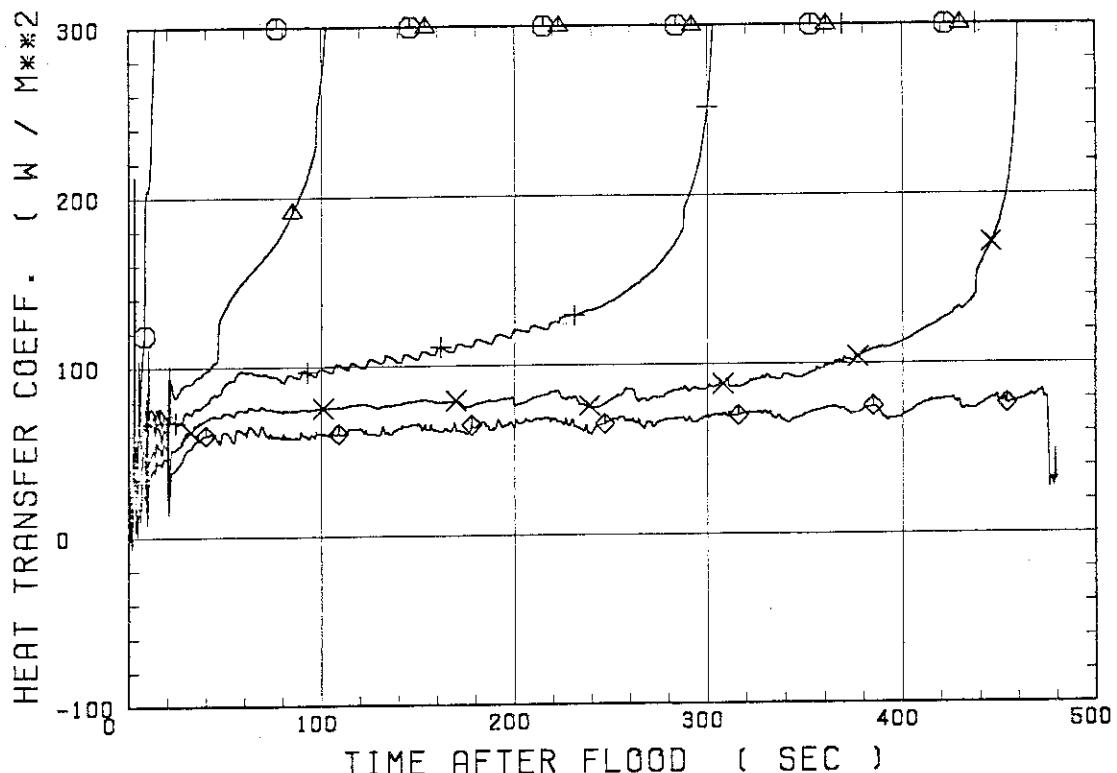
O---HT(EL.1)    ▲---HT(EL.2)    +---HT(EL.3)  
X---HT(EL.4)    ♦---HT(EL.5)    ↗---HT(EL.6)



JAERI-M 85-210

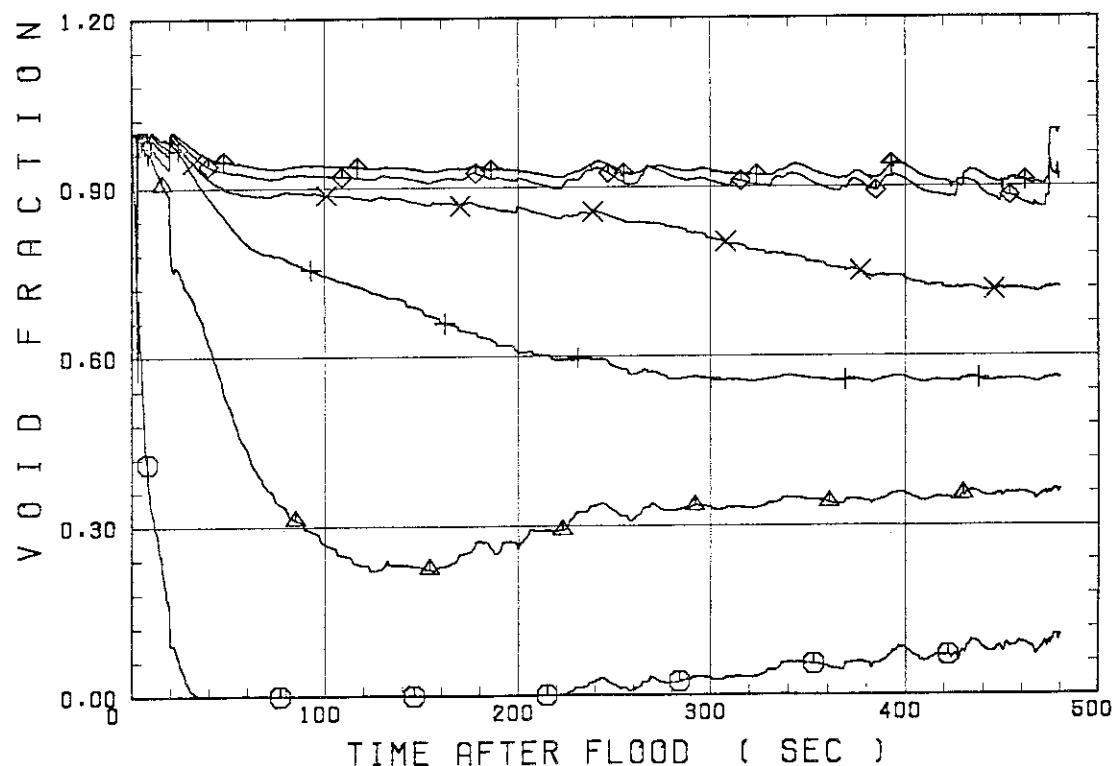
\*\* REFLAP5 RUN ( IOPT = 1,1 ) \*\*  
CCTF CORE-I ( RUN 38 , BUNDLE 17 )

○--- HTP(EL1)    ▲--- HTP(EL2)    +--- HTP(EL3)  
×--- HTP(EL4)    ◇--- HTP(EL5)



\*\* REFLAP5 RUN ( IOPT = 1,1 ) \*\*  
CCTF CORE-I ( RUN 38 , BUNDLE 17 )

○--- AG(EL.1)    ▲--- AG(EL.2)    +--- AG(EL.3)  
×--- AG(EL.4)    ◇--- AG(EL.5)    ♦--- AG(EL.6)

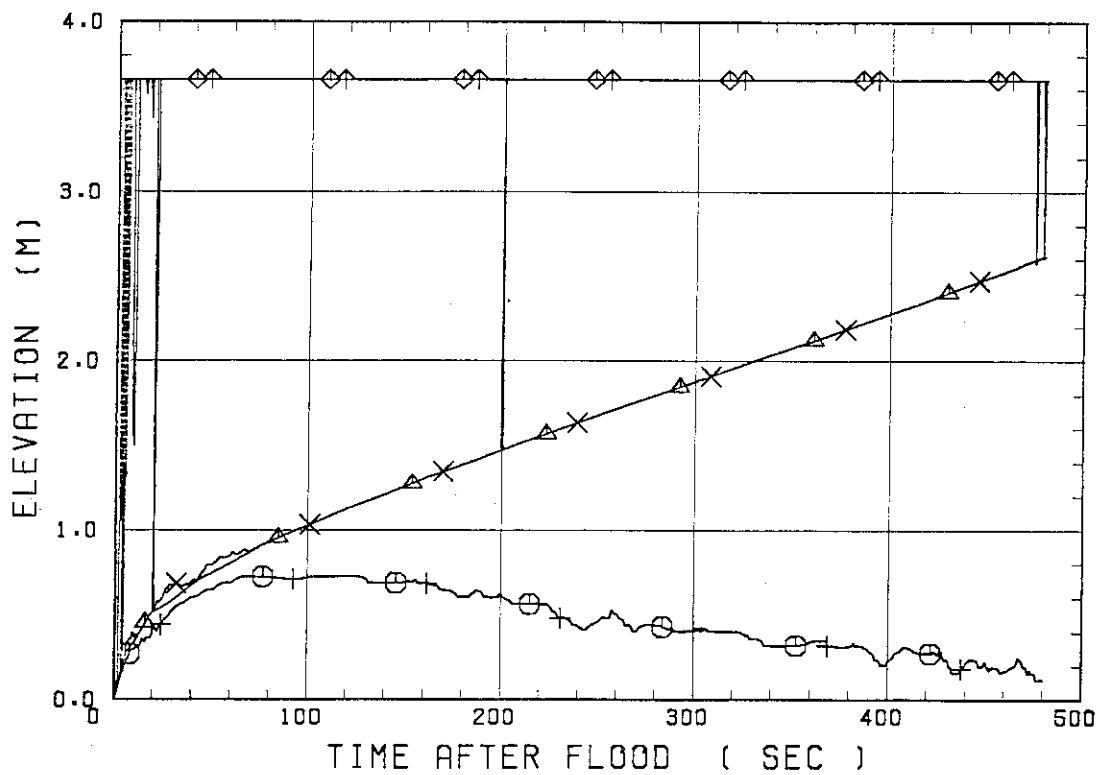


\*\* REFLAPS RUN ( IOPT = 1,1 ) \*\*  
 CCTF CORE-I ( RUN 38 , BUNDLE 17 )

○---L1  
 X---L4

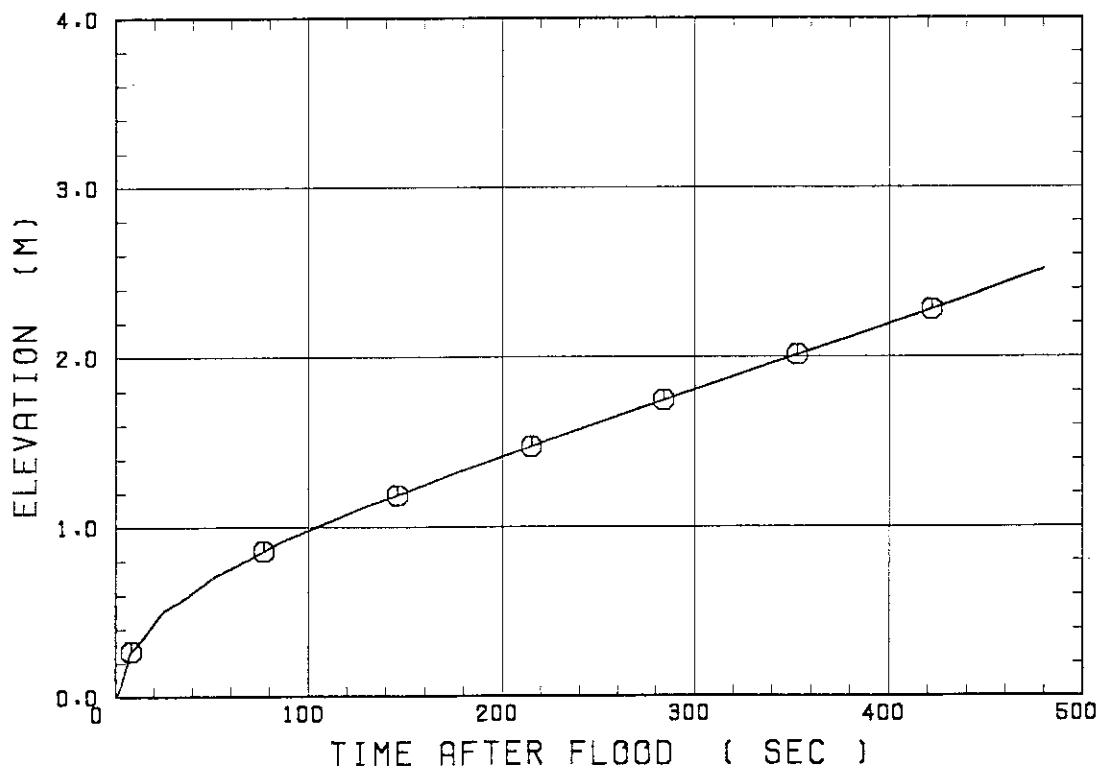
△---L2  
 ◊---L5

+---L3  
 ↑---L7



\*\* REFLAPS RUN ( IOPT = 1,1 ) \*\*  
 CCTF CORE-I ( RUN 38 , BUNDLE 17 )

