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TRANSPORT ANALYSIS OF OH AND NBI  
HEATED DISCHARGES IN JT-60

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Transport Analysis of OH and NBI Heated Discharges in JT-60

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Transport properties of ohmically and NBI heated plasmas in JT-60 have been analysed by using the one-dimensional tokamak transport code. The very flat density profiles observed in ohmic heating discharges are explained by no inward flow velocity of hydrogen. The saturation of the energy confinement time at high density discharges is due to the increase of the ion energy loss channel and the combination of the neoclassical ion heat diffusivity  $\chi_i^{CH}$  with multiplication factor of around 6 and the electron heat diffusivity  $\chi_e = 5 \times 10^{19} / n_e q$  well reproduces experimental data in the density range of  $\bar{n}_e = (2 \sim 8) \times 10^{19} \text{ m}^{-3}$ . The analysis also shows that the electrical conductivity has the Spitzer-type dependence and the trapped electron correction is small. The degradation of the energy confinement under the high power NBI heating is due to the enhancement of electron heat diffusivity. For discharges with 20 MW NBI heating, electron heat diffusivity increases to  $\chi_e = 5 \text{ m}^2/\text{s}$  at  $\bar{n}_e = 5 \times 10^{19} \text{ m}^{-3}$ . By taking into account the beam pressure, it was also shown that stored energies evaluated by the magnetic analysis is consistent with the value evaluated from the transport analysis.

Keywords: Tokamak, JT-60, Ohmic Heating, NBI Heating, Energy Confinement Time, Resistivity, LOOK, SCOOP, LIBRARY

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OH及びNBI加熱時のJT-60プラズマの輸送解析

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(1987年1月30日受理)

一次元トカマク輸送コード・シミュレーションによって、JT-60におけるOH及びNBI加熱プラズマの輸送特性を解析した。

OHプラズマにおけるエネルギー閉じ込め時間のプラズマ密度上昇に伴う飽和現象は、イオン系からのエネルギー損失が支配的となるためであり、イオン熱伝導率が新古典理論の6倍程度あると仮定すると、計算結果は実験結果を良く表現できる。又、プラズマの電気伝導率は古典的であり、捕捉電子効果は小さいことが示された。

NBI加熱に伴うエネルギー閉じ込め時間の劣化は、電子熱伝導率の増加によるものであり、20 MW入射の場合、 $\chi_e$ の値は $5 \text{ m}^2/\text{s}$  ( $\bar{n}_e = 5 \times 10^{19} \text{ m}^{-3}$ )迄増大している事がわかった。又、ビーム粒子のエネルギー密度を考慮すると、平衡から評価された蓄積エネルギーとプラズマ密度及び温度から評価した蓄積エネルギーは良い一致をみる事が示された。

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## Contents

1. Introduction .....	1
2. Ohmically Heated Discharges .....	1
2.1 Experimental data .....	1
2.2 Plasma Resistivity during quasi-steady State .....	4
2.3 Simulation of Ohmically Heated Plasmas .....	5
3. Simulation of NBI Heated Plasmas .....	8
4. Summary .....	11
Acknowledgements .....	11
References .....	12

## 目                    次

1. 序論.....	1
2. OH加熱時のプラズマ.....	1
2.1 実験データ.....	1
2.2 準定常時のプラズマ電気抵抗.....	4
2.3 OH加熱されたプラズマの数値計算.....	5
3. NBI加熱されたプラズマの数値計算.....	8
4. 総括.....	11
謝辞.....	11
参考文献.....	12

## 1. Introduction

The study of plasma confinement in a large tokamak is the key issue of the fusion reactor development. In JT-60, ohmically and neutral beam heated plasmas have been extensively studied in the wide range of plasma density and heating power [1,2,3]. The line averaged electron density has been stably increased up to  $\bar{n}_e = 8 \times 10^{19} \text{ m}^{-3}$  in ohmic discharges and the neutral beam power was increased up to 20 MW with plasma current of  $I_p = 1.0 \sim 2.0 \text{ MA}$ . Clean plasmas with effective charge number of  $Z_{eff} = 1 \sim 2$  and flat density profiles were obtained both for divertor and limiter discharges. The confinement analysis shows that the gross energy confinement time of the ohmically heated plasma saturates at density  $\bar{n}_e \sim 4 \times 10^{19} \text{ m}^{-3}$  and is weakly dependent on the plasma density and the plasma current above this threshold density. The neutral beam heating degrades the energy confinement with heating power as L-mode discharges but the dependence of the confinement time on the plasma density and the plasma current is still very weak as the one in ohmic discharges [4].

In this paper, we study the above-mentioned confinement properties of ohmically and neutral beam heated plasmas in JT-60 from the viewpoint of transport code analysis. In the next section, we analyse the transport process in ohmic discharges. The density profile and the effective charge number of the plasma are also studied in this section. In the section 3, discharges under high power NBI heating are analysed. And results of transport simulation in JT-60 are summarized in the section 4.

## 2. Ohmically Heated Discharges

### 2.1 Experimental data

The experimental data are taken by selecting a plasma current  $I_p$  and the scanning a range of the line averaged electron density  $\bar{n}_e$  up to  $\sim 8 \times 10^{19} \text{ m}^{-3}$  for ohmically heated plasmas in JT-60. Hydrogen and helium plasmas are chosen for the various density scans in the divertor or limiter discharges. In this session, we will present the profile characteristics of the electron temperature and density and the energy



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confinement properties for ohmically heated plasmas.

Figure 1 shows the variation of central electron temperature and resistive voltage  $V_p$  with the line averaged electron density. The central electron temperature rapidly decreases as the density increases to around  $2\sim 3 \times 10^{19} \text{ m}^{-3}$  and is gradually on the decay above that density. The resistive voltage becomes to be high  $\sim 0.6V$  to  $\sim 1V$  with the density but does not show the non-linear increase. The resistive voltage which is important to estimate the ohmic input power accurately is defined by

$$V_l = V_p + \frac{1}{2} I_p L_i \quad (1)$$

where  $V_l$  is the loop voltage and  $L_i$  the internal inductance. Although the discharge duration of JT-60 is about 10 sec, the effect of temporal evolution of  $L_i$  can not be neglected at a high plasma current (2 MA), leading to an uncertainty in the  $V_p$  of less than 10 %, except for discharges with a large  $\dot{n}_e$ . From Shafranov  $\Lambda (= \beta_p + l_i/2)$  measured by the equilibrium, the time derivative of  $L_i$  is expressed as

$$\dot{L}_i = \mu_0 R (\dot{\Lambda} - \dot{\beta}_p) \quad (2)$$

where  $\mu_0$  is the vacuum permeability, R the major radius and  $\beta_p$  the beta poloidal. The time evolution of  $\beta_p$  is approximated by

$$\dot{\beta}_p = \int_0^a (\dot{p}_e(r) + \dot{p}_i(r)) dV / (VB_p^2 / 2\mu_0) \quad (3)$$

$$\dot{p}_e(r) = \dot{n}_e(0) f_{ne}(r) T_e(r) + n_e(r) \dot{T}_e(0) f_{Te}(r),$$

$$\dot{p}_i(r) = \dot{n}_i(0) f_{ni}(r) T_i(r) + n_i(r) \dot{T}_i(0) f_{Ti}(r),$$

where  $\dot{n}_e(0)$  and  $\dot{T}_e(0)$  are measured by FIR and ECE diagnostics, respectively, and  $f_n(r)$  and  $f_T(r)$  are normalized profiles for density and temperature. The time derivative of ion pressure is approximated from electron parameters, assuming  $\dot{T}_i(0) = \dot{T}_e(0)$  and  $\dot{n}_i(0) = \dot{n}_e(0)$ .

The change of the electron temperature profile and the electron

density profile are shown in Fig.2 as a function of the electron density. The axis of ordinates presents the ratio of the central to the volume averaged. The electron temperature profile does not change up to a high density of  $\sim 8 \times 10^{19} m^{-3}$ , though indicating the amount of scatter large in the low density. At the low density, the electron density profile for the limiter discharge is more peaked than the one for the divertor discharges. With the increment of the density, both profiles become broad and show no remarkable difference in their shapes.

We can now calculate the energy confinement time defined as

$$\tau_E = \frac{W_e + W_i}{V_p I_p - (W_e + W_i)}, \quad (4)$$

where  $W_e$  and  $W_i$  are, respectively, kinetic energies of the electrons and ions integrated over the plasma volume. The experimental profiles of  $T_e$  and  $n_e$  are input to the time independent code LOOK/SCOOP [5] together with the global parameters  $I_p, V_i, B_t$ , etc. In the steady transport analysis, ion temperature profile is calculated by employing the neoclassical ion heat diffusivity proposed by Chang-Hinton [6] with the enhancement factor of 3. The power transport from the electrons to the ions is calculated by the classical formula. The power loss due to convection is obtained from the inferred particle flux and the charge exchange loss from the neutral penetration calculation with assumed particle confinement time of 100 ms. Ion density depletion is estimated by using the resistive  $Z_{eff}$  (see §2.2) and by assuming carbon is the only impurity. Figure 3 shows the dependence of  $\tau_E$  on electron density and  $\tau_E^* = \bar{n}_e R^2 a q_{cy}$  scaled with Neo-Alcator, where  $a$  is the minor radius and  $q_{cy}$  the cylindrical safety factor. It is seen from these figures that  $\tau_E$  saturates at about 0.4 sec above around  $n_e \sim 4 \times 10^{19} m^{-3}$  or  $\tau_E^* = 1 \times 10^{21}$ . There are little differences in the energy confinement times between hydrogen and helium plasmas and also between limiter and divertor discharges. Although  $\tau_E$  observed in JET [7] linearly increases with  $\tau_E^*$ , the data of TFTR [8] begin to saturate at  $\tau_E^*$  of  $0.5 \times 10^{21}$  and present the  $\tau_E$  of  $\sim 0.4$  sec, which is almost the same value as the one in JT-60.

## 2.2 Plasma Resistivity during quasi-steady State

The plasma resistivity  $\eta_{//}$  in the quasi-steady state is important in determining the electron energy balance. As have been mentioned uncertainties in the plasma resistivity [9,10,11,12], two kinds of formula are used i.e. Spitzer resistivity and the neoclassical one with trapping correction [13]. In the calculation of the resistivity,  $Z_{eff}$  is obtained by iteration to obtain agreement with the ohmic input power, followed by

$$I_p V_p = \int_0^a \eta_{//}(Z_{eff}, T_e(r)) J_z(r)^2 dV, \quad (5)$$

in which  $J_z(r)$  is the toroidal current density. In the following, we have used the two types of current density profile. The first one is estimated from the usual assumption of the constant electric field over the radius,

$$J_z(r) = \frac{E_z}{\eta_{//}(Z_{eff}, T_e(r))}. \quad (6)$$

Another model of  $J_z(r)$  is represented by

$$J_z(r) = J_0 \left(1 - \left(\frac{r}{a}\right)^2\right)^\alpha. \quad (7)$$

The central current density  $J_0$  is given by assuming  $q(0)=1$  and the value of  $\alpha$  is obtained by making the internal inductance meet to the measured one. As using the eq.(6), large amount of scatter of  $T_e(r)$  at the low density (Fig.2) lead to an uncertainty in the resistive  $Z_{eff}$ . Therefore, the eq.(7) is employed through this work. Both resistive  $Z_{eff}$  from two different  $J_z$  agree well, as reducing the scatter of  $T_e(r)$  at the high density.

The dependence of resistive  $Z_{eff}$  on the electron density is shown in Fig.4. As using the Spitzer formula, the resistive  $Z_{eff}$  rapidly decreases with the increase of electron density from  $1 \times 10^{19} m^{-3}$  to  $2 \sim 3 \times 10^{19} m^{-3}$  and shows the reasonable values less than 1.5 ( $\bar{n}_e \geq 4 \times 10^{19} m^{-3}$ ). On the other hand, the neoclassical resistivity

results in  $Z_{eff} < 1$  in hydrogen discharges and  $Z_{eff} < 2$  in helium discharges, as shown in Fig. 4-b. Especially at the high density, some discharges frequently failed to estimate the resistive  $Z_{eff}$ , because the value of  $Z_{eff}$  is so small that the trapping correction becomes to be negative. In order to make  $Z_{eff}$  value of 0.5 above unity, the electron temperature must increase by 60%. This fact is apparently out of the error for the electron temperature. Figure 5 shows the value of  $Z_{eff}$  measured by visible bremsstrahlung [3] as a function of the electron density at  $I_p = 1.0 \sim 1.5$  MA for the divertor discharges and the limiter discharges. The measured  $Z_{eff}$  shows the good agreement with the resistive  $Z_{eff}$  from Spitzer formula. These results strongly suggest that the trapped particle correction to the resistivity should be reduced or suppressed.

