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ANALYSES OF PWR SPENT FUEL COMPOSITION USING SCALE AND SWAT
CODE SYSTEMS TO FIND CORRECTION FACTORS FOR CRITICALITY SAFETY
APPLICATIONS ADOPTING BURNUP CREDIT

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Hee Sung SHIN*, Kenya SUYAMA, Hiroki MOCHIZUKI,
Hiroshi OKUNO and Yasushi NOMURA

日本原子力研究所
Japan Atomic Energy Research Institute

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Analyses of PWR Spent Fuel Composition Using SCALE and SWAT Code Systems
to Find Correction Factors for Criticality Safety Applications Adopting Burnup Credit

Hee Sung SHIN*, Kenya SUYAMA, Hiroki MOCHIZUKI,
Hiroshi OKUNO and Yasushi NOMURA

Department of Fuel Cycle Safety Research
Nuclear Safety Research Center
Tokai Research Establishment
Japan Atomic Energy Research Institute
Tokai-mura, Naka-gun, Ibaraki-ken

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The isotopic composition calculations were performed for 26 spent fuel samples from the Obrigheim PWR reactor and 55 spent fuel samples from 7 PWR reactors using the SAS2H module of the SCALE4.4 code system with 27, 44 and 238 group cross-section libraries and the SWAT code system with the 107 group cross-section library. For the analyses of samples from the Obrigheim PWR reactor, geometrical models were constructed for each of SCALE4.4/SAS2H and SWAT. For the analyses of samples from 7 PWR reactors, the geometrical model already adopted in the SCALE/SAS2H was directly converted to the model of SWAT.

The four kinds of calculation results were compared with the measured data. For convenience, the ratio of the measured to calculated values was used as a parameter. When the ratio is less than unity, the calculation overestimates the measurement, and the ratio becomes closer to unity, they have a better agreement. For many important nuclides for burnup credit criticality safety evaluation, the four methods applied in this study showed good coincidence with measurements in general. More precise observations showed, however: (1) Less unity ratios were found for Pu-239 and -241 for selected 16 samples out of the 26 samples from the Obrigheim reactor (10 samples were deselected because their burnups were measured with Cs-137 non-destructive method, less reliable than Nd-148 method the rest 16 samples were measured with); (2) Larger than unity ratios were found for Am-241 and Cm-242 for both the 16 and 55 samples; (3) Larger than unity ratios were found for Sm-149 for the 55 samples; (4) SWAT was generally accompanied by larger ratios than those of SAS2H with some exceptions.

Based on the measured-to-calculated ratios for 71 samples of a combined set in which 16 selected samples and 55 samples were included, the correction factors that should be multiplied to the calculated isotopic compositions were generated for a conservative estimate of the neutron multiplication factor of a system containing PWR spent fuel, taking burnup credit into account.

Keywords: Correction Factor, Burnup Credit, Isotopic Composition, PWR Spent Fuel, Tolerance Limit Factor, Normality Test

* On leave from the Korea Atomic Energy Research Institute (KAERI).

SCALE及びSWATコードシステムを用いたPWR使用済燃料核種組成の解析
に基づく燃焼度クレジットを採用した臨界安全への応用のための
補正因子の決定

日本原子力研究所東海研究所安全性試験研究センター燃料サイクル安全工学部
慎 禧晟*・須山 賢也・望月 弘樹・奥野 浩・野村 靖

(2000年10月31日受理)

同位体組成の計算をオブリハイムPWR型原子炉の26個の使用済燃料サンプル及び7つのPWR型原子炉の55個の使用済燃料サンプルを対象とし、SCALE4.4コードシステムのSAS2Hモジュールで27、44及び238群の断面積ライブラリ、及びSWATコードシステムで107群断面積ライブラリを用いて実施した。オブリハイム原子炉からのサンプルの解析では、幾何形状モデルはSCALE4.4/SAS2HとSWATそれぞれに対して作成した。7つのPWR型原子炉からのサンプルの解析では、SCALE4.4/SAS2Hに既に適用された幾何形状モデルをSWATのモデルに直接変換した。

