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RECALCULATION OF SIMULATED POST-SCRAM
CORE POWER DECAY CURVE FOR USE IN
ROSA IV/LSTF EXPERIMENTS ON PWR SMALL-
BREAK LOCAs AND TRANSIENTS

August 1990

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Recalculation of Simulated Post-Scram Core Power Decay
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and Transients

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Simulated post-scrum core power decay curve for use in Large Scale Test Facility (LSTF) tests has been calculated on a best-estimate basis, particularly in two points, i.e. estimation of the delayed neutron fission power and consideration of the stored heat in a pressurized water reactor (PWR) fuel rod. The New Power Curve provides a LSTF heater rod with the heat transfer rate from a PWR fuel rod that was estimated for a typical pressure transient during a PWR small-break loss of coolant accident. This approach neglects conservatively the effect of stored heat release from the LSTF heater rod considering that there is large uncertainty in the thermal conductivity of outer insulator in the LSTF heater rod. When the New Power Curve is used as the LSTF core power curve, the heat transfer rate from a LSTF heater rod gives a little conservative values as compared with the heat transfer rate from a PWR fuel rod.

Keywords: PWR, LOCA, ROSA-IV, LSTF, Core Power Curve, Fuel Rod,
Heater Rod, Stored Heat, Decay Power, Fission Power

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PWR小破断LOCA及び過渡変化に関するROSA-IV/LSTF実験
のためのスクラム後模擬炉心出力減衰曲線

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大型非定常試験装置(LSTF)実験のためのスクラム後模擬炉心出力減衰曲線を、特に遅発中性子による核分裂出力の評価及び加圧水型原子炉(PWR)燃料棒の蓄積熱の考慮という2点において、最適評価ベースで計算した。新出力曲線により、PWR小破断冷却材喪失事故時の典型的な圧力変化に対するPWR燃料棒からの熱伝達量を、LSTFヒーターロッドにより模擬できる。本手法では、LSTFヒーターロッド中の外側絶縁材の熱伝導率の値に不確かさがあるため、LSTFヒーターロッドの蓄積熱は無視し保守的に評価している。新出力曲線をLSTF炉心出力曲線として用いた場合、LSTFヒーターロッドよりの熱伝達量は、PWR燃料棒よりの熱伝達量と比較して、少し保守的な値を与える。

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1. Introduction

The Rig-of-Safety Assessment No. 4 (ROSA-IV) Program⁽¹⁾ was launched in 1980 immediately following the Three Mile Island Unit 2 (TMI-2) accident, and comprises three major tasks: (1) conducting integral simulations of small-break loss-of-coolant accidents (SBLOCAs) and transients for a pressurized water reactor (PWR) using the Large Scale Test Facility (LSTF), (2) conducting separate effects tests using the Two-Phase Flow Test Facility (TPTF), and (3) developing and verifying an advanced thermal-hydraulics code for analyses of SBLOCAs and transients. The LSTF is a volumetrically scaled (1/48) Westinghouse-type PWR simulator with an electrically heated core⁽²⁾. The elevation of each component in the LSTF simulates that of the actual PWR as close as possible for better simulation of the natural circulation behavior during a SBLOCA or transient.

In LSTF tests, as the core electric power curve, the JAERI Power Curve had been used until Run SB-HL-03 conducted on October 21, 1987, except for three acceptance tests (Runs AT-SB-01, 02 and 03) and a Semi-scale counterpart test (Run SB-CL-06). The JAERI Power Curve, however, was estimated conservatively in calculating the delayed neutron fission power. The New Power Curve, therefore, was calculated on best-estimate base, particularly in the above point. The difference in stored heat between a nuclear fuel rod and a LSTF electrical heater rod was also taken into account in determining the New Power Curve. This report describes the calculation method and procedure of the New Power Curve and presents a final result obtained as the New Power Curve.

LSTF 5% and 10% cold-leg break LOCA tests, Run SB-CL-13 and Run SB-CL-14, respectively were performed by using the New Power Curve to investigate the effect of core power curve on thermal-hydraulic behavior in the primary system. The test conditions for Run SB-CL-13 and Run SB-CL-14 were the same as for Run SB-CL-08 and Run SB-CL-09, respectively, except for the core power curve: the JAERI Power Curve were used in Run SB-CL-08 and Run SB-CL-09. Test results of Run SB-CL-13 and Run SB-CL-14, and comparison with those of Run SB-CL-08 and Run SB-CL-09, respectively, are presented in References (3) and (4), respectively.

2. New Power Curve Calculation

As mentioned in the introduction, the JAERI Power Curve had been used in LSTF tests until Run SB-HL-03. The JAERI Power Curve, however, was estimated conservatively in calculating the delayed neutron fission power. The New Power Curve, therefore, was calculated on best-estimate base, particularly in calculation of the delayed neutron fission power. The difference in stored heat between a nuclear fuel rod and a LSTF electrical heater rod was also taken into account in the New Power Curve calculation.

2.1 Calculation Model and Method

(1) LSTF Calculation

The heat transfer from a LSTF electrical heater rod to core fluid was calculated with the RELAP5 / MOD2 code⁽⁵⁾ by using a simple calculation model. Figure 2.1 shows the model used in the LSTF core heat transfer calculation.

The core was modeled with the "single volume" (SV ①), simulating two subchannels in the LSTF core and having a length equal to 1/8 of the heated region of the LSTF core. Two heater rods, one average power rod with a total peaking factor of 1.0 and one peak power rod with a total peaking factor of 2.26 were modeled with the "heat structure" and were attached to the core volume. Figure 2.2 shows details of the LSTF heater rod. The core insulator (Al_2O_3), heating element (Nichrome), outer insulator (packed MgO) and cladding (Inconel 600) were divided into 3, 1, 1 and 3 mesh intervals, respectively. There is uncertainty in the thermal conductivity of the packed MgO. Table 2.1 presents thermal conductivities of the packed MgO from two data sources: values measured by a manufacturer at low temperatures (Case A) and a value used for design of the LSTF heater rod by a manufacturer (Case B). There is a significant difference in the thermal conductivity of the packed MgO between these two data, Case A and Case B. Therefore, these two data (two cases) were tested in calculating the heat transfer from a LSTF heater rod to core fluid (Refer to Section 2.4). The lengths of the modeled heater rods were 1/8 of the heated length of the LSTF heater rod, as was the case for the core volume.

The core inlet condition was modeled with two combinations of the

"time dependent volume" and "time dependent junction" (TV ③ and TJ12, and TV ④ and TJ13), and the "branch" (B ②) and the "junction of branch" (J). As a system pressure transient, two data of lower plenum pressure transient obtained in LSTF 5% and 0.5% break LOCA tests were tested in the heat transfer calculations (Refer to Section 2.4), and these data were given in TV ③ or TV ④. The pressure curves obtained from LSTF 5% (Run SB-CL-08) and 0.5% (Run SB-CL-11) break tests and used in the heat transfer calculations are presented in Fig. 2.3 and Table 2.2, and Fig. 2.4 and Table 2.3, respectively. Until the pressure decreases from 15.5 MPa (a pressure under normal operating condition) to 12.5 MPa, subcooled liquid is injected from the combination of TV ③ and TJ12 to the core (SV ①) through the branch B ②. The temperature of subcooled fluid is changed linearly from 565 K to 593 K during pressure decrease from 15.5 MPa to 12.5 MPa. After the pressure decreases below 12.5 MPa, two-phase mixture (nearly saturated liquid) with a quality of 1×10^{-10} is injected from the combination of TV ④ and TJ13 to the core (SV ①) in order to keep nucleate boiling condition in the core. The flow rate to the core (the core inlet flow rate) is kept at a constant value of 0.5917 kg/s, corresponding to the total flow rate for two subchannels under normal operating condition, throughout whole pressure transient. The switching from subcooled liquid flow to two-phase flow at the core inlet is done in order to prevent occurrence of DNB (departure from nucleate boiling) in the core at high pressures above 15.3 MPa corresponding to high core powers near to the power under normal operating condition.

The core outlet condition was modeled with the "single junction" (SJ14) and the "time dependent volume" (TV ⑤). The pressure in TV ⑤ is adjusted at a lower pressure than in TV ③ or TV ④ by 0.1 MPa at each time during a transient and the quality in TV ⑤ is kept at 1.0 throughout a transient.

An example of the input data for LSTF heat transfer calculation (Case POLS01; Refer to Section 2.4) is presented in Appendix C.

(2) PWR Calculation

The heat transfer from a nuclear fuel rod to core fluid was also calculated with the RELAP5/MOD2 code by using the same model used for the LSTF heat transfer calculation, i.e. Fig. 2.1, except for heat

structures. Two nuclear fuel rods, one average power rod with a total peaking factor of 1.0 and one peak power rod with a total peaking factor of 2.32 were modeled with the "heat structure". The fuel (UO_2), gap (He gas) and cladding (Zirconium) were divided into 5, 1 and 2 mesh intervals, respectively.

The input data for PWR heat transfer calculation (Case POPW01; Refer to Section 2.3) is presented in Appendix B.

2.2 PWR Core Power Calculation

The PWR core power was estimated by dividing into three power terms, i.e. the delayed neutron fission power term, the fission product decay power term and the actinide decay power term, which contribute much to the PWR core power after a reactor scram. (The sum of these three power terms occupy almost the whole part of the PWR core power after a reactor scram.) The major parameters and methods used for the PWR core power calculation for determining the New Power Curve are summarized in Table 2.4. For reference, those used for the PWR core power calculation for determining the JAERI Power Curve are summarized in Table 2.5.

(1) Delayed Neutron Fission Power

The delayed neutron fission power was calculated with the RELAP5/MOD2 code, i.e. by using the reactor kinetics model in the RELAP5/MOD2 code. The same model (noding) as used for the PWR heat transfer calculation, i.e. Fig. 2.1 (Refer to Subsection 2.1(2)), was also used in this calculation. The input data is also the same as used for the PWR heat transfer calculation, except a core power curve input was replaced with inputs for reactor kinetics calculation. The input data used for this calculation, i.e. the delayed neutron fission power calculation, (Case PWPO00) is presented in Appendix A. The major parameters used for this calculation are summarized in Table 2.4. The reactivity feedback was not considered in this calculation.

(2) Fission Product Decay Power

The fission product decay power was taken from data in the JNDC (Japanese Nuclear Data Committee) FP (Fission Product) Nuclear Data Library⁽⁶⁾. (The fission product decay power for determining the JAERI

Power Curve was also from data in the JNDC Nuclear Data Library.)

(3) Actinide Decay Power

The decay powers of ^{239}U and ^{239}Np produced by neutron capture in ^{238}U were calculated by the equations

$$F_{239\text{U}}(t, T) = E_{239\text{U}} R [1 - \exp(-\lambda_1 T)] \exp(-\lambda_1 t), \quad (1a)$$

$$F_{239\text{Np}}(t, T) = E_{239\text{Np}} R \left\{ \frac{\lambda_1}{\lambda_1 - \lambda_2} [1 - \exp(-\lambda_2 T)] \exp(-\lambda_2 t) - \frac{\lambda_2}{\lambda_1 - \lambda_2} [1 - \exp(-\lambda_1 T)] \exp(-\lambda_1 t) \right\}, \quad (1b)$$

respectively, where

- F : Power (MeV/sec) per 1 fission/sec
 $E_{239\text{U}}$: Energy yield from ^{239}U decay = 0.474 MeV
 $E_{239\text{Np}}$: Energy yield from ^{239}Np decay = 0.419 MeV
 R : ^{239}U yield factor (Number of ^{239}U atoms produced per fission)
 λ_1 : Decay constant of ^{239}U = $4.91 \times 10^{-4} \text{ sec}^{-1}$
 λ_2 : Decay constant of ^{239}Np = $3.41 \times 10^{-6} \text{ sec}^{-1}$
 t : Cooling time (Time after reactor scram) (sec)
 T : Irradiation time (Operating time before reactor scram) (sec)

In this calculation, the ^{239}U yield factor and the irradiation time were assumed to be 0.59 and infinitive, respectively.

Final calculated results for the three power terms and the sum of them for determining the New Power Curve are presented in normalized forms in Table 2.6. For reference, those for determining the JAERI Power Curve are presented in Table 2.7.

2.3 PWR Heat Transfer Calculation

The heat transfer from a PWR fuel rod to core fluid was calculated with the RELAP5/MOD2 code by using the model (noding) described in

Subsection 2.1(2). The input data for the PWR heat transfer calculation (Case POPW01) are presented in Appendix B. The PWR power curve, i.e. the sum of the three power terms, obtained in Section 2.2 was given as a core power curve input in this calculation. Calculation cases of heat transfer calculations including the LSTF heat transfer calculation are summarized in Table 2.8.

2.4 LSTF Heat Transfer Calculation

The heat transfer from a LSTF heater rod to core fluid was also calculated with the RELAP5/MOD2 code by using the model (noding) described in Subsection 2.1(1). An example of the input data for LSTF heat transfer calculation (Case POLS01) is presented in Appendix C. Calculation cases of the LSTF heat transfer calculation are summarized in Table 2.8.

The purpose of the LSTF heat transfer calculation is to obtain a LSTF core power curve which gives the LSTF heat transfer (the heat transfer from a LSTF heater rod to core fluid) being in best agreement with the PWR heat transfer (the heat transfer from a PWR fuel rod to core fluid) calculated in Section 2.3 (i.e. in Case POPW01).

(1) Uncertainty in Thermal Conductivity of Packed MgO

As mentioned in Subsection 2.1(1), there is uncertainty in the thermal conductivity of the packed MgO, the outer insulator in the LSTF heater rod: there is a significant difference in the thermal conductivity of the packed MgO between two data, i.e. data measured by a manufacturer at low temperatures (Case A) and data used for design of the LSTF heater rod by a manufacturer (Case B), as shown in Table 2.1. Therefore, also as mentioned in Subsection 2.1(1), these two data (Case A and Case B) were tested in the LSTF heat transfer calculation.

Figure 2.5 compares the PWR heat transfer rate from the average power rod in Case POPW01 and the LSTF heat transfer rates from the average power rod in Case POLS01 and Case POLS02. In Case POLS01 and Case POLS02, the data measured at low temperatures (i.e. Case A in Table 2.1, ~ 4 W/mK) and the data used for design of the LSTF heater rod (i.e. Case B in Table 2.1, ~ 1 W/mK), respectively, were given as the input for the thermal conductivity of packed MgO. The PWR core power calculated

in Section 2.2, i.e. the core power presented in Table 2.6, was given as the input for the core power curve in both Case POLS01 and Case POLS02. It is considered that the stored heat in the LSTF heater rod is smaller than that in the PWR fuel rod, and therefore the LSTF heat transfer rate is smaller than the PWR heat transfer rate if the same core power, i.e. the PWR core power, is given as the input for the core power curve. Hence, the thermal conductivity of packed MgO of ~ 1 W/mK (i.e. Case B in Table 2.1) is less reliable than ~ 4 W/mK (i.e. Case A in Table 2.1).

Oscillation of the heat transfer rate is seen in all of the three calculations, Cases POPW01, POLS01 and POLS02, after approximately 500s. The reason may be that two-phase mixture with a constant flow rate and a constant quality is injected from the combination of time dependent volume and time dependent junction to the core not directly but through a branch component, as mentioned in Subsection 2.1(1). The oscillation of the heat transfer rate is seen in all of the calculations presented in this report.

Figure 2.6 shows the PWR heat transfer rate from the average power rod in Case POPW01 and the LSTF heat transfer rates from the average power rod in Case POLS11 and Case POLS12, together with the LSTF heat transfer rates in Case POLS01 and Case POLS02. In Case POLS11 and Case POLS12, the data measured at low temperatures (~ 4 W/mK) and the data used for design of the LSTF heater rod (~ 1 W/mK), respectively, were given as the input for the thermal conductivity of packed MgO. The PWR heat transfer rate from the average power rod (named "on average power rod base" in this report) calculated in Section 2.3(, i.e. in Case POPW01,) was given as the input for the core power curve in both Case POLS11 and Case POLS12. The LSTF heat transfer rates in both Case POLS11 and POLS12 are larger than the PWR heat transfer rate in Case POPW01 as expected, since there is the stored heat in the LSTF heater rod.

The final goal of the LSTF heat transfer calculation is to obtain a LSTF core power curve which gives the LSTF heat transfer rate being in best agreement with the PWR heat transfer rate in Case POPW01. However, there is uncertainty in the thermal conductivity of packed MgO, as mentioned previously. Therefore, the Case POLS11 calculation was selected as the final goal calculation: the PWR heat transfer rate on average power rod base was adopted as the LSTF core power curve, i.e. the

New Power Curve, since the LSTF heat transfer rate in Case POLS11 gives a little conservative curve comparing with the PWR heat transfer rate in Case POPW01.

