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An Analysis of CSNI Standard Problem NO.8

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The CSNI International Standard Problem (ISP8), based on the Semiscale S-06-3 Test, was analyzed in the course of verification work of the computer code ALARM-P1. In this report, described was the result of the initial trial, which had been submitted to the CSNI. Due to the limitations of ALARM-P1 capability, only the blowdown portion of the transient was calculated. Though the hydraulic behavior before ECCS injection agreed with the test data, the ALARM-P1 could not continue calculation after 26 seconds due to severe predicted instability following the ECCS injection. The prediction of surface temperature of the heater rods was also unsatisfactory. Several problems to be improved have been identified both in the analytical model and the input data.

Key Word: Committee on Safety of Nuclear Installations-Standard Problem,  
Blowdown, Refill, Reflood, Loft L2-3, Semiscale Test

CSNI 標準問題No 8 の解析

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(1980年1月31日受理)

計算コードALARM-P1を用いてセミスケールS-06-3実験の解析がおこなわれたのでここに報告する。本問題は、1979年度NEA国際標準問題No 8として選ばれたものである。

本報告は、入力データ作成後CSNIに送付した最初の計算結果をまとめたものである。使用されたコードの性格上、リフィルリフラッドphaseの解析は除外され、ブローダウンの解析が中心となった。結果として、ECC水の注入以前の水力挙動は概ね実験データと一致してはいるが、ヒータ表面温度はかなり低く予測された。ECC水注入後は、解析モデルに起因する急激な圧力変動のため、26秒以降計算が続行できなかった。データとの比較検討の結果、解析手法と入力データの双方にいくつかの問題点が明らかになり、次回の再解析で十分改善されるであろう。

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## 1. Introduction

One of the 1-1/2 loop Mod-1 experiments<sup>(1)~(4),(6),(11)\*</sup> investigating the system behaviors of a light water-cooled nuclear reactor during a postulated loss-of-coolant-accident was analyzed using the computer code ALARM-P1.

The object of a simulation and analysis is a third test of the Semiscale Test Group 6, which was selected as the CSNI (Committee on Safety of Nuclear Installations) Standard Problem NO.8. This experiment, using an active core simulator, covers three different categories of a blowdown, refill and reflood, and is intended to offer a counterpart to the LOFT nuclear test L2-3.

A lay-out of the Semiscale test facility is exhibited in the Figure 1. A full description of the system configuration can be found in the references.<sup>(2),(3),(4)</sup> The experiment S-06-3 simulates an instantaneous 200 % double-ended cold leg break from the incipient conditions of about a 65 % rated power (1.005 MW). Emergency core cooling (ECC) water from AIS, HPIS, and LPIS was injected only into the intact loop cold leg. A reactor core, consisting of thirty-six electrically heated and four unpowered rods, simulates the LOFT nuclear fuels.

The present ALARM-P1 analysis was restricted to the decompression process up to 40 seconds from the initiation of the accident. Therefore, no calculation of the refill-reflood portions was made. The results of this preliminary analysis indicate that the thermal hydraulic behaviors in the system were reasonably simulated, but the core heater thermal response not.

Comparative analysis of the experimental data provided some valuable suggestions regarding corrections of the input data and/or refinement of

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\*) Numbers in brackets designate References.



the analytical model employed in ALARM-PI. The purpose of this report is to document the comparative analyses on the blowdown phase of the international standard problem 8 (ISP8) submitted to the CSNI.

## 2. System model and assumptions

The ALARM-PI computational model for the Mod-1 facility is divided into 36 control volumes with 40 junctions as depicted in the Figure 2. The volume and junction geometrical data were picked out of the references. (2), (3), (4) A short description of this code is presented in the Table 1.

The core region was nodarized into five axially-stacked volume nodes according to the CSNI request. The upper-plenum and the upper-head was represented by a single combined compartment. The downcomer consists of two volumes: inlet annulus and downcomer annulus. The suppression tank and header were made up of one volume. In the Table 2 and 3, is listed an identification of each control volume and junction.

A bubble separation model, with a bubble density gradient and velocity of 0.8 and 0.914 m/s, respectively, was used in the pressurizer, steam generator secondary side, accumulator and the pressure suppression tank. The remaining control volumes were assumed to be in homogeneous fluid flow conditions.

HPIS (High Pressure Injection System), LPIS (Low Pressure Injection System) and feed water line were treated as fill junctions with time dependent data. On the other hand, the steam generator discharge valve was represented using a leak junction. The initial flow through the fill or leak junction was determined from the mass and energy balance.

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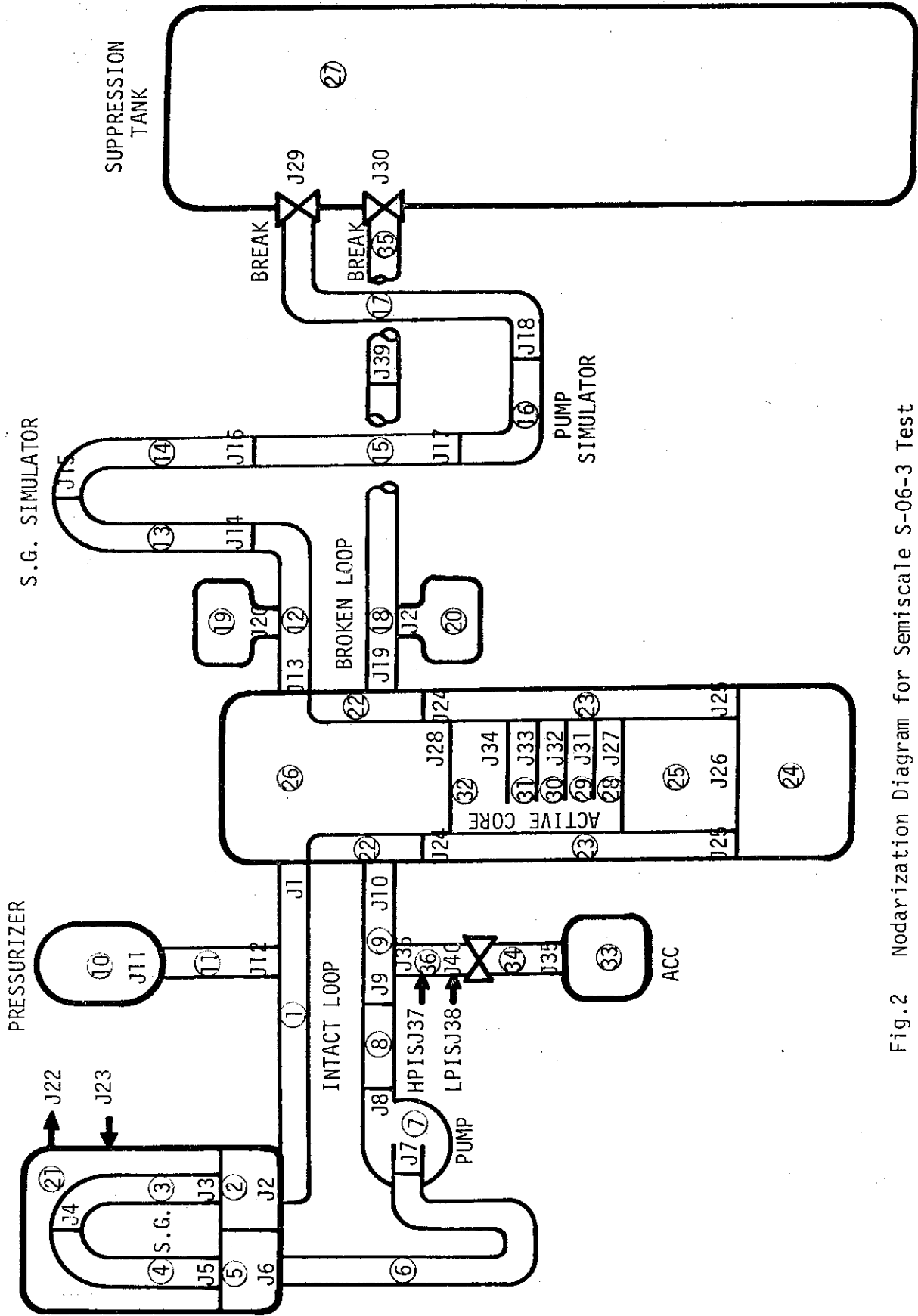


Fig.2 Nodarization Diagram for Semiscale S-06-3 Test

Seven heat slabs in all were used in the reactor core region and the intact loop steam generator U-tubes. In the present analysis, four hot fuel rods in the center were not simulated. Instead, the core was modelled with 40 low power rods, which was divided into five control volumes to predict the surface temperature of the elevation 8", 14", 28" and 39" above the bottom of the heated length of 66".

The initial power generation rates in the individual volumes were selected as follows:

Volume NO.	Ratio
28	0.1323
29	0.2307
30	0.2553
31	0.2086
32	0.1731

The critical flow model used at the break junctions is estimated by the Zaloudek and Moody correlation in the subcooled and the saturated region, respectively. The discharge coefficient of 0.6 was applied in common with two regions.

The pump is assumed to revolve at 1618 rpm as specified. The ALARM-P1 homologous curves equivalent to the RELAP-4 analytical model were given by input. The cavitation effects at the two-phase flow region and the frictional torque were neglected.

For the T-shaped connection (i.e., pressure vessel inlet and outlet, pressurizer surge line outlet and ECC entrance) momentum flux terms were optionally removed.

Break was simulated by a valve which was fully opened within 10 micro seconds. ALARM-P1 employs a forward explicit method in solving the differential equations without any automatic time step control.



Table 1 Basic Features of ALARM-P1 Code

Used language	FORTRAN-IV (for FACOM 230 computer)
Range of Application	PWR-LOCA with large breaks (only blowdown phase)
Assumptions of governing equations and fluid state	(i) one dimensional fluid equation (mass, energy and momentum) and state equation heat transfer equation reactor kinetic equation (IREK) (ii) lumped parameter (node and junction type) (iii) homogeneous flow (iv) thermal equilibrium
Solution technique	Fully explicit method except for Crank Nicolson model in the conduction equation solutions
Time step size	Specified by user
Friction factor	Single phase : Fanning smooth pipe Two phase : Thom and Martinelli-Nelson
Phase separation model	Homogeneous or bubble rise model. Bubble rise velocity and bubble density gradient is required as input data.
Slip model	None
Critical flow model	$x < 0.02$ : Zaloudek $x > 0.02$ : Moody Superheated : Murdock-Bauman $C_D$ (contraction coeff. input)
Pump model	Single phase model by homologous law (non-cavitated)
Heat transfer coeff.	According to ANCR-1127
Dryout correlation	B&W-2, Barnett, Modified Barnett

In the present calculation, the time step widths were selected as follows.

0.0 $\leq t \leq$ 0.01 (sec)	$\Delta t = 0.000005$ (sec)
0.01 $\leq t \leq$ 0.05 (sec)	$\Delta t = 0.00001$ (sec)
0.05 $\leq t \leq$ 0.3 (sec)	$\Delta t = 0.000025$ (sec)
0.3 $\leq t \leq$ 0.5 (sec)	$\Delta t = 0.00005$ (sec)
0.5 $\leq t \leq$ 5.0 (sec)	$\Delta t = 0.0001$ (sec)
5.0 $\leq t \leq$ 10.0 (sec)	$\Delta t = 0.00025$ (sec)
10.0 $\leq t \leq$ 17.0 (sec)	$\Delta t = 0.0005$ (sec)
17.0 $\leq t \leq$ 25.0 (sec)	$\Delta t = 0.0001$ (sec)
25.0 $\leq t \leq$ 30.0 (sec)	$\Delta t = 0.0002$ (sec)
30.0 $\leq t \leq$ 40.0 (sec)	$\Delta t = 0.0004$ (sec)

The junction inertia ( $\rho/A$ ) and form loss coefficient for complicated configurations were estimated by hand calculations. Particularly, K-factor was determined so as to minimize the residual friction loss. The initial conditions used in this calculation are given in the Table 4. In addition, Appendix 1 shows the entire input data list.

### 3. Results and comparisons with experimental data

The calculated results by ALARM-P1 were compared with the Semiscale S-06-3 test data<sup>(1)</sup> in Figures 3 through 48. In these figures, the calculated results were denoted by "A".

Only key parameters requested by the CSNI were mentioned in this section. (Figures 44 to 48 are not the requested parameters.) The experimental data was retrieved from the Semiscale data tape recorded. Application of this tape was made through the LOFT plotter program<sup>(12),(13)</sup> by the introduction of the detector code names (i.e., function codes) similar to the LOFT function codes as listed in Appendix 2. In this section, a simple outline of the calculated results obtained using this code is given. The blowdown calculation was terminated at approximately

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Table 2 Geometrical Description of Semiscale S-06-3 Model Control Volumes

<u>Control volume</u>	<u>Description</u>	<u>Volume(m<sup>3</sup>)</u>	<u>Flow Area(m<sup>2</sup>)</u>
1	Intact loop hot leg piping	0.01082	0.00349
2	Steam Generator inlet plenum	0.00963	0.01984
3	Steam generator U-tubes	0.01140	0.00442
4	Steam generator U-tubes	0.01140	0.00442
5	Steam generator outlet plenum	0.00963	0.01984
6	Pump suction leg	0.01018	0.00349
7	Primary coolant pump	0.00408	0.00349
8	Cold leg piping	0.00425	0.00349
9	Cold leg piping	0.00425	0.00349
10	Pressurizer	0.02741	0.02400
11	Pressurizer surge line	0.00037	4.3E-5
12	Broken loop hot leg piping	0.00315	0.00349
13	S.G. simulator	0.00852	0.00374
14	S.G. simulator	0.00852	0.00374
15	Outlet piping from S.G. simulator	0.00252	0.00158
16	Pump simulator	0.00147	0.00198
17	Break node	0.00227	0.00145
18	Broken loop cold leg	0.00461	0.00349
19	Reflood assist by-pass piping	0.00538	0.00349
20	Reflood assist by-pass piping	0.00640	0.00349
21	Secondary side of steam generator	0.19820	0.04255
22	Upper annular region of the vessel inlet region	0.00504	0.00548
23	Downcomer region	0.02183	0.00534
24	Lower plenum	0.02161	0.00623
25	Turbine flowmeter housing	0.00371	0.00713
26	Upper plenum	0.02620	0.00713
27	Pressure Suppression tank	3.17549	0.70205

Table 2 (continued)

<u>Control volume</u>	<u>Description</u>	<u>Volume(m<sup>3</sup>)</u>	<u>Flow Area(m<sup>2</sup>)</u>
28	Active core region	0.00137	0.00492
29	Active core region	0.00137	0.00492
30	Active core region	0.00137	0.00492
31	Active core region	0.00137	0.00492
32	Active core region	0.00274	0.00492
33	ECCS-accumulator	0.00145	0.03812
34	ECCS-injection line	0.00244	0.00046
35	Break node	0.00161	0.00349
36	ECCS-injection line	0.00244	0.00046

Table 3 Junction Description of ALARM-PI Model

<u>Junction</u>	<u>Volumes</u>		<u>Flow Area</u> (m <sup>2</sup> )	<u>Form Loss Coefficients</u>	
	<u>(From)</u>	<u>(To)</u>		<u>Forward</u>	<u>Reverse</u>
1	26	1	0.00183	0.0	0.0*
2	1	2	0.00349	6.198	6.198
3	2	3	0.00442	0.0	0.0
4	3	4	0.00442	0.0	0.0
5	4	5	0.00442	0.0	0.0
6	5	6	0.00349	15.4395	15.4395
7	6	7	0.00349	5.30	4.86
8	7	8	0.00349	1.65	1.65
9	8	9	0.00349	0.467	7.32
10	9	22	0.00183	0.658	1.466
11	10	11	4.3E-5	10.8	10.8
12	11	1	4.3E-5	0.0	0.0
13	26	12	0.00183	0.677	1.2144
14	12	13	0.00024	1.41181	1.41146
15	13	14	0.00349	285.435	285.435
16	14	15	0.00024	1.40405	1.41583
17	15	16	0.00024	0.844137	1.54353
18	16	17	0.00024	12.8823	12.438
19	22	18	0.00183	0.677051	1.21442
20	19	12	0.00349	0.0	0.0
21	20	18	0.00349	0.0	0.0
22	21	0	0.00203	0.0	0.0
23	0	21	0.00113	0.0	0.0
24	22	23	0.00534	3.9706E-2	2.2542E-3
25	23	24	0.00534	4.6518E-2	0.1465
26	24	25	0.00713	19.569	19.569
27	25	28	0.00492	10.5898	10.5898
28	32	26	0.00492	7.2754	7.2754
29	17	27	0.00024	1.00777	1.13360
30	35	27	0.00024	1.38245	1.15464
31	28	29	0.00492	0.0	0.0
32	29	30	0.00492	0.0	0.0
33	30	31	0.00492	0.0	0.0

Table 3 (continued)

<u>Junction</u>	<u>Volumes</u>		<u>Flow Area</u> (m <sup>2</sup> )	<u>Form Loss Coefficients</u>	
	<u>(From)</u>	<u>(To)</u>		<u>Forward</u>	<u>Reverse</u>
34	31	32	0.00492	0.0	0.0
35	33	34	0.00046	71.095	1.0E-6
36	36	9	0.00046	71.095	1.0E-6
37	0	36	0.00015	0.0	0.0
38	0	36	0.00028	0.0	0.0
39	18	35	0.00349	1.0E-10	1.0E-10
40	34	36	0.00046	142.19	1.0E-6

\*) "0.0" denotes automatic calculation option incorporated  
in ALARM-P1 code

Table 4 Initial Conditions

Pressure (kg/cm<sup>2</sup>)

Upper-plenum	160.8298
Pressurizer	160.7948
Steam Generator Secondary	Sat. at 284 °C
Accumulator	45
Pressure suppression	2.48

Fluid Temperature (°C)

Core inlet fluid temperature	290.889
Core outlet fluid temperature	326.444
Broken loop cold leg	288.80
Broken loop hot leg	322.96
Broken loop hot leg break node	316.97
Accumulator tank	27.778
Pressure suppression	16.1
Feed water supply system	204.8
HPIS, LPIS	27.778
Reflow bypass line	{ Hot leg side
	{ Cold leg side
	315.85
	288.85

ECC Injection

## Accumulator:

Water volume	0.08 (m <sup>3</sup> )
Gas volume	0.058 (m <sup>3</sup> )
Initiation pressure	42.19 (kg/cm <sup>2</sup> )

## HPIS:

Injection initiation	126.58 (kg/cm <sup>2</sup> )
Injection rate	0.0149 (kg/s) (0.0 < t < 30.0)
	0.0817 (kg/s) (30.0 < t < 50.0)

## LPIS:

Injection initiation	17.58 (kg/cm <sup>2</sup> )
Injection rate	0.299 (kg/s) (0 < t < 50.0)

(t : time after tripping)

Others

Core power	1.0058 (MW)
Core flow rate	4.899 (kg/s)
Primary pump speed	1618.9 (rpm)
Pressurizer liquid level	0.625 (m)
Steam generator liquid level	2.9 (m)



Table 5 Parameters Requested for ISP8 Comparison

<u>Required Parameters</u>	<u>Location</u>
<u>(1) Pressures (kPa)</u>	
PU-PRIZE	Pressurizer pressure
PB-42	Upstream of break nozzle (pump side)
PB-23	Upstream of break nozzle (reactor vessel side)
PV-UP+10	Upper plenum
PU-ACC	Intact loop accumulator
PU-SGSD	Steam generator secondary side
<u>(2) Differential pressures (kPa)</u>	
DPU-12-10	Across pump
DPU-7-10	Across pump suction
DPB-32-36L	Across simulated steam generator
DPB-38-40	Across simulated pump
DPV-LP-UP	Across core
<u>(3) Flow rates (KG/s, l/s)</u>	
FTV-COREIN	Core inlet flow
FDB-42, GB-42VR	Break nozzle flow (pump side)
FDB-23, GB-23VR	Break nozzle flow (reactor vessel side)
FTU-15	Intact loop cold leg flow
FTU-PRIZE	Pressurizer surge line flow
FTU-LPIS	Intact loop LPIS flow
FTU-HPIS	Intact loop HPIS flow
FTU-ACC	Intact loop accumulator flow
FDU-10, GU-10	Mass flow rate in spool 10
<u>(4) Fluid density (kg/m<sup>3</sup>)</u>	
GB-42VR	Break volume density (pump side)
GB-23VR	Break volume density (reactor vessel side)
GU-15C	Intact loop cold leg density
GU-10	Pump inlet density
GVCOR-150HZ	Core inlet density
GV161-192D	Lower plenum density
<u>(5) Fluid temperature (°K)</u>	
TFU-PRIZE	Pressurizer surge line fluid temperature
TFB-23	Fluid temperature upstream of break
TFV-UP+13	Fluid temperature in upper plenum

Table 5 (continued)

<u>Required Parameters</u>	<u>Location</u>
(6) <u>Metal temperatures (<math>^{\circ}\text{K}</math>)</u> Rod surface temperatures on average rod (7.59 kW/ft)	Elevations of 8", 14", 28", and 39" above bottom of heated length
(7) <u>Quality and heat transfer coefficient MW/m <math>\cdot</math> K)</u>	Same elevations in core correspond- ing to the thermocouples for the heater rod temperatures
(8) <u>Mass Inventory (kg)</u> FDB-23, FDB-42	Integrated mass leaving the system through break junctions

26 seconds into the transient due to the mass depletion in the core inlet volume (mixer housing).

### 3.1 Break flow and system pressure

The break flow through the cold leg at the initial period of blowdown significantly disagrees with the experimentally observed data as seen in the Figure 3, though the reported mass flow rate data may contain some extent of errors due to inaccurate measurements of momentum flux and fluid density. On examination, the major discrepancy is attributable to the treatment of the discharge coefficient applied to both the subcooled and the saturated regions. The present ALARM-PI is modelled so as to use the same discharge coefficient irrespective of the two distinguished regions, which was 0.6 in the present calculation. Consequently, the Zaloudek critical flow at the subcooled or low quality phase ( $< 0.02$ ) underpredicted the test data, while the choked flow at the Moody's region is in better agreement.

On the other hand, the vessel side break flow (JW 29) in the Figure 4 was predicted pretty well because the fluid in the hot leg line flashed immediately after the rupture and the Zaloudek correlation had an insignificant effect on the flow through the valve. Thus, an improvement at the subcooled or low quality phase ( $< 0.02$ ) could evidently be made if a multiplier other than 0.6 was used to Zaloudek correlation. As can be seen in Figures 5 and 6, the overall decompression transient up to the ECC injection agreed reasonably with the S-06-3 measured data. The pressure profiles in both the broken loop cold leg and hot leg were almost correctly predicted. A slight pressure difference in the Figure might come from the resistance factor across the pump simulator (see Fig.8). Differential pressure across the steam generator simulator

was not far from agreement (see Figure 9). As indicated in the Figure 7, the upper-plenum pressure representative of the whole system pressure was estimated somewhat low, which resulted in the initiation of the accumulator flow earlier than observed (see Figure 13). After the start of ECC injection, the rapid depressurization in the calculation produced untraceable disagreement with the experimental data. For example, the measured temperature in the upper-plenum, as seen in the Figure 33, was in the superheated state unlike the calculated result. This problem is of particular importance in order to analyze the effect of ECCS. In the current model, an assumed instantaneous mixing of two different fluids causes an unphysically severe transient, and is the principal factor unabling the continuation of the calculations. In the lower-plenum calculation shown in the Figure 34, more control volumes should have been employed because the fluid temperature and flow were significantly different between lower and upper parts of the lower-plenum.

### 3.2 ECCS behaviors

As mentioned above, the initiation time of the accumulator injection was predicted slightly earlier (see Figures 10, 13). Moreover, the injection flow (volumetric) was overpredicted considerably from the measured data. This was mainly due to the fact that the system pressure was calculated to drop faster than that in the experiment.

In the Figure 10, the disagreement of the initial state prior to injection is unknown. ALARM-input data was taken from the reference (7). After the initiation of the coolant inflow, the incompatibility of the decompression rate between the two is possibly ascribable to overrating of gas volume input data. This value in the tank was input in accordance with the initial condition in the same reference. In addition the

calculated temperature in the accumulator line (see Figure 44) seemed unreasonable. On investigation, an error was found in the program which was solely responsible for such a temperature behavior.

The small differences in the temperature before injection may be improved by considering heat transfer between the structure and the fluid. At all events, the control volume in this surge line had better be removed from the model shown in the Figure 2. The behaviors of HPIS and LPIS were given in the Figures 11 and 12.

### 3.3 Rod surface temperature in low power heater

The surface temperature response in the average channels was calculated much lower than the experimental data. Temperature traces in Figures 14 to 17 were measured at elevations 8", 14", 28" and 39", respectively above the bottom of the core.

In the calculation, the heat transfer area and slab volume in the reactor core were determined for forty heater rods. In reality, heater rods were thirty six and the others unheated. This data should be corrected at the re-analyses. The predicted time of DNB at all elevations was slightly earlier as compared with the data. These figures indicate that the surface temperature increase tends to be arrested when heat transfer falls into the pool film boiling mode.

The current correlation in this mode is based on the Berenson's, which is insensitive to local flow conditions of the core inlet or outlet because it is represented as a simple function of the bulk pressure and  $\Delta T_{\text{sat}} \cdot (h = F(p)(\Delta T)^{\frac{4}{3}})$ . Accordingly, the heat transfer coefficients became stable in the pool film boiling mode as seen in Figs.35~38, and they were presumably too large resulting in the predicted low temperature. As used in the RELAP/MOD5,<sup>(14)</sup> the modified Bromley correlation may predict a lower coefficient than the Berenson model.

Rewetting phenomena were calculated during blowdown at the elevations 8" and 39", and at all elevations at the initiation of the accumulator injection while no rewetting was observed in the experiment. The reason of such unrealistic rewetting is now under examination.

### 3.4 Core flow

Although the core flow traces the test data to a considerable degree till the emergency cooling is initiated, the inflow of the accumulator liquid into the cold leg piping produced the drastic fluctuations (see Figure 18). The direction of the computed flow was predominantly downward. As seen in this figure, the ECC mixing model has a great influence on the core flow characteristics.

After 8 seconds did dissimilarity of the core flow directions make a significant difference in the density of core inlet volume (see Figure 19).

### 3.5 Temperature and density in the break volume

The temperature and density transient in the broken loop are shown in the Figures 20 to 22. The prediction of the pump side break density compares well to the data, while improvements should be directed to the cold leg density. The influence of ECCS is visible since 22 seconds.

### 3.6 Intact loop features

The comparisons of the intact loop characteristics are given in the Figures 23 to 31. The great fluctuations due to condensation effects by the ECC injection were manifestly demonstrated. With the exception of this problem, the calculated results were generally close to the

experimental data. The predictions of the pressurizer and steam generator secondary system are necessary to be improved (see Figures 27 to 30). Probably the one ascribes to input data such as the K-factor,  $\lambda/A$  and bubble rise data while the other to the timing of a trip action in the fill/leak systems.