### 2.3 Simulation of Ohmically Heated Plasmas

The computer simulation are carried out with the LIBRARY transport code [14] and concentrate more on the flat density profile and the saturated energy confinement time.

In many other tokamaks, the experimentally observed profiles of electron densities have a nearly parabolic or Gaussian shape in the inner region of the plasma column. An anomalous inward flux of the form  $-2n_e D r / a^2$  [15] is introduced and successfully explains such density profiles. In JT-60, flat density profiles showing  $n_e(0) / \langle n_e \rangle = 1.1 \sim 1.2$  are realized for middle- and high density discharges, though peaked profiles like a parabolic shape are seen in limiter discharges at the low density. The characteristics of the density profiles are satisfactorily simulated with no anomalous inward flux and differences in cold neutral energy. In Figs 6 and 7, computed density profiles are compared with the measurements. The anomalous inward flux (shown in broken-line) leads to more peaked density profiles for both limiter and divertor discharges. The differences in cold neutral energies i.e.  $E_0 = 5eV$  for divertor discharges and  $E_0 = 30eV$  for limiter discharges, could be responsible for the observed differences in  $n_e$  profiles at low densities. This is because that cold neutrals which directly recycle with limiter have a higher energy of

dozens to hundred eV.

There are some candidates for the saturated energy confinement time. 1) Impurity radiation: Since the impurity radiation power for the divertor discharges is only 20~30 % of the input power, the radiation losses due to impurities should not be responsible for the  $\tau_E$  saturation. 2) Convection loss : In a transient stage , the large diffusion coefficient of  $\sim 1 \text{ m}^2/\text{s}$  was observed. This large diffusion coefficient is not employed in our simulation study, because there are no inward flux which must compensate for the large outward flux due to the large diffusion. 3) Electron heat diffusivity  $\chi_e$  : Figure 8 shows the electron heat diffusivity  $\chi_e^E$  estimated at  $a/3$  for the observed profiles of the electron temperature and density for the plasma current of 2.0 MA, in which ion conduction loss is fixed to be 3 times the neoclassical ion heat diffusivity of Chang-Hinton and convection loss  $3/2\Gamma$ . The INTOR scaling  $\chi_e$  of  $5 \times 10^{19}/n_e$  and the  $\chi_e^{HP}$  measured by the heat pulse of the sawtooth are also shown in this figure. The  $\chi_e^E$  is almost the same as  $\chi_e^{HP}$ . It is reported that the  $\chi_e^{HP}$  is greater than the  $\chi_e^E$  by a factor of 10, because of including the convection loss [16]. Therefore, the  $\chi_e$  can not be enhanced so as to cause the  $\tau_e$  saturation. 4) Ion heat diffusivity  $\chi_i$  : Figure 9 presents the experimental profile of the electron density and temperature for the shot of E1791 with  $I_p=1.5 \text{ MA}$ . As the factor of 6 for  $\chi_i^{CH}$  is taken, the  $\chi_i$  is the same as the  $\chi_e^E$  over the radius. This result shows that the ion energy loss catches up with the electron energy loss at the high density regime and also suggests that the enhanced ion heat diffusivity may be responsible for the  $\tau_E$  saturation.

Figure 10 shows the simulation results for E1791 ( $I_p=1.5 \text{ MA}$ ) based on the following empirical transport coefficients,

$$\chi_e = 5 \times 10^{19} / n_e q_{cy},$$

$$\chi_i = 6 \chi_i^{CH},$$

$$D = 1 \times 10^{19} / n_e,$$

Spitzer resistivity,

Spitzer resistivity,  
 no anomalous inward flux,  
 cold neutral energy of 5 eV.

The plasma profiles at the low density of  $2.5 \times 10^{19} \text{m}^{-3}$  are presented in Fig. 10-a ; the temperature profiles of electron and ion, the profiles of electron density and safety factor  $q$ . Figure 10-b shows the profiles at the high density of  $6.6 \times 10^{19} \text{m}^{-3}$ . The calculated electron temperature profiles are in good agreement with the observed temperature denoted in open circles, although the central temperature is slightly decreased due to the sawtooth effect.

Figure 11 shows the simulation results for 2MA discharge (E1709) based on the same transport mentioned above. Figures 11-a and -b correspond to the cases at the density of  $6.0 \times 10^{19} \text{m}^{-3}$  and of  $7.5 \times 10^{19} \text{m}^{-3}$ , respectively. The used transport parameters yield good fits with the observed  $T_e$  profiles within error bars.

We show the  $\tau_E$  versus the electron density, comparing with the calculated  $\tau_E$  shown in solid lines in Fig. 12. As for the plasma parameters with  $I_p=2.0\text{MA}$ , in Fig. 12-a, the calculated  $\tau_E$  is good agreements in the experimental values at the low density ( $\bar{n}_e \leq 3 \times 10^{19} \text{m}^{-3}$ ) and shows a tendency toward the saturation. As for the plasma with  $I_p=1.5\text{MA}$ , in Fig. 12-b, the calculated  $\tau_E$  also shows good agreement with the experiments on both the  $\tau_E$  value and the tendency of the  $\tau_E$  saturation. The assumption that ion loss channel becomes dominant in energy loss channels at the high density brings about good agreement with the experimental measurements.

### 3. Simulation of NBI Heated Plasmas

The degradation of the electron diffusivity  $\chi_e$  during NB heating phase is estimated by using the tokamak transport code. The power deposition profile of the Neutral Beam Injection and the stored fast ion energy are calculated in detail by using the Orbit Following Monte Carlo code (OFMC code) [5]. We also estimated the charge exchange loss of fast ion for various neutral density profiles.

We analyzed a series of helium discharge with the beam power  $P_b=10$  MW and a series of hydrogen discharge with  $P_b=20$  MW. Time evolution of the parameters for relatively high density discharge  $\bar{n}_e=5.4 \times 10^{19} m^{-3}$  and low density discharge  $\bar{n}_e=2.4 \times 10^{19} m^{-3}$  are shown in Fig. 13 and Fig. 14, respectively. In both discharges, we observed the rapid saturation of the central electron temperature and the plasma stored energy estimated from the magnetic equilibrium measurement.

The local transport analysis assumed steady state (SCOOP result) shows that the electron heat diffusivity  $\chi_e$  during NBI heating is about  $3 \sim 5 m^2/s$  [4]. These estimated values are very sensitive to the local gradient of electron temperature  $dT_e/dr$ . It is difficult to determine  $dT_e/dr$  from the 6-point Thomson scattering measurement with 10~20 % error bars. So we estimated the electron heat diffusivity during NBI heating by using the prediction transport code.

The procedure of the simulation is as follows:

- (1) The density profile is determined from 3-ch FIR data. Instead of solving the particle balance equation, this density profile is used in the simulation.
- (2) The energy transfer from fast ions to bulk electron and ions are calculated by OFMC code. In this calculation the experimental data is used for plasma parameter, such as  $n_e$  and  $T_e$ . The neutral density profile is calculated by 2-Dimensional Neutral transport code [17]. The absolute value is determined assuming that the particle confinement time is 50 msec.
- (3) We solve the time-dependent equations of electron and ion energy balance employing the INTOR scaling for the anomalous diffusion;

$$D=10^{19}/n_e$$



$$\chi_e = 5 \times 10^{19} / n_e$$

$$\chi_i = 3 \times \chi_i^{CH}$$

- (4) The electron heat diffusivity during NBI heating  $\chi_e^{NB}$  is enhanced by a factor 2-4.

$$\chi_e^{NB} = f_e \times \chi_e^{INTOR}$$

At first, we carried out the simulation for helium discharge with  $P_b=10$  MW. The content ratio of hydrogen ion in helium plasma is not clear. But the amount of the beam shine through in helium discharge is less than that in hydrogen discharge with same densities. This fact indicates that the helium ion content is larger than hydrogen ion. So the density ratio of helium and hydrogen  $n_{He}/n_H$  is assumed to be 2.0 in the calculation of beam deposition. We used the cross section for  $He^{++}$  ionization which scales as  $Z^2$  times the proton ionization, where  $Z$  is the charge number of ion [18].

Figure 15(a) shows the density dependence of the stored energy of fast ions. The incremental stored energy estimated from the magnetic measurement  $\Delta W_{mag}$ , which include the contribution from the fast ions, and the incremental kinetic energy calculated from the plasma parameters  $\Delta W_{kin}$  are also plotted in this figure. The ratio of beam components to the incremental stored energy decreases with the electron density. For low density discharges with  $\bar{n}_e < 3 \times 10^{19} m^{-3}$ , the beam component is dominant in the incremental stored energy. The agreement between the thermal energy estimated from the magnetic measurement and from the kinetic method is fairly good. The density dependence of the partition of beam power is shown in Fig 15(b). For low density discharge with  $\bar{n}_e < 2 \times 10^{19} m^{-3}$ , the major part of the beam power is lost by the shine-through and the charge exchange loss. The power deposited from the fast ions to the electrons is larger than that to the bulk ions because of the low electron temperature.

The charge exchange loss reduces the power deposited to ions. We estimated the C.X. loss for the various neutral density profile. The results are summarized in Table 1. When the particle confinement time  $\tau_p$  is reduced from 50 msec to 30 msec, the C.X. loss increases from 12 % to 16 %. The change of neutral density profile due to the neutral energy is insignificant for the C.X. loss. In JT-60 divertor discharges, recycling neutrals are localized at the divertor side. This asymmetric neutral profile has no influence on C.X. loss. Figure

16 shows the density profile of halo neutral and recycling neutral. Halo neutrals contribute only to the neutral density at center and the recycling neutral dominate outer region. Most of the fast particle neutralized at center region are reionized. Therefore, the C.X. loss due to halo neutrals is negligible.

Figure 17 shows the power deposition profile calculated by OFMC code for E2151 and E2154 discharge. The deposition profile is hollow even for the low density discharge due to the off-axis injection and the very flat density profile.

Figure 18 shows the simulation result for E2154 discharge ( $\bar{n}_e = 5.4 \times 10^{19} \text{ m}^{-3}$ ,  $P_B = 10 \text{ MW}$ ). We used the enhanced electron heat diffusivity  $\chi_e^{NB} = 2. \times \chi_e^{INTOR}$  during NBI heating. The electron temperature measured by Thomson Scattering at  $t = 6.4$  sec shows by the closed symbol. The simulation result is in good agreement with the experimental data. The broad temperature profile is due partly to the hollow deposition profile and partly to the homogeneous thermal diffusion  $\chi_e$  in the core region.

Figure 19 shows the simulation result for E2151 discharge ( $\bar{n}_e = 2.4 \times 10^{19} \text{ m}^{-3}$ ,  $P_B = 10 \text{ MW}$ ). This result indicated that the enhancement factor for low density must be smaller than 2 in order to reproduce the experimental data. As for the ion temperature, there is a possibility of the degradation of the ion energy confinement during NBI heating. However, it should be noted that the ion temperature measured by the doppler broadening of TiXXI is not always coincident with the central bulk ion temperature. Impurity transport analysis point out that the doppler broadening evaluate the central ion temperature too lower according to the impurity density profile [19].

So we did not make an effort to investigate the degradation of ion thermal diffusivity.

We also executed the simulation for the hydrogen discharge with high beam power  $P_B = 20 \text{ MW}$ . The incremental stored energy  $\Delta W_{mag}$  and the stored fast ion energy  $W_b$  for several density scan are plotted in Fig. 20(a). Figure 20(b) shows the density dependence of the partition of beam power. In order to keep the shine through below 10 %, the line density must be higher than about  $5 \times 10^{19} \text{ m}^{-3}$ . Figure 21 shows the experimental result and the simulation result by using  $\chi_e^{NB}$  enhanced by a factor 4. INTOR scaling can not reproduce the density dependence of

the central electron temperature. In the high density region of  $\bar{n}_e > 6 \times 10^{19} m^{-3}$ , the difference between the simulation and the experiment is significant. This fact implies that the electron heat diffusivity during NBI phase has weak density dependence. In the middle density region of  $\bar{n}_e = 5 \times 10^{19} m^{-3}$ , where  $\chi_e$  about  $5 m^2/s$ , the simulation agrees with the experimental data fairly well. Comparing with the simulation of helium discharge with 10 MW,  $\chi_e^{NB}$  seems to degrade with the beam power. We can conclude that the degradation of the confinement during NBI heating is due to enhanced electron heat diffusivity.