○---LP2



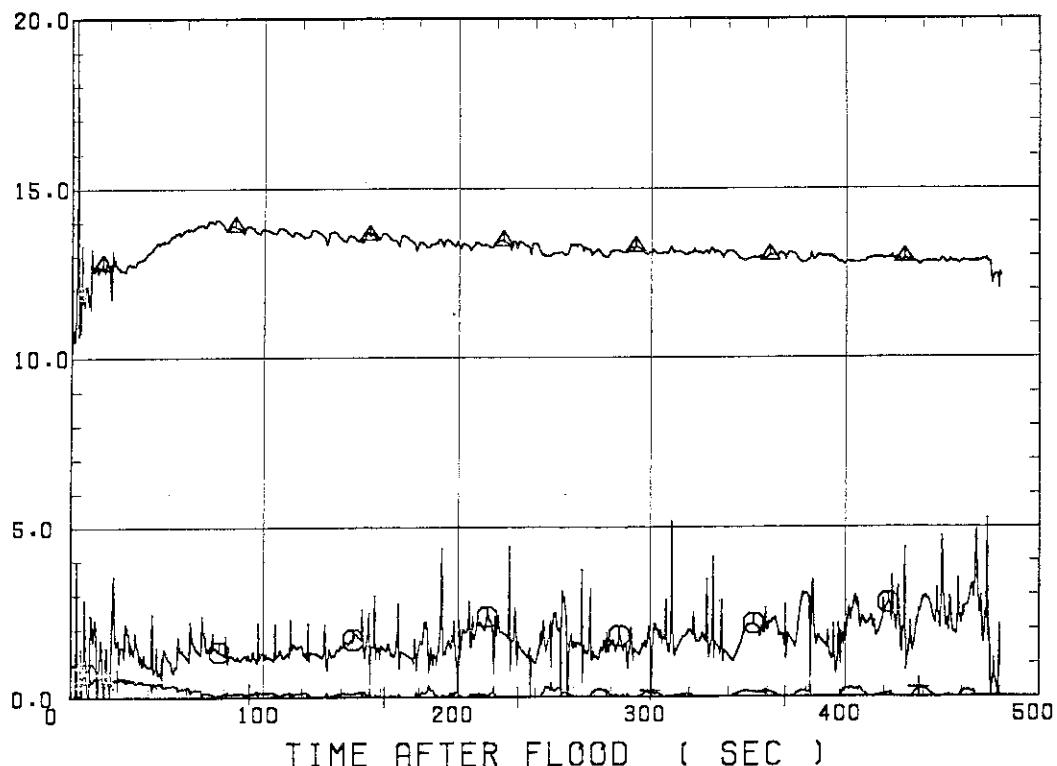
JAERI-M 85-210

\*\* REFLAP5 RUN ( IOPT = 1,1 ) \*\*  
CCTF CORE-I ( RUN 38 , BUNDLE 17 )

○--- GLOUT/G1

△--- GN1/G1

+--- MCDOT/G1

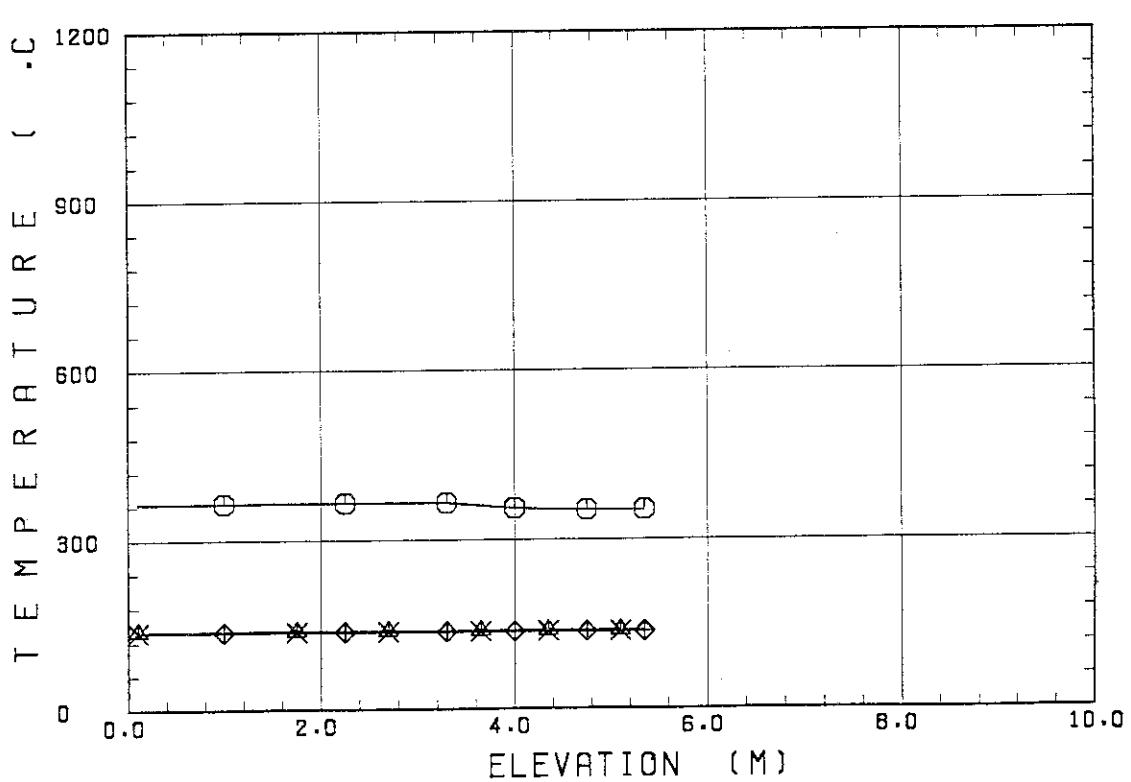


\*\* REFLAP5 RUN ( IOPT = 1,1 ) \*\*  
CCTF CORE-I ( RUN 38 , BUNDLE 17 )

○--- 0 SEC      X--- 300 SEC

△--- 100 SEC      ◆--- 400 SEC

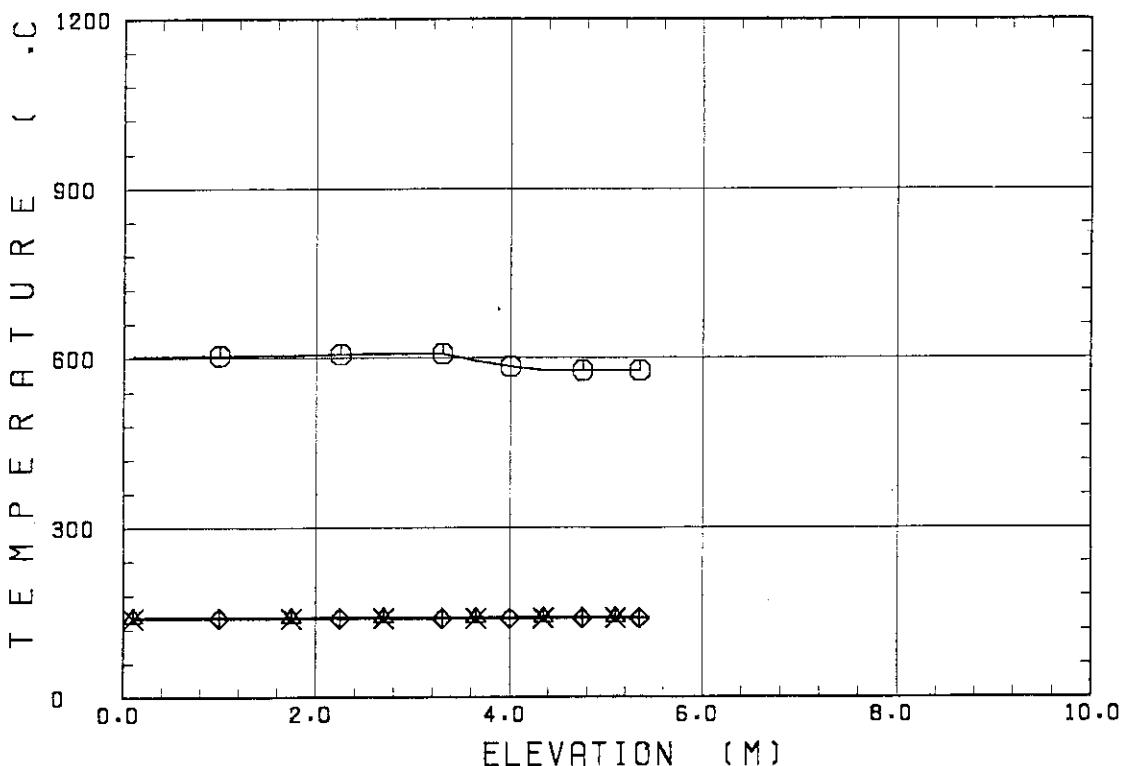
+--- 200 SEC



JAERI-M 85-210

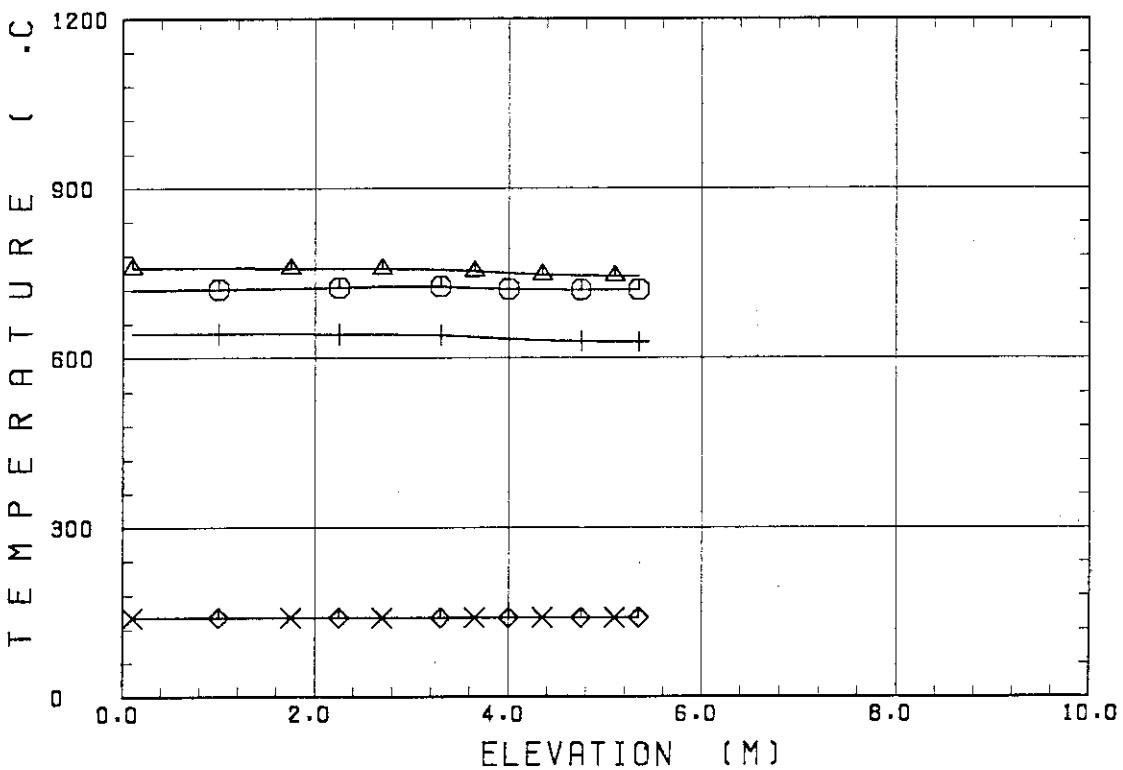
\*\* REFLAP5 RUN ( IOPT = 1,1 ) \*\*  
CCTF CORE-I ( RUN 38 , BUNDLE 17 )

O--- 0 SEC      △--- 100 SEC      +--- 200 SEC  
X--- 300 SEC      ◆--- 400 SEC



\*\* REFLAP5 RUN ( IOPT = 1,1 ) \*\*  
CCTF CORE-I ( RUN 38 , BUNDLE 17 )