#### 4. Conclusions

Based on the calculation results obtained, the following conclusions were reached. Only the blowdown portion of the S-06-3 Test was evaluated due to the inability of this code to calculate the refill/reflood behaviors. The prediction of the fluid pressure, density and the temperature up to the ECC injection was reasonably satisfactory. The overall system behavior after the ECC injection was far from satisfaction unabling the further continuation of the computation.

The surface temperature was much underpredicted. The cause of this underprediction should be carefully examined. Through the present analysis, the following several problems to be improved were found. These informations acquired are expected to serve the betterment of the present results or the future code assessment study.

##### (A) Input data

1. Corrections to provide more exact representation for all the junction configuration such as inertia and formloss coefficients (In particular, the inlet and outlet of the pressurizer, steam generator and the pressure vessel).
2. Nodarization  
Removal of ECC surge line. Two or more control volumes for the lower plenum, two channel model for the downcomer.

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Removal of ECC surge line. Two or more control volumes for the lower plenum, two channel model for the downcomer.



3. ECCS

Examination of the accumulator gas volume shown in the reference.

4. Core

Correction of the heat transfer data in the core by reducing four heater pins' area and volume.

5. Steam generator

A more reasonable data set about fill/leak trip data in the steam generator secondary side.

6. Time Step

A smaller size after the accumulator injection.

(B) Analytical models in the code

1. The treatment of the contraction coefficients in the critical flows
2. Heat transfer correlation and mode selection to make the quantitative investigations between Bromley and Berenson model in the pool film boiling.
3. Modification of the junction enthalpy routine.
4. Check of numerical values in two-phase friction multiplier given in block data (In particular, in Martinelli-Nelson region).
5. Modification of the pump model so as to give a more reasonable revolution during blowdown.
6. Condensation effects due to mixing during the emergency cooling water injections

5. References

- (1) B.L. Collins, et al., "Experiment Data Report for Semiscale Mod-1 Test S-06-3 (LOFT Counterpart Test)", NUREG/CR-0251, TREE-1123, July, 1978

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- (1) B.L. Collins, et al., "Experiment Data Report for Semiscale Mod-1 Test S-06-3 (LOFT Counterpart Test)", NUREG/CR-0251, TREE-1123, July, 1978

- (2) L.J. Ball, et al., "Semiscale Program Description", TREE-NUREG-1210, May, 1978
- (3) W.D. Laning, "System Design Description for the 1-1/2-Loop Mod-1 Semiscale System" (SDD1), June, 1975
- (4) E.M. Feldman, D.J. Olson, "Semiscale Mod-1 Program and System Description for the Blowdown Heat Transfer Tests (TEST SERIES 2)", ANCR-1230, August, 1975
- (5) L.E. Phillips, letter to International Standard Problem Participants, "Reference for Standard Problem NO.8 (Semiscale Test S-06-3)", May 8, 1978
- (6) Appendix 6 Experimental Operating Specifications Tests S-06-1 through S-06-5 LOFT Counterpart Tests in the Mod-1 System (Test Series 6) Semiscale Program, February, 1977
- (7) D.J. Olson, letter to R.E. Tiller, "Transmittal of Initial Conditions-Semiscale Mod-1 Test S-06-3 (Regulatory Standard Problem 8)", DJO-222-77, November 28, 1977
- (8) D.J. Olson, letter to R.E. Tiller, "Test S-06-3 (Standard Problem 8) PSS Prenure", DJO-4-78
- (9) D.J. Olson, letter to R.E. Tiller, "Transmittal of Additional Requested Conditions-Semiscale Mod-1 Test S-06-3 (Regulatory Standard Problem 8)", DJO-35-78, March 28, 1978
- (10) L.E. Phillips to International Standard Problem Participants, "Additional Informations-CSNI Standard Problem NO.8" (Semiscale Test S-06-3), December 21, 1978
- (11) P.M. Lang to P.E. Litteneker, "Transmittal of Mod-1 Experimental Operating Specification", PML-32-74, January 31, 1974
- (12) K. Soda, et al., "LFTPLT7-LOFT Plotter Program", JAERI-M 7695, April 27, 1978
- (13) K. Soda, et al., "Editing System of LOFT Data Tape", JAERI-memo 7861, September, 1978
- (14) "RELAP4/MOD5 — A Computer Program for Transient Thermal-Hydraulic Analysis of Nuclear Reactors and Related Systems user's manual", Volume 1, ANCR-NUREG-1335, September 1976

COMPARISON OF SEMISCALE S-06-3 DATA AND ALARM-P1 ANALYSIS

□ FA000263 ○ A JWJ30

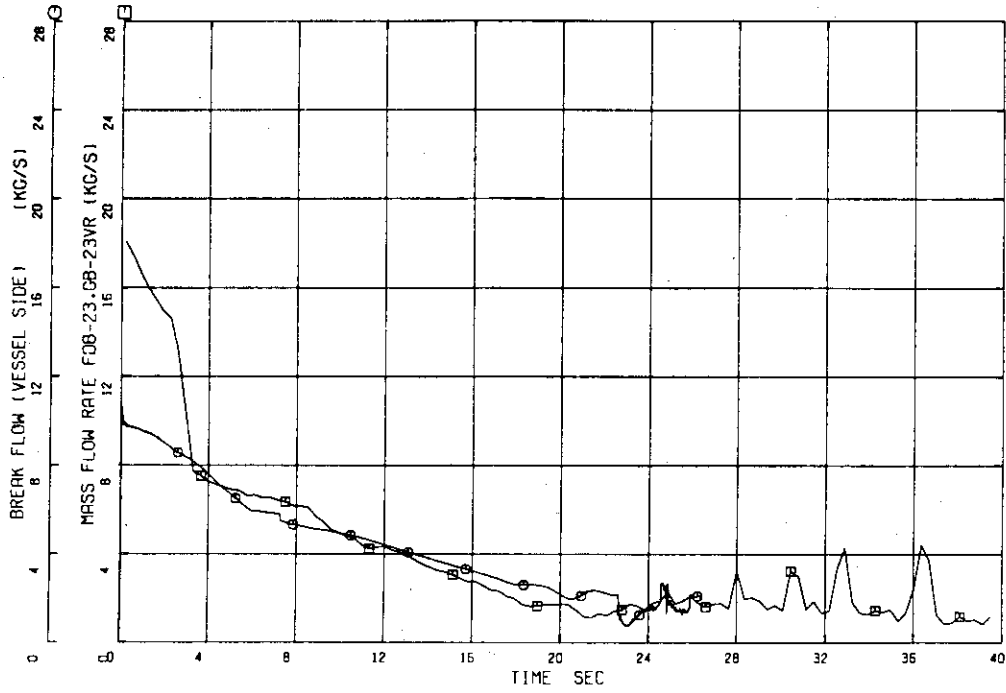


Fig.3 Mass Flow Rate at Break Nozzle — Reactor Vessel Side (FDB-23, GB-23VR)

COMPARISON OF SEMISCALE S-06-3 DATA AND ALARM-P1 ANALYSIS

□ FA000281 ○ A JWJ29

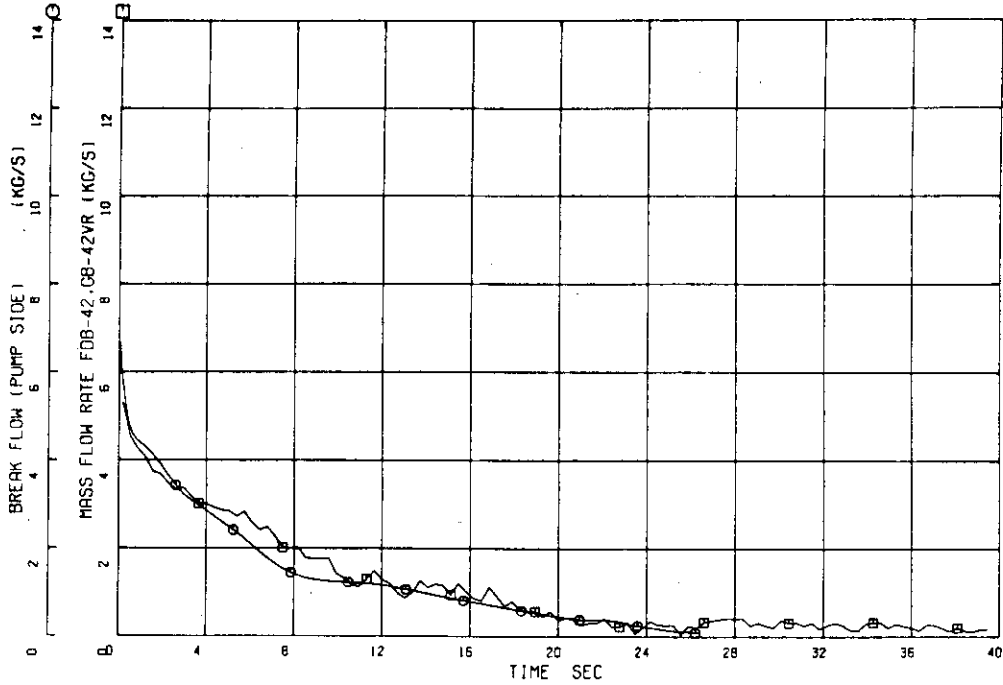


Fig.4 Mass Flow Rate at Break Nozzle — Pump Side (FDB-42, GB-42VR)

COMPARISON OF SEMISCALE S-06-3 DATA AND ALARM-P1 ANALYSIS

□ PG000073 ○ A APV17

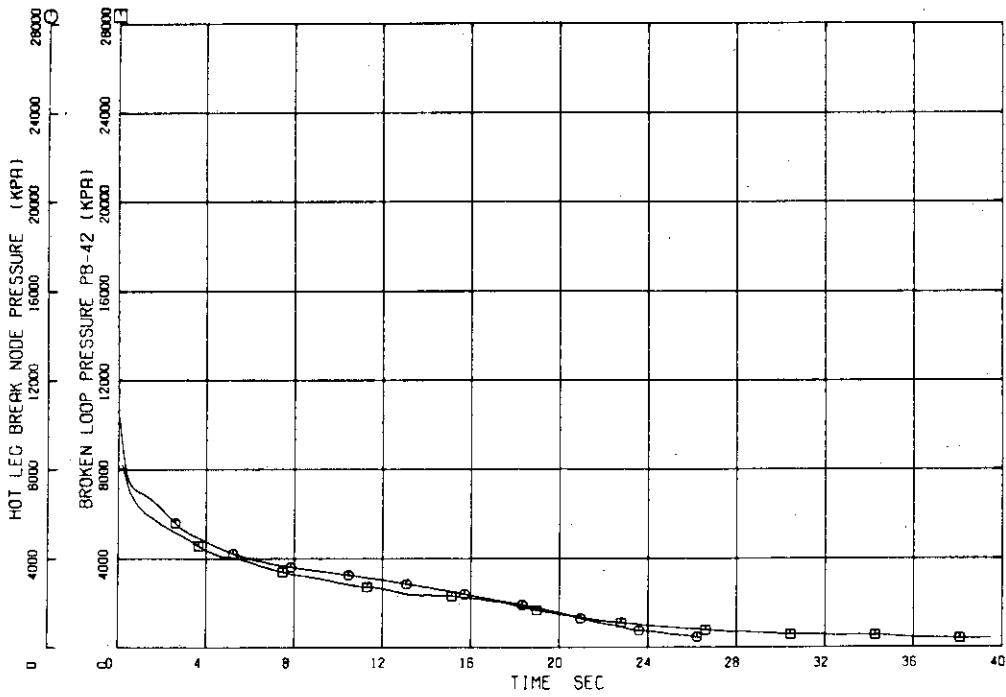


Fig.5 Pressure History Upstream of Break Nozzle — Pump Side (PB-42)

COMPARISON OF SEMISCALE S-06-3 DATA AND ALARM-P1 ANALYSIS

□ PG000072 ○ A APV35

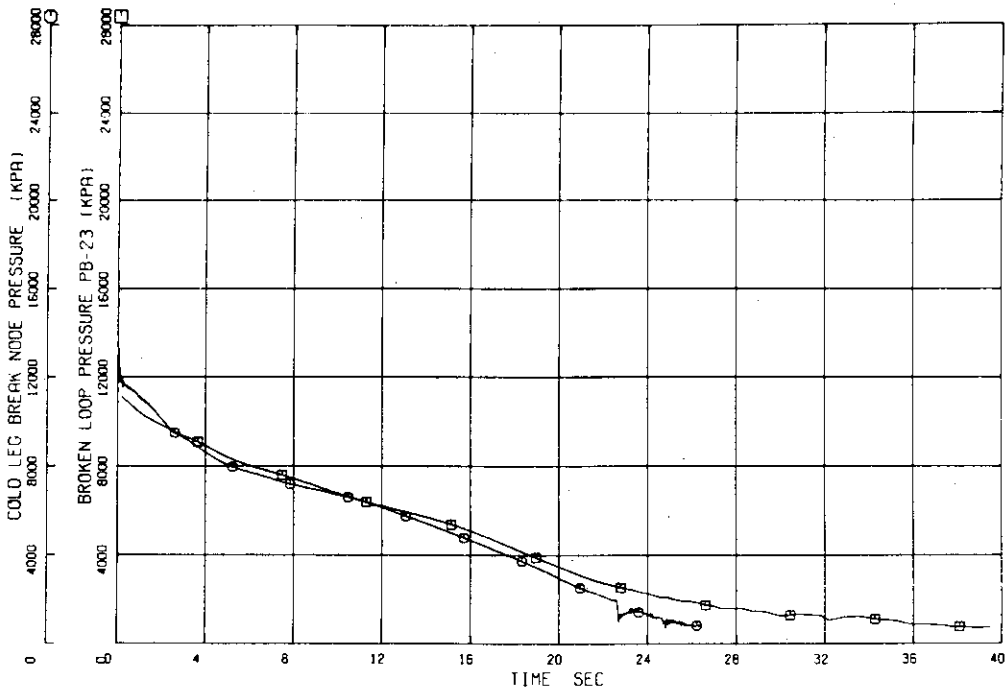


Fig.6 Pressure History upstream of Break Nozzle — Reactor Vessel Side (PB-23)

COMPARISON OF SEMISCALE S-06-3 DATA AND ALARM-P1 ANALYSIS

□: PG000046 ○: A APV25

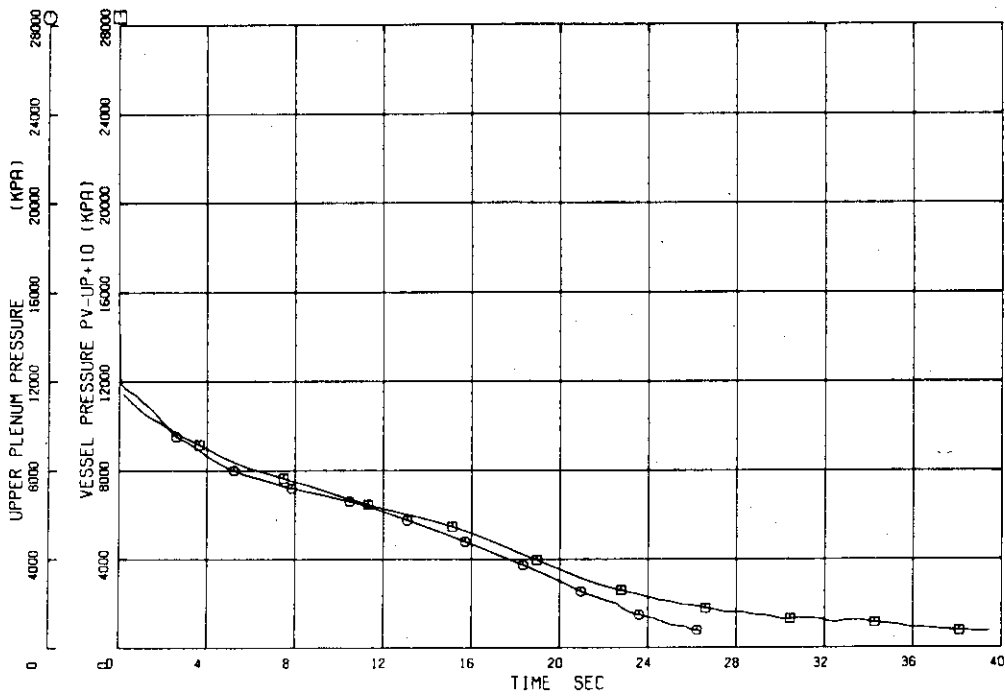


Fig.7 Upper Plenum Pressure History (PV-UP+10)

COMPARISON OF SEMISCALE S-06-3 DATA AND ALARM-P1 ANALYSIS

□: PD000081 ○: A TOJ3

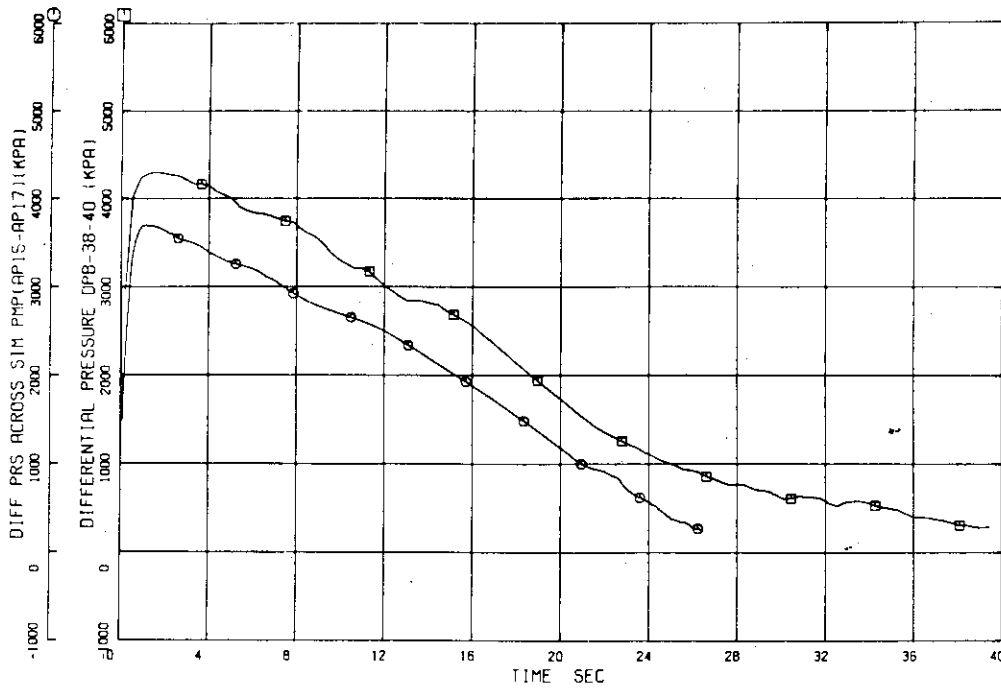


Fig.8 Differential Pressure Across the Simulated Pump (DPB-38-40)

COMPARISON OF SEMISCALE S-06-3 DATA AND ALARM-P1 ANALYSIS

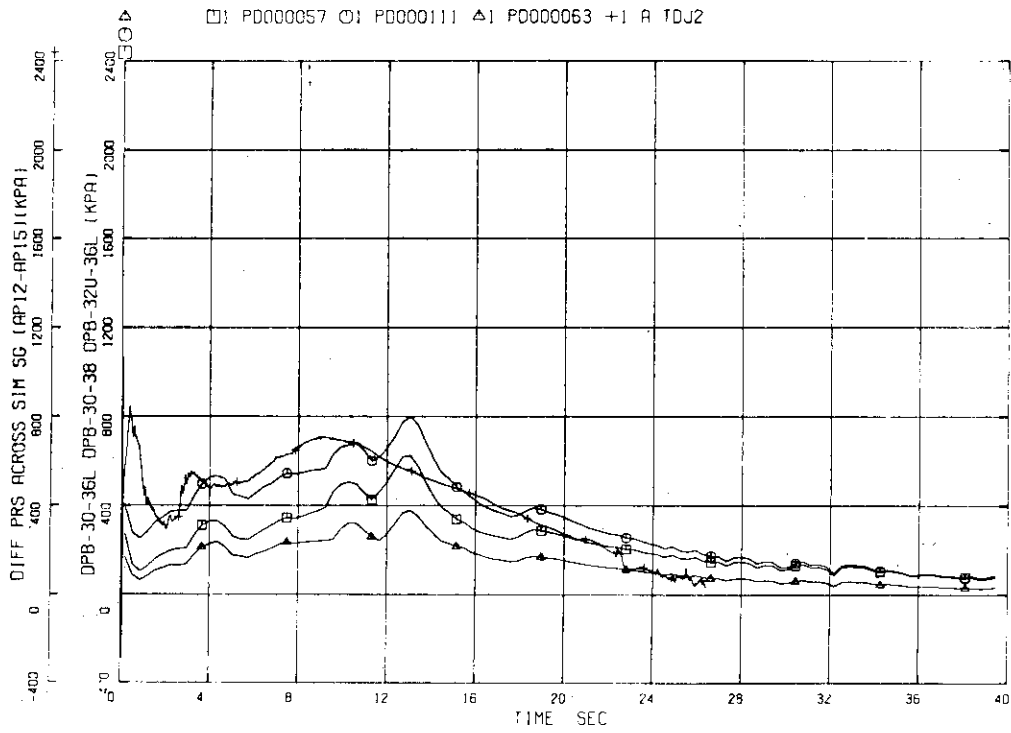


Fig.9 Differential Pressure Across the Simulated Steam Generator (DPB-32U-36L)

COMPARISON OF SEMISCALE S-06-3 DATA AND ALARM-P1 ANALYSIS

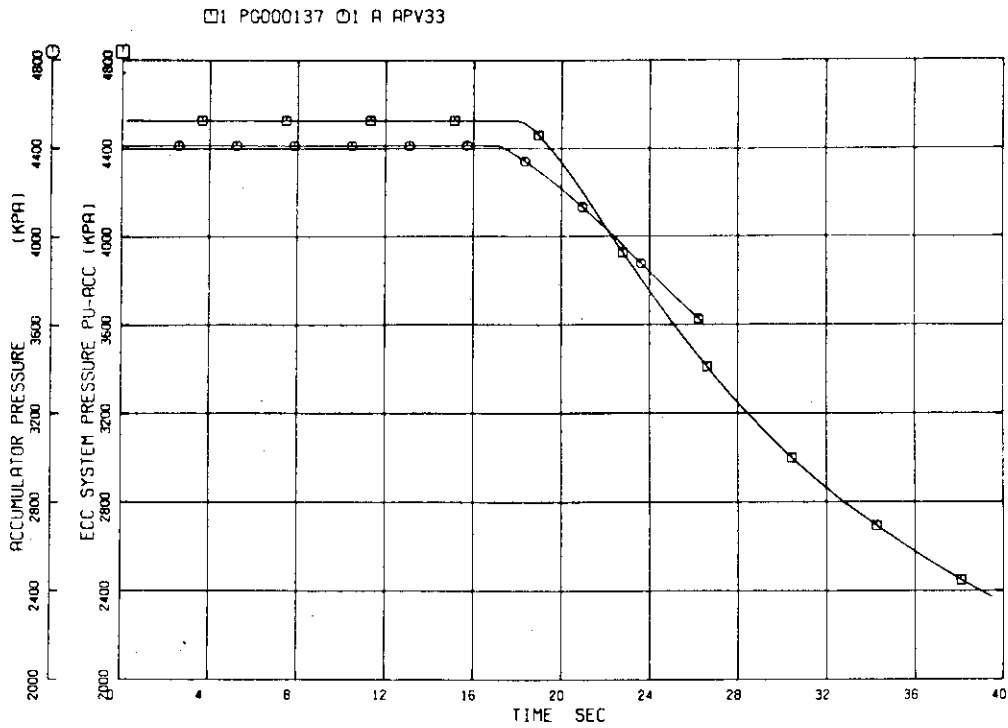


Fig.10 Intact Loop Accumulator Pressure History (PU-ACC)

COMPARISON OF SEMISCALE S-06-3 DATA AND ALARM-P1 ANALYSIS

□ FV000016 ○ A JWJ37

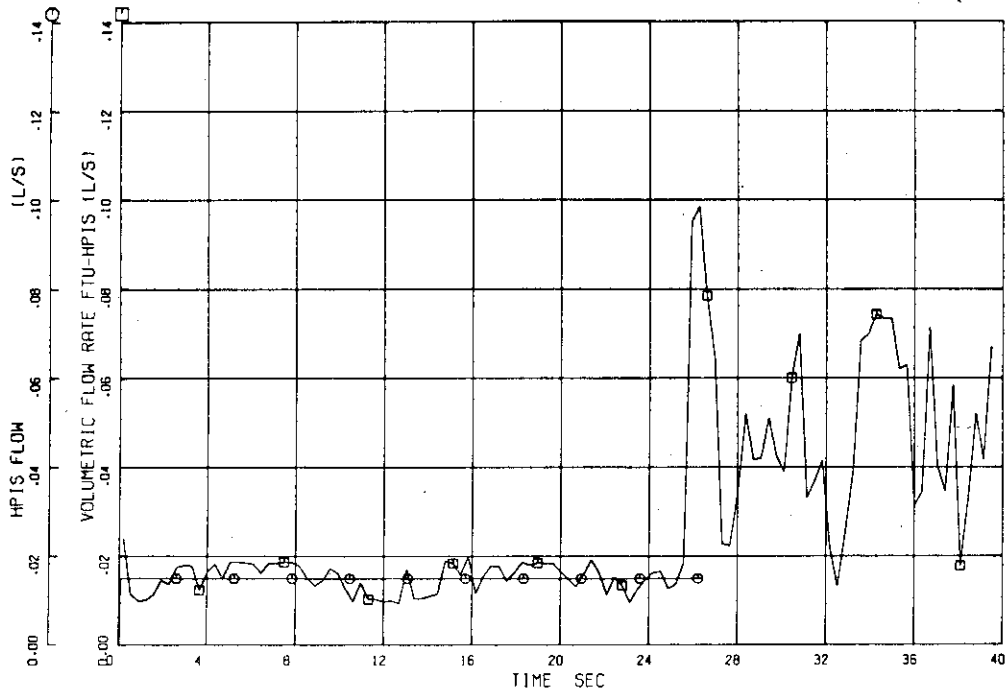


Fig.11 Volumetric Flow Rate in Intact Loop HPIS (FTU-HPIS)