#### 4. Summary

Transport properties of ohmically and NBI heated plasmas in JT-60 have been analysed by using the one-dimensional tokamak transport code. The very flat density profiles observed in ohmic heating discharges are explained by no inward flow velocity of hydrogen. The saturation of the energy confinement time at high density discharges is due to the increase of the ion energy loss channel and the combination of the neoclassical ion heat diffusivity  $\chi_i^{CH}$  with multiplication factor of around 6 and the electron heat diffusivity  $\chi_e = 5 \times 10^{19}/n_e q$  well reproduces experimental data in the density range of  $\bar{n}_e = (2 \sim 8) \times 10^{19} m^{-3}$ . The analysis also shows that the electrical conductivity has the Spitzer-type dependence and the trapped electron correction is small. The degradation of the energy confinement under the high power NBI heating is due to the enhancement of electron heat diffusivity. For discharges with 20 MW NBI heating, electron thermal conductivity increases to  $\chi_e = 5 m^2/s$  at  $\bar{n}_e = 5 \times 10^{19} m^{-3}$ . By taking into account the beam pressure, it was also shown that stored energies evaluated by the magnetic analysis is consistent with the value evaluated from the transport analysis.

#### Acknowledgements

The authors wish to thank Drs. Y. Shimomura and M. Azumi for fruitful discussions. The continuing support of Drs. S. Mori, K. Tomabechi, M. Yoshikawa and T. Iijima, is gratefully acknowledged.

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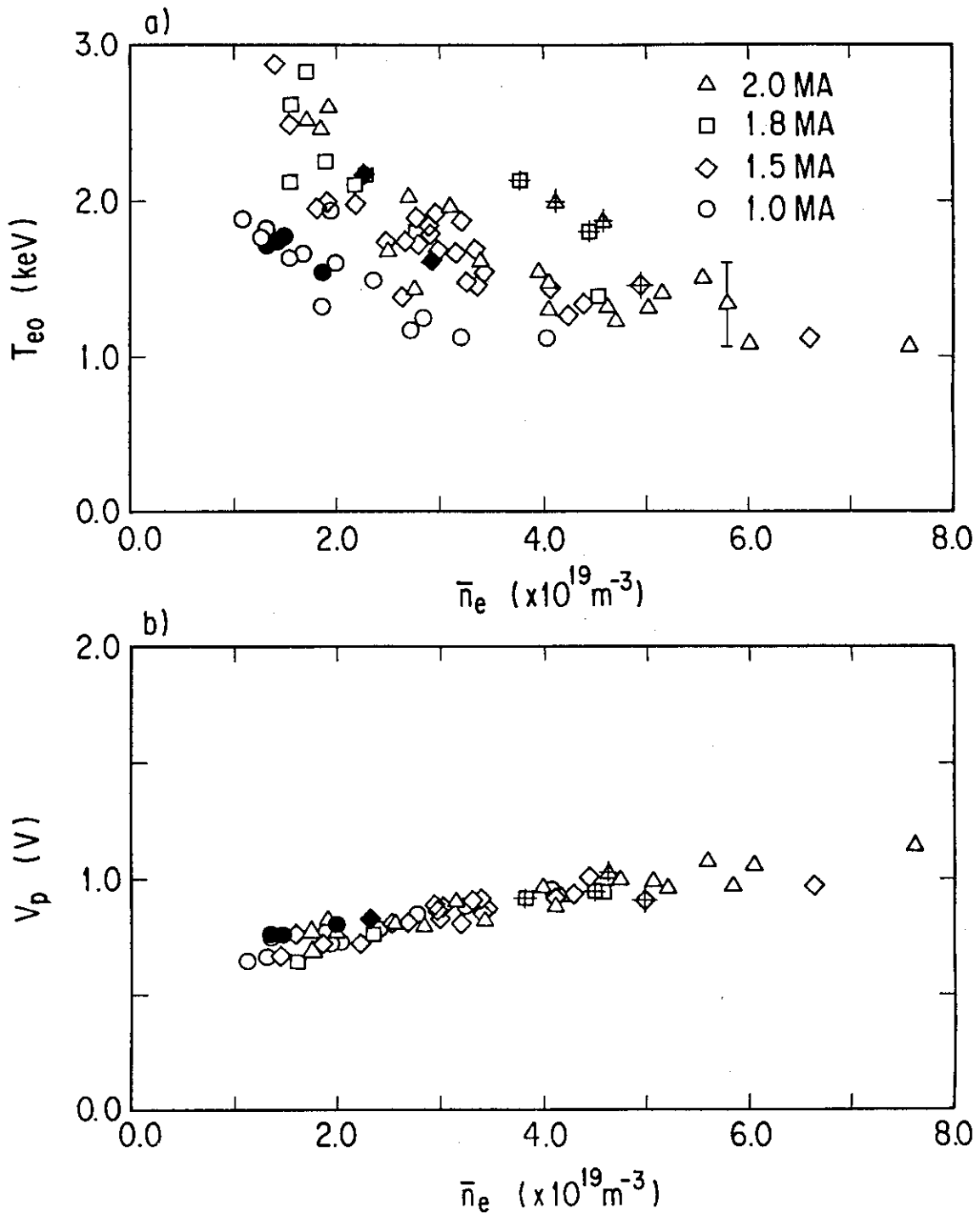


Fig. 1. a) The central electron temperatures versus the line averaged electron density. b) The resistive voltages versus the line averaged electron density. Circle means  $I_p=1.0\text{MA}$ , diamond  $I_p=1.5\text{MA}$ , tetragon  $I_p=1.8\text{MA}$  and triangle  $I_p=2.0\text{MA}$ . Open symbol and closed one present, respectively, the hydrogen divertor discharges and the hydrogen limiter discharges. Symbol with '+' means the helium divertor discharges.



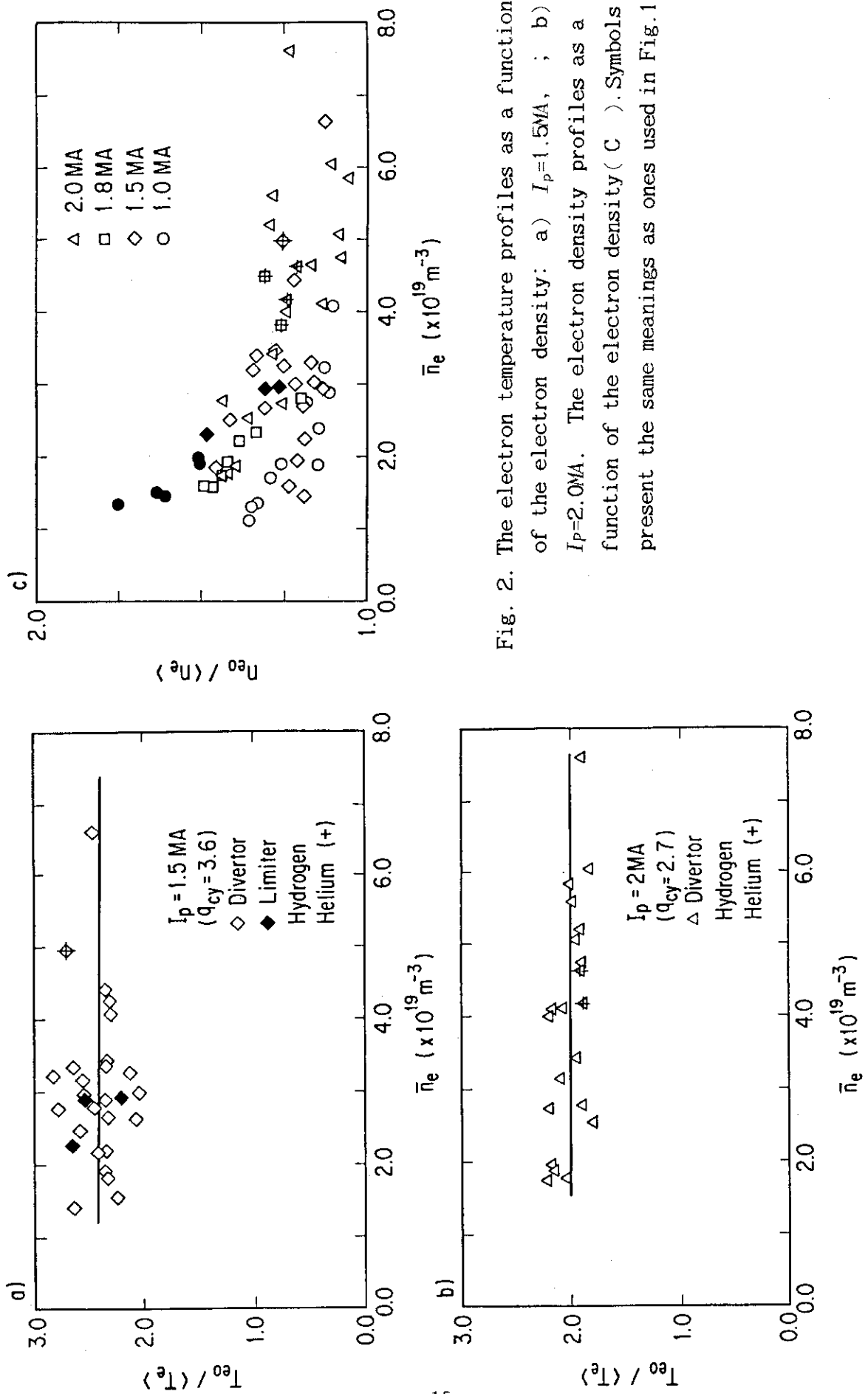


Fig. 2. The electron temperature profiles as a function of the electron density: a)  $I_p=1.5\text{MA}$ , ; b)  $I_p=2.0\text{MA}$ . The electron density profiles as a function of the electron density ( C ). Symbols present the same meanings as ones used in Fig.1.

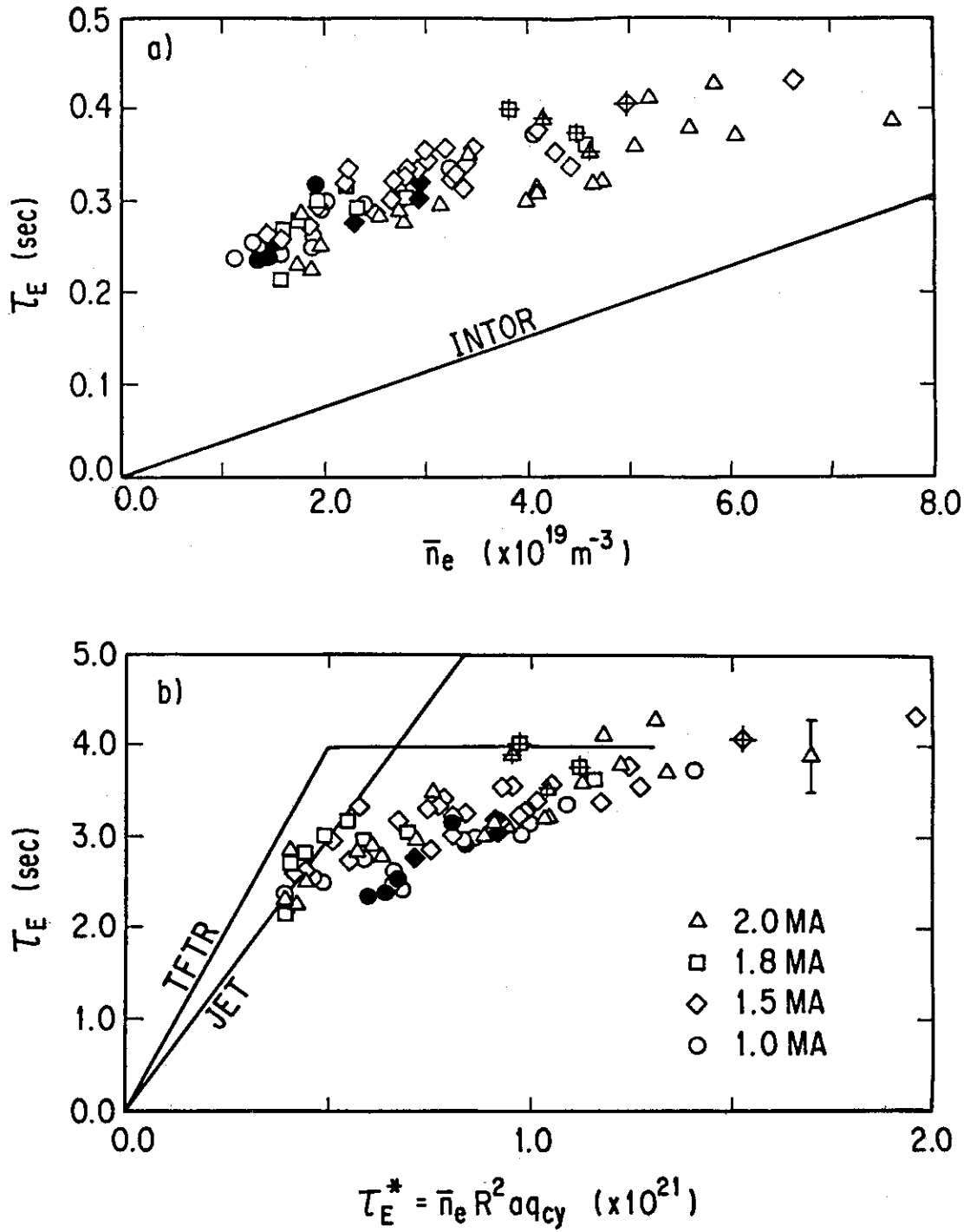


Fig. 3. The energy confinement time versus the line averaged electron density (a) and neo Alcator value scaled with  $\bar{n}_e R^2 a q_{cy}$  (b). Symbols present the same meanings as ones used in Fig.1.