これら4種類の計算結果を測定データと比較した。便宜上、測定値対計算値の比をパラメタとした。この比が1より小さいとき、計算値は測定値よりも大きく、1に近いと測定値との一致がよい。燃焼度クレジットを採用した臨界安全評価のための多くの重要な核種について、この研究で適用した4つの計算手法は一般的に測定値とよい一致を示した。しかし、更に細かく見ると、以下の点に気付く:(1)オブリハイムPWR型原子炉の選ばれた16サンプル(26サンプルのうち16サンプルはNd-148法で測定されたが、10サンプルはNd-148法より信頼性の低いCs-137非破壊法で測定された)では、Pu-239及び-241で1より小さな比となった;(2)Am-241とCm-242については、16サンプル及び55サンプルともに、1より大きな比となった;(3)Sm-149は55サンプルで1より大きな比となった;(4)SWATは概してSAS2Hよりも大きな比の値を示した。

燃焼度クレジットを取り入れた、最近のPWR燃料などを含めた中性子増倍率の保守的な評価のために、核種組成の計算値に掛ける補正因子を、71サンプル(選択した16サンプルと55サンプルとを併せたもの)の測定値対計算値の比に基づき生成した。

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1. Introduction

It is known that an application of burnup credit in the spent fuel management is economically beneficial if the nuclear criticality safety is ensured in the allowable limit. Since the burnup credit safety analysis is essentially based on nuclide inventories in a system under consideration, the prediction of the conservative isotopic composition is very important for burnup credit criticality safety analysis. One of the methods of the conservative isotopic composition determination is the application of the correction factors which are obtained by statistical analysis on the basis of the calculated and measured isotopic composition of PWR spent fuel. The conservative composition can be easily obtained by multiplying the calculated isotopic composition by them.

Since ORIGEN2 code[1,2] is world-widely used for the inventory calculation, the comparison of ORIGEN2 calculation results with the experimental data has been studied in a lot of papers. Although some papers have shown the comparison results of ORIGEN2-calculated composition with the experiments, the correction factors of isotopes contained in PWR spent fuel for conservative criticality calculation was not studied in the papers[3-11]. The experimental isotopic compositions of Mihama-3 and Genkai-1 spent fuel with assembly-averaged burnup from 8,400 to 38,600 MWD/MTU were presented in the references[3,12] and compared with SRAC-FPGS[3] and ORIGEN2 calculation results, respectively. The correction factors for ORIGEN2 composition calculation were determined and presented in reference[13] on the basis of experimental data of PWR spent fuel isotopic compositions [2,14].

SWAT(Step-Wise Burnup Analysis Code System)[15,16] which has been developed by Tohoku University and JAERI can generate effective one-group cross-section sets for ORIGEN2.1 calculation. In comparison of SWAT and ORIGEN2.1 results, SWAT has seemed to be more precisely predict nuclide composition of the latest PWR assemblies than ORIGEN2.1[15,16].

Hermann et al. presented the validation results of SCALE4.2 (modular code system for performing standardized computer analysis for licensing evaluation version 4.2) SAS2H(shielding analysis sequence No 2)[17] module and the 27 group cross section

library using 19 spent fuel experimental concentrations in 1995 [14]. DeHart et al. updated the results using 38 spent fuel experimental concentrations and presented the correction factors of 39 nuclides in 1996 [18]. Isotopic validation for actinide-only burnup credit using 55 spent fuel experimental data were presented in a U.S. DOE report in 1997 [19].

Isotopic validation of the SCALE4.4 SAS2H module with 27, 44 and 238 group cross-section libraries which are available was carried out for fifty-five chemical assay data[20]. A statistical treatment was performed to determine biases and corresponding uncertainties based on the benchmark set of chemical assay data, which gave rise to conservative correction factors for each isotope. Isotopic correction factors were then obtained on the basis of the measured and calculated concentrations of 38 isotopes for both selected actinides and fission products(FPs) [20].