COMPARISON OF SEMISCALE S-06-3 DATA AND ALARM-P1 ANALYSIS

□ FV000017 ○ A JWJ38

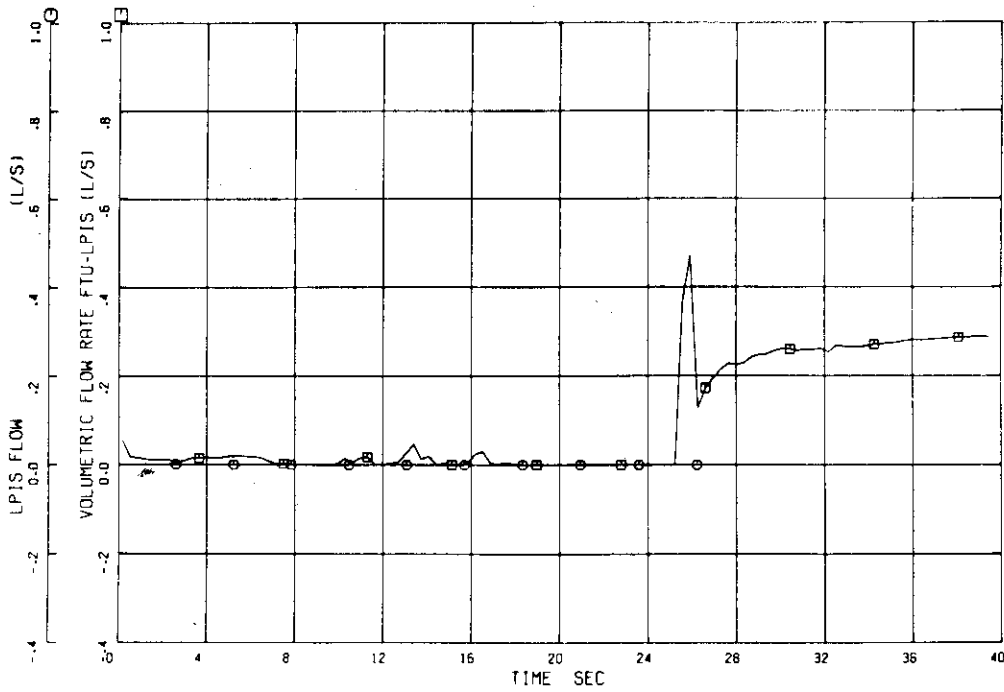


Fig.12 Volumetric Flow Rate in Intact Loop LPIS (FTU-LPIS)



COMPARISON OF SEMISCALE S-06-3 DATA AND ALARM-P1 ANALYSIS

□ FV000022 ○ A JWJ35

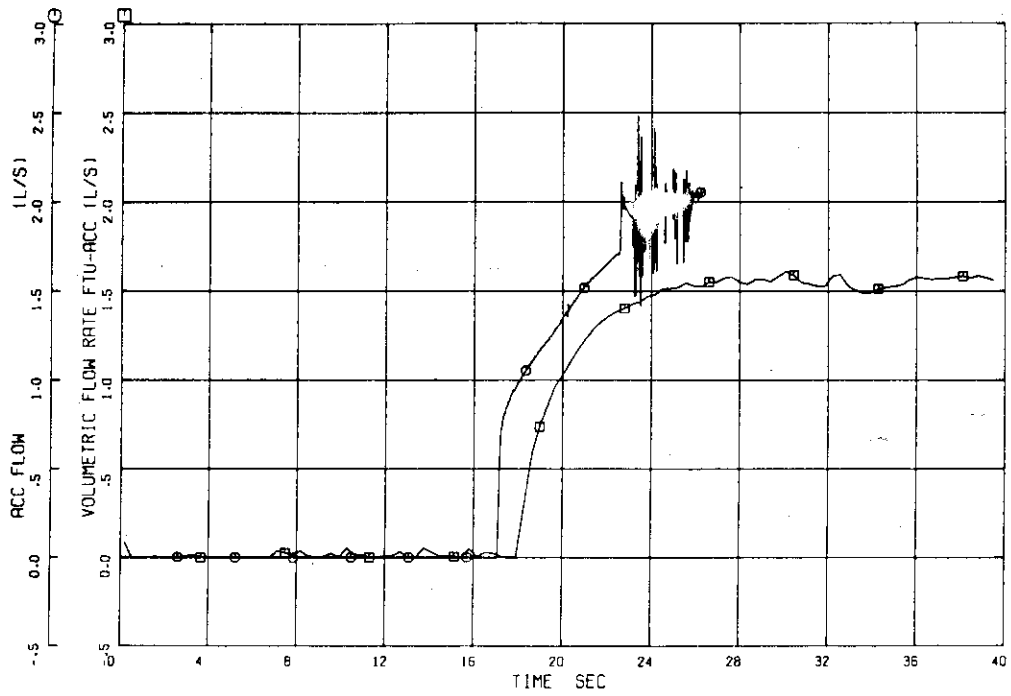


Fig.13 Volumetric Flow Rate in Accumulator Tank (FTU-ACC)

COMPARISON OF SEMISCALE S-06-3 DATA AND ALARM-P1 ANALYSIS

□ TE000154 ○ TE000179 △ A STV28

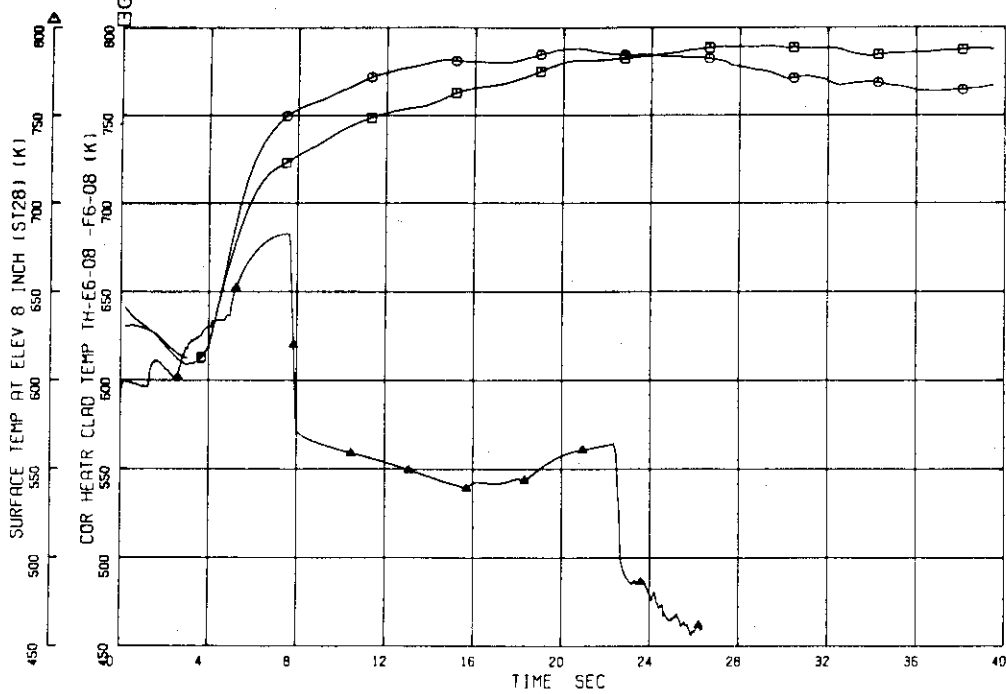


Fig.14 Surface Temperature History on Average Rods (Elevation of 8" above Bottom of Heated Length)

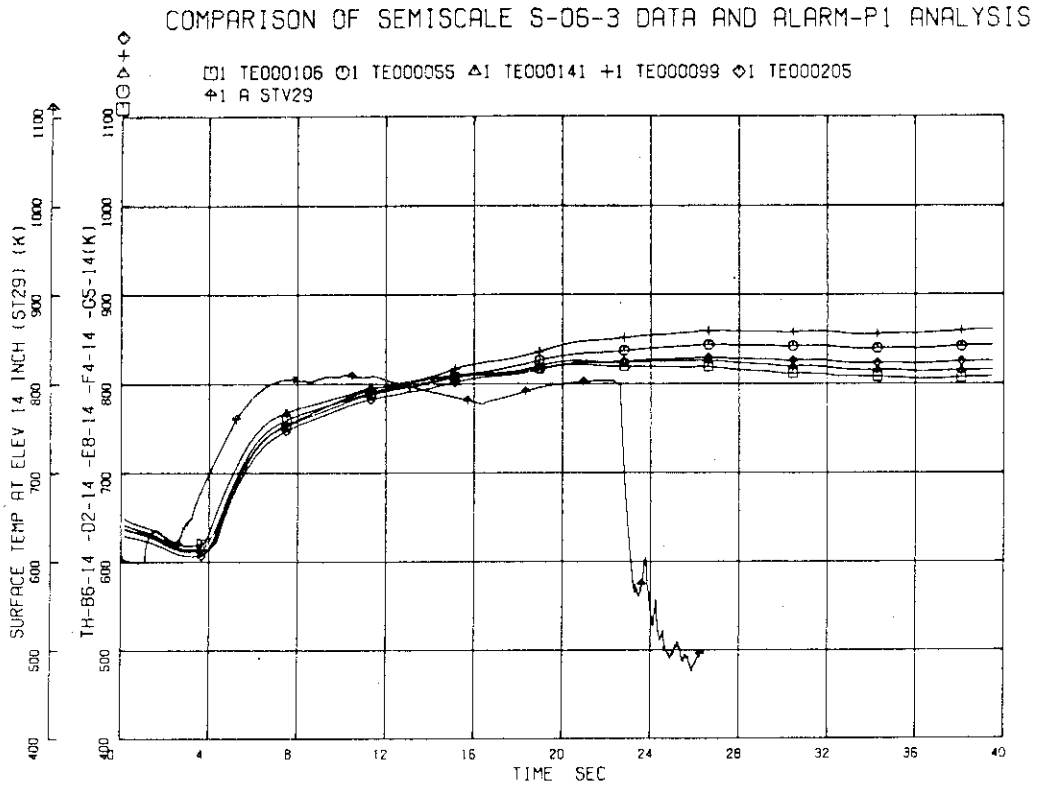


Fig.15 Surface Temperature History on Average Rods (Elevation of 14" above Bottom of Heated Length)

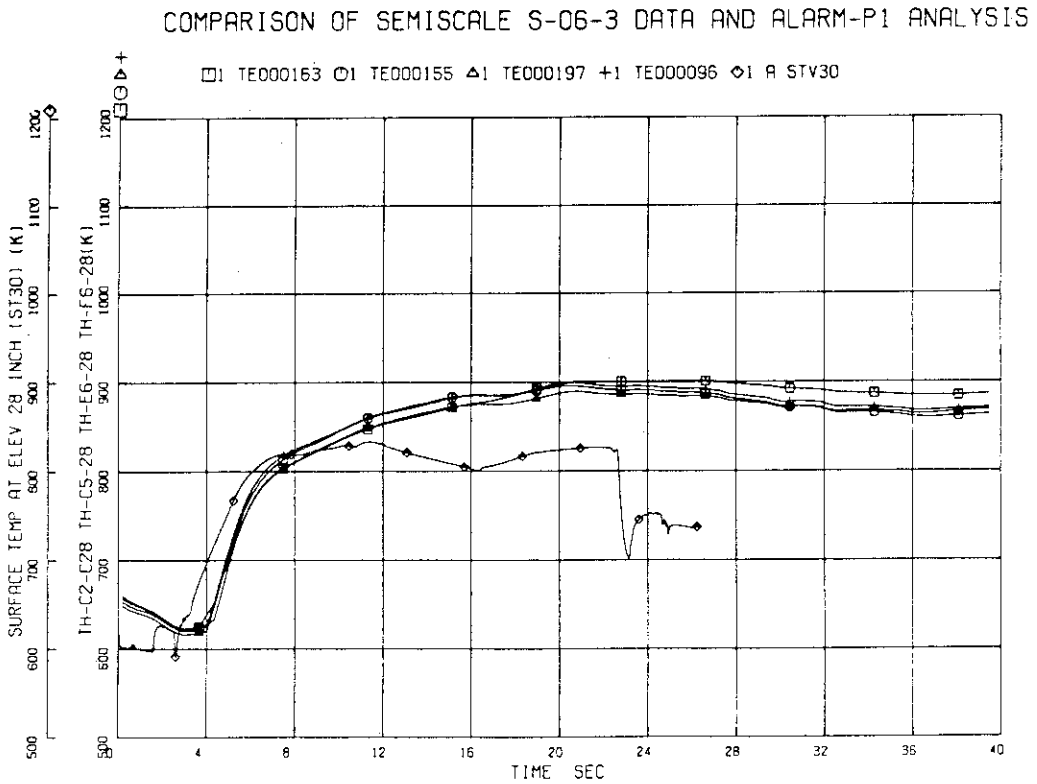


Fig.16 Surface Temperature History on Average Rods (Elevation of 28" above Bottom of Heated Length)

COMPARISON OF SEMISCALE S-06-3 DATA AND ALARM-P1 ANALYSIS

□ TE000190 ○ A STV31

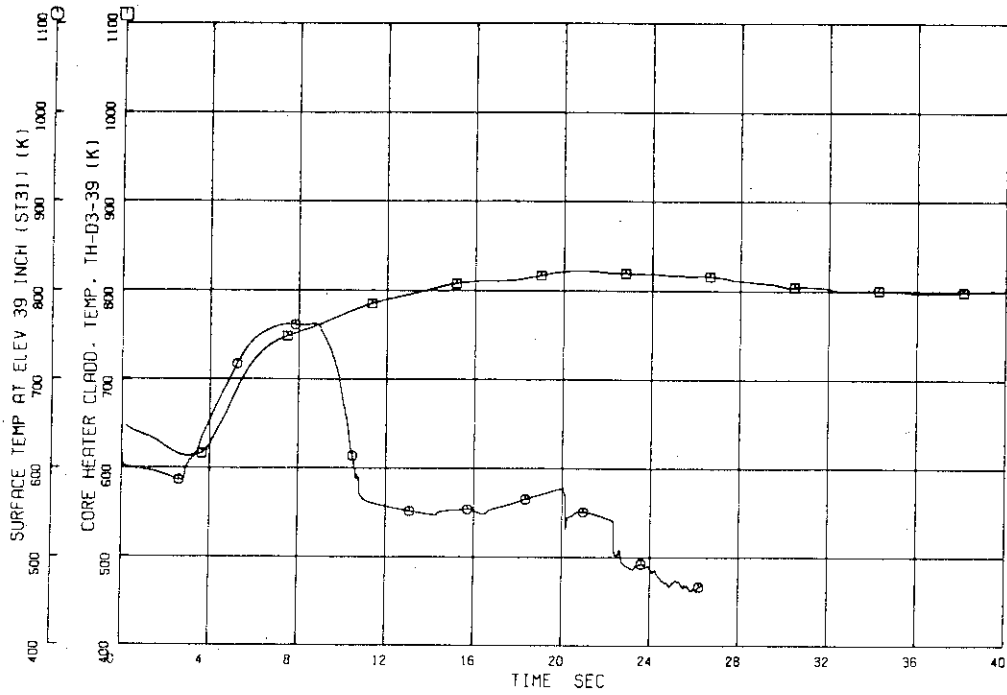


Fig.17 Surface Temperature History on Average Rods (Elevation of 39" above Bottom of Heated Length)

COMPARISON OF SEMISCALE S-06-3 DATA AND ALARM-P1 ANALYSIS

□ FV000010 ○ A JWJ27

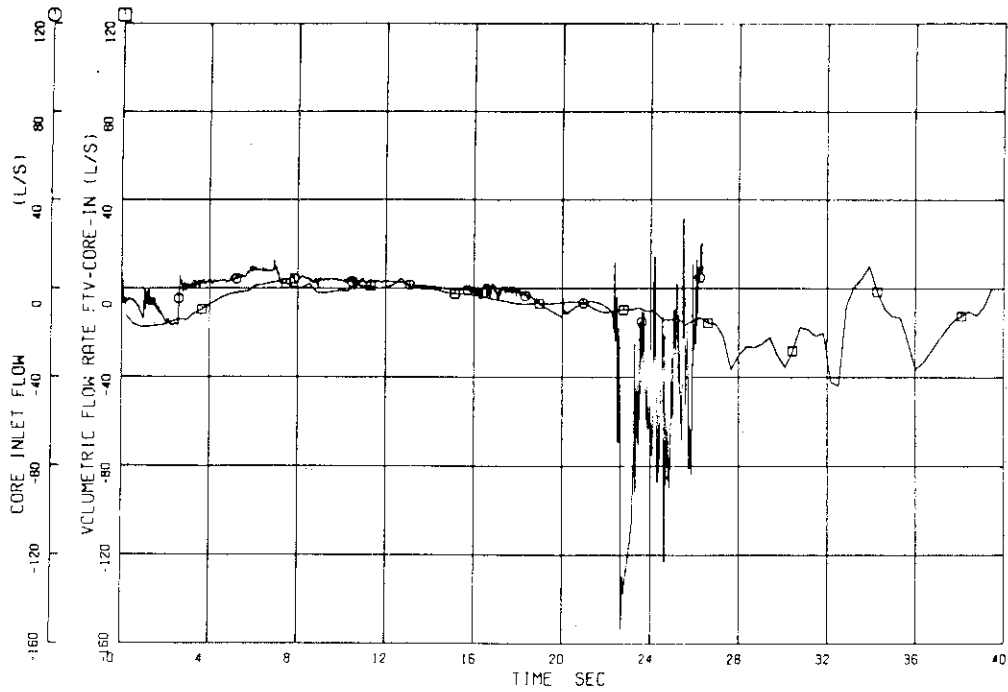


Fig.18 Volumetric Flow Rate at Core Inlet (FTV-COREIN)

COMPARISON OF SEMISCALE S-06-3 DATA AND ALARM-P1 ANALYSIS

□ DE000212 ○ A ARV25

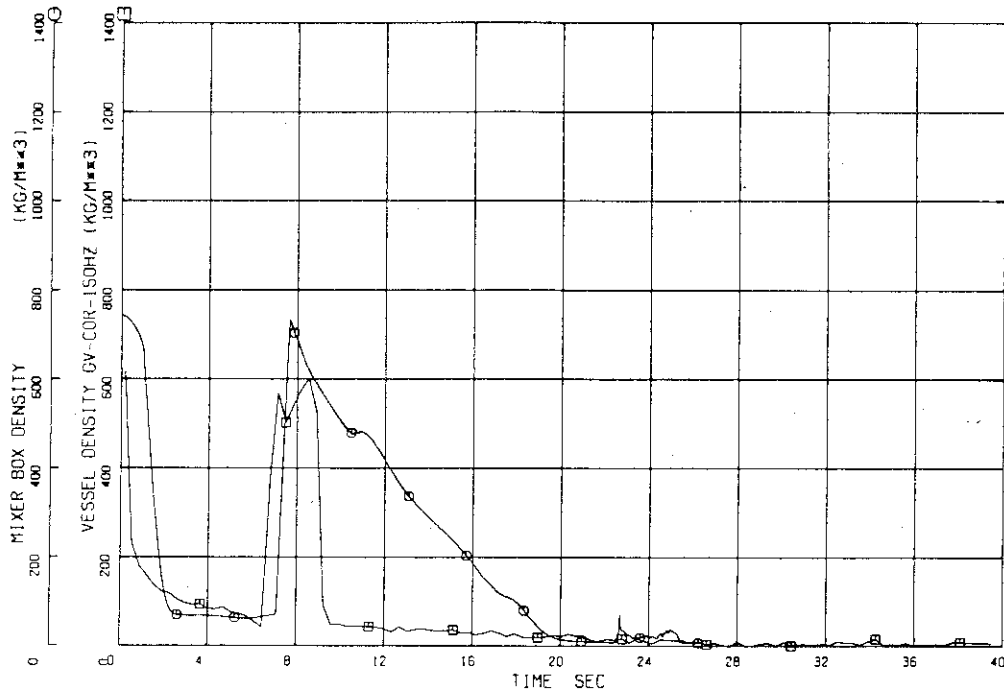


Fig.19 Density History at Core Inlet (GVCOR-150HZ)

COMPARISON OF SEMISCALE S-06-3 DATA AND ALARM-P1 ANALYSIS

□ DE000217 ○ A ARV17

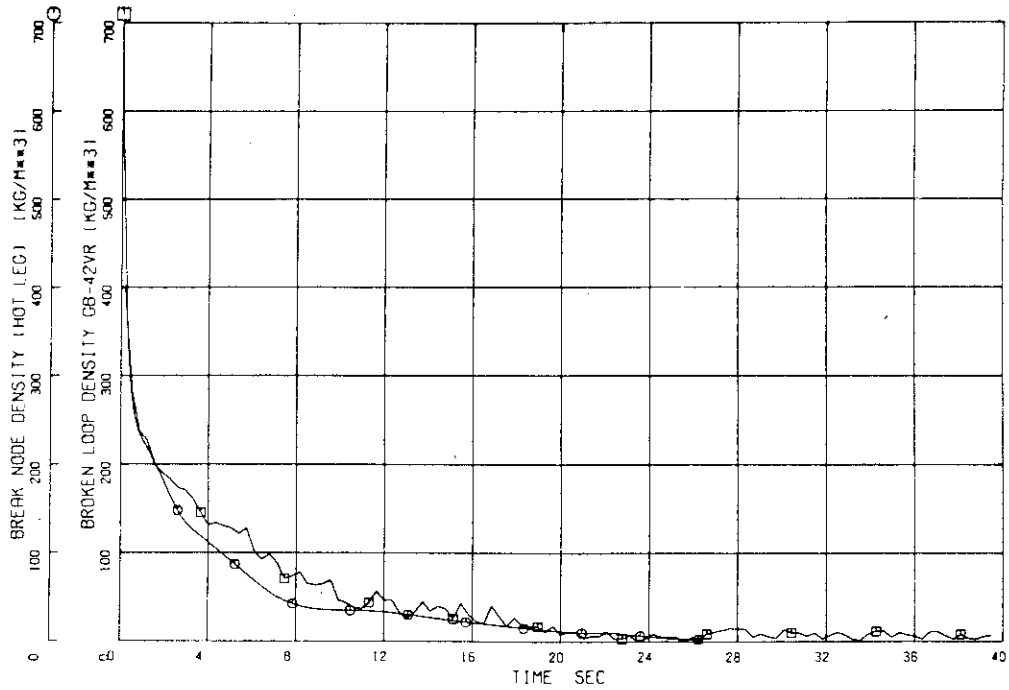


Fig.20 Density History in Break Volume — Pump Side (GB-42VR)

COMPARISON OF SEMISCALE S-06-3 DATA AND ALARM-P1 ANALYSIS

□ DE000219 ○ A ARV35

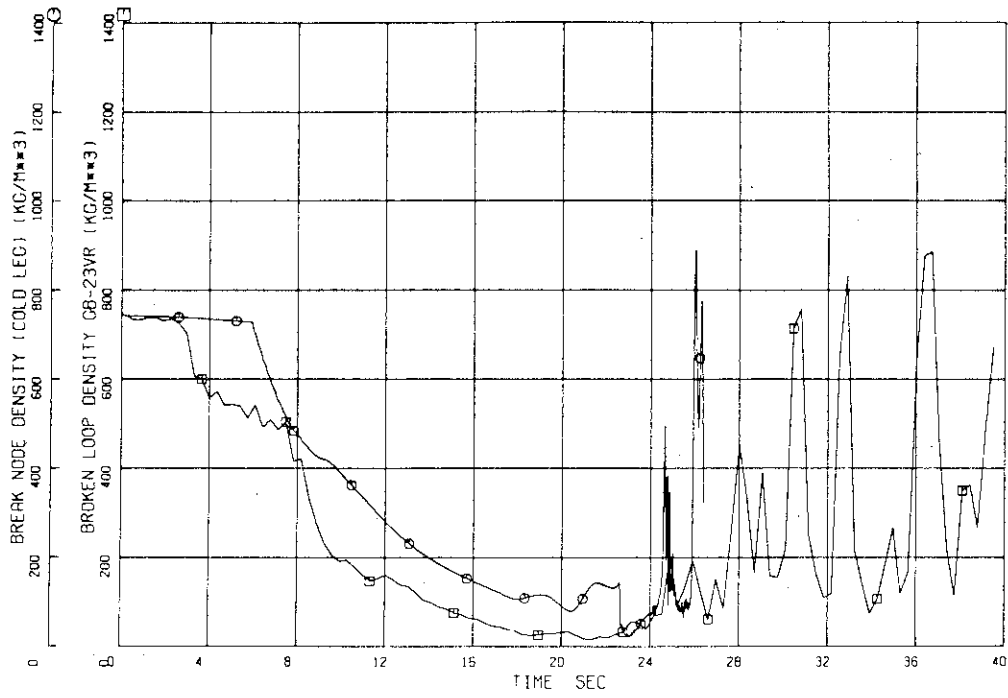


Fig.21 Density History in Break Volume — Reactor Vessel Side (GB-23VR)

COMPARISON OF SEMISCALE S-06-3 DATA AND ALARM-P1 ANALYSIS

□ TE000149 ○ A ATV35

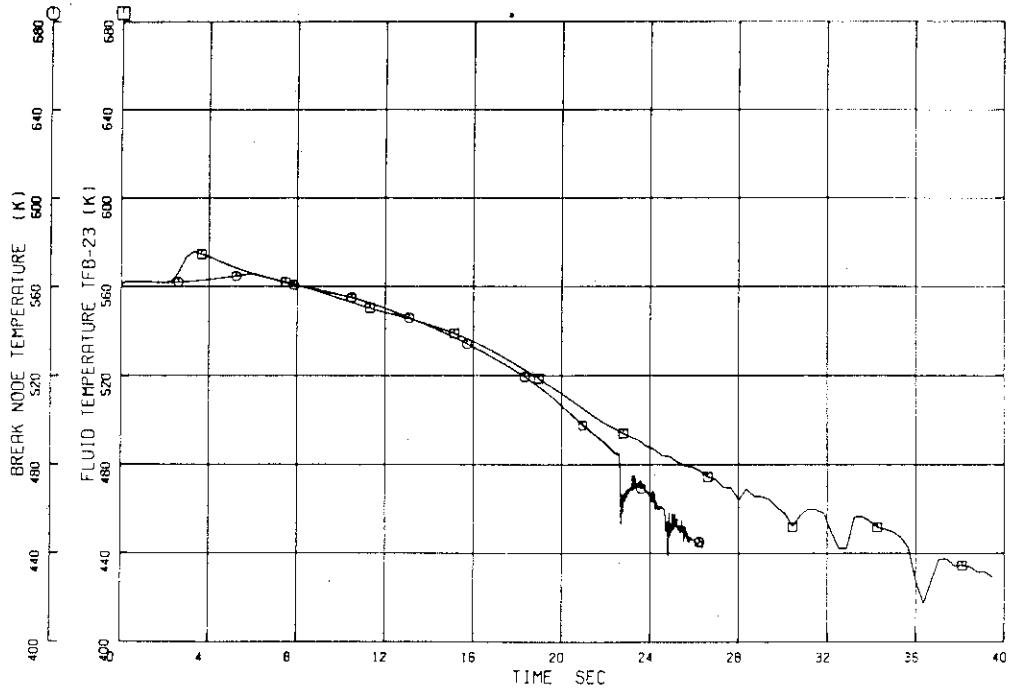


Fig.22 Fluid Temperature History Upstream of Break (TFB-23)