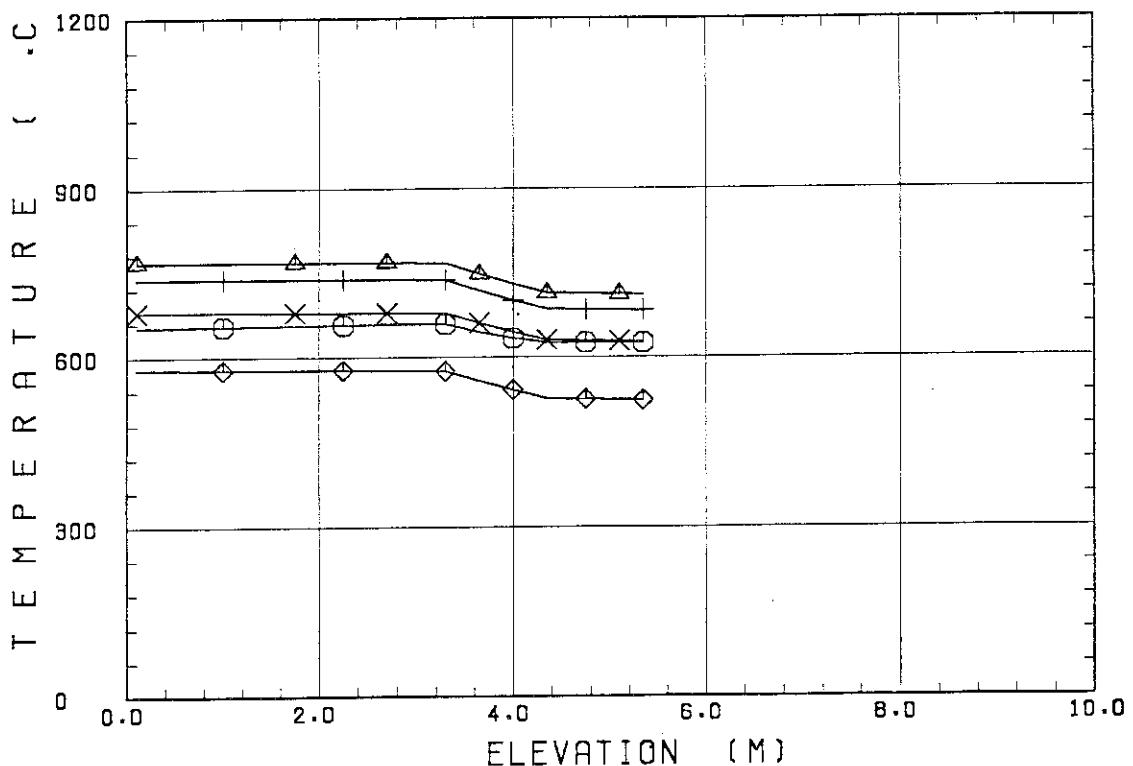
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X--- 300 SEC      ◆--- 400 SEC



JAERI-M 85-210

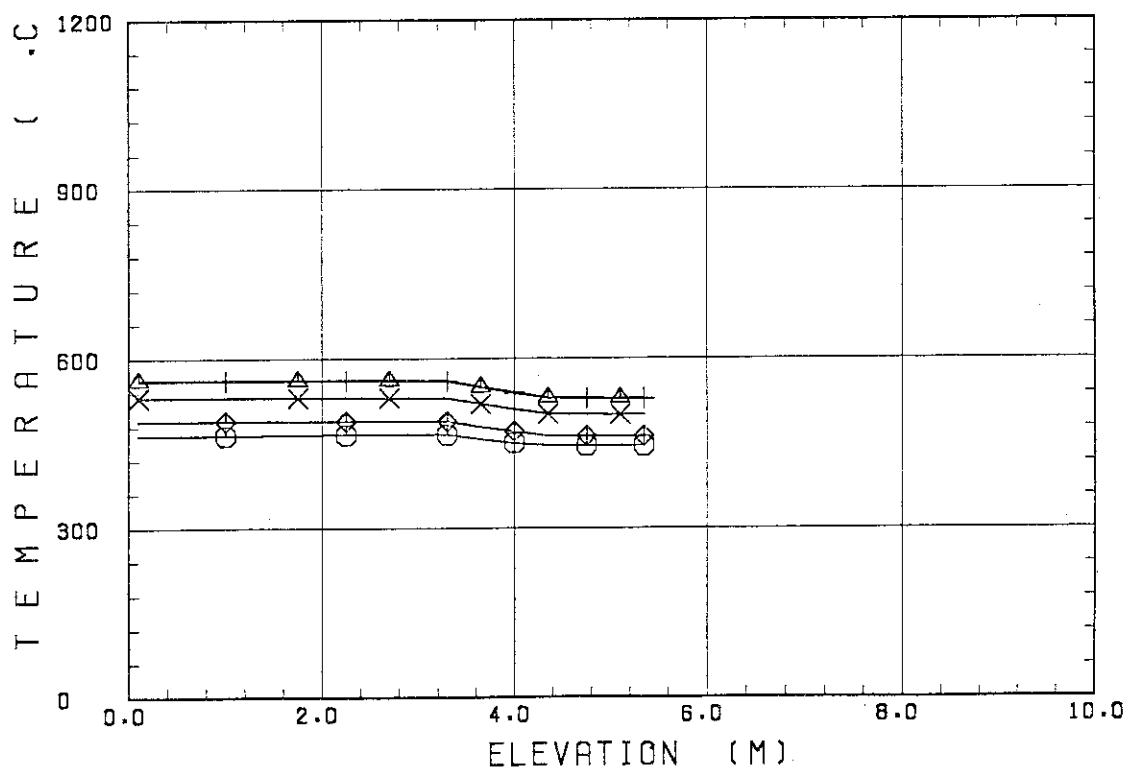
\*\* REFLAPS RUN ( IOPT = 1,1 ) \*\*  
CCTF CORE-I ( RUN 38 , BUNDLE 17 )

O--- 0 SEC      ▲--- 100 SEC      +--- 200 SEC  
X--- 300 SEC      ◆--- 400 SEC

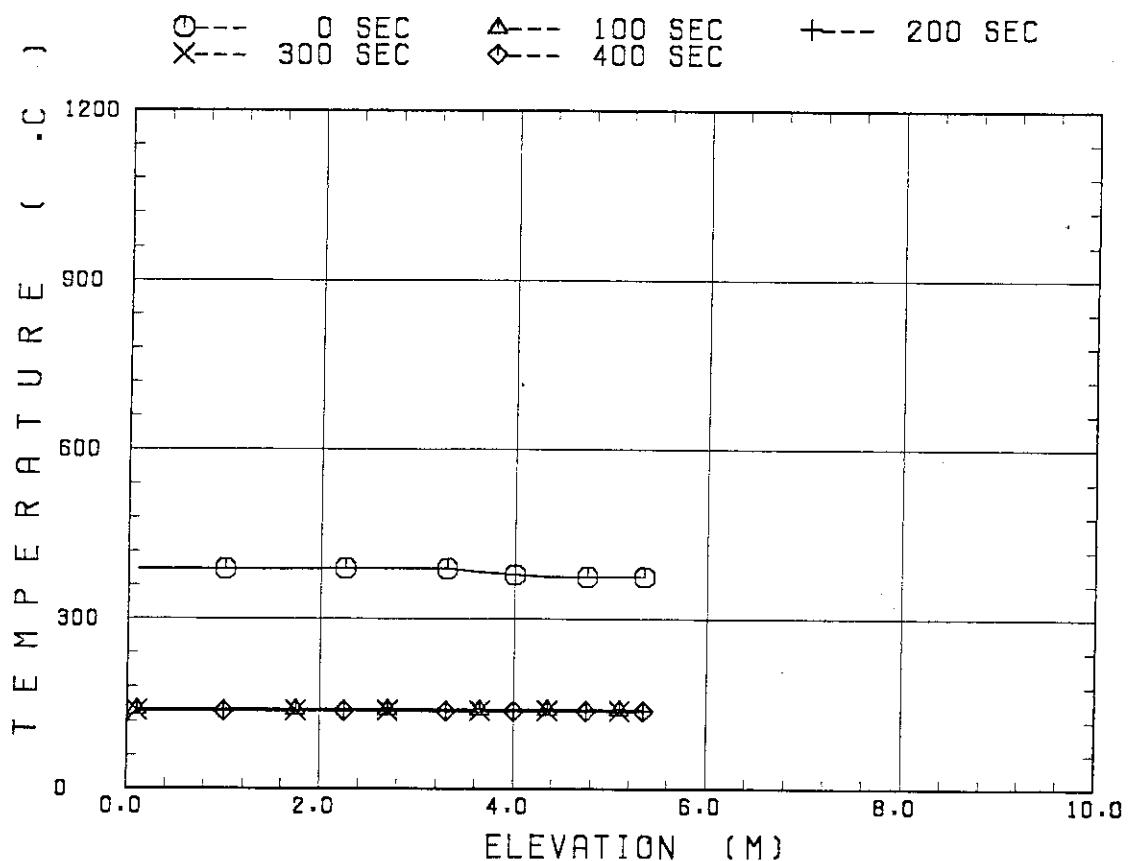


\*\* REFLAPS RUN ( IOPT = 1,1 ) \*\*  
CCTF CORE-I ( RUN 38 , BUNDLE 17 )

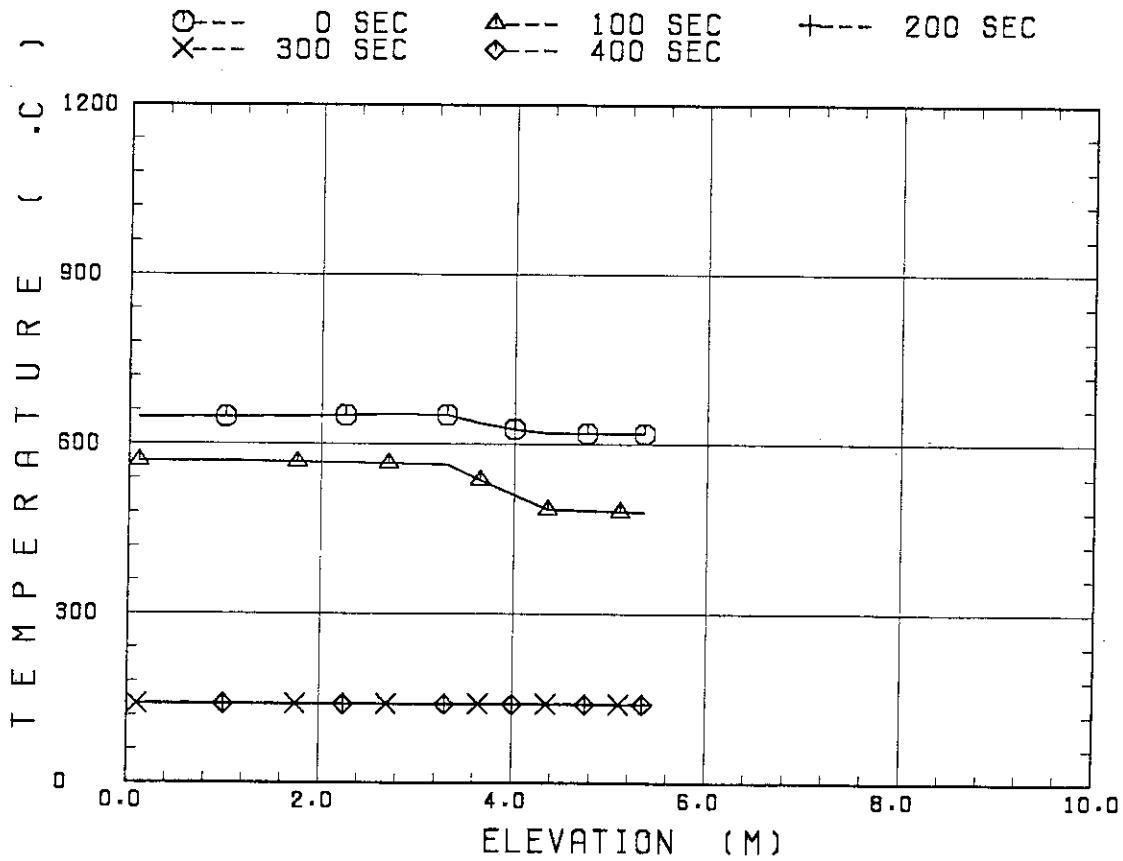
O--- 0 SEC      ▲--- 100 SEC      +--- 200 SEC  
X--- 300 SEC      ◆--- 400 SEC



\*\* REFLAP5 RUN ( IOPT = 1,1 ) \*\*  
 CCTF CORE-I ( RUN 38 , BUNDLE 17 )