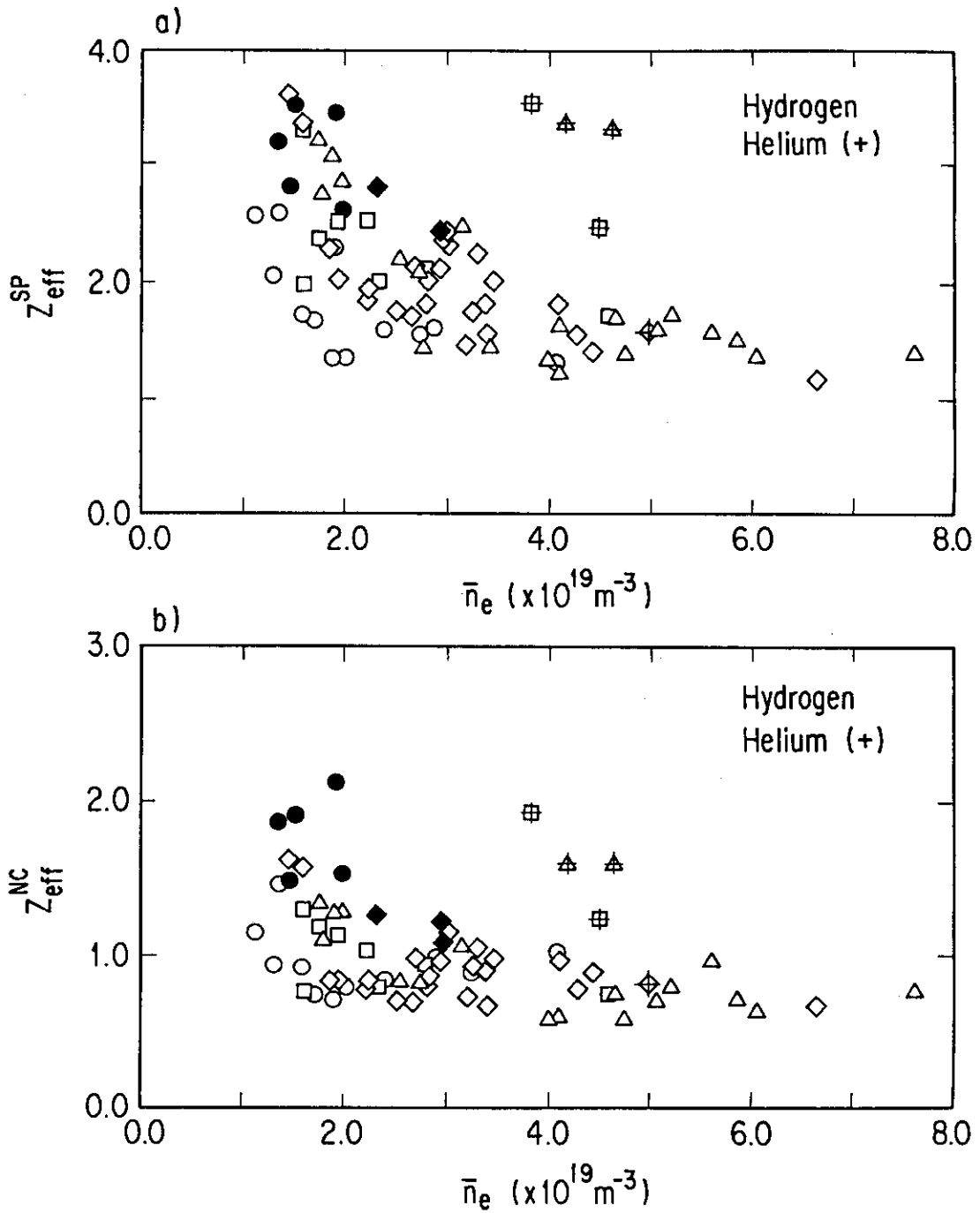


Fig. 4. The resistive  $Z_{eff}$  from Spitzer resistivity (a) and from the neoclassical resistivity with trapping correction (b) versus the line averaged electron density. Symbols present the same meanings as ones used in Fig.1.

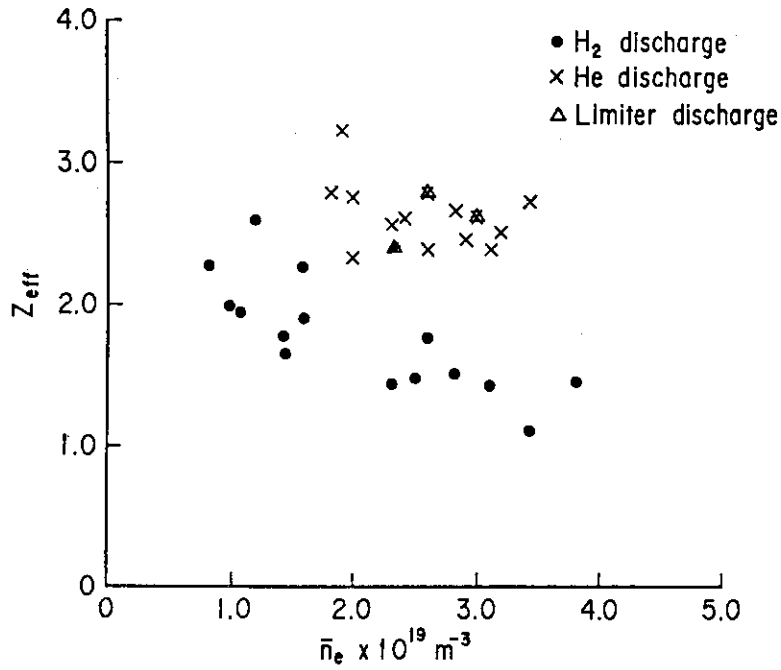


Fig. 5. The value of  $Z_{eff}$  measured by visible bremsstrahlung versus the line averaged electron density.

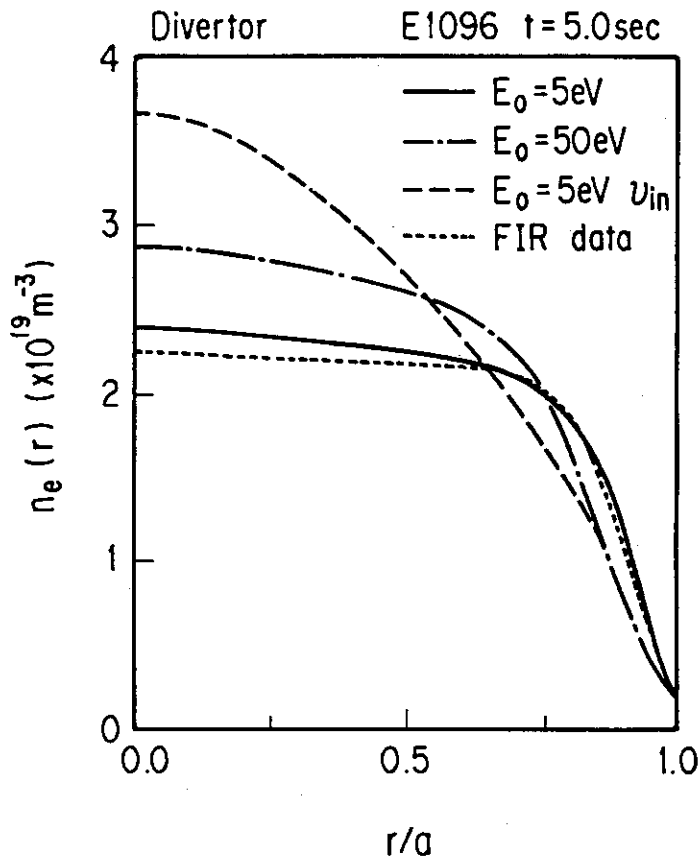


Fig. 6. The electron density profiles computed with empirical transport coefficients and cold neutral energies compared with profile measured by FIR diagnostic (dotted line) for the shot of E1096 divertor discharge.  $v_{in}$  is represented by  $-2Dr/a^2$ .

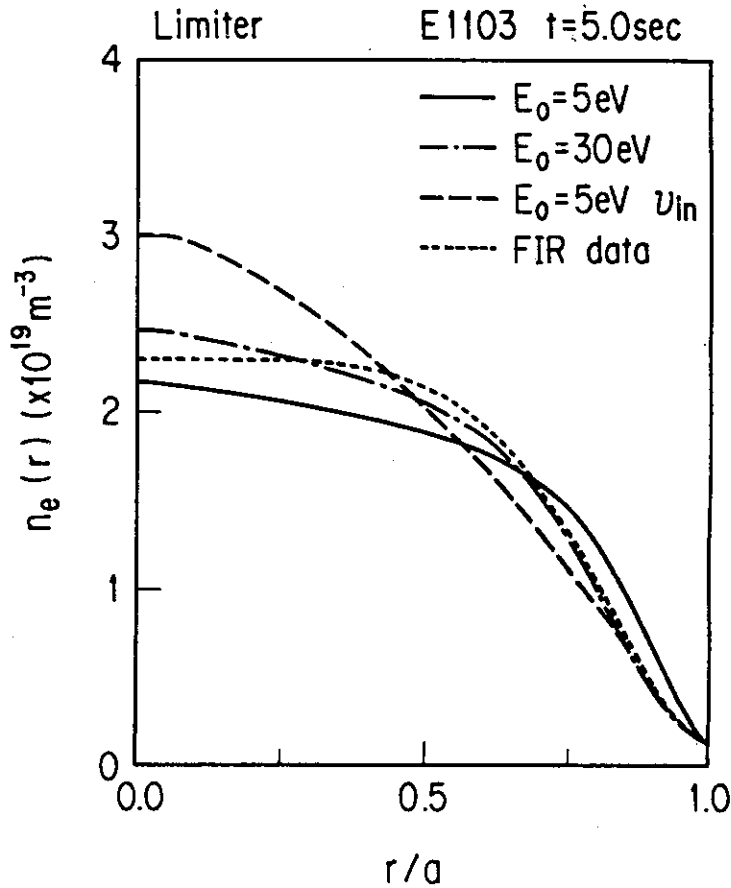


Fig. 7. The electron density profiles computed with empirical transport coefficients and cold neutral energies compared with profile measured by FIR diagnostic (dotted line) for the shot of E1103 limiter discharge.  $V_{in}$  is represented by  $-2Dr/a^2$ .

