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RE-ANALYSIS OF CSNI STANDARD PROBLEM NO.8

December 1981

Shinobu SASAKI and Fumimasa ARAYA

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Japan Atomic Energy Research Institute

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Re-analysis of CSNI Standard Problem No.8

Shinobu SASAKI and Fumimasa ARAYA
Division of Reactor Safety Evaluation,
Tokai Research Establishment, JAERI

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This report presents the results of computer runs which carried out with the use of ALARM-P1 code. The object of analyses is the Semiscale S-06-3 experiment accepted as the CSNI International Standard Problem 8. According to the preliminary results reported before, the agreement between ALARM-P1 and this experiment was very poor for the key parameters such as the break flow or fuel cladding surface temperature. Hence, much effort has been made to improve the disagreement.

Through the re-examination of both the code and input-data, the agreement between the calculated and measured results for key parameters has been much better than that gained in the foregoing test run.

Keywords: Semiscale Test, Blowdown, Rewet, Heat Transfer Mode,
Subcooled Critical Flow, International Standard Problem

CSNI 標準問題No.8 の再解析

日本原子力研究所東海研究所安全解析部

佐々木 忍・新谷 文将

(1981年11月20日受理)

本報は、計算コードALARM-P1を用いて行なったセミスケールS-06-3実験に基づくCSNI国際標準問題No.8の再解析の結果を示す。

以前に報告された解析においては、ALARM-P1と実験値との比較を行なうと破断流量や炉心表面温度といった主要パラメータに対して十分な結果が得られなかった。そこで本解析では、これらのパラメータ改善に向けられた。

予備解析から見出された結論に基づき、入力データと計算コード双方の問題点を調査し、再び計算を行なった結果、炉心表面温度、破断流量等は大きく改善され、実験データをかなり正確に再現した。

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1. Introduction

An improved analysis of the Semiscale S-06-3 test was completed using the ALARM-P1 and described in this report. This experiment was designed to duplicate as closely as possible the LOFT nuclear test L2-3. The experiment conducted on May 1977 has been selected as the CSNI International Standard Problem No.8 (ISP8). A preliminary calculation for this exercise was already submitted from Japan to NEA-CSNI (Nuclear Energy Agency-Committee on Safety of Nuclear Installations).^{(1)*}

The blowdown heat transfer test S-06-3 was executed from the initial conditions of 15768 kPa and 598 °K (in the upper-plenum) with a core power of 1.004 MW and simulated a 200 % double-ended offset shear in the cold leg. ECC (Emergency Core Cooling) water was only injected into the intact loop cold leg from HPIS, LPIS (High Pressure Injection System, Low Pressure Injection System) and accumulator. The specific purpose of this experiment was to evaluate the core heat transfer phenomena at the intermediate power.

The results previously submitted to CSNI had included significant disagreements with the experimental data. Based on this experience, efforts have been made to improve the analytical results, by correcting errors and inadequacies in the computer code ALARM-P1, which was used in the previous and present analysis, as well as revising the input data set. Though the experiment covered from blowdown to refill-reflood phase of transient, both previous and present analyses by ALARM-P1 covered only the blowdown portion (0-40 seconds), since this code was originally designed to analyse only the blowdown phase.

Analytical results were compared with selected pertinent thermal-hydraulic data obtained from the experiment⁽²⁾, being documented in this

*) Number in bracket designates reference

report with a discussion of modelling changes and corrections of input data. As seen in the following section, the discharge flow or the clad surface temperature response for low-powered rods were excellently assessed in the current runs. However, several parameters were still out of the agreement with the measured data. Using useful information obtained from the current analysis, they are expected to be improved much better by means of the refinements of the analytical methodology and more reasonable input data.

An outline relative to the Semiscale Mod-1 system is given in the Figure 1 and 2. Figure 3 represents the noding scheme of this facility which is the same as that of the previous calculation. In addition, the geometrical data and initial conditions are provided in the Tables 1 through 3.

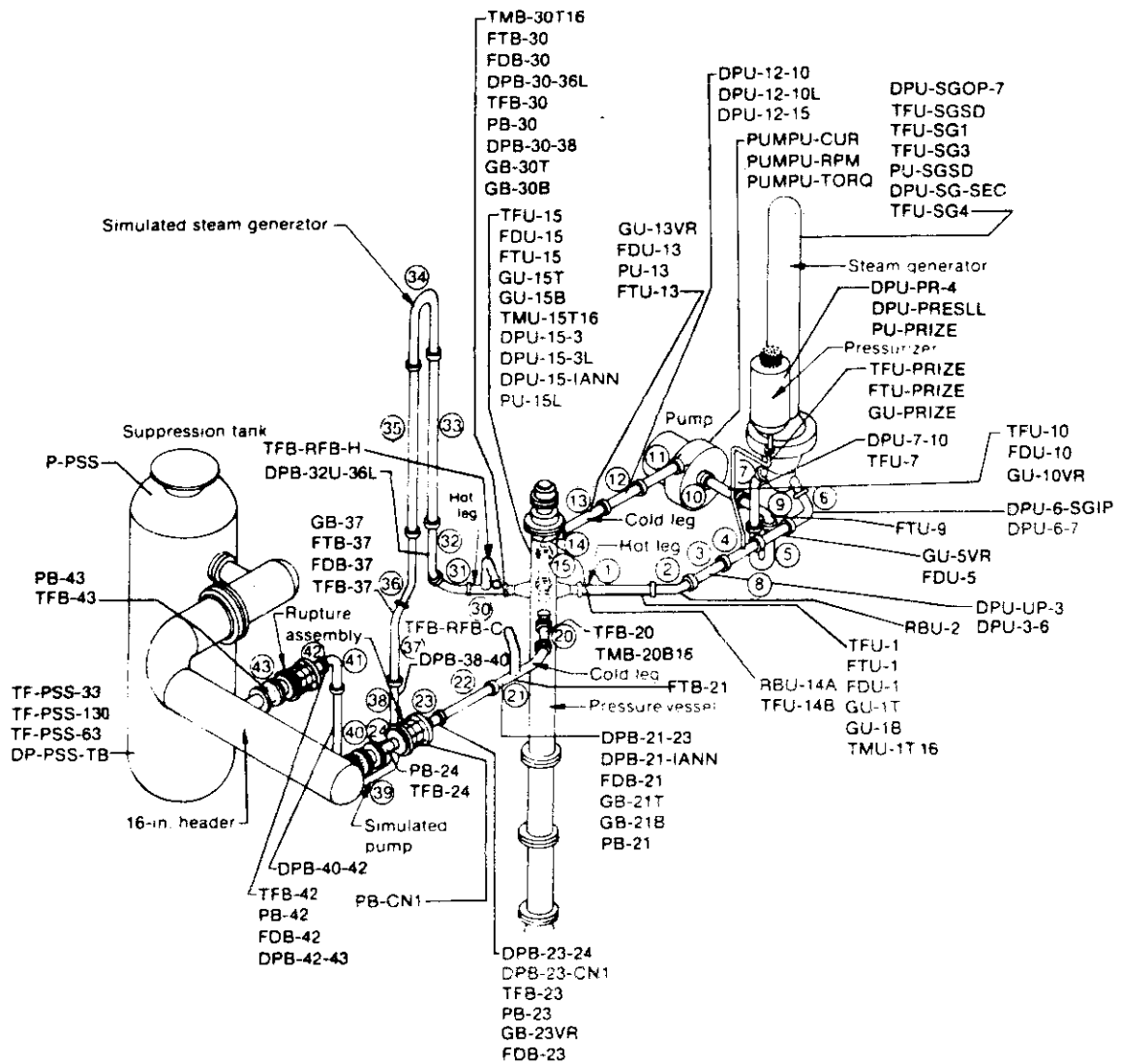


Fig.1 Semiscale Mod-1 system and instrumentation for cold leg break configuration -- isometric.

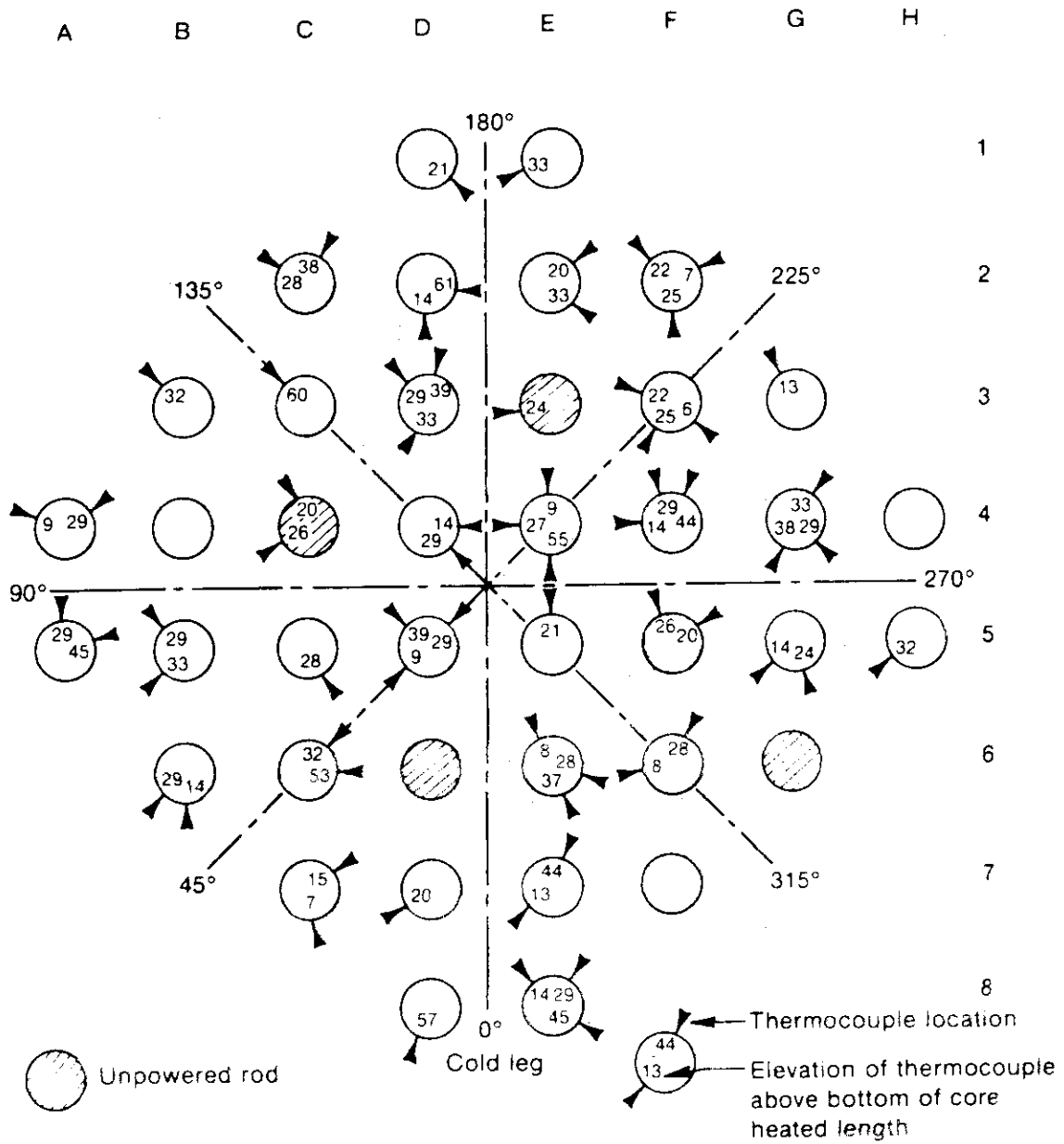


Fig.2 Semiscale Mod-1 heated core Lay-out.

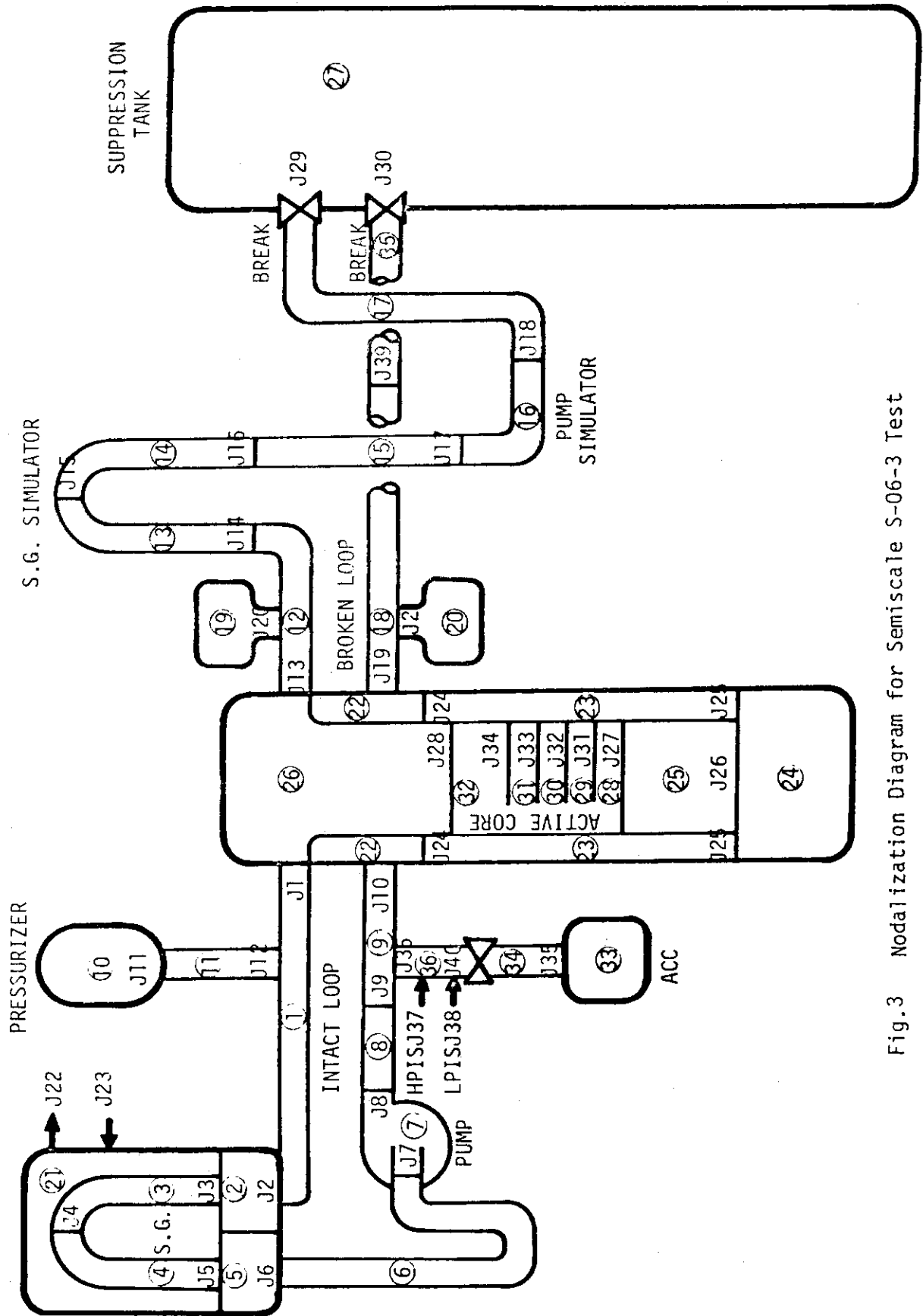


Fig.3 Nodalization Diagram for Semiscale S-06-3 Test

Table 1 Geometrical Description of Semiscale S-06-3 Model Control Volumes

<u>Control volume</u>	<u>Description</u>	<u>Volume(m³)</u>	<u>Flow Area(m²)</u>
1	Intact loop hot leg piping	0.01082	0.00349
2	Steam Generator inlet plenum	0.00963	0.01984
3	Steam generator U-tubes	0.01140	0.00442
4	Steam generator U-tubes	0.01140	0.00442
5	Steam generator outlet plenum	0.00963	0.01984
6	Pump suction leg	0.01018	0.00349
7	Primary coolant pump	0.00408	0.00349
8	Cold leg piping	0.00425	0.00349
9	Cold leg piping	0.00425	0.00349
10	Pressurizer	0.02741	0.02466
11	Pressurizer surge line	0.00037	4.3E-5
12	Broken loop hot leg piping	0.00315	0.00349
13	S.G. simulator	0.00852	0.00374
14	S.G. simulator	0.00852	0.00374
15	Outlet piping from S.G. simulator	0.00252	0.00158
16	Pump simulator	0.00147	0.00198
17	Break node	0.00227	0.00145
18	Broken loop cold leg	0.00461	0.00349
19	Reflood assist by-pass piping	0.00538	0.00349
20	Reflood assist by-pass piping	0.00640	0.00349
21	Secondary side of steam generator	0.19820	0.04255
22	Upper annular region of the vessel inlet region	0.00504	0.00548
23	Downcomer region	0.02183	0.00534
24	Lower plenum	0.02161	0.00623
25	Turbine flowmeter housing	0.00371	0.00713
26	Upper plenum	0.02620	0.00713
27	Pressure Suppression tank	3.17549	0.70205

Table 1 (continued)

<u>Control volume</u>	<u>Description</u>	<u>Volume(m³)</u>	<u>Flow Area(m²)</u>
28	Active core region	0.00137	0.00492
29	Active core region	0.00137	0.00492
30	Active core region	0.00137	0.00492
31	Active core region	0.00137	0.00492
32	Active core region	0.00274	0.00492
33	ECCS-accumulator	0.1145	0.03812
34	ECCS-injection line	0.00244	0.00046
35	Break node	0.00161	0.00349
36	ECCS-injection line	0.00244	0.00046

Table 2 Junction Description of ALARM-PI Model

Junction	Volumes		Flow Area (m ²)	Form Loss Coefficients			
	(From)	(To)		Forward		Reverse	
				(Run 1)	(Run 2,3)	(Run 1)	(Run 2,3)
1	26	1	0.00183	1.0E-6	0.0*	1.0E-6	0.0*
2	1	2	0.00349	0.0	6.198	0.0	6.198
3	2	3	0.00442	0.0	0.0	0.0	0.0
4	3	4	0.00442	0.0	0.0	0.0	0.0
5	4	5	0.00442	0.0	0.0	0.0	0.0
6	5	6	0.00349	0.0	15.4395	0.0	15.4395
7	6	7	0.00349	5.3	5.3	4.86	4.86
8	7	8	0.00349	1.65	1.65	1.65	1.65
9	8	9	0.00349	0.0	0.467	0.0	0.467
10	9	22	0.00183	1.0E-6	0.658	1.0E-6	1.466
11	10	11	4.3E-5	10.8	10.8	10.8	10.8
12	11	1	4.3E-5	0.0	0.0	0.0	0.0
13	26	12	0.00183	0.677051	0.677051	1.2144	1.2144
14	12	13	0.00024	1.41181	1.41181	1.41146	1.41146
15	13	14	0.00349	285.435	285.435	285.435	285.435
16	14	15	0.00024	1.40405	1.40405	1.41583	1.41583
17	15	16	0.00024	0.844137	0.844137	1.54353	1.54353
18	16	17	0.00024	12.8823	12.8823	12.438	12.438
19	22	18	0.00183	0.677051	0.677051	1.21442	1.21442
20	19	12	0.00349	0.0	0.0	0.0	0.0
21	20	18	0.00349	0.0	0.0	0.0	0.0
22	21	0	0.00203	0.0	0.0	0.0	0.0
23	0	21	0.00113	0.0	0.0	0.0	0.0
24	22	23	0.00534	0.0	3.9706E-2	0.0	2.2542E-3
25	23	24	0.00534	0.0	4.6518E-2	0.0	0.1465
26	24	25	0.00713	0.0	19.569	0.0	19.569
27	25	28	0.00492	0.0	10.5899	0.0	10.5898
28	32	26	0.00492	0.0	7.2754	0.0	7.2754
29	17	27	0.00024	1.00777	1.00777	1.13360	1.13360
30	35	27	0.00024	1.38245	1.38245	1.15464	1.15464
31	28	29	0.00492	0.0	0.0	0.0	0.0
32	29	30	0.00492	0.0	0.0	0.0	0.0

Table 2 (continued)

<u>Junction</u>	<u>Volumes</u>		<u>Flow Area</u> (m ²)	<u>Form Loss Coefficients</u>			
	<u>(From)</u>	<u>(To)</u>		<u>Forward</u>		<u>Reverse</u>	
				(Run 1)	(Run 2,3)	(Run 1)	(Run 2,3)
33	30	31	0.00492	0.0	0.0	0.0	0.0
34	31	32	0.00492	0.0	0.0	0.0	0.0
35	33	34	0.00046	0.0	71.095	0.0	1.0E-6
36	36	9	0.00046	284.38	71.095	1.0E-6	1.0E-6
37	0	36	0.00015	0.0	0.0	0.0	0.0
38	0	36	0.00028	0.0	0.0	0.0	0.0
39	18	35	0.00349	1.0E-10	1.0E-10	1.0E-10	1.0E-10
40	34	36	0.00046	0.0	142.19	0.0	1.0E-6

*) "0.0" denotes automatic calculation option incorporated in ALARM-PI code

Table 3 Initial Conditions

<u>Pressure (kg/cm²)</u>		
Upper-plenum		160.8298
Pressurizer		160.6254
Steam Generator Secondary		Sat. at 284.65 °C
Accumulator		45.007
Pressure suppression		2.482
<u>Fluid Temperature (°C)</u>		
Core inlet fluid temperature		290.889
Core outlet fluid temperature		326.444
Broken loop cold leg		288.80
Broken loop hot leg		322.96
Broken loop hot leg break node		316.97
Accumulator tank		27.778
Pressure suppression		16.35
Feed water supply system		204.8
HPIS, LPIS		27.778
Reflood bypass line	Hot leg side	315.85
	Cold leg side	288.85
<u>ECC Injection</u>		
Accumulator:		
Water volume		0.04958 (m ³)
Gas volume		0.06492 (m ³)
Initiation pressure		43.1914 (kg/cm ²)
HPIS:		
Injection initiation		126.5823 (kg/cm ²)
Injection rate	0.0149 (kg/s) (0.0 < t < 30.0)	
	0.0817 (kg/s) (30.001 ≤ t ≤ 50.0)	
LPIS:		
Injection initiation		17.58 (kg/cm ²)
Injection rate	0.299 (kg/s) (0 ≤ t ≤ 50.0)	
	(t : time after tripping)	
<u>Others</u>		
Core power		1.0058 (MW)
Core flow rate		4.899 (kg/s)
Primary pump speed		1618.9 (rpm)
Pressurizer liquid level		0.062547 (m)
Steam generator liquid level		2.9 (m)

Table 4 Parameters Requested for ISP8 Comparisons

<u>Required Parameters</u>	<u>Location</u>
<u>(1) Pressures (kPa)</u>	
PU-PRIZE	Pressurizer pressure
PB-42	Upstream of break nozzle (pump side)
PB-23	Upstream of break nozzle (reactor vessel side)
PV-UP+10	Upper plenum
PU-ACC	Intact loop accumulator
PU-SGSD	Steam generator secondary side
<u>(2) Differential pressures (kPa)</u>	
DPU-12-10	Across pump
DPU-7-10	Across pump suction
DPB-32U-36L	Across simulated steam generator
DPB-38-40	Across simulated pump
DPV-LP-UP	Across core
<u>(3) Flow rates (KG/s, l/s)</u>	
FTV-COREIN	Core inlet flow
FDB-42, GB-42VR	Break nozzle flow (pump side)
FDB-23, GB-23VR	Break nozzle flow (reactor vessel side)
FTU-15	Intact loop cold leg flow
FTU-PRIZE	Pressurizer surge line flow
FTU-LPIS	Intact loop LPIS flow
FTU-HPIS	Intact loop HPIS flow
FTU-ACC	Intact loop accumulator flow
FDU-10, GU-10	Mass flow rate in spool 10
<u>(4) Fluid density (kg/m³)</u>	
GB-42VR	Break volume density (pump side)
GB-23VR	Break volume density (reactor vessel side)
GU-15C	Intact loop cold leg density
GU-10	Pump inlet density
GVCOR-150HZ	Core inlet density
GVI61-192D	Lower plenum density
<u>(5) Fluid temperature (°K)</u>	
TFU-PRIZE	Pressurizer surge line fluid temperature
TFB-23	Fluid temperature upstream of break
TFV-UP+13	Fluid temperature in upper plenum
<u>(6) Metal temperatures (°K)</u>	
Rod surface temperatures on average rod (7.59 KW/ft)	Elevations of 8", 14", 28", and 39" above bottom of heated length

Table 4 (continued)

<u>Required Parameters</u>	<u>Location</u>
(7) <u>Quality and heat transfer coefficient ($MW/m^2 \cdot K$)</u>	Same elevations in core corresponding to the thermocouples for the heater rod temperatures
(8) <u>Mass Inventory (kg)</u> FDB-23, FDB-42	Integrated mass leaving the system through break junctions

Table 5 Description of Checkout Runs

<p>RUN 1</p> <p>Physical Time 26.6 sec</p> <p>CPU Time 8.3 hr</p>	<p>Initial results for CSNI Exercise</p> <p>Findings:</p> <ol style="list-style-type: none"> 1. Poor Prediction for Subcooled Critical Flow 2. Underprediction of Clad Surface Temperature for Low-Powered Rods 3. Others
<p>RUN 2</p> <p>Physical Time 28.7 sec</p> <p>CPU Time 9.9 hr</p>	<p>Post-test Calculation (NO.1)</p> <p>Principal Items of Checkout Works Performed on the Basis of the Drawn Conclusions of RUN 1</p> <p><u>Concerning Input-data</u></p> <ol style="list-style-type: none"> 1. An increase of Flow Length (in Pump Simulator) and Change of Form-loss Coefficient (K-value) Across the Pump Simulator. 2. To Tune up the Fill-Leak Data Table for Steam Generator Secondary Side Behaviors 3. Correction of the Gas Volume in the Accumulator Tank 4. Junction Level Modification at the Pressurizer Outlet <p><u>Concerning Code Model</u></p> <ol style="list-style-type: none"> 5. Modification in the Temperature Conversion ($^{\circ}\text{C} \leftrightarrow ^{\circ}\text{F}$) 6. Assumption of a Constant speed prior to Pump Tripping
<p>RUN 3</p> <p>Physical Time 26.4 sec</p> <p>CPU Time 11.2 hr</p>	<p>Post-test calculation (NO.2)</p> <p><u>Concerning Input-data</u></p> <ol style="list-style-type: none"> 1. Correction of Heat Transfer Area and Slab Volumes in the Core Region 2. Change of Form-loss Coefficient at the Pressurizer Surge Line <p><u>Concerning Code Model</u></p> <ol style="list-style-type: none"> 3. Application of Contraction Coefficient C_D in the Subcooled Critical Flow and Interpolation method in the Transition Region between the Zaloudek Flow at Zero Quality and Moody Choked Flow at 2 % Quality 4. Replacement of Berenson Model with Modified Bromley's at the Pool Film Boiling Heat Transfer Mode 5. Removal of Miscoding in the Routine of Calculating the Junction Enthalpy

2. Results Presentation and Discussions

The results of the present runs are shown in the Figure 4 through 45, where comparisons are made and discussed with the experimental and previous analytical results. However, the comparisons with experimental data were made with only those which had been specified by CSNI (see Table 4).

The present analysis consists of two runs, thus including the previous one, three runs were made for this ISP8. These runs are shown in the Table 5 together with brief explanations. As indicated in the Table 5, RUN 1 is the one which was submitted to CSNI and referred to as the base case in the following discussion, while RUN 2 and 3 are the post test calculations with various improvements based on the experiences of RUN 1. In the comparison plot, the ALARM-P1 computation is indicated by the A's, while the Semiscale S-06-3 data by the function codes which were defined in the previous report⁽¹⁾. The post test calculations were conducted on FACOM-230-75 machine by using the ALARM-P1 (Mod 2 / Version 2), being terminated at approximately 26~29 seconds into the transient due to the occurrence of the reverse flow at the break plane. A complete listing of the input data in the post test calculations is given in Appendices 1 to 2.

Figure 4 shows the comparison of the calculated and the measured differential pressure across the simulated pump. Form the first item of modification for the RUN 2 indicated in the Table 5, an increase of the flow length (in the simulated pump volume) led to the good agreement with the observed data. In addition, the form-loss coefficient (K-factor) was adjusted lest the residual friction term is predominant in the total ΔP . However, in RUN 3 the deviation from the measured data became somewhat larger during the latter portion of the comparison period, of which the cause has not been fully identified. In general, the calculated pressure

difference dropped rapidly in consequence of ECC water injection beyond 20 seconds while that indication was not clearly seen in the experimental data.

The pressure difference across the simulated steam generator is much smaller than that across the simulated pump (see Figure 5). This implies that the pump simulator resistance was very high compared with that in the simulated steam generator.

As the result of modification to the fill-leak input data, the steam generator secondary pressure fell closer to the experimental data as seen in the Figure 6. At the present analysis, a feed water reservoir temperature was assumed to be 73.6 degrees from the hand calculations of the energy balance since it was not provide in the initial conditions.

A slight increase in the pressure appearing in RUN-2 and 3, at the early period of the blowdown, suggests to need a further examination toward the improvement. Heat flux reversal occurred at 16 seconds in the calculation (RUN 2).

The accumulator pressure history was much better reproduced in RUN 2 than in RUN 1 (see Figure 7). This is due to a change of the gas volume in the tank. It was reduced to 0.0346 (m³) from 0.0649 (m³).