COMPARISON OF SEMISCALE S-06-3 DATA AND ALARM-P1 ANALYSIS

□ FV000004 ○ A JWJ10

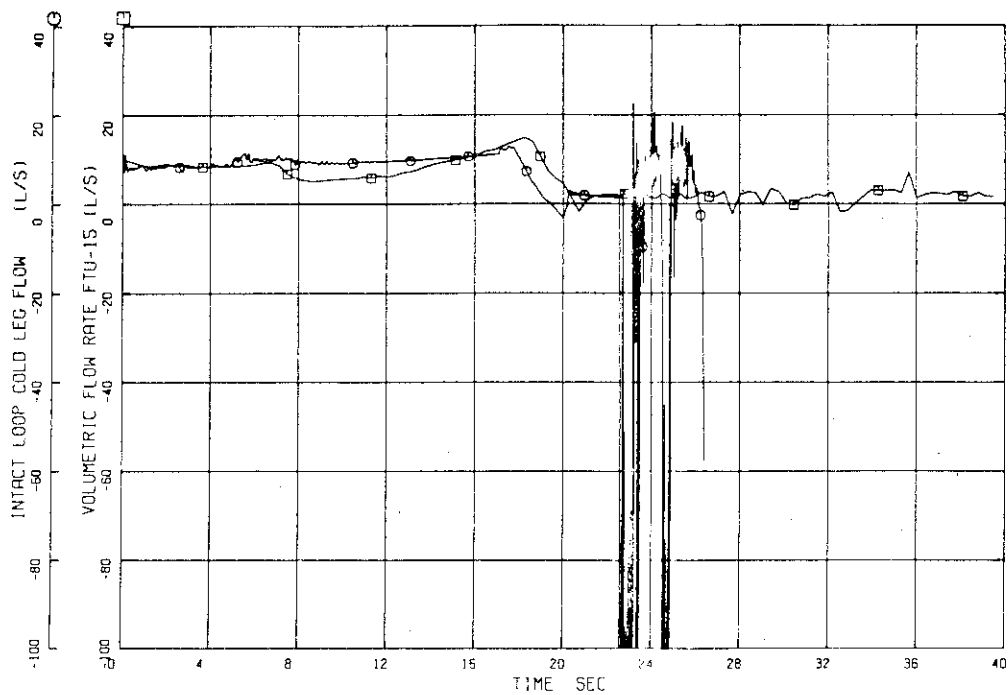


Fig.23 Volumetric Flow Rate in Intact Loop Cold Leg (FTU-15)

COMPARISON OF SEMISCALE S-06-3 DATA AND ALARM-P1 ANALYSIS

□ FA000359 ○ A JWJ7

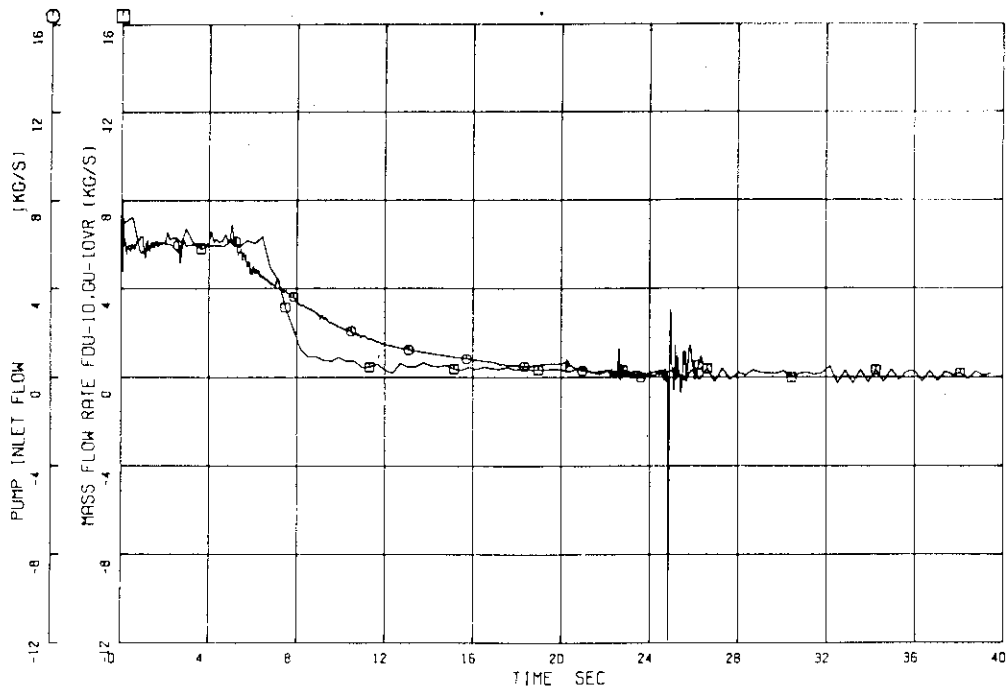


Fig.24 Mass Flow Rate in Spool 10 (FDU-10, GU-10VR)

COMPARISON OF SEMISCALE S-06-3 DATA AND ALARM-P1 ANALYSIS

□ DE000214 ○ A ARV6

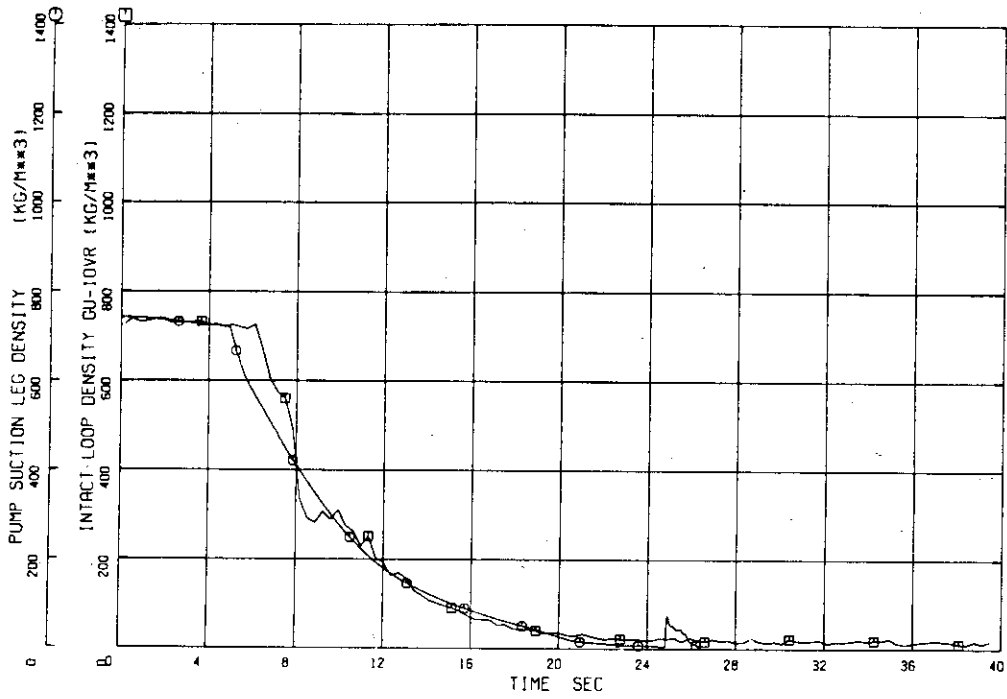


Fig.25 Density History at Pump Inlet (GU-10VR)

COMPARISON OF SEMISCALE S-06-3 DATA AND ALARM-P1 ANALYSIS

□ DE000239 ○ A ARV9

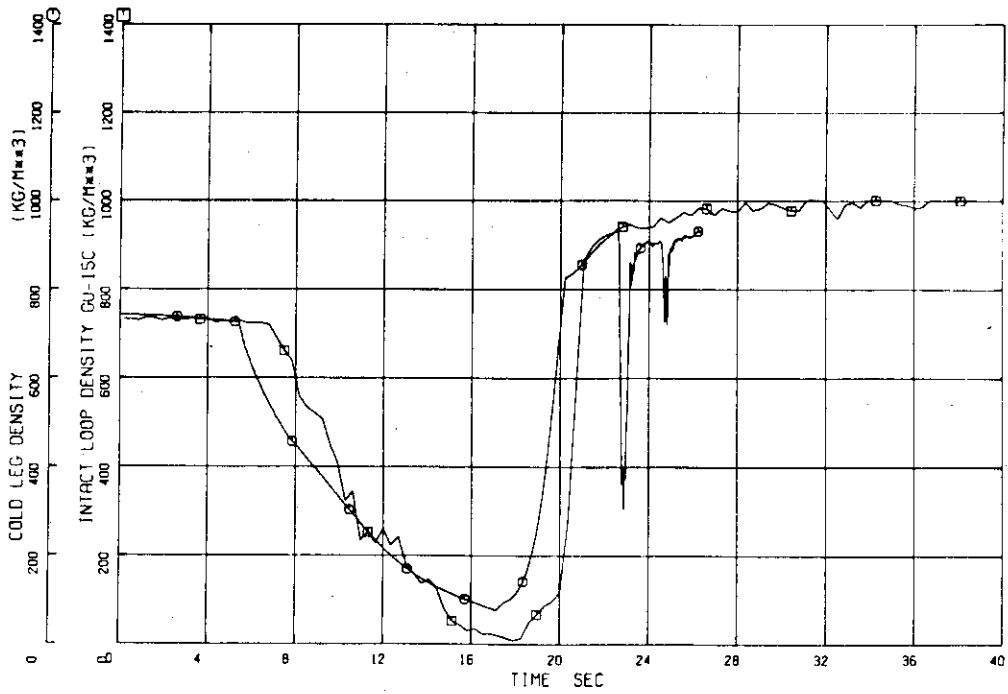


Fig.26 Density History in Intact Loop Cold Leg (GU-15C)

COMPARISON OF SEMISCALE S-06-3 DATA AND ALARM-P1 ANALYSIS

□ FV000020 ○ A JWJ12

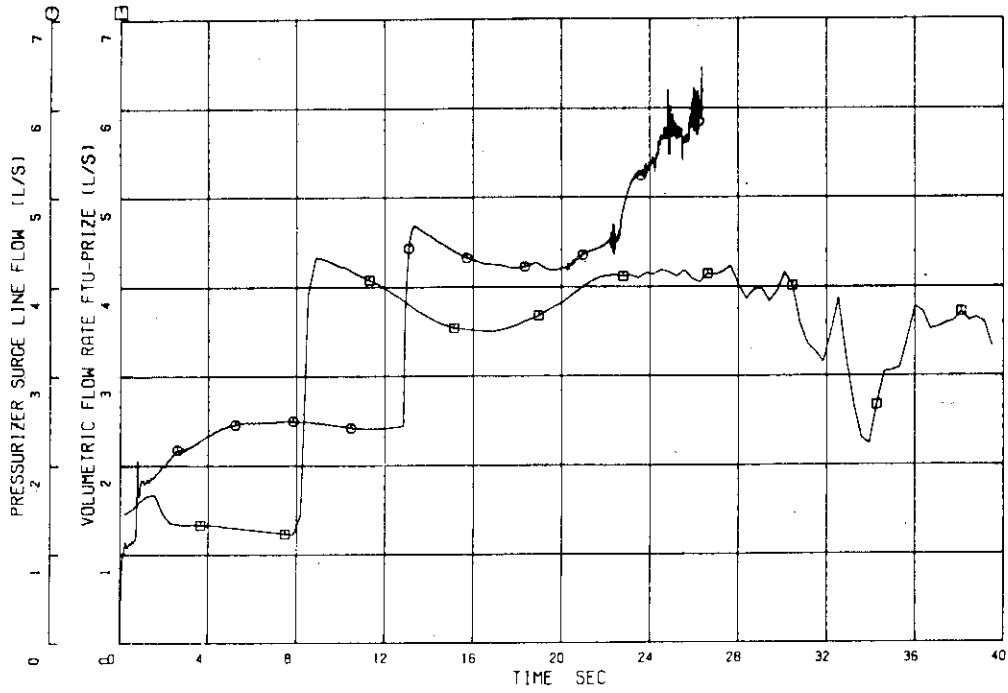


Fig.27 Volumetric Flow Rate in Pressurizer Surge Line Outlet (FTU-PRIZE)

COMPARISON OF SEMISCALE S-06-3 DATA AND ALARM-P1 ANALYSIS

□ TE000080 ○ A ATV11

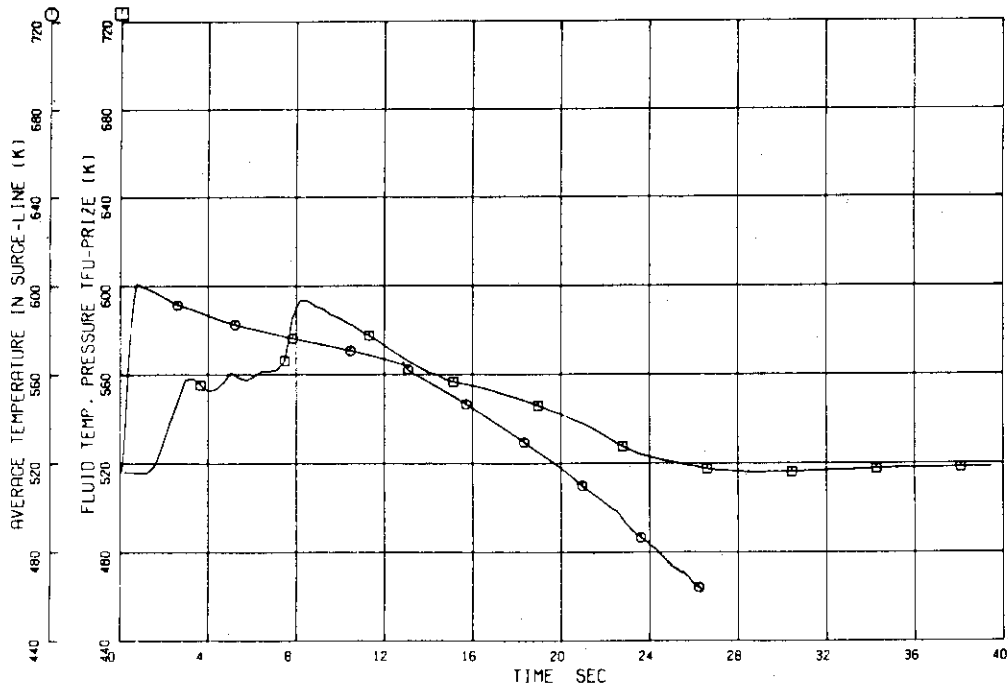


Fig.28 Fluid Temperature History in Pressurizer Surge Line (TFU-PRIZE)



COMPARISON OF SEMISCALE S-06-3 DATA AND ALARM-P1 ANALYSIS

□ PG000056 ○ A APV10

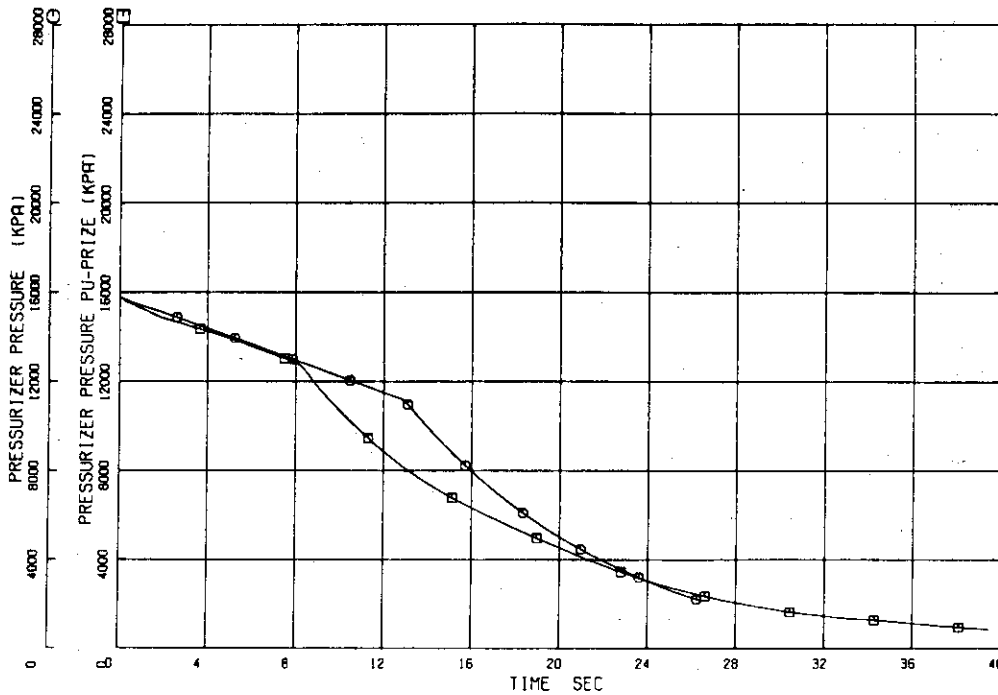


Fig.29 Pressurizer Pressure History (PU-PRIZE)

COMPARISON OF SEMISCALE S-06-3 DATA AND ALARM-P1 ANALYSIS

□ PG000043 ○ A APV21

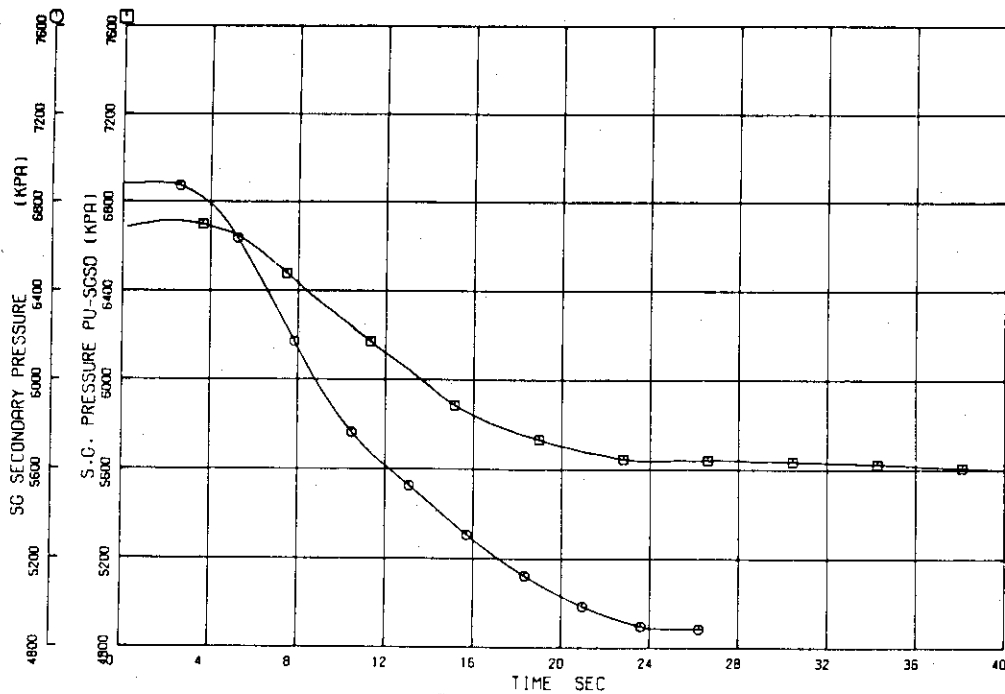


Fig.30 Pressure History in the Steam Generator Secondary System (PU-SGSD)

COMPARISON OF SEMISCALE S-06-3 DATA AND ALARM-P1 ANALYSIS

□ P0000093 ○ P0000094 ▲ A TOJ1

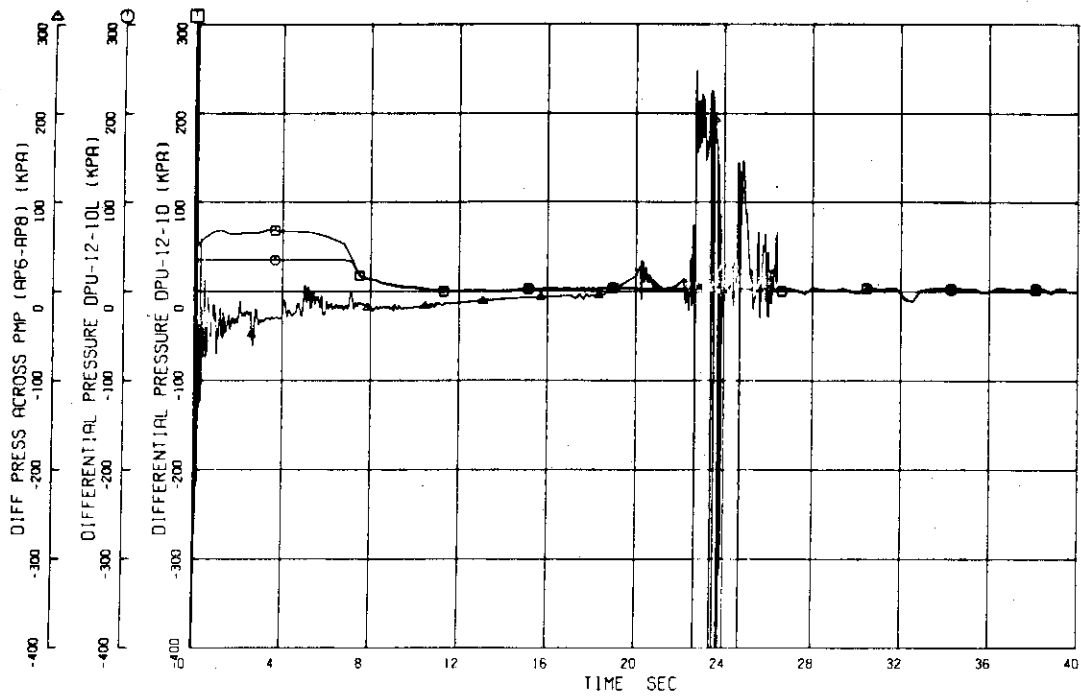


Fig.31 Differential Pressure Across Pump (DPU-12-10)

COMPARISON OF SEMISCALE S-06-3 DATA AND ALARM-P1 ANALYSIS

□ P0000120 ○ A TOJ4

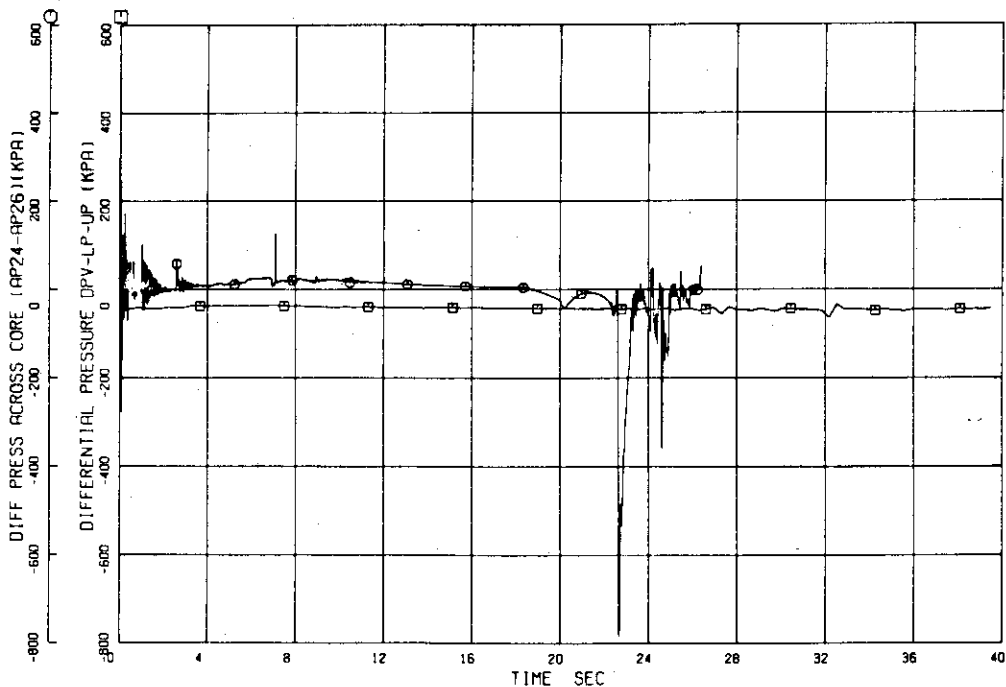


Fig.32 Differential Pressure Across Core (DPV-LP-UP)

COMPARISON OF SEMISCALE S-06-3 DATA AND ALARM-P1 ANALYSIS

□ TE000135 ○ R ATV26

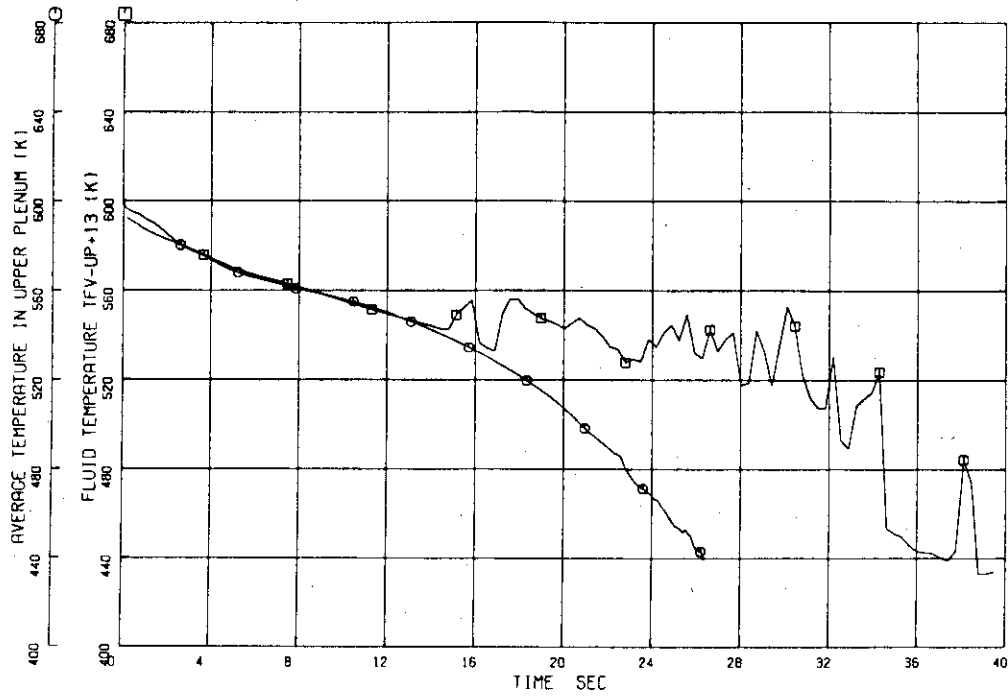


Fig.33 Fluid Temperature History in Upper Plenum (TFV-UP+13)