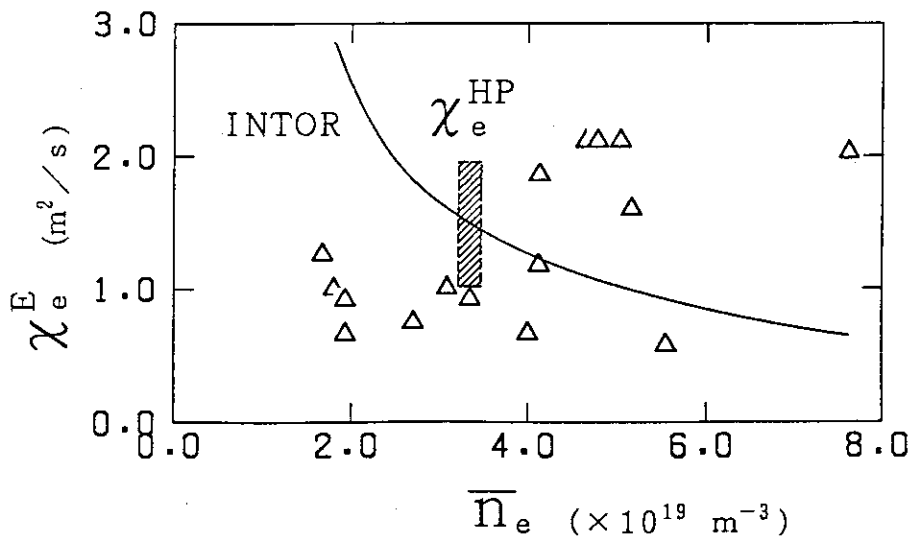


Fig. 8. The electron heat diffusivity  $\chi_e^E$  estimated at  $r=a/3$  from observed profiles of the electron temperature and density for  $I_p=1.8MA$  and  $I_p=2.0MA$ . Symbols present the same meanings as ones used in Fig.1. The INTOR scaling of  $5 \times 10^{19}/n_e$  and  $\chi_e^{HP}$  founded by the heat pulse of the sawtooth are also shown.

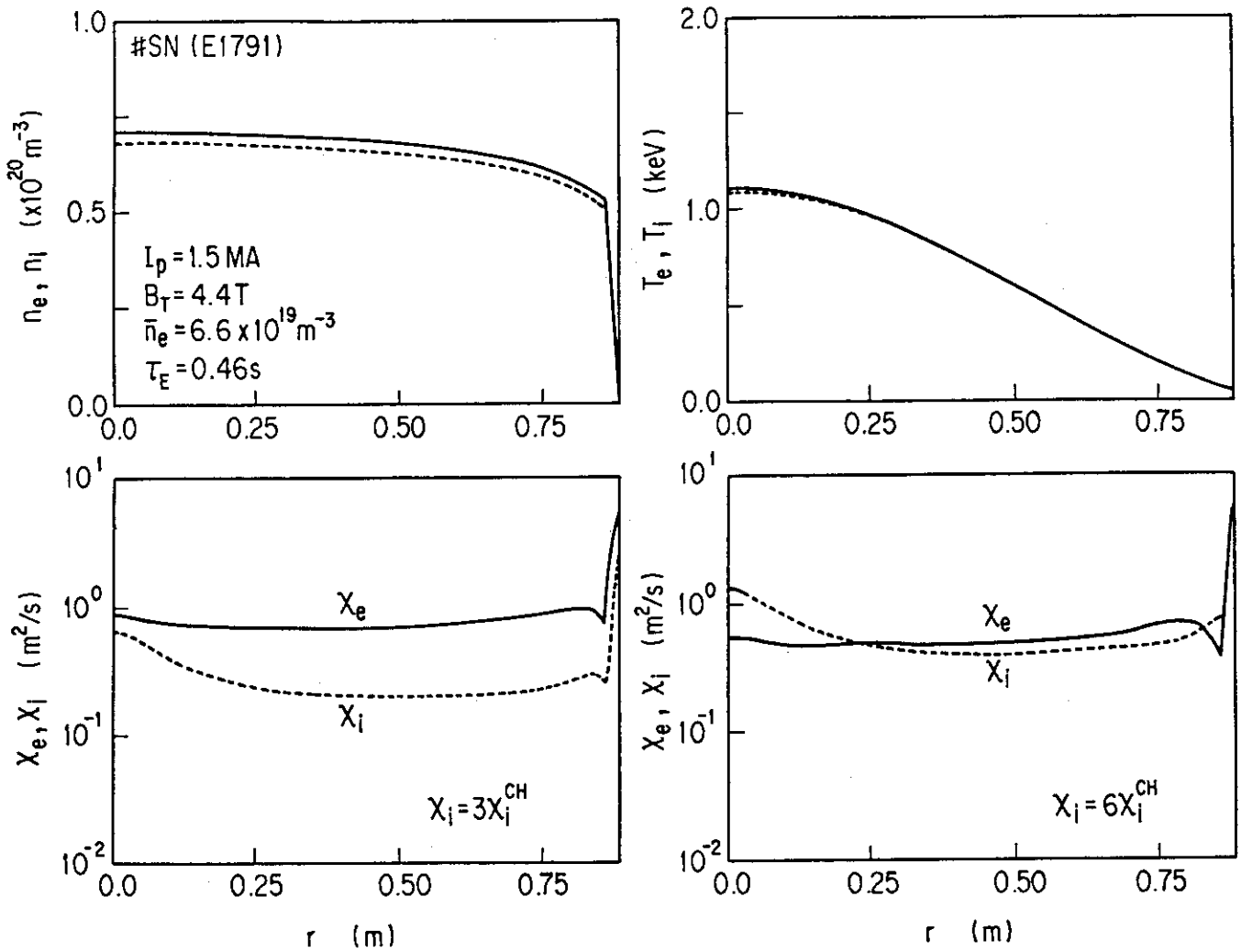


Fig. 9. The comparison of  $\chi_e^E$  estimated by using the enhancement factor of 3 or 6 for  $\chi_i^{\text{CH}}$ . The experimental profiles of the electron density and temperature for the shot of E1791 with  $I_p = 1.5 \text{ MA}$  and  $\bar{n}_e = 6.6 \times 10^{19} \text{ m}^{-3}$ . The calculated profiles of the ion density diluted with assumed carbon impurity denoted in a dotted line and the ion temperature from  $\chi_i^{\text{CH}}$  with the multiplication factor denoted in a dotted line.

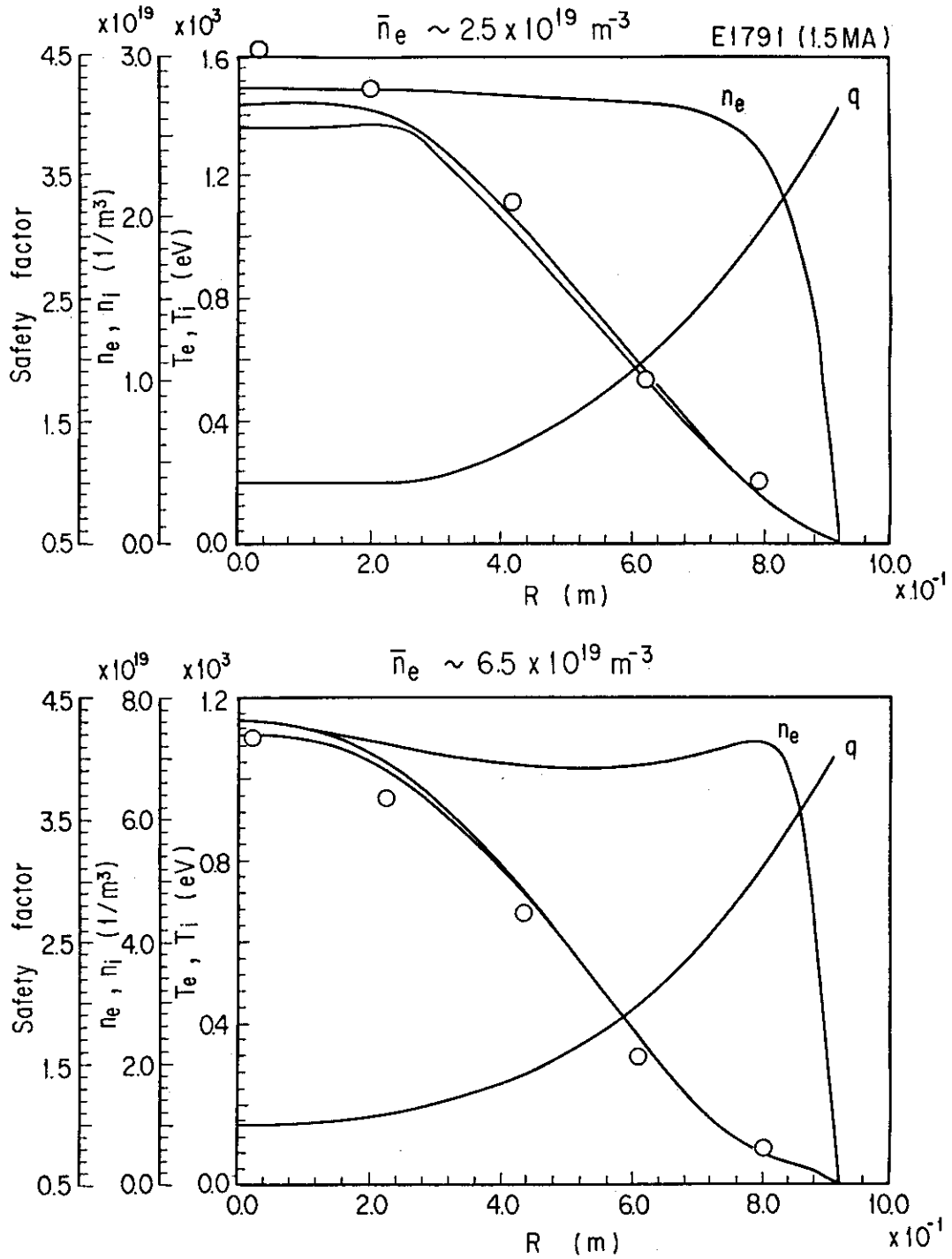


Fig.10. The profiles of electron temperature, ion temperature, electron density and safety factor  $q$  calculated with the empirical transport coefficients for the shot E1791 with  $I_p=1.5MA$ . Open circles show the electron temperature measure by Thomson scattering.

- a)  $\bar{n}_e=2.5 \times 10^{19} m^{-3}$ ,
- b)  $\bar{n}_e=6.5 \times 10^{19} m^{-3}$ ,

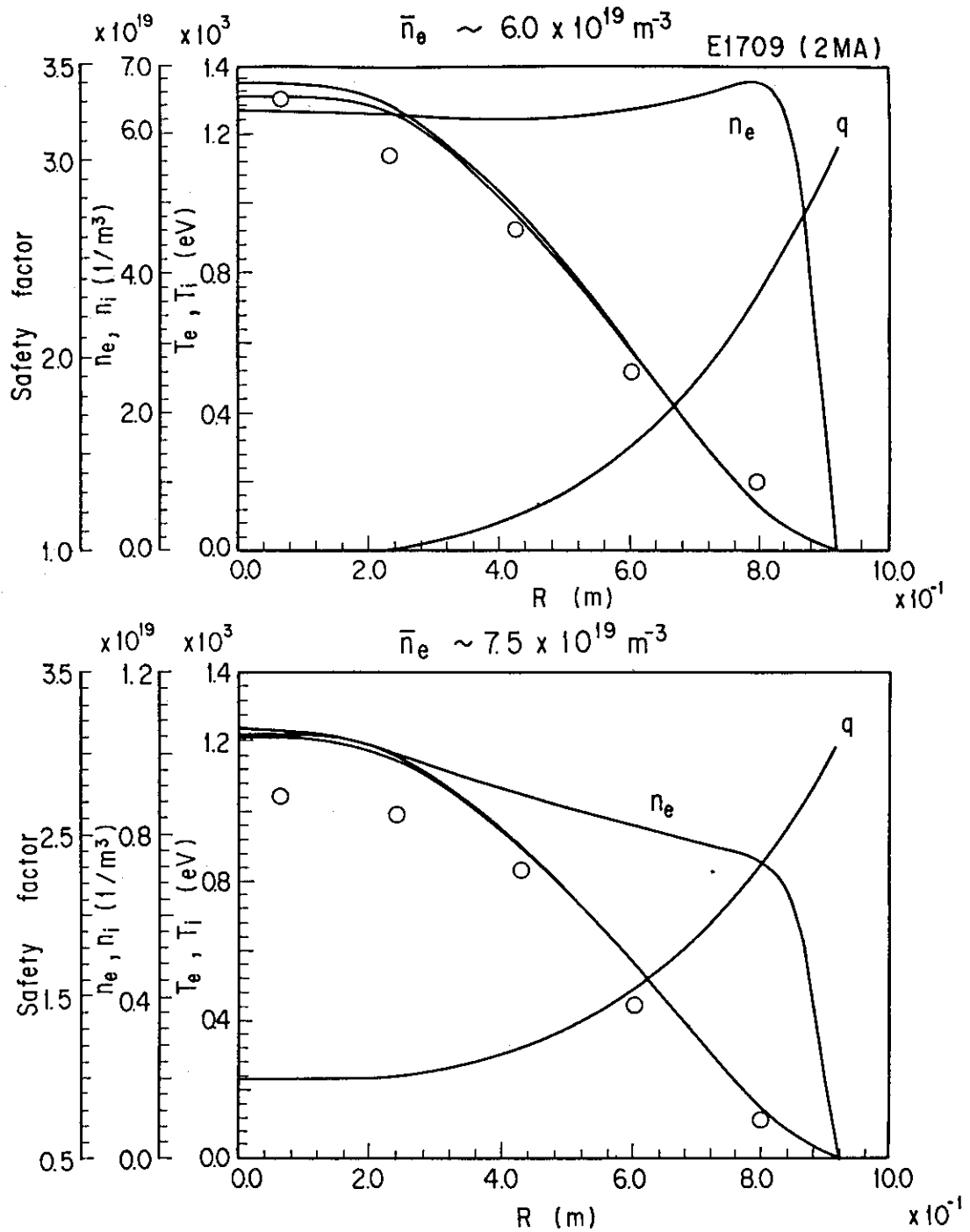


Fig.11. The profiles of electron temperature, ion temperature, electron density and safety factor  $q$  calculated with the empirical transport coefficients for the shot E1709 with  $I_p=2.0\text{MA}$ . Open circles show the electron temperature measured by Thomson scattering.