The model of the accumulator injection was slightly modified in RUN 2 and 3. In these runs the onset of injection was controlled by time (18.2 seconds) while in RUN 1 it was controlled by the pressure. The injection rate is highly sensitive to the system pressure which was calculated slightly lower than the measurement, hence the calculated injection rate was significantly higher (see Figure 8).

Due to a homogeneous equilibrium model of the ALARM-P1, an unphysically severe transient was calculated when subcooled accumulator water was injected. Various attempts have been made to avoid this difficulty,

however, so far not successful.

In the Figure 9 to 11, the pressurizer analysis was made with the use of new junction data. Figure 9 shows the pressure history comparison in the pressurizer vessel. While the initial depressurization rate up to a steam discharge was relatively close to the experimental data, the computed pressure in RUN 1 indicates emptying to occur at approximately 13 seconds compared to 8 seconds in the measured data. Since emptying time is highly dependent upon the liquid level (more exactly speaking, the depth of the surge line inlet below the surface of the water) in the pressurizer, the effort was directed to modify the geometrical junction elevation at surge line entrance. Although the liquid level in the pressurizer can be tuned up by changing the bubble velocity, this method was not used here. Additionally, for RUN 3, a more reasonable K-factor through the surge line was given. As a result, the ALARM-PI result approached the Semiscale data more closely.

Figure 10 compares the calculated fluid temperature in the surge line to the test data. The fluid in this volume was initially subcooled, then reaching saturation at about 8 seconds in the observation. On the other hand, the computation showed the saturation around one seconds.

This difference is due to the modelling of the pressurizer. The figure explains that significant subcooled water was present near the pressurizer bottom. Contrary to this, the computation was assumed to be saturated prior to a rupture because of having no regard for the partial existence of the subcooled water in the two phases mixture. At the later portion of the transient, the fluid temperature obtained from the measured data shows to be superheated (e.g., $P = 1000$ kPa, $T = 518$ °K at 36 seconds). No explanation for the discrepancy after 14 seconds from the break has so far been given.

Similarly, it is noticed that in the surge line flow, the difference in emptying time was reflected in this flow behavior (see Figure 11).

Admitting that the volumetric flow rate was slightly over-calculated up to 8 seconds from the reason stated above, then the result of RUN 2 was nearly identical to the measurement until approximately 20 seconds.

From RUN 3, the cladding surface temperature histories for the low-powered core heater rods are shown in the Figures 12 to 15 together with the data measured by the thermocouples. In the current analysis, the core was simulated by a single-average channel, where the active heater pins were changed from forty into thirty-six according to the data report⁽²⁾.

Looking at these figures, the effect on the four un-powered rods removed was found to be significant. By means of modification of the heat transfer area in the core region, the ALARM-P1 post-test analysis was excellently improved so that the clad temperatures were within the spread in the experimental data except elevation 8". Through all the test runs, the predicted time of DNB, as indicated by a sharp temperature rise, was slightly earlier than the measured, resulting in an over-estimation of a peak cladding temperature.

In the Figure 12, the computed rod heat up rate falls down drastically around 8 seconds due to a rapid increase of heat transfer, which falls into the nucleate boiling mode from this time (see RUN 1 or 2 in the Figure 20). As seen in RUN 1 or 2 in the Figure 12, these two predictions were the furthest compared with the experimental data. An unrealistic rewet occurred at about 22.5 seconds due to the core flow reversal extended the difference further (RUN 1).

On the other hand, in RUN 3, a sharp rise in temperature up to about 8 seconds occurs in the mode 6 (Bromely correlation), then passing through the transition boiling with a temperature drop by 60 °K, the heat transfer

was calculated again using the correlation in the pool film boiling region (mode 6). So, the temperature decrease beyond 8 seconds was markedly arrested in contrast with RUN 1 or RUN 2. During the remainder of the transient (RUN 3), the heat transfer was in mode 8 (forced convection in superheated vapor). In the absence of this rewet around 8 seconds, the difference in the temperature would have appeared to be much smaller.

The pool film boiling Berenson correlation used for RUN 1 or RUN 2 was:

$$h = 0.425 \left[\frac{k_g^3 \rho_g (\rho_f - \rho_g) g h_{fg}}{\mu_g \Delta T_{sat} \sqrt{\frac{g_0 \sigma}{g(\rho_f - \rho_g)}}} \right]^{1/4}$$

For RUN 3, it was replaced by a modified Bromley's⁽⁴⁾

$$h = \frac{0.62}{\sqrt[4]{2\pi}} \left[\frac{k_g^3 \rho_g (\rho_f - \rho_g) g h_{fg}}{\mu_g \Delta T_{sat} \sqrt{\frac{g_0 \sigma}{g(\rho_f - \rho_f)}}} \right]^{1/4}$$

As seen in the figures of the heat transfer coefficient (see Figures 20 to 23) there was little difference between the two correlations mentioned above. For example, until 5 to 7.5 seconds in the Figure 20 the modified Bromley's model predicted a slightly lower coefficient than the Borenson's. For the core heater rods at elevation 39", DNB was calculated in RUN 3 at 1.8 seconds, while the test data experienced it later. Consequently the peak cladding temperature in this zone was conservatively predicted beyond the observed data (see Figure 15). The overall temperature profile, however, was calculated reasonably well at this level. Between 8" and 39", the predicted maximum clad surface temperatures were slightly high to the experimental data, but subsequently within the measured data scatter (see Figures 13 to 14).

For clad surface temperature curve shown, the reason why the calculated temperature was lower than the Semiscale data at the steady state is because: the thermocouples used in the experiment were located inside the composite sheath while the calculation was estimated at the fuel rod surface.

In the Figures 16 to 19, the behaviors of the fluid quality were influenced strongly by the core fluid flow direction. It suggests the core fluid conditions of RUN 3 were somewhat different from that of RUN 1 or RUN 2.

Figures 24 to 30 show the comparative results in the broken loop. Herein, it was scrutinized as to how the item 3 specified in RUN 3 was reflected in the computed results (see Table 5).

Apart from the calculated results made in RUN 3, the ALARM-P1 break flow through the cold leg produced the most significant disagreement with the measured data during the first 3.5 seconds of the transient because the discharge flow multiplier selected was too small. Thus, the predicted time of saturation was late. In order to reduce this disparity between the prediction and measurement, the analytical technique for RUN 3 was so extended that respective contraction coefficients were applied separately to the two different flow regions. Accordingly the cold leg break flow was obviously improved getting nearer the measured data in the trend as can be seen in the Figure 24.

The Zaloudek's critical flow formula used is as follows:

$$\text{mass flux } G_{\text{crit}} = C_z \sqrt{2g_c \rho (P - C_2 P_{\text{sat}})}$$

where $C_z \triangleq$ (Zaloudek experimental constant) \times (contraction coefficient)

$C_2 =$ a constant related to a bubble delay time

In the present analysis, arbitrary constant C_z and C_2 were assumed to be

0.6 and 0.4 respectively. By selecting these two parameters appropriately, the subcooled choked flow could approach the measured data more closely.

As can be seen in this experimental data, the identical transition from a subcooled flow into the two-phase flow is predicted distinctly. This change to saturation can be controlled by the transition quality, which was in the ALARM-PI model assumed to be 0.02. According to the reference⁽⁵⁾, it suggests this value is smaller than 0.02.

Although the present prediction for RUN 3 was greatly improved on the cold leg break flow, the corresponding pressure transient was underestimated (see Figure 25). There was an apparent paradox about the results gained from the pressure and the break flow. The cause of this disagreement is considered to occur from a wide variety of sources:

- i.e. (1) Low heat transfer in the core region.
(2) Incomplete break flow predictions that have something yet to be improved.
(3) Significant influence from the pressurizer or the steam generator.
(4) Ignorance of energy stored in the structure.
(5) Mixing effect of ECC water with the primary coolant.

At any rate it requires further examinations.

Figure 26 compares the broken loop cold leg density data with the calculated results. In case of RUN 3, the calculated density was somewhat reformed throughout the transient. The resulting generation time of void in the piping came near the experimental data. Beyond 20 seconds, the calculated behavior shows the presence of ECC water passing through the cold leg, while the measured data is delayed by 3~4 seconds.

In the Figure 27, the calculated fluid temperature was somewhat lower corresponding to the underpredicted pressure. Around 26 seconds, the result of RUN 3 differs with the observed data by 70 °K. A sudden anomaly

in temperature caused by a reverse flow from the containment resulted in the termination of computation.

The major results in the broken loop hot leg are demonstrated in the Figures 28 through 30. Unlike the cold leg, there were similar trends between the experimental and calculated values. For the RUN 3, the hot leg pressure and break flow were, in general, below the measured data during most of the transient (see Figures 28 and 29). Rather, the computed results obtained from RUN 1 or RUN 2 agreed with the S-06-3 data relatively well. Regarding the measured flow data, the calibration of the fluid flow is generally considered to contain a large extent of errors produced by the measurement of momentum flux and the fluid density. At the present stage, it suffices to assess the code ability, if the predicted flows followed the trends of the measured data.

Next, the comparisons between the predictions and the experiment in the pressure vessel are given in the Figures 31 through 36. The calculated upper-plenum pressure representative of the whole system pressure was considerably low. The pressure was underestimated by 500 kPa at 4 seconds, 750 kPa at 16 seconds and 1250 kPa at 20 seconds in RUN 3. At the last portion of the calculation, the divergence was enhanced by the mixing effect of ECC injection. As encountered in the break pressure presentation, a fast pressure decay should be checked on the basis of the possible reasons mentioned above.

The core inlet flow is illustrated in the Figure 32. In the RUN 3, it is strongly influenced by the high flow rate of the initial subcooled fluid, thereby showing a large negative flow after the rupture. The core inlet density for RUN 3 (see Figure 33) behaves differently from the other runs after 5 seconds. It was in the close agreement with the experimental value except for a spike caused by the high density fluid from the

lower-plenum.

An influence on the core flow reversal was more or less reflected in the RUN 3. Likely, the lower-plenum density for the RUN 3 (see Figure 34) showed a different trend compared with the others. The downcomer flow was perhaps responsible for such a faster reduction of density. The pressure difference across the core is presented in the Figure 35. The calculated results remains slightly positive near or at zero from 2.5 to 26 seconds, while the measured value remained negative throughout the transient. The difference between the two is under investigation.

Figure 36 shows the fluid temperature history in the upper-plenum. All the prediction decreased with time like that in the broken loop cold leg. Beyond approximately 10 seconds, the departure of the calculated fluid temperature from the measured data was enhanced particularly in RUN 3.

Figure 37 to 44 provide the comparison plot related to the system behaviors in the intact loop. The intact loop pump behavior prior to a coast-down in the post-test analysis was calculated under the assumption that an electrical torque is equal to a hydraulic one in order to keep the regular revolution during the blowdown. The pump characteristics was calculated using the single phase homologous curves. The frictional torque and the energy added to the fluid were neglected in the ALARM-P1 code. As can be seen in the Figure 41, the pump head began decreasing at about 7 seconds while pretty earlier in the prediction. The pump degradation exclusively depends on the faster system decompression. Large oscillations shown near the end of the computation are ascribable to the effect of the ECC water injection.

Parameters other than those identified so far were practically identical through three test runs. In the Figure 42, the fluid temperature in the accumulator line was recovered to a realistic value by mending the

computation logic of the junction enthalpy. With respect to HPIS and LPIS behaviors, these remained nearly unchanged. Finally for the RUN 3, a total mass accumulated in the suppression tank was somewhat overpredicted due to the high critical flow rate in the early portion of blowdown.

(see Figure 45)

3. Conclusions

The post-test analysis following the initial calculation for ISP8 was made with the use of the ALARM-P1 code. Several conclusions were drawn from the code-data comparisons. In the present analysis, the first target was successfully accomplished which was intended to improve behaviors of a few key parameters.

Some of results obtained were in good agreement with Semiscale S-06-3 test data. Defects discovered in the calculated results will be made up in further calculations. Findings were classified in the following.

(A) Improved Items

(1) Fuel cladding surface temperature

The temperature response for a low-powered zone was excellently improved by the severe degradation of the heat transfer.

Provided that more exact core hydraulic conditions were traced, the clad temperature at 8" elevation would have been adequately predicted. The difference between the Berenson and modified Bromley model was not significant.

(2) Discharge flow at early part of depressurization

The discharge flow through the cold leg was not complete, but the similarity between the calculated and measured result was exhibited to be much better than the initial trial. Furthermore, it was proved that the discharge flow has a large influence on the hydraulic and thermal response in the core region.

(B) Unsolved Items

(1) Underpredicted system pressure

In every case, the calculation underpredicted the experimental data during most of the transient.

(2) Early CHF prediction and rod surface rewetting

In general, the prediction of a core heater rod thermal response experienced early DNB, resulting in the overprediction of the clad temperatures. Therefore, it is required to fully investigate the capability of currently used CHF correlations. It should be noted that the occurrence of a rewetting at some of a low-powered zone

was predicted by the analysis as opposed to the S-06-3 experimental data.

(3) Pressurizer behavior

Some significant thermal stratification observed in the pressurizer vessel during the early period of the experiment was not sufficiently tracked by the code.

(4) Lower-plenum density and core differential pressure

The code-data comparisons about these two parameters were not good. From the measured curves in the lower-plenum, the effect of using two or more control volume is worthy investigating.

(5) Others

The present homogeneous equilibrium model (1V-1T) which causes an unphysically severe transient must be substituted by the more realistic models. The development is under way. Moreover, refinements for the critical flow models are expected to reproduce the accurate break flow rate over the every range of thermodynamical condition.

References

1. S. Sasaki and F. Araya, "An Analysis of CENI Standard Problem NO.8", JAERI-M 8746, March 1980.
2. B.L. Collins, et al., "Experimental Data Report for Semiscale Mod-1 Test S-06-3 (LOFT Counterpart Test)", NUREG/CR-025/TREE-1123, July 1978.
3. F.R. Zaloudek, "The Critical Flow of Hot Water through Short Tubes", HW-77594, May 1966.
4. RELAP4/MOD5: A computer Program for Transient Thermal-Hydraulic Analysis of Nuclear Reactor and Related Systems, User's Manual Volume 1 (p.75), ANCR-NUREG 1335, September 1976.
5. J.R. White, W.H. Grosh and C.D. Keeler, "Preliminary Post test Analysis of LOFT Loss-of-Coolant Experiment L2-2, Appendix B", LTR20 - 103, June 1979.

Acknowledgement

Much appreciation is expressed to Mr. K. Sato, Chief of Reactor Safety Code Development Laboratory who critically read a draft of the paper and made useful suggestions.

References

1. S. Sasaki and F. Araya, "An Analysis of CENI Standard Problem NO.8", JAERI-M 8746, March 1980.
2. B.L. Collins, et al., "Experimental Data Report for Semiscale Mod-1 Test S-06-3 (LOFT Counterpart Test)", NUREG/CR-025/TREE-1123, July 1978.
3. F.R. Zaloudek, "The Critical Flow of Hot Water through Short Tubes", HW-77594, May 1966.
4. RELAP4/MOD5: A computer Program for Transient Thermal-Hydraulic Analysis of Nuclear Reactor and Related Systems, User's Manual Volume 1 (p.75), ANCR-NUREG 1335, September 1976.
5. J.R. White, W.H. Grosh and C.D. Keeler, "Preliminary Post test Analysis of LOFT Loss-of-Coolant Experiment L2-2, Appendix B", LTR20 - 103, June 1979.

Acknowledgement

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COMPARISON OF SEMISCALE 5-06-3 DATA AND ALARM-P1 ANALYSES

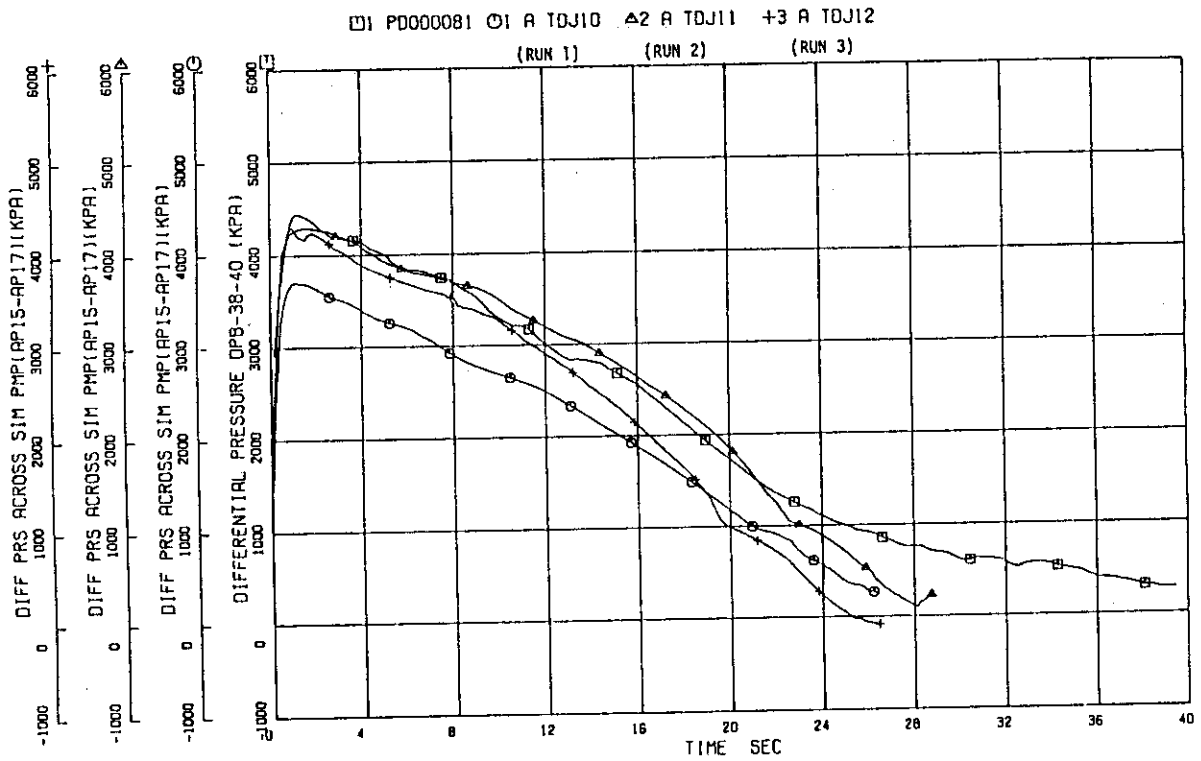


Figure 4 Pressure Difference Across the Simulated Pump (DPB-38-40)

COMPARISON OF SEMISCALE 5-06-3 DATA AND ALARM-P1 ANALYSES

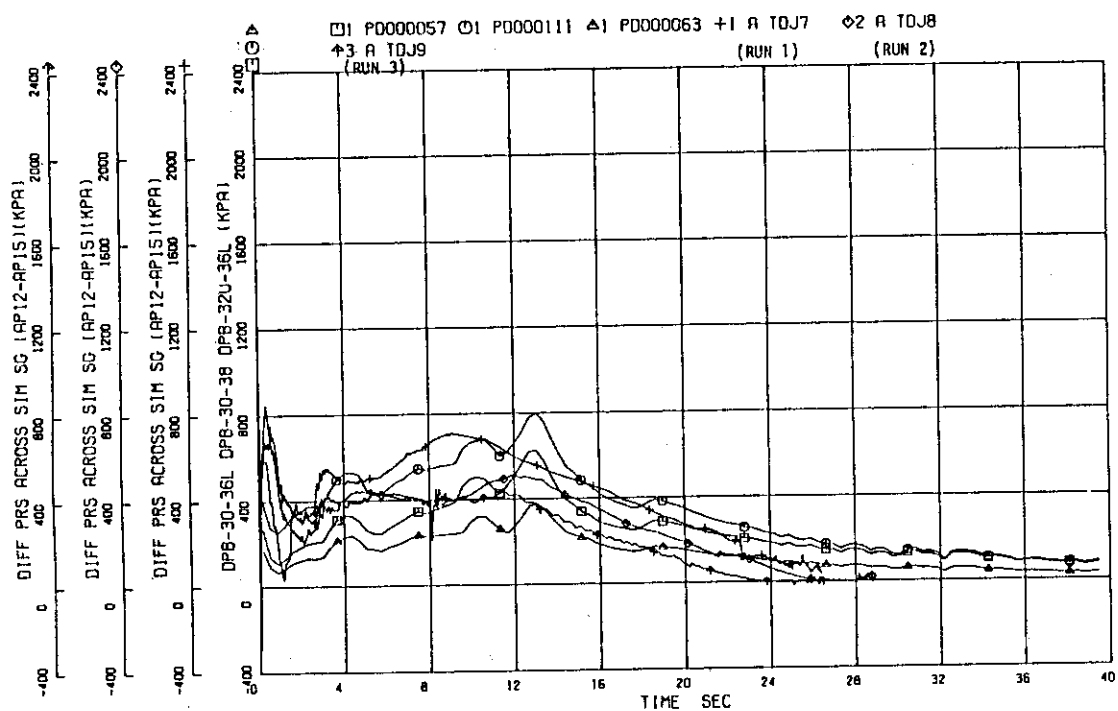


Figure 5 Pressure Difference Across the Simulated Steam Generator (DPB-32U-36L, DPB-30-36L, DPB-30-38)

COMPARISON OF SEMISCALE S-06-3 DATA AND ALARM-P1 ANALYSES

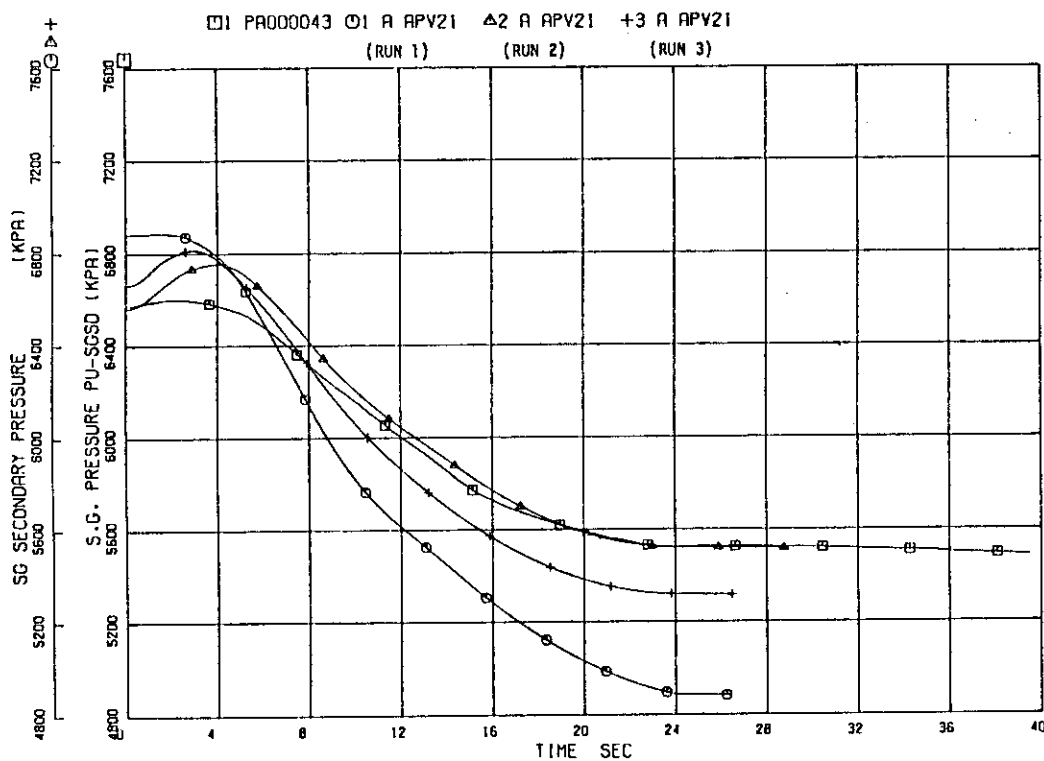


Figure 6 Pressure History in the Steam Generator Secondary System (PU-SGSD)

COMPARISON OF SEMISCALE S-06-3 DATA AND ALARM-P1 ANALYSES

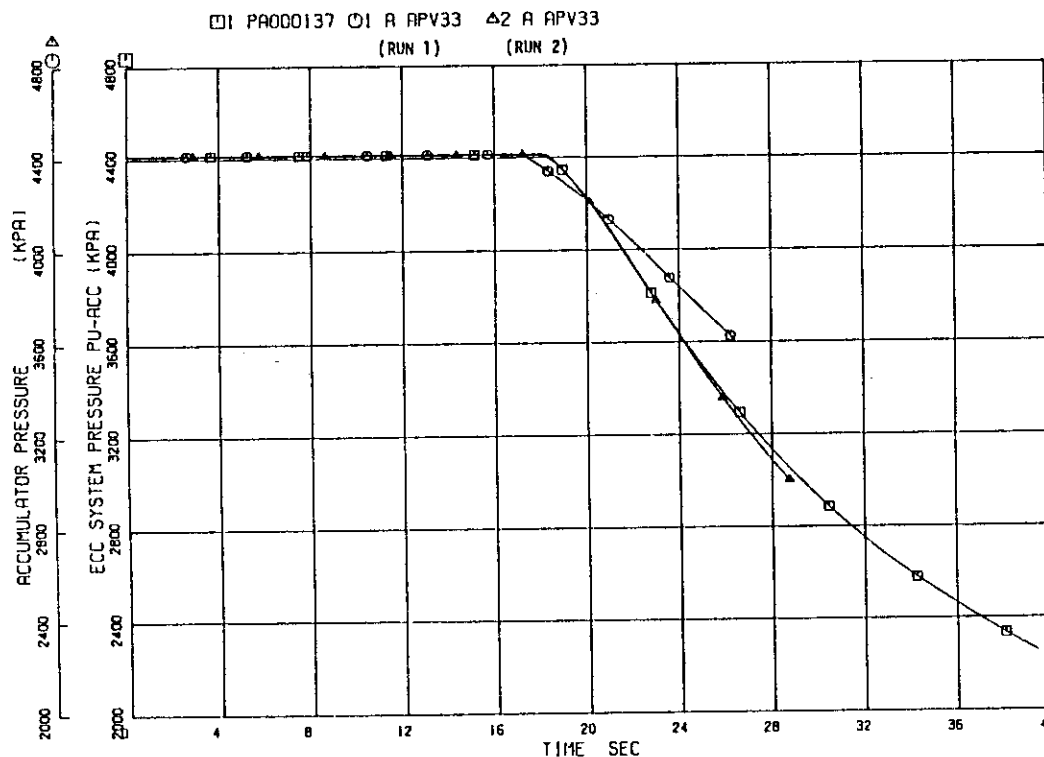


Figure 7 Intact Loop Accumulator Pressure History (PU-ACC)

COMPARISON OF SEMISCALE S-06-3 DATA AND ALARM-P1 ANALYSES

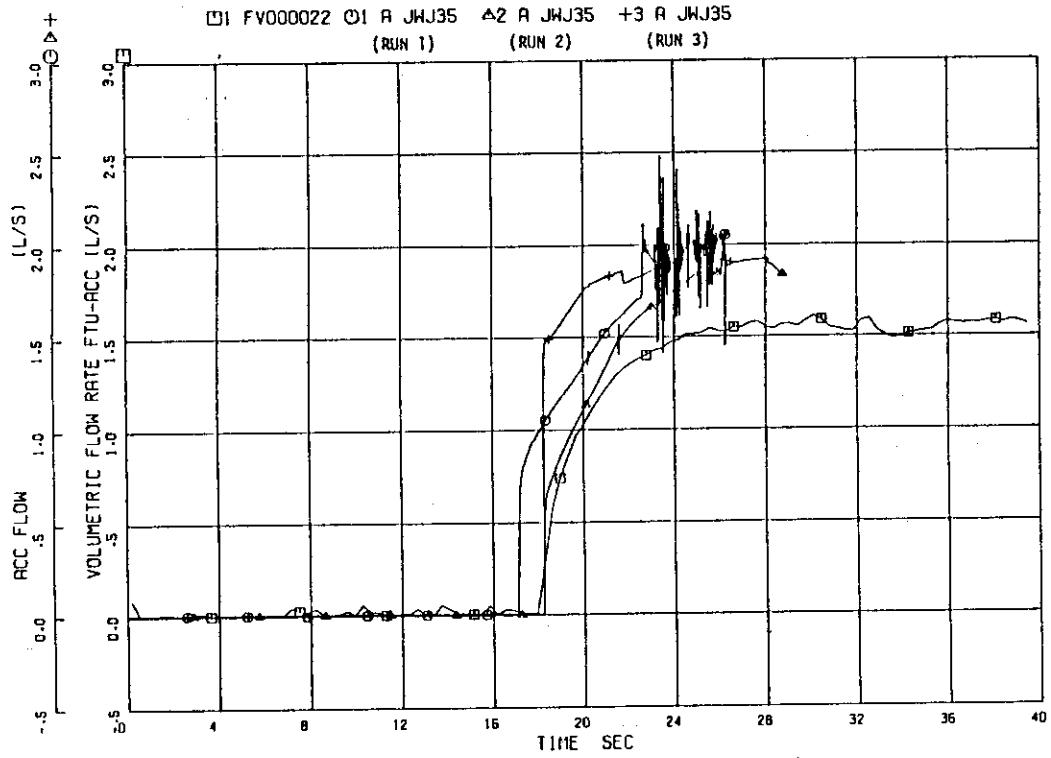


Figure 8 Volumetric Flow Rate in Accumulator Tank (FTU-ACC)