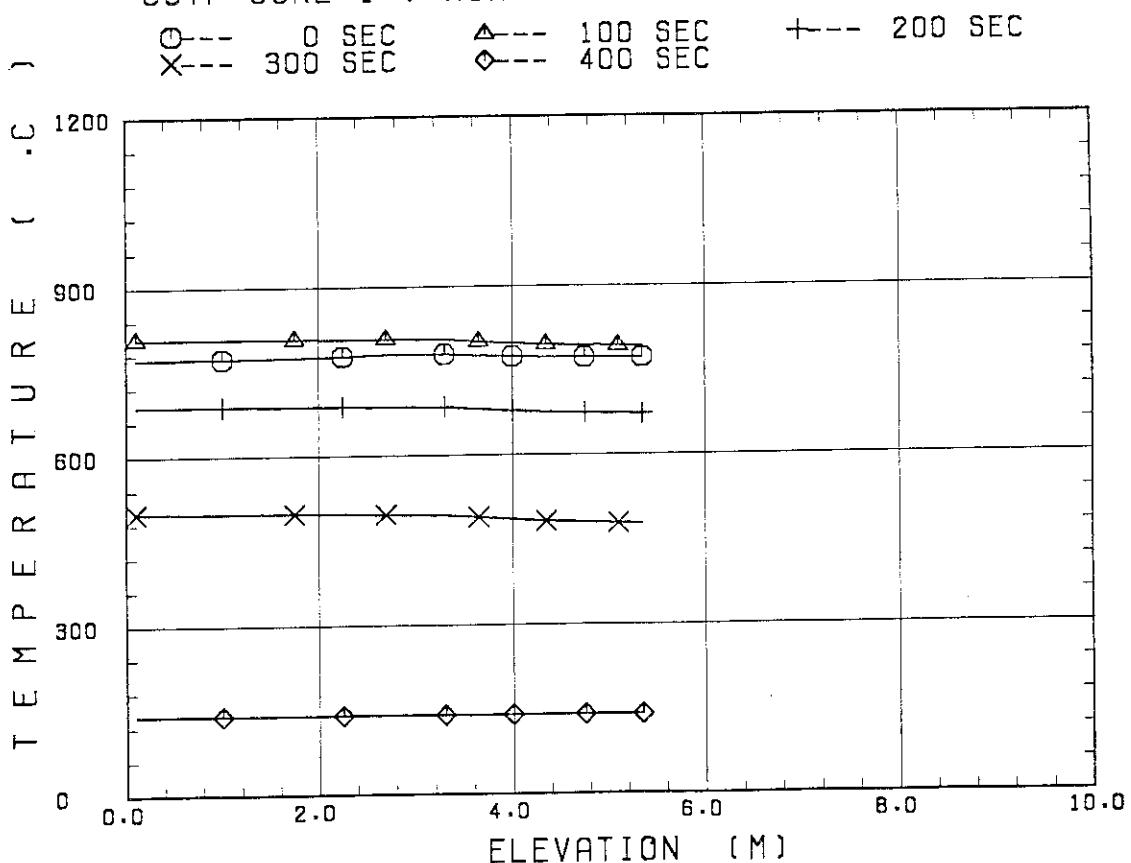


\*\* REFLAP5 RUN ( IOPT = 1,1 ) \*\*  
 CCTF CORE-I ( RUN 38 , BUNDLE 17 )

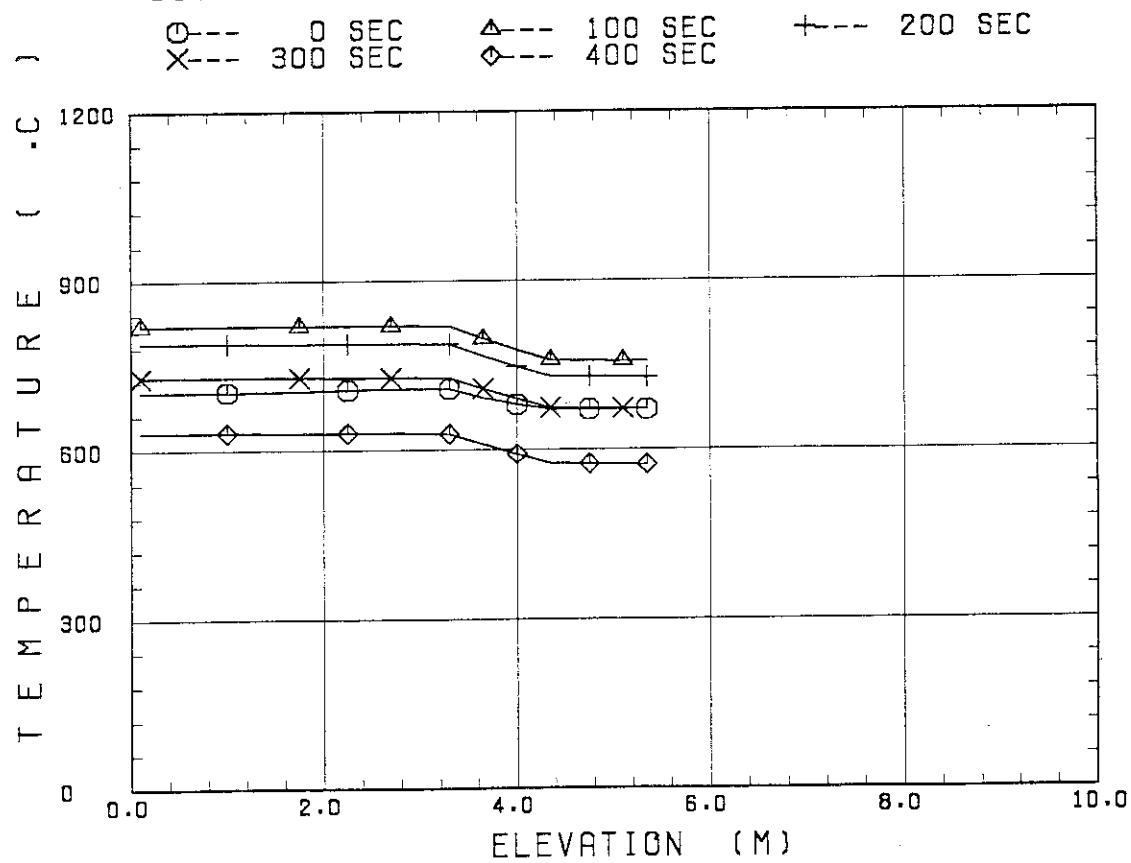


JAERI-M 85-210

\*\* REFLAPS RUN ( IOPT = 1,1 ) \*\*  
CCTF CORE-I ( RUN 38 , BUNDLE 17 )



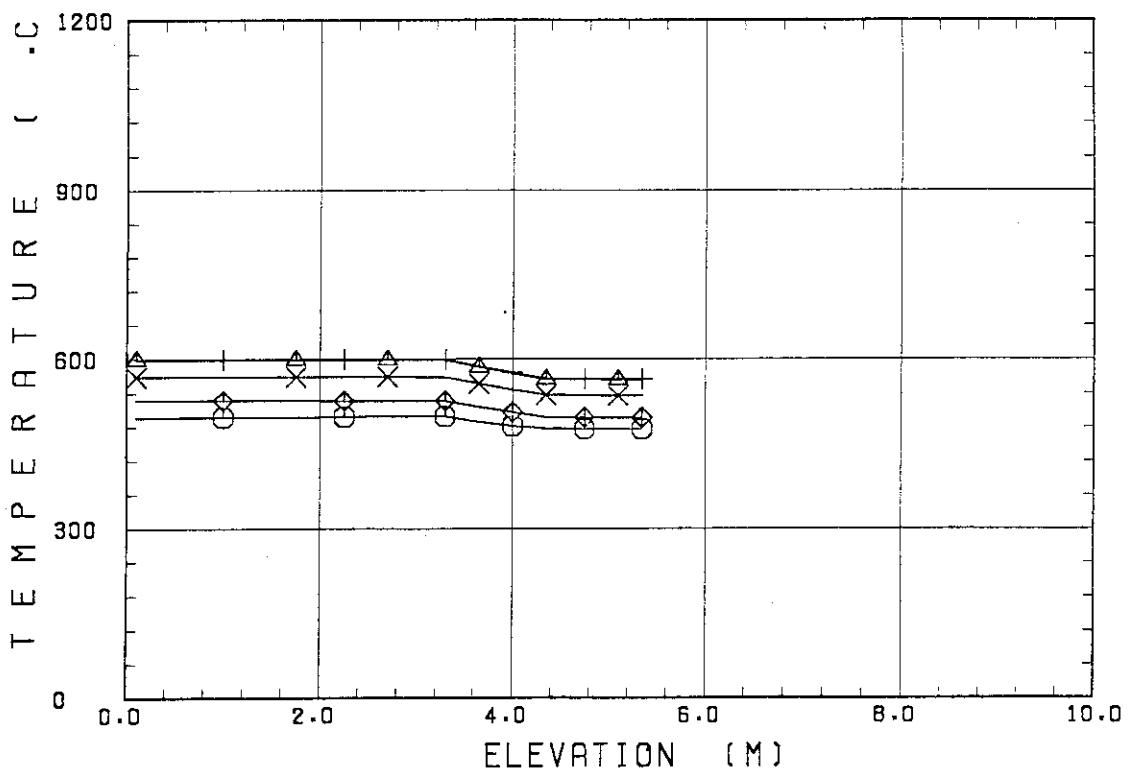
\*\* REFLAPS RUN ( IOPT = 1,1 ) \*\*  
CCTF CORE-I ( RUN 38 , BUNDLE 17 )



JAERI-M 85-210

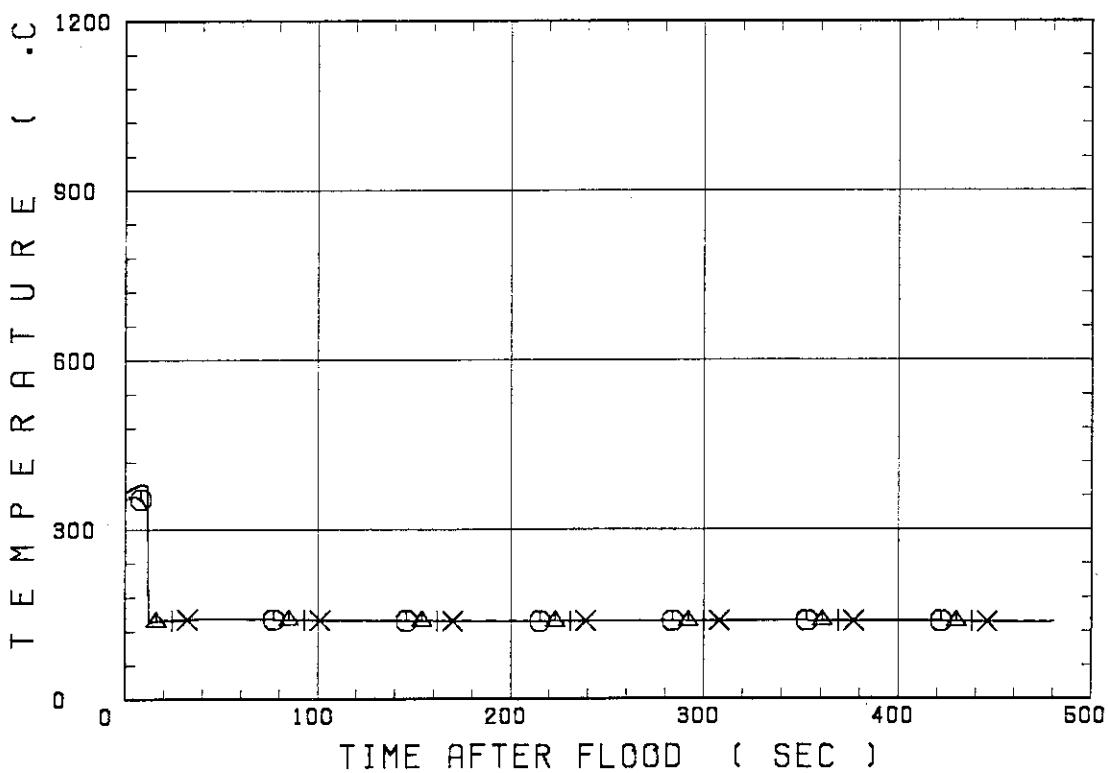
\*\* REFLAPS RUN ( IOPT = 1,1 ) \*\*  
CCTF CORE-I ( RUN 38 , BUNDLE 17 )