In this work, using SAS2H with 27, 44 and 238 group cross-section libraries and SWAT with 107 group, the isotopic compositions are calculated and compared on the basis of 26 Obrigheim samples[21,22] and 55 experimental samples of PWR spent fuel of seven plants: Yankee Rowe, Mihama-3, Trino Vercellese, Turkey Point, Calvert Cliff, H. B. Robinson, and Obrigheim. Finally, the correction factors are generated on the basis of the measured-to-calculated ratios.

2. Experimental data

Fifty-five PWR spent fuel experimental samples of seven reactors and 26 Obrigheim spent fuel samples have been published to be available for the determination of isotopic correction factor.

2.1. 55 Experimental Samples

Fifty-five chemical assay data were obtained from fuel assemblies discharged at seven different nuclear reactors: Yankee Rowe, Mihama-3, Trino Vercellese, Turkey Point, Calvert Cliffs, H.B.Robinson, and Obrigheim as shown in Table. 2.1. Validation analysis results of the chemical assay data for all but Yankee Rowe and Mihama-3 were presented in the ORNL report [18]. All the chemical assays above-mentioned also were analyzed and described in the U.S. DOE report[19]. Operating parameters for each sample were presented in Table 2.2. Initial enrichments and burnups, which are important parameter for concentration calculations, range from 2.453 to 3.897 wt% and from 6.92 to 46.46 GWd/tU, respectively.

2.2. 26 Obrigheim Spent Fuel Samples[20,21]

The Obrigheim Nuclear Power Plant, operated by KWO, was equipped with a pressurized water reactor rated at 350 MW(e). Six fuel rods were chosen for examination. The fuel assemblies BE 124 (average burnup of 29,000 MWd/tU) and BE 210 (average burnup of 30,000 MWd/tU) selected for post-irradiation analyses were composed of 180 rods with initial U-235 enrichment of 3.00 wt% and 2.83 wt%, respectively. In Table 2.3 the main characteristics of the fuel assembly were presented. Although 27 experimental samples of Obrigheim spent fuel composition were included in the SFCOMPO database[21], only 26 samples were used for this work because one sample didn't have absolute isotopic composition data but ratio data.

2.3. Reliability of Experimental Data

Since the correction factors are determined on the basis of the experimental data, the reliability of the experimental data is very important for the assurance that the generated correction factors are applicable to burnup credit criticality calculation. Some of 55

experimental samples mentioned above were measured during 1960 – 1980. Considering the lower level of measuring technique in that time than now, the experimental data might be unreliable.

It is obvious that total depletion amount of actinide nuclides, the difference between the charged and discharged actinide amounts, are linearly proportioned to burnup. In Fig. 2.1 seven depletion amounts obtained from seven different institutes' experimental data are compared on the basis of the calculation values which are obtained by using SAS2H with 44 group cross-section library. It might be considered as a kind of inter-comparison. Fig. 2.1 shows that most experimental data appears closely to the line of the relative error of zero and Mihama-3 and Yankee Rowe experiments are more apart from the zero line than others. But the relative errors are not too much large to exclude two institutes' experimental data. Although Trino Vercellese's experimental data had been expected to have a large error because those are measured in 1964 and the oldest of the published experiments, all data are around zero line within $\pm 3\%$ as shown in Fig.2.1.

The measurements of 26 Obrigheim samples were carried out at both Ispra and Karlsruhe Establishments. As shown in Table 2.4, Samples E3-P4, G7-P1, G7-P3 and G14-P3(1) were measured both institutes simultaneously. Since two measured burnup values of G7-P1 are much different, one of two institute's measurements must be not correct. As reported in reference[12], Karlsruhe's result might be not reliable. In the case of E3-P2, the burnup values measured with Nd-148 is also much different from that of Cs-137 non-destructive method. Therefore, it is expected that a big difference between experimental data and calculated values will appear in the cases. In this work, the depletion calculations were carried out on the basis of the burnup values of Nd-148 method which are known as the best burnup estimation method.

Recently, isotopic compositions of PWR and BWR spent fuels were measured in the PIEF(Post Irradiation Examination Facility) of JAERI. The experimental data are expected to be useful for the verification of the experimental data mentioned above.