(2) Average Power Rod and Peak Power Rod

Figure 2.7 compares the PWR heat transfer rate from the average power rod in Case POPW01 and the LSTF heat transfer rates from the average power rod in Case POLS11 and Case POLS21. In Case POLS21, the data measured at low temperatures (~ 4 W/mK) was given as the input for the thermal conductivity of packed MgO, as in the case of Case POLS11. The PWR heat transfer rate from the peak power rod (named "on peak power rod base" in this report) calculated in Section 2.3 was given as the input for the core power curve in Case POLS21, whereas the PWR heat transfer rate from the average power rod (named "on average power rod base"), i.e. the New Power Curve, was given as the input for the core power curve in Case POLS11. In all of the LSTF heat transfer calculations, the initial total core power was the same, and the normalized PWR heat transfer rate on peak power rod base or average power rod base (normalized by each initial PWR heat transfer rate) was given as the input for the core power curve. The normalized PWR heat transfer rates on peak power rod base and average power rod base differ a little from each other, since the stored heats in the PWR peak power rod and PWR average power rod differ a little from each other due to a difference in the initial temperatures between the two rods. As shown in Fig. 2.7, while the LSTF heat transfer rate from the average power rod in Case POLS21 is a little larger than that in Case POLS11 as expected, there is almost no significant difference in the LSTF heat transfer rate from the average power rod between Case POLS21 and Case POLS11.

Figure 2.8 compares the PWR heat transfer rate from the peak power rod in Case POPW01 and the LSTF heat transfer rates from the peak power rod in Case POLS11 and Case POLS21. As shown in this figure, there is also almost no significant difference in the LSTF heat transfer rate from the peak power rod between Case POLS21 and Case POLS11.

(3) Break Area

As mentioned in Subsection 2.1(1), in order to investigate the effect of system pressure transient on the LSTF heat transfer, two

pressure transient data obtained in LSTF 5% and 0.5% break LOCA tests, shown in Fig. 2.3 and Table 2.2, and Fig. 2.4 and Table 2.3, respectively, were tested in the LSTF heat transfer calculation. Figure 2.9 compares the PWR heat transfer rate from the average power rod in Case POPW01 and the LSTF heat transfer rates from the average power rod in Case POLS11 and Case POLS32, together with the LSTF heat transfer rates in Case POLS01 and Case POLS31. The data measured at low temperatures (~ 4 W/mK) were given as the input for the thermal conductivity of packed MgO in Case POLS31 and Case POLS32, as in the cases of Case POLS01 and Case POLS11. The PWR heat transfer rate on average power rod base, i.e. the New Power Curve, was given as the input for the core power curve in Case POLS32 as in the case of Case POLS11, while the PWR core power was given as the input for the core power curve in Case POLS31 as in the case of Case POLS01. The pressure transient data obtained in a LSTF 0.5% break LOCA test were given as the input for the core inlet condition in Case POLS31 and Case POLS32, though the pressure transient data obtained in a LSTF 5% break LOCA test were used as the input for the core inlet condition in Case POLS01 and Case POLS11. Except for Case POLS31 and Case POLS32, the pressure transient data obtained in a LSTF 5% break LOCA test were given as the input for the core inlet condition in all of the LSTF heat transfer calculations presented in this section (, i.e. Section 2.4,) and also in the PWR delayed neutron fission power calculation described in Subsection 2.2(1).

It is obvious from comparing the LSTF heat transfer rates in Case POLS11 and Case POLS32 shown in Fig. 2.9 that there is almost no significant difference in the LSTF heat transfer rate between Case POLS11 and Case POLS32: the LSTF heat transfer rate is not affected very much by a difference in the pressure transient, i.e. the break area.

(4) BN Outer Insulator

In the LSTF heater rods in the present LSTF fuel assembly (named the "LSTF first fuel assembly"), packed MgO is used as the outer insulator. Packed BN (Boron-Nitride) will be used as the outer insulator in LSTF heater rods in a next LSTF fuel assembly (named the "LSTF second fuel assembly"). The geometries and materials used are the same between the LSTF heater rods in the LSTF first fuel assembly and in the LSTF second fuel assembly, except packed MgO in the outer insulator is replaced

by packed BN. The LSTF first fuel assembly will be replaced by the LSTF second fuel assembly in March, 1989. A difference in the LSTF heat transfer between the LSTF heater rod in the LSTF first fuel assembly (packed MgO outer insulator) and that in the LSTF second fuel assembly (packed BN outer insulator) will be examined in this subsection.

Figure 2.10 shows the PWR heat transfer rate from the average power rod in Case POPW01 and the LSTF heat transfer rates from the average power rod in Case POLS01 and Case POLS81, together with the LSTF heat transfer rate in Case POLS02. In Case POLS81, data for the packed BN were given as the input for physical properties of the outer insulator, and the PWR core power was given as the input for the core power curve as in the cases of Case POLS01 and Case POLS02.

Figure 2.11 compares the PWR heat transfer rate from the average power rod in Case POPW01 and the LSTF heat transfer rates from the average power rod in Case POLS11 and Case POLS82, together with the LSTF heat transfer rate in Case POLS12. In Case POLS82, data for the packed BN were given as the input for physical properties of the outer insulator, and the PWR heat transfer rate on average power rod base, i.e. the New Power Curve, was given as the input for the core power curve as in the cases of Case POLS11 and Case POLS12.

It is seen from comparing the PWR heat transfer rate in Case POPW01 and the LSTF heat transfer rates in Case POLS11 and Case POLS82 shown in Fig. 2.11 that while the LSTF heat transfer rate in Case POLS82 (the LSTF heater rod in the LSTF second fuel assembly) is a little smaller than the LSTF heat transfer rate in Case POLS11 (the LSTF heater rod in the LSTF first fuel assembly), the LSTF heat transfer rate in Case POLS82 gives a little conservative curve comparing with the PWR heat transfer rate in Case POPW01. This means that the LSTF heat transfer rate from the heater rod in the LSTF second fuel assembly is a little conservative comparing with the PWR heat transfer rate and is also in approximately agreement with the LSTF heat transfer rate from the heater rod in the LSTF first fuel assembly, if the New Power Curve is used as the core power curve.

(5) JAERI Power Curve

A difference between the PWR heat transfer rate and the LSTF heat transfer rate in the case where the JAERI Power Curve is used as the core

power curve is examined in this subsection. Figure 2.12 compares the PWR heat transfer rate from the average power rod in Case POPW01 and the LSTF heat transfer rate from the average power rod in Case POLS91, together with the LSTF heat transfer rates in Case POLS01, Case POLS02 and Case POLS92. The data measured at low temperature (~ 4 W/mK) were given as the input for the thermal conductivity of packed MgO in Case POLS91 as in the case of Case POLS01, while the data used for design of the LSTF heater rod (~ 1 W/mK) were used as the input for the thermal conductivity of packed MgO in Case POLS92 as in the case of Case POLS02. The JAERI Power Curve was given as the input for the core power curve in Case POLS91 and Case POLS92. It is seen from comparing the PWR heat transfer rate in Case POPW01 and the LSTF heat transfer rate in Case POLS91 shown in Fig. 2.12 that the LSTF heat transfer rate in the case where the JAERI Power Curve is used as the core power curve is considerably lower until approximately 15s and considerably larger between approximately 15s and 400s than the PWR heat transfer rate. The reason of this disagreement may be that the PWR delayed neutron fission power was estimated approximately using one delayed neutron group in determining the JAERI Power Curve.

As mentioned in Subsection 2.4(1), finally, the PWR heat transfer rate on average power rod base was selected as the New Power Curve. The PWR power, the New Power Curve and the JAERI Power Curve are compared in Fig. 2.13. In a LSTF LOCA test, the LSTF core power is kept at 10 MW for approximately 18s and 29s after a reactor scram due to limitation of electric power supply, when the New Power Curve and JAERI Power Curve are used as the LSTF core power, respectively. Digital values of the New Power Curve and JAERI Power Curve are presented in Tables 2.9 and 2.10, respectively. As shown in Fig. 2.13, the New Power Curve used in a LSTF test is considerably lower between approximately 20s and 300s and a little higher after approximately 300s than the JAERI Power Curve used in a LSTF test. The reason of this discrepancy may be that the PWR delayed neutron fission power was estimated using 6 delayed neutron groups and the stored heat in a PWR fuel rod was considered in determining the New Power Curve, though the former was estimated approximately using 1 delayed neutron group and the latter was not considered in determining the JAERI Power Curve.

The times in Tables 2.2 and 2.3 and Figs. 2.3 and 2.4 are the time after a break, and the times in the other tables (i.e. Tables 2.6, 2.7, 2.9 and 2.10) and in the other figures (i.e. Figs. 2.5 through 2.13) are the time after a reactor scram.

3. Concluding Remarks

The New Power Curve for LSTF tests was calculated on best-estimate base, particularly in two points, i.e. estimation of the delayed neutron fission power and consideration of the stored heat in a PWR fuel rod. Finally, the PWR heat transfer rate on average power rod base was adopted as the New Power Curve, neglecting the stored heat in a LSTF heater rod since there is uncertainty in the thermal conductivity of outer insulator in the LSTF heater rod. When the New Power Curve is used as the LSTF core power curve, the LSTF heat transfer rate gives a little conservative values comparing with the PWR heat transfer rate.

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Table 2.1 Thermal Conductivity of MgO

(a) Case A; Values measured by manufacturer at low temperatures, ~ 4 W/mK

Temperature (K)	Thermal Conductivity (W/mK)
334.15	1.3142
443.15	2.3493
554.15	3.9309
3473.15*	3.9309*

* Extrapolation of measured value at 554.15K

(b) Case B; Value used for design of heater rod by manufacturer, ~ 1 W/mK

Temperature (K)	Thermal Conductivity (W/mK)
273.15	1.1049
3473.15	1.1049

Table 2.2 Pressure Curve for 5% Break (SB-CL-08)
used in Calculations

	Time (s)	Pressure (MPa)
1	0.0	15.50
2	(15.3)	(12.50)
3	25.0	10.60
4	60.0	9.25
5	77.0	8.95
6	124.0	8.45
7	148.0	8.40
8	167.0	8.15
9	207.0	7.75
10	239.0	7.25
11	400.0	5.10
12	486.0	3.95
13	549.0	3.30
14	557.0	3.05
15	582.0	2.60
16	609.0	2.40
17	627.0	2.30
18	774.0	2.20
19	810.0	2.05
20	910.0	2.00
21	938.0	1.85
22	969.0	1.65
23	1000.0	1.55

Table 2.3 Pressure Curve for 0.5% Break (SB-CL-11)
used in Calculations

	Time (s)	Pressure (MPa)
1	0.0	15.50
2	20.0	14.25
3	90.0	12.70
4	130.0	13.50
5	(167.5)	(12.50)
6	190.0	11.90
7	390.0	8.75
8	430.0	8.45
9	520.0	8.30
10	2600.0	8.00

Table 2.4 PWR Power Curve Calculation for
Determining New Power Curve

1. Delayed Neutron Fission Power
 - Used Code : RELAP5/MOD2 (Point Reactor Kinetics Model)
 - 6 Delayed Neutron Groups
 - Control Rod Worth : -4%
 - Control Rod Drop Time : 3s
 - Delayed Neutron Fraction : 0.75%

2. Fission Product Decay Power
 - JNDC (Japanese Nuclear Data Committee), Ref. (6)

3. Actinide Decay Power
 - Eq. (1)
 - Energy Yield from U^{239} Decay : 0.474 MeV
 - Energy Yield from Np^{239} Decay : 0.419 MeV
 - Decay Constant of U^{239} : $4.91 \times 10^{-4} \text{ s}^{-1}$
 - Decay Constant of Np^{239} : $3.41 \times 10^{-6} \text{ s}^{-1}$
 - U^{239} Production Factor : 0.59

Table 2.5 PWR Power Curve Calculation for
Determining JAERI Power Curve

1. Delayed Neutron Fission Power
 - Used Code : — (Hand Calculation)
 - 1 Delayed Neutron Group with Average Neutron Life Time of 80s
 - Control Rod Worth : -4%
 - Control Rod Drop Time : 3s
 - Delayed Neutron Fraction : 0.7%

2. Fission Product Decay Power
 - JNDC (Japanese Nuclear Data Committee), Ref. (6)

3. Actinide Decay Power
 - Eq. (1)
 - Energy Yield from U^{239} Decay : 0.474 MeV
 - Energy Yield from Np^{239} Decay : 0.419 MeV
 - Decay Constant of U^{239} : $4.91 \times 10^{-4} \text{ s}^{-1}$
 - Decay Constant of Np^{239} : $3.41 \times 10^{-6} \text{ s}^{-1}$
 - U^{239} Production Factor : 0.59

Table 2.6 Normalized Delayed Neutron Fission Power, and Fission Product and Actinide Decay Powers for determining New Power Curve

Time (s)	DN Fission Power	FP Decay Power	Actinides Decay Power	Total
0	0.933498	0.0639013	2.60028×10^{-3}	1.00000
1	0.813366	0.0590464	2.59960×10^{-3}	0.875012
1.5	0.636461	0.0573887	2.59926×10^{-3}	0.696449
2	0.361606	0.0559959	2.59892×10^{-3}	0.420201
3	0.107936	0.0537360	2.59825×10^{-3}	0.164270
4	0.0924713	0.0519435	2.59757×10^{-3}	0.147012
5	0.0814024	0.0504658	2.59689×10^{-3}	0.134465
6	0.0727933	0.0492146	2.59621×10^{-3}	0.124604
8	0.0601687	0.0471896	2.59487×10^{-3}	0.109953
10	0.0514425	0.0455997	2.59352×10^{-3}	0.0996357
15	0.0382506	0.0427264	2.59015×10^{-3}	0.0835672
20	0.0306565	0.0407292	2.58679×10^{-3}	0.0739725
30	0.0216180	0.0379898	2.58010×10^{-3}	0.0621879
40	0.0161113	0.0360901	2.57343×10^{-3}	0.0547748
50	0.0123328	0.0346322	2.56680×10^{-3}	0.0495318
60	9.59011×10^{-3}	0.0334497	2.56020×10^{-3}	0.0456000
80	5.98466×10^{-3}	0.0316091	2.54711×10^{-3}	0.0401409
100	3.86642×10^{-3}	0.0302191	2.53413×10^{-3}	0.0366196
150	1.48610×10^{-3}	0.0278325	2.50226×10^{-3}	0.0318209
200	6.66549×10^{-4}	0.0262741	2.47114×10^{-3}	0.0294117
300	1.68548×10^{-4}	0.0242586	2.41115×10^{-3}	0.0268382
400	4.68085×10^{-5}	0.0229210	2.35401×10^{-3}	0.0253218
500	1.32219×10^{-5}	0.0219114	2.29959×10^{-3}	0.0242242
600	3.74563×10^{-6}	0.0210933	2.24775×10^{-3}	0.0233447
800	3.00913×10^{-7}	0.0198010	2.15136×10^{-3}	0.0219527
1000	$\sim 3.7 \times 10^{-8}$	0.0187908	2.06390×10^{-3}	0.0208547
1500		0.0169359	1.87907×10^{-3}	0.0188150
2000		0.0156228	1.73402×10^{-3}	0.0173568
3000		0.0138385	1.53053×10^{-3}	0.0153690
4000		0.0126595	1.40439×10^{-3}	0.0140639
5000		0.0118064	1.32560×10^{-3}	0.0131320
6000		0.0111501	1.27579×10^{-3}	0.0124259
8000		0.0101867	1.22253×10^{-3}	0.0114092
1×10^4		9.49787×10^{-3}	1.19751×10^{-3}	0.0106954
2×10^4		7.67865×10^{-3}	1.14767×10^{-3}	8.82632×10^{-3}
5×10^4		5.85228×10^{-3}	1.03600×10^{-3}	6.88828×10^{-3}

Table 2.6 (Continued)

Time (s)	DN Fission Power	FP Decay Power	Actinides Decay Power	Total
1×10^5		4.80086×10^{-3}	8.73605×10^{-4}	5.67446×10^{-3}
2×10^5		4.02849×10^{-3}	6.21182×10^{-4}	4.64967×10^{-3}
5×10^5		3.26068×10^{-3}	2.23323×10^{-4}	3.48400×10^{-3}
1×10^6		2.70896×10^{-3}	4.05942×10^{-5}	2.74955×10^{-3}
2×10^6		2.17399×10^{-3}	1.34128×10^{-6}	2.17533×10^{-3}
5×10^6		1.56445×10^{-3}	4.83824×10^{-11}	1.56445×10^{-3}
1×10^7		1.20688×10^{-3}	1.90530×10^{-18}	1.20688×10^{-3}
2×10^7		9.11667×10^{-4}		9.11667×10^{-4}
5×10^7		6.85618×10^{-4}		6.85618×10^{-4}
1×10^8		5.86748×10^{-4}		5.86748×10^{-4}
2×10^8		5.22337×10^{-4}		5.22337×10^{-4}
5×10^8		4.19465×10^{-4}		4.19465×10^{-4}
1×10^9		2.96290×10^{-4}		2.96290×10^{-4}
1×10^{10}		2.79366×10^{-5}		2.79366×10^{-5}
1×10^{11}		2.72816×10^{-5}		2.72816×10^{-5}
1×10^{12}		2.44637×10^{-5}		2.44637×10^{-5}
1×10^{13}		9.90464×10^{-6}		9.90464×10^{-6}

Table 2.7 Normalized Delayed Neutron Fission Power,
and Fission Product and Actinide Decay
Powers for determining JAERI Power Curve