O--- 0 SEC      ▲--- 100 SEC      +--- 200 SEC  
X--- 300 SEC      ◆--- 400 SEC



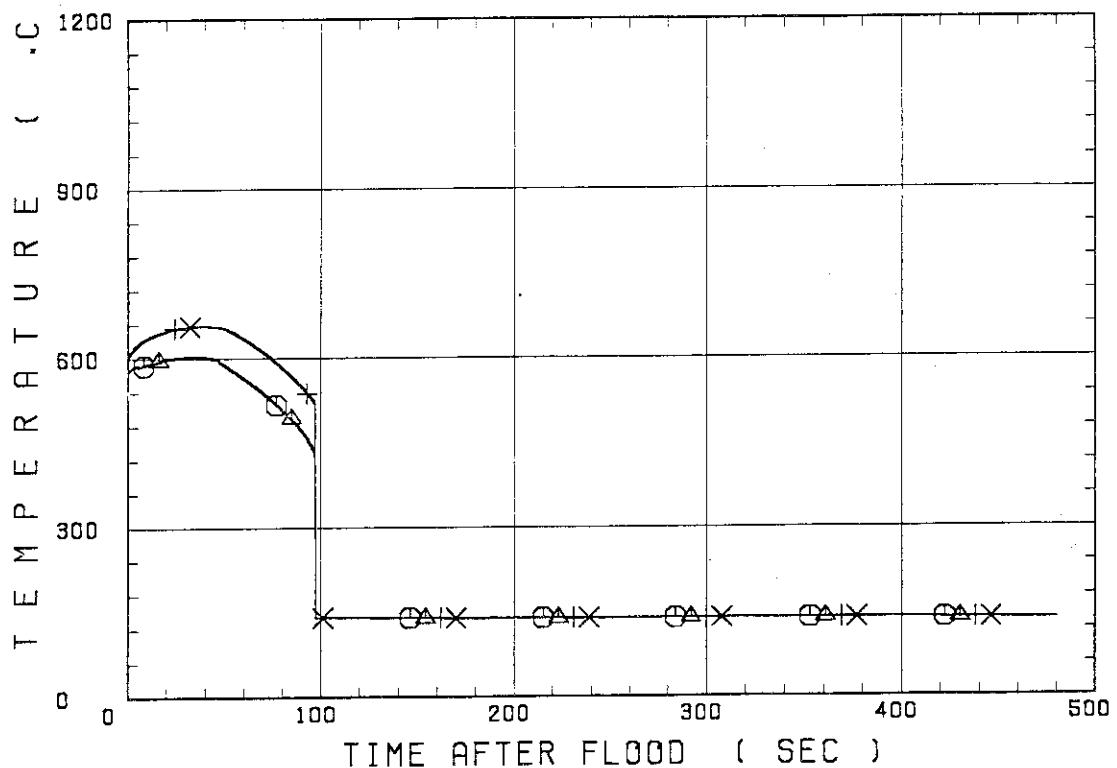
\*\* REFLAPS RUN ( IOPT = 1,1 ) \*\*  
CCTF CORE-I ( RUN 38 , BUNDLE 17 )

O--- TF(1,1)      ▲--- TF(2,1)      +--- TF(3,1)  
X--- TF(4,1)



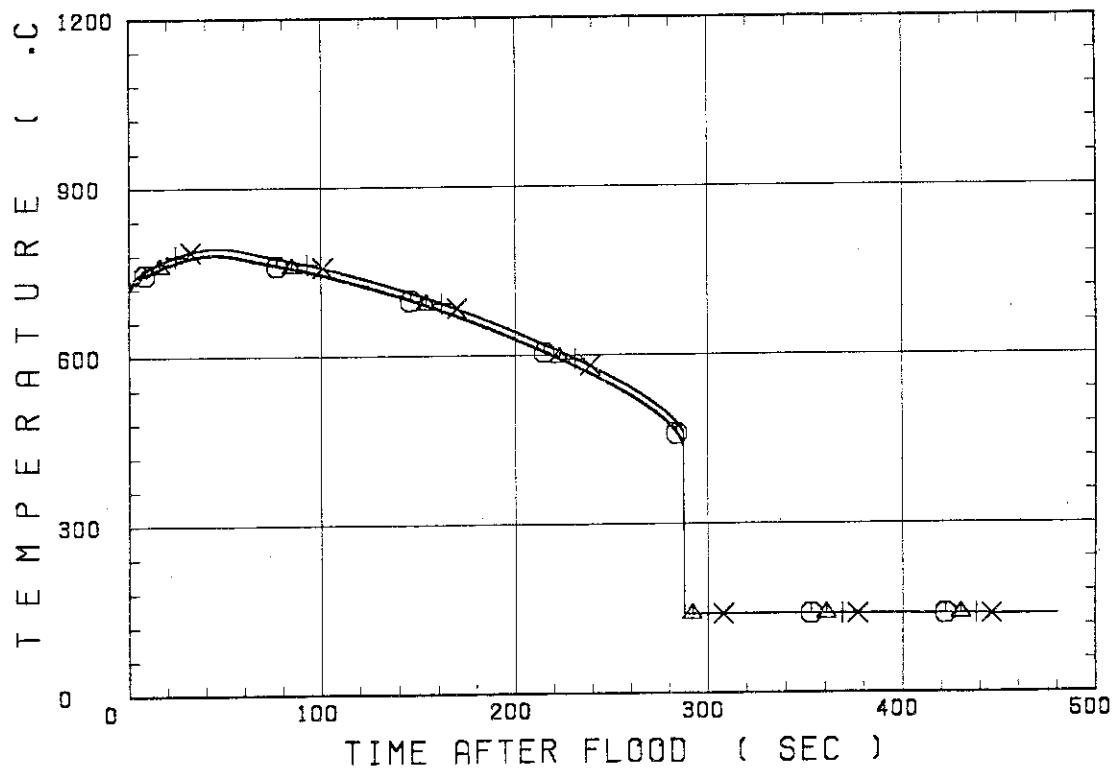
\*\* REFLAP5 RUN ( IOPT = 1,1 ) \*\*  
 CCTF CORE-I ( RUN 38 , BUNDLE 17 )

○--- TF(1,2)    △--- TF(2,2)    +--- TF(3,2)  
 X--- TF(4,2)



\*\* REFLAP5 RUN ( IOPT = 1,1 ) \*\*  
 CCTF CORE-I ( RUN 38 , BUNDLE 17 )

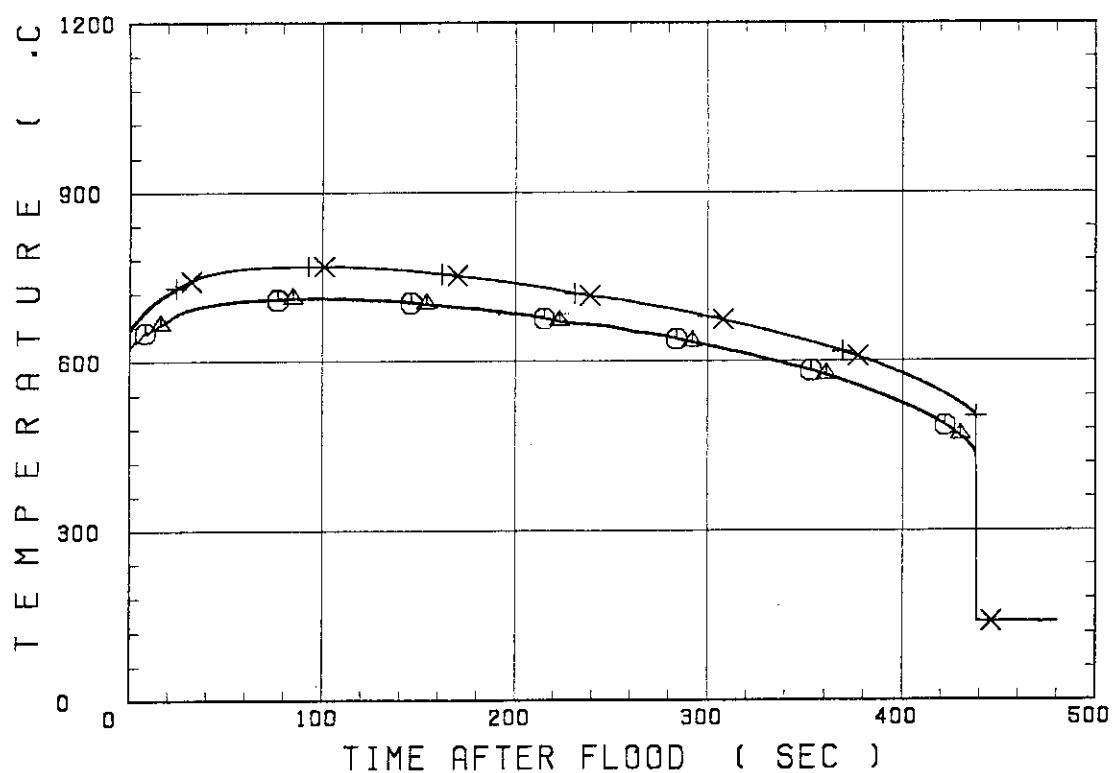
○--- TF(1,3)    △--- TF(2,3)    +--- TF(3,3)  
 X--- TF(4,3)



JAERI-M 85-210

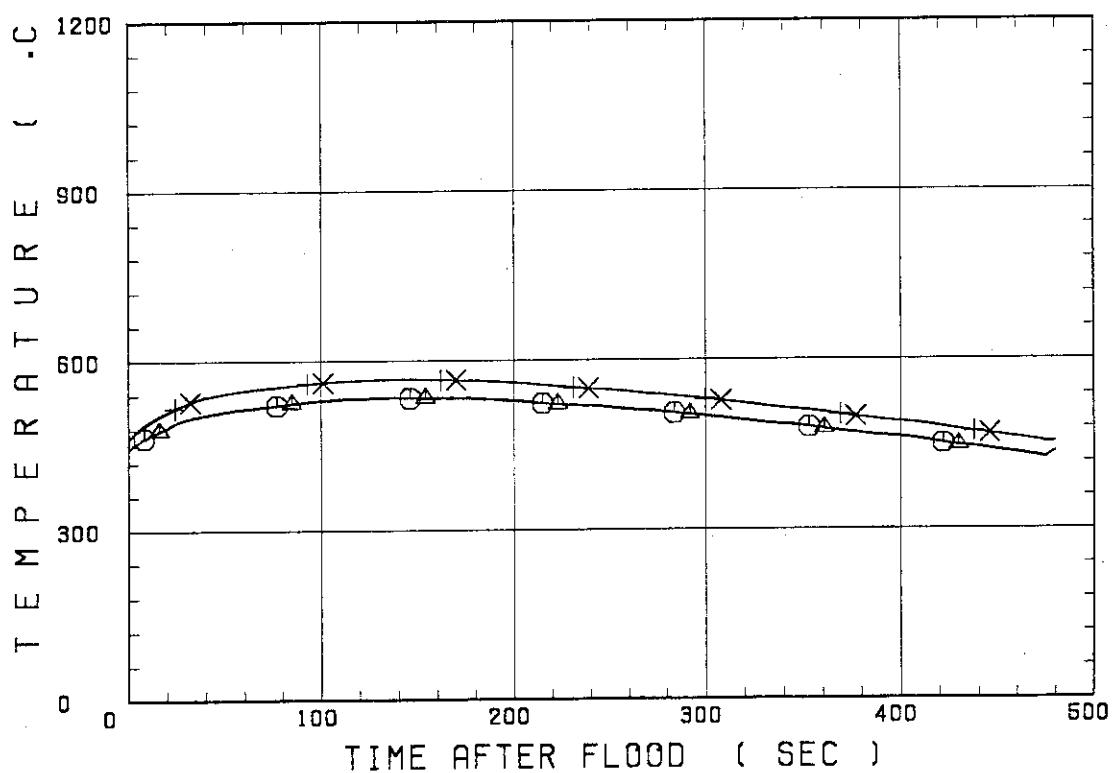
\*\* REFLAP5 RUN ( IOPT = 1,1 ) \*\*  
CCTF CORE-I ( RUN 38 , BUNDLE 17 )

○--- TF(1,4)      △--- TF(2,4)      +--- TF(3,4)  
X--- TF(4,4)