COMPARISON OF SEMISCALE S-06-3 DATA AND ALARM-P1 ANALYSIS

□ DE000221 ○ DE000211 ▲ R ARV24

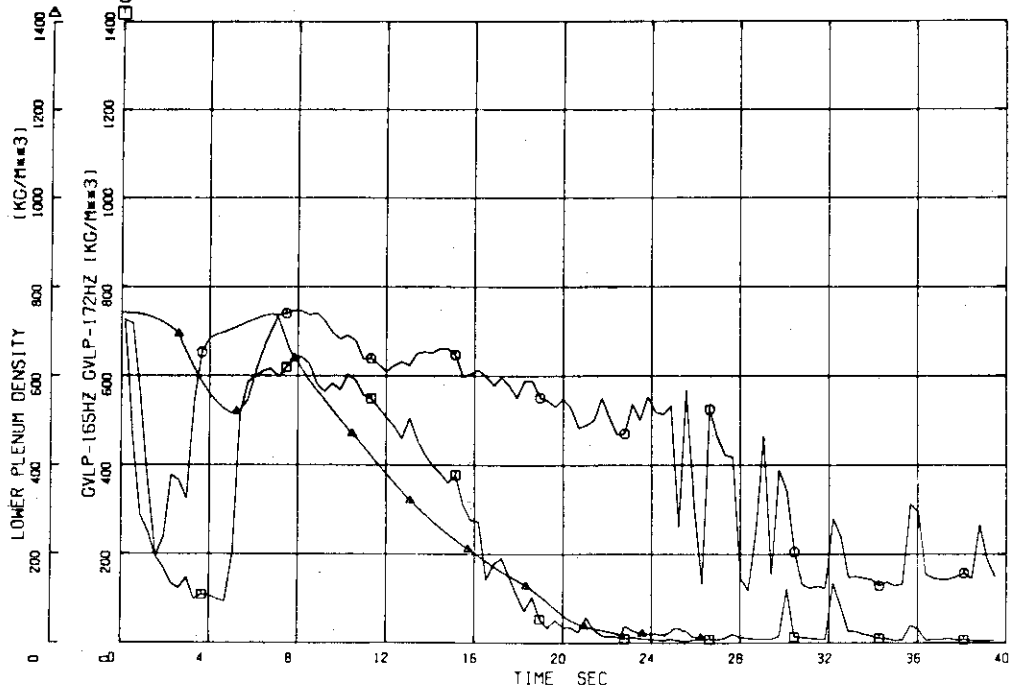


Fig.34 Density History in Lower Plenum (GV161/192D)

COMPARISON OF SEMISCALE S-06-3 DATA AND ALARM-P1 ANALYSIS

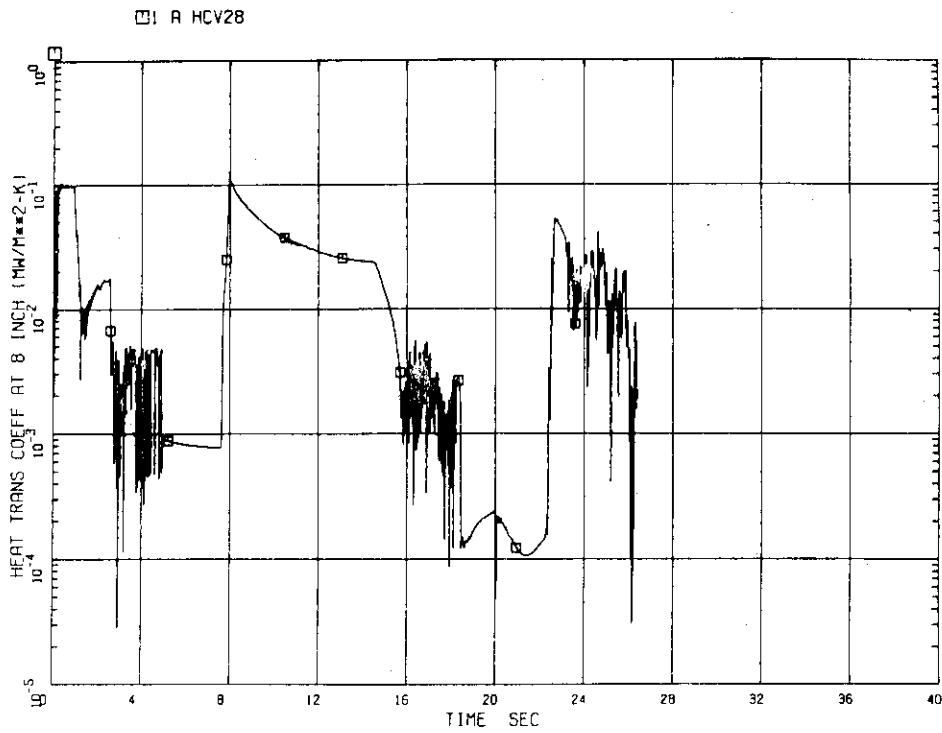


Fig.35 Heat Transfer Coefficient History (Elevation of 8" above Bottom of Core)

COMPARISON OF SEMISCALE S-06-3 DATA AND ALARM-P1 ANALYSIS

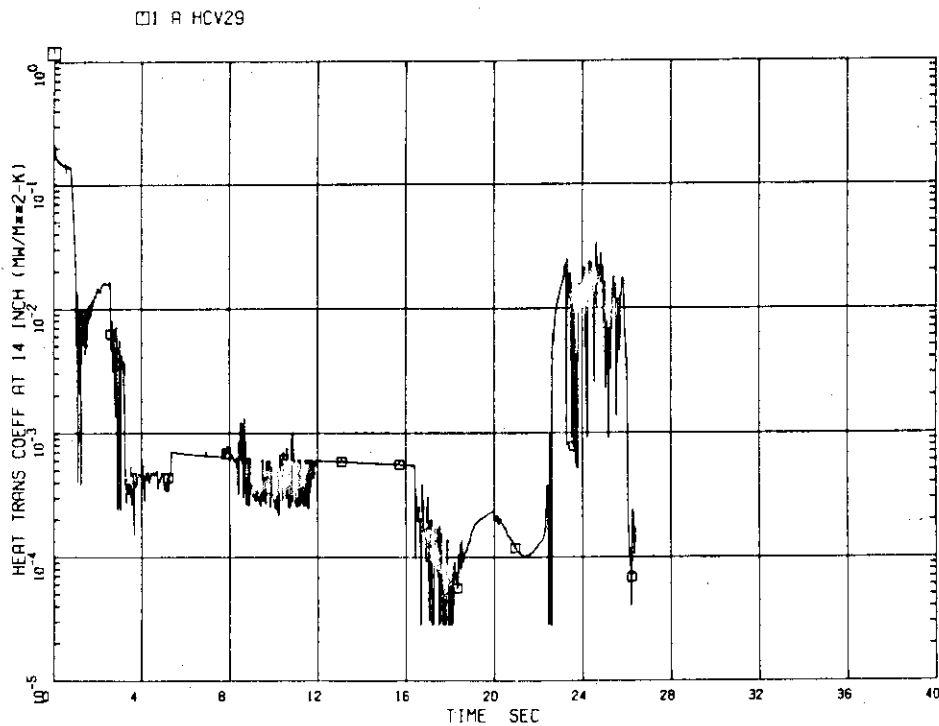


Fig.36 Heat Transfer Coefficient History (Elevation of 14" above Bottom of Core)

COMPARISON OF SEMISCALE S-06-3 DATA AND ALARM-P1 ANALYSIS

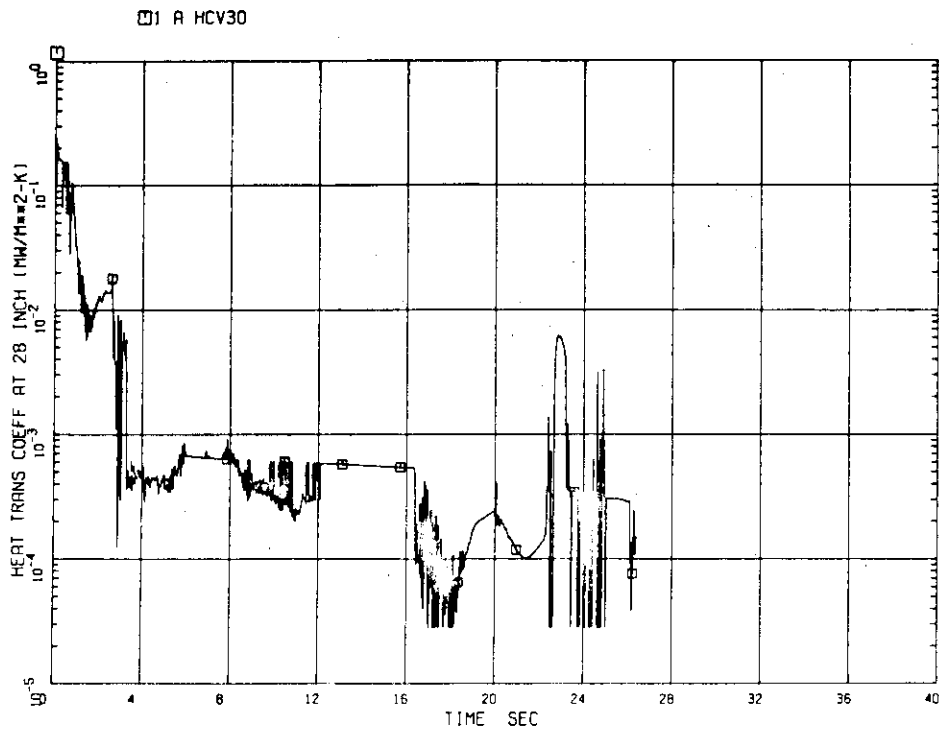


Fig.37 Heat Transfer Coefficient History (Elevation of 28" above Bottom of Core)

COMPARISON OF SEMISCALE S-06-3 DATA AND ALARM-P1 ANALYSIS

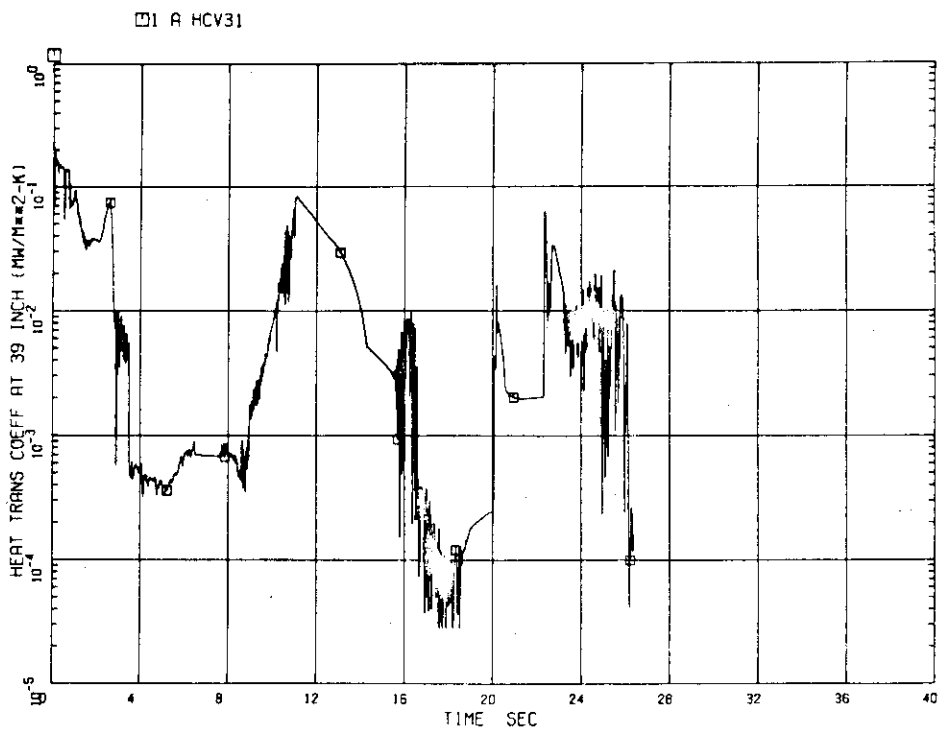


Fig.38 Heat Transfer Coefficient History (Elevation of 39" above Bottom of Core)

COMPARISON OF SEMISCALE S-06-3 DATA AND ALARM-P1 ANALYSIS

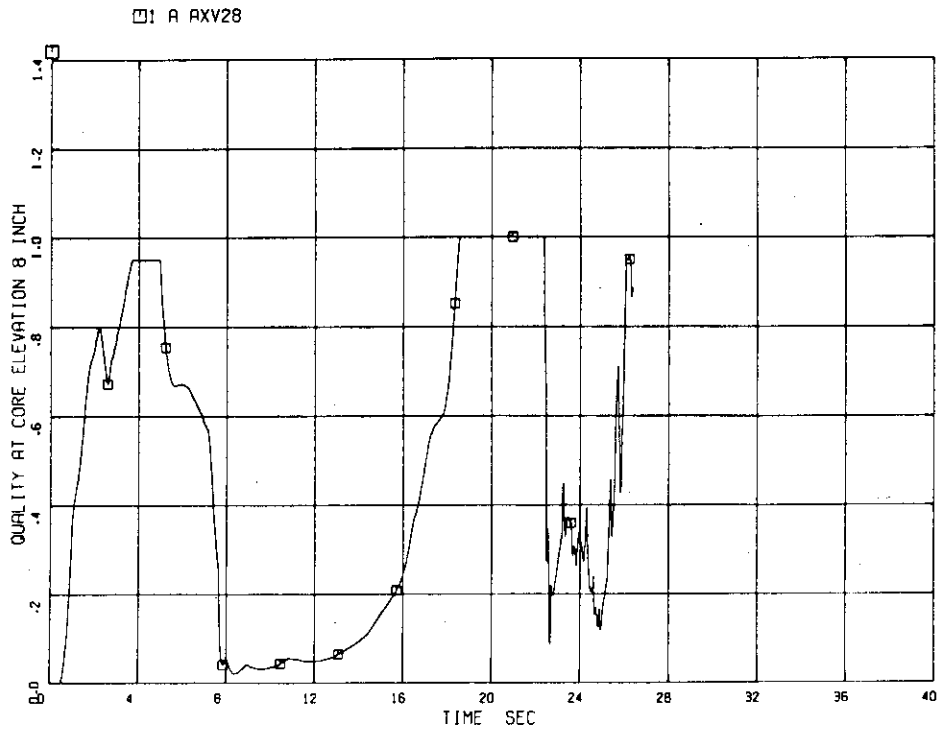


Fig.39 Fluid Quality History (Elevation of 8" above Bottom of Core)

COMPARISON OF SEMISCALE S-06-3 DATA AND ALARM-P1 ANALYSIS

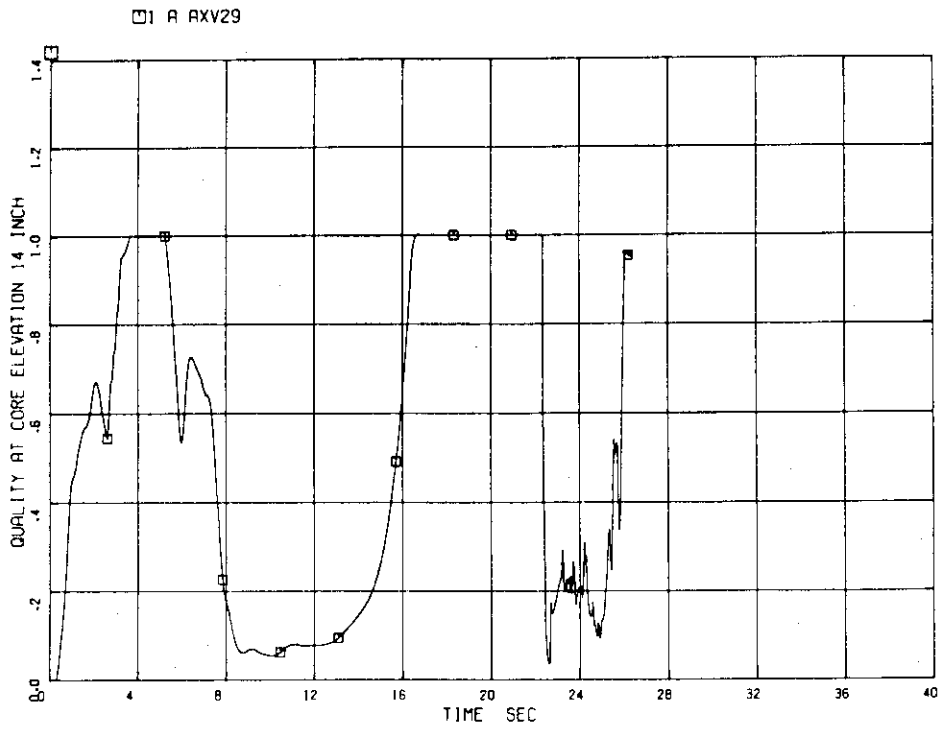


Fig.40 Fluid Quality History (Elevation of 14" above Bottom of Core)

COMPARISON OF SEMISCALE S-06-3 DATA AND ALARM-P1 ANALYSIS

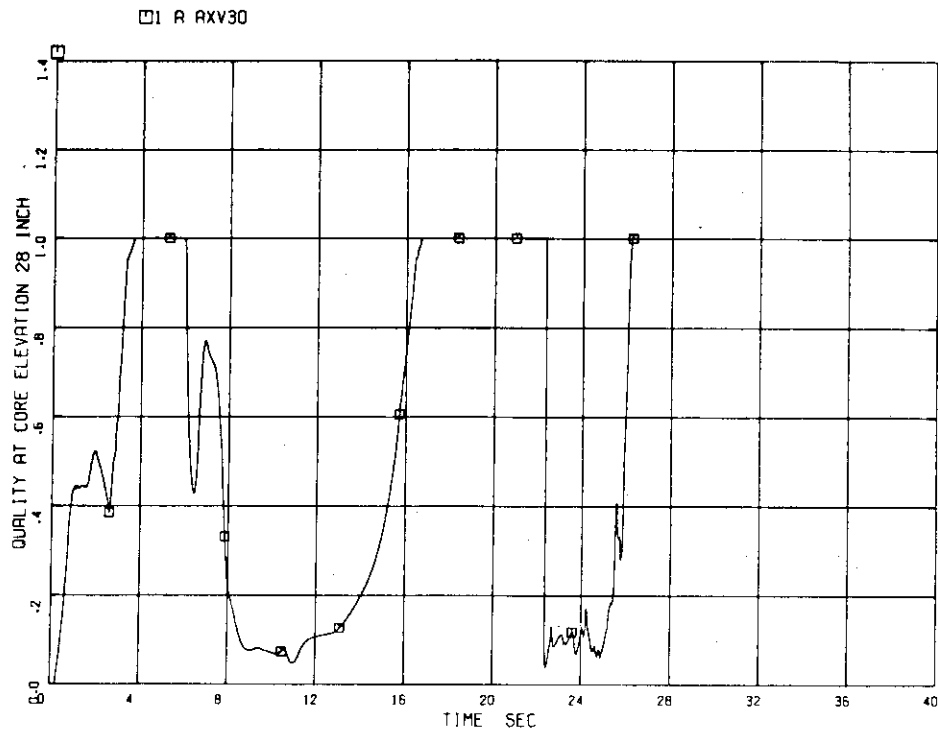


Fig.41 Fluid Quality History (Elevation of 28" above bottom of Core)

COMPARISON OF SEMISCALE S-06-3 DATA AND ALARM-P1 ANALYSIS

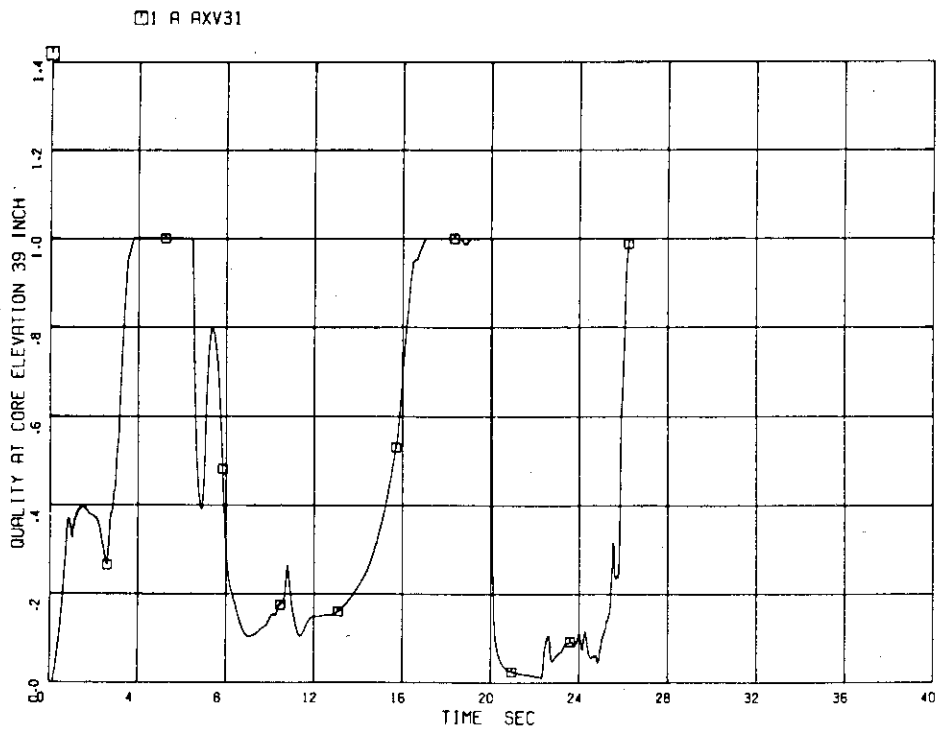


Fig.42 Fluid Quality History (Elevation of 39" above Bottom of Core)

COMPARISON OF SEMISCALE S-06-3 DATA AND ALARM-P1 ANALYSIS

□: A TDJS

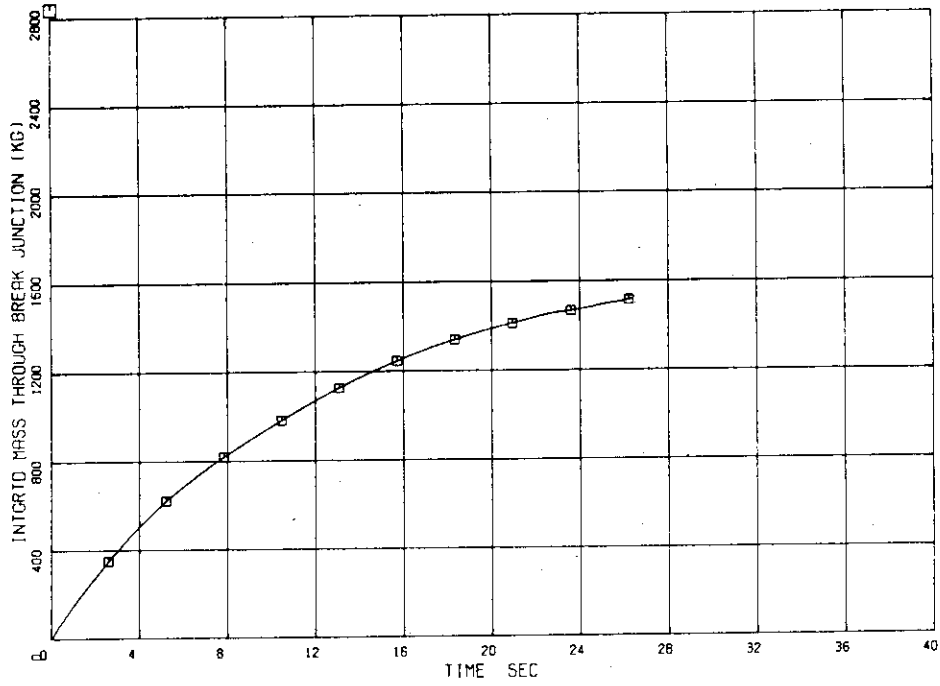


Fig.43 System Mass Inventory History (FDB-23, FDB-42)

COMPARISON OF SEMISCALE S-06-3 DATA AND ALARM-P1 ANALYSIS

□: TE000031 ○: A ATV36

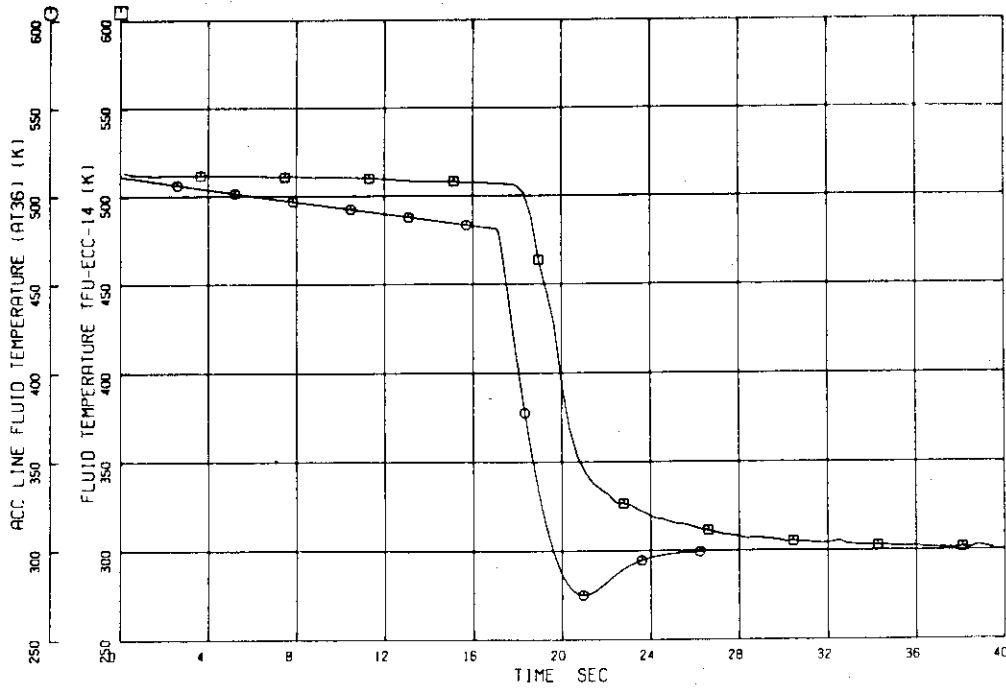


Fig.44 Fluid Temperature History in Accumulator Line (TFU-ECC-14)



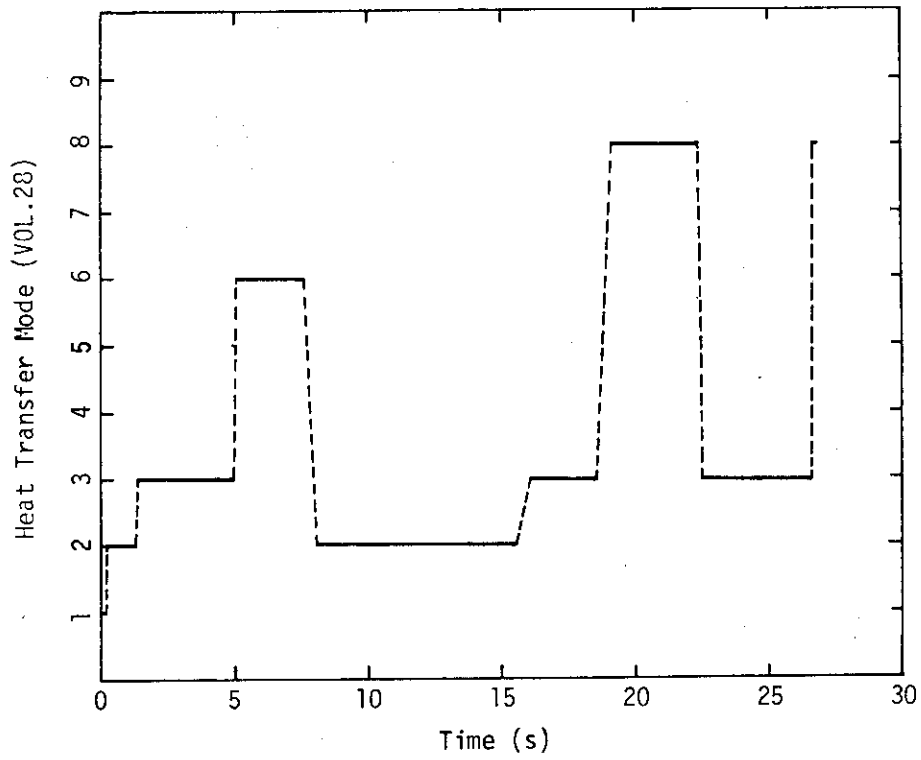


Fig.45 Heat Transfer Mode (Elevation of 8" above Bottom of Core)