Time (s)	DN Fission Power	FP Decay Power	Actinide Decay Power	Total
0	0.9333	0.064	0.00270	1.0
1	0.8129	0.059	0.00270	0.874
1.5	0.6505	0.058	0.00270	0.710
2	0.3845	0.056	0.00270	0.441
3	0.1391	0.054	0.00270	0.193
4	0.1391	0.052	0.00270	0.191
5				
6	0.1335	0.050	0.00270	0.183
8	0.1307	0.048	0.00270	0.179
10	0.1269	0.046	0.00263	0.173
15	0.1195	0.043		0.163
20	0.1120	0.041	0.00262	0.153
30				
40	0.08773	0.037	0.00261	0.125
50				
60	0.06813	0.034	0.00259	0.103
80	0.05320	0.032	0.00258	0.086
100	0.04107	0.031	0.00257	0.073
150	0.02240	0.028		0.051
200	0.01213	0.027	0.00250	0.040
300				
400	9.333×10^{-4}	0.023		0.025
500			0.00233	
600	~0	0.021		0.022
800		0.020		0.021
1000		0.019	0.00209	0.020
1500		0.017		0.018
2000		0.016	0.00176	0.017
3000				
4000		0.013		0.014
5000			0.00134	
6000		0.011		0.012
8000		0.010		0.011
1×10^4		0.010	0.00121	0.011
2×10^4		0.0077	0.00116	0.0083
5×10^4		0.0059	0.00105	0.0065

Table 2.7 (Continued)

Time (s)	DN Fission Power	FP Decay Power	Actinide Decay Power	Total
1×10^5		0.0048	0.000885	0.0053
2×10^5				
5×10^5				
1×10^6				
2×10^6				
5×10^6				
1×10^7				
2×10^7				
5×10^7				
1×10^8				
2×10^8				
5×10^8				
1×10^9				
1×10^{10}				
1×10^{11}				
1×10^{12}				
1×10^{13}				

Table 2.8 Cases of Heat Transfer Calculations

Case	Contents
POPW01	PWR Case
POLS01	Power = Power of PWR Case $\lambda(\text{MgO}) \Rightarrow 4 \text{ W/m}^2\text{K}$ 5% Break
POLS02	Power = Power of PWR Case $\lambda(\text{MgO}) \Rightarrow 1 \text{ W/m}^2\text{K}$ 5% Break
POLS11	Power = Heat Transfer Rate of PWR Case $\lambda(\text{MgO}) \Rightarrow 4 \text{ W/m}^2\text{K}$ 5% Break
POLS12	Power = Heat Transfer Rate of PWR Case $\lambda(\text{MgO}) \Rightarrow 1 \text{ W/m}^2\text{K}$ 5% Break
POLS21	Power = Heat Transfer Rate of PWR Case (Peak Power Rod Base) $\lambda(\text{MgO}) \Rightarrow 4 \text{ W/m}^2\text{K}$ 5% Break
POLS22	Power = Heat Transfer Rate of PWR Case (Peak Power Rod Base) $\lambda(\text{MgO}) \Rightarrow 1 \text{ W/m}^2\text{K}$ 5% Break
POLS31	Power = Power of PWR Case $\lambda(\text{MgO}) \Rightarrow 4 \text{ W/m}^2\text{K}$ 0.5% Break
POLS32	Power = Heat Transfer Rate of PWR Case $\lambda(\text{MgO}) \Rightarrow 4 \text{ W/m}^2\text{K}$ 0.5% Break
POLS81	Power = Power of PWR Case Outer Insulator = BN 5% Break
POLS82	Power = Heat Transfer Rate of PWR Case Outer Insulator = BN 5% Break
POLS91	Power = JAERI Power Curve $\lambda(\text{MgO}) \Rightarrow 4 \text{ W/m}^2\text{K}$ 5% Break
POLS92	Power = JAERI Power Curve $\lambda(\text{MgO}) \Rightarrow 1 \text{ W/m}^2\text{K}$ 5% Break

Table 2.9 New Power Curve

Time (s)	Power (MW)	Normalized Power (-)	Power used in Test (MW)
0	71.313	1.0	10.000
1	70.324	0.98614	10.000
1.5	68.688	0.96320	10.000
2	65.300	0.91568	10.000
3	56.428	0.79128	10.000
4	48.645	0.68214	10.000
5	42.614	0.59757	10.000
6	37.472	0.52546	10.000
8	29.133	0.40853	10.000
10	22.820	0.32000	10.000
15	12.503	0.17533	10.000
17.87			10.000
20	8.1497	0.11428	8.1497
30	5.3662	0.075249	5.3662
40	4.5044	0.063164	4.5044
50	3.9056	0.054767	3.9056
60	3.5384	0.049619	3.5384
80	3.0425	0.042664	3.0425
100	2.7633	0.038749	2.7633
150	2.4228	0.033974	2.4228
200	2.2631	0.031735	2.2631
300	2.0795	0.029160	2.0795
400	2.0000	0.028045	2.0000
500	1.9127	0.026821	1.9127
600	1.8317	0.025685	1.8317
800	1.5768	0.022111	1.5768
1000	1.4872	0.020855	1.4872
1500	1.3417	0.018815	1.3417
2000	1.2378	0.017357	1.2378
3000	1.0960	0.015369	1.0960
4000	1.0029	0.014064	1.0029
5000	0.93648	0.013132	0.93648
6000	0.88612	0.012426	0.88612
8000	0.81362	0.011409	0.81362
1×10^4	0.76272	0.010695	0.76272
2×10^4	0.62943	8.8263×10^{-3}	0.62943
5×10^4	0.49122	6.8883×10^{-3}	0.49122
1×10^5	0.40466	5.6745×10^{-3}	0.40466

Table 2.10 JAERI Power Curve

Time (s)	Power (MW)	Normalized Power (-)	Power used in Test (MW)
0	71.313	1.0	10.000
1	62.327	0.874	10.000
1.5	50.632	0.710	10.000
2	31.449	0.441	10.000
3	13.763	0.193	10.000
4	13.621	0.191	10.000
5			
6	13.050	0.183	10.000
8	12.765	0.179	10.000
10	12.337	0.173	10.000
15	11.624	0.163	10.000
20	10.911	0.153	10.000
29.12			10.000
30			
40	8.9141	0.125	8.9141
50			
60	7.3452	0.103	7.3452
80	6.1329	0.086	6.1329
100	5.2058	0.073	5.2058
150	3.6369	0.051	3.6369
200	2.8525	0.040	2.8525
300			
400	1.7828	0.025	1.7828
500			
600	1.5689	0.022	1.5689
800	1.4976	0.021	1.4976
1000	1.4263	0.020	1.4263
1500	1.2836	0.018	1.2836
2000	1.2123	0.017	1.2123
3000			
4000	0.99838	0.014	0.99838
5000			
6000	0.85575	0.012	0.85575
8000	0.78444	0.011	0.78444
1×10 ⁴	0.78444	0.011	0.78444
2×10 ⁴	0.59189	0.0083	0.59189
5×10 ⁴	0.46353	0.0065	0.46353
1×10 ⁵	0.37796	0.0053	0.37796