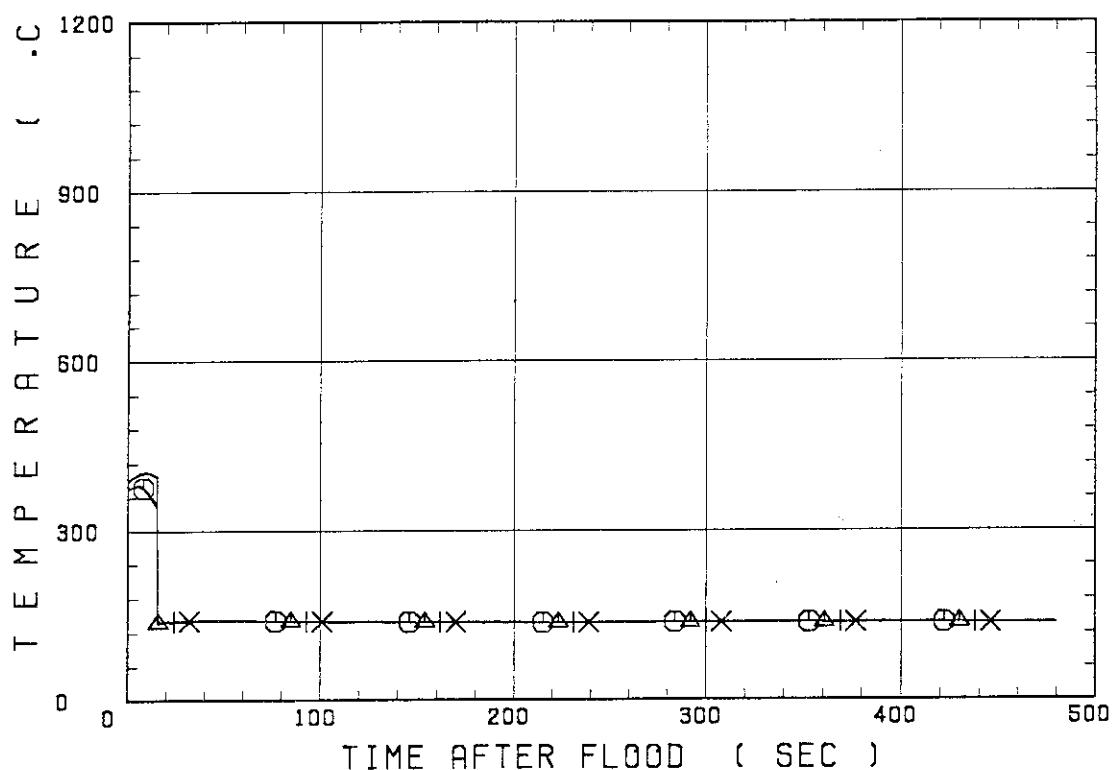


\*\* REFLAP5 RUN ( IOPT = 1,1 ) \*\*  
CCTF CORE-I ( RUN 38 , BUNDLE 17 )

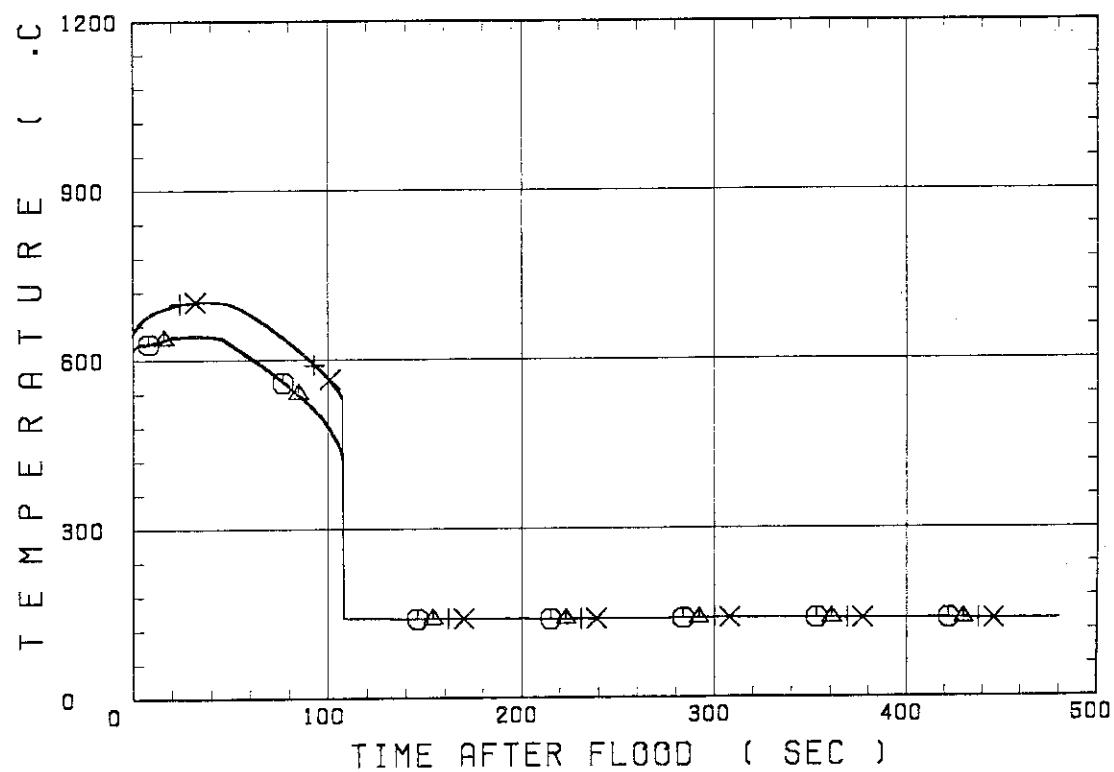
○--- TF(1,5)      △--- TF(2,5)      +--- TF(3,5)  
X--- TF(4,5)



\*\* REFLAP5 RUN ( IOPT = 1,1 ) \*\*  
 CCTF CORE-I ( RUN 38 , BUNDLE 17 )  
 ○--- TFP(1,1)    △--- TFP(2,1)    +--- TFP(3,1)  
 X--- TFP(4,1)

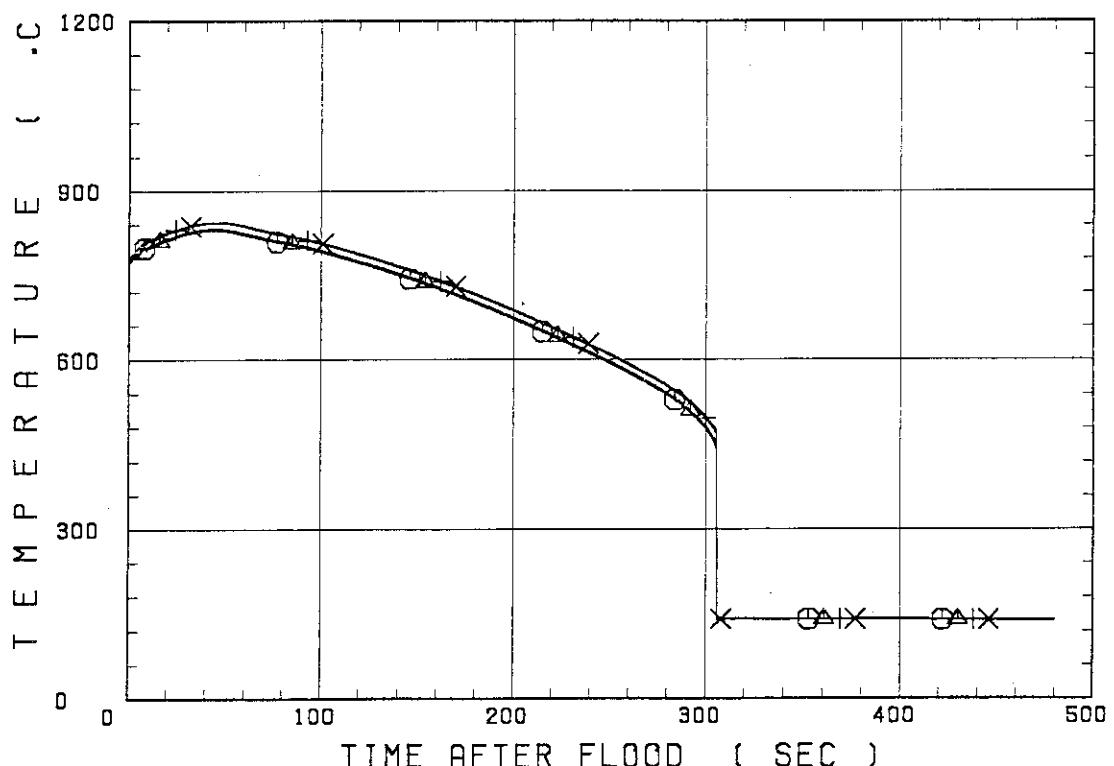


\*\* REFLAP5 RUN ( IOPT = 1,1 ) \*\*  
 CCTF CORE-I ( RUN 38 , BUNDLE 17 )  
 ○--- TFP(1,2)    △--- TFP(2,2)    +--- TFP(3,2)  
 X--- TFP(4,2)



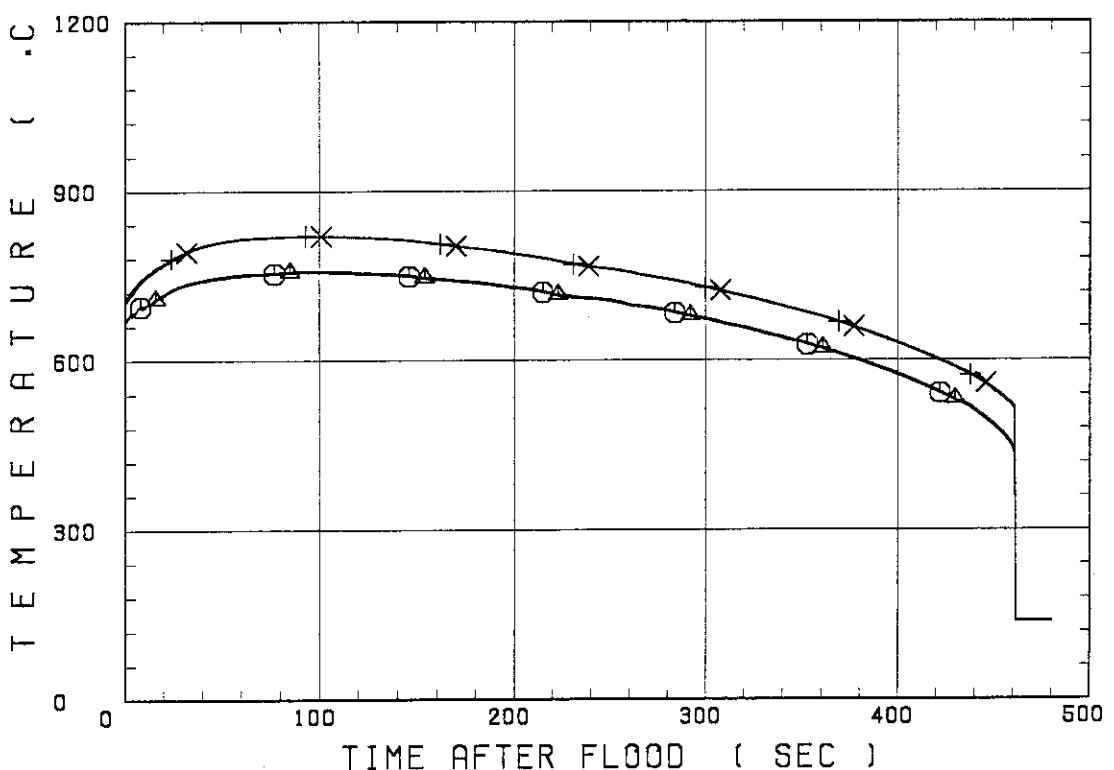
\*\* REFLAP5 RUN ( IOPT = 1,1 ) \*\*  
 CCTF CORE-I ( RUN 38 , BUNDLE 17 )

○--- TFP(1,3)    △--- TFP(2,3)    +--- TFP(3,3)  
 X--- TFP(4,3)