- a)  $\bar{n}_e=6.6 \times 10^{19} \text{ m}^{-3}$ ,
- b)  $\bar{n}_e=7.5 \times 10^{19} \text{ m}^{-3}$ ,



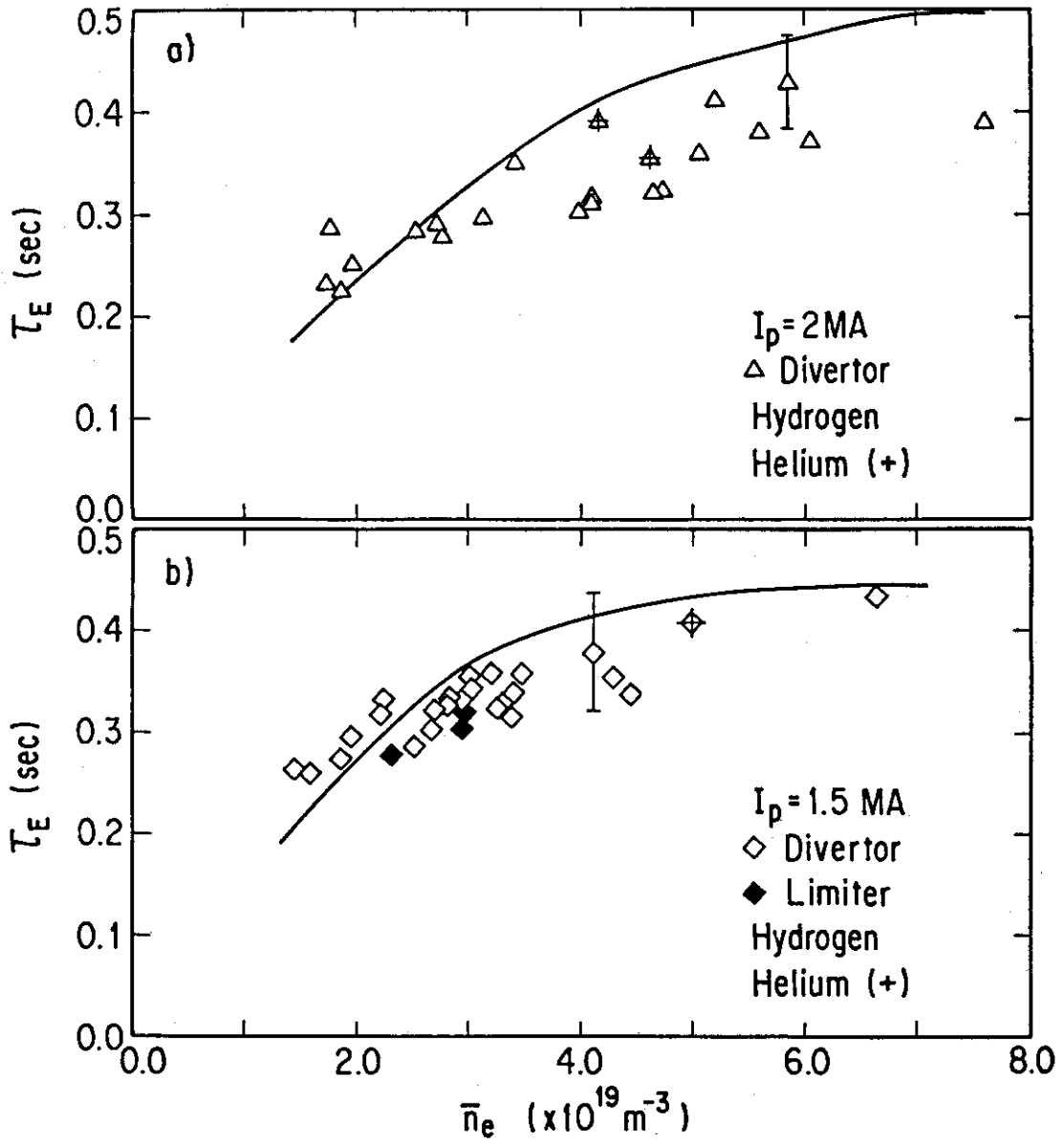


Fig.12.  $\tau_E$  versus  $\bar{n}_e$ , comparing with INTOR scaling  $\tau_E$  (a) and the calculated  $\tau_E$  (b) ;  $I_p=1.5\text{MA}$ , (c) ;  $I_p=2.0\text{MA}$ . Symbols present the same meanings as ones used in Fig.1.

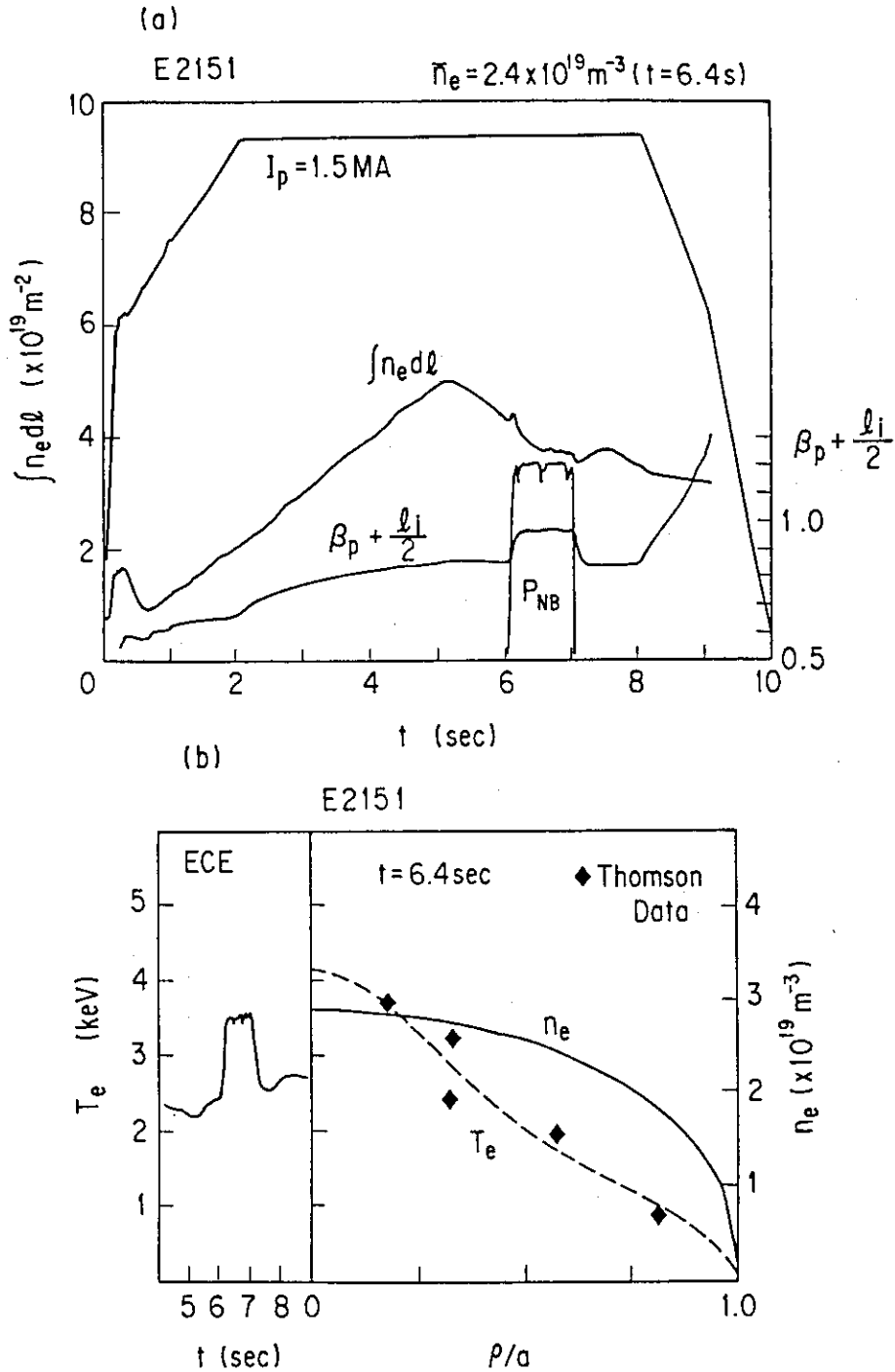


Fig.13. Time evolution and radial profile of the plasma parameters for the relatively high density discharge with 10 MW NBI heating. (a) the plasma current  $I_p$ , the line-integrated electron density  $\int n_e dl$  and the beta value  $\beta_p + 1/2 l_i$  estimated by the magnetic fitting code. (b) The time evolution of the central electron temperature measured by ECE, the density profile obtained from 3-ch FIR data and the electron temperature profile measured by Thomson scattering at  $t=6.4$  sec.

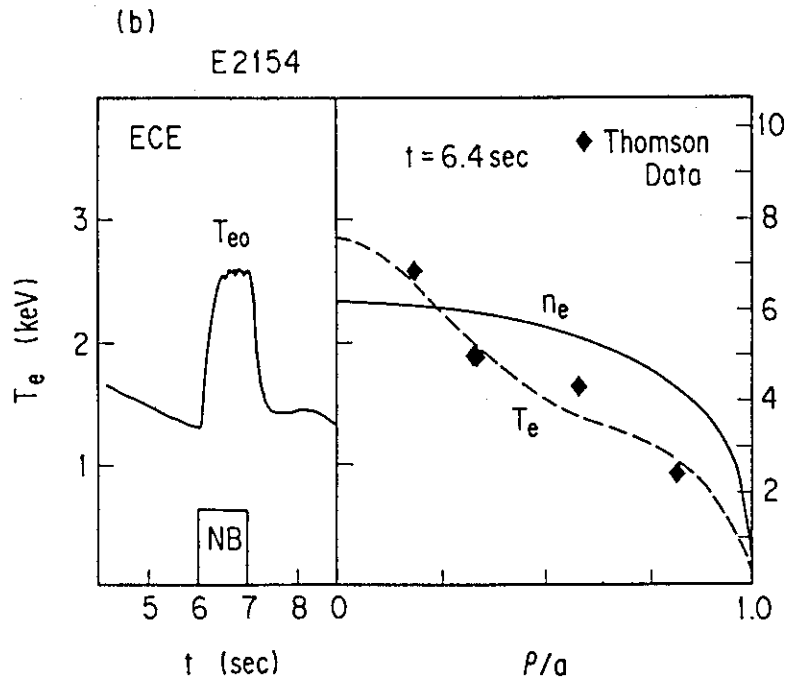
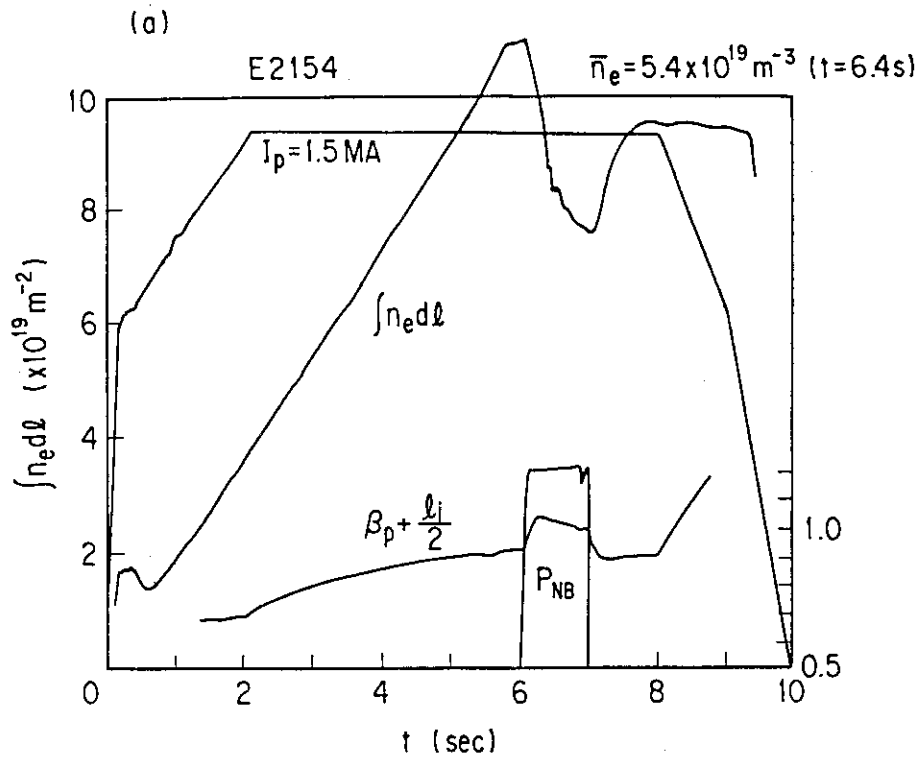


Fig.14. Time evolution and radial profile of the plasma parameters for the low density discharge with 10 MW NBI heating.