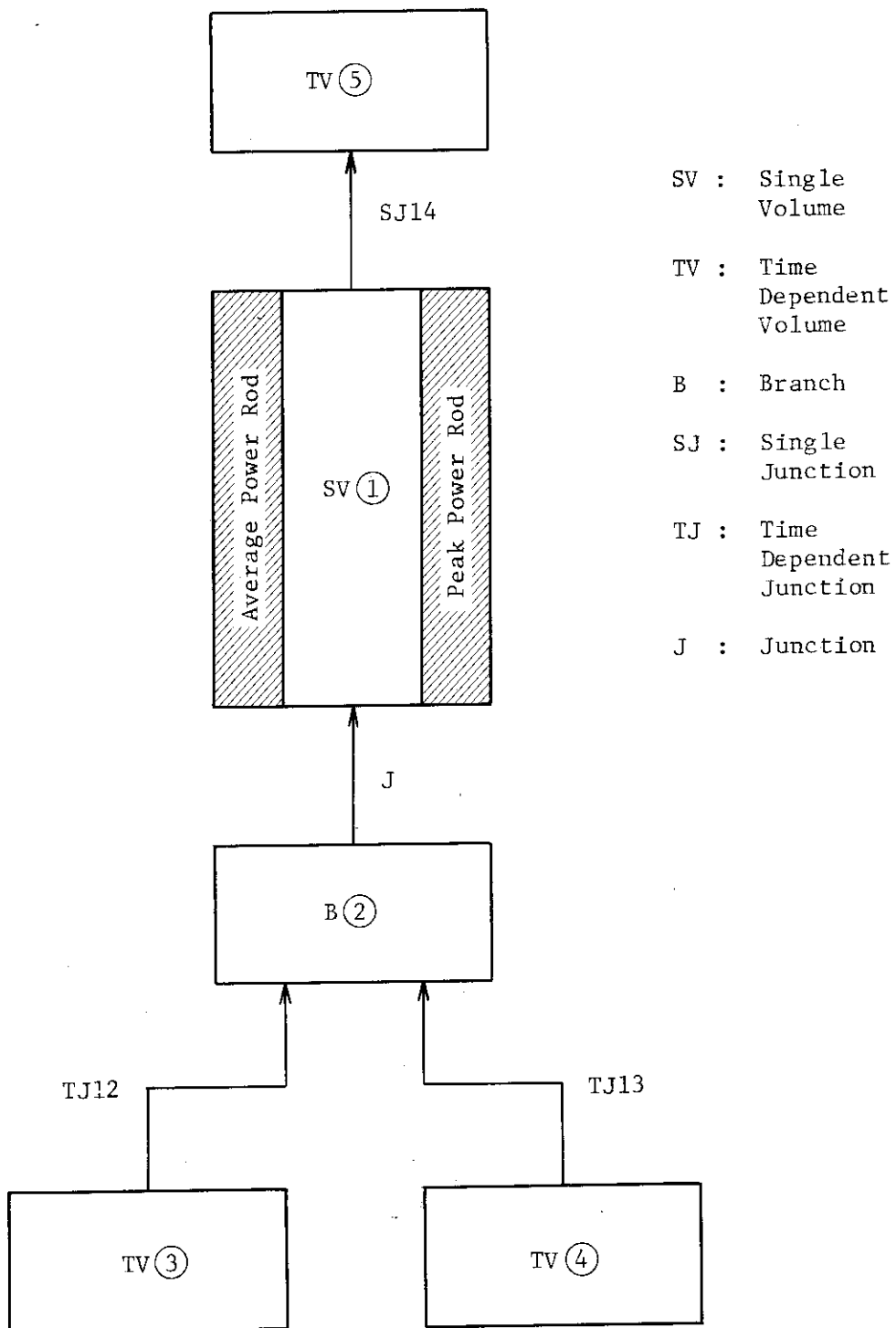


Fig. 2.1 Model used in LSTF and PWR Core Heat Transfer Calculations

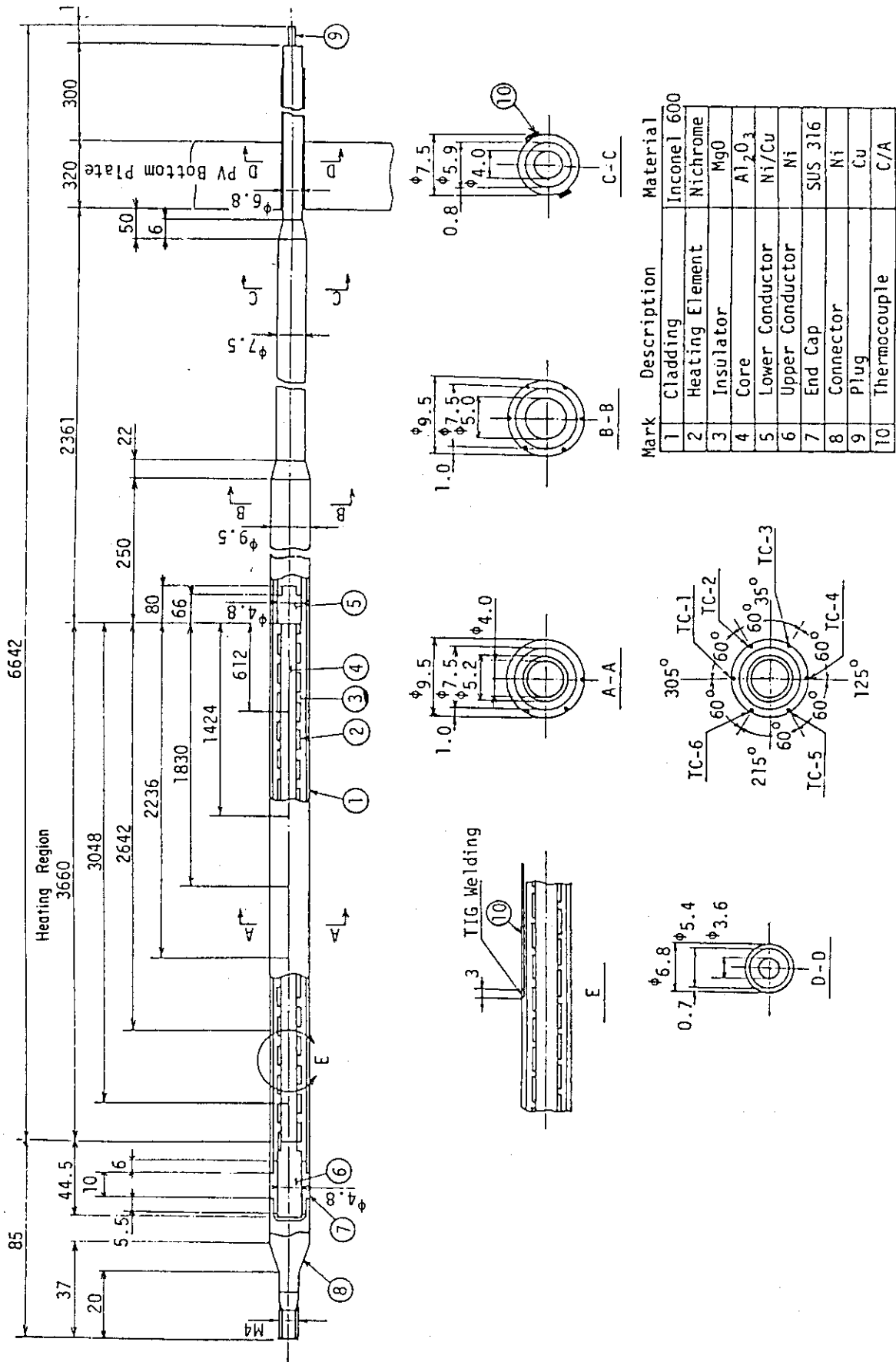


Fig. 2.2 LSTF Heater Rod

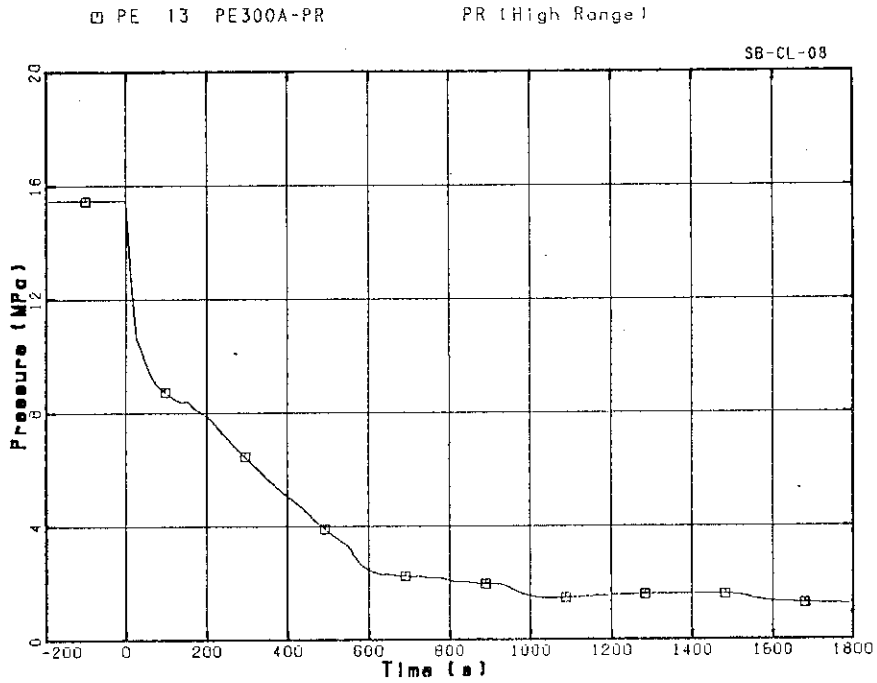


Fig. 2.3 Pressure Curve for 5% Break (SB-CL-08) used in Calculations

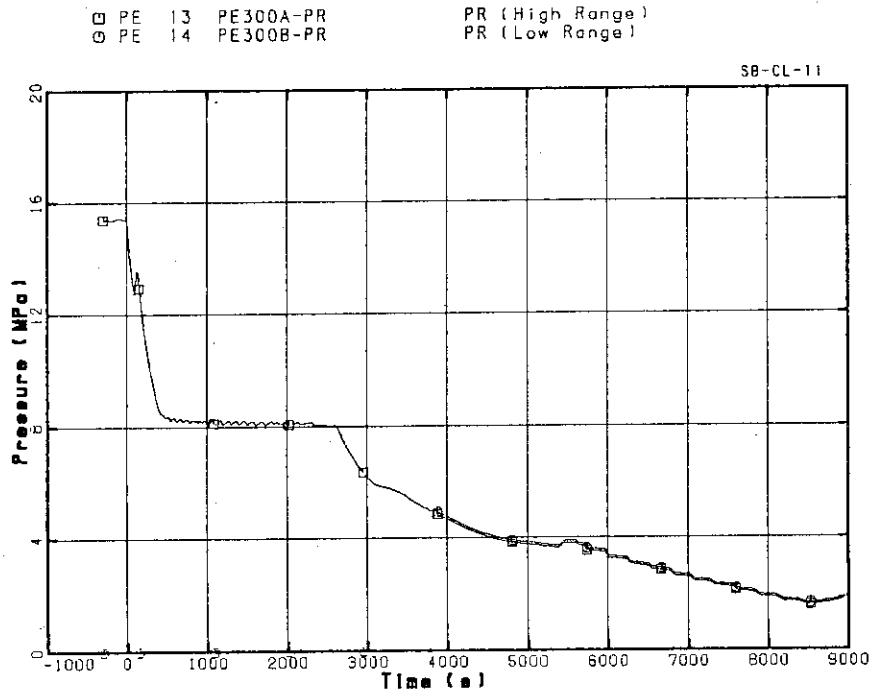


Fig. 2.4 Pressure Curve for 0.5% Break (SB-CL-11) used in Calculations

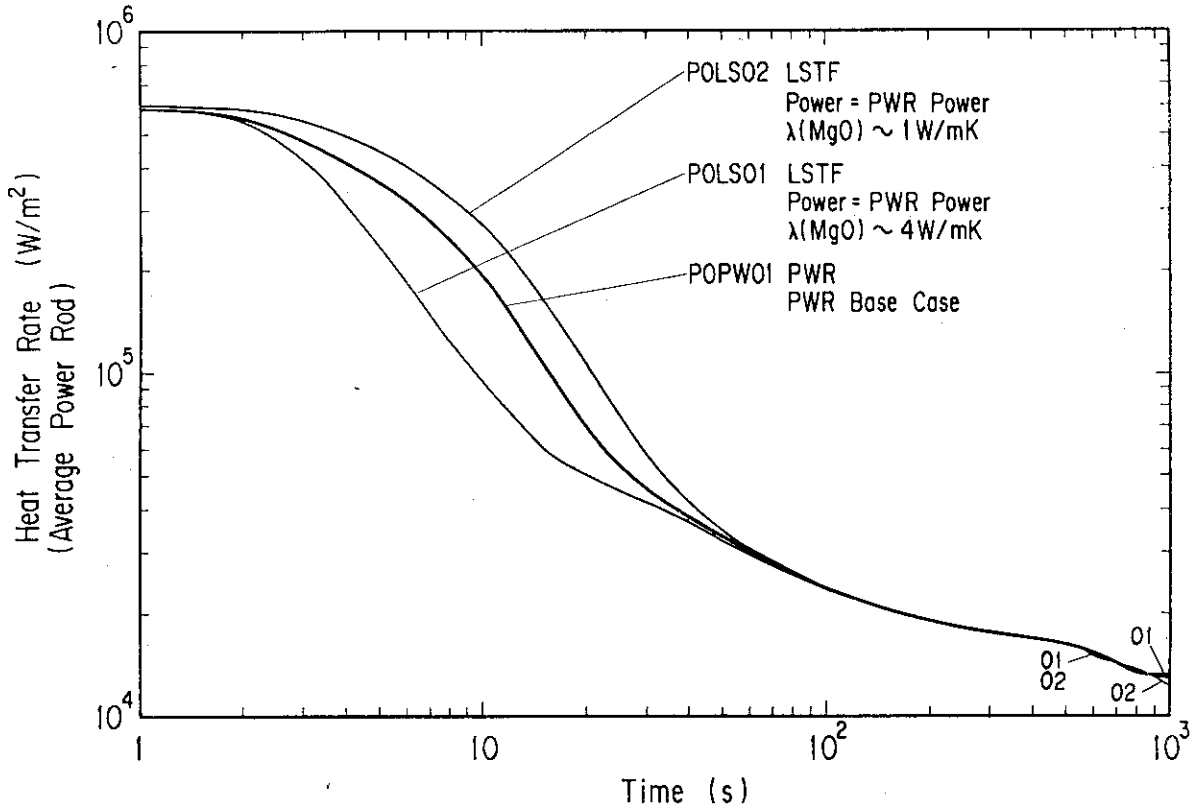


Fig. 2.5 Comparison of Heat Transfer Rates in Case POPW01 and Cases POLS01 and POLS02

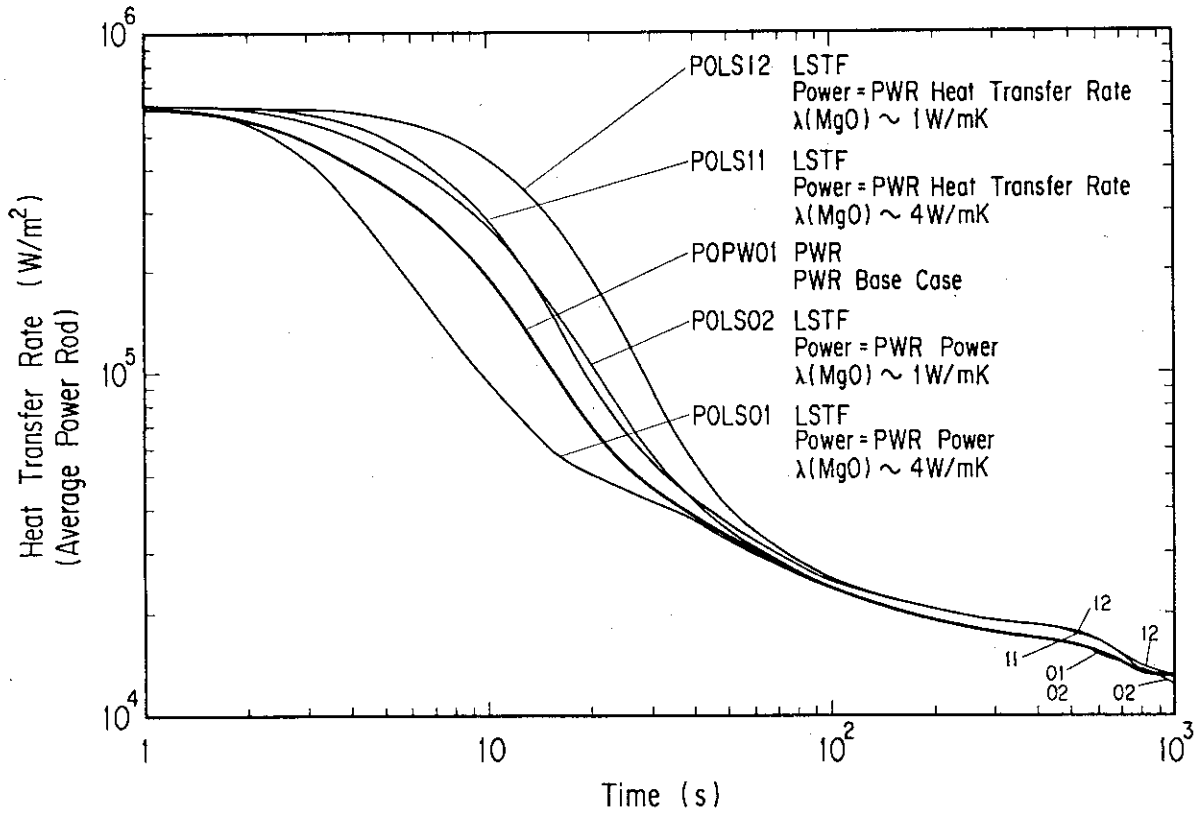


Fig. 2.6 Comparison of Heat Transfer Rates in Case POPW01 and Cases POLS11 and POLS12

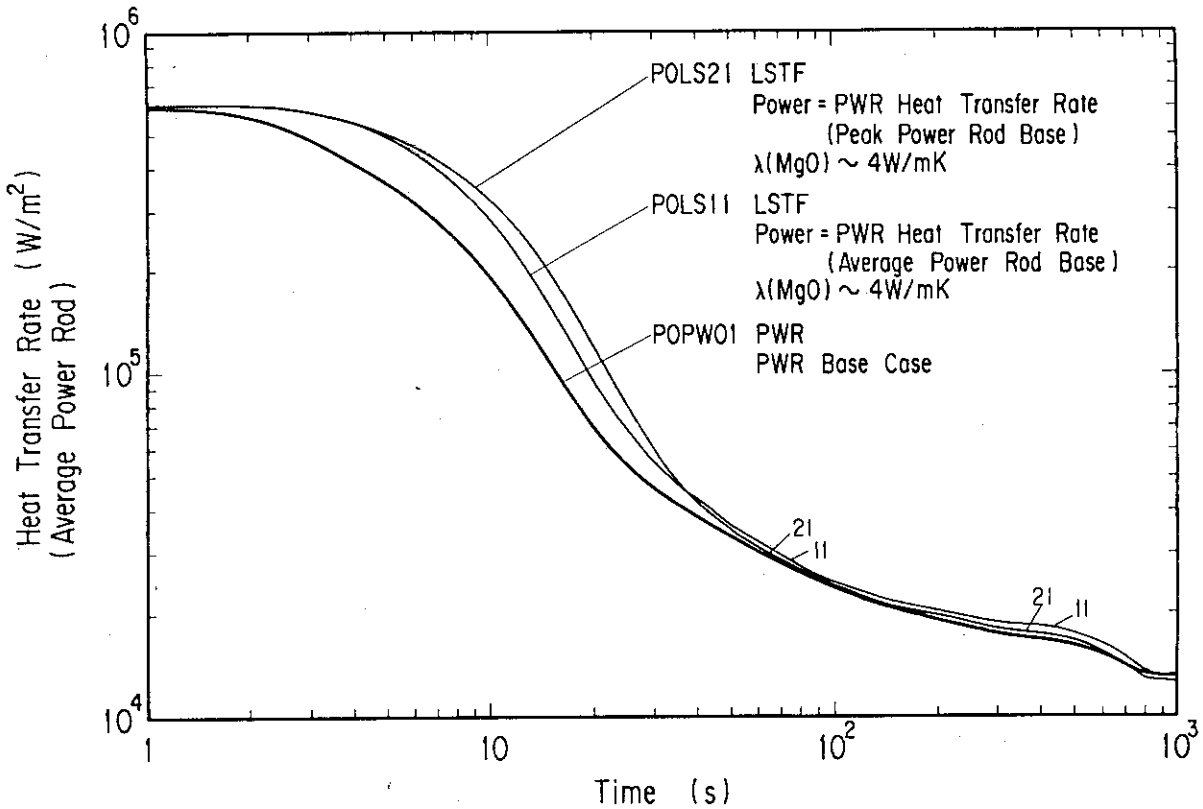


Fig. 2.7 Comparison of Heat Transfer Rates in Case POPW01 and Cases POLS11 and POLS21; Average Power Rod

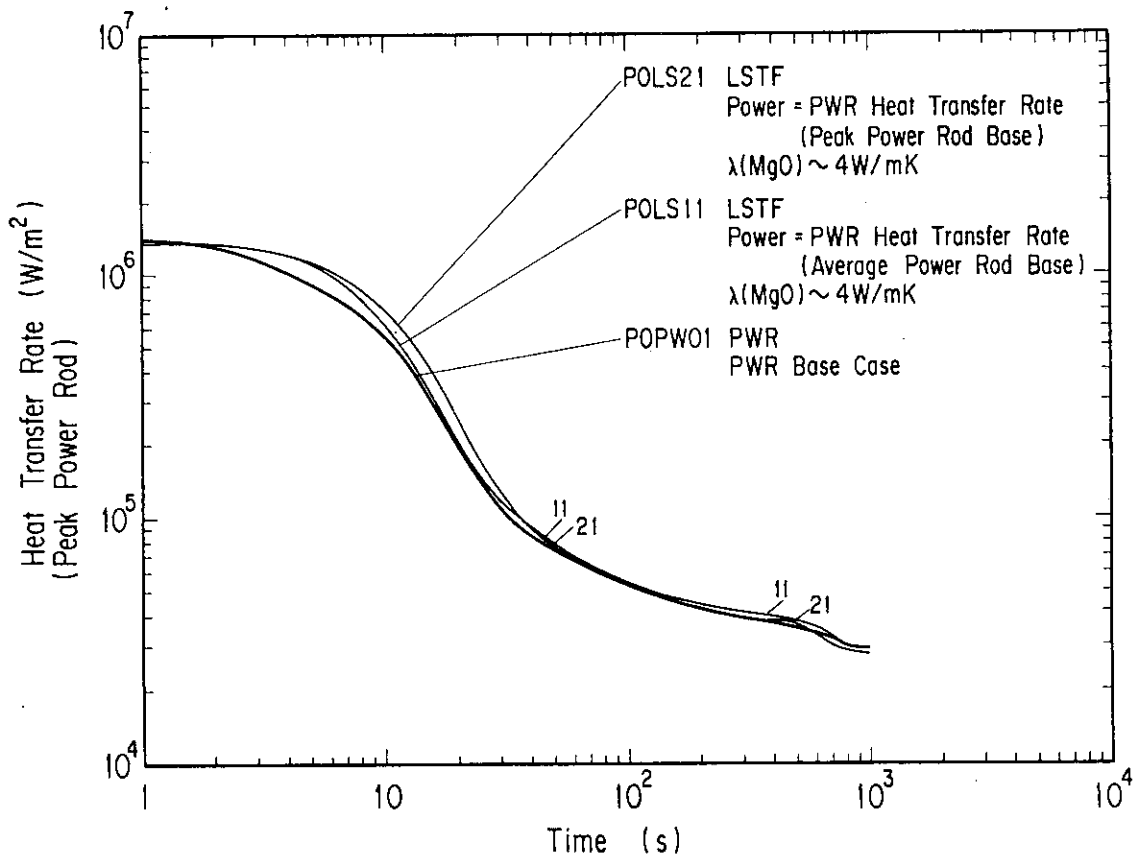


Fig. 2.8 Comparison of Heat Transfer Rates in Case POPW01 and POLS11 and POLS21; Peak Power Rod

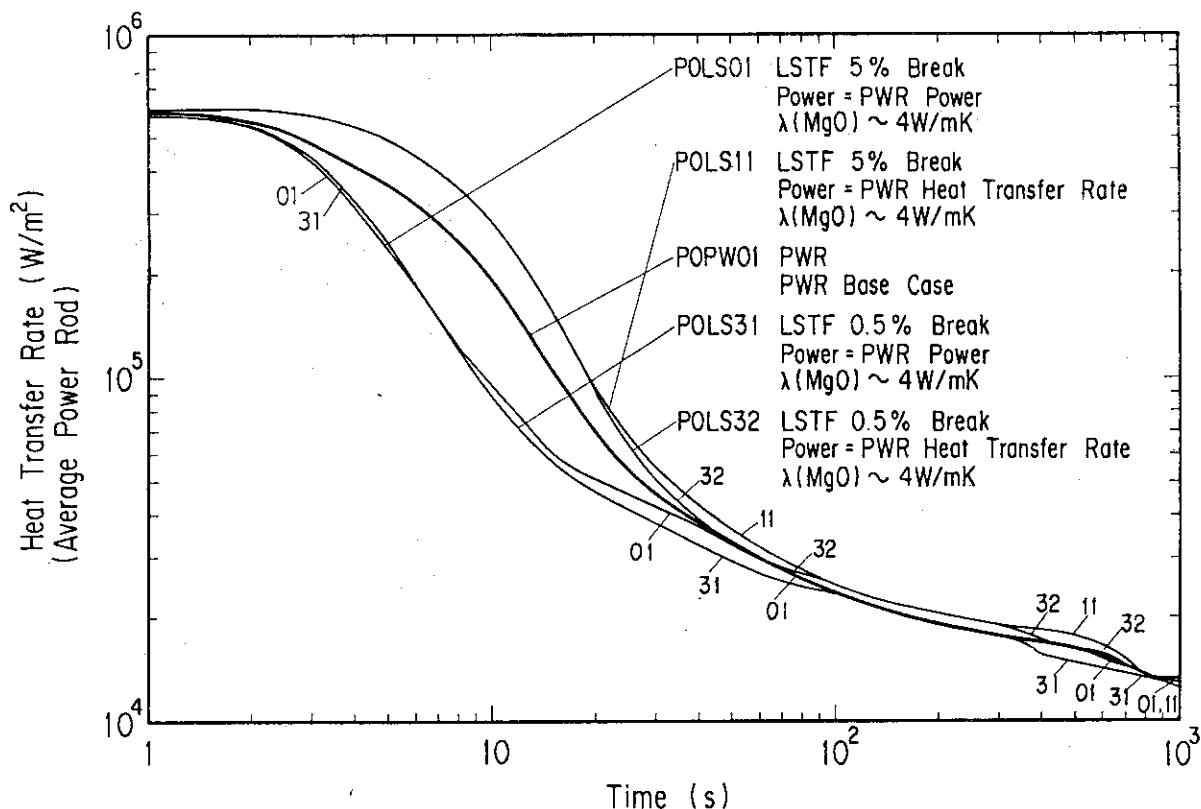


Fig. 2.9 Comparison of Heat Transfer Rates in Case POPW01 and Cases POLS11 and POLS32