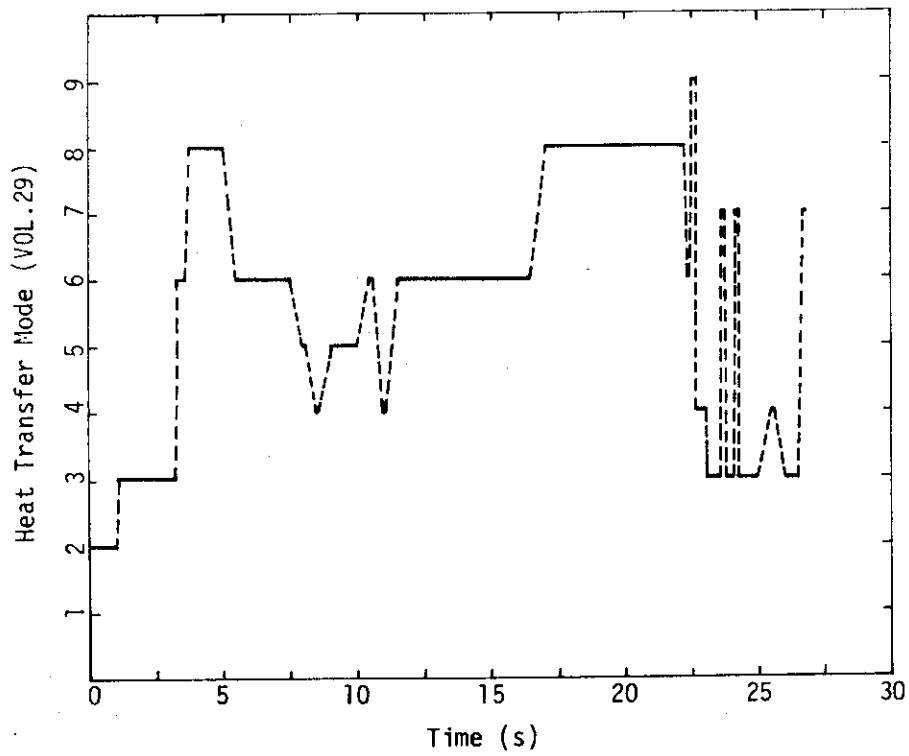


Fig.46 Heat Transfer Mode (Elevation of 14" above Bottom of Core)

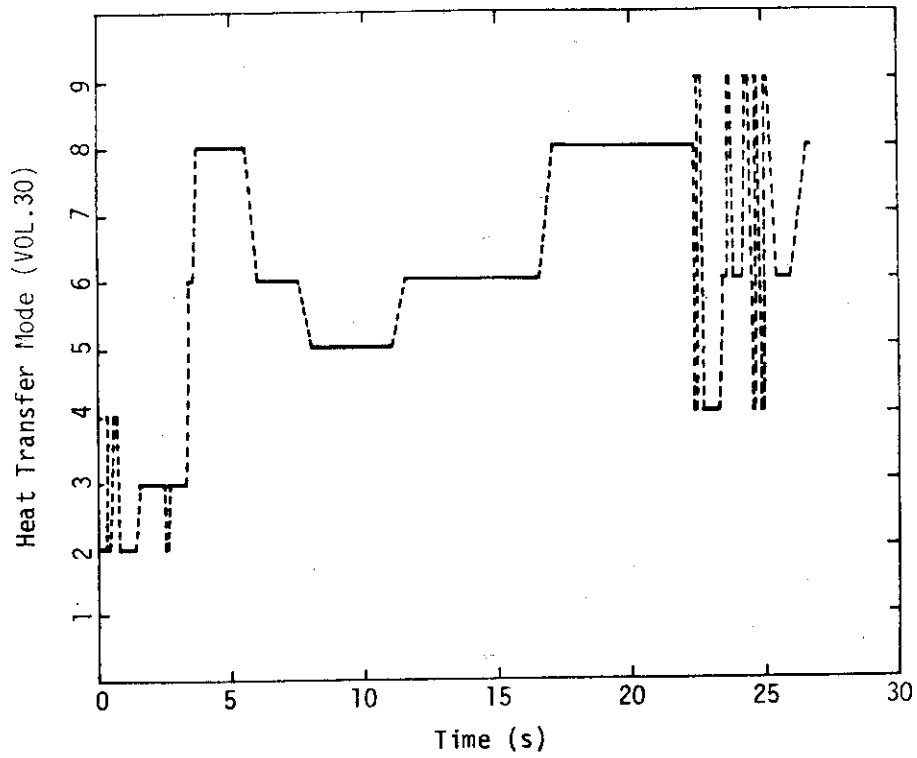


Fig.47 Heat Transfer Mode (Elevation of 28" above Bottom of Core)

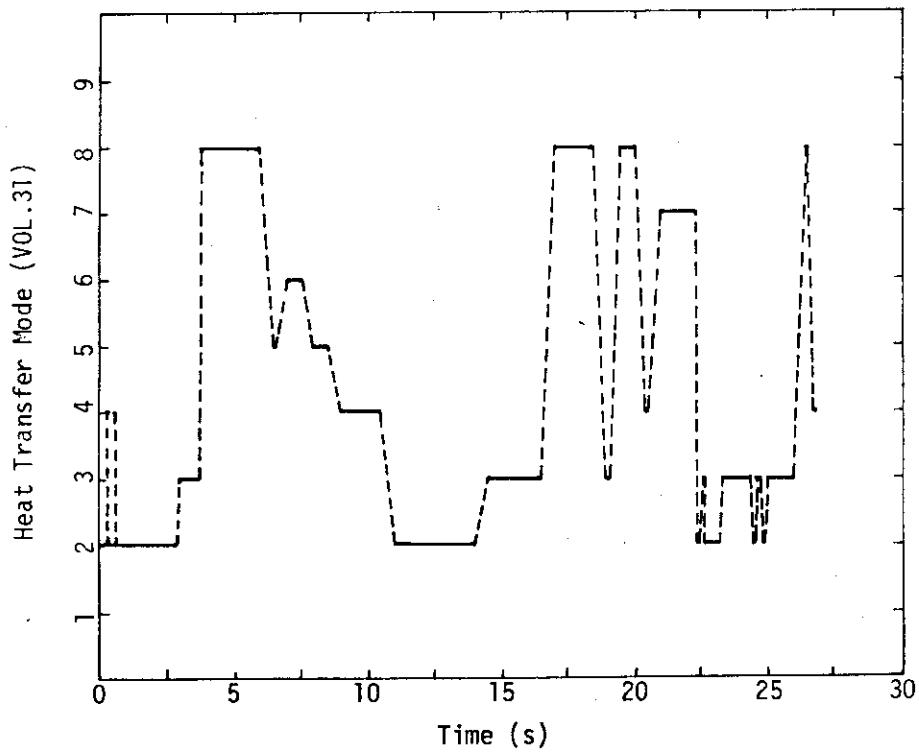


Fig.48 Heat Transfer Mode (Elevation of 39" above Bottom of Core)

Appendix 1

List of Input-data

```

/*
/*      AN ANALYSIS OF SEMISCALE S-06-3 TEST BY ALARM-P1 CODE
/*
/*      ALARM-P1 PREDICTION OF CSNI STANDARD PROBLEM NO.8
/*
/*      PROBLEM DIMENSION
/*
/*      -3   18   12   10   36   3   40   1   1   3   1   3
/*      7   5   2   4   0   1.0058
/*
/*      EDIT VARIABLE
/*
/*      JW  J29 JW  J30 AP  N10 AP  N17 AP  N35 AP  N21 AP  N26 ST  N28 ST  N29
/*      ST  N30 ST  N31 JW  J7  AT  N11 AT  N18 AT  N26 WM  N27 TM  N27 HC  N28
/*
/*      TIME STEP SIZE
/*
/*      100    20    1    2000    0.000005    0.01
/*      100    10    1    1000    0.00001    0.05
/*      100    4    1    400    0.000025    0.1
/*      100    4    1    400    0.000025    0.3
/*      100    20   1    200    0.00005    0.5
/*      100    10   1    100    0.0001    5.0
/*      100    20   1    40    0.00025    10.0
/*      100    10   1    20    0.0005    17.0
/*      200    10   1    40    0.00025    22.0
/*      100    10   1    100    0.0001    24.5
/*      100    50   1    200    0.0001    25.0
/*      100    10   1    100    0.0002    50.0
/*
/*      TRIP CONTROL
/*
/*      1      1    0    0    40.0    0.0    / END OF PROBLEM
/*      21     1    0    0    0.0    0.0    / STEAM OUTLET J22
/*      3      1    0    0    0.0    0.0    / POWER
/*      4      1    0    0    100.0   0.0    / PUMP TRIP
/*      51     1    0    0    0.0    0.0    / FEED WATER J23
/*      52    -4   36   0    126.5823E4  0.0    / HPIS J37
/*      53    -4   36   0    17.5809E4  0.0    / LPIS J38
/*      6      1    0    0    0.00001   0.0    / BREAK
/*      7      1    0    0    0.00001   0.0    / BREAK
/*      8     -4   36   0    43.1941E4  0.0    / ACC VALVE J40
/*
/*      VOLUME DATA
/*
/*      ***** VCL,1 INTACT LOOP HOT LEG *****
/*      0 0 160.7718E4 326.444 -1.0 0.01082 0.3086735
/*      0.3086735 0.00349 0.0667 0.1825625 3.17
/*
/*      ***** VCL,2 SG INLET PLENUM *****
/*      0 0 160.6312E4 326.444 -1.0 0.00963 0.48514
/*      0.48514 0.01984 0.1590 0.491236 0.0

```

```

/*
/* ***** VOL.3 SG U-TUBE *****
   0  0  160.4933E4  -343.52  -1.0  0.01140  2.629916
   2.629916  0.00442  0.0102  0.976376  0.0
/*
/* ***** VOL.4 SG U-TUBE *****
   0  0  160.4606E4  -320.14  -1.0  0.01140  2.629916
   2.629916  0.00442  0.0102  0.976376  0.0
/*
/* ***** VOL.5 SG OUTLET PLENUM *****
   0  0  160.5583E4  290.889  -1.0  0.00963  0.48514
   0.48514  0.01984  0.1590  0.491236  0.0
/*
/* ***** VOL.6 PUMP SUCTION LEG *****
   0  0  160.3786E4  290.889  -1.0  0.01018  1.543812
   1.543812  0.00349  0.0667  -1.052576  0.0
/*
/* ***** VOL.7 ACTIVE PUMP *****
   0  1  160.6698E4  290.889  -1.0  0.00408  0.2809875
   0.2809875  0.00349  0.0667  -0.24765  0.0
   169.53
/*
/* ***** VOL.8 INTACT LOOP COLD LEG NEAR PUMP *****
   0  0  161.0171E4  290.889  -1.0  0.00425  0.066675
   0.066675  0.00349  0.0667  -0.0333375  1.25
/*
/* ***** VOL.9 INTACT LOOP COLD LEG *****
   0  0  161.0078E4  290.889  -1.0  0.00425  0.066675
   0.066675  0.00349  0.0667  -0.0333375  1.25
/*
/* ***** VOL.10 PRESSURIZER *****
   3  0  160.6254E4  -1.0  0.0  0.02741  1.143
   0.62547  0.02466  0.0  1.86055  0.0
/*
/* ***** VOL.11 PRESSURIZER SURGE LINE *****
   0  0  160.7034E4  242.850  -1.0  0.00037  1.6113125
   1.6113125  4.3E-5  0.0  0.2492375  4.0
/*
/* ***** VOL.12 BROKEN LOOP HOT LEG *****
   0  0  160.8332E4  322.960  -1.0  0.00315  0.2190115
   0.2190115  0.00349  0.0667  0.1825625  1.00646
/*
/* ***** VOL.13 SG SIMULATOR *****
   0  0  160.7478E4  -349.762  -1.0  0.00852  2.6099135
   2.6099135  0.00374  0.0690  0.401574  2.57658
/*
/* ***** VOL.14 SG SIMULATOR *****
   0  0  160.7478E4  -346.519  -1.0  0.00852  2.6099135
   2.6099135  0.00374  0.0690  0.401574  2.57658
/*
/* ***** VOL.15 PUMP SUCTION LEG *****
   0  0  160.7948E4  317.800  -1.0  0.00252  1.417574
   1.417574  0.00158  0.0449  -1.016  1.40081
/*
ISP80520
ISP80530
ISP80540
ISP80550
ISP80560
ISP80570
ISP80580
ISP80590
ISP80600
ISP80610
ISP80620
ISP80630
ISP80640
ISP80650
ISP80660
ISP80670
ISP80680
ISP80690
ISP80700
ISP80710
ISP80720
ISP80730
ISP80740
ISP80750
ISP80760
ISP80770
ISP80780
ISP80790
ISP80800
ISP80810
ISP80820
ISP80830
ISP80840
ISP80850
ISP80860
ISP80870
ISP80880
ISP80890
ISP80900
ISP80910
ISP80920
ISP80930
ISP80940
ISP80950
ISP80960
ISP80970
ISP80980
ISP80990
ISP81000
ISP81010
ISP81020
ISP81030
ISP81040
ISP81050

```

```

/* ***** VOL.16 PUMP SIMULATOR *****
   0 0 160.8552E4 317.000 -1.0 0.00147 0.2301875
   0.2301875 0.00198 0.0502 -1.2461875 0.768382
/*
/* ***** VOL.17 HOT LEG BREAK NODE *****
   0 0 160.8077E4 316.970 -1.0 0.00227 1.4954250
   1.4954250 0.00145 0.0429 -1.2461875 1.50799
/*
/* ***** VOL.18 BROKEN LOOP COLD LEG *****
   0 0 161.0465E4 290.720 -1.0 0.00461 0.066675
   0.066675 0.00349 0.0667 -0.0333375 1.44331
/*
/* ***** VOL.19 HOT LEG SIDE REFLOOD BYPASS LINE *****
   0 0 160.8141E4 315.850 -1.0 0.00538 0.552323
   0.552323 0.00349 0.0667 0.1825625 0.0
/*
/* ***** VOL.20 COLD LEG SIDE REFLOOD BYPASS LINE *****
   0 0 161.0177E4 288.850 -1.0 0.00640 0.768223
   0.768223 0.00349 0.0667 -0.0333375 0.0
/*
/* ***** VOL.21 SG SECONDARY SYSTEM *****
   1 0 0.0 284.650 0.0287 0.19820 4.6580
   2.90 0.04255 0.0 0.976376 0.0
/*
/* ***** VOL.22 PRESSURE VESSEL INLET PLENUM *****
   0 0 161.0066E4 290.889 -1.0 0.00504 0.45847
   0.45847 0.00548 0.0412 -0.2667 0.0
/*
/* ***** VOL.23 DOWNCOMER ANNULUS *****
   0 0 161.1592E4 290.889 -1.0 0.02183 3.880612
   3.880612 0.00534 0.0214 -4.147312 3.9
/*
/* ***** VOL.24 LOWER PLENUM *****
   0 0 161.3225E4 290.889 -1.0 0.02161 0.731774
   0.731774 0.00623 0.0 -4.879086 1.0
/*
/* ***** VOL.25 MIXER HOUSING *****
   0 0 161.2122E4 290.889 -1.0 0.00371 0.520446
   0.520446 0.00713 0.0 -4.147312 0.0
/*
/* ***** VOL.26 UPPER PLENUM *****
   1 0 160.8298E4 326.444 -1.0 0.02620 2.972816
   2.972816 0.00713 0.0 -1.950466 2.5
/*
/* ***** VOL.27 PRESSURE SUPPRESSION SYSTEM *****
   1 0 2.4820E4 16.350 0.0 3.17549 4.5225462
   1.21 0.70205 0.9454 -2.5654 0.0
/*
/* ***** VOL.28 CORE REGION #1 *****
   0 0 161.1054E4 -311.09 -1.0 0.00137 0.2794
   0.2794 0.00492 0.0113 -3.626866 0.0
/*
/* ***** VOL.29 CORE REGION #2 *****
   0 0 161.0817E4 -319.99 -1.0 0.00137 0.2794

```

```

ISP81060
ISP81070
ISP81080
ISP81090
ISP81100
ISP81110
ISP81120
ISP81130
ISP81140
ISP81150
ISP81160
ISP81170
ISP81180
ISP81190
ISP81200
ISP81210
ISP81220
ISP81230
ISP81240
ISP81250
ISP81260
ISP81270
ISP81280
ISP81290
ISP81300
ISP81310
ISP81320
ISP81330
ISP81340
ISP81350
ISP81360
ISP81370
ISP81380
ISP81390
ISP81400
ISP81410
ISP81420
ISP81430
ISP81440
ISP81450
ISP81460
ISP81470
ISP81480
ISP81490
ISP81500
ISP81510
ISP81520
ISP81530
ISP81540
ISP81550
ISP81560
ISP81570
ISP81580
ISP81590

```

```

0.2794      0.00492    0.0113    -3.347466    0.0      ISP81600
/*
/* ***** VOL.30 CORE REGION #3 ***** ISP81610
0 0      161.0582E4    -331.90    -1.0    0.00137    0.2794    ISP81620
0.2794      0.00492    0.0113    -3.068066    0.0      ISP81630
/*
/* ***** VOL.31 CORE REGION #4 ***** ISP81640
0 0      161.0352E4    -343.28    -1.0    0.00137    0.2794    ISP81650
0.2794      0.00492    0.0113    -2.788666    0.0      ISP81660
/*
/* ***** VOL.32 CORE REGION #5 ***** ISP81670
0 0      161.0018E4    -352.64    -1.0    0.00274    0.2794    ISP81680
0.5588      0.00492    0.0113    -2.509266    0.0      ISP81690
/*
/* ***** VOL.33 ACCUMULATOR TANK ***** ISP81700
3 0      45.0070E4      27.778    0.0    0.1145    0.5588    ISP81710
1.3007      0.03812    0.2203    0.9877425    0.0      ISP81720
/*
/* ***** VOL.34 ACCUMULATOR LINE ***** ISP81730
0 0      45.0070E4      27.778    -1.0    0.00244    3.0036    ISP81740
0.02430    0.00046    0.0243    1.0301175    0.0      ISP81750
/*
/* ***** VOL.35 COLD LEG BREAK NODE ***** ISP81760
0 0      161.0465E4      288.800    -1.0    0.00161    0.0243    ISP81770
0.066675    0.00349    0.0667    -0.0333375    5.31      ISP81780
/*
/* ***** VOL.36 ACCUMULATOR LINE ***** ISP81810
0 0      160.9655E4      238.850    -1.0    0.00244    0.066675    ISP81820
1.02108    0.00046    0.0243    0.0333375    0.601748    ISP81830
/*
/* BUBBLE RISE PARAMETER ISP81840
/* ISP81850
0.0      0.9144    ISP81860
0.0      3.048    ISP81870
0.8      0.9144    ISP81880
/*
/* PUMP DESCRIPTION DATA AND CURVE DATA ISP81890
/* ISP81900
6 5 9 10 13 12 13 11 2 ISP81910
0.0      1.0E-5      997.856    58.522    0*0114    372.8    ISP81920
4.8111    1.6139    0.0      ISP81930
/*
/* HEAD ISP81940
/* ISP81950
-1.0      1.5      -0.8      1.275    -0.6      1.375    -0.4      1.375    ISP81960
0.0      1.2      1.0      1.0      ISP81970
/*
-1.0      0.175    -0.5      0.65      0.0      0.975    0.5      1.35    ISP81980
1.0      1.95    ISP81990
/*
-1.0      0.175    -0.75    -0.15    -0.55    -0.3      -0.275    -0.4    ISP82000
0.0      -0.35    0.30    -0.20    0.50    0.0      0.80      0.545    ISP82010
1.0      1.0    ISP82100
/*
ISP82110
ISP82120
ISP82130

```

	-1.0	1.50	-0.80	1.15	-0.60	0.95	-0.40	0.83	ISP82140		
	-0.2	0.775	0.0	0.725	0.20	0.725	0.40	0.80	ISP82150		
	0.6	1.025	1.0	1.95					ISP82160		
/*									ISP82170		
/*	TORQUE								ISP82180		
/*									ISP82190		
	-1.0	0.62	-0.80	0.68	-0.60	0.53	-0.40	0.46	ISP82200		
	-0.20	0.49	0.0	0.54	0.20	0.59	0.40	0.65	ISP82210		
	0.60	0.77	0.80	0.95	0.90	0.98	0.95	0.96	ISP82220		
	1.0	0.87							ISP82230		
/*									ISP82240		
	-1.0	-1.44	-0.80	-1.25	-0.60	-1.08	-0.40	-0.92	ISP82250		
	-0.20	-0.77	0.0	-0.63	0.20	-0.51	0.40	-0.39	ISP82260		
	0.60	-0.29	0.80	-0.20	0.90	-0.16	1.0	-0.13	ISP82270		
/*									ISP82280		
	-1.0	-1.44	-0.80	-1.12	-0.60	-0.79	-0.40	-0.52	ISP82290		
	-0.20	-0.31	0.0	-0.15	0.20	0.02	0.40	0.22	ISP82300		
	0.60	0.46	0.80	0.71	0.90	0.81	0.95	0.85	ISP82310		
	1.0	0.87							ISP82320		
/*									ISP82330		
	-1.0	0.62	-0.80	0.53	-0.60	0.46	-0.40	0.42	ISP82340		
	-0.2	0.39	0.0	0.36	0.20	0.32	0.40	0.27	ISP82350		
	0.6	0.18	0.80	0.05	1.0	-0.13			ISP82360		
/*									ISP82370		
	0.0	0.0	1.0E8	0.0					ISP82380		
/*									ISP82390		
/*	JUNCTION DATA								ISP82400		
/*									ISP82410		
/*	*****	JUN.1	UPPER PLENUM TO HOT LEG	*****					ISP82420		
	26	1	0	0	2	1	4.899	0.00183	0.2159	0.0	ISP82430
		1.0E-6	1.0E-6	0	0.85	1.0					ISP82440
/*	*****	JUN.2	SG INLET	*****							ISP82450
	1	2	0	0	0	1	4.899	0.00349	0.491236	0.0	ISP82460
		0.0	0.0	0	0.85	1.0					ISP82470
/*	*****	JUN.3	INLET PLENUM TO U-TUBE	*****							ISP82480
	2	3	0	0	0	1	4.899	0.00442	0.976376	0.0	ISP82490
		0.0	0.0	0	0.85	1.0					ISP82500
/*	*****	JUN.4	TOP OF U-TUBE	*****							ISP82510
	3	4	0	0	0	1	4.899	0.00442	3.531108	0.0	ISP82520
		0.0	0.0	0	0.85	1.0					ISP82530
/*	*****	JUN.5	U-TUBE TO OUTLET PLENUM	*****							ISP82540
	4	5	0	0	0	1	4.899	0.00442	0.976376	0.0	ISP82550
		0.0	0.0	0	0.85	1.0					ISP82560
/*	*****	JUN.6	SG OUTLET	*****							ISP82570
	5	6	0	0	0	1	4.899	0.00349	0.491236	0.0	ISP82580
		0.0	0.0	0	0.85	1.0					ISP82590
/*	*****	JUN.7	PUMP INLET	*****							ISP82600
	6	7	-1	0	0	1	4.899	0.00349	-0.24765	0.0	ISP82610
		5.30	4.86	0	0.85	1.0					ISP82620
/*	*****	JUN.8	PUMP OUTLET	*****							ISP82630
	7	8	1	0	0	1	4.899	0.00349	0.0	0.0	ISP82640
		1.65	1.65	0	0.85	-1.0					ISP82650
/*	*****	JUN.9	WITHIN COLD LEG	*****							ISP82660
	8	9	0	0	0	1	4.899	0.00349	0.0	0.0	ISP82670