COMPARISON OF SEMISCALE S-06-3 DATA AND ALARM-P1 ANALYSES

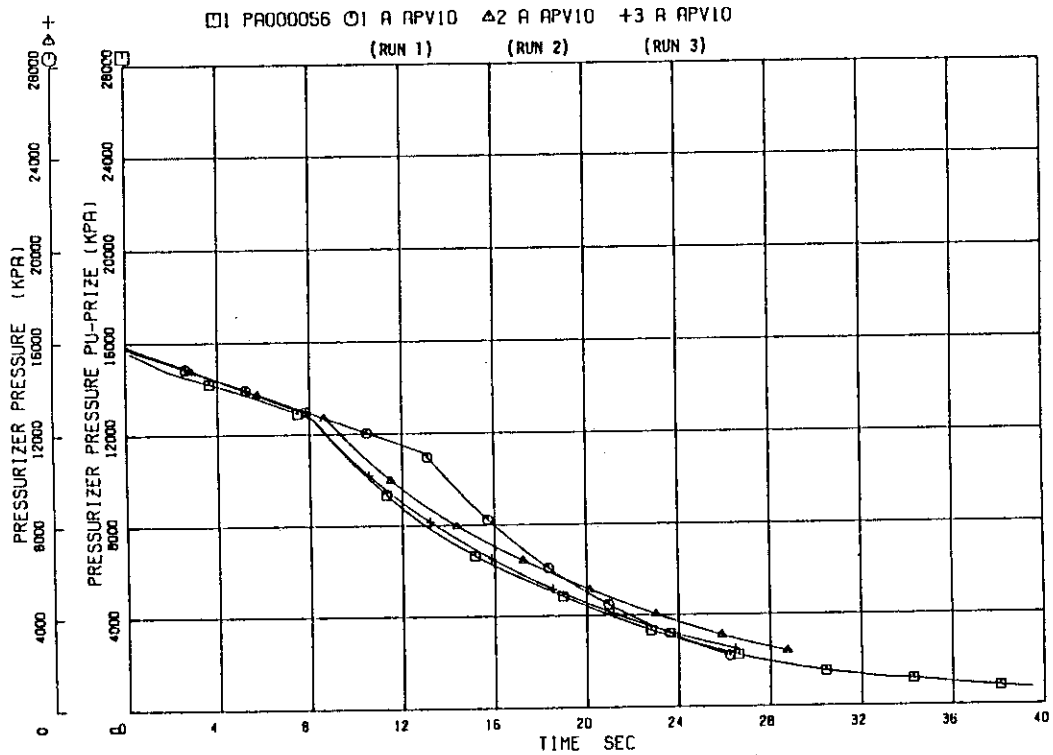


Figure 9 Pressurizer Pressure History (PU-PRIZE)

COMPARISON OF SEMISCALE S-06-3 DATA AND ALARM-P1 ANALYSES

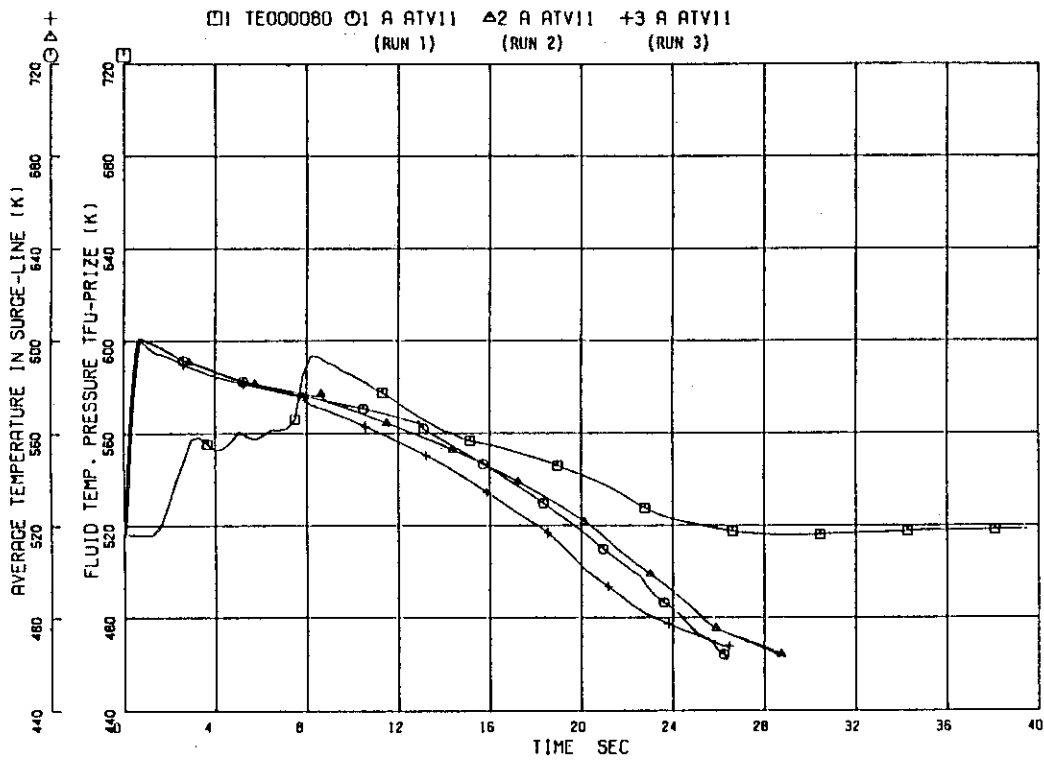


Figure 10 Fluid Temperature History in Pressurizer Surge Line (TFU-PRIZE)

COMPARISON OF SEMISCALE S-06-3 DATA AND ALARM-P1 ANALYSES

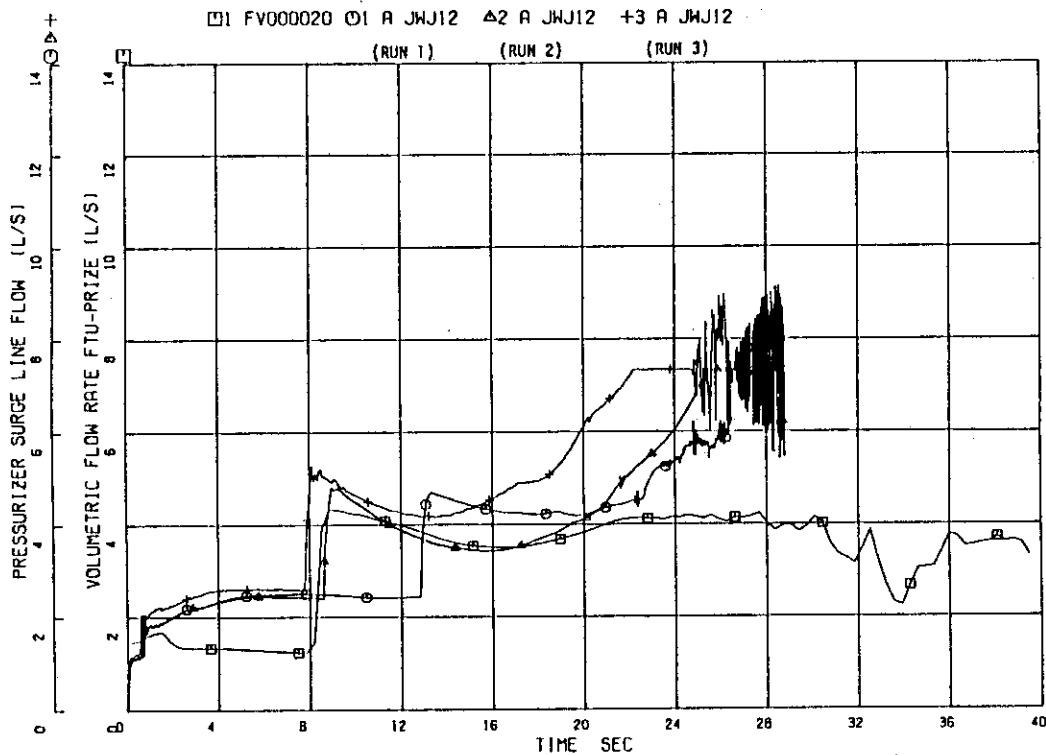


Figure 11 Volumetric Flow Rate in Pressurizer Surge Line Outlet (FTU-PRIZE)

COMPARISON OF SEMISCALE S-06-3 DATA AND ALARM-P1 ANALYSES

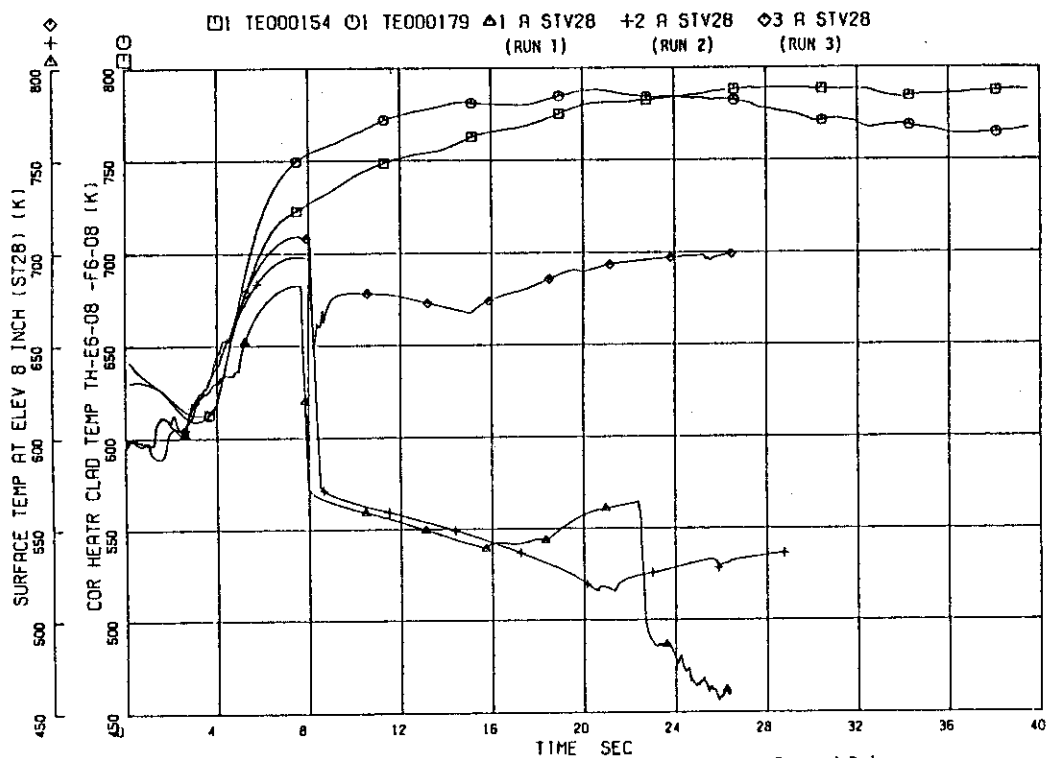


Figure 12 Clad Surface Temperature History for Low-Powered Rods (Elevation of 8" above Bottom of Heated Length)

COMPARISON OF SEMISCALE S-06-3 DATA AND ALARM-P1 ANALYSES

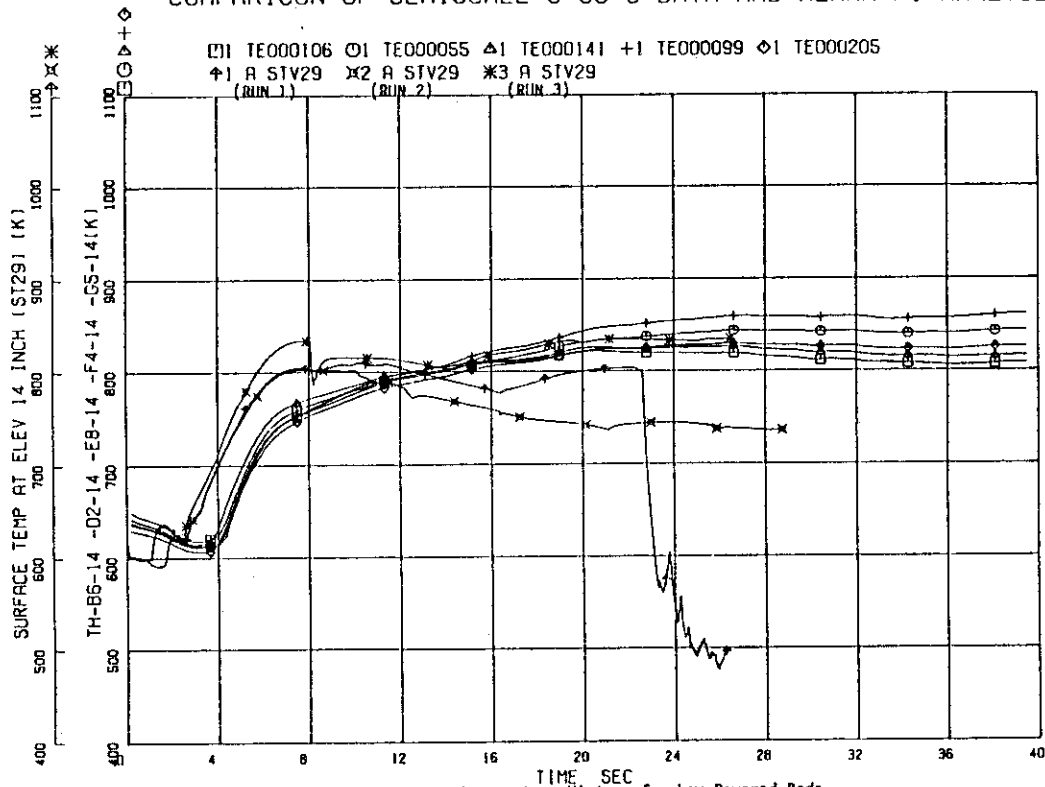


Figure 13 Clad Surface Temperature History for Low-Powered Rods (Elevation of 14" above Bottom of Heated Length)

COMPARISON OF SEMISCALE S-06-3 DATA AND ALARM-P1 ANALYSES

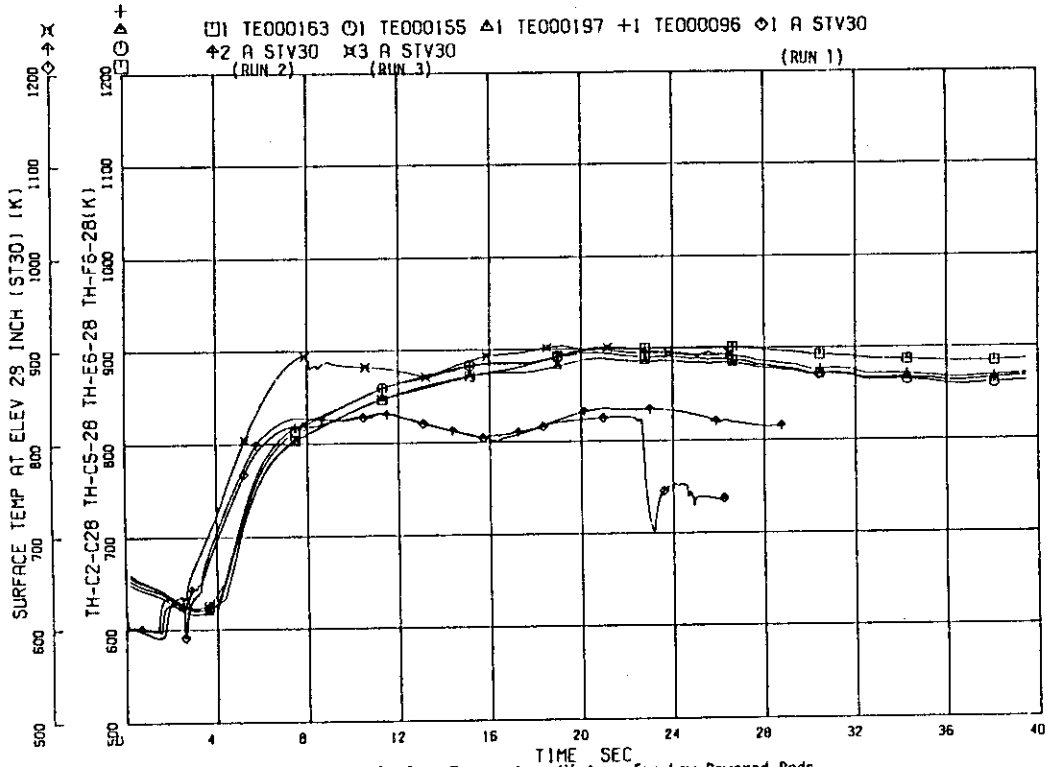


Figure 14 Clad Surface Temperature History for Low-Powered Rods (Elevation of 28" above Bottom of Heated Length)

COMPARISON OF SEMISCALE S-06-3 DATA AND ALARM-P1 ANALYSES

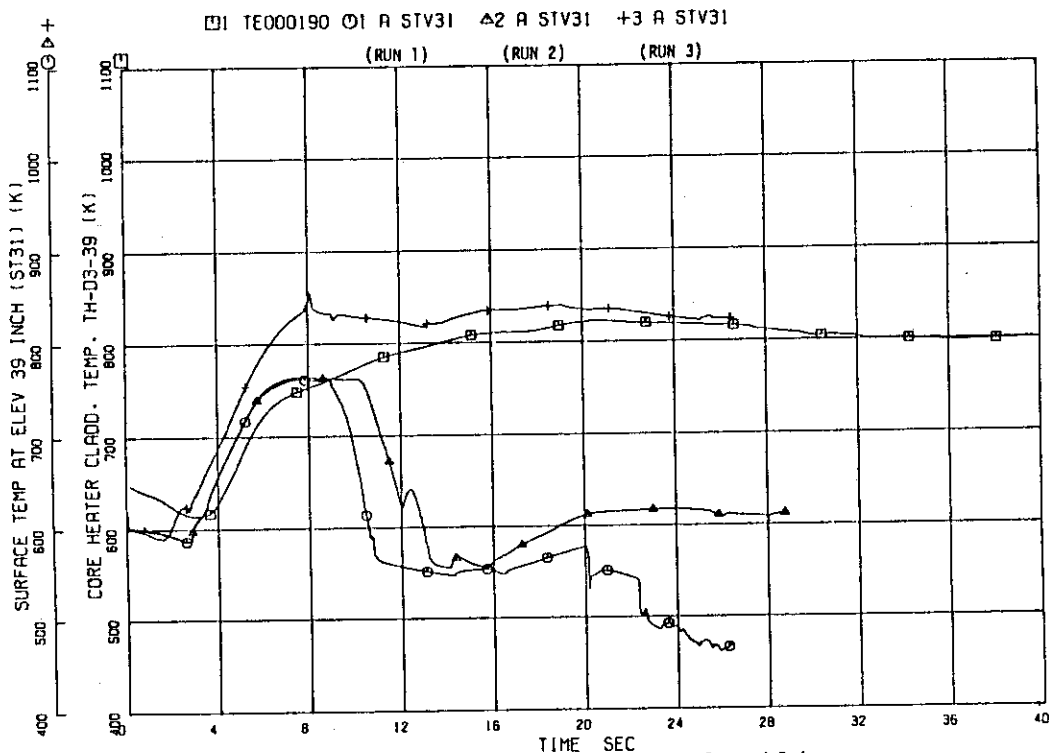


Figure 15 Clad Surface Temperature History for Low-Powered Rods (Elevation of 39" above Bottom of Heated Length)

COMPARISON OF ALARM-P1 ANALYSES

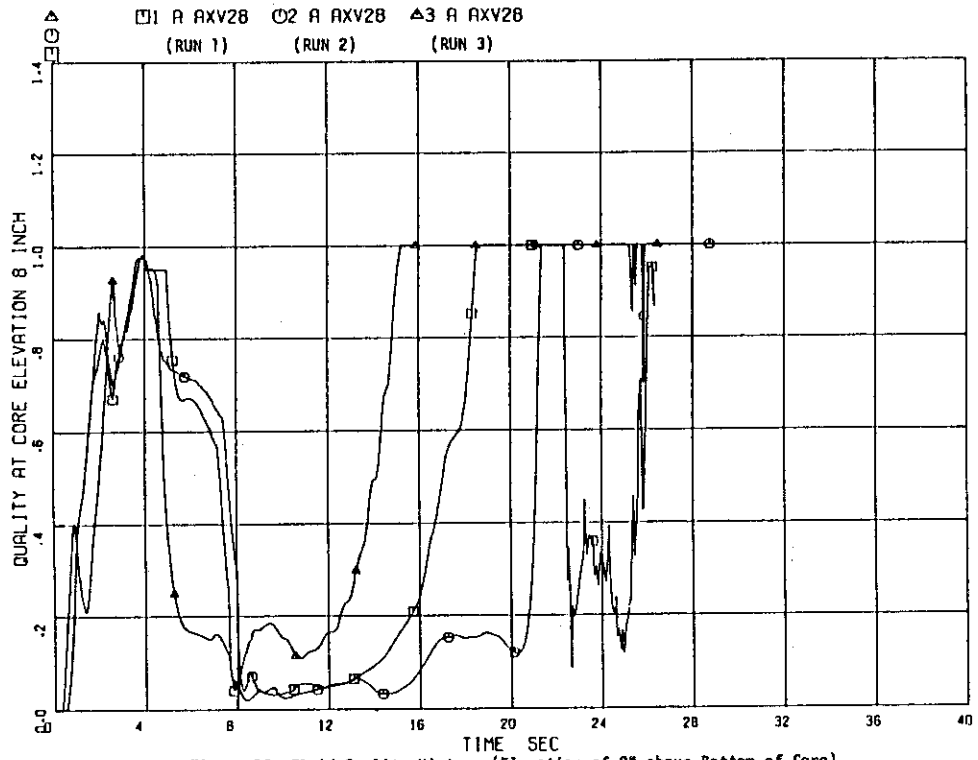


Figure 16 Fluid Quality History (Elevation of 8" above Bottom of Core)

COMPARISON OF ALARM-P1 ANALYSES

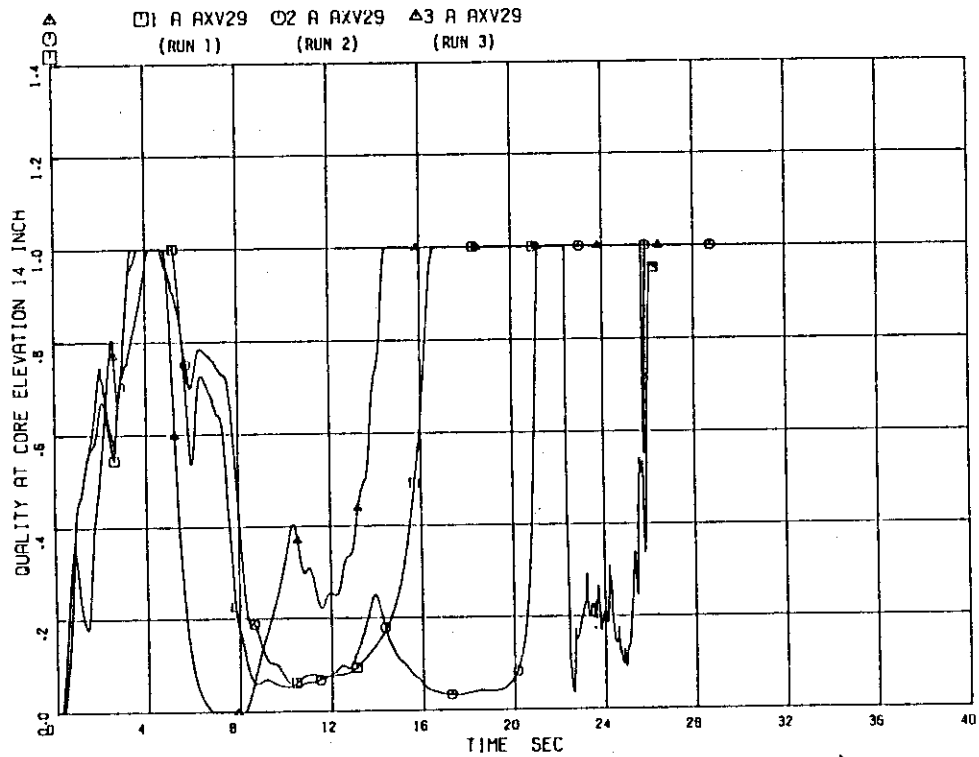


Figure 17 Fluid Quality History (Elevation of 14" above Bottom of Core)

COMPARISON OF ALARM-P1 ANALYSES

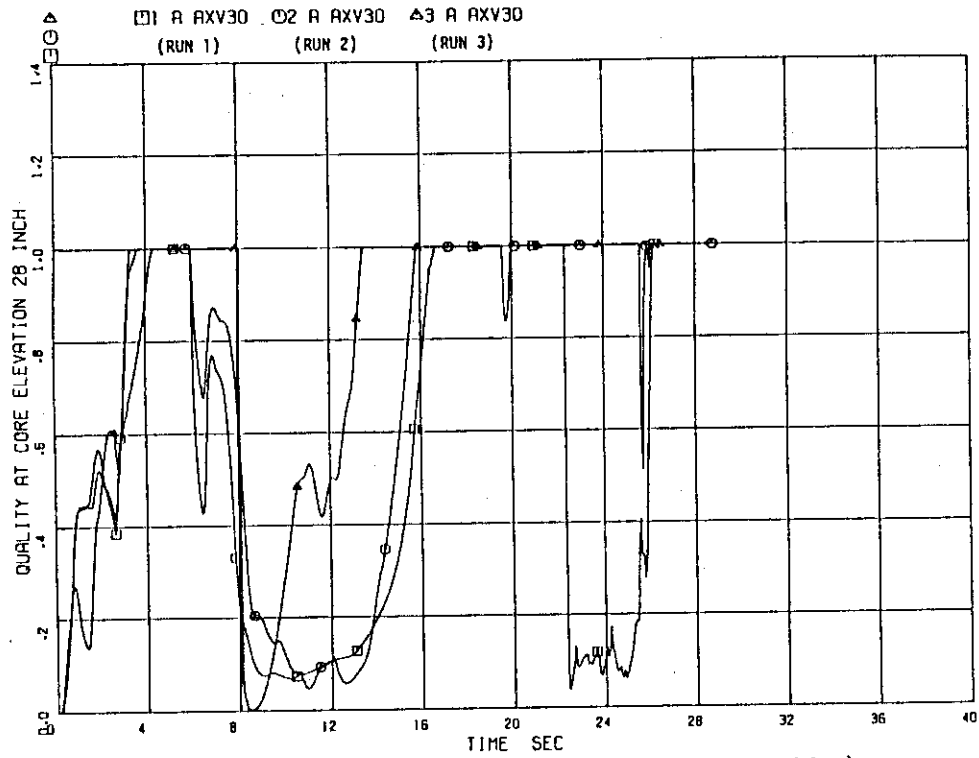


Figure 18 Fluid Quality History (Elevation of 28" above Bottom of Core)

COMPARISON OF ALARM-P1 ANALYSES

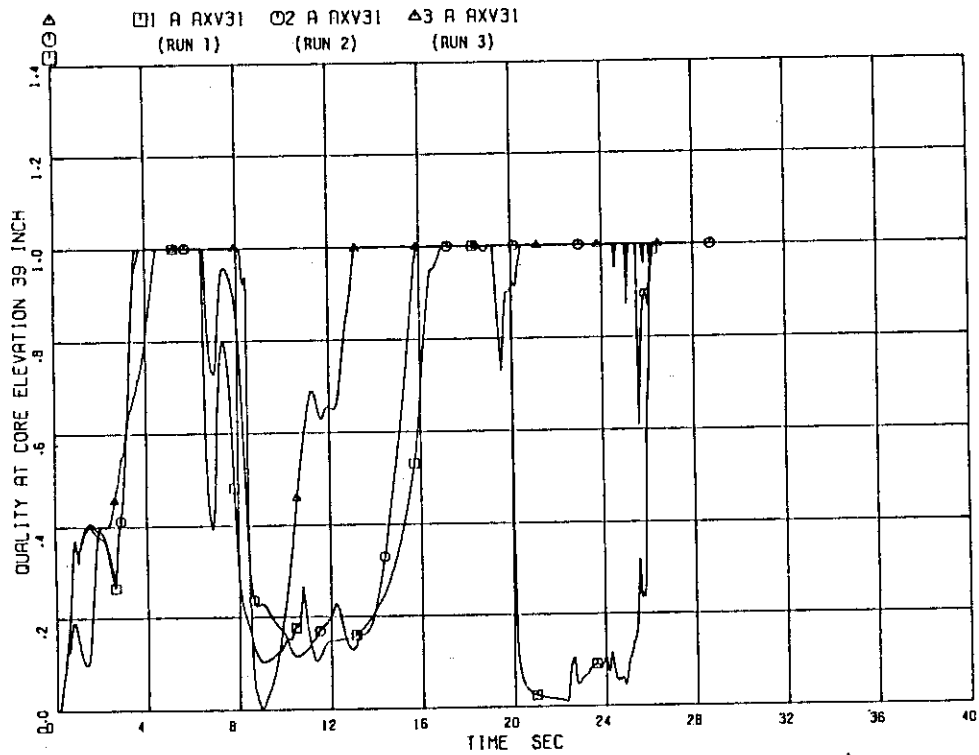


Figure 19 Fluid Quality History (Elevation of 39" above Bottom of Core)