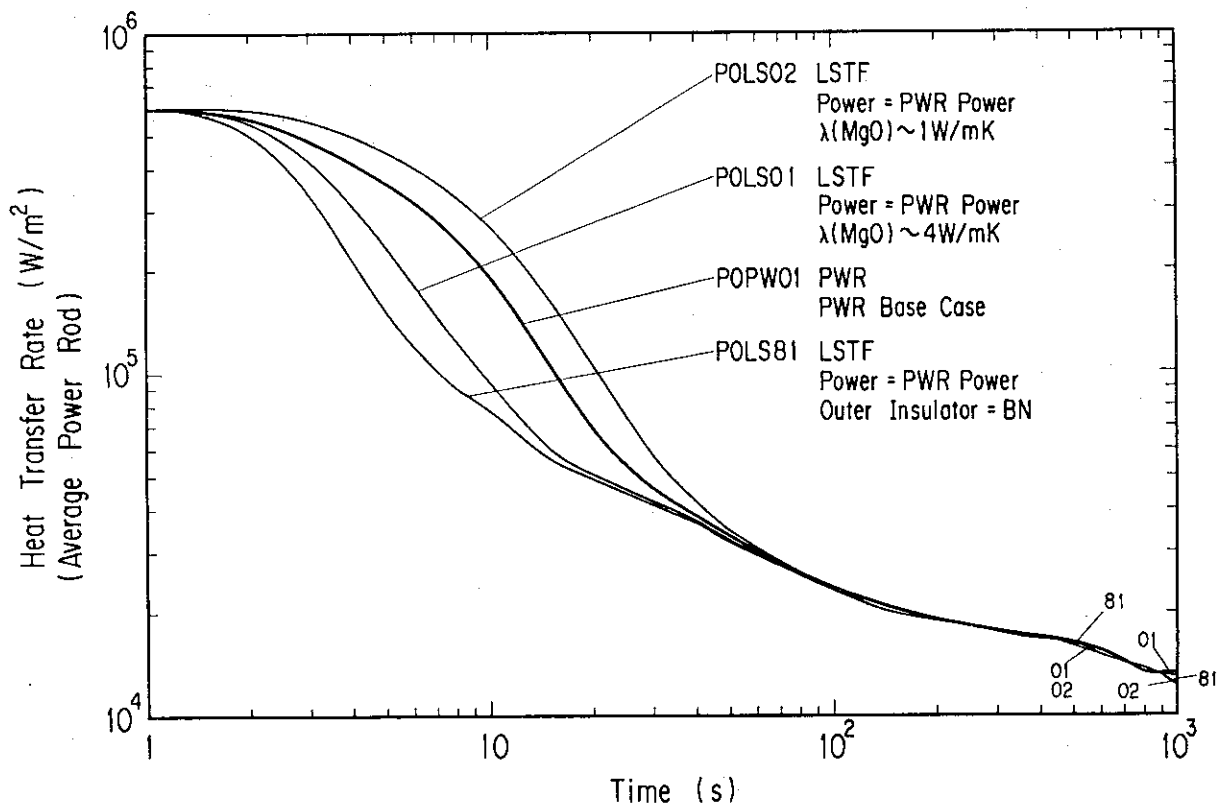


Fig. 2.10 Comparison of Heat Transfer Rates in Case POPW01 and Cases POLS01 and POLS81

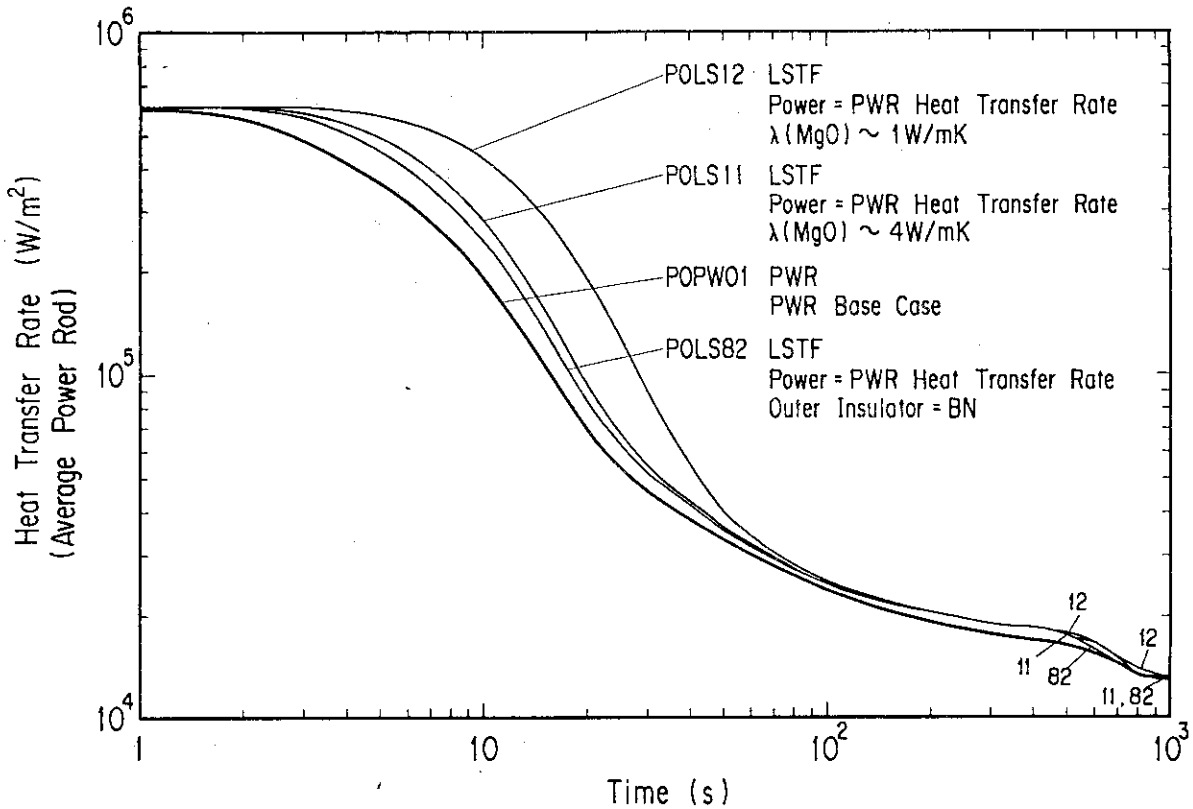


Fig. 2.11 Comparison of Heat Transfer Rates in Case POPW01 and Cases POLS11 and POLS82

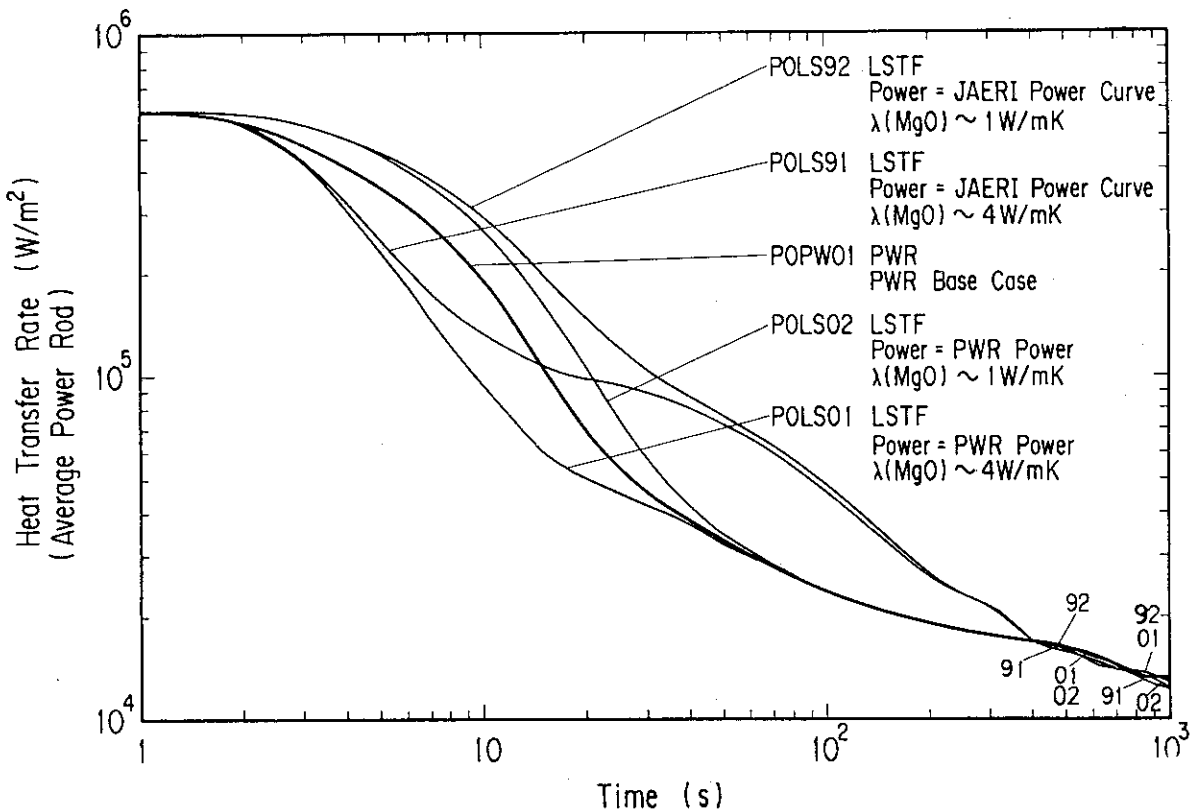


Fig. 2.12 Comparison of Heat Transfer Rates in Case POPW01 and Cases POLS91

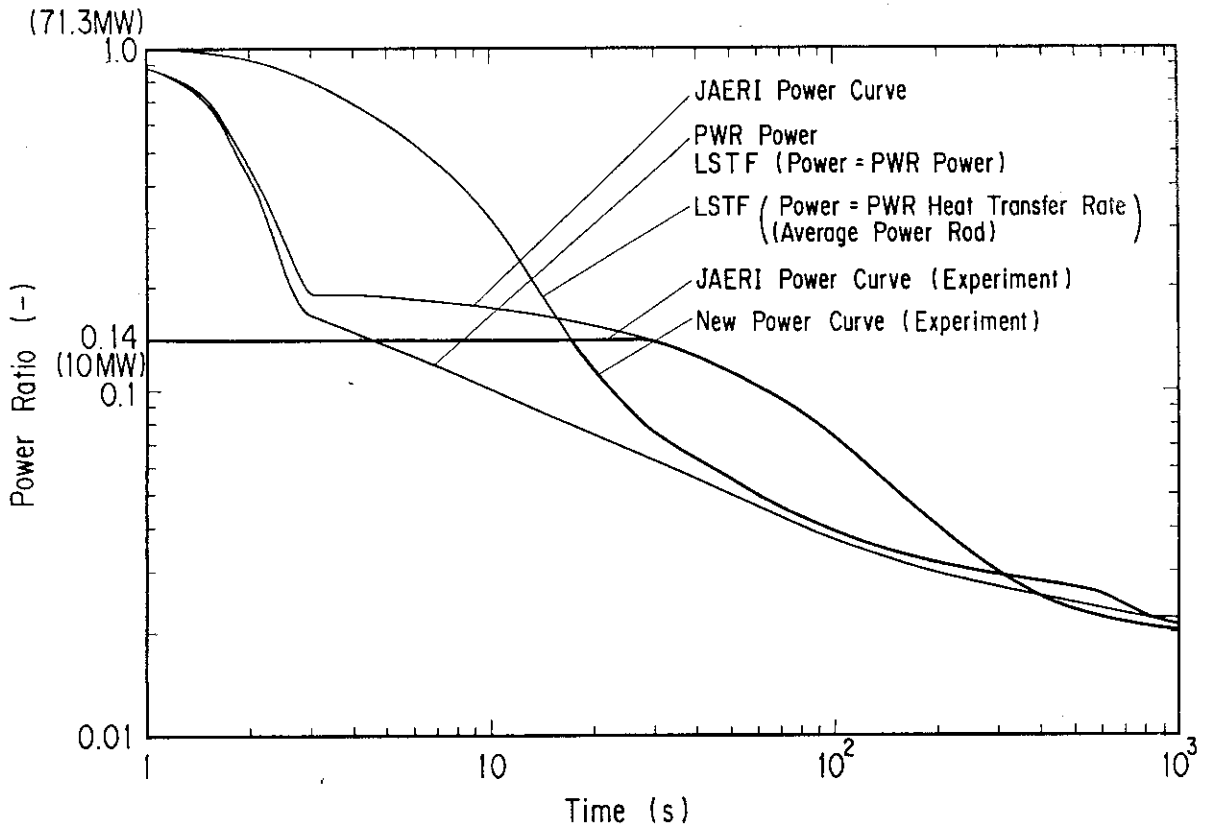


Fig. 2.13 Comparison of PWR Power, New Power Curve and JAERI Power Curve

Appendix A Input Data used for Delayed Neutron Fission Power
Calculation (Case PWPO00)

FILE = J3491.LSR5P2.DATA DATE 88/08/05(FRIDAY) TIME 17:41:39 PAGE 0001 *VIVAPO*

```

*****
** PWP000 **
*****

= PWR POWER CURVE
* RELAPS/MOD2 INPUT DATA
*****
MODULE NAME = PWP000
*****
87/6/16 BY KUMAMARU
*****
- INLET QUALITY = 0.05
*****
- CORE FLOW RATE = 0.59170 KG/S
*****
- POWER = 26.886 KW
*****
*
* TYPE OPTION
* NEW TRANSNT
*
0000100
*
* INPUT CHECK
* RUN
*
* INPUT OUTPUT
* SI SI
*
* T END MIN MAX CON MIE MAE MR
* 0000201 20.0 1.0-10 0.005 1 20 1000 1000
* 0000202 50.0 1.0-10 0.005 1 100 4000 1000
* 0000203 1000.0 1.0-10 0.010 1 500 4000 1000
*
*****
* TRIP ; REACTOR SCRAM
*
0000501 TIME 0 GE NULL 0 15.0 L
*
*****
* MINOR EDIT REQUESTS
*
0000301 P 005010000
0000302 TEMPF 005010000
0000303 P 003010000
0000304 TEMPF 003010000
0000305 TEMPG 003010000
0000306 QUALS 003010000
0000307 P 004010000
0000308 TEMPF 004010000
0000309 TEMPG 004010000
0000310 QUALS 004010000
0000311 P 001010000
0000312 TEMPF 001010000
0000313 TEMPG 001010000
0000314 QUALS 001010000
0000315 VOIDF 001010000
0000316 VOIDG 001010000
0000317 P 002010000
0000318 TEMPF 002010000

* 00010000 PWP013
* 00020000 PWP013
* 00030000 PWP013
* 00040012 PWP013
* 00050000 PWP013
* 00060000 PWP013
* 00070000 PWP013
* 00080000 PWP013
* 00090000 PWP013
* 00100000 PWP013
* 00110000 PWP013
* 00120000 PWP013
* 00130000 PWP013
* 00140000 PWP013
* 00150000 PWP013
* 00160000 PWP013
* 00170000 PWP013
* 00180000 PWP013
* 00190000 PWP013
* 00200000 PWP013
* 00210000 PWP013
* 00220000 PWP013
* 00230000 PWP013
* 00240000 PWP013
* 00240211 PWP013
* 00240311 PWP013
* 00241011 PWP013
* 00242011 PWP013
* 00250000 PWP013
* 00260000 PWP013
* 00270000 PWP013
* 00280006 PWP013
* 00290006 PWP013
* 00300006 PWP013
* 00310006 PWP013
* 00320006 PWP013
* 00330006 PWP013
* 00331006 PWP013
* 00332006 PWP013
* 00333006 PWP013
* 00334006 PWP013
* 00340006 PWP013
* 00350006 PWP013
* 00360006 PWP013
* 00370006 PWP013
* 00380006 PWP013
* 00390006 PWP013
* 00391006 PWP013
* 00392006 PWP013

```

FILE = J3491.LSR5P2.DATA DATE 88/08/05(FRIDAY) TIME 17:41:39 PAGE 0001

```

0000319     TEMP                                                                 PWP013
0000320     QUALS                                                                     PWP013
0000321     VOIDF                                                                 PWP013
0000322     VOIDG                                                                 PWP013
0000323     MFLOWJ                                                                PWP013
0000324     MFLOWK                                                                PWP013
0000325     MFLOWL                                                               PWP013
0000326     MFLOWM                                                              PWP013
0000327     HTTEMP                                                                PWP013
0000328     HTTEMP                                                                PWP013
0000329     HTTEMP                                                                PWP013
0000330     HTTEMP                                                                PWP013
0000331     HTTEMP                                                                PWP013
0000332     HTTEMP                                                                PWP013
0000333     HTTEMP                                                                PWP013
0000334     HTTEMP                                                                PWP013
0000335     HTTEMP                                                                PWP013
0000336     HTTEMP                                                                PWP013
0000337     HTTEMP                                                                PWP013
0000338     HTTEMP                                                                PWP013
0000339     HTTEMP                                                                PWP013
0000340     HTTEMP                                                                PWP013
0000341     HTTEMP                                                                PWP013
0000342     HTTEMP                                                                PWP013
0000343     HTTEMP                                                                PWP013
0000344     HTTEMP                                                                PWP013
0000345     HTRNR                                                                 PWP013
0000346     HTRNR                                                                 PWP013
0000347     RKTIPOW                                                               PWP013
0000348     RKFIPOW                                                               PWP013
0000349     RKGAPOW                                                               PWP013
0000350     RKREAC                                                                 PWP013
0000351     RKRECPER                                                                PWP013
*
*****
* CORE ( VOLUME 1 )
*
* NAME TYPE
* COO1 SNGLVOL
*
* AREA LEN VOL HZ VR ELV ROUGH HYD FE
* 0010101 1.7576-4 0.4575 0.0 0.0 90.0 0.4575 0.0 1.1778-2 0.0
*
* CTL PRESSURE TEMP
* 0010200 3 15.45+6 582.0
*
*****
* CORE INLET ( BRANCH 2 )
*
* NAME TYPE
* COO2 BRANCH
* 0020000.
*