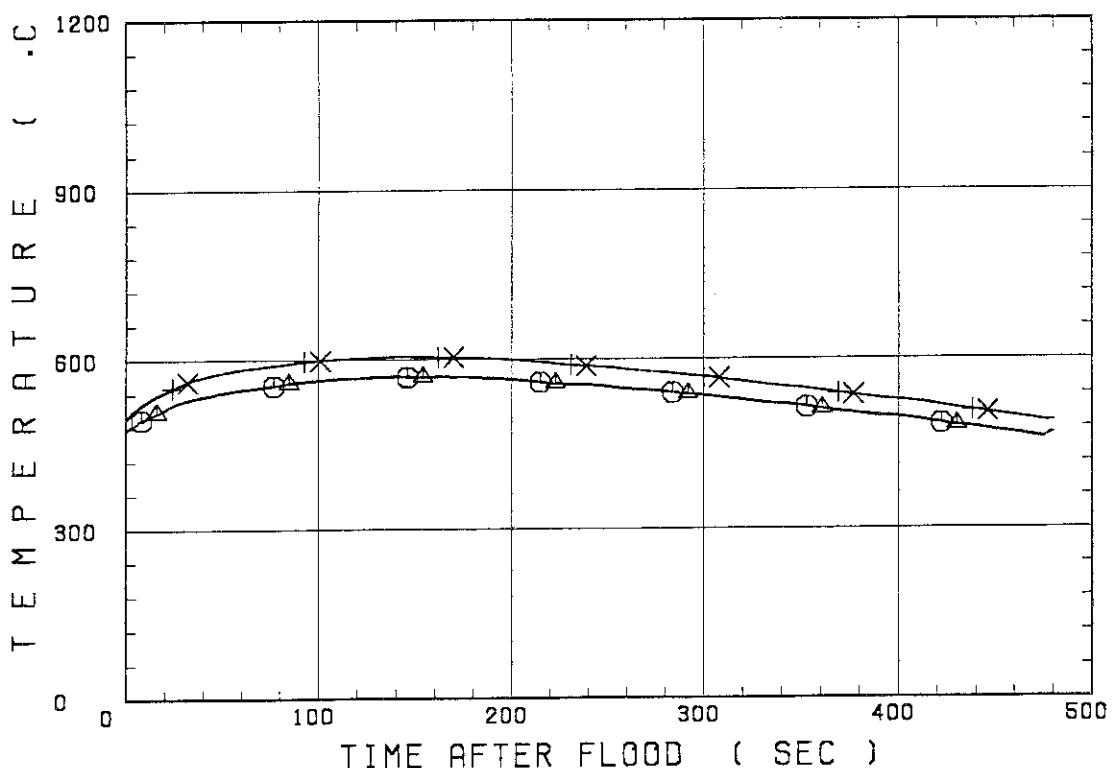
\*\* REFLAP5 RUN ( IOPT = 1,1 ) \*\*  
 CCTF CORE-I ( RUN 38 , BUNDLE 17 )

○--- TFP(1,4)    △--- TFP(2,4)    +--- TFP(3,4)  
 X--- TFP(4,4)

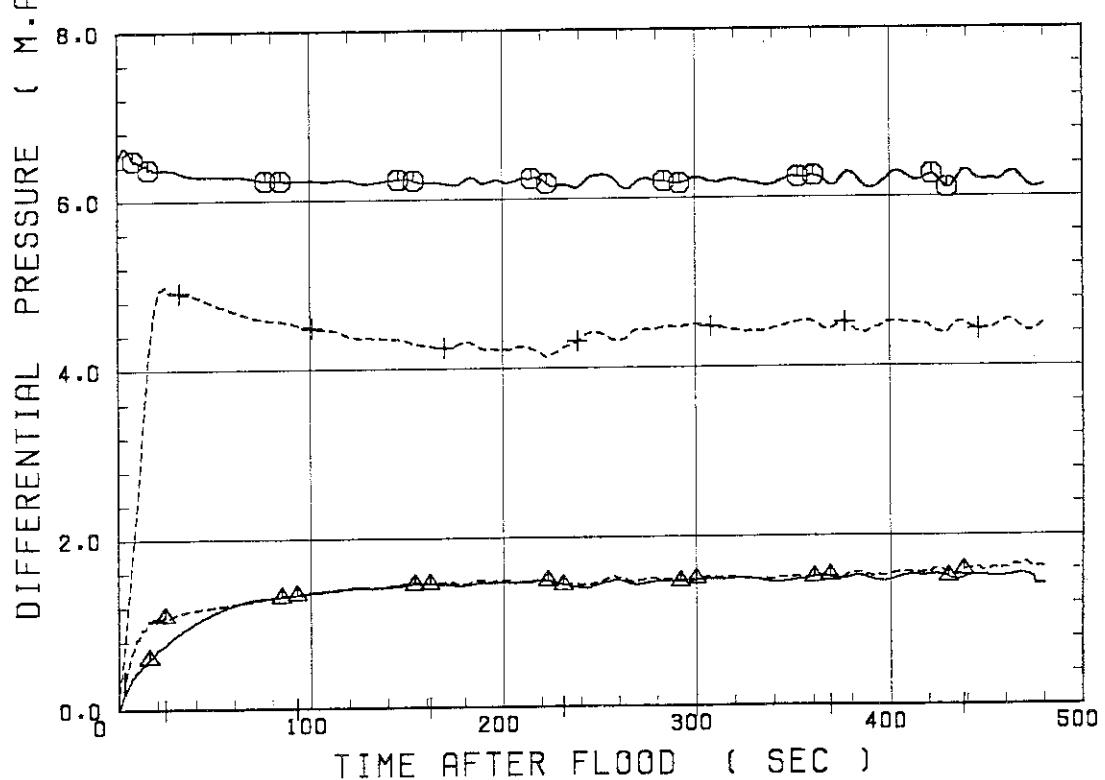


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\*\* REFLAPS RUN ( IOPT = 1,1 ) \*\*  
CCTF CORE-I ( RUN 38 , BUNDLE 17 )  
○--- TFP(1.5)    △--- TFP(2.5)    +--- TFP(3.5)  
X--- TFP(4.5)

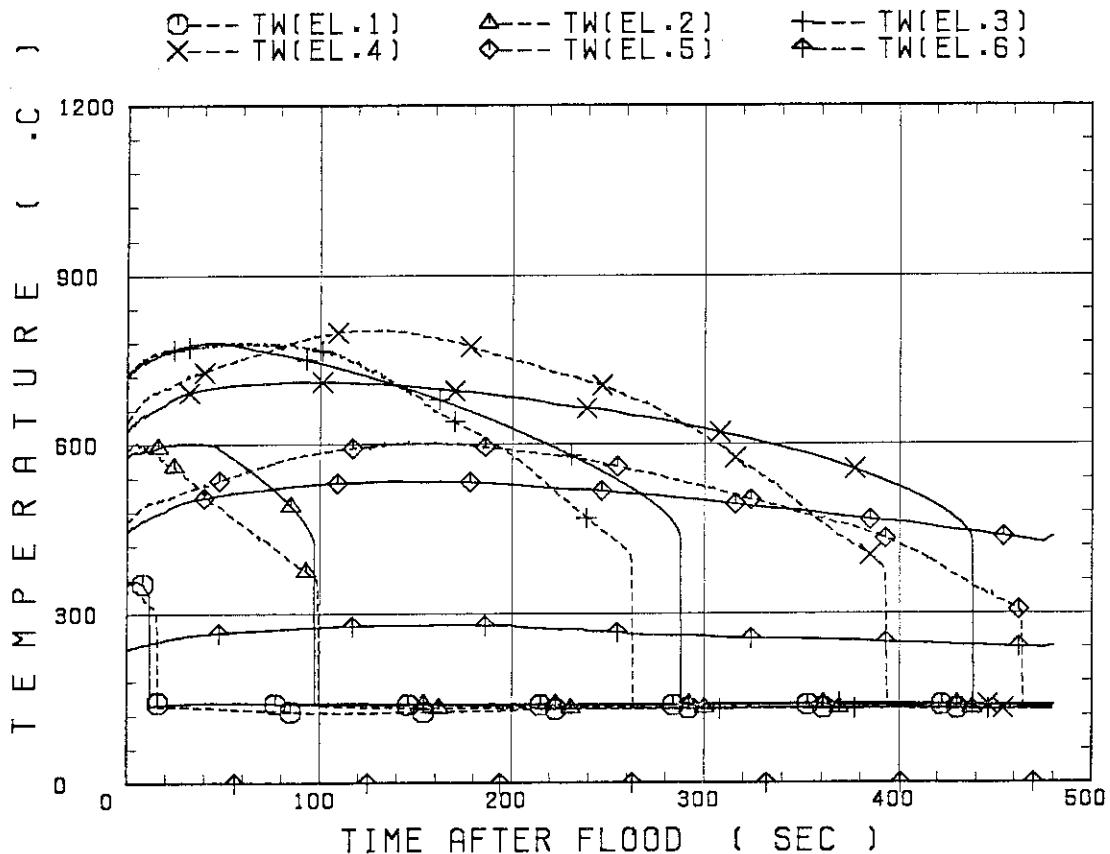


\*\* REFLAPS RUN ( IOPT = 1,1 ) \*\*  
CCTF CORE-I ( RUN 38 , BUNDLE 17 )  
○--- UL1/5+6    △--- PC1-PCN1    +--- DPDWN

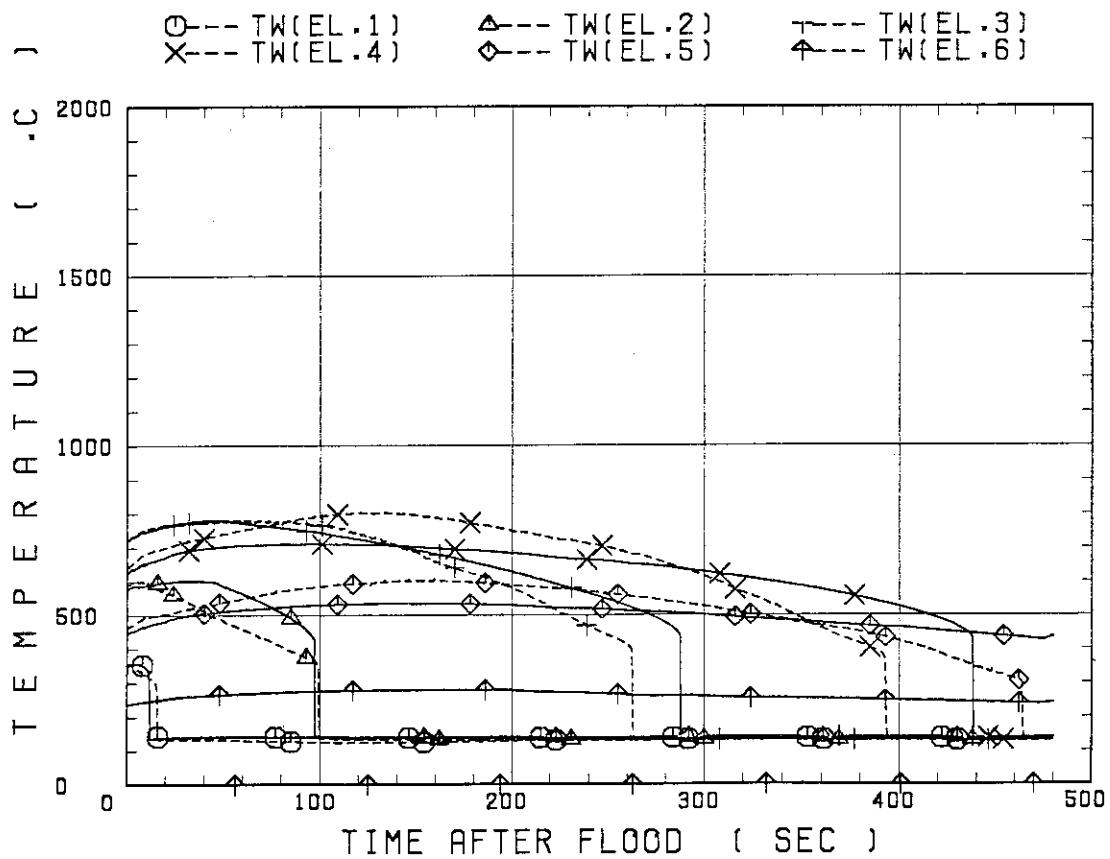


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\*\* REFLAP5 RUN ( IOPT = 1,1 ) \*\*  
CCTF CORE-I ( RUN 38 , BUNDLE 17 )