COMPARISON OF ALARM-P1 ANALYSES

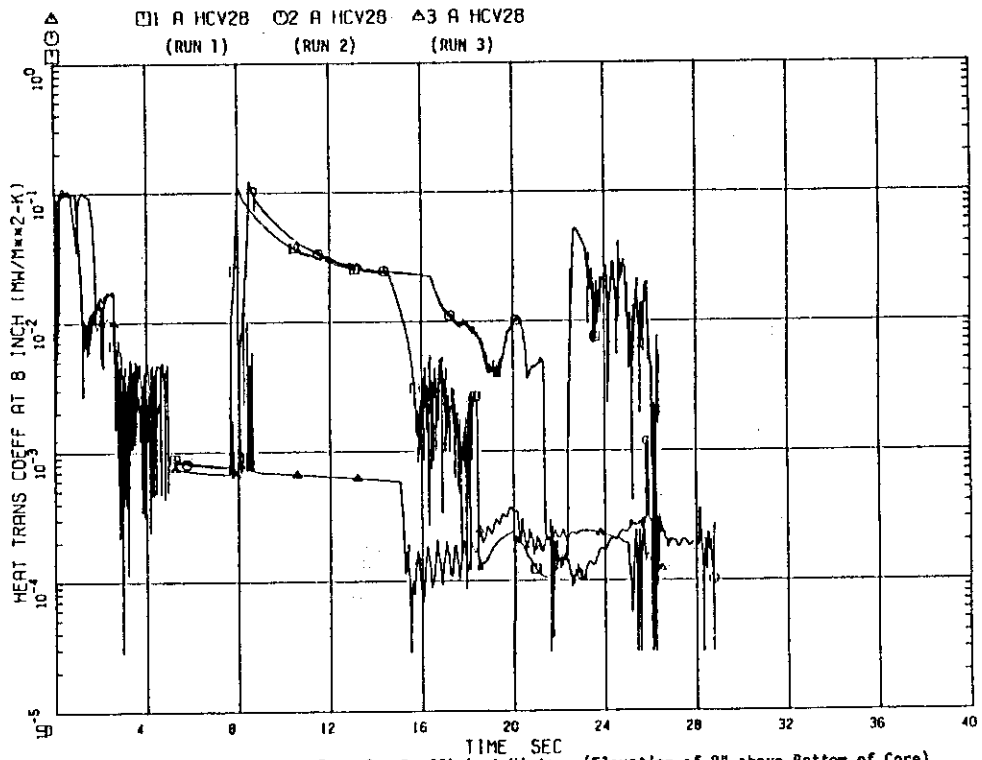


Figure 20 Heat Transfer Coefficient History (Elevation of 8" above Bottom of Core)

COMPARISON OF ALARM-P1 ANALYSES

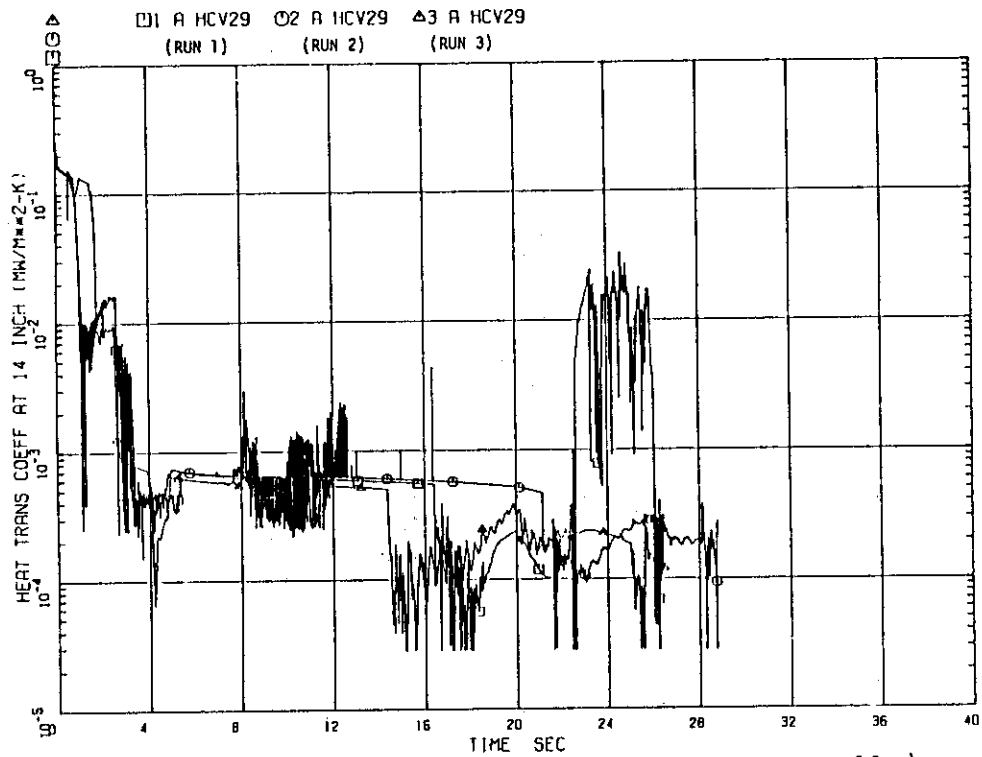


Figure 21 Heat Transfer Coefficient History (Elevation of 14" above Bottom of Core)

COMPARISON OF ALARM-P1 ANALYSES

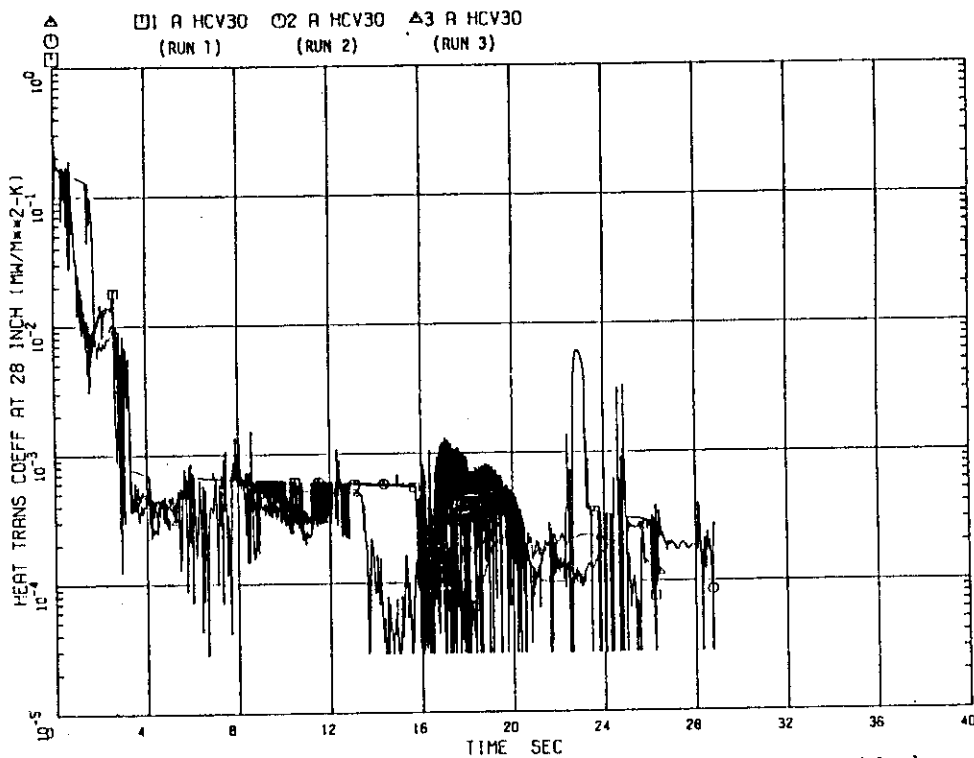


Figure 22 Heat Transfer Coefficient History (Elevation of 28" above Bottom of Core)

COMPARISON OF ALARM-P1 ANALYSES

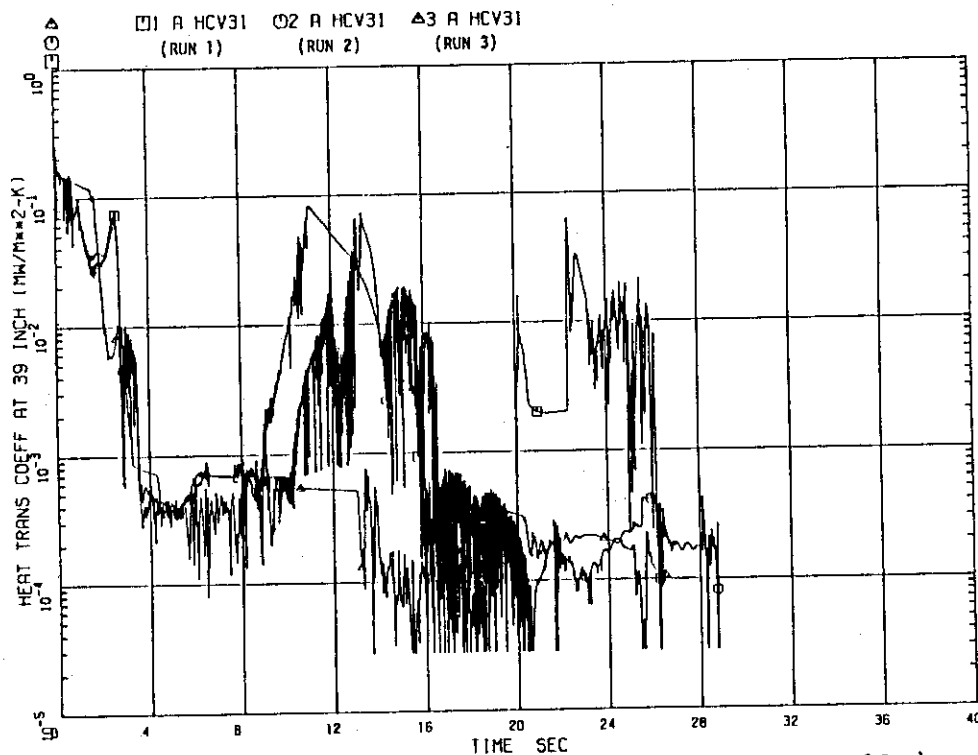


Figure 23 Heat Transfer Coefficient History (Elevation of 39" above Bottom of Core)

COMPARISON OF SEMISCALE S-06-3 DATA AND ALARM-P1 ANALYSES

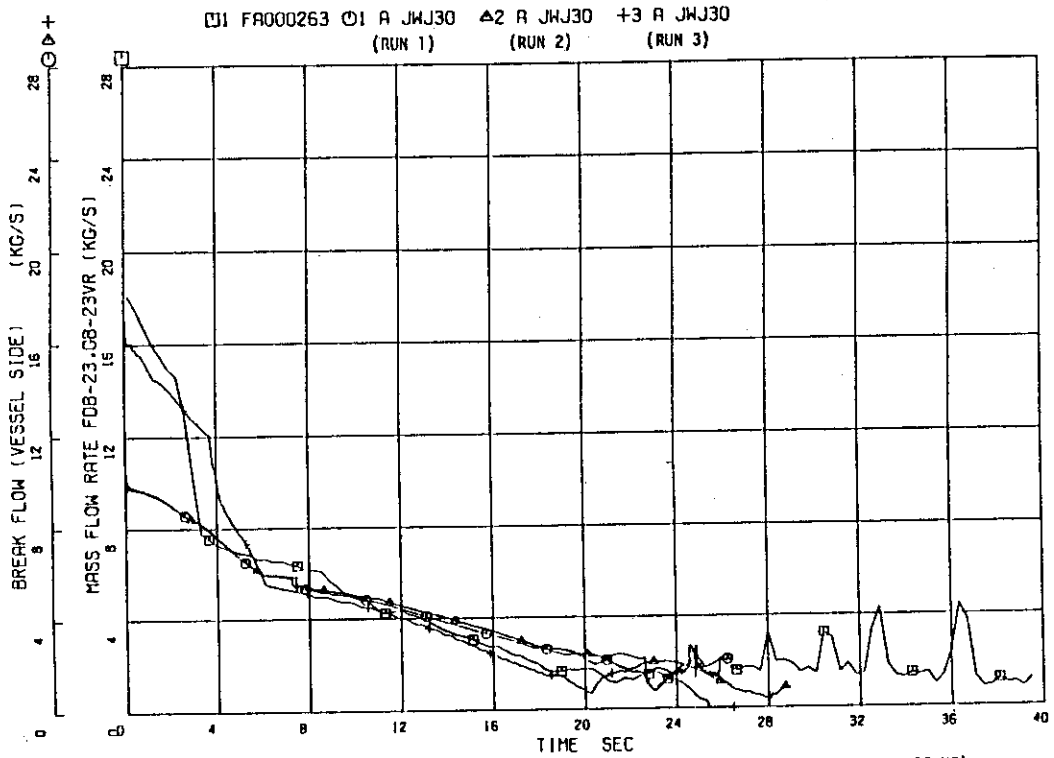


Figure 24 Mass Flow Rate at Break Nozzle — Reactor Vessel Side (FOB-23, GB-23 VR)

COMPARISON OF SEMISCALE S-06-3 DATA AND ALARM-P1 ANALYSES

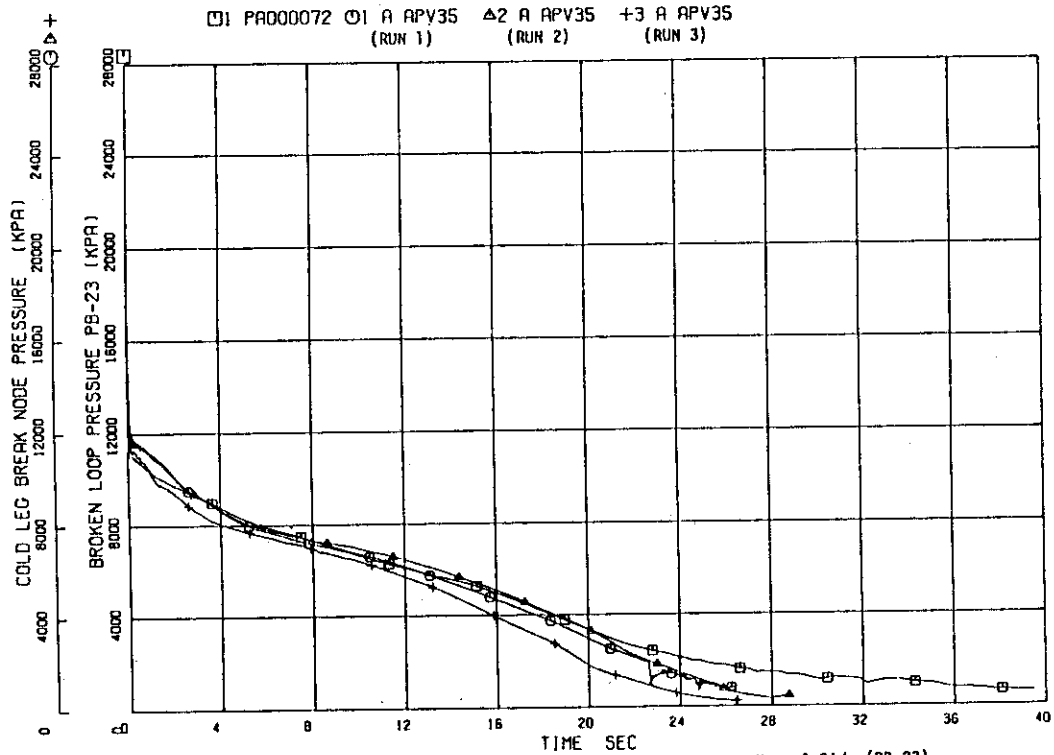


Figure 25 Pressure History upstream of Break Nozzle — Reactor Vessel Side (PB-23)

COMPARISON OF SEMISCALE S-06-3 DATA AND ALARM-P1 ANALYSES

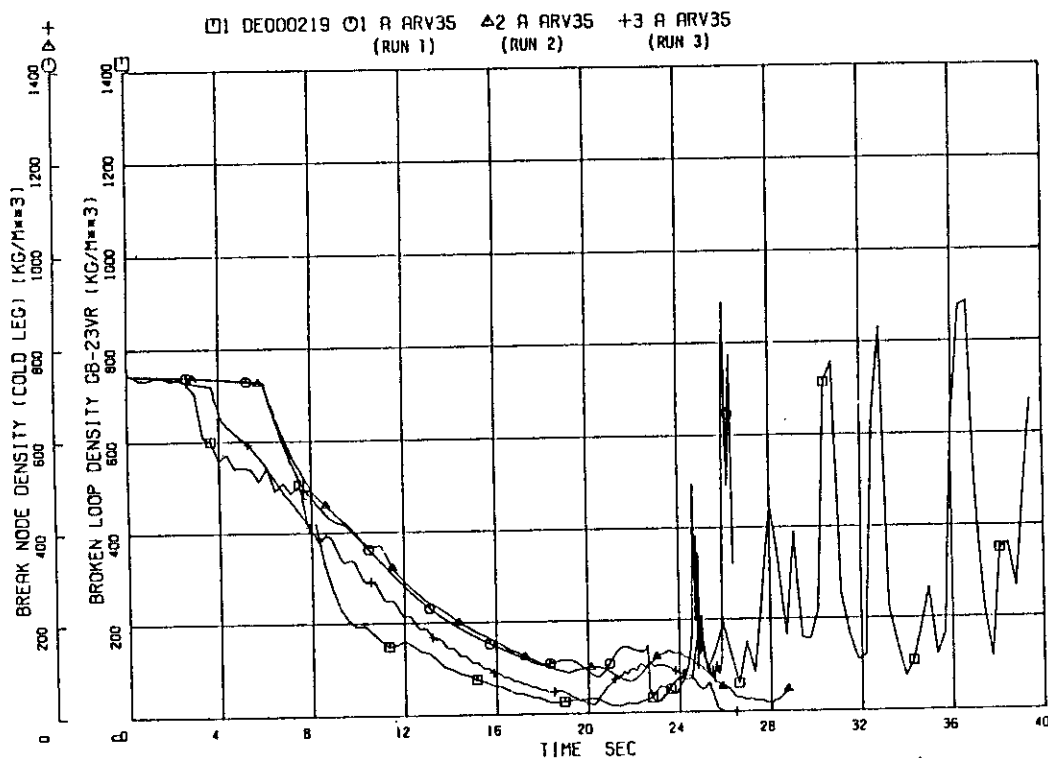


Figure 26 Fluid Density History in Break Volume — Reactor Vessel Side (GD-23 VR)

COMPARISON OF SEMISCALE S-06-3 DATA AND ALARM-P1 ANALYSES

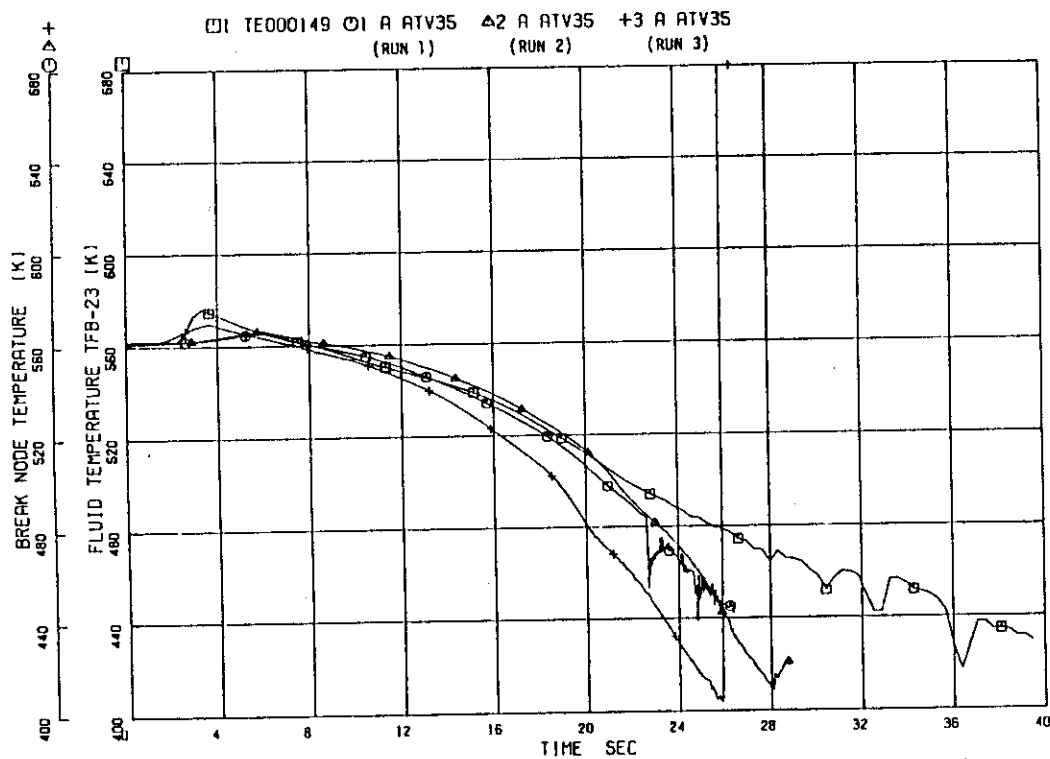


Figure 27 Fluid Temperature History upstream of Break — Reactor Vessel Side (TFB-23)

COMPARISON OF SEMISCALE S-06-3 DATA AND ALARM-P1 ANALYSES

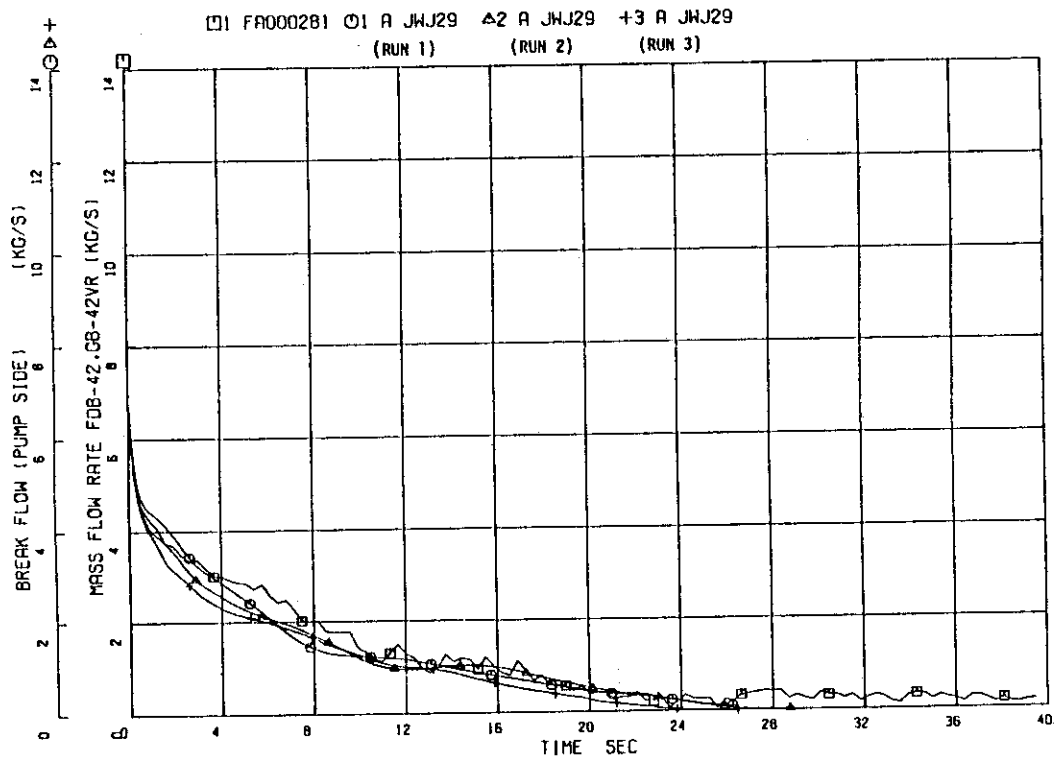


Figure 28 Mass Flow Rate at Break Nozzle — Pump Side (FDB-42, GB-42 VR)

COMPARISON OF SEMISCALE S-06-3 DATA AND ALARM-P1 ANALYSES

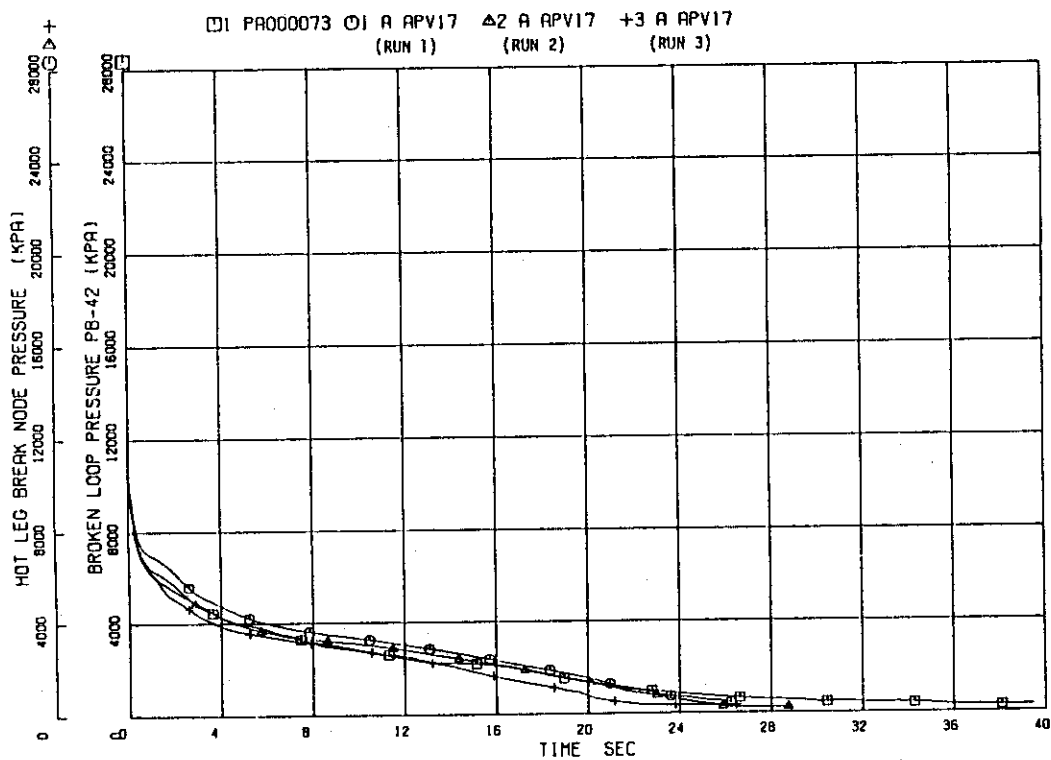


Figure 29 Pressure History upstream of Break Nozzle — Pump Side (PB-42)

COMPARISON OF SEMISCALE S-06-3 DATA AND ALARM-P1 ANALYSES

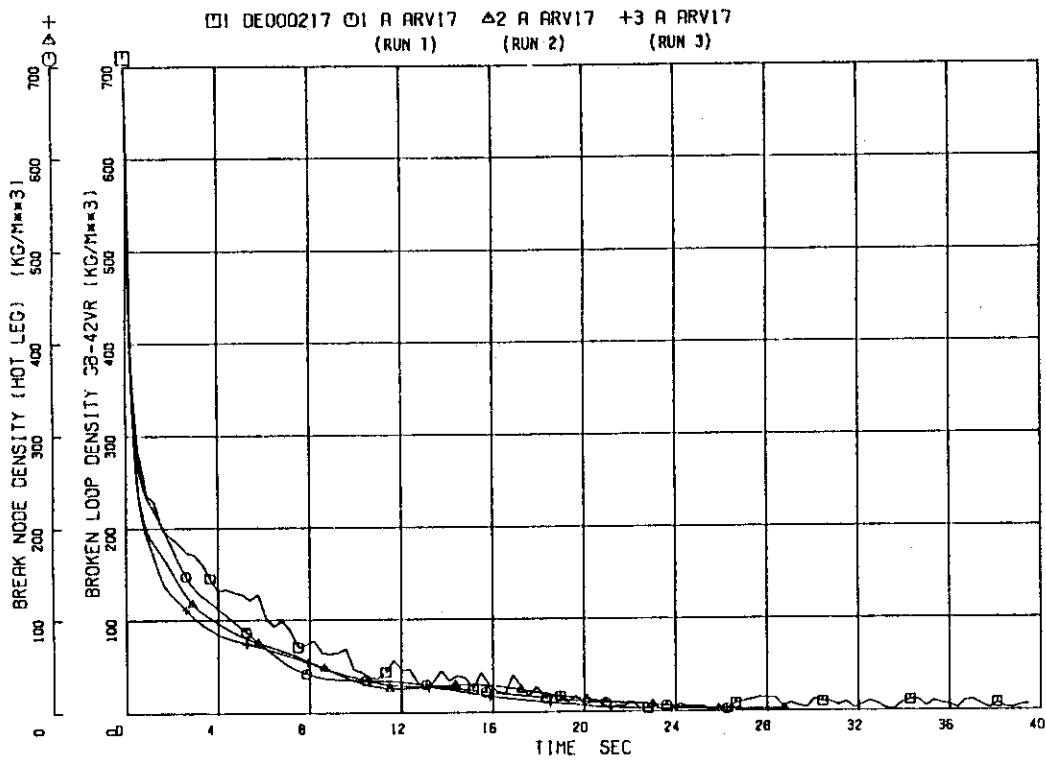


Figure 30 Fluid Density History in Break Volume — Pump Side (GB-42 VR)