		0.0	0.0	0	0.85	-1.0						ISP82680
/*	*****	JUN.10	VESSEL INLET	*****								ISP82690
		9	22	0	0	2	1	4.899	0.00183	0.0	0.0	ISP82700
				1.0E-6	1.0E-6	0	0.85	-1.0				ISP82710
/*	*****	JUN.11	PRESSURIZER OUTLET	*****								ISP82720
		10	11	0	0	0	1	0.0	4.3E-5	1.86055	0.0	ISP82730
				10.8	10.8	0	0.85	0.6				ISP82740
/*	*****	JUN.12	SURGE LINE OUTLET	*****								ISP82750
		11	1	0	0	2	1	0.0	4.3E-5	0.2492375	0.0	ISP82760
				0.0	0.0	0	0.85	0.6				ISP82770
/*	*****	JUN.13	VESSEL TO HOT LEG	*****								ISP82780
		26	12	0	0	2	1	0.0	0.00183	0.2159	747.499	ISP82790
				0.677051	1.2144	0	0.85	1.0				ISP82800
/*	*****	JUN.14	SG SIMULATOR INLET	*****								ISP82810
		12	13	0	0	0	1	0.0	0.00024	0.401574	1012.61	ISP82820
				1.41181	1.41146	0	0.85	1.0				ISP82830
/*	*****	JUN.15	TOP OF SG SIMULATOR	*****								ISP82840
		13	14	0	0	0	1	0.0	0.00349	2.9448125	1030.44	ISP82850
				285.435	285.435	0	0.85	1.0				ISP82860
/*	*****	JUN.16	SG SIMULATOR OUTLET	*****								ISP82870
		14	15	0	0	0	1	0.0	0.00024	0.401574	1387.54	ISP82880
				1.40405	1.41583	0	0.85	1.0				ISP82890
/*	*****	JUN.17	PUMP SIMULATOR INLET	*****								ISP82900
		15	16	0	0	0	1	0.0	0.00024	-1.016	827.54	ISP82910
				0.844137	1.54353	0	0.85	1.0				ISP82920
/*	*****	JUN.18	PUMP SIMULATOR OUTLET	*****								ISP82930
		16	17	0	0	0	1	0.0	0.00024	-1.21285	2018.77	ISP82940
				12.8823	12.438	0	0.85	1.0				ISP82950
/*	*****	JUN.19	VESSEL EXIT	*****								ISP82960
		22	18	0	0	2	1	0.0	0.00183	0.0	574.74	ISP82970
				0.677051	1.21442	0	0.85	-1.0				ISP82980
/*	*****	JUN.20	REFLOOD BYPASS EXIT (HOT LEG)	*****								ISP82990
		19	12	0	0	0	1	0.0	0.00349	0.2492375	0.0	ISP83000
				0.0	0.0	0	0.85	1.0				ISP83010
/*	*****	JUN.21	REFLOOD BYPASS EXIT (COLD LEG)	*****								ISP83020
		20	18	0	0	0	1	0.0	0.00349	0.0333375	0.0	ISP83030
				0.0	0.0	0	0.85	1.0				ISP83040
/*	*****	JUN.22	STEAM OUTLET	*****								ISP83050
		21	0	1	0	2	1	0.5296	0.00203	5.345176	0.0	ISP83060
				0.0	0.0	0	0.85	0.6				ISP83070
/*	*****	JUN.23	FEED WATER INLET	*****								ISP83080
		0	21	1	0	2	1	0.5296	0.00113	3.9307262	0.0	ISP83090
				0.0	0.0	0	0.85	0.6				ISP83100
/*	*****	JUN.24	DOWNCOMER ANNULUS INLET	*****								ISP83110
		22	23	0	0	2	1	4.899	0.00534	-0.2667	0.0	ISP83120
				0.0	0.0	0	0.85	-1.0				ISP83130
/*	*****	JUN.25	DOWNCOMER TO LOWER PLENUM	*****								ISP83140
		23	24	0	0	2	1	4.899	0.00534	-4.147312	0.0	ISP83150
				0.0	0.0	0	0.85	-1.0				ISP83160
/*	*****	JUN.26	LOWER PLENUM TO MIXER BOX	*****								ISP83170
		24	25	0	0	2	1	4.899	0.00713	-4.147312	0.0	ISP83180
				0.0	0.0	0	0.85	-1.0				ISP83190
/*	*****	JUN.27	CORE INLET	*****								ISP83200
		25	28	0	0	2	1	4.899	0.00492	-3.626866	0.0	ISP83210



```

0.0 0.0 0 0.85 -1.0
/* ***** JUN.28 CORE OUTLET ***** ISP83220
32 26 0 0 2 1 4.899 0.00492 -1.950466 0.0 ISP83230
0.0 0.0 0 0.85 -1.0 ISP83240
/* ***** JUN.29 BREAK PLANE ***** ISP83250
17 27 0 1 0 1 0.0 0.00024 0.2159 978.25 ISP83260
1.00777 1.13360 0 0.85 0.6 ISP83270
/* ***** JUN.30 BREAK PLANE ***** ISP83280
35 27 0 2 0 1 0.0 0.00024 0.0 318.823 ISP83290
1.38245 1.15464 0 0.85 0.6 ISP83300
/* ***** JUN.31 WITHIN CORE REGION ***** ISP83310
28 29 0 0 0 1 4.899 0.00492 -3.347466 0.0 ISP83320
0.0 0.0 0 0.85 -1.0 ISP83330
/* ***** JUN.32 WITHIN CORE REGION ***** ISP83340
29 30 0 0 0 1 4.899 0.00492 -3.068066 0.0 ISP83350
0.0 0.0 0 0.85 -1.0 ISP83360
/* ***** JUN.33 WITHIN CORE REGION ***** ISP83370
30 31 0 0 0 1 4.899 0.00492 -2.788666 0.0 ISP83380
0.0 0.0 0 0.85 -1.0 ISP83390
/* ***** JUN.34 WITHIN CORE REGION ***** ISP83400
31 32 0 0 0 1 4.899 0.00492 -2.509266 0.0 ISP83410
0.0 0.0 0 0.85 -1.0 ISP83420
/* ***** JUN.35 ACC EXIT ***** ISP83430
33 34 0 0 0 1 0.0 0.00046 1.0301175 0.0 ISP83440
0.0 0.0 0 0.85 -1.0 ISP83450
/* ***** JUN.36 ECC INJECTION POINT ***** ISP83460
36 9 0 0 2 1 0.0 0.00046 0.0333375 0.0 ISP83470
284.38 1.E6 0 0.85 -1.0 ISP83480
/* ***** JUN.37 HPIS ***** ISP83490
0 36 2 0 2 1 0.0 0.00015 0.1111111 0.0 ISP83500
0.0 0.0 0 0.85 1.0 ISP83510
/* ***** JUN.38 LPIS ***** ISP83520
0 36 3 0 2 1 0.0 0.00028 0.1111111 0.0 ISP83530
0.0 0.0 0 0.85 1.0 ISP83540
/* ***** JUN.39 COLD LEG BREAK NODE ENTRANCE ***** ISP83550
18 35 0 0 0 1 0.0 0.00349 0.0 292.636 ISP83560
1.0E-10 1.0E-10 0 0.85 1.0 ISP83570
/* ***** JUN.40 WITHIN ACC LINE ***** ISP83580
34 36 0 3 0 1 0.0 0.00046 1.0301175 0.0 ISP83590
0.0 0.0 0 0.85 -1.0 ISP83600
/* ISP83610
/* CHECK VALVE DATA ISP83620
/* -6 0.0 0.0 0.0 0.0 / BREAK VALVE (J29) ISP83630
/* -7 0.0 0.0 0.0 0.0 / BREAK VALVE (J30) ISP83640
/* -8 0.0 0.0 0.0 0.0 / ACC LINE (J40) ISP83650
/* ISP83660
/* LEAK DATA ISP83670
/* AT JUNCTION 22 OF SG SECONDARY SIDE ISP83680
/* 1 12 1.0338E4 0.85 1.0 ISP83690
/* 2 6 1.0338E4 0.6 0.85 ISP83700
0.0 0.5296 8.0 0.5296 12.0 0.2354 24.0 0.0471 24.001 0.0 50.0 0.0 ISP83710
ISP83720
ISP83730
ISP83740
ISP83750

```

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/*
/*      FILL DATA
/*      AT JUNCTION 23 OF SG SECONDARY SIDE      FEED WATER
/*
/*      6      0      61.1814E4      204.8
0.0 0.5296 8.0 0.5296 12.0 0.2354 24.0 0.0471 24.001 0.0 50.0 0.0
/*      HPIS      (JUNCTION 37)
/*
/*      4      0      7.0338E4      27.778
0.0 0.0149 30.0 0.0149 30.001 0.0817 50.0 0.0817
/*
/*      LPIS      (JUNCTION 38)
/*
/*      2      0      7.0338E4      27.778
0.0 0.299 50.0 0.299
/*
/*      KINETICS CONSTANT DATA
/*
/*      1      0      0.0      0.0
30
0.0 1.0 1.23 1.0 1.64 0.795 2.05 0.597
2.18 0.579 2.51 0.579 2.59 0.597 2.86 0.795
3.27 1.0 5.05 1.0 5.45 0.795 6.00 0.597
6.68 0.398 7.36 0.216 7.64 0.199 11.05 0.199
11.45 0.138 12.00 0.121 15.27 0.121 15.82 0.086
16.91 0.086 17.45 0.147 18.00 0.156 19.36 0.156
20.18 0.061 20.72 0.052 26.45 0.022 36.00 0.022
39.55 0.038 42.00 0.038
/*
/*      HEAT SLAB DATA
/*
/*      3      21      1      3.09632      3.85116      6.2100E-3      0.0      0.0      / U-TUBE1
4      21      1      3.09632      3.85116      6.2100E-3      0.0      0.0      / U-TUBE2
0      28      2      0.0      0.3763      1.0085E-3      0.0      0.0      / CORE #1
0      29      2      0.0      0.3763      1.0085E-3      0.0      0.0      / CORE #2
0      30      2      0.0      0.3763      1.0085E-3      0.0      0.0      / CORE #3
0      31      2      0.0      0.3763      1.0085E-3      0.0      0.0      / CORE #4
0      32      2      0.0      0.7526      2.0170E-3      0.0      0.0      / CORE #5
/*
/*      CORE SECTION DATA
/*
/*      3      0.2794      0.0113      0.1323
4      0.2794      0.0113      0.2307
5      0.2794      0.0113      0.2553
6      0.2794      0.0113      0.2086
7      0.5588      0.0113      0.1731
/*
/*      SLAB GEOMETRY DATA
/*
/*      ***** GEOMETRY INDEX 1 *****
2      1      0      1      2      12.446E-4      1.0      5.1054E-3 / INCONEL600
/*      ***** GEOMETRY INDEX 2 *****
2      4      0      2      2      8.690E-4      0.0      0.0 / B.N.
0      0      3      2      21.830E-4      1.0 / CONSTANTAN

```

	0	2	2	12,960E-4	0.0		/ B.N.	ISP84300
	0	4	2	9,910E-4	0.0		/ ST	ISP84310
/*								ISP84320
/*	MATERIAL THERMAL PROPERTY DATA							ISP84330
/*	THERMAL CONDUCTIVITY OF INCONEL-600							ISP84340
/*								ISP84350
/*								ISP84360
	5							ISP84370
	37.8	3.5133E-3	148.9	3.9597E-3	315.6	4.6087E-3		ISP84380
	593.3	5.6420E-3	1000.0	7.1553E-3				ISP84390
/*								ISP84400
/*	HEAT CAPACITY OF INCONEL-600							ISP84410
/*								ISP84420
	5							ISP84430
	37.8	916.024	204.4	979.463	315.6	1021.595		ISP84440
	426.7	1063.888	1000.0	1282.129				ISP84450
/*								ISP84460
/*	GAP CONDUCTANCE DATA							ISP84470
/*								ISP84480
	2							ISP84490
	0.0	0.0	1000	0.0				ISP84500
/*								ISP84510
/*	THERMAL CONDUCTIVITY OF BORON-NITRIDE							ISP84520
/*								ISP84530
	22							ISP84540
	50.0	0.5995E-2	100.0	0.5966E-2	150.0	0.5936E-2		ISP84550
	200.0	0.5907E-2	250.0	0.5877E-2	300.0	0.5848E-2		ISP84560
	350.0	0.5819E-2	400.0	0.5789E-2	450.0	0.5760E-2		ISP84570
	500.0	0.5731E-2	550.0	0.5701E-2	600.0	0.5672E-2		ISP84580
	650.0	0.5643E-2	700.0	0.5613E-2	750.0	0.5584E-2		ISP84590
	800.0	0.5555E-2	850.0	0.5525E-2	900.0	0.5496E-2		ISP84600
	950.0	0.5467E-2	1000.0	0.5437E-2	1050.0	0.5408E-2		ISP84610
	1100.0	0.5379E-2						ISP84620
/*								ISP84630
/*	HEAT CAPACITY OF BORON-NITRIDE							ISP84640
/*								ISP84650
	22							ISP84660
	50.0	0.4625E3	100.0	0.5279E3	150.0	0.5874E3		ISP84670
	200.0	0.6413E3	250.0	0.6899E3	300.0	0.7335E3		ISP84680
	350.0	0.7726E3	400.0	0.8074E3	450.0	0.8382E3		ISP84690
	500.0	0.8654E3	550.0	0.8895E3	600.0	0.9105E3		ISP84700
	650.0	0.9289E3	700.0	0.9451E3	750.0	0.9593E3		ISP84710
	800.0	0.9718E3	850.0	0.9831E3	900.0	0.9935E3		ISP84720
	950.0	0.1003E4	1000.0	0.1013E4	1050.0	0.1022E4		ISP84730
	1100.0	0.1032E4						ISP84740
/*								ISP84750
/*	GAP CONDUCTANCE							ISP84760
/*								ISP84770
	2							ISP84780
	0.0	0.0	1000.0	0.0				ISP84790
/*								ISP84800
/*	THERMAL CONDUCTIVITY OF CONSTANTAN							ISP84810
/*								ISP84820
	22							ISP84830
	50.0	0.6138E-2	100.0	0.6336E-2	150.0	0.6535E-2		ISP84840

200.0	0.6733E-2	250.0	0.6931E-2	300.0	0.7129E-2	ISP84840	
350.0	0.7328E-2	400.0	0.7526E-2	450.0	0.7724E-2	ISP84850	
500.0	0.7923E-2	550.0	0.8121E-2	600.0	0.8319E-2	ISP84860	
650.0	0.8517E-2	700.0	0.8716E-2	750.0	0.8914E-2	ISP84870	
800.0	0.9112E-2	850.0	0.9311E-2	900.0	0.9509E-2	ISP84880	
950.0	0.9707E-2	1000.0	0.9905E-2	1050.0	0.1010E-1	ISP84890	
1100.0	0.1030E-1					ISP84900	
/*						ISP84910	
/*	HEAT CAPACITY OF CONSTANTAN						ISP84920
	22					ISP84930	
50.0	0.8771E3	100.0	0.8945E3	150.0	0.9120E3	ISP84940	
200.0	0.9294E3	250.0	0.9469E3	300.0	0.9643E3	ISP84950	
350.0	0.9818E3	400.0	0.9992E3	450.0	0.1017E4	ISP84960	
500.0	0.1034E4	550.0	0.1052E4	600.0	0.1069E4	ISP84970	
650.0	0.1086E4	700.0	0.1104E4	750.0	0.1121E4	ISP84980	
800.0	0.1139E4	850.0	0.1156E4	900.0	0.1174E4	ISP84990	
950.0	0.1191E4	1000.0	0.1209E4	1050.0	0.1226E4	ISP85000	
1100.0	0.1244E4					ISP85010	
/*						ISP85020	
/*	GAP CONDUCTANCE DATA						ISP85030
	2					ISP85040	
	0.0	0.0	1000.0	0.0		ISP85050	
/*						ISP85060	
/*	THERMAL CONDUCTIVITY OF STAINLESS STEEL						ISP85070
/*	22					ISP85080	
	22					ISP85090	
50.0	0.3287E-2	100.0	0.3446E-2	150.0	0.3604E-2	ISP85100	
200.0	0.3763E-2	250.0	0.3921E-2	300.0	0.4079E-2	ISP85110	
350.0	0.4238E-2	400.0	0.4396E-2	450.0	0.4555E-2	ISP85120	
500.0	0.4713E-2	550.0	0.4872E-2	600.0	0.5030E-2	ISP85130	
650.0	0.5189E-2	700.0	0.5347E-2	750.0	0.5505E-2	ISP85140	
800.0	0.5664E-2	850.0	0.5822E-2	900.0	0.5981E-2	ISP85150	
950.0	0.6139E-2	1000.0	0.6298E-2	1050.0	0.6456E-2	ISP85160	
1100.0	0.6614E-2					ISP85170	
/*						ISP85180	
/*	HEAT CAPACITY OF STAINLESS STEEL						ISP85190
/*	22					ISP85200	
	22					ISP85210	
50.0	0.9204E3	100.0	0.9350E3	150.0	0.9495E3	ISP85220	
200.0	0.9640E3	250.0	0.9783E3	300.0	0.9926E3	ISP85230	
350.0	0.1007E4	400.0	0.1021E4	450.0	0.1035E4	ISP85240	
500.0	0.1049E4	550.0	0.1062E4	600.0	0.1076E4	ISP85250	
650.0	0.1090E4	700.0	0.1103E4	750.0	0.1117E4	ISP85260	
800.0	0.1130E4	850.0	0.1143E4	900.0	0.1156E4	ISP85270	
950.0	0.1170E4	1000.0	0.1182E4	1050.0	0.1195E4	ISP85280	
1100.0	0.1208E4					ISP85290	
/*						ISP85300	
/*	GAP CONDUCTANCE DATA						ISP85310
/*	2					ISP85320	
	2					ISP85330	
	0.0	0.0	1000.0	0.0		ISP85340	
/*						ISP85350	
/*	END OF DATA						ISP85360
/*						ISP85370	

```

/*****
/*      INDIVIDUAL PARAMETERS CORRESPONDING TO MEASUREMENT DATA      *
/*      PRESSURE                                                         *
/*          PU=PRIZE      -----          AP 10          *          *
/*          PB=42         -----          AP 17          *          *
/*          PB=43         -----          AP 35          *          *
/*          PV=UP+10     -----          AP 26          *          *
/*          PU=ACC       -----          AP 33          *          *
/*          PU=SGSD      -----          AP 21          *          *
/*      DIFFERENTIAL PRESSURE                                           *
/*          DPU-10-12    -----          AP 10- AP 12    *          *
/*          DPU-7-10     -----          AP 7 - AP 10    *          *
/*          DPB-32-36L   -----          AP 12- AP 15    *          *
/*          DPB-38-40   -----          AP 15- AP 17    *          *
/*          DPV-LP-UP    -----          AP 24- AP 26    *          *
/*      FLOW RATE                                                       *
/*          FTV-COREIN (V) -----          JW 27          *          *
/*          FTU-15      (V) -----          JW 10          *          *
/*          FTU-PRIZE  (V) -----          JW 12          *          *
/*          FTU-LPIS   (V) -----          JW 38          *          *
/*          FTU-HPIS   (V) -----          JW 37          *          *
/*          FTU-ACC    (V) -----          JW 35          *          *
/*          FTU-10, GU-10 -----          JW 7           *          *
/*          FDB-42, GB-42R -----          JW 29          *          *
/*          FDR-23, GB-23R -----          JW 30          *          *
/*      FLUID DENSITY                                                  *
/*          GB-42VR     -----          AR 17          *          *
/*          GB-23VR     -----          AR 35          *          *
/*          GU-15C      -----          AR 9           *          *
/*          GU-10       -----          AR 6           *          *
/*          GVCOR-150HZ -----          AR 25          *          *
/*          GV161/192D -----          AR 24          *          *
/*      FLUID TEMPERATURE                                             *
/*          TFU-PRIZE   -----          AT 11          *          *
/*          TFB-23      -----          AT 35          *          *
/*          TFV-UP+23   -----          AT 26          *          *
/*          *
/*****
/*

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ISP85380
ISP85390
ISP85400
ISP85410
ISP85420
ISP85430
ISP85440
ISP85450
ISP85460
ISP85470
ISP85480
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ISP85600
ISP85610
ISP85620
ISP85630
ISP85640
ISP85650
ISP85660
ISP85670
ISP85680
ISP85690
ISP85700
ISP85710
ISP85720
ISP85730
ISP85740
ISP85750
ISP85760

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## Appendix 2

Table 6 List of the Semiscale Function Code

Measurement	Function Code	Location and Comments
<u>FLUID TEMPERATURE</u>		Chromel-Alumel thermocouples unless specified otherwise.
Intact Loop		
TFU-1	TE000150	Hot leg, Spool 1, 54 cm from vessel center.
RBU-2	TE000023	Hot leg, Spool 2, 117 cm from vessel center (platinum resistance bulb).
TFU-7	TE000069	Cold leg, Spool 7, 624 cm from vessel center.
TFU-10	TE000152	Cold leg, Spool 10, 367 cm from vessel center.
RBU-14A	TE000024	Cold leg, Spool 14, 109 cm from vessel center, upstream of cold leg injection port (platinum resistance bulb).
TFU-14B	TE000162	Cold leg, Spool 14, 99 cm from vessel center, downstream of cold leg injection port.
TFU-15	TE000168	Cold leg, Spool 15, 54 cm from vessel center.
Broken Loop		
TFB-20	TE000159	Cold leg, Spool 20, 52 cm from vessel center.
TFB-23	TE000149	Cold leg, Spool 23, 232 cm from vessel center, upstream of vessel-side nozzle.
TFB-24	TE000201	Cold leg, Spool 24, 264 cm from vessel center, downstream from vessel-side nozzle.
TFB-30	TE000148	Hot leg, Spool 30, 40 cm from vessel center.
TFB-37	TE000161	Cold leg, Spool 37, 703 cm from vessel center along hot leg, discharge of simulated steam generator.
TFB-42	TE000151	Cold leg, Spool 42, 1054 cm from vessel center along hot leg, upstream of pump-side nozzle.
TFB-43	TE000200	Cold leg, Spool 43, 1086 cm from vessel center along hot leg.
TFB-RFB-C	TE000145	Reflood bypass, near end cap, cold leg side.
TFB-RFB-H	TE000166	Reflood bypass, near end cap, hot leg side.
Inlet Annulus		10 cm below cold leg centerline, 0.5 cm from vessel wall, Type iron-constantan thermocouples.
TFV-ANN-4A	TE000202	0°.
TFV-ANN-4M	TE000191	180°.

Measurement	Function Code	Location and Comments
Downcomer Annulus		Centered in annulus, Type J iron-constantan thermocouples.
TFV-ANN-15T	TE000180	38 cm below cold leg centerline, 270°.
TFV-ANN-35A	TE000176	89 cm below cold leg centerline, 0°.
TFV-ANN-35T	TE000181	89 cm below cold leg centerline, 270°.
TFV-ANN-70A	TE000178	178 cm below cold leg centerline, 0°.
TFV-ANN-115A	TE000177	292 cm below cold leg centerline, 0°.
TFV-ANN-115M	TE000182	292 cm below cold leg centerline, 180°.
TFV-ANN-156A	TE000184	396 cm below cold leg centerline, 0°.
Upper Plenum TFV-UP+13	TE000135	In upper plenum, 34 cm above cold leg centerline at 180°.
Lower Plenum		On fluid thermocouple rack, 2.54 cm from vessel center, 45°.
TFV-LP-8	TE000186	19 cm from bottom of vessel.
TFV-LP-15	TE000187	37 cm from bottom of vessel.
TFV-LP-22	TE000188	55 cm from bottom of vessel.
Core TFV-CORE-IN	TE000196	In core flow mixer box, 381 cm below cold leg centerline (a part of FDV-CORE-IN).
Core Grid Spacers Grid Spacer 5		140 cm below cold leg centerline, 54.6 cm above top of heated length.
TFG-5CD-45	TE000050	Thermocouple in space defined by Columns C and D, Rows 4 and 5.
Grid Spacer 6		193 cm below cold leg centerline, 1.3 cm above top of heated length.
TFG-6CD-45	TE000158	Thermocouple in space defined by Columns C and D, Rows 4 and 5.
TFG-6DE-67	TE000130	Thermocouple in space defined by Columns D and E, Rows 6 and 7.
Grid Spacer 10		363 cm below cold leg centerline at bottom of heated length.
TFG-10AB-45	TE000033	Thermocouple in space defined by Columns A and B, Rows 4 and 5.
TFG-10GH-45	TE000103	Thermocouple in space defined by Columns G and H, Rows 4 and 5.

Measurement	Function Code	Location and Comments
ECC System TFU-ECC-14	TE000031	In ECC line leading to intact loop spool 14.
Steam Generator TFU-SGFW	TE000167	In feedwater line leading to steam generator.
TFU-SGSD	TE000028	In steam dome, 329 cm above bottom of tube sheet.
TFU-SG1	TE000124	Secondary side, 30 cm above bottom of tube sheet.
TFU-SG3	TE000077	Secondary side, 122 cm above bottom of tube sheet.
TFU-SG4	TE000027	Secondary side, 244 cm above bottom of tube sheet.
Pressurizer TFU-PRISE	TE000080	In surge line, near pressurizer exit, between turbine flowmeter and pressurizer.
Pressure Suppression System TF-PSS-33	TE000082	84 cm from bottom of tank.
TF-PSS-63	TE000107	160 cm from bottom of tank.
TF-PSS-130	TE000085	330 cm from bottom of tank.
<u>MATERIAL TEMPERATURE</u>		Chromel-Alumel thermocouples unless specified otherwise.
Intact Loop TMU-1T16	TE000110	Hot leg, Spool 1, top, 1.6 mm from pipe ID, 54 cm from vessel center.
TMU-15T16	TE000142	Cold leg, Spool 15, top, 1.6 mm from pipe ID, 54 cm from vessel center.
Broken Loop TMB-20B16	TE000157	Cold leg, Spool 20, bottom, 1.6 mm from pipe ID, 52 cm from vessel center.
TMB-30B16	TE000087	Hot leg, Spool 30, bottom, 1.6 mm from pipe ID, 40 cm from vessel center.
Vessel Filler TMV-FI-115A	TE000122	Type J iron-constantan 292 cm below cold leg centerline, 1.6 mm from filler ID, 0°.
Core Barrel TMV-CI-35A	TE000192	Type J iron-constantan thermocouples. 89 cm below cold leg centerline, 1.6 mm from core barrel ID, 0°.



Measurement	Function Code	Location and Comments
<u>CORE HEATER CLADDING TEMPERATURE</u>		Chromel-Alumel thermocouples.
High Power Heaters		
TH-D4-14	TE000194	Heater at Column D, Row 4. Thermocouples 36 cm (270°) and 74 cm (315°) above bottom of core.
TH-D4-29	TE000193	
TH-D5-09	TE000052	Heater at Column D, Row 5. Thermocouples 23 cm (45°), 74 cm (225°) and 99 cm (135°) above bottom of core.
TH-D5-29	TE000102	
TH-D5-39	TE000037	
TH-E4-09	TE000054	Heater at Column E, Row 4. Thermocouples 23 cm (180°), 69 cm (90°) and 140 cm (0°) above bottom of core.
TH-E4-27	TE000169	
TH-E4-55	TE000170	
TH-E5-21	TE000164	Heater at Column E, Row 5. Thermocouple 53 cm (180°) above bottom of core.
Low Power Heaters		
TH-A4-09	TE000172	Heater at Column A, Row 4. Thermocouples 23 cm (105°) and 74 cm (240°) above bottom of core.
TH-A4-29	TE000128	
TH-A5-29	TE000147	Heater at Column A, Row 5. Thermocouples 74 cm (180°) and 114 cm (255°) above bottom of core.
TH-A5-45	TE000160	
TH-B3-32	TE000171	Heater at Column B, Row 3. Thermocouple 81 cm (135°) above bottom of core.
TH-B5-29	TE000098	Heater at Column B, Row 5. Thermocouples 74 cm (150°) and 85 cm (45°) above bottom of core.
TH-B5-33	TE000140	
TH-B6-14	TE000106	Heater at Column B, Row 6. Thermocouples 36 cm (0°) and 74 cm (45°) above bottom of core.
TH-B6-29	TE000104	
TH-C2-28	TE000163	Heater at Column C, Row 2. Thermocouples 71 cm (135°) and 97 cm (225°) above bottom of core.
TH-C2-38	TE000199	
TH-C3-60	TE000032	Heater at Column C, Row 3. Thermocouple 152 cm (135°) above bottom of core.
TH-C4-20	TE000066	Heater at Column C, Row 4. Thermocouples 51 cm (150°) and 66 cm (75°) above bottom of core.
TH-C4-26	TE000203	
TH-C5-28	TE000155	Heater at Column C, Row 5. Thermocouple 71 cm (315°) above bottom of core.
TH-C6-32	TE000079	Heater at Column C, Row 6. Thermocouples 81 cm (225°) and 135 cm (270°) above bottom of core.
TH-C6-53	TE000070	

Measurement	Function Code	Location and Comments
Low Power Heaters (continued)		
TH-C7-07 TH-C7-15	TE000097 TE000143	Heater at Column C, Row 7. Thermocouples 18 cm (345°) and 38 cm (255°) above bottom of core.
TH-D1-21	TE000146	Heater at Column D, Row 1. Thermocouple 53 cm (330°) above bottom of core.
TH-D2-14 TH-D2-61	TE000055 TE000053	Heater at Column D, Row 2. Thermocouples 36 cm (0°) and 155 cm (270°) above bottom of core.
TH-D3-29 TH-D3-33 TH-D3-39	TE000034 TE000165 TE000190	Heater at Column D, Row 3. Thermocouples 74 cm (150°), 84 cm (45°) and 99 cm (210°) above bottom of core.
TH-D7-20	TE000189	Heater at Column D, Row 7. Thermocouple 51 cm (60°) above bottom of core.
TH-D8-57	TE000132	Heater at Column D, Row 8. Thermocouple 145 cm (15°) above bottom of core.
TH-E1-33	TE000195	Heater at Column E, Row 1. Thermocouple 84 cm (60°) above bottom of core.
TH-E2-20 TH-E2-33	TE000129 TE000026	Heater at Column E, Row 2. Thermocouples 51 cm (210°) and 84 cm (315°) above bottom of core.
TH-E3-24	TE000116	Heater at Column E, Row 3. Thermocouple 61 cm (75°) above bottom of core.
TH-E6-08 TH-E6-28 TH-E6-37	TE000154 TE000197 TE000153	Heater at Column E, Row 6. Thermocouples 20 cm (150°), 71 cm (285°) and 94 cm (330°) above bottom of core.
TH-E7-13 TH-E7-44	TE000101 TE000035	Heater at Column E, Row 7. Thermocouples 33 cm (45°) and 112 cm (195°) above bottom of core.
TH-E8-14 TH-E8-29 TH-E8-45	TE000141 TE000144 TE000173	Heater at Column E, Row 8. Thermocouples 36 cm (150°), 74 cm (225°) and 114 cm (300°) above bottom of core.
TH-F2-07 TH-F2-22 TH-F2-25	TE000138 TE000084 TE000095	Heater at Column F, Row 2. Thermocouples 18 cm (255°), 56 cm (105°) and 64 cm (0°) above bottom of core.
TH-F3-06 TH-F3-22 TH-F3-25	TE000036 TE000183 TE000185	Heater at Column F, Row 3. Thermocouples 15 cm (315°), 56 cm (105°) and 64 cm (30°) above bottom of core.
TH-F4-14 TH-F4-29 TH-F4-44	TE000099 TE000156 TE000136	Heater at Column F, Row 4. Thermocouples 36 cm (90°), 74 cm (165°) and 112 cm (210°) above bottom of core.
TH-F5-20 TH-F5-26	TE000175 TE000126	Heater at Column F, Row 5. Thermocouples 51 cm (255°) and 66 cm (165°) above bottom of core.