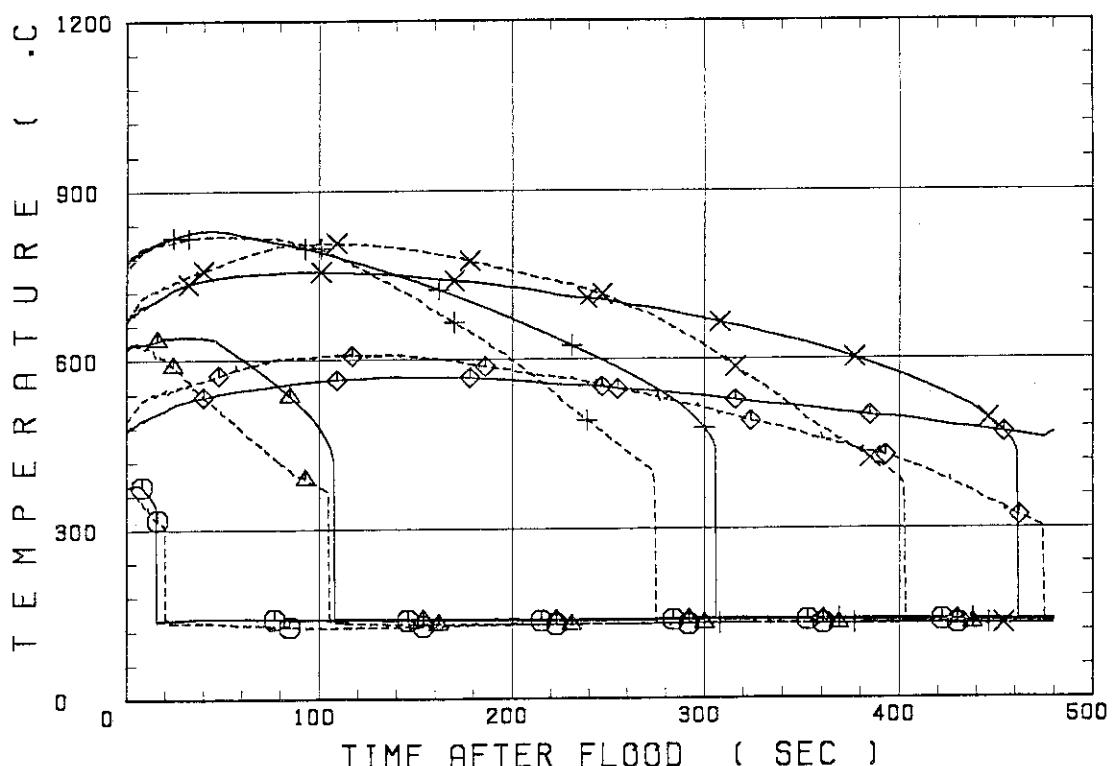


\*\* REFLAP5 RUN ( IOPT = 1,1 ) \*\*  
CCTF CORE-I ( RUN 38 , BUNDLE 17 )



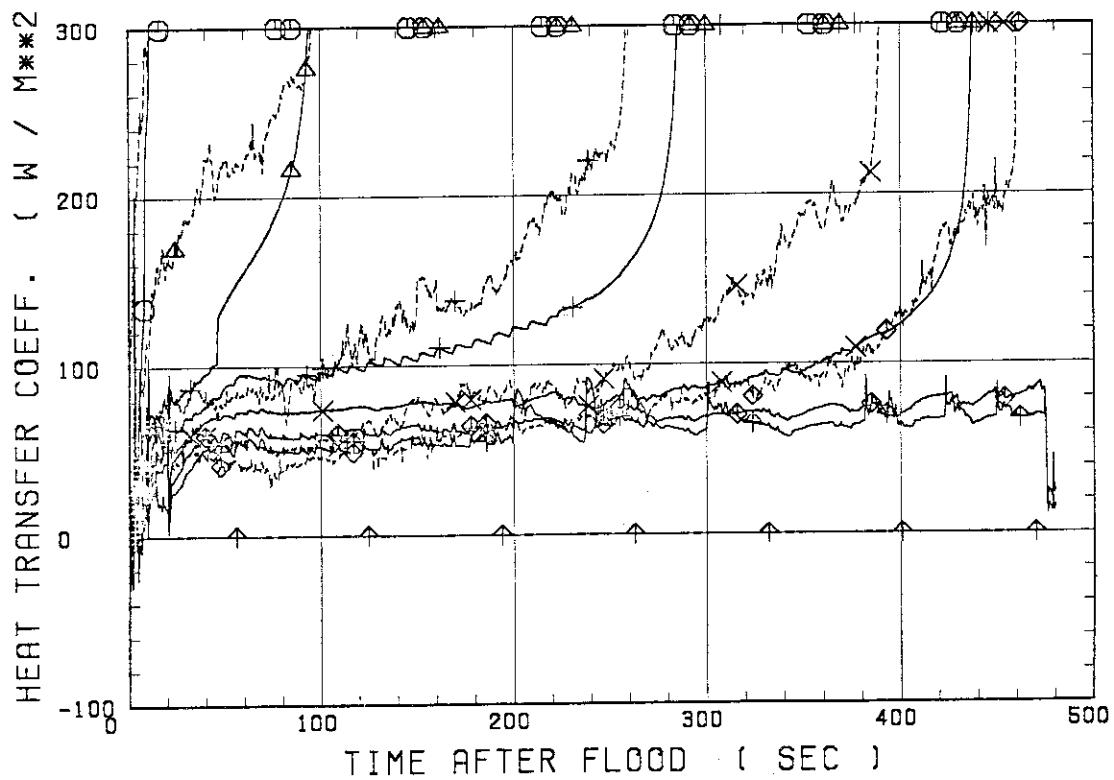
\*\* REFLAP5 RUN ( IOPT = 1,1 ) \*\*  
 CCTF CORE-I ( RUN 38 , BUNDLE 17 )

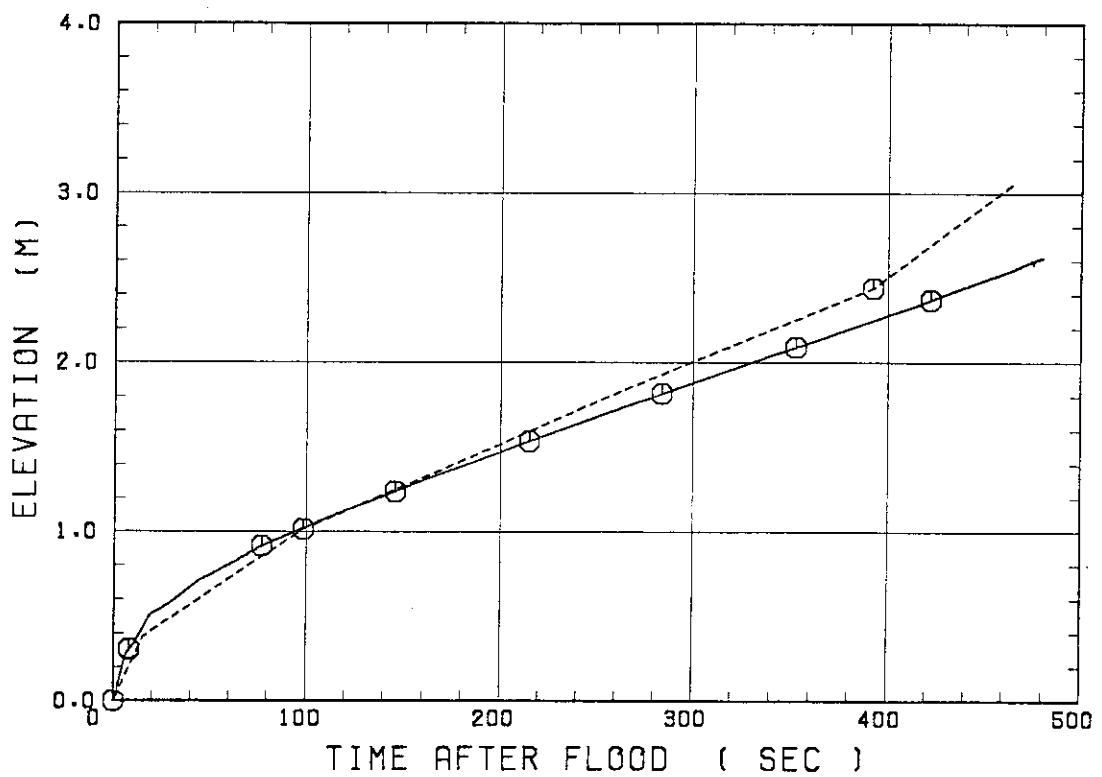
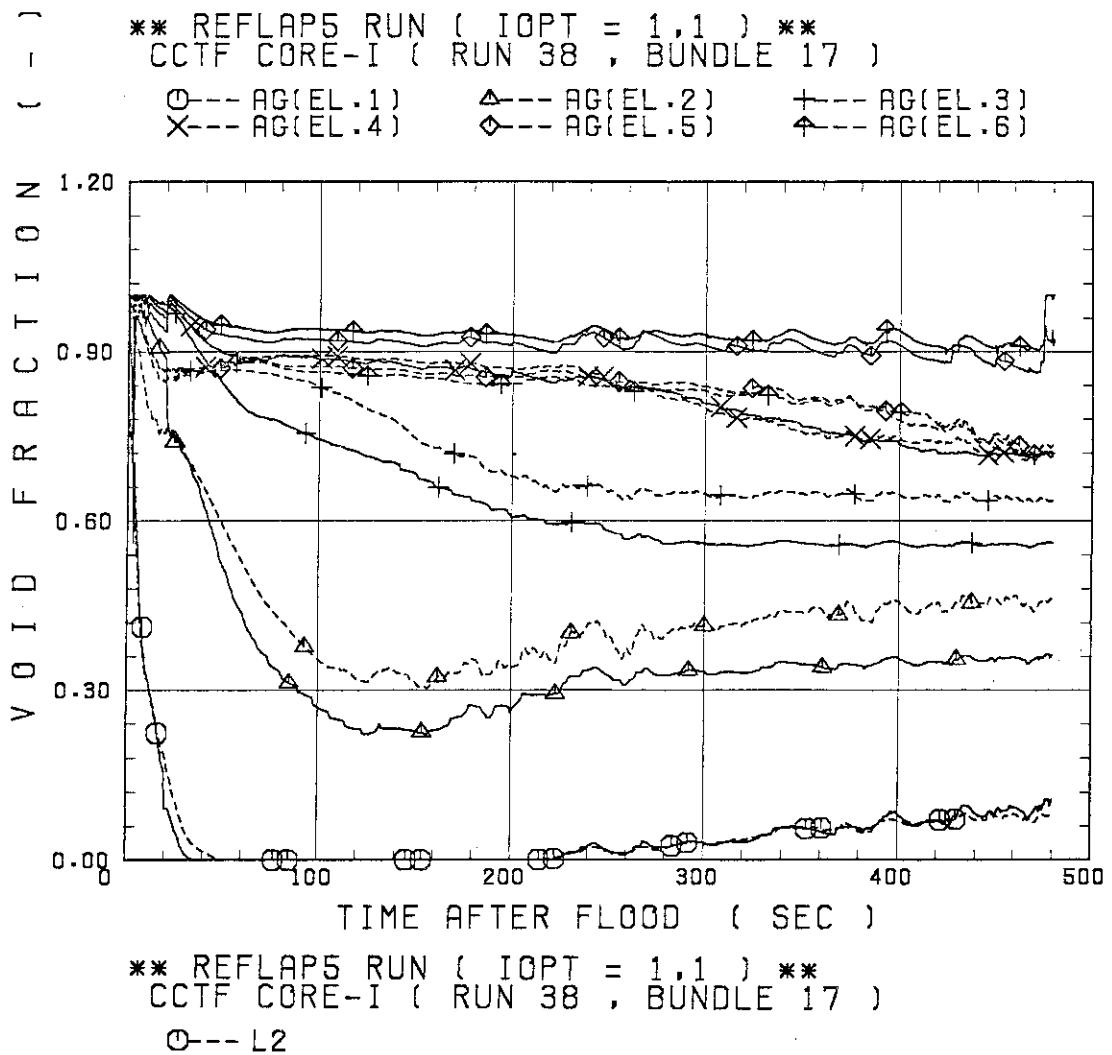
( O--- TWP(EL1) ) ( ▲--- TWP(EL2) ) ( +--- TWP(EL3) )  
 ( X--- TWP(EL4) ) ( ◆--- TWP(EL5) )



\*\* REFLAP5 RUN ( IOPT = 1,1 ) \*\*  
 CCTF CORE-I ( RUN 38 , BUNDLE 17 )

( O--- HT(EL.1) ) ( ▲--- HT(EL.2) ) ( +--- HT(EL.3) )  
 ( X--- HT(EL.4) ) ( ◆--- HT(EL.5) ) ( ↑--- HT(EL.6) )





\*\* REFLAP5 RUN ( IOPT = 1,1 ) \*\*  
CCTF CORE-I ( RUN 38 , BUNDLE 17 )

○--- LP2