COMPARISON OF SEMISCALE S-06-3 DATA AND ALARM-P1 ANALYSES

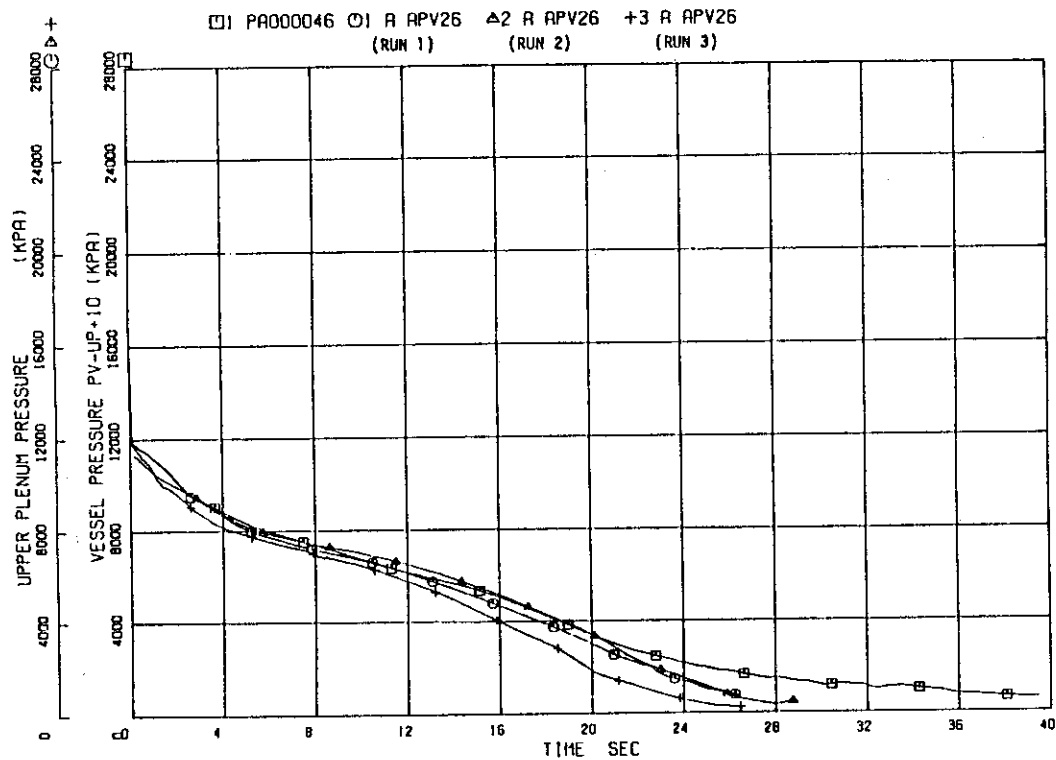
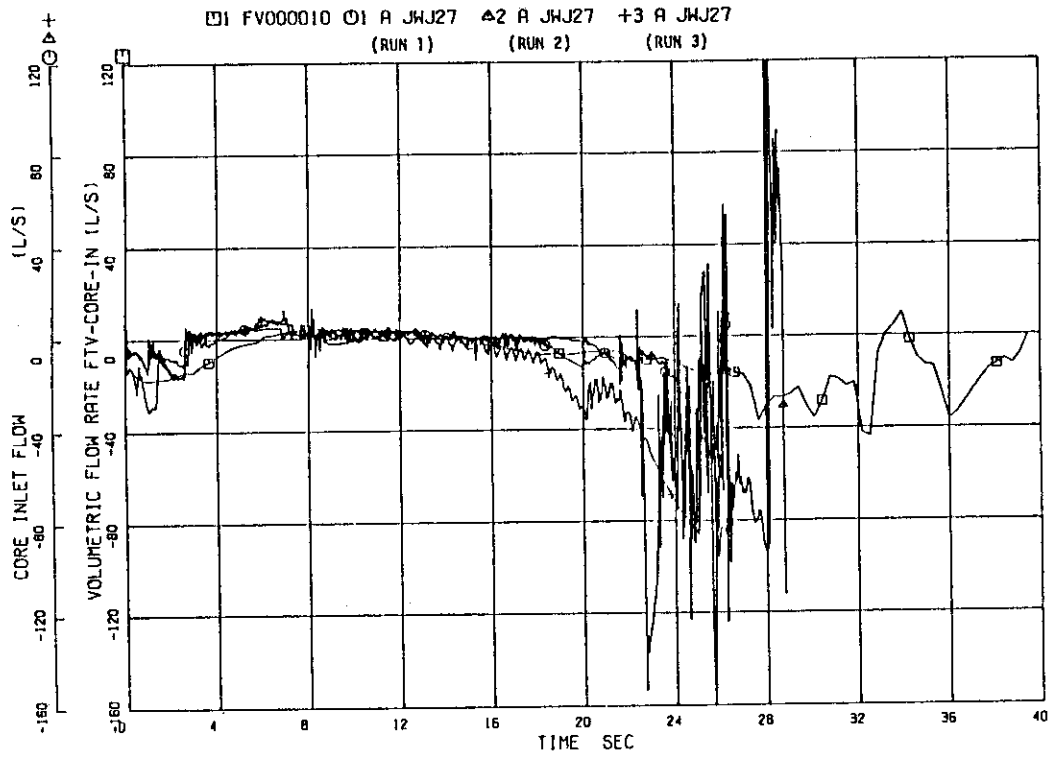
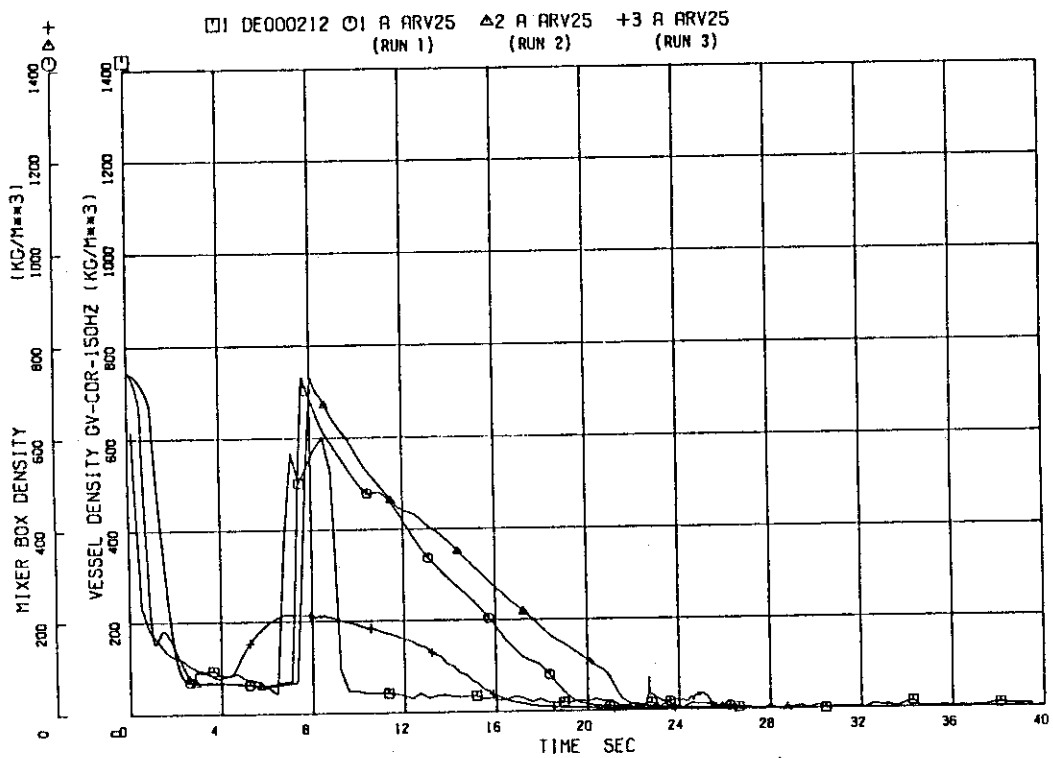


Figure 31 Upper-plenum Pressure History (PV-UP+10)

COMPARISON OF SEMISCALE S-06-3 DATA AND ALARM-P1 ANALYSES



COMPARISON OF SEMISCALE S-06-3 DATA AND ALARM-P1 ANALYSES



COMPARISON OF SEMISCALE S-06-3 DATA AND ALARM-P1 ANALYSES

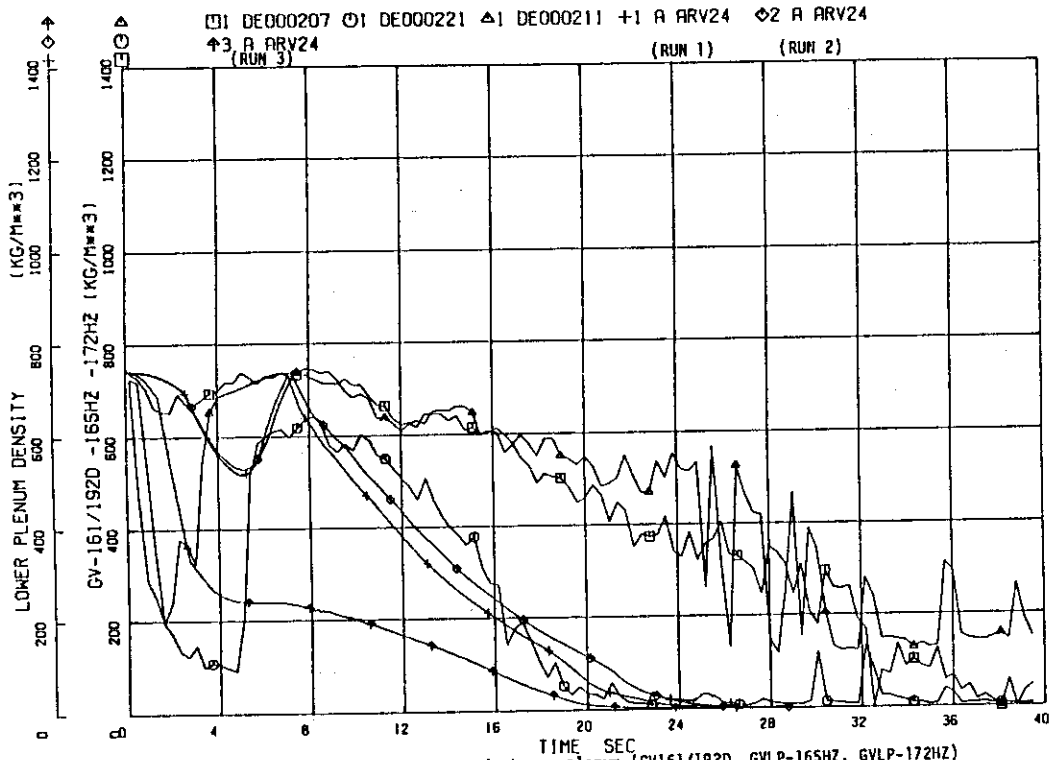


Figure 34 Fluid Density History In Lower-plenum (GV161/192D, GVLP-165HZ, GVLP-172HZ)

COMPARISON OF SEMISCALE S-06-3 DATA AND ALARM-P1 ANALYSES

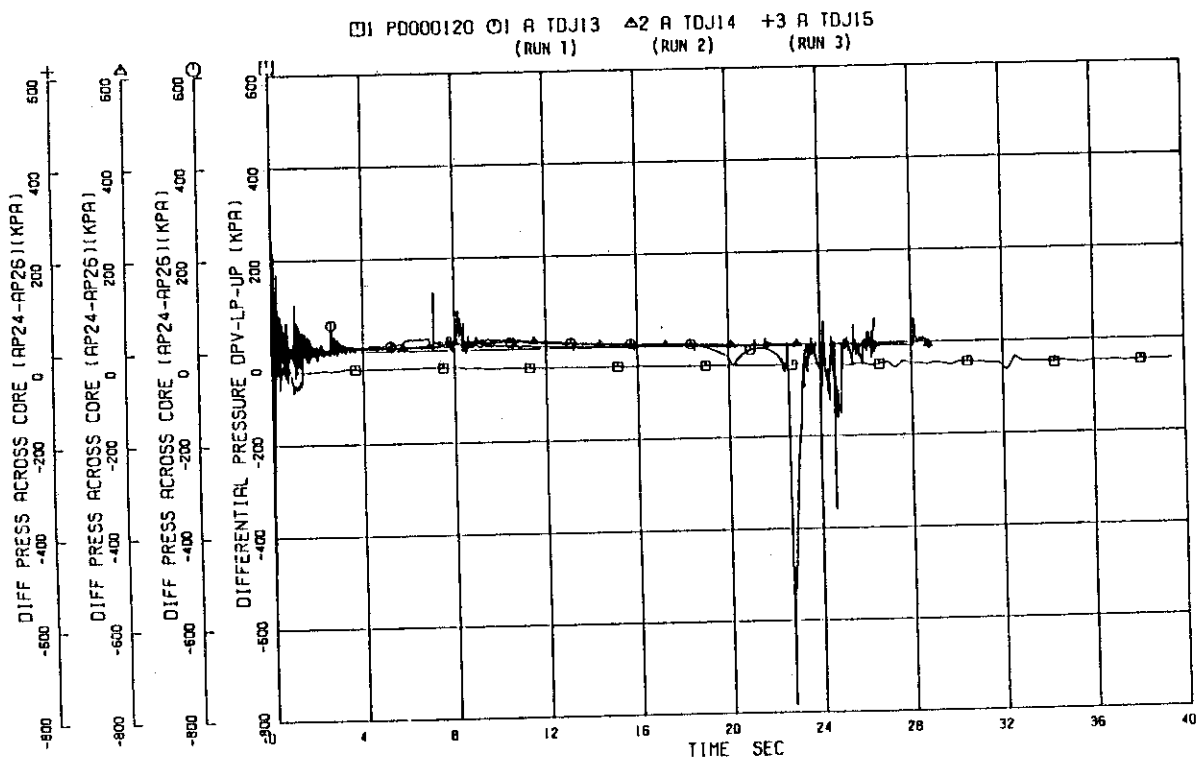


Figure 35 Pressure Difference Across Core (DPV-LP-UP)

COMPARISON OF SEMISCALE S-06-3 DATA AND ALARM-P1 ANALYSES

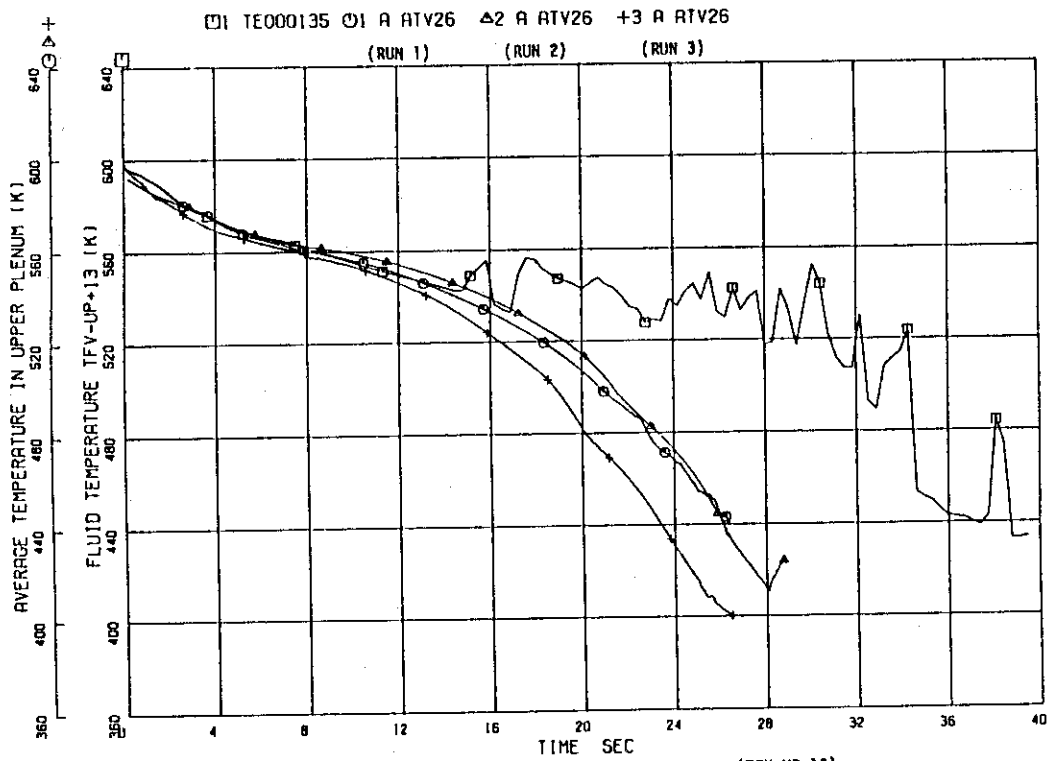


Figure 36 Fluid Temperature History in Upper-plenum (TFV-UP+13)

COMPARISON OF SEMISCALE S-06-3 DATA AND ALARM-P1 ANALYSES

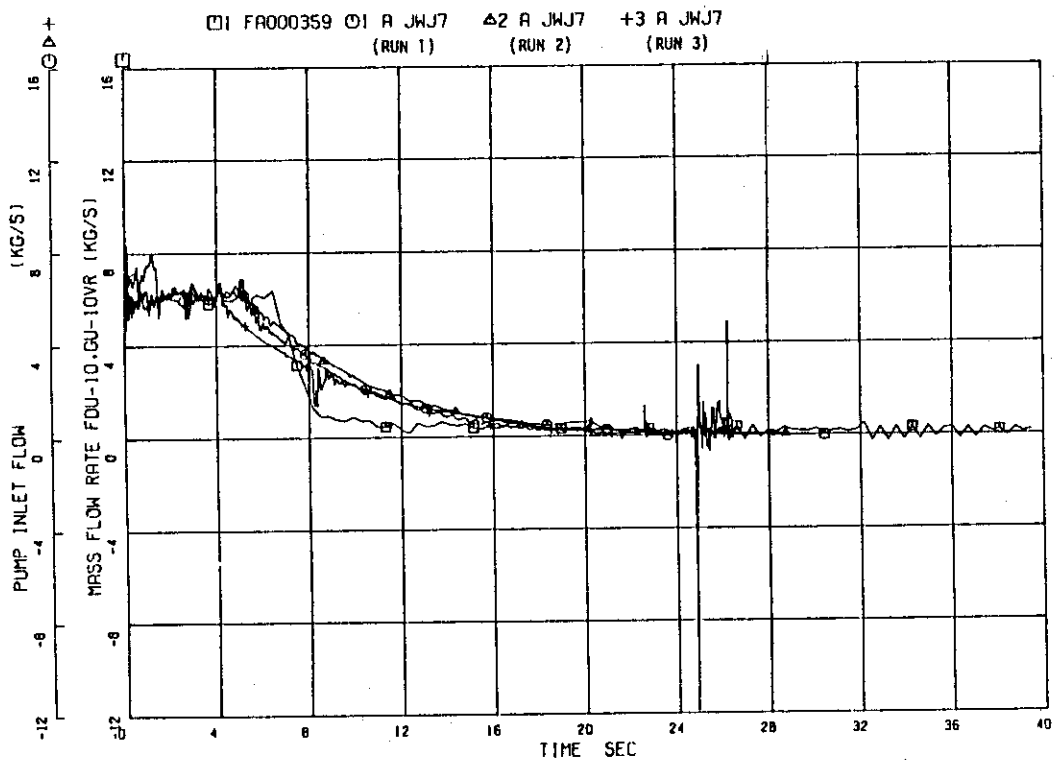
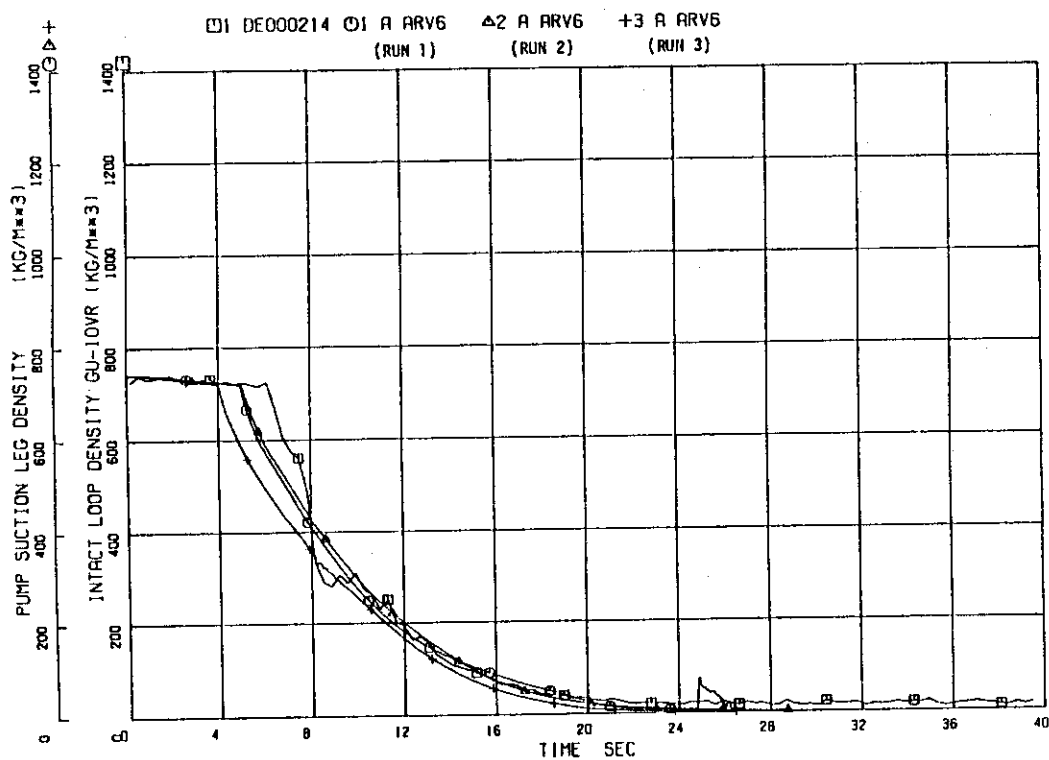
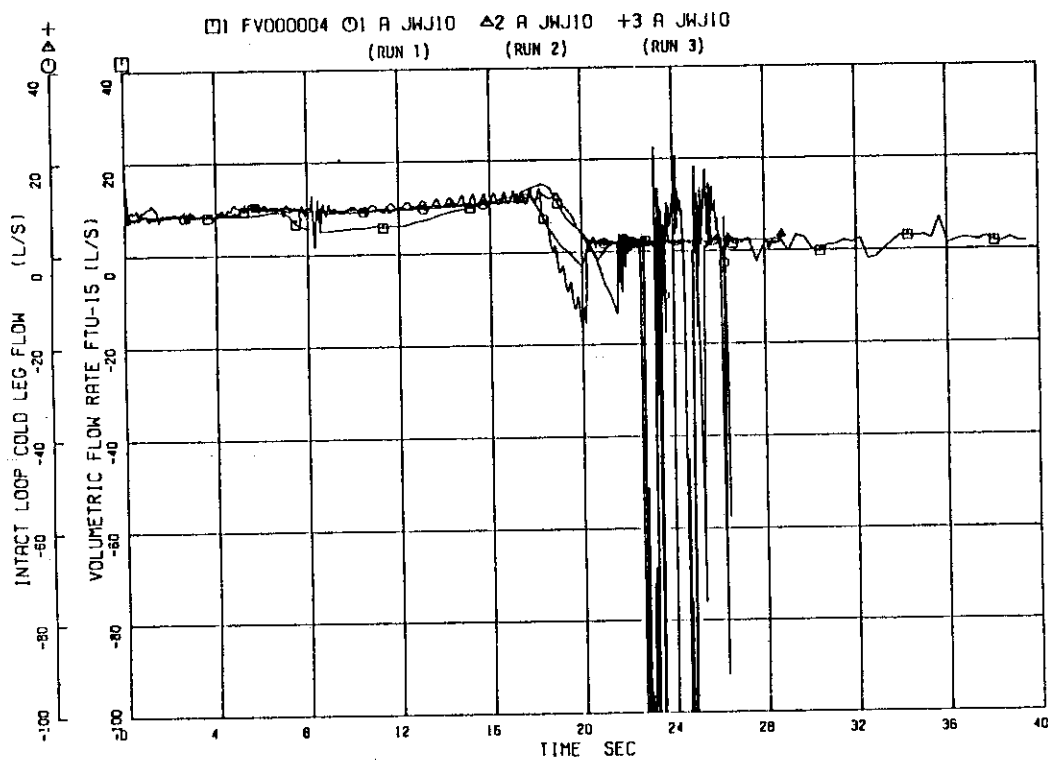


Figure 37 Mass Flow Rate in Spool 10 — Pump Inlet Flow (FDU-10, GU-10 VR)

COMPARISON OF SEMISCALE S-06-3 DATA AND ALARM-P1 ANALYSES



COMPARISON OF SEMISCALE S-06-3 DATA AND ALARM-P1 ANALYSES



COMPARISON OF SEMISCALE S-06-3 DATA AND ALARM-P1 ANALYSES

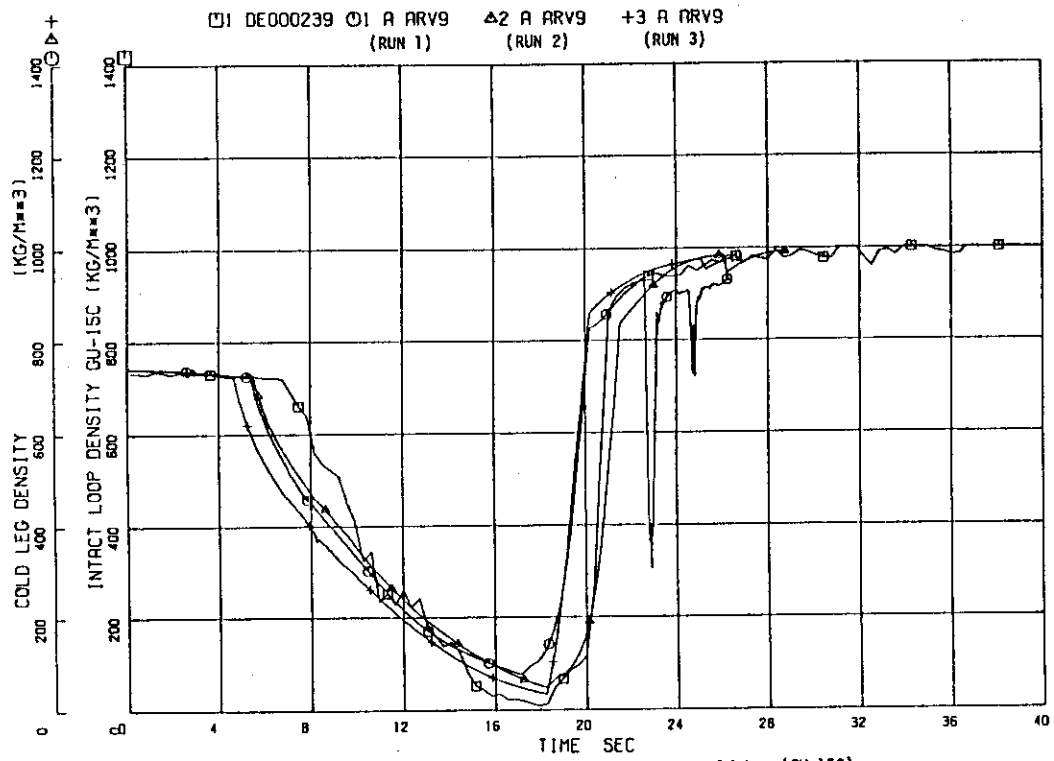


Figure 40 Fluid Density History in Intact Loop Cold Leg (GU-15C)

COMPARISON OF SEMISCALE S-06-3 DATA AND ALARM-P1 ANALYSES

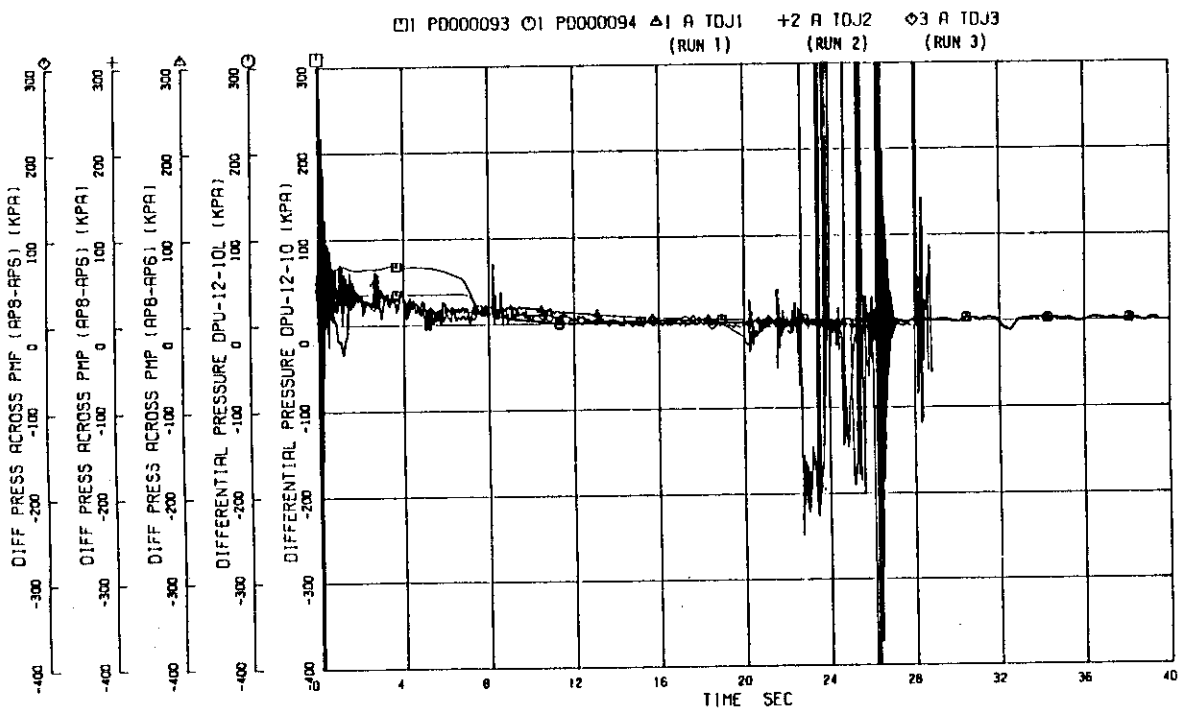


Figure 41 Pressure Difference Across Pump (DPU-12-10)