Measurement	Function Code	Location and Comments
<b>Low Power Heaters (continued)</b>		
TH-F6-08 TH-F6-28	TE000179 TE000096	Heater at Column F, Row 6. Thermocouples 20 cm (60°) and 71 cm (210°) above bottom of core.
TH-G3-13	TE000059	Heater at Column G, Row 3. Thermocouples 33 cm (150°) above bottom of core.
TH-G4-29 TH-G4-33 TH-G4-38	TE000198 TE000174 TE000139	Heater at Column G, Row 4. Thermocouples 74 cm (300°), 84 cm (225°) and 97 cm (30°) above bottom of core.
TH-G5-14 TH-G5-24	TE000205 TE000204	Heater at Column G, Row 5. Thermocouples 36 cm (45°) and 61 cm (330°) above bottom of core.
TH-H5-32	TE000133	Heater at Column H, Row 5. Thermocouple 81 cm (45°) above bottom of core.
<b>PRESSURE</b>		
<b>Intact Loop</b>		
PU-13	PG000042	Cold leg, Spool 13, 138 cm from vessel center.
PU-15L	PG000040	Cold leg, Spool, 15, 55 cm from vessel center, to atmosphere (low range).
<b>Broken Loop</b>		
PB-21	PG000065	Cold leg, Spool 21, 112 cm from vessel center.
PB-23	PG000072	Cold leg, Spool 23, 235 cm from vessel center, upstream of nozzle (tee off DP tap).
PB-24	PG000076	Cold leg, Spool 24, 264 cm from vessel center, downstream of nozzle.
PB-30	PG000051	Hot leg, Spool 30, 45 cm from vessel center (tee off DP tap).
PB-42	PG000073	Cold leg, Spool 42, 1057 cm from vessel center along hot leg, upstream of pump-side nozzle (tee off DP tap).
PB-43	PG000105	Cold leg, Spool 43, 1086 cm from vessel center along hot leg, upstream of rupture discs.
PB-CN1	PG000062	Vessel-side nozzle, nozzle throat 245 cm from vessel center (tee off DP tap).
<b>Vessel</b>		
PV-UP+10	PG000046	In upper plenum, 25 cm above cold leg centerline, mounted on standoff, 30°.
PV-LP-180	PG000119	In upper part of lower plenum, 457 cm below cold leg centerline, mounted on standoff, 225°.

Measurement	Function Code	Location and Comments
ECC System PU-ACC	PG000137	In intact loop accumulator.
Steam Generator PU-SGSD	PG000043	Secondary side steam dome.
Pressurizer PU-PRIZE	PG000056	Pressurizer steam dome.
Pressure Suppression System P-PSS	PG000091	Suppression tank top.
<u>DIFFERENTIAL PRESSURE</u>		Elevation difference between transducer taps is zero unless otherwise specified.
Intact Loop DPU-UP-3	PD000049	Upper plenum 26.7 cm above cold leg centerline at 30° to hot leg, Spool 3, 158 cm from vessel center. Upper plenum tap is approximately 5 cm above Spool 3 tap.
DPU-3-6	PD000045	Hot leg Spool 3, 158 cm from vessel center to hot leg Spool 6, 290 cm from vessel center.
DPU-6-SGIP	PD000089	Hot leg, Spool 6, 290 cm from vessel center to steam generator inlet plenum 368 cm from vessel center. Spool 6 tap is 41 cm below SGIP tap.
DPU-6-7	DP000047	Across steam generator, hot leg Spool 6, 290 cm from vessel center to cold leg. Spool 7, 587 cm from vessel center. Spool 6 tap is 48 cm above Spool 7 tap.
DPU-SGOP-7	PD000088	From steam generator outlet plenum 683 cm from vessel center along cold leg to cold leg Spool 7, 587 cm from vessel center, including orifice. Spool 7 tap is 89 cm below SGOP tap.
DPU-7-10	PD000109	Steam generator outlet to pump inlet, cold leg Spool 7, 587 cm from vessel center, to cold leg Spool 10, 359 cm from vessel center.
DPU-12-10	PD000093	Pump outlet to pump inlet, cold leg Spool 12, 192 cm from vessel center, to cold leg Spool 10, 359 cm from vessel center. Spool 10 tap is 25 cm below Spool 12 tap.
DPU-12-10L	PD000094	Pump outlet to pump inlet, cold leg Spool 12, 192 cm from vessel center, to cold leg Spool 10, 359 cm from vessel center. Spool 10 tap is 25 cm below Spool 12 tap (low range).
DPU-12-15	PD000048	Cold leg Spool 12, 192 cm from vessel center, to cold leg Spool 15, 55 cm from vessel center.

Measurement	Function Code	Location and Comments
Intact Loop (continued)		
DPU-15-3	PD000074	Cold leg to hot leg; cold leg Spool 15, 55 cm from vessel center, to hot leg Spool 3, 158 cm from vessel center. Spool 15 tap is 22 cm below Spool 3 tap.
DPU-15-3L	PD000075	Cold leg to hot leg, cold leg Spool 15, 55 cm from vessel center, to hot leg Spool 3, 158 cm from vessel center. Spool 15 tap is 22 cm below Spool 3 tap (low range).
DPU-15-IANN	PD000108	Cold leg Spool 15, 55 cm from vessel center, to inlet annulus, 23 cm below cold leg centerline at 225°. Spool 15 tap is 23 cm above inlet annulus tap.
DPU-PRESLL	PD000058	Pressurizer water level. Elevation difference between taps is 135 cm. Lower tap is 9 cm above pressurizer exit.
DPU-PR-4	PD000100	Pressurizer bottom to Spool 4. Elevation difference between taps is 157 cm. Spool 4 tap is 140 cm below pressurizer exit.
Broken Loop		
DPB-21-IANN	PD000092	Cold leg Spool 21, 112 cm from vessel center, to vessel inlet annulus, 23 cm below cold leg centerline at 225°. Inlet annulus tap is 23 cm below Spool 21 tap.
DPB-21-23	PD000067	Cold leg, Spool 21, 112 cm from vessel center, to cold leg 23, 235 cm from vessel center.
DPB-23-CNI	PD000078	Cold leg, Spool 23, 235 cm from vessel center to vessel-side nozzle throat, 245 cm from vessel center.
DPB-23-24	PD000068	Across vessel-side nozzle, Spool 23, 235 cm from vessel center to Spool 24, 264 cm from vessel center.
DPB-30-36L	PD000057	Across entire simulated steam generator assembly, hot leg Spool 30, 45 cm from vessel center, to cold leg Spool 36 lower tap, 617 cm from vessel center. Spool 30 tap is 48 cm below Spool 36 lower tap.
DPB-30-38	PD000111	Across entire simulated steam generator assembly and instrument spool down-stream of simulated steam generator; hot leg Spool 30, 45 cm from vessel center to cold leg, Spool 38, 776 cm from vessel center along hot leg. Spool 30 tap is 102 cm above Spool 38 tap.

Measurement	Function Code	Location and Comments
Broken Loop (continued)		
DPB-32U-36L	PD000063	Across simulated steam generator orifice assembly, hot leg Spool 32 upper tap, 189 cm from vessel center, to Spool 36 lower tap, 617 cm from vessel center. Spool 32 upper tap is 41 cm above Spool 36 lower tap.
DPB-38-40	PD000081	Across simulated pump, cold leg Spool 38, 776 cm from vessel center along hot leg, to cold leg Spool 40, 929 cm from vessel center along hot leg.
DPB-40-42	PD000086	Across elbow leading to spool up-stream of pump-side nozzle. Cold leg Spool 40, 929 cm from vessel center along hot leg, to Spool 42, 1057 cm from vessel center along hot leg. Spool 40 tap is 102 cm below Spool 42 tap.
DPB-42-43	PD000090	Across pump-side nozzle cold leg Spool 42, 1057 cm from vessel center along hot leg, to cold leg, Spool 43 1086 cm from vessel center along hot leg.
Vessel		
DPV-UP-IANN	PD000115	Upper plenum, 27 cm above cold leg centerline at 30° to inlet annulus, 23 cm below cold leg centerline at 225°. Elevation difference between taps is 48 cm.
DPV-0-9GQ	PD000044	Inlet annulus cold leg centerline at 90°, to 23 cm below cold leg centerline at 225°. Elevation difference between taps is 23 cm.
DPV-9-26QQ	PD000117	Inlet annulus, 23 cm below cold leg centerline at 225°, to downcomer gap, 66 cm below cold leg centerline at 225°. Elevation difference between taps is 43 cm.
DPV-9-180QQ	PD000112	Inlet annulus, 23 cm below cold leg centerline at 225°, to lower plenum, 457 cm below cold leg centerline at 225°. Elevation difference between taps is 434 cm.
DPV-26-55QM	PD000118	Across part of downcomer, 66 cm (225°), to 140 cm (180°), below cold leg centerline. Elevation difference between taps is 74 cm.
DPV-55-110MM	PD000121	Across part of downcomer, 140 cm (180°), to 279 cm (180°), below cold leg centerline. Elevation difference between taps is 140 cm.
DPV-110-15MQ	PD000127	Across part of downcomer, 279 cm (180°), to 396 cm (225°), below cold leg centerline. Elevation difference between taps is 117 cm.

Measurement	Function Code	Location and Comments
Vessel (continued) DPV-156-173QQ	PD000113	Across part of lower plenum, 396 cm (225°), to 439 cm (225°), below cold leg centerline. Elevation difference between taps is 43 cm.
DPV-166-192QT	PD000114	Across lower plenum, 422 cm (225°) to 488 cm (270°), below cold leg centerline. Elevation difference between taps is 66 cm.
DPV-173-180QQ	PD000123	Across part of lower plenum, 439 cm (225°) to 457 cm (225°), below cold leg centerline. Elevation difference between taps is 18 cm.
DPV-LP-UP	PD000120	Lower plenum, 457 cm below cold leg centerline at 225° to upper plenum, 27 cm above cold leg centerline at 30°. Elevation difference between taps is 485 cm.
ECC System DPU-ACC-TB	PD000030	Top to bottom of intact loop accumulator. Elevation difference between taps is 274 cm.
Steam Generator DPU-SGFW	PD000018	In steam generator feedwater line.
DPU-SG-SEC	PD000060	Secondary side, differential pressure taps at 114 cm and 320 cm above bottom of tube sheet. Elevation difference between taps is 206 cm.
DPU-SG-DISC	PD000029	Across venturi tube, 168 cm downstream from steam generator discharge.
Pressure Suppression System DP-PSS-TB	PD000125	Top to bottom of pressure suppression tank. Elevation difference between taps is 338 cm.
<u>VOLUMETRIC FLOW RATE</u>		Turbine flowmeter, bidirectional.
Intact Loop		3-in. Schedule 160 pipe.
FTU-1	FV000001	Hot leg, Spool 1, 42 cm from vessel center.
FTU-9	FV000002	Cold leg, Spool 9, 393 cm from vessel center.
FTU-13	FV000003	Cold leg, Spool 13, 163 cm from vessel center.
FTU-15	FV000004	Cold leg, Spool 15, 42 cm from vessel center.
Broken Loop		Schedule 160 pipe.
FTB-21	FV000006	Cold leg, Spool 21, 146 cm from vessel center; 3-in. pipe.
FTB-30	FV000007	Hot leg, Spool 30, 63 cm from vessel center; 3-in. pipe.

Measurement	Function Code	Location and Comments
Broken Loop (continued) FTB-37	FV000005	Cold leg, Spool 37, 739 cm from vessel center along hot leg; 2-in. pipe.
Core FTV-CORE-IN	FV000010	Entrance to core, 401 cm below cold leg centerline.
ECC System FTU-HPIS	FV000016	In line immediately after HPIS pump for intact loop, 1/2-in. line.
FTU-LPIS	FV000017	In line leading from LPIS pump for intact loop, 1/2-in. line.
FTU-ACC	FV000022	In line leading from intact loop accumulator, 1-in. line.
Pressurizer FTU-PRIZE	FV000020	1-1/2-in. turbine Surge line.
<u>FLUID VELOCITY</u>		Turbine flowmeter, bidirectional.
Downcomer FTV-40A	VE000008	102 cm below cold leg centerline, 0°.
FTV-40M	VE000009	102 cm below cold leg centerline, 180°.
<u>MOMENTUM FLUX</u>		Drag disc, bidirectional.
Intact Loop		3-in. pipe.
FDU-1	MF000131	Hot leg, Spool 1, 60 cm from vessel center; target size 2.22 cm.
FDU-5	MF000011	Hot leg, Spool 5, 256 cm from vessel center; target size 2.54 cm.
FDU-10	MF000038	Cold leg, Spool 10, 349 cm from vessel center; target size 2.22 cm.
FDU-13	MF000039	Cold leg, Spool 13, 138 cm from vessel center; target size 2.22 cm.
FDU-15	MF000134	Cold leg, Spool 15, 60 cm from vessel center; target size 2.22 cm.
Broken Loop FDB-21	MF000061	Cold leg, Spool 21, 134 cm from vessel center, 3-in. pipe; target size 1.67 cm.
FDB-23	MF000064	Cold leg, Spool 23, 238 cm from vessel center, upstream of vessel side nozzle, 2-in. pipe; target size 1.03 cm.
FDB-30	MF000041	Hot leg, Spool 30, 52 cm from vessel center, 3-in. pipe; target size 1.03 cm.



Measurement	Function Code	Location and Comments
Broken Loop (continued) FDB-37	MF000083	Cold leg, Spool 37, 725 cm from vessel center along hot leg, steam generator outlet, vertical pipe, 2-in. pipe; target size 1.03 cm.
FDB-42	MF000071	Cold leg, Spool 42, 1057 cm from vessel center along hot leg, upstream of pump-side nozzle, downstream of injection point, 2-in. pipe; target size 1.03 cm.
Vessel FDV-CORE-IN	MF000019	In core flow mixer box, 381 cm below cold leg centerline; target size 2.54 cm.
<u>DENSITY</u>		
Intact Loop GU-1T GU-1B GU-1C	DE000233 DE000232 DE000238	Hot leg, Spool 1, 77 cm from vessel center. T (top) ranges 270 to 360°. B (bottom) ranges 30 to 330°. C is a mathematical composite of T and B.
GU-5VR	DE000213	Hot leg, Spool 5, 246 cm from vessel center, vertical.
GU-10VR	DE000214	Cold leg, Spool 10, 359 cm from vessel center, vertical.
GU-13VR	DE000215	Cold leg, Spool 13, 142 cm from vessel center, vertical.
GU-15T GU-15B GU-15C	DE000235 DE000234 DE000239	Cold leg, Spool 15, 77 cm from vessel center. T (top) ranges 270 to 360°. B (bottom) ranges 30 to 330°. C is a mathematical composite of T and B.
Broken Loop GB-21T GB-21B GB-21C	DE000229 DE000228 DE000236	Cold leg, Spool 21, 123 cm from vessel center. T (top) ranges 270 to 360°. B (bottom) ranges 30 to 330°. C is a mathematical composite of T and B.
GB-23VR	DE000219	Cold leg, Spool 23, 235 cm from vessel center, vertical.
GB-30T GB-30B GB-30C	DE000231 DE000230 DE000237	Hot leg, Spool 30, 49 cm from vessel center. T (top) ranges 270 to 360°. B (bottom) ranges 30 to 330°. C is a mathematical composite of T and B.
GB-37	DE000218	Cold leg, Spool 37, 709 cm from vessel center along hot leg, across vertical pipe, simulated steam generator discharge.
GB-42VR	DE000217	Cold leg, Spool 42, 1057 cm from vessel center along hot leg, vertical.

Measurement	Function Code	Location and Comments
Vessel GV-COR-150HZ	DE000212	Core flow mixer box, 386 cm below cold leg centerline, horizontal, 0 to 180°.
GV-161/192D	DE000207	Lower plenum, 409 cm below cold leg centerline (270°) to 488 cm below cold leg centerline (90°), 79 cm vertical, 82 cm diagonal.
GVLP-165HZ	DE000221	Upper part of lower plenum, 419 cm below cold leg centerline, 4.379 cm below downcomer exit, horizontal 0 to 180°.
GVLP-172HZ	DE000211	Lower plenum, 437 cm below cold leg centerline, 22 cm below downcomer exit, horizontal, 90 to 270°.
Pressurizer GU-PRIZE	DE000224	Surge line.
<u>CORE CHARACTERISTICS</u>		
PWRCOR T-1	PP000012	Core power.
PWRCOR T-2	PP000013	Core power.
VOLTCOR-T	V0000015	Core voltage.
AMPCOR-T	CT000014	Core current.
<u>PUMP CHARACTERISTICS</u>		
PUMPU-CUR	CT000021	Pump current.
PUMPU-RPM	SR000025	Pump speed.
<u>MASS FLOW RATE</u>		
Mass flow rate obtained by combining density (gamma attenuation technique) with volumetric flow rate (turbine flowmeter) or momentum flux (drag disc).		
Intact Loop		
FDU-1, GU-1C	FA000347	Hot Leg, Spool 1.
FTU-1, GU-1C	FA000287	
FDU-5, GU-5VR	FA000353	Hot Leg, Spool 5.
FTU-9, GU-10VR	FA000293	Cold Leg, Spool 9.
FDU-10, GU-10VR	FA000359	Cold Leg, Spool 10.
FDU-13, GU-13VR	FA000245	Cold Leg, Spool 13.
FTU-13, GU-13VR	FA000299	
FDU-15, GU-15C	FA000251	Cold Leg, Spool 15.
FTU-15, GU-15C	FA000305	
Broken Loop		
FDB-21, GB-21C	FA000257	Cold Leg, Spool 21.
FTB-21, GB-21C	FA000311	

Measurement	Function Code	Location and Comments
<b>Broken Loop (continued)</b>		
FDB-23, GB-23VR	FA000263	Cold Leg, Spool 23.
FDB-30, GB-30C	FA000269	Hot Leg, Spool 30.
FTB-30, GB-30C	FA000317	
FDB-37, GB-37	FA000275	Hot Leg, Spool 37.
FTB-37, GB-37	FA000323	
FDB-42, GB-42VR	FA000281	Hot Leg, Spool 42.
<b>Vessel</b>		
FDV-CORE-IN GV-COR-150HZ	FA000341	Entrance to Core.
FTV-CORE-IN GV-COR-150HZ	FA000329	Entrance to Core.
<b>Pressurizer</b>		
FTU-PRIZE GU-PRIZE	FA000335	Pressurizer Surge Line.
<b>INTEGRATED FLOW RATE</b>		
<b>Intact Loop</b>		
FD01IFLO	IF000348	Hot Leg, Spool 1.
FT01IFLO	IF000288	
FD05IFLO	IF000354	Hot Leg, Spool 5.
FT09IFLO	IF000294	Cold Leg, Spool 9.
FD13IFLO	IF000246	Cold Leg, Spool 13.
FT13IFLO	IF000300	
FD15IFLO	IF000252	Cold Leg, Spool 15.
FT15IFLO	IF000306	
<b>Broken Loop</b>		
FD21IFLO	IF000258	Cold Leg, Spool 21.
FT21IFLO	IF000312	
FD23IFLO	IF000264	Cold Leg, Spool 23.
FD30IFLO	IF000270	Hot Leg, Spool 30.
FT30IFLO	IF000318	
FD37IFLO	IF000276	Hot Leg, Spool 37.
FT37IFLO	IF000324	
FD42IFLO	IF000282	Hot Leg, Spool 42.
<b>Vessel</b>		
FDC0IFLO	IF000342	Entrance to Core.
FTC0IFLO	IF000330	Entrance to Core.
<b>Pressurizer</b>		
FTPZIFLO	IF000336	Pressurizer Surge Line.

Measurement	Function Code	Location and Comments
<u>MOMENTUM FLUX</u>		
Intact Loop		
FD01R*V2	MF000349	Hot Leg, Spool 1.
FT01R*V2	MF000289	
FD05R*V2	MF000355	Hot Leg, Spool 5.
FT09R*V2	MF000295	Cold Leg, Spool 9.
FD10R*V2	MF000241	Cold Leg, Spool 10.
FD13R*V2	MF000247	Cold Leg, Spool 13.
FT13R*V2	MF000301	
FD15R*V2	MF000253	Cold Leg, Spool 15.
FT15R*V2	MF000307	
Broken Loop		
FD21R*V2	MF000259	Cold Leg, Spool 21.
FT21R*V2	MF000313	
FD23R*V2	MF000265	Cold Leg, Spool 23.
FD30R*V2	MF000271	Hot Leg, Spool 30.
FT30R*V2	MF000319	
FD37R*V2	MF000277	Hot Leg, Spool 37.
FT37R*V2	MF000325	
FD42R*V2	MF000283	Hot Leg, Spool 42.
Vessel		
FDCOR*V2	MF000343	Entrance to Core.
FTCOR*V2	MF000331	Entrance to Core.
Pressurizer		
FTPZR*V2	MF000337	Pressurizer Surge Line.
<u>VOLUMETRIC FLOW RATE</u>		
Intact Loop		
FD01GPM	FV000350	Hot Leg, Spool 1.
FT01GPM	FV000290	
FD05GPM	FV000356	Hot Leg, Spool 5.
FT09GPM	FV000296	Cold Leg, Spool 9.
FD10GPM	FV000242	Cold Leg, Spool 10.
FD13GPM	FV000248	Cold Leg, Spool 13.
FT13GPM	FV000302	
FD15GPM	FV000254	Cold Leg, Spool 15.
FT15GPM	FV000308	
Broken Loop		
FD21GPM	FV000260	Cold Leg, Spool 21.
FT21GPM	FV000314	

Measurement	Function Code	Location and Comments
<b>Broken Loop (continued)</b>		
FD23GPM	FV000266	Cold Leg, Spool 23.
FD30GPM	FV000272	Hot Leg, Spool 30.
FT30GPM	FV000320	
FD37GPM	FV000278	Hot Leg, Spool 37.
FT37GPM	FV000326	
FD42GPM	FV000284	Hot Leg, Spool 42.
<b>Vessel</b>		
FDCOGPM	FV000344	Entrance to Core.
FTCOGPM	FV000332	
<b>Pressurizer</b>		
FTPZGPM	FV000338	Pressurizer Surge Line.
<b>VELOCITY</b>		
<b>Intact Loop</b>		
FD01VELO	VE000345	Hot Leg, Spool 1.
FT01VELO	VE000285	
FD05VELO	VE000351	Hot Leg, Spool 5.
FT09VELO	VE000291	Cold Leg, Spool 9.
D10VELOC	VE000357	Cold Leg, Spool 10.
FD13VELO	VE000243	Cold Leg, Spool 13.
FT13VELO	VE000297	
FD15VELO	VE000249	Cold Leg, Spool 15.
FT15VELO	VE000303	
<b>Broken Loop</b>		
FD21VELO	VE000255	Cold Leg, Spool 21.
FT21VELO	VE000309	
FD23VELO	VE000261	Cold Leg, Spool 23.
FD30VELO	VE000267	Hot Leg, Spool 30.
FT30VELO	VE000315	
FD37VELO	VE000273	Hot Leg, Spool 37.
FT37VELO	VE000321	
FD42VELO	VE000279	Hot Leg, Spool 42.
FDCOVELO	VE000339	Entrance to Core.
FTCOVELO	VE000327	
<b>Pressurizer</b>		
FTPZVELO	VE000333	Pressurizer Surge Line.

Measurement	Function Code	Location and Comments
<u>MOMENTUM FLUX</u>		
Intact Loop		
FD01MFLU	MF000346	Hot Leg, Spool 1.
FT01MFLU	MF000286	
FD05MFLU	MF000352	Hot Leg, Spool 5.
FT09MFLU	MF000292	Cold Leg, Spool 9.
D10MFLUX	MF000358	Cold Leg, Spool 10.
FD13MFLU	MF000244	Cold Leg, Spool 13.
FT13MFLU	MF000298	
FD15MFLU	MF000250	Cold Leg, Spool 15.
FT15MFLU	MF000304	
Broken Loop		
FD21MFLU	MF000256	Cold Leg, Spool 21.
FT21MFLU	MF000310	
FD23MFLU	MF000262	Cold Leg, Spool 23.
FD30MFLU	MF000268	Hot Leg, Spool 30.
FT30MFLU	MF000316	
FD37MFLU	MF000274	Hot Leg, Spool 37.
FT37MFLU	MF000322	
FD42MFLU	MF000280	Hot Leg, Spool 42.
Vessel		
FDCOMFLU	MF000340	Entrance to core.
FTCOMFLU	MF000328	
Pressurizer		
FTPZMFLU	MF000334	Pressurizer Surge Line.
<u>UNKNOWN DATA</u>		
BDV-23	BD000209	