Table 2.1. Nuclear Power Plants & Experimental Conditions

Name (Location)	Reactor						Plant						Measurement		
	Core Size (cm)	Power (MWe)		Assy. No.	Pitch (cm)	Rod No.	Lattice Array	Pitch (cm)	Pellet Density (g/cm ³)	Cladding I.D. (cm)	Cladding O.D. (cm)	Active Fuel Length (cm)	Irradiation History	Burnup	Inventory
Yankee Rowe (U.S.A.)	190.75		WEC ^{a)}	76	19.46	305	18x 18	1.072	10.18	0.747	0.757	0.864	230.05	HE ^{b)} Method Nd-148	Mass Spectrometry, Alpha Spectrographic Radiochemical Analyses
Mihama-3 (JAPAN)	304	826	JAERI ^{b)}	157	21.50	204	15x 15	1.430	9.96	0.929	0.948	1.072	365.76	1975.2	Mass Spectrometry, α,γ Spectrometry
Trino Vercellese (ITALY)	249	260	ISPR ^{c)} Karlsruhe	120 /112	20.0	221	15x 15	1.303	10.353	0.890	0.902	0.979	264.1	1964.10	Nd-148 Cs-137
Calvert Cliffs (U.S.A.)	2560th		PNL ^{c)}	217	20.78	160 ~176	14x 14	1.4732	10.036 ~10.045	0.9563 ~0.9639	0.948	1.072	347.22	1977.3.22- 1982.4.17	Alpha, Beta, Gamma Scan
Turkey Point (U.S.A.)			HEDL ^{d)} & BCL ^{e)}	21.50	204	15x 15	1.430	10.235	0.9296	0.985	1.118	365.8	1972.1.12- 1975.11.25	Nd-148 ASTM E-321	
H. B. Robinson (U.S.A.)	304	700	HEDL	157	21.50	204	15x 15	1.430	9.944	0.9294	0.948	10.072	365.8	1971.3- 1974.5.6	ASTM E-321
Obrigheim (GERMANY)	250	350	ISPR ^{f)} Karlsruhe	121	20.12	180	14x 14	1.430	9.742	0.925	0.930	1.074	295.6	1970.9.30- 1974.8.16	Mass Spectrometry

^{a)} WEC : Westinghouse Electric Corporation.^{b)} JAERI: Japan Atomic Energy Research Institute^{c)} PNL : Pacific Northwest Laboratory.^{d)} HEDL : Hanford Engineering Development Laboratory.^{e)} BCL : Battelle Columbus Laboratory.^{f)} HE : Heavy Element(Pu/U)