COMPARISON OF SEMISCALE S-06-3 DATA AND ALARM-P1 ANALYSES

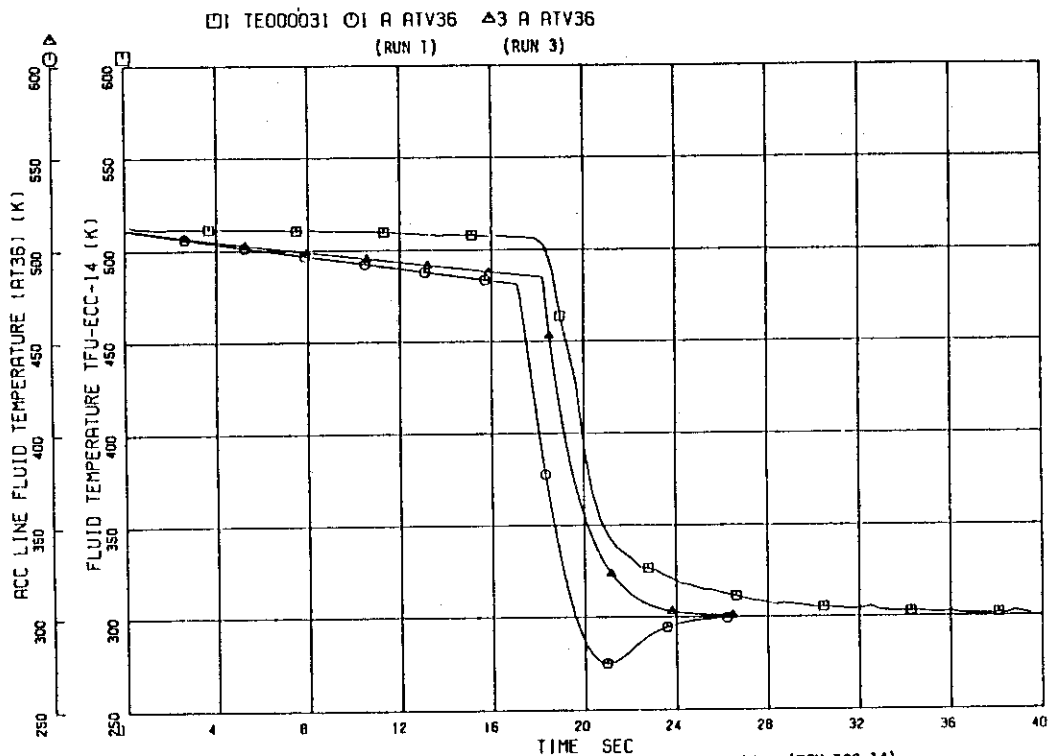


Figure 42 Fluid Temperature History in Accumulator Line (TFU-ECC-14)

COMPARISON OF SEMISCALE S-06-3 DATA AND ALARM-P1 ANALYSES

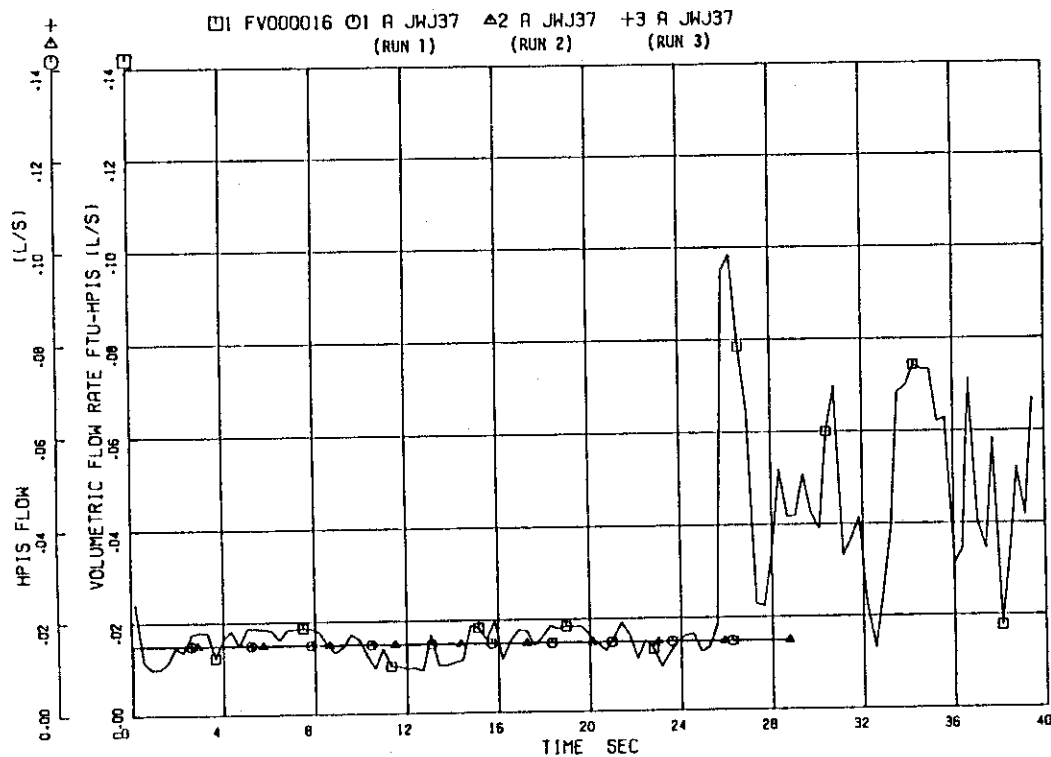


Figure 43 Volumetric Flow Rate in Intact Loop HPIS (FTU-HPIS)

COMPARISON OF SEMISCALE S-06-3 DATA AND ALARM-P1 ANALYSES

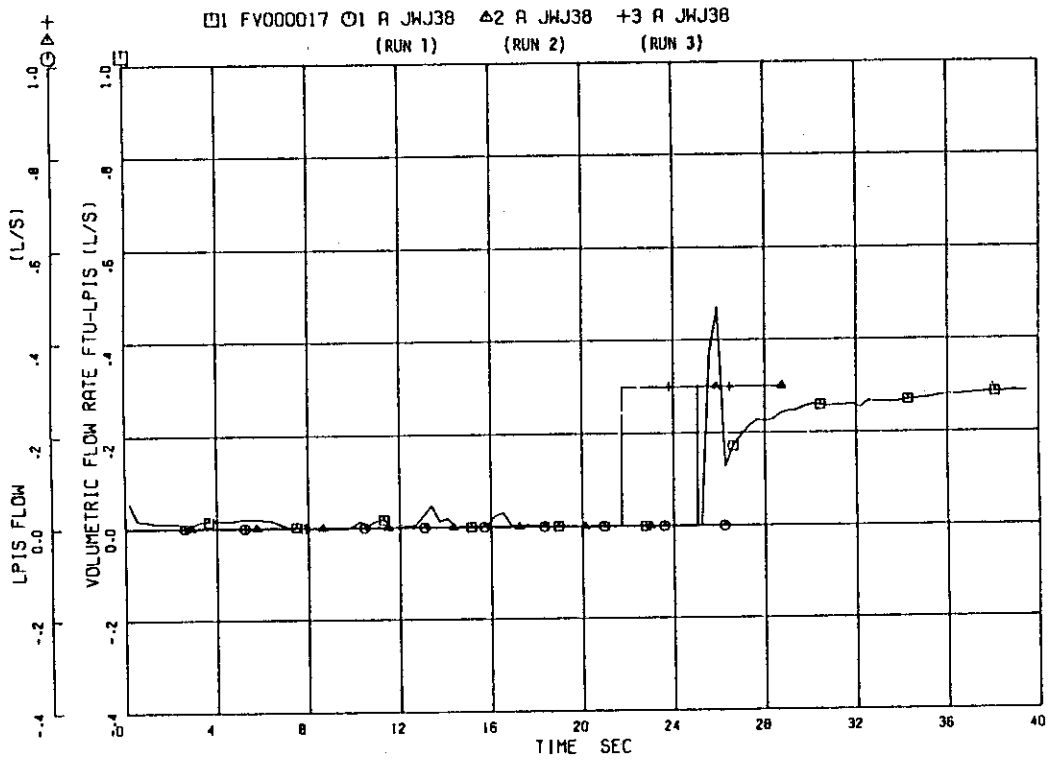


Figure 44 Volumetric Flow Rate in Intact Loop LPIS (FTU-LPIS)

COMPARISON OF SEMISCALE S-06-3 DATA AND ALARM-P1 ANALYSES

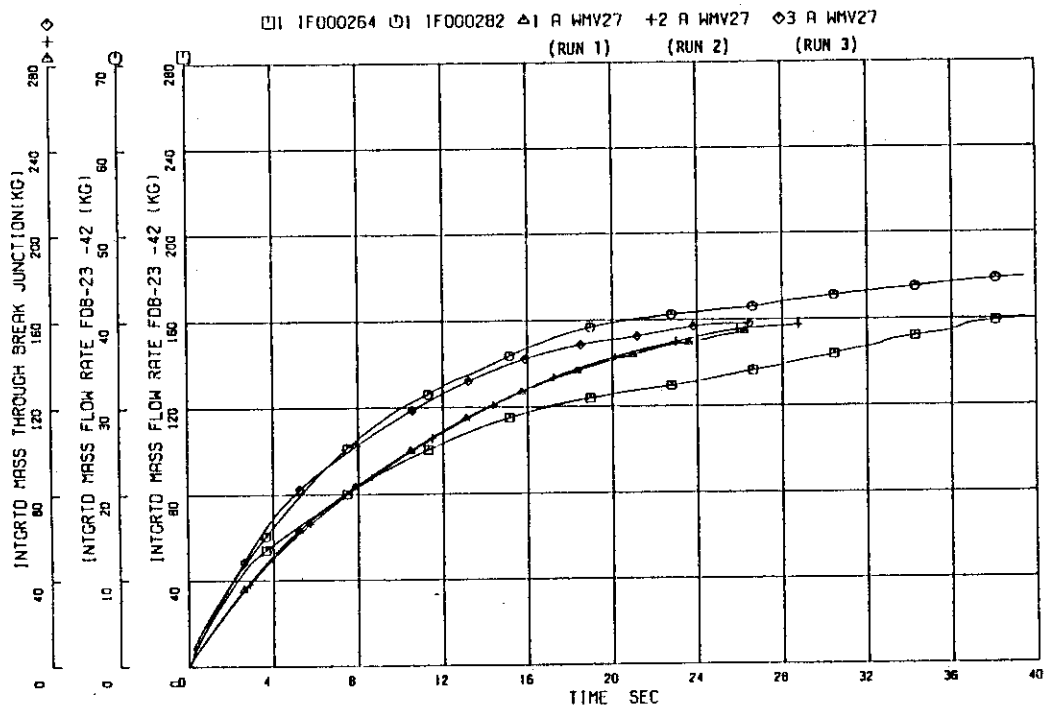


Figure 45 System Mass Inventory History

Appendix 1 List of Input-data (RUN 2)

```

/*
/*      AN ANALYSIS OF SEMISCALE S-06-3 TEST BY ALARM-P1 CODE
/*
/*      ALARM-P1 PREDICTION OF CSNI STANDARD PROBLEM NO.8
/*
/*      PROBLEM DIMENSION
/*
/*      LDMP NEDI NTC  NTRP  NVOL NBUB NJUN NPMP  NPMPC NCKV NLK NFLL
/*      NSLB NOCOR NGOM  NMAT NHTX      POWRO
/*      -3  18  9  10  36  2  40  1  1  3  1  3
/*      7  5  2  4  0  1.0058
/*
/*      EDIT VARIABLE
/*
/*      JW  J29 JW  J30 AP  N10 AP  N17 AP  N35 AP  N21 AP  N26 ST  N28 ST  N29
/*      ST  N30 ST  N31 JW  J7  AT  N11 AT  N18 AT  N26 WM  N27 TM  N27 HC  N28
/*
/*      TIME STEP SIZE
/*
/*      100  20  1  2000  0.000005  0.01
/*      100  10  1  1000  0.00001  0.05
/*      100  4  1  400  0.000025  0.3
/*      100  20  1  200  0.00005  0.5
/*      100  10  1  100  0.0001  5.0
/*      100  20  1  40  0.00025  10.0
/*      100  10  1  20  0.0005  18.0
/*      200  10  1  40  0.00025  24.0
/*      100  50  1  100  0.0001  50.0
/*
/*      TRIP CONTROL
/*
/*      1  1  0  0  40.0  0.0  / END OF PROBLEM
/*      21  1  0  0  0.0  0.0  / STEAM OUTLET J22
/*      3  1  0  0  0.0  0.0  / POWER
/*      4  1  0  0  100.0  0.0  / PUMP TRIP
/*      51  1  0  0  0.0  0.0  / FEED WATER J23
/*      52  -4  36  0  126.5448E4  0.0  / HPIS J37
/*      53  -4  36  0  17.5796E4  0.0  / LPIS J38
/*      6  1  0  0  0.00001  0.0  / BREAK
/*      7  1  0  0  0.00001  0.0  / BREAK
/*      8  1  0  0  18.2  0.0  / ACC VALVE J40
/*
/*      VOLUME DATA
/*
/*      IBUB NPUMP P TEMP HORX V ZVOL
/*      ZM FLOWA DIAMV ELEV FLOWL
/*      ***** VOL.1 INTACT LOOP HOT LEG *****
/*      0 0 160.7410E4 326.444 -1.0 0.01082 0.3086735
/*      0.3086735 0.00349 0.0667 0.1825625 3.17
/*

```

JAERI-M 9842

	1	2	3	4	5	6	7-R	8
/* ***** VOL.2 SG INLET PLENUM *****								ISP80510
0 0 160.6312E4			326.444	-1.0	0.00963	0.48514		ISP80520
0.48514		0.01984	0.1590		0.491236	0.0		ISP80530
/*								ISP80540
/* ***** VOL.3 SG U-TUBE *****								ISP80550
0 0 160.4933E4			-343.52	-1.0	0.01140	2.629916		ISP80560
2.629916		0.00442	0.0102		0.976376	0.0		ISP80570
/*								ISP80580
/* ***** VOL.4 SG U-TUBE *****								ISP80590
0 0 160.4606E4			-320.14	-1.0	0.01140	2.629916		ISP80600
2.629916		0.00442	0.0102		0.976376	0.0		ISP80610
/*								ISP80620
/* ***** VOL.5 SG OUTLET PLENUM *****								ISP80630
0 0 160.5583E4			290.889	-1.0	0.00963	0.48514		ISP80640
0.48514		0.01984	0.1590		0.491236	0.0		ISP80650
/*								ISP80660
/* ***** VOL.6 PUMP SUCTION LEG *****								ISP80670
0 0 160.4092E4			290.889	-1.0	0.01018	1.543812		ISP80680
1.543812		0.00349	0.0667		-1.052576	0.0		ISP80690
/*								ISP80700
/* ***** VOL.7 ACTIVE PUMP *****								ISP80710
0 1 160.7004E4			290.889	-1.0	0.00408	0.2809875		ISP80720
0.2809875		0.00349	0.0667		-0.24765	0.0		ISP80730
169.53								ISP80740
/*								ISP80750
/* ***** VOL.8 INTACT LOOP COLD LEG NEAR PUMP *****								ISP80760
0 0 161.0477E4			290.889	-1.0	0.00425	0.066675		ISP80770
0.066675		0.00349	0.0667		-0.0333375	1.25		ISP80780
/*								ISP80790
/* ***** VOL.9 INTACT LOOP COLD LEG *****								ISP80800
0 0 161.0384E4			290.889	-1.0	0.00425	0.066675		ISP80810
0.066675		0.00349	0.0667		-0.0333375	1.25		ISP80820
/*								ISP80830
/* ***** VOL.10 PRESSURIZER *****								ISP80840
2 0 160.6254E4			-1.0	0.0	0.02741	1.143		ISP80850
0.62547		0.02466	0.0		1.86055	0.0		ISP80860
/*								ISP80870
/* ***** VOL.11 PRESSURIZER SURGE LINE *****								ISP80880
0 0 160.7034E4			242.850	-1.0	0.00037	1.7888225		ISP80890
1.7888225		4.3E-5	0.0		0.2492375	3.9000		ISP80900
/*								ISP80910
/* ***** VOL.12 BROKEN LOOP HOT LEG *****								ISP80920
0 0 160.8332E4			322.960	-1.0	0.00315	0.2190115		ISP80930
0.2190115		0.00349	0.0667		0.1825625	1.00646		ISP80940
/*								ISP80950
/* ***** VOL.13 SG SIMULATOR *****								ISP80960
0 0 160.7478E4			-349.762	-1.0	0.00852	2.6099135		ISP80970
2.6099135		0.00374	0.0690		0.401574	2.57658		ISP80980
/*								ISP80990
/* ***** VOL.14 SG SIMULATOR *****								ISP81000
0 0 160.7478E4			-346.519	-1.0	0.00852	2.6099135		ISP81010
2.6099135		0.00374	0.0690		0.401574	2.57658		ISP81020
/*								ISP81030
/* ***** VOL.15 PUMP SUCTION LEG *****								ISP81040
0 0 160.7948E4			317.800	-1.0	0.00252	1.417574		ISP81050
1.417574		0.00158	0.0449		-1.016	1.40081		ISP81060
/*								ISP81070
/* ***** VOL.16 PUMP SIMULATOR *****								ISP81080
0 0 160.8552E4			317.000	-1.0	0.00147	0.2301875		ISP81090

```

-----1-----2-----3-----4-----5-----6-----7-R-----8
      0.2301875      0.00198      0.0016      -1.2461875      23.3      ISP81100
/*
/* ***** VOL.17 HOT LEG BREAK NODE ***** ISP81110
      0 0      160.8077E4      316.970      -1.0      0.00227      1.4954250      ISP81120
      1.4954250      0.00145      0.0429      -1.2461875      1.50799      ISP81130
/*
/* ***** VOL.18 BROKEN LOOP COLD LEG ***** ISP81140
      0 0      161.0465E4      290.720      -1.0      0.00461      0.066675      ISP81150
      0.066675      0.00349      0.0667      -0.0333375      100.      ISP81160
/*
/* ***** VOL.19 HOT LEG SIDE REFLOOD BYPASS LINE ***** ISP81170
      0 0      160.8141E4      315.850      -1.0      0.00538      0.552323      ISP81180
      0.552323      0.00349      0.0667      0.1825625      0.0      ISP81190
/*
/* ***** VOL.20 COLD LEG SIDE REFLOOD BYPASS LINE ***** ISP81200
      0 0      161.0177E4      288.850      -1.0      0.00640      0.768223      ISP81210
      0.768223      0.00349      0.0667      -0.0333375      0.0      ISP81220
/*
/* ***** VOL.21 SG SECONDARY SYSTEM ***** ISP81230
      1 0      66.8923E4      0.0      0.03208      0.19820      4.6580      ISP81240
      2.90      0.04255      0.0      0.976376      0.0      ISP81250
/*
/* ***** VOL.22 PRESSURE VESSEL INLET PLENUM ***** ISP81260
      0 0      161.0066E4      290.889      -1.0      0.00504      0.45847      ISP81270
      0.45847      0.00548      0.0412      -0.2667      0.0      ISP81280
/*
/* ***** VOL.23 DOWNCOMER ANNULUS ***** ISP81290
      0 0      161.1592E4      290.889      -1.0      0.02183      3.880612      ISP81300
      3.880612      0.00534      0.0214      -4.147312      3.9      ISP81310
/*
/* ***** VOL.24 LOWER PLENUM ***** ISP81320
      0 0      161.3225E4      290.889      -1.0      0.02161      0.731774      ISP81330
      0.731774      0.00623      0.0      -4.879086      1.0      ISP81340
/*
/* ***** VOL.25 MIXER HOUSING ***** ISP81350
      0 0      161.2122E4      290.889      -1.0      0.00371      0.520446      ISP81360
      0.520446      0.00713      0.0      -4.147312      0.0      ISP81370
/*
/* ***** VOL.26 UPPER PLENUM ***** ISP81380
      0 0      160.8298E4      326.444      -1.0      0.02620      2.972816      ISP81390
      2.972816      0.00713      0.0      -1.950466      2.5      ISP81400
/*
/* ***** VOL.27 PRESSURE SUPPRESSION SYSTEM ***** ISP81410
      1 0      2.4820E4      16.35      0.0      100.      4.5225462      ISP81420
      1.21      0.70205      0.9454      -2.5654      0.0      ISP81430
/*
/* ***** VOL.28 CORE REGION #1 ***** ISP81440
      0 0      161.1054E4      -311.09      -1.0      0.00137      0.2794      ISP81450
      0.2794      0.00492      0.0113      -3.626866      0.0      ISP81460
/*
/* ***** VOL.29 CORE REGION #2 ***** ISP81470
      0 0      161.0817E4      -319.99      -1.0      0.00137      0.2794      ISP81480
      0.2794      0.00492      0.0113      -3.347466      0.0      ISP81490
/*
/* ***** VOL.30 CORE REGION #3 ***** ISP81500
      0 0      161.0582E4      -331.90      -1.0      0.00137      0.2794      ISP81510
      0.2794      0.00492      0.0113      -3.068066      0.0      ISP81520
/*
/* ***** VOL.31 CORE REGION #4 ***** ISP81530
      0.2794      0.00492      0.0113      -3.068066      0.0      ISP81540
      0.2794      0.00492      0.0113      -3.068066      0.0      ISP81550
      0.2794      0.00492      0.0113      -3.068066      0.0      ISP81560
      0.2794      0.00492      0.0113      -3.068066      0.0      ISP81570
      0.2794      0.00492      0.0113      -3.068066      0.0      ISP81580
      0.2794      0.00492      0.0113      -3.068066      0.0      ISP81590
      0.2794      0.00492      0.0113      -3.068066      0.0      ISP81600
      0.2794      0.00492      0.0113      -3.068066      0.0      ISP81610
      0.2794      0.00492      0.0113      -3.068066      0.0      ISP81620
      0.2794      0.00492      0.0113      -3.068066      0.0      ISP81630
      0.2794      0.00492      0.0113      -3.068066      0.0      ISP81640
      0.2794      0.00492      0.0113      -3.068066      0.0      ISP81650
      0.2794      0.00492      0.0113      -3.068066      0.0      ISP81660
      0.2794      0.00492      0.0113      -3.068066      0.0      ISP81670
      0.2794      0.00492      0.0113      -3.068066      0.0      ISP81680

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-----1-----2-----3-----4-----5-----6-----7-R-----8
      0  0  161.0352E4  -343.28  -1.0  0.00137  0.2794  ISP81690
      0.2794  0.00492  0.0113  -2.788666  0.0  ISP81700
/*  ISP81710
/* ***** VOL.32 CORE REGION #5 ***** ISP81720
      0  0  161.0018E4  -352.64  -1.0  0.00274  0.5588  ISP81730
      0.5588  0.00492  0.0113  -2.509266  -0.0  ISP81740
/*  ISP81750
/* ***** VOL.33 ACCUMULATOR TANK ***** ISP81760
      2  0  45.0070E4  27.778  0.0  0.1145  3.0036  ISP81770
      2.096  0.03812  0.2203  0.0576375  0.0  ISP81780
/*  ISP81790
/* ***** VOL.34 ACCUMULATOR LINE ***** ISP81800
      0  0  45.0350E4  27.778  -1.0  0.00244  0.0243  ISP81810
      0.02430  0.00046  0.0243  0.0333375  5.31  ISP81820
/*  ISP81830
/* ***** VOL.35 COLD LEG BREAK NODE ***** ISP81840
      0  0  161.0465E4  288.800  -1.0  0.00161  0.066675  ISP81850
      0.066675  0.00349  0.0667  -0.0333375  0.601748  ISP81860
/*  ISP81870
/* ***** VOL.36 ACCUMULATOR LINE ***** ISP81880
      0  0  161.0359E4  238.850  -1.0  0.00244  0.0243  ISP81890
      0.0243  0.00046  0.0243  0.0333375  5.31  ISP81900
/*  ISP81910
/*  BUBBLE RISE PARAMETER ISP81920
/*  0.0  0.9144  ISP81930
/*  0.8  0.9144  ISP81940
/*  ISP81950
/*  PUMP DESCRIPTION DATA AND CURVE DATA ISP81960
/*  6  5  9  10  13  12  13  11  2  ISP81970
      0.0  1.0E-5  997.856  58.522  0.0114  372.8  ISP81980
      4.8111  1.6139  0.3  ISP81990
/*  ISP82000
/*  HEAD ISP82010
/*  -1.0  1.5  -0.8  1.275  -0.6  1.375  -0.4  1.375  ISP82020
      0.0  1.2  1.0  1.0  ISP82030
/*  -1.0  0.175  -0.5  0.65  0.0  0.975  0.5  1.35  ISP82040
      1.0  1.95  ISP82050
/*  -1.0  0.175  -0.75  -0.15  -0.55  -0.3  -0.275  -0.4  ISP82060
      0.0  -0.35  0.30  -0.20  0.50  0.0  0.80  0.545  ISP82070
      1.0  1.0  ISP82080
/*  -1.0  1.50  -0.80  1.15  -0.60  0.95  -0.40  0.83  ISP82090
      -0.2  0.775  0.0  0.725  0.20  0.725  0.40  0.80  ISP82100
      0.6  1.025  1.0  1.95  ISP82110
/*  TORQUE ISP82120
/*  -1.0  0.62  -0.80  0.68  -0.60  0.53  -0.40  0.46  ISP82130
      -0.20  0.49  0.0  0.54  0.20  0.59  0.40  0.65  ISP82140
      0.60  0.77  0.80  0.95  0.90  0.98  0.95  0.96  ISP82150
      1.0  0.87  ISP82160
/*  -1.0  -1.44  -0.80  -1.25  -0.60  -1.08  -0.40  -0.92  ISP82170
      -0.20  -0.77  0.0  -0.63  0.20  -0.51  0.40  -0.39  ISP82180
      ISP82190
      ISP82200
      ISP82210
      ISP82220
      ISP82230
      ISP82240
      ISP82250
      ISP82260
      ISP82270

```

	1	2	3	4	5	6	7-R	8
	0.60	-0.29	0.80	-0.20	0.90	-0.16	1.0	-0.13
/*								ISP82280
	-1.0	-1.44	-0.80	-1.12	-0.60	-0.79	-0.40	-0.52
/*								ISP82290
	-0.20	-0.31	0.0	-0.15	0.20	0.02	0.40	0.22
	0.60	0.46	0.80	0.71	0.90	0.81	0.95	0.85
	1.0	0.87						
/*								ISP82300
	-1.0	0.62	-0.80	0.53	-0.60	0.46	-0.40	0.42
/*								ISP82310
	-0.2	0.39	0.0	0.36	0.20	0.32	0.40	0.27
	0.6	0.18	0.80	0.05	1.0	-0.13		
/*								ISP82320
	0.0	0.0	1.0E8	0.0				
/*								ISP82330
/*								ISP82340
/*								ISP82350
/*								ISP82360
/*								ISP82370
/*								ISP82380
/*								ISP82390
/*								ISP82400
/*								ISP82410
/*								ISP82420
/*								ISP82430
/*								ISP82440
/*								ISP82450
/*								ISP82460
/*								ISP82470
/*								ISP82480
/*								ISP82490
/*								ISP82500
/*								ISP82510
/*								ISP82520
/*								ISP82530
/*								ISP82540
/*								ISP82550
/*								ISP82560
/*								ISP82570
/*								ISP82580
/*								ISP82590
/*								ISP82600
/*								ISP82610
/*								ISP82620
/*								ISP82630
/*								ISP82640
/*								ISP82650
/*								ISP82660
/*								ISP82670
/*								ISP82680
/*								ISP82690
/*								ISP82700
/*								ISP82710
/*								ISP82720
/*								ISP82730
/*								ISP82740
/*								ISP82750
/*								ISP82760
/*								ISP82770
/*								ISP82780
/*								ISP82790
/*								ISP82800
/*								ISP82810
/*								ISP82820
/*								ISP82830
/*								ISP82840
/*								ISP82850
/*								ISP82860