```

FILE = J3491.LSR5P2.DATA DATE 88/08/05(FRIDAY) TIME 17:41:39 PAGE 0003 *VIVAPO*

```

* 0020001 NO.J CTL
* 1 1
* AREA LEN VOL HZ VR ELV FLOS RLOS CAHS
* 1.7576-4 0.05 0.0 0.0 90.0 0.05 0.0 0.0 0.0 10
* CTL PRESSURE TEMP
* 3 15.49+6 565.0
* FROM TO AREA FLOS RLOS CAHS
* 0021101 002010000 001000000 1.7576-4 0.0 0.0 0000
* FLOW-F FLOW-G VEL-G
* 0021201 0.59170 0.0 0.0
* *****
* VOLUME 3
* NAME TYPE
* C003 TMDPVOL
* AREA LEN VOL HZ VR ELV FLOS RLOS CAHS
* 0030101 1.7576-4 1.0 1.7576-4 0.0 90.0 1.0 0.0 0.0 11
* CTL TRIP ALPH NUME
* 3
* TIME PRESSURE TEMP
* 0030201 0.0 15.50+6 565.0
* 0030202 15.3 12.50+6 593.1
* 0030203 1000.0 12.50+6 593.1
* *****
* VOLUME 4
* NAME TYPE
* C004 TMDPVOL
* AREA LEN VOL HZ VR ELV FLOS RLOS CAHS
* 0040101 1.7576-4 1.0 1.7576-4 0.0 90.0 1.0 0.0 0.0 11
* CTL TRIP ALPH NUME
* 2
* TIME PRESSURE QUALITY
* 0040201 0.0 15.50+6 0.05
* 0040202 15.3 12.50+6 0.05
* 0040203 25.0 10.60+6 0.05
* 0040204 60.0 9.25+6 0.05
* 0040205 77.0 8.95+6 0.05
* 0040206 124.0 8.45+6 0.05
* 0040207 148.0 8.40+6 0.05
* 0040208 167.0 8.15+6 0.05

```

FILE = J3491.LSR5P2.DATA DATE 88/08/05(FRIDAY) TIME 17:41:39 PAGE 0003

FILE = J3491.LSR5P2.DATA DATE 88/08/05(FRIDAY) TIME 17:41:39 PAGE 0004 *VIVAPO*

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0040209 207.0 7.75+6 0.05 *01160407 PWP013
0040210 239.0 7.25+6 0.05 *01160507 PWP013
0040211 400.0 5.10+6 0.05 *01160607 PWP013
0040212 486.0 3.95+6 0.05 *01160707 PWP013
0040213 549.0 3.30+6 0.05 *01160807 PWP013
0040214 557.0 3.05+6 0.05 *01160907 PWP013
0040215 582.0 2.60+6 0.05 *01161007 PWP013
0040216 609.0 2.40+6 0.05 *01161107 PWP013
0040217 627.0 2.30+6 0.05 *01161207 PWP013
0040218 774.0 2.20+6 0.05 *01161307 PWP013
0040219 810.0 2.05+6 0.05 *01161407 PWP013
0040220 910.0 2.00+6 0.05 *01161507 PWP013
0040221 938.0 1.85+6 0.05 *01161607 PWP013
0040222 969.0 1.65+6 0.05 *01161707 PWP013
0040223 1000.0 1.55+6 0.05 *01161807 PWP013
* * * * * *01161907 PWP013
* * * * * *01162007 PWP013
* * * * * *01162107 PWP013
* * * * * *01162207 PWP013
* * * * * *01170000 PWP013
* * * * * *01180007 PWP013
* * * * * *01190000 PWP013
* * * * * *01200000 PWP013
* * * * * *01210007 PWP013
* * * * * *01220000 PWP013
* * * * * *01230000 PWP013
* * * * * *01240007 PWP013
* * * * * *01250000 PWP013
* * * * * *01260000 PWP013
* * * * * *01270007 PWP013
* * * * * *01280000 PWP013
* * * * * *01290000 PWP013
* * * * * *01300007 PWP013
* * * * * *01310007 PWP013
* * * * * *01311007 PWP013
* * * * * *01320007 PWP013
* * * * * *01330007 PWP013
* * * * * *01340007 PWP013
* * * * * *01350007 PWP013
* * * * * *01360007 PWP013
* * * * * *01370007 PWP013
* * * * * *01380007 PWP013
* * * * * *01390007 PWP013
* * * * * *01400007 PWP013
* * * * * *01410007 PWP013
* * * * * *01420007 PWP013
* * * * * *01430007 PWP013
* * * * * *01440007 PWP013
* * * * * *01450007 PWP013
* * * * * *01460007 PWP013
* * * * * *01470007 PWP013
* * * * * *01480007 PWP013
* * * * * *01490007 PWP013
* * * * * *01500007 PWP013
* * * * * *01510007 PWP013
* * * * * *01520000 PWP013
* * * * * *01530000 PWP013

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FILE = J3491.LSR5P2.DATA DATE 88/08/05(FRIDAY) TIME 17:41:39 PAGE 0004

FILE = J3491.LSR5P2.DATA DATE 88/08/05(FRIDAY) TIME 17:41:39 PAGE 0005 *VIVAP0*

```

* * *
* * JUNCTION BETWEEN VOLUME 3 AND BRANCH 2 ( JUNCTION 12 )
* *
* * NAME TYPE
* * C012 TMDPJUN
* *
* * FROM TO AREA
* * 0120101 003000000 002000000 1.7576-4
* *
* * CTL
* * 1
* *
* * TIME FLOW-F FLOW-G VEL-J
* * 0120201 0.0 0.59170 0.0 0.0
* * 0120202 15.3 0.59170 0.0 0.0
* * 0120203 15.4 0.0 0.0 0.0
* * 0120204 1000.0 0.0 0.0 0.0
* *
* * *****
* * JUNCTION BETWEEN VOLUME 4 AND BRANCH 2 ( JUNCTION 13 )
* *
* * NAME TYPE
* * C013 TMDPJUN
* *
* * FROM TO AREA
* * 0130101 004000000 002000000 1.7576-4
* *
* * CTL
* * 1
* *
* * TIME FLOW-F FLOW-G VEL-J
* * 0130201 0.0 0.0 0.0 0.0
* * 0130202 15.2 0.0 0.0 0.0
* * 0130203 15.3 0.56211 0.029585 0.0
* * 0130204 1000.0 0.56211 0.029585 0.0
* *
* * *****
* * JUNCTION BETWEEN VOLUME 1 AND VOLUME 5 ( JUNCTION 14 )
* *
* * NAME TYPE
* * C014 SNGLJUN
* *
* * FROM TO AREA FLOS RLOS CAHS SUBC TWOC
* * 0140101 005000000 001010000 1.7576-4 0.0 0.0 0000 1.0 1.0
* *
* * CTL FLOW-F FLOW-G VEL-J
* * 0140201 1 -0.59170 0.0 0.0
* *
* * *****
* * HEAT SLAB
* * *****
* * *****
* * *****

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FILE = J3491.LSR5P2.DATA DATE 88/08/05(FRIDAY) TIME 17:41:39 PAGE 0005

FILE = J3491.LSR5P2.DATA DATE 88/08/05(FRIDAY) TIME 17:41:39 PAGE 0006 *VIVARO*

```

*****
***** AVERAGE POWER CHANNEL HEAT STRUCTURE *****
*****
* NH NP TYPE S-FLG L-COR *****01870000 PWP013
* 10010000 1 9 2 1 0.0 *****01880000 PWP013
* *****01890000 PWP013
* *****01900000 PWP013
* *****01910000 PWP013
* *****01920000 PWP013
* *****01930000 PWP013
* *****01940000 PWP013
* *****01950000 PWP013
* *****01960000 PWP013
* *****01970000 PWP013
* *****01980000 PWP013
* *****01990000 PWP013
* *****02000000 PWP013
* *****02010000 PWP013
* *****02020000 PWP013
* *****02030000 PWP013
* *****02040000 PWP013
* *****02050000 PWP013
* *****02060000 PWP013
* *****02070000 PWP013
* *****02080000 PWP013
* *****02090000 PWP013
* *****02100000 PWP013
* *****02110000 PWP013
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* *****02150000 PWP013
* *****02160000 PWP013
* *****02170000 PWP013
* *****02180000 PWP013
* *****02190000 PWP013
* *****02200000 PWP013
* *****02210000 PWP013
* *****02220000 PWP013
* *****02230004 PWP013
* *****02231004 PWP013
* *****02240000 PWP013
* *****02250000 PWP013
* *****02260000 PWP013
* *****02270000 PWP013
* *****02280000 PWP013
* *****02290000 PWP013
* *****02300000 PWP013
* *****02310000 PWP013
* *****02320000 PWP013
* *****02330000 PWP013
* *****02340000 PWP013
* *****02350000 PWP013
* *****02360000 PWP013
* *****02370000 PWP013
* *****02380000 PWP013
* *****02390000 PWP013
* *****02400000 PWP013
*****
***** AVERAGE POWER CHANNEL HEAT STRUCTURE *****
*****
* NO ITV R-COR NO ITV R-COR NO ITV R-COR
* 10010101 5 0.00410, 1 0.00414, 2 0.00475
* *****
* CMP NO CMP NO CMP NO
* 10010201 1 5, 2 6, 3 8
* *****
* SOURCE
* 10010301 1.0 5, 0.0 6, 0.0 8
* *****
* FLG
* 10010400 0
* *****
* TEMP NP
* 10010401 617.7 9
* ***** LEFT *****
* ***** RIGHT *****
* 8.V. INC BCT A-C AREA NH
* 10010501 0 0 0 0.0 1
* *****
* B.V. INC BCT A-C AREA NH
* 10010601 001010000 0 1 0 1.3654-2 1
* *****
* TYPE IS MULTI L-O-H R-D-H NH
* 10010701 1000 0.30899 0.0 0.0 1
* 10010701 1000 0.30145 0.0 0.0 1
* ***** LEFT *****
* ***** RIGHT *****
* CHF HYD HEQ CHAN-L NH
* 10010801 0 0.0 0.0 0.0 1
* *****
* CHF HYD HEQ CHAN-L NH
* 10010901 0 0.011778 0.011778 0.4575 1
* *****
***** HIGH POWER CHANNEL HEAT STRUCTURE *****
*****
* NH NP TYPE S-FLG L-COR *****
* 10020000 1 9 2 1 0.0 *****

```

FILE = J3491.LSR5P2.DATA DATE 88/08/05(FRIDAY) TIME 17:41:39 PAGE 0006

FILE = J3491.LSRSP2.DATA DATE 88/08/05(FRIDAY) TIME 17:41:39 PAGE 0007 *VIVAP0*

```

*
* LOC-F MESH-F
* 10020100 0010
*
* FLG
* 10020400 0010
*
* ***** LEFT *****
*
* B.V. INC BCT A-C AREA NH
* 10020501 0 0 0 0.0 1
*
* ***** RIGHT *****
*
* B.V. INC BCT A-C AREA NH
* 10020601 001010000 0 1 0 1.3654-2 1
*
* TYPE IS MULTI L-D-H R-D-H NH
* 0020701 1000 0.69301 0.0 0.0 1
* 10020701 1000 0.69855 0.0 0.0 1
*
* ***** LEFT *****
*
* CHF HYD HEQ CHAN-L NH
* 10020801 0 0.0 0.0 0.0 1
*
* ***** RIGHT *****
*
* CHF HYD HEQ CHAN-L NH
* 10020901 0 0.011778 0.011778 0.4575 1
*
* ***** HEAT STRUCTURE THERMAL PROPERTY DATA *****
*
* TYPE K-FLAG CV-FLAG
*
* UO2 TBL/FCTN 1 1
* HE GAS
* 20100200 TBL/FCTN 1 1
* ZIRCONIUM
* 20100300 ZR
*
* ***** THERMAL CONDUCTIVITY (W/MK) *****
*
* TEMP COND TEMP COND TEMP COND
* UO2
* 20100101 311.1 8.657 422.1 6.915 533.2 5.759
* 20100102 644.3 4.939 755.4 4.329 866.5 3.858
* 20100103 977.6 3.488 1088.8 3.190 1199.9 2.947
* 20100104 1311.0 2.683 1421.2 2.553 1533.2 2.396
* 20100105 1644.2 2.309 1927.2 2.197
* 20100105 1644.2 2.309 1927.2 2.197 3927.2 2.197
*

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FILE = J3491.LSRSP2.DATA DATE 88/08/05(FRIDAY) TIME 17:41:39 PAGE 0007


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FILE = J3491.LSR5P2.DATA
DATE      88/08/05(FRIDAY)      TIME 17:41:39      PAGE 0009      *VIVAP0*
20211102      0.5      0.53333      *03410011      PWP013
20211103      1.0      3.3333      *03420011      PWP013
20211104      1.4      8.2667      *03430011      PWP013
20211105      1.6      12.000      *03440011      PWP013
20211106      1.8      18.667      *03450011      PWP013
20211107      2.0      33.333      *03460011      PWP013
20211108      2.2      75.333      *03470011      PWP013
20211109      2.4      116.00      *03480011      PWP013
20211110      2.6      127.20      *03490011      PWP013
20211111      2.8      131.47      *03500011      PWP013
20211112      3.0      133.33      *03510011      PWP013
20211113      1000.0      *****      *03520011      PWP013
*      *****      *03530000      PWP013
.      *****      *03540000      PWP013
          *****      *03550000      PWP013

```

Appendix B Input Data used for PWR Heat Transfer Calculation
(Case POPW01)

FILE = J3491.LSRSP2.DATA DATE 87/10/13(TUESDAY) TIME 20:03:49 PAGE 0001 *VIVAPO*

** POPW01 **

```

= PWR POWER CURVE
* RELAP5/MD2 INPUT DATA
*****
MODULE NAME = POPW01
87/6/16 BY KUMAMARU
- INLET CONDITION :
- SUBCOOLED TO SATURATED
- CORE FLOW RATE = 0.59170 KG/S
- POWER = 26.886 KW
*****
*
* TYPE OPTION
* NEW TRANSNT
0000100
*
* INPUT CHECK
0000101
*
* INPUT OUTPUT
SI SI
*
* T END MIN MAX CON MIE MAE MR
0000201 20.0 1.0-10 0.005 1 100 4000 1000
0000202 50.0 1.0-10 0.005 1 200 4000 1000
0000203 200.0 1.0-10 0.01 1 250 4000 1000
0000204 500.0 1.0-10 0.02 1 250 4000 1000
0000205 1050.0 1.0-10 0.04 1 125 4000 1000
*
*****
* TRIP ; REACTOR SCRAM
*****
0000501 TIME 0 GE NULL 0 15.0 L
*
*****
* MINOR EDIT REQUESTS
*****
0000301 P 005010000
0000302 TEMPF 005010000
0000303 P 003010000
0000304 TEMPF 003010000
0000305 TEMPG 003010000
0000306 GUALS 003010000
0000307 P 004010000
0000308 TEMPF 004010000
0000309 TEMPG 004010000
0000310 GUALS 004010000
0000311 P 001010000
0000312 TEMPF 001010000
0000313 TEMPG 001010000
0000314 GUALS 001010000
0000315 VOIDF 001010000

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FILE = J3491.LSRSP2.DATA DATE 87/10/13(TUESDAY) TIME 20:03:49 PAGE 0001

FILE = J3491.LSR5P2.DATA DATE 87/10/13(TUESDAY) TIME 20:03:49 PAGE 0002 *VIVAF0*

```

0000316 VOIDG 001010000 POPW01
0000317 P 002010000 POPW01
0000318 TEMPF 002010000 POPW01
0000319 TEMPG 002010000 POPW01
0000320 QVALS 002010000 POPW01
0000321 VOIDF 002010000 POPW01
0000322 VOIDG 002010000 POPW01
0000323 MFLOWJ 012000000 POPW01
0000324 MFLOWJ 013000000 POPW01
0000325 MFLOWJ 014000000 POPW01
0000326 MFLOWJ 002010000 POPW01
0000327 HTTEMP 001000101 POPW01
0000328 HTTEMP 001000102 POPW01
0000329 HTTEMP 001000103 POPW01
0000330 HTTEMP 001000104 POPW01
0000331 HTTEMP 001000105 POPW01
0000332 HTTEMP 001000106 POPW01
0000333 HTTEMP 001000107 POPW01
0000334 HTTEMP 001000108 POPW01
0000335 HTTEMP 001000109 POPW01
0000336 HTTEMP 002000101 POPW01
0000337 HTTEMP 002000102 POPW01
0000338 HTTEMP 002000103 POPW01
0000339 HTTEMP 002000104 POPW01
0000340 HTTEMP 002000105 POPW01
0000341 HTTEMP 002000106 POPW01
0000342 HTTEMP 002000107 POPW01
0000343 HTTEMP 002000108 POPW01
0000344 HTTEMP 002000109 POPW01
0000345 HTRNR 001000101 POPW01
0000346 HTRNR 002000101 POPW01
*000347 RKTPOW 000000000 POPW01
*000348 RKFIPW 000000000 POPW01
*000349 RKGAPW 000000000 POPW01
*000350 RKREAC 000000000 POPW01
*000351 RKRECPER 000000000 POPW01
*
*****
* CORE ( VOLUME 1 )
*****
* NAME TYPE SINGLVOL
* C001
*
* AREA LEN VOL HZ VR ELV ROUGH HYD FE
* 0010101 1.7576-4 0.4575 0.0 0.0 90.0 0.4575 0.0 1.1778-2 00
*
* CTL PRESSURE TEMP
* 0010200 3 15.45+6 582.0
*
*****
* CORE INLET ( BRANCH 2 )
*****
*
*
*
*