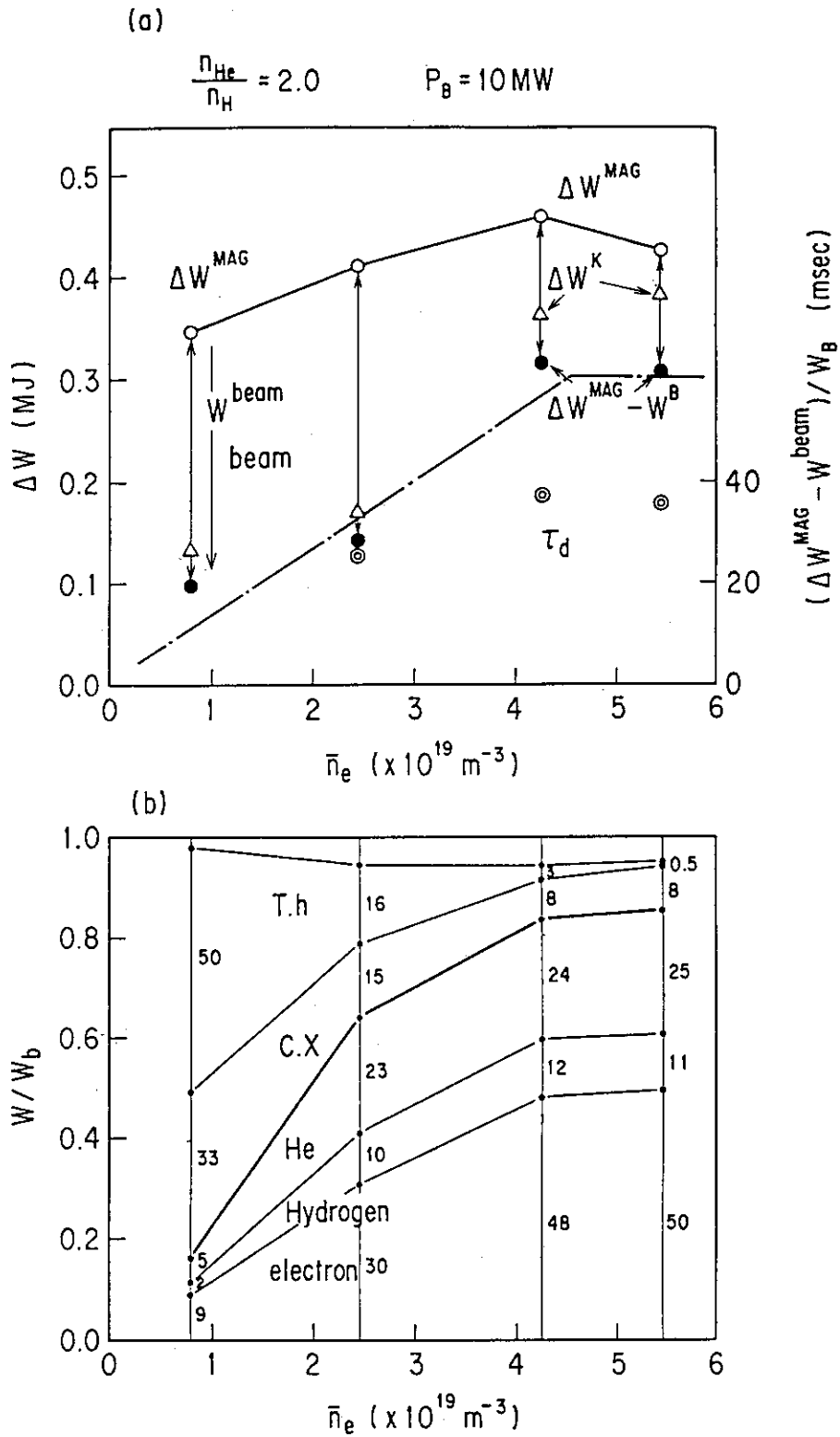


Fig.15. The density dependence of the incremental stored energy and the partition of the beam power for the helium discharge with 10 MW NBI heating.

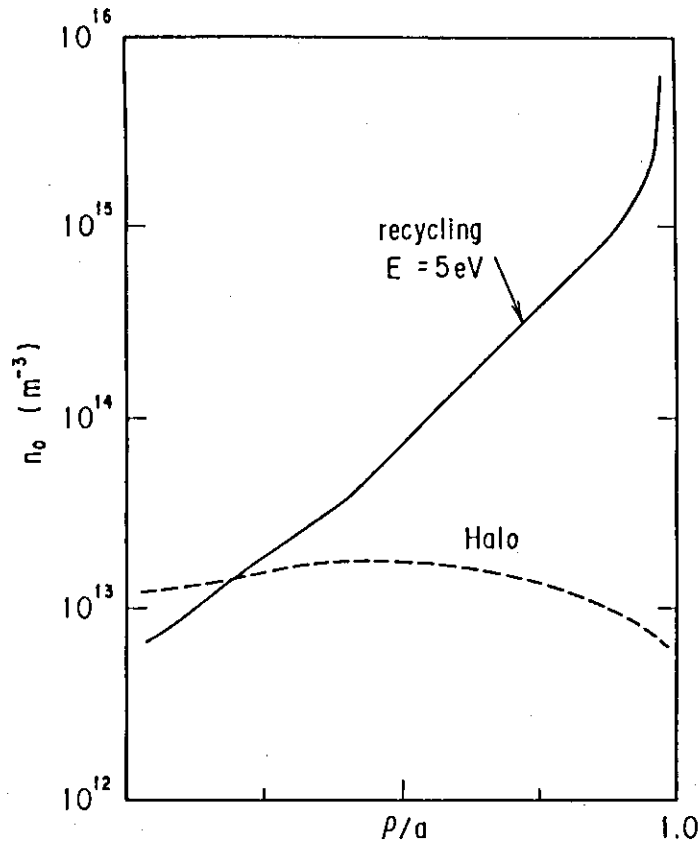


Fig.16. The density profile of recycling neutral and halo neutral

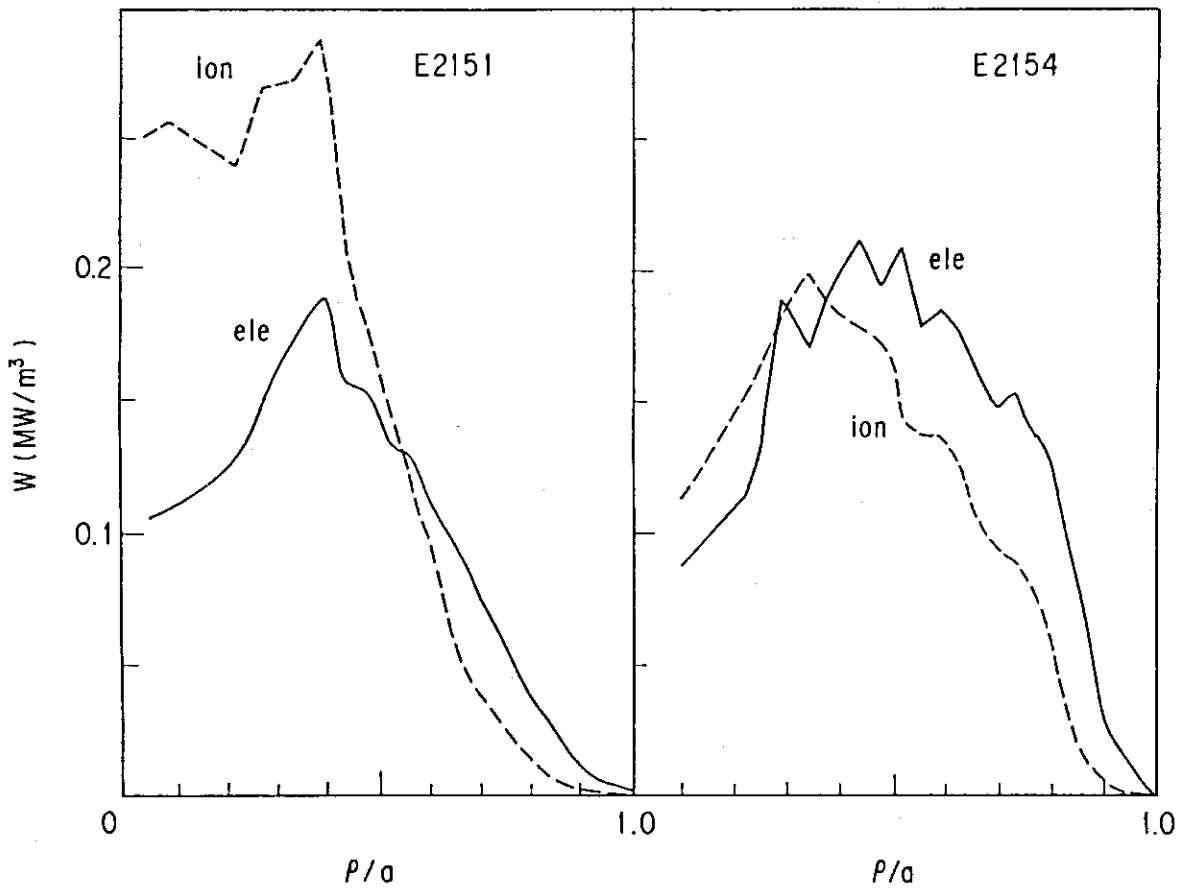


Fig.17. The power deposition profile calculated by OFMC code for E2151 and E2152 discharge.