Table 2.2. Operating Parameters for 55 Spent PWR Fuel Samples

Reactor	Assembly ID	Calculation Sample ID	Enrichment (U-235 wt%)	Burnup (GWd/tU)	Cooling Time (d)	Axial Location (cm)	Temperature(°C)			Water Density (g/cm³)
							Fuel	Cladding	Coolant	
Yankee rowe	E6-C-f6	ya1	3.400	15.95	281.5	220.22	771.3	559.1	548.7	0.770
	E6-C-f6	ya2	3.400	30.39	717.0	138.94	889.5	560.2	540.8	0.783
	E6-C-f6	ya3	3.400	31.33	281.5	57.66	876.6	550.8	531.7	0.797
	E6-C-f6	ya4	3.400	20.19	281.5	17.02	787.1	540.6	528.0	0.803
	E6-SE-c2	ya5	3.400	32.03	281.5	138.94	889.5	560.2	540.8	0.783
	E6-SE-c2	ya6	3.400	31.41	281.5	57.66	876.6	550.8	531.7	0.797
	E6-SE-e4	ya7	3.400	35.97	281.5	138.94	889.5	560.2	540.8	0.783
	E6-SE-e4	ya8	3.400	35.26	281.5	57.66	876.6	550.8	531.7	0.797
Mihamo-3	86b02	mi1	3.208	8.30	1825		923.0	600.4	560.4	0.752
	86b03	mi2	3.208	6.92	1825		863.0	633.6	593.6	0.679
	86g05	mi3	3.208	15.36	1825		823.0	611.7	71.7	0.730
	86g03	mi4	3.203	21.29	1825		933.0	625.4	585.4	0.700
	86g07	mi5	3.203	14.22	1825		863.0	600.3	560.3	0.755
	86c03	mi6	3.203	29.50	1825		863.0	600.3	560.3	0.752
	87c04	mi7	3.210	32.20	1825		891.0	607.0	567.0	0.739
	87c07	mi8	3.210	33.71	1825		905.0	600.8	560.8	0.751
	87c08	mi9	3.210	34.32	1825		913.0	625.9	585.9	0.698
	509-104-M11-7	tr1	3.897	12.04	10	79.2	1001.0	570.0	543.0	0.780
Trino Vercellese	509-032-E11-4	tr2	3.130	15.38	10	158.5	1015.0	570.0	557.0	0.755
	509-032-E11-7	tr3	3.130	15.90	10	79.2	1001.0	570.0	543.0	0.780
	509-032-E11-9	tr4	3.130	11.53	10	26.4	927.0	570.0	537.0	0.789
	509-069-E11-1	tr5	3.130	12.86	10	237.7	915.0	570.0	563.0	0.737
	509-069-E11-2	tr6	3.130	20.60	10	211.3	968.0	570.0	561.0	0.741
	509-069-E11-4	tr7	3.130	23.72	10	158.5	1015.0	570.0	553.0	0.755
	509-069-E11-7	tr8	3.130	24.30	10	79.2	1001.0	570.0	540.0	0.780
	509-069-E5-4	tr9	3.130	23.87	10	158.5	1015.0	570.0	553.0	0.755
	509-069-E5-7	tr10	3.130	24.55	10	79.2	1001.0	570.0	540.0	0.780
	509-069-L11-4	tr11	3.130	23.93	10	158.5	1015.0	570.0	553.0	0.755
	509-069-L11-7	tr12	3.130	24.36	10	79.2	1001.0	570.0	540.0	0.780
	509-069-L5-4	tr13	3.130	24.33	10	158.5	1015.0	570.0	553.0	0.755
	509-069-L5-7	tr14	3.130	24.31	10	79.2	1001.0	570.0	540.0	0.780
Calvert Cliffs Units 1	D047-MKP109	ca1	3.038	27.35	1870	13.2	922.0	595.0	570.0	0.731
	D047-MKP109	ca2	3.038	37.12	1870	27.7	922.0	595.0	570.0	0.731
	D047-MKP109	ca3	3.038	44.34	1870	165.22	922.0	595.0	570.0	0.731
	D101-MLA098	ca4	2.720	18.68	2374	9.10	922.0	595.0	570.0	0.731
	D101-MLA098	ca5	2.720	26.62	2374	24.50	922.0	595.0	570.0	0.731
	D101-MLA098	ca6	2.720	33.17	2374	161.90	790.0	620.0	557.0	0.757
	BT03-NBD107	ca7	2.453	31.40	2447	11.28	841.0	620.0	558.0	0.757
	BT03-NBD107	ca8	2.453	37.27	2447	19.92	873.0	620.0	570.0	0.733
Turkey point 3	BT03-NBD107	ca9	2.453	46.46	2447	161.21	816.0	620.0	557.0	0.758
	D01-G9	tk1	2.556	30.72	927		880.0	620.0	558.0	0.757
	D01-G10	tk2	2.556	30.51	927		910.0	620.0	570.0	0.734
	D01-H9	tk3	2.556	31.56	927		790.0	620.0	557.0	0.758
	D04-G9	tk4	2.556	31.26	927		841.0	620.0	557.0	0.758
H. B. Rorinson	D04-G10	tk5	2.556	31.31	927		873.0	620.0	570.0	0.758
	N-9B-S	ro1	2.560	16.02	3936		743.0	595.0	559.0	0.687
	N-9B-N	ro2	2.560	23.81	3936		830.0	595.0	559.0	0.687
	N-9C-J	ro3	2.560	28.47	3631		883.0	595.0	576.0	0.656
Obrigheim	N-9C-D	ro4	2.560	31.66	3631		923.0	595.0	579.0	0.650
	170-94	or1	3.130	25.93	10		846.0	605.0	572.0	0.728
	172-92	or2	3.130	26.54	10		841.0	605.0	572.0	0.728
	176-91	or3	3.130	27.99	10		849.0	605.0	572.0	0.728
	168-86	0b4	3.130	28.40	10		859.0	605.0	572.0	0.728
	171-89	0b5	3.130	29.04	10		867.0	605.0	572.0	0.728
	176-90	or6	3.130	29.52	10		771.3	560.2	540.8	0.783