	1	2	3	4	5	6	7-R	8	
/* *****	JUN.15	TOP OF SG SIMULATOR				*****			ISP82870
	13 14	0 0 0 1	0.0	0.00349	2.9448125	1030.44		ISP82880	
		285.435 285.435 0 0.85	1.0					ISP82890	
/* *****	JUN.16	SG SIMULATOR OUTLET				*****		ISP82900	
	14 15	0 0 0 1	0.0	0.00024	0.401574	1387.54		ISP82910	
		1.40405 1.41583 0 0.85	1.0					ISP82920	
/* *****	JUN.17	PUMP SIMULATOR INLET				*****		ISP82930	
	15 16	0 0 0 1	0.0	0.00024	-1.016	827.54		ISP82940	
		0.844137 1.54353 0 0.85	1.0					ISP82950	
/* *****	JUN.18	PUMP SIMULATOR OUTLET				*****		ISP82960	
	16 17	0 0 0 1	0.0	0.00024	-1.21285	2018.77		ISP82970	
		12.8823 12.438 0 0.85	1.0					ISP82980	
/* *****	JUN.19	VESSEL EXIT				*****		ISP82990	
	22 18	0 0 2 1	0.0	0.00183	0.0	574.74		ISP83000	
		0.677051 1.21442 0 0.85	-1.0					ISP83010	
/* *****	JUN.20	REFLOOD BYPASS EXIT (HOT LEG)				*****		ISP83020	
	19 12	0 0 0 1	0.0	0.00349	0.2492375	0.0		ISP83030	
		0.0 0.0 0 0.85	1.0					ISP83040	
/* *****	JUN.21	REFLOOD BYPASS EXIT (COLD LEG)				*****		ISP83050	
	20 18	0 0 0 1	0.0	0.00349	0.0333375	0.0		ISP83060	
		0.0 0.0 0 0.85	1.0					ISP83070	
/* *****	JUN.22	STEAM OUTLET				*****		ISP83080	
	21 0	1 0 2 1	0.4082	0.00203	5.345176	0.0		ISP83090	
		0.0 0.0 0 0.85	0.6					ISP83100	
/* *****	JUN.23	FEED WATER INLET				*****		ISP83110	
	0 21	1 0 2 1	0.4082	0.00113	3.9307262	0.0		ISP83120	
		0.0 0.0 0 0.85	0.6					ISP83130	
/* *****	JUN.24	DOWNCOMER ANNULUS INLET				*****		ISP83140	
	22 23	0 0 2 1	4.899	0.00534	-0.2667	0.0		ISP83150	
		3.9706E-2 2.2542E-3 0 0.85	-1.0					ISP83160	
/* *****	JUN.25	DOWNCOMER TO LOWER PLENUM				*****		ISP83170	
	23 24	0 0 2 1	4.899	0.00534	-4.147312	0.0		ISP83180	
		4.6518E-2 0.1465 0 0.85	0.0					ISP83190	
/* *****	JUN.26	LOWER PLENUM TO MIXER BOX				*****		ISP83200	
	24 25	0 0 2 1	4.899	0.00713	-4.147312	0.0		ISP83210	
		19.569 19.569 0 0.85	0.0					ISP83220	
/* *****	JUN.27	CORE INLET				*****		ISP83230	
	25 28	0 0 0 2	4.899	0.00492	-3.626866	0.0		ISP83240	
		10.5898 10.5898 0 0.85	0.0					ISP83250	
/* *****	JUN.28	CORE OUTLET				*****		ISP83260	
	32 26	0 0 0 2	4.899	0.00492	-1.950466	0.0		ISP83270	
		7.2754 7.2754 0 0.85	0.0					ISP83280	
/* *****	JUN.29	BREAK PLANE				*****		ISP83290	
	17 27	0 1 0 1	0.0	0.00024	0.2159	978.25		ISP83300	
		1.00777 1.13360 0 0.85	0.6					ISP83310	
/* *****	JUN.30	BREAK PLANE				*****		ISP83320	
	35 27	0 2 0 1	0.0	0.00024	0.0	318.823		ISP83330	
		1.38245 1.15464 0 0.85	0.6					ISP83340	
/* *****	JUN.31	WITHIN CORE REGION				*****		ISP83350	
	28 29	0 0 0 2	4.899	0.00492	-3.347466	0.0		ISP83360	
		0.0 0.0 0 0.85	0.0					ISP83370	
/* *****	JUN.32	WITHIN CORE REGION				*****		ISP83380	
	29 30	0 0 0 2	4.899	0.00492	-3.068066	0.0		ISP83390	
		0.0 0.0 0 0.85	0.0					ISP83400	
/* *****	JUN.33	WITHIN CORE REGION				*****		ISP83410	
	30 31	0 0 0 2	4.899	0.00492	-2.788666	0.0		ISP83420	
		0.0 0.0 0 0.85	0.0					ISP83430	
/* *****	JUN.34	WITHIN CORE REGION				*****		ISP83440	
	31 32	0 0 0 2	4.899	0.00492	-2.509266	0.0		ISP83450	

```

-----1-----2-----3-----4-----5-----6-----7-R-----8
0.0 0.0 0 0.85 0.0 ISP83460
/* ***** JUN.35 ACC EXIT ***** ISP83470
33 34 0 0 0 1 0.0 0.00046 0.0576375 0.0 ISP83480
71.095 1.E6 0 0.85 -1.0 ISP83490
/* ***** JUN.36 ECC INJECTION POINT ***** ISP83500
36 9 0 0 2 1 0.0 0.00046 0.0333375 0.0 ISP83510
71.095 1.E6 0 0.85 -1.0 ISP83520
/* ***** JUN.37 HPIS ***** ISP83530
0 36 2 0 2 1 0.0 0.00015 0.0454875 0.0 ISP83540
0.0 0.0 0 0.85 1.0 ISP83550
/* ***** JUN.38 LPIS ***** ISP83560
0 36 3 0 2 1 0.0 0.00028 0.0454875 0.0 ISP83570
0.0 0.0 0 0.85 1.0 ISP83580
/* ***** JUN.39 COLD LEG BREAK NODE ENTRANCE ***** ISP83590
18 35 0 0 0 1 0.0 0.00349 0.0 292.636 ISP83600
1.0E-10 1.0E-10 0 0.85 1.0 ISP83610
/* ***** JUN.40 WITHIN ACC LINE ***** ISP83620
/* 34 36 0 3 0 1 0.0 0.00046 1.0301175 0.0 ISP83630
/* 142.19 1.E6 0 0.85 -1.0 ISP83640
/* 34 36 0 3 0 1 0.0 0.00046 0.0454875 0.0 ISP83650
142.19 1.E6 0 0.85 -1.0 ISP83660
/* ISP83670
/* CHECK VALVE DATA ISP83680
/* ISP83690
-6 0.0 0.0 0.0 0.0 / BREAK VALVE (J29) ISP83700
-7 0.0 0.0 0.0 0.0 / BREAK VALVE (J30) ISP83710
-8 0.0 0.0 0.0 0.0 / ACC LINE (J40) ISP83720
/* ISP83730
/* ISP83740
/* LEAK DATA ISP83750
/* AT JUNCTION 22 OF SG SECONDARY SIDE ISP83760
/* ISP83770
2 6 1.0338E4 0.6 0.85 ISP83780
0.0 0.4082 8.0 0.4082 12.0 0.2041 24.0 0.0 24.001 0.0 50.0 0.0 ISP83790
/* ISP83800
/* FILL DATA ISP83810
/* AT JUNCTION 23 OF SG SECONDARY SIDE FEED WATER ISP83820
/* ISP83830
3 0 61.1814E4 73.6 ISP83840
0.0 0.4082 1.0 0.0 50.0 0.0 ISP83850
/* HPIS (JUNCTION 37) ISP83860
/* ISP83870
4 0 7.0338E4 27.778 ISP83880
0.0 0.0149 30.0 0.0149 30.001 0.0817 50.0 0.0817 ISP83890
/* ISP83900
/* LPIS (JUNCTION 38) ISP83910
/* ISP83920
2 0 7.0338E4 27.778 ISP83930
0.0 0.299 50.0 0.299 ISP83940
/* ISP83950
/* KINETICS CONSTANT DATA ISP83960
/* ISP83970
1 0 0.0 0.0 ISP83980
30 ISP83990
0.0 1.0 1.23 1.0 1.64 0.795 2.05 0.597 ISP84000
2.18 0.579 2.51 0.579 2.59 0.597 2.86 0.795 ISP84010
3.27 1.0 5.05 1.0 5.45 0.795 6.00 0.597 ISP84020
6.68 0.398 7.36 0.216 7.64 0.199 11.05 0.199 ISP84030
11.45 0.138 12.00 0.121 15.27 0.121 15.82 0.086 ISP84040

```



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-----*-----1-----*-----2-----*-----3-----*-----4-----*-----5-----*-----6-----*-----7-R-----*-----8
16.91  0.086 17.45  0.147 18.00  0.156 19.36  0.156  ISP84050
20.18  0.061 20.72  0.052 26.45  0.022 36.00  0.022  ISP84060
39.55  0.038 42.00  0.038                               ISP84070
/*                               ISP84080
/* HEAT SLAB DATA                               ISP84090
/*                               ISP84100
3  21  1  2.73053 3.39619  6.2100E-3  0.0  0.0  / U-TUBE1  ISP84110
4  21  1  2.73053 3.39619  6.2100E-3  0.0  0.0  / U-TUBE2  ISP84120
0  28  2  0.0     0.3763  1.0085E-3  0.0  0.0  / CORE #1  ISP84130
0  29  2  0.0     0.3763  1.0085E-3  0.0  0.0  / CORE #2  ISP84140
0  30  2  0.0     0.3763  1.0085E-3  0.0  0.0  / CORE #3  ISP84150
0  31  2  0.0     0.3763  1.0085E-3  0.0  0.0  / CORE #4  ISP84160
0  32  2  0.0     0.7526  2.0170E-3  0.0  0.0  / CORE #5  ISP84170
/*                               ISP84180
/* CORE SECTION DATA                               ISP84190
/*                               ISP84200
3      0.2794      0.0146      0.1323      ISP84210
4      0.2794      0.0146      0.2307      ISP84220
5      0.2794      0.0146      0.2553      ISP84230
6      0.2794      0.0146      0.2086      ISP84240
7      0.5588      0.0146      0.1731      ISP84250
/*                               ISP84260
/* SLAB GEOMETRY DATA                               ISP84270
/*                               ISP84280
/* ***** GEOMETRY INDEX 1 *****                               ISP84290
2      1      0      1      3      12.446E-4      1.0      5.1054E-3 / INCONEL600 ISP84300
/* ***** GEOMETRY INDEX 2 *****                               ISP84310
2      4      0      2      2      8.890E-4      0.0      0.0      / B.N.      ISP84320
0      0      3      5      21.830E-4      1.0      / CONSTANTAN ISP84330
0      0      2      3      12.960E-4      0.0      / B.N.      ISP84340
0      0      4      2      9.910E-4      0.0      / ST        ISP84350
/*                               ISP84360
/* MATERIAL THERMAL PROPERTY DATA                               ISP84370
/*                               ISP84380
/* THERMAL CONDUCTIVITY OF INCONEL-600                               ISP84390
/*                               ISP84400
5                               ISP84410
37.8  3.5133E-3  148.9  3.9597E-3  315.6  4.6087E-3  ISP84420
593.3  5.6420E-3  1000.0  7.1553E-3                               ISP84430
/*                               ISP84440
/* HEAT CAPACITY OF INCONEL-600                               ISP84450
/*                               ISP84460
5                               ISP84470
37.8  916.024      204.4  979.463  315.6  1021.595  ISP84480
426.7 1063.888      1000.0  1282.129                               ISP84490
/*                               ISP84500
/* GAP CONDUCTANCE DATA                               ISP84510
/*                               ISP84520
2                               ISP84530
0.0  0.0  1000.0  0.0                               ISP84540
/*                               ISP84550
/* THERMAL CONDUCTIVITY OF BORON-NITRIDE                               ISP84560
/*                               ISP84570
22                               ISP84580
50.0  0.5995E-2  100.0  0.5966E-2  150.0  0.5936E-2  ISP84590
200.0  0.5907E-2  250.0  0.5877E-2  300.0  0.5848E-2  ISP84600
350.0  0.5819E-2  400.0  0.5789E-2  450.0  0.5760E-2  ISP84610
500.0  0.5731E-2  550.0  0.5701E-2  600.0  0.5672E-2  ISP84620
650.0  0.5643E-2  700.0  0.5613E-2  750.0  0.5584E-2  ISP84630

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	1	2	3	4	5	6	7-R	8	
	800.0	0.5555E-2	850.0	0.5525E-2	900.0	0.5496E-2	ISP84640		
	950.0	0.5467E-2	1000.0	0.5437E-2	1050.0	0.5408E-2	ISP84650		
	1100.0	0.5379E-2					ISP84660		
/*							ISP84670		
/*	HEAT CAPACITY OF BORON-NITRIDE							ISP84680	
/*							ISP84690		
	22						ISP84700		
	50.0	0.4625E3	100.0	0.5279E3	150.0	0.5874E3	ISP84710		
	200.0	0.6413E3	250.0	0.6899E3	300.0	0.7335E3	ISP84720		
	350.0	0.7726E3	400.0	0.8074E3	450.0	0.8382E3	ISP84730		
	500.0	0.8654E3	550.0	0.8895E3	600.0	0.9105E3	ISP84740		
	650.0	0.9289E3	700.0	0.9451E3	750.0	0.9593E3	ISP84750		
	800.0	0.9718E3	850.0	0.9831E3	900.0	0.9935E3	ISP84760		
	950.0	0.1003E4	1000.0	0.1013E4	1050.0	0.1022E4	ISP84770		
	1100.0	0.1032E4					ISP84780		
/*							ISP84790		
/*	GAP CONDUCTANCE							ISP84800	
	2						ISP84810		
	0.0	0.0	1000.0	0.0			ISP84820		
/*							ISP84830		
/*	THERMAL CONDUCTIVITY OF CONSTANTAN							ISP84840	
/*							ISP84850		
	22						ISP84860		
	50.0	0.6138E-2	100.0	0.6336E-2	150.0	0.6535E-2	ISP84870		
	200.0	0.6733E-2	250.0	0.6931E-2	300.0	0.7129E-2	ISP84880		
	350.0	0.7328E-2	400.0	0.7526E-2	450.0	0.7724E-2	ISP84890		
	500.0	0.7923E-2	550.0	0.8121E-2	600.0	0.8319E-2	ISP84900		
	650.0	0.8517E-2	700.0	0.8716E-2	750.0	0.8914E-2	ISP84910		
	800.0	0.9112E-2	850.0	0.9311E-2	900.0	0.9509E-2	ISP84920		
	950.0	0.9707E-2	1000.0	0.9905E-2	1050.0	0.1010E-1	ISP84930		
	1100.0	0.1030E-1					ISP84940		
/*							ISP84950		
/*	HEAT CAPACITY OF CONSTANTAN							ISP84960	
	22						ISP84970		
	50.0	0.8771E3	100.0	0.8945E3	150.0	0.9120E3	ISP84980		
	200.0	0.9294E3	250.0	0.9469E3	300.0	0.9643E3	ISP84990		
	350.0	0.9818E3	400.0	0.9992E3	450.0	0.1017E4	ISP85000		
	500.0	0.1034E4	550.0	0.1052E4	600.0	0.1069E4	ISP85010		
	650.0	0.1086E4	700.0	0.1104E4	750.0	0.1121E4	ISP85020		
	800.0	0.1139E4	850.0	0.1156E4	900.0	0.1174E4	ISP85030		
	950.0	0.1191E4	1000.0	0.1209E4	1050.0	0.1226E4	ISP85040		
	1100.0	0.1244E4					ISP85050		
/*							ISP85060		
/*	GAP CONDUCTANCE DATA							ISP85070	
	2						ISP85080		
	0.0	0.0	1000.0	0.0			ISP85090		
/*							ISP85100		
/*	THERMAL CONDUCTIVITY OF STAINLESS STEEL							ISP85110	
/*							ISP85120		
	22						ISP85130		
	50.0	0.3287E-2	100.0	0.3446E-2	150.0	0.3604E-2	ISP85140		
	200.0	0.3763E-2	250.0	0.3921E-2	300.0	0.4079E-2	ISP85150		
	350.0	0.4238E-2	400.0	0.4396E-2	450.0	0.4555E-2	ISP85160		
	500.0	0.4713E-2	550.0	0.4872E-2	600.0	0.5030E-2	ISP85170		
	650.0	0.5189E-2	700.0	0.5347E-2	750.0	0.5505E-2	ISP85180		
	800.0	0.5664E-2	850.0	0.5822E-2	900.0	0.5981E-2	ISP85190		
	950.0	0.6139E-2	1000.0	0.6298E-2	1050.0	0.6456E-2	ISP85200		
	1100.0	0.6614E-2					ISP85210		
/*							ISP85220		

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-----1-----2-----3-----4-----5-----6-----7-R-----8
/* HEAT CAPACITY OF STAINLESS STEEL                                ISP85230
/*                                                                    ISP85240
    22                                                                ISP85250
    50.0  0.9204E3  100.0  0.9350E3  150.0  0.9495E3  ISP85260
    200.0 0.9640E3  250.0  0.9783E3  300.0  0.9926E3  ISP85270
    350.0 0.1007E4  400.0  0.1021E4  450.0  0.1035E4  ISP85280
    500.0 0.1049E4  550.0  0.1062E4  600.0  0.1076E4  ISP85290
    650.0 0.1090E4  700.0  0.1103E4  750.0  0.1117E4  ISP85300
    800.0 0.1130E4  850.0  0.1143E4  900.0  0.1156E4  ISP85310
    950.0 0.1170E4 1000.0  0.1182E4 1050.0  0.1195E4  ISP85320
    1100.0 0.1208E4                                         ISP85330
/*                                                                    ISP85340
/* GAP CONDUCTANCE DATA                                         ISP85350
/*                                                                    ISP85360
    2                                                                    ISP85370
    0.0  0.0  1000.0  0.0                                         ISP85380
/*                                                                    ISP85390
/* END OF DATA                                                  ISP85400
/*                                                                    ISP85410
/*                                                                    ISP85420
/******
/* INDIVIDUAL PARAMETERS CORRESPONDING TO MEASUREMENT DATA * ISP85430
/* PRESSURE * ISP85440
/* PU-PRIZE ----- AP 10 * ISP85450
/* PB-42 ----- AP 17 * ISP85460
/* PB-23 ----- AP 35 * ISP85470
/* PV-UP+10 ----- AP 26 * ISP85480
/* PU-ACC ----- AP 33 * ISP85490
/* PU-SGSD ----- AP 21 * ISP85500
/* DIFFERENTIAL PRESSURE * ISP85510
/* DPU-10-12 ----- AP 6 - AP 8 * ISP85520
/* DPB-32-36L ----- AP 12- AP 15 * ISP85530
/* DPB-38-40 ----- AP 15- AP 17 * ISP85540
/* DPV-LP-UP ----- AP 24- AP 26 * ISP85550
/* FLOW RATE * ISP85560
/* FTV-COREIN (V) ----- JW 27 * ISP85570
/* FTU-15 (V) ----- JW 10 * ISP85580
/* FTU-PRIZE (V) ----- JW 12 * ISP85590
/* FTU-LPIS (V) ----- JW 38 * ISP85600
/* FTU-HPIS (V) ----- JW 37 * ISP85610
/* FTU-ACC (V) ----- JW 35 * ISP85620
/* FTU-10, GU-10 ----- JW 7 * ISP85630
/* FDB-42, GB-42R ----- JW 29 * ISP85640
/* FDR-23, GB-23R ----- JW 30 * ISP85650
/* FLUID DENSITY * ISP85660
/* GB-42VR ----- AR 17 * ISP85670
/* GB-23VR ----- AR 35 * ISP85680
/* GU-15C ----- AR 9 * ISP85690
/* GU-10 ----- AR 6 * ISP85700
/* GVCOR-15OHZ ----- AR 25 * ISP85710
/* GV161/192D ----- AR 24 * ISP85720
/* FLUID TEMPERATURE * ISP85730
/* TFU-PRIZE ----- AT 11 * ISP85740
/* TFB-23 ----- AT 35 * ISP85750
/* TFV-UP+10 ----- AT 26 * ISP85760
/* HT COEFF. AND AVERAGE QUALITY OF AVERAGE CORE REGION * ISP85770
/* HC 28 , AX 28 ----- AT ELEVATION 8"ABOVE BOTTOM * ISP85780
/* HC 29 , AX 29 ----- AT ELEVATION 14"ABOVE BOTTOM* ISP85790
/* HC 30 , AX 30 ----- AT ELEVATION 28"ABOVE BOTTOM* ISP85800
/* HC 31 , AX 31 ----- AT ELEVATION 39"ABOVE BOTTOM* ISP85810

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-----*-----1-----*-----2-----*-----3-----*-----4-----*-----5-----*-----6-----*-----7-R-----*-----8
/*      INTEGRATED MASS INVENTORY                                     *      ISP85820
/*                                                                 *      ISP85830
/******                                                           *      ISP85840
/*                                                                 *      ISP85850
```

Appendix 2 List of Input-data (RUN 3)

```

/*
/*      AN ANALYSIS OF SEMISCALE S-06-3 TEST BY ALARM-P1 CODE
/*
/*      ALARM-P1 PREDICTION OF CSNI STANDARD PROBLEM NO.8
/*
/*      PROBLEM DIMENSION
/*
/* LDMP NEDI NTC  NTRP  NVOL NBUB NJUN NPMP NPMPC NCKV NLK NLL
/* NSLB NOCOR NGOM  NMTX NHTX  POWRO
/* -3  18  10  10  36  2   40  1   1   3  1  3
/*   7   5   2   4   0   1.0058
/*
/*      EDIT VARIABLE
/*
/* JW J29 JW J30 AP N10 AP N17 AP N35 AP N21 AP N26 ST N28 ST N29
/* ST N30 ST N31 JW J7  AT N11 AT N18 AT N26 WM N27 TM N27 HC N28
/*
/*      TIME STEP SIZE
/*
/*      100      20      1      2000      0.000005      0.01
/*      100      10      1      1000      0.00001      0.05
/*      100      40      1      400      0.000025      0.3
/*      100      20      1      200      0.00005      0.5
/*      100      20      1      100      0.0001      5.0
/*      100      20      1      40      0.00025      10.0
/*      100      10      1      20      0.0005      14.0
/*      100      20      1      40      0.00025      25.0
/*      100      50      1      100      0.0001      25.0
/*      100      20      1      200      0.00005      50.0
/*
/*      TRIP CONTROL
/*
/*      1      1      0      0      40.0      0.0      / END OF PROBLEM
/*      21     1      0      0      0.0      0.0      / STEAM OUTLET J22
/*      3      1      0      0      0.0      0.0      / POWER
/*      4      1      0      0      100.0     0.0      / PUMP TRIP
/*      51     1      0      0      0.0      0.0      / FEED WATER J23
/*      52     -4     36     0      127.5778E4  0.0      / HPIS J37
/*      53     -4     36     0      18.6126E4  0.0      / LPIS J38
/*      6      1      0      0      0.00001   0.0      / BREAK
/*      7      1      0      0      0.00001   0.0      / BREAK
/*      8      1      0      0      18.2      0.0      / ACC VALVE J40
/*
/*      VOLUME DATA
/*
/*      IBUB NPUMP P      TEMP      HORX      V      ZVOL
/*      ZM      FLOWA      DIAMV      ELEV      FLOWL
/* ***** VOL.1 INTACT LOOP HOT LEG *****
/*      0      0      161.7740E4      326.444      -1.0      0.01082      0.3086735
/*      0.3086735      0.00349      0.0667      0.1825625      3.17
/*

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-----1-----2-----3-----4-----5-----6-----7-R-----8
/* ***** VOL.2 SG INLET PLENUM ***** ISP80510
   0 0 161.6642E4 326.444 -1.0 0.00963 0.48514 ISP80520
   0.48514 0.01984 0.1590 0.491236 0.0 ISP80530
/* ISP80540
/* ***** VOL.3 SG U-TUBE ***** ISP80550
   0 0 161.5263E4 -343.52 -1.0 0.01140 2.629916 ISP80560
   2.629916 0.00442 0.0102 0.976376 0.0 ISP80570
/* ISP80580
/* ***** VOL.4 SG U-TUBE ***** ISP80590
   0 0 161.4936E4 -320.14 -1.0 0.01140 2.629916 ISP80600
   2.629916 0.00442 0.0102 0.976376 0.0 ISP80610
/* ISP80620
/* ***** VOL.5 SG OUTLET PLENUM ***** ISP80630
   0 0 161.5913E4 290.889 -1.0 0.00963 0.48514 ISP80640
   0.48514 0.01984 0.1590 0.491236 0.0 ISP80650
/* ISP80660
/* ***** VOL.6 PUMP SUCTION LEG ***** ISP80670
   0 0 161.4422E4 290.889 -1.0 0.01018 1.543812 ISP80680
   1.543812 0.00349 0.0667 -1.052576 0.0 ISP80690
/* ISP80700
/* ***** VOL.7 ACTIVE PUMP ***** ISP80710
   0 1 161.7334E4 290.889 -1.0 0.00408 0.2809875 ISP80720
   0.2809875 0.00349 0.0667 -0.24765 0.0 ISP80730
   169.53 ISP80740
/* ISP80750
/* ***** VOL.8 INTACT LOOP COLD LEG NEAR PUMP ***** ISP80760
   0 0 162.0807E4 290.889 -1.0 0.00425 0.066675 ISP80770
   0.066675 0.00349 0.0667 -0.0333375 1.25 ISP80780
/* ISP80790
/* ***** VOL.9 INTACT LOOP COLD LEG ***** ISP80800
   0 0 162.0714E4 290.889 -1.0 0.00425 0.066675 ISP80810
   0.066675 0.00349 0.0667 -0.0333375 1.25 ISP80820
/* ISP80830
/* ***** VOL.10 PRESSURIZER ***** ISP80840
   2 0 161.6584E4 -1.0 0.0 0.02741 1.143 ISP80850
   0.62547 0.02466 0.0 1.86055 0.0 ISP80860
/* ISP80870
/* ***** VOL.11 PRESSURIZER SURGE LINE ***** ISP80880
   0 0 161.7364E4 242.850 -1.0 0.00037 1.8077125 ISP80890
   1.8077125 4.3E-5 0.0 0.2492375 3.9000 ISP80900
/* ISP80910
/* ***** VOL.12 BROKEN LOOP HOT LEG ***** ISP80920
   0 0 161.8662E4 322.960 -1.0 0.00315 0.2190115 ISP80930
   0.2190115 0.00349 0.0667 0.1825625 1.00646 ISP80940
/* ISP80950
/* ***** VOL.13 SG SIMULATOR ***** ISP80960
   0 0 161.7808E4 -349.762 -1.0 0.00852 2.6099135 ISP80970
   2.6099135 0.00374 0.0690 0.401574 2.57658 ISP80980
/* ISP80990
/* ***** VOL.14 SG SIMULATOR ***** ISP81000
   0 0 161.7808E4 -346.519 -1.0 0.00852 2.6099135 ISP81010
   2.6099135 0.00374 0.0690 0.401574 2.57658 ISP81020
/* ISP81030
/* ***** VOL.15 PUMP SUCTION LEG ***** ISP81040
   0 0 161.8278E4 317.800 -1.0 0.00252 1.417574 ISP81050
   1.417574 0.00158 0.0449 -1.016 1.40081 ISP81060
/* ISP81070
/* ***** VOL.16 PUMP SIMULATOR ***** ISP81080
   0 0 161.8882E4 317.000 -1.0 0.00147 0.2301875 ISP81090

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	1	2	3	4	5	6	7-R	8
	0.2301875		0.00198	0.0016	-1.2461875	23.3		ISP81100
/*								ISP81110
/* ***** VOL.17 HOT LEG BREAK NODE *****								ISP81120
	0	0	161.8407E4	316.970	-1.0	0.00227	1.4954250	ISP81130
				0.00145	0.0429	-1.2461875	1.50799	ISP81140
/*								ISP81150
/* ***** VOL.18 BROKEN LOOP COLD LEG *****								ISP81160
	0	0	162.0795E4	290.720	-1.0	0.00461	0.066675	ISP81170
				0.00349	0.0667	-0.0333375	100.	ISP81180
/*								ISP81190
/* ***** VOL.19 HOT LEG SIDE REFLOOD BYPASS LINE *****								ISP81200
	0	0	161.8471E4	315.850	-1.0	0.00538	0.552323	ISP81210
				0.00349	0.0667	0.1825625	0.0	ISP81220
/*								ISP81230
/* ***** VOL.20 COLD LEG SIDE REFLOOD BYPASS LINE *****								ISP81240
	0	0	162.0507E4	288.850	-1.0	0.00640	0.768223	ISP81250
				0.00349	0.0667	-0.0333375	0.0	ISP81260
/*								ISP81270
/* ***** VOL.21 SG SECONDARY SYSTEM *****								ISP81280
	1	0	67.9253E4	0.0	0.03208	0.19820	4.6580	ISP81290
				0.0	0.976376		0.0	ISP81300
/*								ISP81310
/* ***** VOL.22 PRESSURE VESSEL INLET PLENUM *****								ISP81320
	0	0	162.0396E4	290.889	-1.0	0.00504	0.45847	ISP81330
				0.00548	0.0412	-0.2667	0.0	ISP81340
/*								ISP81350
/* ***** VOL.23 DOWNCOMER ANNULUS *****								ISP81360
	0	0	162.1922E4	290.889	-1.0	0.02183	3.880612	ISP81370
				0.00534	0.0214	-4.147312	3.9	ISP81380
/*								ISP81390
/* ***** VOL.24 LOWER PLENUM *****								ISP81400
	0	0	162.3555E4	290.889	-1.0	0.02161	0.731774	ISP81410
				0.00623	0.0	-4.879086	1.0	ISP81420
/*								ISP81430
/* ***** VOL.25 MIXER HOUSING *****								ISP81440
	0	0	162.2452E4	290.889	-1.0	0.00371	0.520446	ISP81450
				0.00713	0.0	-4.147312	0.0	ISP81460
/*								ISP81470
/* ***** VOL.26 UPPER PLENUM *****								ISP81480
	0	0	161.8628E4	326.444	-1.0	0.02620	2.972816	ISP81490
				0.00713	0.0	-1.950466	2.5	ISP81500
/*								ISP81510
/* ***** VOL.27 PRESSURE SUPPRESSION SYSTEM *****								ISP81520
	1	0	3.5150E4	16.35	0.0	100.	4.5225462	ISP81530
				0.70205	0.9454	-2.5654	0.0	ISP81540
/*								ISP81550
/* ***** VOL.28 CORE REGION #1 *****								ISP81560
	0	0	162.1384E4	-311.09	-1.0	0.00137	0.2794	ISP81570
				0.00492	0.0113	-3.626866	0.0	ISP81580
/*								ISP81590
/* ***** VOL.29 CORE REGION #2 *****								ISP81600
	0	0	162.1147E4	-319.99	-1.0	0.00137	0.2794	ISP81610
				0.00492	0.0113	-3.347466	0.0	ISP81620
/*								ISP81630
/* ***** VOL.30 CORE REGION #3 *****								ISP81640
	0	0	162.0912E4	-331.90	-1.0	0.00137	0.2794	ISP81650
				0.00492	0.0113	-3.068066	0.0	ISP81660
/*								ISP81670
/* ***** VOL.31 CORE REGION #4 *****								ISP81680