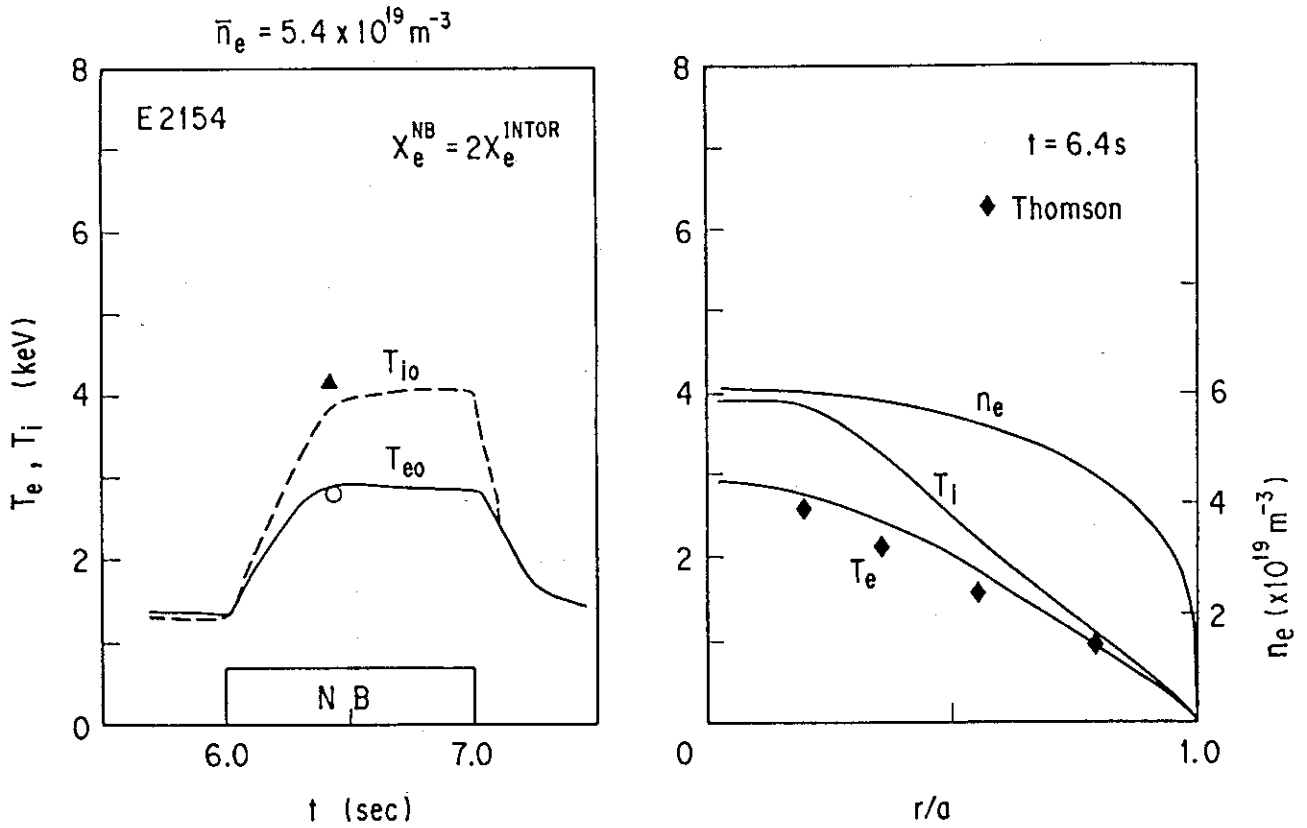


Fig.18. The simulation result for E2154 discharge ( $\bar{n}_e = 5.4 \times 10^{19} \text{ m}^{-3}$ ) using the enhanced electron heat diffusivity  $\chi_e^{NB} = 2 \times \chi_e^{INTOR}$  during NBI heating phase.

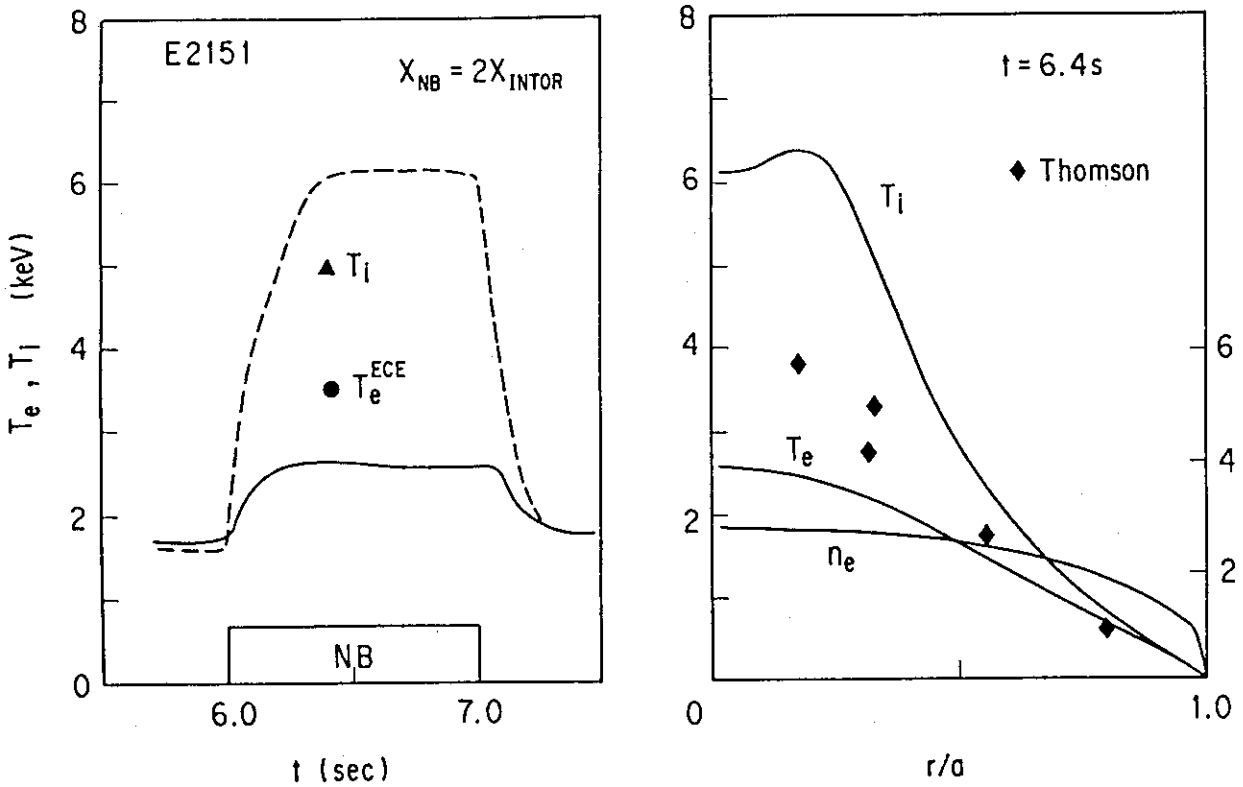


Fig.19. The simulation result for E2151 discharge ( $\bar{n}_e = 2.4 \times 10^{19} \text{ m}^{-3}$ ) using the same anomalous transport of E2154 simulation.

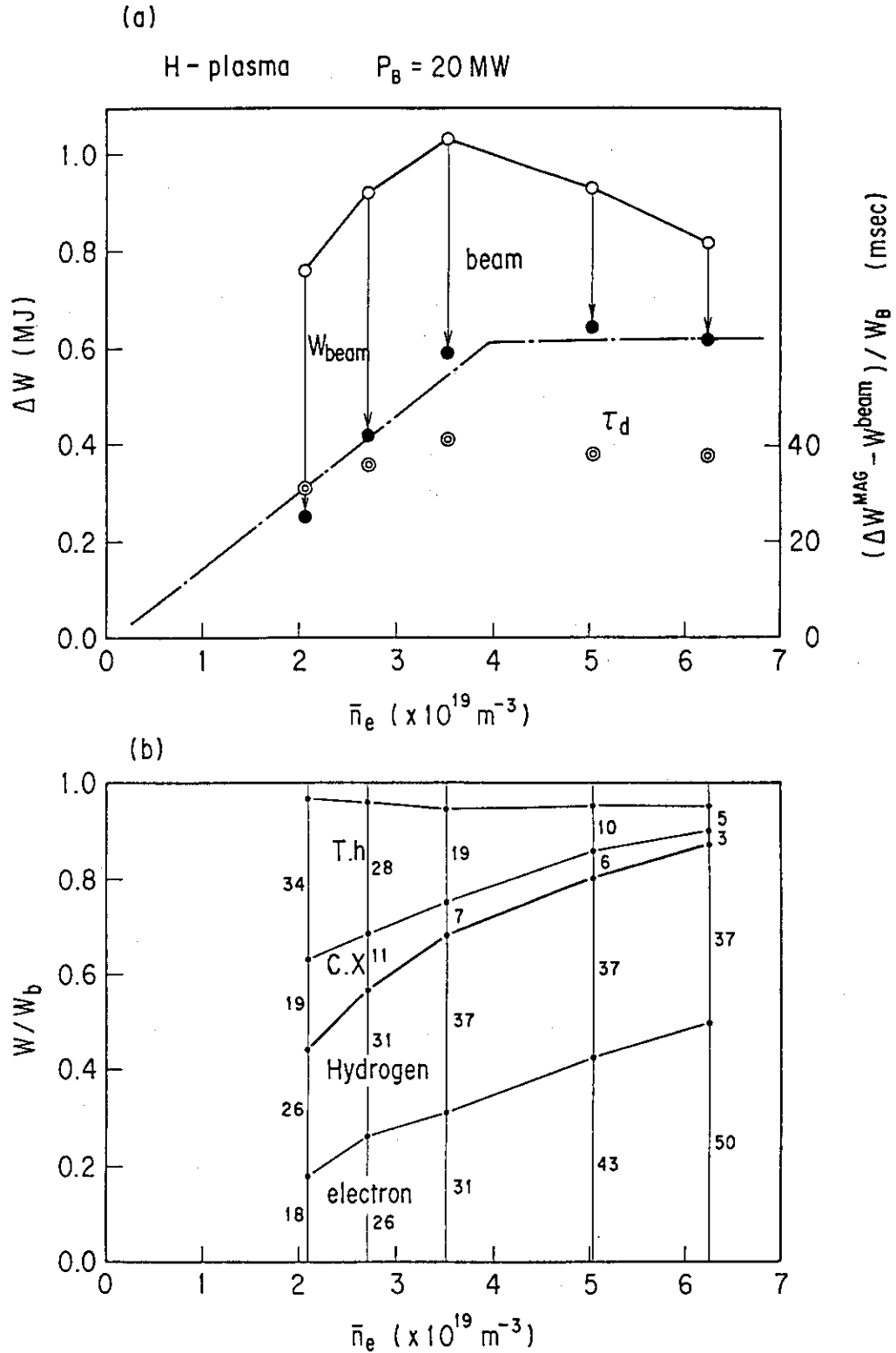


Fig.20. The density dependence of the incremental stored energy and the partition of the beam power for the hydrogen discharges with 20 MW NBI heating.

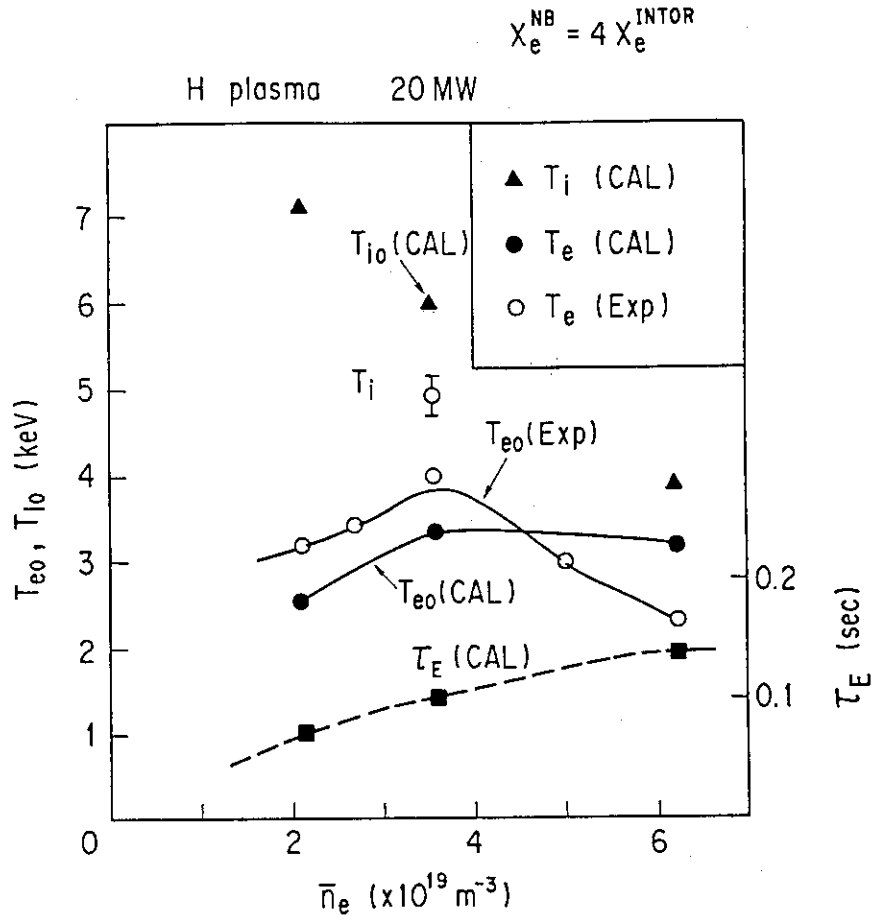


Fig.21. The simulation results for a series of the hydrogen discharge with 20 MW NBI heating and the experimental data. The electron heat diffusivity  $\chi_e^{NB}$  is enhanced by a factor 4.