```

FILE = J3491.LSR5P2.DATA DATE 87/10/13(TUESDAY) TIME 20:03:49 PAGE 0002

FILE = J3491.LSR5P2.DATA DATE 87/10/13(TUESDAY) TIME 20:03:49 PAGE 0003 *VIVAPD*

```

* 0020000 NAME CODE TYPE BRANCH POPW01
* 00785008
* 00786008 POPW01
* 00786108 POPW01
* 00786208 POPW01
* 00786308 POPW01
* 00786408 POPW01
* 00786508 POPW01
* 00786608 POPW01
* 00786708 POPW01
* 00786808 POPW01
* 00786908 POPW01
* 00787008 POPW01
* 00787108 POPW01
* 00787208 POPW01
* 00787308 POPW01
* 00787408 POPW01
* 00787508 POPW01
* 00787608 POPW01
* 00787708 POPW01
* 00787808 POPW01
* 00787908 POPW01
* 00788008 POPW01
* 00788108 POPW01
* 00788208 POPW01
* 00788308 POPW01
* 00788408 POPW01
* 00788508 POPW01
* 00788608 POPW01
* 00788708 POPW01
* 00788808 POPW01
* 00788908 POPW01
* 00789008 POPW01
* 00789108 POPW01
* 00789208 POPW01
* 00789308 POPW01
* 00789408 POPW01
* 00789508 POPW01
* 00789608 POPW01
* 00789708 POPW01
* 00789808 POPW01
* 00789908 POPW01
* 00790008 POPW01
* 00790108 POPW01
* 00790208 POPW01
* 00790308 POPW01
* 00800000 POPW01
* 00810006 POPW01
* 00820000 POPW01
* 00830000 POPW01
* 00840006 POPW01
* 00850000 POPW01
* 00860000 POPW01
* 00870006 POPW01
* 00880000 POPW01
* 00890000 POPW01
* 00900006 POPW01
* 00910000 POPW01
* 00920007 POPW01
* 00930007 POPW01
* 00940007 POPW01
* 00950007 POPW01
* 01150000 POPW01
* 01151006 POPW01
* 01152006 POPW01
* 01153007 POPW01
* 01154006 POPW01
* 01155006 POPW01
* 01156007 POPW01
* 01157006 POPW01
* 01158006 POPW01
* 01159007 POPW01
* 01159106 POPW01
* 01159206 POPW01
* 01159307 POPW01
* 01159406 POPW01
* 01159506 POPW01
* 01159619 POPW01
* 01159719 POPW01
* 01159819 POPW01
* 01159919 POPW01
* 01160019 POPW01

```

FILE = J3491.LSR5P2.DATA DATE 87/10/13(TUESDAY) TIME 20:03:49 PAGE 0003

FILE = J3491.LSRSP2.DATA DATE 87/10/13(TUESDAY) TIME 20:03:49 PAGE 0004 *VIVAPO*

NO	AREA	LEN	VOL	HZ	VR	ELV	ROUGH	HYD	FE	POPW01
0040206	124.0	8.45+6	1.0-10							*01160119
0040207	148.0	8.40+6	1.0-10							*01160219
0040208	167.0	8.15+6	1.0-10							*01160319
0040209	207.0	7.75+6	1.0-10							*01160419
0040210	239.0	7.25+6	1.0-10							*01160519
0040211	400.0	5.10+6	1.0-10							*01160619
0040212	486.0	3.95+6	1.0-10							*01160719
0040213	549.0	3.30+6	1.0-10							*01160819
0040214	557.0	3.05+6	1.0-10							*01160919
0040215	582.0	2.60+6	1.0-10							*01161019
0040216	609.0	2.40+6	1.0-10							*01161119
0040217	627.0	2.30+6	1.0-10							*01161219
0040218	774.0	2.20+6	1.0-10							*01161319
0040219	810.0	2.05+6	1.0-10							*01161419
0040220	910.0	2.00+6	1.0-10							*01161519
0040221	938.0	1.85+6	1.0-10							*01161619
0040222	969.0	1.65+6	1.0-10							*01161719
0040223	1000.0	1.55+6	1.0-10							*01161819
*										*01161907
*										*01162007
*										*01170000
*										*01180007
*										*01190000
*										*01200000
*										*01210007
*										*01220000
*										*01230000
*										*01240007
*										*01250000
*										*01260000
*										*01270007
*										*01280000
*										*01290000
*										*01300007
*										*01310007
*										*01320007
*										*01330007
*										*01340007
*										*01350007
*										*01360007
*										*01370007
*										*01380007
*										*01390007
*										*01400007
*										*01410007
*										*01420007
*										*01430007
*										*01440007
*										*01450007
*										*01460007
*										*01470007
*										*01480007
*										*01490007
*										*01500007

FILE = J3491.LSRSP2.DATA DATE 87/10/13(TUESDAY) TIME 20:03:49 PAGE 0004

FILE = J3491.LSR5P2.DATA DATE 87/10/13(TUESDAY) TIME 20:03:49 PAGE 0005 *VIVAPO*

```

0050223 1000.0 1.45+6 1.0
*
*****
* JUNCTION BETWEEN VOLUME 3 AND BRANCH 2 ( JUNCTION 12 )
*
* NAME TYPE
* C012 TMDPJUN
*
* FROM TO AREA
* 0120101 003000000 002000000 1.7576-4
*
* CTL
* 1
*
* TIME FLOW-F FLOW-G VEL-J
* 0120201 0.0 0.59170 0.0 0.0
* 0120202 15.3 0.59170 0.0 0.0
* 0120203 15.4 0.0 0.0 0.0
* 0120204 1000.0 0.0 0.0 0.0
*
*****
* JUNCTION BETWEEN VOLUME 4 AND BRANCH 2 ( JUNCTION 13 )
*
* NAME TYPE
* C013 TMDPJUN
*
* FROM TO AREA
* 0130101 004000000 002000000 1.7576-4
*
* CTL
* 1
*
* TIME FLOW-F FLOW-G VEL-J
* 0130201 0.0 0.0 0.0 0.0
* 0130202 15.2 0.0 0.0 0.0
* 0130203 15.3 0.59170 0.59170-10 0.0
* 0130204 1000.0 0.59170 0.59170-10 0.0
*
*****
* JUNCTION BETWEEN VOLUME 1 AND VOLUME 5 ( JUNCTION 14 )
*
* NAME TYPE
* C014 SNGLJUN
*
* FROM TO AREA FLOS RLODS CAHS SUBC TWQC
* 0140101 005000000 001010000 1.7576-4 0.0 0.0 0000 1.0 1.0
*
* CTL FLOW-F FLOW-G VEL-J
* 1 -0.59170 0.0 0.0
*
*****

```

FILE = J3491.LSR5P2.DATA DATE 87/10/13(TUESDAY) TIME 20:03:49 PAGE 0005

```

***** HEAT SLAB *****
***** 01840000 POPW01
***** 01850000 POPW01
***** 01860000 POPW01
***** 01870000 POPW01
***** 01880000 POPW01
***** 01890000 POPW01
***** 01900000 POPW01
***** 01910000 POPW01
***** 01920000 POPW01
***** 01930000 POPW01
***** 01940000 POPW01
***** 01950000 POPW01
***** 01960000 POPW01
***** 01970000 POPW01
***** 01980000 POPW01
***** 01990000 POPW01
***** 02000000 POPW01
***** 02010000 POPW01
***** 02020000 POPW01
***** 02030000 POPW01
***** 02040000 POPW01
***** 02050000 POPW01
***** 02060000 POPW01
***** 02070000 POPW01
***** 02080000 POPW01
***** 02090000 POPW01
***** 02100000 POPW01
***** 02110000 POPW01
***** 02120000 POPW01
***** 02130000 POPW01
***** 02140000 POPW01
***** 02150000 POPW01
***** 02160000 POPW01
***** 02170000 POPW01
***** 02180000 POPW01
***** 02190000 POPW01
***** 02200000 POPW01
***** 02210000 POPW01
***** 02220000 POPW01
***** 02230000 POPW01
***** 02231012 POPW01
***** 02232012 POPW01
***** 02240000 POPW01
***** 02250000 POPW01
***** 02260000 POPW01
***** 02270000 POPW01
***** 02280000 POPW01
***** 02290000 POPW01
***** 02300000 POPW01
***** 02310000 POPW01
***** 02320000 POPW01
***** 02330000 POPW01
***** 02340000 POPW01
***** 02350000 POPW01
***** 02360000 POPW01

```


FILE = J3491.LSR5P2.DATA DATE 87/10/13(TUESDAY) TIME 20:03:49 PAGE 0007 *VIVAP0*

```

*****
*      NH NP TYPE S-FLG L-COR POPW01
* 10020000 1 9 2 1 0.0 POPW01
*      LOC-F MESH-F POPW01
* 10020100 0010 POPW01
*      FLG POPW01
* 10020400 0010 POPW01
***** LEFT *****
*      B-V. INC BCT A-C AREA NH
* 10020501 0 0 0 0.0 1
***** RIGHT *****
*      B-V. INC BCT A-C AREA NH
* 10020601 001010000 0 1 0 1.3654-2 1
*      TYPE IS MULTI L-D-H R-D-H NH
* 0020701 1000 0.69301 0.0 0.0 1
* 0020701 1000 0.69855 0.0 0.0 1
* 10020701 900 0.69855 0.0 0.0 1
***** LEFT *****
*      CHF HYD HEQ CHAN-L NH
* 10020801 0 0.0 0.0 0.0 1
***** RIGHT *****
*      CHF HYD HEQ CHAN-L NH
* 10020901 0 0.01178 0.01178 0.4575 1
***** HEAT STRUCTURE THERMAL PROPERTY DATA *****
*****
*      TYPE K-FLAG CV-FLAG
* 20100100 TBL/FCTN 1 1
* HE GAS
* 20100200 TBL/FCTN 1 1
* ZIRCONIUM
* 0100300 ZR
* 20100300 TBL/FCTN 1 1
*****
*      THERMAL CONDUCTIVITY (W/MK)
*
*      TEMP COND TEMP COND TEMP COND
* 02380000 POPW01
* 02390000 POPW01
* 02400000 POPW01
* 02410000 POPW01
* 02420000 POPW01
* 02430000 POPW01
* 02440000 POPW01
* 02450000 POPW01
* 02460000 POPW01
* 02470000 POPW01
* 02480000 POPW01
* 02490000 POPW01
* 02500000 POPW01
* 02510000 POPW01
* 02520000 POPW01
* 02530000 POPW01
* 02540000 POPW01
* 02550000 POPW01
* 02560000 POPW01
* 02570000 POPW01
* 02580000 POPW01
* 02590004 POPW01
* 02591012 POPW01
* 02592012 POPW01
* 02600000 POPW01
* 02610000 POPW01
* 02620000 POPW01
* 02630000 POPW01
* 02640000 POPW01
* 02650000 POPW01
* 02660000 POPW01
* 02670000 POPW01
* 02680000 POPW01
* 02690000 POPW01
* 02700000 POPW01
* 02710000 POPW01
* 02720000 POPW01
* 02730000 POPW01
* 02740000 POPW01
* 02750000 POPW01
* 02760000 POPW01
* 02770000 POPW01
* 02780000 POPW01
* 02790000 POPW01
* 02800000 POPW01
* 02810000 POPW01
* 02820000 POPW01
* 02830014 POPW01
* 02831014 POPW01
* 02840000 POPW01
* 02850000 POPW01
* 02860000 POPW01
* 02870000 POPW01
* 02880000 POPW01

```

FILE = J3491.LSR5P2.DATA DATE 87/10/13(TUESDAY) TIME 20:03:49 PAGE 0007

FILE = J3491.LSR5P2.DATA DATE 87/10/13(TUESDAY) TIME 20:03:49 PAGE 0008 *VIVAF0*

20100101	311.1	8.657	422.1	6.915	533.2	5.759	*02890000	POPW01
20100102	644.3	4.939	755.4	4.329	866.5	3.858	*02900000	POPW01
20100103	977.6	3.488	1088.8	3.190	1199.9	2.947	*02910000	POPW01
20100104	1311.0	2.683	1421.2	2.553	1533.2	2.396	*02920000	POPW01
*0100105	1644.2	2.309	1927.2	2.197			*02930002	POPW01
20100105	1644.2	2.309	1927.2	2.197	3927.2	0.7915	*02931014	POPW01
*							*02940000	POPW01
*							*02950000	POPW01
*HE GAS							*02960000	POPW01
20100201	0.221						*02970000	POPW01
*							*02971014	POPW01
*							*02972014	POPW01
*ZR-4							*02973014	POPW01
*0100301			380.4	13.6	469.3	14.6	*02974014	POPW01
20100301	300.0	12.8	380.4	13.6	469.3	14.6	*02974114	POPW01
20100302	577.6	15.8	685.9	17.3	774.8	18.4	*02975014	POPW01
20100303	872.0	19.8	973.2	21.8	1073.2	23.2	*02976014	POPW01
20100304	1123.2	25.4	1152.3	24.2	1232.2	25.5	*02977014	POPW01
20100305	1331.2	26.6	1404.2	28.2	1576.2	33.0	*02979014	POPW01
20100306	1625.2	36.7	1755.2	41.2	2273.2	55.0	*02979114	POPW01
*0100307							*02979214	POPW01
20100307	4273.2	108.3					*02979314	POPW01
*							*02980000	POPW01
*							*02990000	POPW01
*****							*****03000000	POPW01
*							03010000	POPW01
*UO2							03020000	POPW01
*0100151	311.0	1076.0	422.1	1217.7	533.2	1287.4	03030000	POPW01
*0100152	644.3	1330.0	755.4	1360.4	866.5	1384.4	*03040000	POPW01
*0100153	977.6	1404.5	1088.8	1422.4	1199.9	1439.0	*03050001	POPW01
*0100154	1644.3	1484.0					*03060001	POPW01
20100151	311.0	3.8736+6	422.1	4.3837+6	533.2	4.6346+6	*03070001	POPW01
20100152	644.3	4.7880+6	755.4	4.8974+6	866.5	4.9838+6	*03071001	POPW01
20100153	977.6	5.0562+6	1088.8	5.1206+6	1199.9	5.1804+6	*03072001	POPW01
*0100154	1644.3	5.3424+6					*03073001	POPW01
20100154	1644.3	5.3424+6	3644.3	6.0715+6			*03074002	POPW01
*							*03075014	POPW01
*							*03080000	POPW01
*HE GAS							*03090000	POPW01
*0100251	0.245						*03100000	POPW01
20100251	882.0						*03110001	POPW01
*							*03110014	POPW01
*							*03112014	POPW01
*ZR-4							*03113014	POPW01
20100351	300.0	1.841+6	400.0	1.978+6	640.0	2.168+6	*03114014	POPW01
20100352	1090.0	2.456+6	1093.0	3.288+6	1113.0	3.865+6	*03119015	POPW01
20100353	1133.0	4.028+6	1153.0	4.709+6	1173.0	5.345+6	*03119115	POPW01
20100354	1193.0	5.044+6	1213.0	4.054+6	1233.0	3.072+6	*03119215	POPW01
*0100355	1243.0	2.332+6	1477.0	2.332+6			*03119415	POPW01
20100355	1243.0	2.332+6	1477.0	2.332+6			*03119515	POPW01
*0100355	1243.0	2.332+6	1477.0	2.332+6			*03119615	POPW01
*							*03120000	POPW01
*							*03130000	POPW01
*****							*****03140000	POPW01
*****							*****03150000	POPW01

VOLUMETRIC HEAT CAPACITY (J/M3K)

FILE = J3491.LSR5P2.DATA DATE 87/10/13(TUESDAY) TIME 20:03:49 PAGE 0008


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FILE = J3491.LSR5P2.DATA
DATE      87/10/13(TUESDAY)    TIME 20:03:49    PAGE 0010    *VIVAPO*
20290043  1.0+7                1.20688-3      *03531112      POPW01
20290044  2.0+7                9.11667-4      *03531212      POPW01
20290045  5.0+7                6.85618-4      *03531312      POPW01
20290046  1.0+8                5.86748-4      *03531412      POPW01
20290047  2.0+8                5.22337-4      *03531512      POPW01
20290048  5.0+8                4.19465-4      *03531612      POPW01
20290049  1.0+9                2.96290-4      *03531712      POPW01
20290050  1.0+10               2.79366-5      *03531812      POPW01
20290051  1.0+11               2.72816-5      *03531912      POPW01
20290052  1.0+12               2.44637-5      *03532012      POPW01
20290053  1.0+13               9.90464-6      *03532112      POPW01
*
*****
*03532312      POPW01
*03540000      POPW01
*03550000      POPW01

```

Appendix C Example of Input Data used for LSTF Heat Transfer
Calculation (Case POLS01)

** P0LS01 **