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-----1-----2-----3-----4-----5-----6-----7-R-----8
      0  0  162.0682E4  -343.28  -1.0  0.00137  0.2794  ISP81690
      0.2794  0.00492  0.0113  -2.788666  0.0  ISP81700
/*  ISP81710
/* ***** VOL.32 CORE REGION #5 ***** ISP81720
      0  0  162.0348E4  -352.64  -1.0  0.00274  0.5588  ISP81730
      0.5588  0.00492  0.0113  -2.509266  0.0  ISP81740
/*  ISP81750
/* ***** VOL.33 ACCUMULATOR TANK ***** ISP81760
      2  0  46.0400E4  27.778  0.0  0.1145  3.0036  ISP81770
      2.096  0.03812  0.2203  0.0576375  0.0  ISP81780
/*  ISP81790
/* ***** VOL.34 ACCUMULATOR LINE ***** ISP81800
      0  0  46.0680E4  27.778  -1.0  0.00244  0.0243  ISP81810
      0.02430  0.00046  0.0243  0.0333375  5.31  ISP81820
/*  ISP81830
/* ***** VOL.35 COLD LEG BREAK NODE ***** ISP81840
      0  0  162.0795E4  288.800  -1.0  0.00161  0.066675  ISP81850
      0.066675  0.00349  0.0667  -0.0333375  0.601748  ISP81860
/*  ISP81870
/* ***** VOL.36 ACCUMULATOR LINE ***** ISP81880
      0  0  162.0689E4  238.850  -1.0  0.00244  0.0243  ISP81890
      0.0243  0.00046  0.0243  0.0333375  5.31  ISP81900
/*  ISP81910
/*  BUBBLE RISE PARAMETER ISP81920
/*  0.0  0.9144 ISP81930
/*  0.8  0.9144 ISP81940
/*  0.0  0.9144 ISP81950
/*  PUMP DESCRIPTION DATA AND CURVE DATA ISP81960
/*  6  5  9  10  13  12  13  11  2 ISP81970
      0.0  1.0E-5  997.856  58.522  0.0114  372.8  ISP81980
      4.8111  1.6139  0.3  ISP81990
/*  ISP82000
/*  HEAD ISP82010
/*  -1.0  1.5  -0.8  1.275  -0.6  1.375  -0.4  1.375  ISP82020
      0.0  1.2  1.0  1.0  ISP82030
/*  -1.0  0.175  -0.5  0.65  0.0  0.975  0.5  1.35  ISP82040
      1.0  1.95  ISP82050
/*  -1.0  0.175  -0.75  -0.15  -0.55  -0.3  -0.275  -0.4  ISP82060
      0.0  -0.35  0.30  -0.20  0.50  0.0  0.80  0.545  ISP82070
      1.0  1.0  ISP82080
/*  -1.0  1.50  -0.80  1.15  -0.60  0.95  -0.40  0.83  ISP82090
      -0.2  0.775  0.0  0.725  0.20  0.725  0.40  0.80  ISP82100
      0.6  1.025  1.0  1.95  ISP82110
/*  TORQUE ISP82120
/*  -1.0  0.62  -0.80  0.68  -0.60  0.53  -0.40  0.46  ISP82130
      -0.20  0.49  0.0  0.54  0.20  0.59  0.40  0.65  ISP82140
      0.60  0.77  0.80  0.95  0.90  0.98  0.95  0.96  ISP82150
      1.0  0.87  ISP82160
/*  -1.0  -1.44  -0.80  -1.25  -0.60  -1.08  -0.40  -0.92  ISP82170
      -0.20  -0.77  0.0  -0.63  0.20  -0.51  0.40  -0.39  ISP82180

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	1	2	3	4	5	6	7-R	8
	0.60	-0.29	0.80	-0.20	0.90	-0.16	1.0	-0.13
/*								ISP82280
								ISP82290
/*	-1.0	-1.44	-0.80	-1.12	-0.60	-0.79	-0.40	-0.52
								ISP82300
	-0.20	-0.31	0.0	-0.15	0.20	0.02	0.40	0.22
								ISP82310
	0.60	0.46	0.80	0.71	0.90	0.81	0.95	0.85
								ISP82320
	1.0	0.87						
								ISP82330
/*								ISP82340
								ISP82350
/*	-1.0	0.62	-0.80	0.53	-0.60	0.46	-0.40	0.42
								ISP82360
	-0.2	0.39	0.0	0.36	0.20	0.32	0.40	0.27
								ISP82370
	0.6	0.18	0.80	0.05	1.0	-0.13		
								ISP82380
/*								ISP82390
	0.0	0.0	1.0E8	0.0				
								ISP82400
/*								ISP82410
/*	JUNCTION DATA							
/*								ISP82420
/*	IW1	IW2	IP	IV	IA	JEN	JCH	WP
/*								AJUN
/*								ZJUN
/*								INERTA
/*	FRIFF	FRIFR	ANG	ZACOE	CONTCZ	CONTCM		
/*	***** JUN.1 UPPER PLENUM TO HOT LEG *****							
	26	1	0	2	1	0	4.899	0.00183
								0.2159
	0.0		0.0	0	0.4		0.6	1.0
								0.0
/*	***** JUN.2 SG INLET *****							
	1	2	0	0	1	0	4.899	0.00349
								0.491236
	6.198		6.198	0	0.4		0.6	1.0
								0.0
/*	***** JUN.3 INLET PLENUM TO U-TUBE *****							
	2	3	0	0	1	0	4.899	0.00442
								0.976376
	0.0		0.0	0	0.4		0.6	1.0
								0.0
/*	***** JUN.4 TOP OF U-TUBE *****							
	3	4	0	0	1	0	4.899	0.00442
								3.531108
	0.0		0.0	0	0.4		0.6	1.0
								0.0
/*	***** JUN.5 U-TUBE TO OUTLET PLENUM *****							
	4	5	0	0	1	0	4.899	0.00442
								0.976376
	0.0		0.0	0	0.4		0.6	1.0
								0.0
/*	***** JUN.6 SG OUTLET *****							
	5	6	0	0	1	0	4.899	0.00349
								0.491236
	15.4395		15.4395	0	0.4		0.6	1.0
								0.0
/*	***** JUN.7 PUMP INLET *****							
	6	7	-1	0	0	1	4.899	0.00349
								-0.24765
	5.30		4.86	0	0.4		0.6	1.0
								0.0
/*	***** JUN.8 PUMP OUTLET *****							
	7	8	1	0	0	1	4.899	0.00349
								0.0
	1.65		1.65	0	0.4		0.6	-1.0
								0.0
/*	***** JUN.9 WITHIN COLD LEG *****							
	8	9	0	0	0	1	4.899	0.00349
								0.0
	0.467		7.32	0	0.4		0.6	-1.0
								0.0
/*	***** JUN.10 VESSEL INLET *****							
	9	22	0	0	2	1	4.899	0.00183
								0.0
	0.658		1.466	0	0.4		0.6	-1.0
								0.0
/*	***** JUN.11 PRESSURIZER OUTLET *****							
	10	11	0	0	0	1	0	0.0
								4.3E-5
	10.0		10.0	0	0.4		0.6	0.6
								2.05695
/*	***** JUN.12 SURGE LINE OUTLET *****							
	11	1	0	0	2	1	0	0.0
								4.3E-5
	0.0		0.0	0	0.4		0.6	0.6
								0.2492375
/*	***** JUN.13 VESSEL TO HOT LEG *****							
	26	12	0	0	2	1	0	0.0
								0.00183
	0.677051		1.2144	0	0.4		0.6	1.0
								0.2159
/*	***** JUN.14 SG SIMULATOR INLET *****							
	12	13	0	0	0	1	0	0.0
								0.00024
	1.41181		1.41146	0	0.4		0.6	1.0
								0.401574
								1012.61
								ISP82850
								ISP82860

	1	2	3	4	5	6	7-R	8
/*	*****	JUN.15	TOP OF SG SIMULATOR	*****				ISP82870
	13	14	0 0 0 1 0 0.0	0.00349	2.9448125	1030.44		ISP82880
			285.435 285.435 0 0.4 0.6 1.0					ISP82890
/*	*****	JUN.16	SG SIMULATOR OUTLET	*****				ISP82900
	14	15	0 0 0 1 0 0.0	0.00024	0.401574	1387.54		ISP82910
			1.40405 1.41583 0 0.4 0.6 1.0					ISP82920
/*	*****	JUN.17	PUMP SIMULATOR INLET	*****				ISP82930
	15	16	0 0 0 1 0 0.0	0.00024	-1.016	827.54		ISP82940
			0.844137 1.54353 0 0.4 0.6 1.0					ISP82950
/*	*****	JUN.18	PUMP SIMULATOR OUTLET	*****				ISP82960
	16	17	0 0 0 1 0 0.0	0.00024	-1.21285	2018.77		ISP82970
			12.8823 12.438 0 0.4 0.6 1.0					ISP82980
/*	*****	JUN.19	VESSEL EXIT	*****				ISP82990
	22	18	0 0 2 1 0 0.0	0.00183	0.0	574.74		ISP83000
			0.677051 1.21442 0 0.4 0.6 -1.0					ISP83010
/*	*****	JUN.20	REFLOOD BYPASS EXIT (HOT LEG)	*****				ISP83020
	19	12	0 0 0 1 0 0.0	0.00349	0.2492375	0.0		ISP83030
			0.0 0.0 0 0.4 0.6 1.0					ISP83040
/*	*****	JUN.21	REFLOOD BYPASS EXIT (COLD LEG)	*****				ISP83050
	20	18	0 0 0 1 0 0.0	0.00349	0.0333375	0.0		ISP83060
			0.0 0.0 0 0.4 0.6 1.0					ISP83070
/*	*****	JUN.22	STEAM OUTLET	*****				ISP83080
	21	0	1 0 2 1 0 0.4082	0.00203	5.345176	0.0		ISP83090
			0.0 0.0 0 0.4 0.6 0.6					ISP83100
/*	*****	JUN.23	FEED WATER INLET	*****				ISP83110
	0	21	1 0 2 1 0 0.4082	0.00113	3.9307262	0.0		ISP83120
			0.0 0.0 0 0.4 0.6 0.6					ISP83130
/*	*****	JUN.24	DOWNCOMER ANNULUS INLET	*****				ISP83140
	22	23	0 0 2 1 0 4.899	0.00534	-0.2667	0.0		ISP83150
			3.9706E-2 2.2542E-3 0 0.4 0.6 -1.0					ISP83160
/*	*****	JUN.25	DOWNCOMER TO LOWER PLENUM	*****				ISP83170
	23	24	0 0 2 1 0 4.899	0.00534	-4.147312	0.0		ISP83180
			4.6518E-2 0.1465 0 0.4 0.6 1.0					ISP83190
/*	*****	JUN.26	LOWER PLENUM TO MIXER BOX	*****				ISP83200
	24	25	0 0 2 1 0 4.899	0.00713	-4.147312	0.0		ISP83210
			19.569 19.569 0 0.4 0.6 1.0					ISP83220
/*	*****	JUN.27	CORE INLET	*****				ISP83230
	25	28	0 0 0 2 0 4.899	0.00492	-3.626866	0.0		ISP83240
			10.5898 10.5898 0 0.4 0.6 1.0					ISP83250
/*	*****	JUN.28	CORE OUTLET	*****				ISP83260
	32	26	0 0 0 2 0 4.899	0.00492	-1.950466	0.0		ISP83270
			7.2704 7.2704 0 0.4 0.6 1.0					ISP83280
/*	*****	JUN.29	BREAK PLANE	*****				ISP83290
	17	27	0 1 0 1 0 0.0	0.00024	0.2159	978.25		ISP83300
			1.00777 1.13360 0 0.4 0.6 0.6					ISP83310
/*	*****	JUN.30	BREAK PLANE	*****				ISP83320
	35	27	0 2 0 1 0 0.0	0.00024	0.0	318.823		ISP83330
			1.38245 1.15464 0 0.4 0.6 0.6					ISP83340
/*	*****	JUN.31	WITHIN CORE REGION	*****				ISP83350
	28	29	0 0 0 2 0 4.899	0.00492	-3.347466	0.0		ISP83360
			0.0 0.0 0 0.4 0.6 1.0					ISP83370
/*	*****	JUN.32	WITHIN CORE REGION	*****				ISP83380
	29	30	0 0 0 2 0 4.899	0.00492	-3.068066	0.0		ISP83390
			0.0 0.0 0 0.4 0.6 1.0					ISP83400
/*	*****	JUN.33	WITHIN CORE REGION	*****				ISP83410
	30	31	0 0 0 2 0 4.899	0.00492	-2.788666	0.0		ISP83420
			0.0 0.0 0 0.4 0.6 1.0					ISP83430
/*	*****	JUN.34	WITHIN CORE REGION	*****				ISP83440
	31	32	0 0 0 2 0 4.899	0.00492	-2.509266	0.0		ISP83450

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-----1-----2-----3-----4-----5-----6-----7-R-----8
0.0 0.0 0 0.4 0.6 1.0 ISP83460
/* ***** JUN.35 ACC EXIT ***** ISP83470
33 34 0 0 0 1 0 0.0 0.00046 0.0576375 0.0 ISP83480
92.4 1.E6 0 0.4 0.6 -1.0 ISP83490
/* ***** JUN.36 ECC INJECTION POINT ***** ISP83500
36 9 0 0 2 1 0 0.0 0.00046 0.0333375 0.0 ISP83510
92.4 1.E6 0 0.4 0.6 -1.0 ISP83520
/* ***** JUN.37 HPIS ***** ISP83530
0 36 2 0 2 1 0 0.0 0.00015 0.0454875 0.0 ISP83540
0.0 0.0 0 0.4 0.6 1.0 ISP83550
/* ***** JUN.38 LPIS ***** ISP83560
0 36 3 0 2 1 0 0.0 0.00028 0.0454875 0.0 ISP83570
0.0 0.0 0 0.4 0.6 1.0 ISP83580
/* ***** JUN.39 COLD LEG BREAK NODE ENTRANCE ***** ISP83590
18 35 0 0 0 1 0 0.0 0.00349 0.0 292.636 ISP83600
1.0E-10 1.0E-10 0 0.4 0.6 1.0 ISP83610
/* ***** JUN.40 WITHIN ACC LINE ***** ISP83620
34 36 0 3 0 1 0 0.0 0.00046 0.0454875 0.0 ISP83630
184.8 1.E6 0 0.4 0.6 -1.0 ISP83640
/* ISP83650
/* CHECK VALVE DATA ISP83660
/* ISP83670
-6 0.0 0.0 0.0 0.0 / BREAK VALVE (J29) ISP83680
-7 0.0 0.0 0.0 0.0 / BREAK VALVE (J30) ISP83690
-8 0.0 0.0 0.0 0.0 / ACC LINE (J40) ISP83700
/* ISP83710
/* ISP83720
/* LEAK DATA ISP83730
/* AT JUNCTION 22 OF SG SECONDARY SIDE ISP83740
/* ISP83750
2 6 0 2.0668E4 0.6 0.6 0.4 ISP83760
0.0 0.4082 8.0 0.4082 12.0 0.2041 24.0 0.0 24.001 0.0 50.0 0.0 ISP83770
/* ISP83780
/* FILL DATA ISP83790
/* AT JUNCTION 23 OF SG SECONDARY SIDE FEED WATER ISP83800
/* ISP83810
3 0 62.2144E4 73.6 ISP83820
0.0 0.4082 1.0 0.0 50.0 0.0 ISP83830
/* HPIS (JUNCTION 37) ISP83840
/* ISP83850
4 0 8.0668E4 27.778 ISP83860
0.0 0.0149 30.0 0.0149 30.001 0.0817 50.0 0.0817 ISP83870
/* ISP83880
/* LPIS (JUNCTION 38) ISP83890
/* ISP83900
2 0 8.0668E4 27.778 ISP83910
0.0 0.299 50.0 0.299 ISP83920
/* ISP83930
/* KINETICS CONSTANT DATA ISP83940
/* ISP83950
1 0 0.0 0.0 ISP83960
30 ISP83970
0.0 1.0 1.23 1.0 1.64 0.795 2.05 0.597 ISP83980
2.18 0.579 2.51 0.579 2.59 0.597 2.86 0.795 ISP83990
3.27 1.0 5.05 1.0 5.45 0.795 5.70 0.605 ISP84000
6.40 0.400 7.36 0.216 7.64 0.199 11.05 0.199 ISP84010
11.45 0.138 12.00 0.124 15.00 0.124 15.82 0.086 ISP84020
16.91 0.086 17.45 0.147 18.20 0.160 19.36 0.156 ISP84030
20.30 0.055 26.20 0.055 27.30 0.023 34.00 0.023 ISP84040

```

```

-----*-----1-----*-----2-----*-----3-----*-----4-----*-----5-----*-----6-----*-----7-R-----*-----8
39.55  0.038 40.20  0.043
/*
/* HEAT SLAB DATA
/*
3  21  1  2.73053 3.39619 6.2100E-3  0.0  0.0  / U-TUBE1  ISP84090
4  21  1  2.73053 3.39619 6.2100E-3  0.0  0.0  / U-TUBE2  ISP84100
0  28  2  0.0      0.3384 9.0699E-4  0.0  0.0  / CORE #1  ISP84110
0  29  2  0.0      0.3384 9.0699E-4  0.0  0.0  / CORE #2  ISP84120
0  30  2  0.0      0.3384 9.0699E-4  0.0  0.0  / CORE #3  ISP84130
0  31  2  0.0      0.3384 9.0699E-4  0.0  0.0  / CORE #4  ISP84140
0  32  2  0.0      0.6768 1.8140E-3  0.0  0.0  / CORE #5  ISP84150
/*
/* CORE SECTION DATA
/*
3  0.2794  0.0146  0.1323  ISP84160
4  0.2794  0.0146  0.2307  ISP84170
5  0.2794  0.0146  0.2553  ISP84180
6  0.2794  0.0146  0.2086  ISP84190
7  0.5588  0.0146  0.1731  ISP84200
/*
/* SLAB GEOMETRY DATA
/*
***** GEOMETRY INDEX 1 *****
2  1  0  1  3  12.446E-4  1.0  5.1054E-3 / INCONEL600 ISP84280
***** GEOMETRY INDEX 2 *****
2  4  0  2  2  8.890E-4  0.0  0.0 / B.N.      ISP84290
0  3  5  21.830E-4  1.0 / CONSTANTAN ISP84300
0  2  3  12.960E-4  0.0 / B.N.      ISP84310
0  4  2  9.910E-4  0.0 / ST        ISP84320
/*
/* MATERIAL THERMAL PROPERTY DATA
/*
/* THERMAL CONDUCTIVITY OF INCONEL-600
/*
5
37.8  3.5133E-3  148.9  3.9597E-3  315.6  4.6087E-3  ISP84330
593.3  5.6420E-3  1000.0  7.1553E-3  ISP84340
/*
/* HEAT CAPACITY OF INCONEL-600
/*
5
37.8  916.024  204.4  979.463  315.6  1021.595  ISP84350
426.7  1063.888  1000.0  1282.129  ISP84360
/*
/* GAP CONDUCTANCE DATA
/*
2
0.0  0.0  1000.0  0.0  ISP84370
/*
/* THERMAL CONDUCTIVITY OF BORON-NITRIDE
/*
22
50.0  0.5995E-2  100.0  0.5966E-2  150.0  0.5936E-2  ISP84380
200.0  0.5907E-2  250.0  0.5877E-2  300.0  0.5848E-2  ISP84390
350.0  0.5819E-2  400.0  0.5789E-2  450.0  0.5760E-2  ISP84400
500.0  0.5731E-2  550.0  0.5701E-2  600.0  0.5672E-2  ISP84410
650.0  0.5643E-2  700.0  0.5613E-2  750.0  0.5584E-2  ISP84420
800.0  0.5555E-2  850.0  0.5525E-2  900.0  0.5496E-2  ISP84430
950.0  0.5467E-2  1000.0  0.5437E-2  1050.0  0.5408E-2  ISP84440

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	1	2	3	4	5	6	7-R	8
	1100.0	0.5379E-2						ISP84640
/*								ISP84650
/*	HEAT CAPACITY OF BORON-NITRIDE							ISP84660
/*								ISP84670
	22							ISP84680
	50.0	0.4625E3	100.0	0.5279E3	150.0	0.5874E3		ISP84690
	200.0	0.6413E3	250.0	0.6899E3	300.0	0.7335E3		ISP84700
	350.0	0.7726E3	400.0	0.8074E3	450.0	0.8382E3		ISP84710
	500.0	0.8654E3	550.0	0.8895E3	600.0	0.9105E3		ISP84720
	650.0	0.9289E3	700.0	0.9451E3	750.0	0.9593E3		ISP84730
	800.0	0.9718E3	850.0	0.9831E3	900.0	0.9935E3		ISP84740
	950.0	0.1003E4	1000.0	0.1013E4	1050.0	0.1022E4		ISP84750
	1100.0	0.1032E4						ISP84760
/*								ISP84770
/*	GAP CONDUCTANCE							ISP84780
	2							ISP84790
	0.0	0.0	1000.0	0.0				ISP84800
/*								ISP84810
/*	THERMAL CONDUCTIVITY OF CONSTANTAN							ISP84820
/*								ISP84830
	22							ISP84840
	50.0	0.6138E-2	100.0	0.6336E-2	150.0	0.6535E-2		ISP84850
	200.0	0.6733E-2	250.0	0.6931E-2	300.0	0.7129E-2		ISP84860
	350.0	0.7328E-2	400.0	0.7526E-2	450.0	0.7724E-2		ISP84870
	500.0	0.7923E-2	550.0	0.8121E-2	600.0	0.8319E-2		ISP84880
	650.0	0.8517E-2	700.0	0.8716E-2	750.0	0.8914E-2		ISP84890
	800.0	0.9112E-2	850.0	0.9311E-2	900.0	0.9509E-2		ISP84900
	950.0	0.9707E-2	1000.0	0.9905E-2	1050.0	0.1010E-1		ISP84910
	1100.0	0.1030E-1						ISP84920
/*								ISP84930
/*	HEAT CAPACITY OF CONSTANTAN							ISP84940
	22							ISP84950
	50.0	0.8771E3	100.0	0.8945E3	150.0	0.9120E3		ISP84960
	200.0	0.9294E3	250.0	0.9469E3	300.0	0.9643E3		ISP84970
	350.0	0.9818E3	400.0	0.9992E3	450.0	0.1017E4		ISP84980
	500.0	0.1034E4	550.0	0.1052E4	600.0	0.1069E4		ISP84990
	650.0	0.1086E4	700.0	0.1104E4	750.0	0.1121E4		ISP85000
	800.0	0.1139E4	850.0	0.1156E4	900.0	0.1174E4		ISP85010
	950.0	0.1191E4	1000.0	0.1209E4	1050.0	0.1226E4		ISP85020
	1100.0	0.1244E4						ISP85030
/*								ISP85040
/*	GAP CONDUCTANCE DATA							ISP85050
	2							ISP85060
	0.0	0.0	1000.0	0.0				ISP85070
/*								ISP85080
/*	THERMAL CONDUCTIVITY OF STAINLESS STEEL							ISP85090
/*								ISP85100
	22							ISP85110
	50.0	0.3287E-2	100.0	0.3446E-2	150.0	0.3604E-2		ISP85120
	200.0	0.3763E-2	250.0	0.3921E-2	300.0	0.4079E-2		ISP85130
	350.0	0.4238E-2	400.0	0.4396E-2	450.0	0.4555E-2		ISP85140
	500.0	0.4713E-2	550.0	0.4872E-2	600.0	0.5030E-2		ISP85150
	650.0	0.5189E-2	700.0	0.5347E-2	750.0	0.5505E-2		ISP85160
	800.0	0.5664E-2	850.0	0.5822E-2	900.0	0.5981E-2		ISP85170
	950.0	0.6139E-2	1000.0	0.6298E-2	1050.0	0.6456E-2		ISP85180
	1100.0	0.6614E-2						ISP85190
/*								ISP85200
/*	HEAT CAPACITY OF STAINLESS STEEL							ISP85210
/*								ISP85220

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-----*-----1-----*-----2-----*-----3-----*-----4-----*-----5-----*-----6-----*-----7-R-----*-----8
22
50.0 0.9204E3 100.0 0.9350E3 150.0 0.9495E3 ISP85230
200.0 0.9640E3 250.0 0.9783E3 300.0 0.9926E3 ISP85240
350.0 0.1007E4 400.0 0.1021E4 450.0 0.1035E4 ISP85250
500.0 0.1049E4 550.0 0.1062E4 600.0 0.1076E4 ISP85260
650.0 0.1090E4 700.0 0.1103E4 750.0 0.1117E4 ISP85270
800.0 0.1130E4 850.0 0.1143E4 900.0 0.1156E4 ISP85280
950.0 0.1170E4 1000.0 0.1182E4 1050.0 0.1195E4 ISP85290
1100.0 0.1208E4 ISP85300
/* ISP85310
/* GAP CONDUCTANCE DATA ISP85320
/* ISP85330
/* 2 ISP85340
/* 0.0 0.0 1000.0 0.0 ISP85350
/* ISP85360
/* END OF DATA ISP85370
/* ISP85380
/* ISP85390
/* ***** ISP85400
/* INDIVIDUAL PARAMETERS CORRESPONDING TO MEASUREMENT DATA * ISP85410
/* PRESSURE * ISP85420
/* PU-PRIZE ----- AP 10 * ISP85430
/* PB-42 ----- AP 17 * ISP85440
/* PB-23 ----- AP 35 * ISP85450
/* PV-UP+10 ----- AP 26 * ISP85460
/* PU-ACC ----- AP 33 * ISP85470
/* PU-SGSD ----- AP 21 * ISP85480
/* DIFFERENTIAL PRESSURE * ISP85490
/* DPU-10-12 ----- AP 6 - AP 8 * ISP85500
/* DPB-32-36L ----- AP 12- AP 15 * ISP85510
/* DPB-38-40 ----- AP 15- AP 17 * ISP85520
/* DPV-LP-UP ----- AP 24- AP 26 * ISP85530
/* FLOW RATE * ISP85540
/* FTU-COREIN (V) ----- JW 27 * ISP85550
/* FTU-15 (V) ----- JW 10 * ISP85560
/* FTU-PRIZE (V) ----- JW 12 * ISP85570
/* FTU-LPIS (V) ----- JW 38 * ISP85580
/* FTU-HPIS (V) ----- JW 37 * ISP85590
/* FTU-ACC (V) ----- JW 35 * ISP85600
/* FTU-10, GU-10 ----- JW 7 * ISP85610
/* FDB-42, GB-42R ----- JW 29 * ISP85620
/* FDR-23, GB-23R ----- JW 30 * ISP85630
/* FLUID DENSITY * ISP85640
/* GB-42VR ----- AR 17 * ISP85650
/* GB-23VR ----- AR 35 * ISP85660
/* GU-15C ----- AR 9 * ISP85670
/* GU-10 ----- AR 6 * ISP85680
/* GVCOR-150HZ ----- AR 25 * ISP85690
/* GV161/192D ----- AR 24 * ISP85700
/* FLUID TEMPERATURE * ISP85710
/* TFU-PRIZE ----- AT 11 * ISP85720
/* TFB-23 ----- AT 35 * ISP85730
/* TFV-UP+10 ----- AT 26 * ISP85740
/* HT COEFF. AND AVERAGE QUALITY OF AVERAGE CORE REGION * ISP85750
/* HC 28 , AX 28 ----- AT ELEVATION 8" ABOVE BOTTOM * ISP85760
/* HC 29 , AX 29 ----- AT ELEVATION 14" ABOVE BOTTOM * ISP85770
/* HC 30 , AX 30 ----- AT ELEVATION 28" ABOVE BOTTOM * ISP85780
/* HC 31 , AX 31 ----- AT ELEVATION 39" ABOVE BOTTOM * ISP85790
/* INTEGRATED MASS INVENTORY * ISP85800
/* * ISP85810

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