```

= LSTF POWER CURVE
* RELAPS/MOD2 INPUT DATA
*****
***** MODULE NAME = P0LS01
***** 87/7/3 BY KUNAMARU
***** - INLET CONDITION :
***** SUBCOOLED TO SATURATED
***** - CORE FLOW RATE = 0.59170 KG/S
***** - POWER = 26.886 KW
*****
* TYPE OPTION
* NEW TRANSNT
0000100
* INPUT CHECK
RUN
* INPUT OUTPUT
SI
*
* T END MIN MAX CON MIE MAE MR
* 0000201 20.0 1.0-10 0.005 1 100 4000 1000
* 0000202 50.0 1.0-10 0.005 1 200 4000 1000
* 0000203 200.0 1.0-10 0.01 1 250 4000 1000
* 0000204 500.0 1.0-10 0.02 1 250 4000 1000
* 0000205 1050.0 1.0-10 0.04 1 125 4000 1000
*
***** REACTOR SCRAM
* TRIP ;
*
0000501 TIME 0 GE NULL 0 15.0 L
*
***** MINOR EDIT REQUESTS
*
0000301 P 005010000
0000302 TEMPF 005010000
0000303 P 003010000
0000304 TEMPF 003010000
0000305 TEMPG 003010000
0000306 QUALS 003010000
0000307 P 004010000
0000308 TEMPF 004010000
0000309 TEMPG 004010000
0000310 QUALS 004010000
0000311 P 001010000
0000312 TEMPF 001010000
0000313 TEMPG 001010000
0000314 QUALS 001010000
0000315 VOIDF 001010000

```

```

0000316 VOIDG
0000317 P
0000318 TEMP
0000319 TEMPG
0000320 QUALS
0000321 VOIDF
0000322 VOIDG
0000323 MFLOWJ
0000324 MFLOWJ
0000325 MFLOWJ
0000326 MFLOWJ
0000327 HTTEMP
0000328 HTTEMP
0000329 HTTEMP
0000330 HTTEMP
0000331 HTTEMP
0000332 HTTEMP
0000333 HTTEMP
0000334 HTTEMP
0000335 HTTEMP
0000336 HTTEMP
0000337 HTTEMP
0000338 HTTEMP
0000339 HTTEMP
0000340 HTTEMP
0000341 HTTEMP
0000342 HTTEMP
0000343 HTTEMP
0000344 HTTEMP
0000345 HTNR
0000346 HTNR
0000347 HTPOW
*****
* CORE ( VOLUME 1 )
*
* NAME TYPE
* C001 SINGL VOL
*
* AREA LEN VOL HZ VR ELV ROUGH HYD FE
* 0010101 1.7576-4 0.4575 0.0 0.0 90.0 0.4575 0.0 1.1778-2 00
*
* CTL PRESSURE TEMP
* 0010200 3 15.43+6 582.0
*****
* CORE INLET ( BRANCH 2 )
*
* NAME TYPE
* C002 BRANCH
*
* NO.J CTL
* 0020001 1 1
    
```

FILE = J3491.LSRSP2.DATA DATE 87/10/13(TUESDAY) TIME 16:16:21 PAGE 0003 *VIVAP0*

```

* * * * *
* 0020101 AREA LEN VOL HZ VR ELV ROUGH HYD FE PLS01
* 1.7576-4 0.05 0.0 0.0 90.0 0.05 0.0 0.0 10 PLS01
* * * * *
* 0020200 CTL PRESSURE TEMP PLS01
* 3 15.49+6 565.0 PLS01
* * * * *
* 0021101 FROM TO AREA FLOS RLOS CAHS PLS01
* 002010000 001000000 1.7576-4 0.0 0.0 0000 PLS01
* * * * *
* 0021201 FLOW-F FLOW-G VEL-J PLS01
* 0.59170 0.0 0.0 PLS01
* * * * *
* *****
* VOLUME 3 *****
* * * * *
* 0030000 NAME TYPE PLS01
* C003 TMDPVOL PLS01
* * * * *
* 0030101 AREA LEN VOL HZ VR ELV ROUGH HYD FE PLS01
* 1.7576-4 1.0 1.7576-4 0.0 90.0 1.0 0.0 0.0 11 PLS01
* * * * *
* 0030200 CTL TRIP ALPH NUME PLS01
* 3 PLS01
* * * * *
* 0030201 TIME PRESSURE TEMP PLS01
* 0.0 15.50+6 565.0 PLS01
* 0030202 15.3 12.50+6 593.1 PLS01
* 0030203 1000.0 12.50+6 593.1 PLS01
* * * * *
* *****
* VOLUME 4 *****
* * * * *
* 0040000 NAME TYPE PLS01
* C004 TMDPVOL PLS01
* * * * *
* 0040101 AREA LEN VOL HZ VR ELV ROUGH HYD FE PLS01
* 1.7576-4 1.0 1.7576-4 0.0 90.0 1.0 0.0 0.0 11 PLS01
* * * * *
* 0040200 CTL TRIP ALPH NUME PLS01
* 2 PLS01
* * * * *
* 0040201 TIME PRESSURE QUALITY PLS01
* 0.0 15.50+6 1.0-10 PLS01
* 0040202 15.3 12.50+6 1.0-10 PLS01
* 0040203 25.0 10.60+6 1.0-10 PLS01
* 0040204 60.0 9.25+6 1.0-10 PLS01
* 0040205 77.0 8.95+6 1.0-10 PLS01
* 0040206 124.0 8.45+6 1.0-10 PLS01
* 0040207 148.0 8.40+6 1.0-10 PLS01
* 0040208 167.0 8.15+6 1.0-10 PLS01
* 0040209 207.0 7.75+6 1.0-10 PLS01
* 0040210 239.0 7.25+6 1.0-10 PLS01

```

FILE = J3491.LSRSP2.DATA DATE 87/10/13(TUESDAY) TIME 16:16:21 PAGE 0003

FILE = J3491.LSRSP2.DATA DATE 87/10/13(TUESDAY) TIME 16:16:21 PAGE 0005 *VIVAF0*

```

* * * * *
* 0120000 NAME TYPE PLS01
* C012 TMDPJUN PLS01
* * * * *
* 0120101 FROM TO AREA PLS01
* 003000000 002000000 1.7576-4 PLS01
* * * * *
* 0120200 CTL PLS01
* 1 PLS01
* * * * *
* 0120201 TIME FLOW-F FLOW-G VEL-J PLS01
* 0.0 0.59170 0.0 0.0 PLS01
* 0120202 15.3 0.59170 0.0 0.0 PLS01
* 0120203 15.4 0.0 0.0 0.0 PLS01
* 0120204 1000.0 0.0 0.0 0.0 PLS01
* * * * *
* JUNCTION BETWEEN VOLUME 4 AND BRANCH 2 ( JUNCTION 13 )
* * * * *
* 0130000 NAME TYPE PLS01
* C013 TMDPJUN PLS01
* * * * *
* 0130101 FROM TO AREA PLS01
* 004000000 002000000 1.7576-4 PLS01
* * * * *
* 0130200 CTL PLS01
* 1 PLS01
* * * * *
* 0130201 TIME FLOW-F FLOW-G VEL-J PLS01
* 0.0 0.0 0.0 0.0 PLS01
* 0130202 15.2 0.0 0.0 0.0 PLS01
* 0130203 15.3 0.59170 0.59170-10 0.0 PLS01
* 0130204 1000.0 0.59170 0.59170-10 0.0 PLS01
* * * * *
* JUNCTION BETWEEN VOLUME 1 AND VOLUME 5 ( JUNCTION 14 )
* * * * *
* 0140000 NAME TYPE PLS01
* C014 SNGLJUN PLS01
* * * * *
* 0140101 FROM TO AREA FLOS RLOS CAHS SUBC TWOC PLS01
* 005000000 001010000 1.7576-4 0.0 0.0 0000 1.0 1.0 PLS01
* * * * *
* 0140201 CTL FLOW-F FLOW-G VEL-J PLS01
* 1 -0.59170 0.0 0.0 PLS01
* * * * *
* AVERAGE POWER CHANNEL HEAT STRUCTURE
* * * * *

```

FILE = J3491.LSRSP2.DATA DATE 87/10/13(TUESDAY) TIME 16:16:21 PAGE 0005

FILE = J3491.LSR5P2.DATA DATE 87/10/13(TUESDAY) TIME 16:16:21 PAGE 0006 *VIVAP0*

```

*****
* NH NP TYPE S-FLG L-COR POLS01
* 10010000 1 9 2 1 0.0 POLS01
* LOC-F MESH-F POLS01
* 10010100 0 1 POLS01
* NO ITV R-COR NO ITV R-COR NO ITV R-COR
* 10010101 3 0.00200 , 1 0.00260 , 1 0.00375 , POLS01
* 10010102 3 0.00475 POLS01
* CMP NO CMP NO CMP NO CMP NO
* 10010201 1 3 , 2 4 , 3 5 , 4 8 POLS01
* SOURCE 0.0 3 , 1.0 4 , 0.0 5 , 0.0 8 POLS01
* FLG 0 POLS01
* TEMP NP POLS01
* 10010401 617.7 9 POLS01
* ***** LEFT ***** POLS01
* B.V. INC BCT A-C AREA NH
* 10010501 0 0 0 0 0.0 1 POLS01
* ***** RIGHT ***** POLS01
* B.V. INC BCT A-C AREA NH
* 10010601 001010000 0 1 0 1.3654-2 1 POLS01
* TYPE IS MULTI L-D-H R-D-H NH
* 10010701 900 0.30699 0.0 0.0 1 POLS01
* ***** LEFT ***** POLS01
* CHF HYD HEQ CHAN-L NH
* 10010801 0 0.0 0.0 0.0 1 POLS01
* ***** RIGHT ***** POLS01
* CHF HYD HEQ CHAN-L NH
* 10010901 0 0.011778 0.011778 0.4575 1 POLS01
* *****
* HIGH POWER CHANNEL HEAT STRUCTURE
* *****
* NH NP TYPE S-FLG L-COR POLS01
* 10020000 1 9 2 1 0.0 POLS01
* LOC-F MESH-F POLS01
*****

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FILE = J3491.LSR5P2.DATA DATE 87/10/13(TUESDAY) TIME 16:16:21 PAGE 0006

FILE = J3491.LSR5P2.DATA DATE 87/10/13(TUESDAY) TIME 16:16:21 PAGE 0007 *VIVAPD*

```

10020100 0010 POLS01 *00032300
* FLG POLS01 *00033300
10020400 0010 POLS01 *00044300
***** LEFT ***** POLS01 *00049300
* POLS01 *00050300
* B.V. INC BCT A-C AREA NH POLS01 *00051300
10020501 0 0 0 0.0 1 POLS01 *00052300
***** RIGHT ***** POLS01 *00053300
* POLS01 *00054300
* B.V. INC BCT A-C AREA NH POLS01 *00055300
10020601 001010000 0 1 0 1.3654-2 1 POLS01 *00056300
* POLS01 *00057300
* TYPE IS MULTI L-D-H R-D-H NH POLS01 *00058300
10020701 900 0.69301 0.0 0.0 1 POLS01 *00059300
* POLS01 *00060300
***** LEFT ***** POLS01 *00061300
* POLS01 *00062300
* CHF HYD HEQ CHAN-L NH POLS01 *00063300
10020801 0 0.0 0.0 0.0 1 POLS01 *00064300
* POLS01 *00065300
***** RIGHT ***** POLS01 *00066300
* CHF HYD HEQ CHAN-L NH POLS01 *00067300
10020901 0 0.011778 0.011778 0.4575 1 POLS01 *00068300
* POLS01 *00069300
***** HEAT STRUCTURE THERMAL PROPERTY DATA ***** POLS01 *00070300
***** POLS01 *00071300
***** POLS01 *00072300
***** POLS01 *00073300
***** POLS01 *00168700
***** POLS01 *00168800
***** POLS01 *00168900
***** POLS01 *00169000
***** POLS01 *00169010
***** POLS01 *00169100
***** POLS01 *00169200
***** POLS01 *00169210
***** POLS01 *00169300
***** POLS01 *00169310
***** POLS01 *00169400
***** POLS01 *00169410
***** POLS01 *00169500
***** POLS01 *00169510
***** POLS01 *00169600
***** POLS01 *00169800
***** POLS01 *00169800
***** POLS01 *00169900
***** POLS01 *00170000
***** POLS01 *00170200
***** POLS01 *00170300
***** POLS01 *00170400
***** POLS01 *00170500
***** POLS01 *00170600
***** POLS01 *00170600
***** POLS01 *00170700
***** POLS01 *00170800
***** POLS01 *00170800

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FILE = J3491.LSR5P2.DATA DATE 87/10/13(TUESDAY) TIME 16:16:21 PAGE 0007

FILE = J3491.LSR5P2.DATA DATE 87/10/13(TUESDAY) TIME 16:16:21 PAGE 0008 *VIVAPO*

```

*NICHRROME
*0100201 273.15 1473.15 6.1988 0.015933 0.0 0.0 0.0 0.0 273.15 P0LS01
*0100201 273.15 3473.15 6.1988 0.015933 0.0 0.0 0.0 0.0 273.15 P0LS01
*
* MGO
*0100301 273.15 1273.15 1.1049 0.0 0.0 0.0 0.0 0.0 273.15 P0LS01
*0100301 273.15 3473.15 1.1049 0.0 0.0 0.0 0.0 0.0 273.15 P0LS01
*0100301 334.15 1.3142 443.15 2.3493 554.15 3.9309 P0LS01
*0100302 3473.15 3.9309 P0LS01
*
* INCONEL600
*0100401 273.15 1173.15 13.956 0.016747 0.0 0.0 0.0 0.0 273.15 P0LS01
*0100401 273.15 3473.15 13.956 0.016747 0.0 0.0 0.0 0.0 273.15 P0LS01
*
*****
***** VOLUMETRIC HEAT CAPACITY (J/M3K) *****
*
* AL203
*0100151 373.15 3.0246+6 473.15 3.5751+6 673.15 4.0014+6 P0LS01
*0100152 873.15 4.2959+6 1073.15 4.5106+6 1273.15 4.6649+6 P0LS01
*0100153 1473.15 4.7732+6 P0LS01
*0100153 1473.15 4.7732+6 3473.15 4.7732+6 P0LS01
*
* NICHRROME
*0100251 273.15 1473.15 3.1058+6 2.0775+3 0.0 0.0 0.0 0.0 273.15 P0LS01
*0100251 273.15 3473.15 3.1058+6 2.0775+3 0.0 0.0 0.0 0.0 273.15 P0LS01
*
* MGO
*0100351 273.15 1173.15 2.8723+6 0.97658+3 0.0 0.0 0.0 0.0 273.15 P0LS01
*0100351 273.15 3473.15 2.8723+6 0.97658+3 0.0 0.0 0.0 0.0 273.15 P0LS01
*
* INCONEL600
*0100451 273.15 1373.15 3.7061+6 1.9237+3 0.0 0.0 0.0 0.0 273.15 P0LS01
*0100451 273.15 3473.15 3.7061+6 1.9237+3 0.0 0.0 0.0 0.0 273.15 P0LS01
*
*****
***** POWER TRANSIENT DATA *****
*****
*
* 20290000 T TYPE TRIP F1 F2
POWER 501 1.0 26.886+3
*
* BELOW IS HEAT TRANSFER RATE IN PWR
*
* TIME R POWER
0.0 1.0
20290001 1.0 0.875012
20290002 1.5 0.696449
20290003 2.0 0.420201
20290004 3.0 0.164270
20290005

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FILE = J3491.LSR5P2.DATA DATE 87/10/13(TUESDAY) TIME 16:16:21 PAGE 0008

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FILE = J3491.LSRSP2.DATA
DATE      87/10/13(TUESDAY)      TIME 16:16:21      PAGE 0009      *VIVAP0*
20290006      4.0      0.147012      *00195600      P0LS01
20290007      5.0      0.134465      *00195700      P0LS01
20290008      6.0      0.124604      *00195800      P0LS01
20290009      8.0      0.109953      *00195900      P0LS01
20290010     10.0     0.0996357     *00196000      P0LS01
20290011     15.0     0.0835672     *00196100      P0LS01
20290012     20.0     0.0739725     *00196200      P0LS01
20290013     30.0     0.0621879     *00196300      P0LS01
20290014     40.0     0.0547748     *00196400      P0LS01
20290015     50.0     0.0495318     *00196500      P0LS01
20290016     60.0     0.0456000     *00196600      P0LS01
20290017     80.0     0.0401409     *00196700      P0LS01
20290018    100.0    0.0366196     *00196800      P0LS01
20290019    150.0    0.0318209     *00196900      P0LS01
20290020    200.0    0.0294117     *00197000      P0LS01
20290021    300.0    0.0268382     *00200101      P0LS01
20290022    400.0    0.0253218     *00200102      P0LS01
20290023    500.0    0.0242242     *00200103      P0LS01
20290024    600.0    0.0233447     *00200104      P0LS01
20290025    800.0    0.0219527     *00200105      P0LS01
20290026   1000.0   0.0208547     *00200106      P0LS01
*
*****
*00200122      P0LS01
*00362400      P0LS01
*00364200      P0LS01

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