Table 2.3. Design Specifications for Obrigheim Spent Fuel

Design Specification	Value
Fuel Rod	
-Pellet Density	10.422 g/cm ³
-Pellet Diameter	0.9040 cm
-Cladding ID	0.9318 cm
-Cladding OD	1.0760 cm
-Pitch	1.4300 cm
Assembly	
-Rod No	180
-Array	14 x 14

Table 2.4. Operating Parameters for 26 Obrigheim Samples

Calculation Sample ID	Sample ID	Measurement Institute	Enrichment (U-235wt%)	Burnup (GWd/tU)	Axial Location (cm)	Temperature(°C)		
						Fuel	Cladding	Coolant
or1	D1-P1	Karlsruhe	3.00	21.17	15.0	900.0	600.0	556.3
or2	D1-P3	Ispra	3.00	33.75	143.5	900.0	600.0	570.5
or3	E3-P1	Ispra	3.00	20.18	15.0	900.0	600.0	556.3
or4	E3-P2	Karlsruhe	3.00	35.10	31.5	900.0	600.0	557.0
or5	E3-P3	Ispra	3.00	36.26	143.5	900.0	600.0	570.5
or6	E3-P4	Ispra	3.00	30.89	231.5	900.0	600.0	582.8
or7	E3-P4	Karlsruhe	3.00	30.94	231.5	900.0	600.0	582.8
or8	E3-P5	Ispra	3.00	22.86	258.5	900.0	600.0	585.0
or9	G7-P1	Ispra	3.00	17.13	15.0	900.0	600.0	556.3
or10	G7-P1	Karlsruhe	3.00	22.70	15.0	900.0	600.0	556.3
or11	G7-P2	Ispra	3.00	25.83	31.5	900.0	600.0	557.0
or12	G7-P3	Ispra	3.00	31.50	143.5	900.0	600.0	570.5
or13	G7-P3	Karlsruhe	3.00	31.14	143.5	900.0	600.0	570.5
or14	G7-P4	Ispra	3.00	27.71	231.5	900.0	600.0	582.8
or15	G7-P5	Karlsruhe	3.00	25.81	258.5	900.0	600.0	585.0
or16	M14-P1	Karlsruhe	3.00	15.60	15.0	900.0	600.0	556.3
or17	M14-P3	Ispra	3.00	29.36	143.5	900.0	600.0	570.5
or18	M14-P4	Karlsruhe	3.00	24.90	231.5	900.0	600.0	582.8
or19	G14-P3(1)	Ispra	2.83	38.10	132.8	900.0	600.0	568.8
or20	G14-P3(1)	Karlsruhe	2.83	36.88	132.8	900.0	600.0	568.8
or21	G14-P4(1)	Ipara	2.83	35.64	220.6	900.0	600.0	581.6
or22	G14-P5(1)	Ispra	2.83	30.16	242.6	900.0	600.0	583.8
or23	G14-P5(2)	Ispra	2.83	24.22	254.7	900.0	600.0	584.8
or24	K14-P1	Ispra	2.83	25.45	15.0	900.0	600.0	556.3
or25	K14-P3(1)	Ispra	2.83	36.67	132.8	900.0	600.0	568.8
or26	K14-P4(1)	Karlsruhe	2.83	32.90	220.6	900.0	600.0	581.6

* Cooling Time: 0.0 day

*Cooling Water Density:

-SAS2H: 0.8238 g/cm³

-SWAT: water density, corresponding to the coolant temperature, is calculated in SWAT.

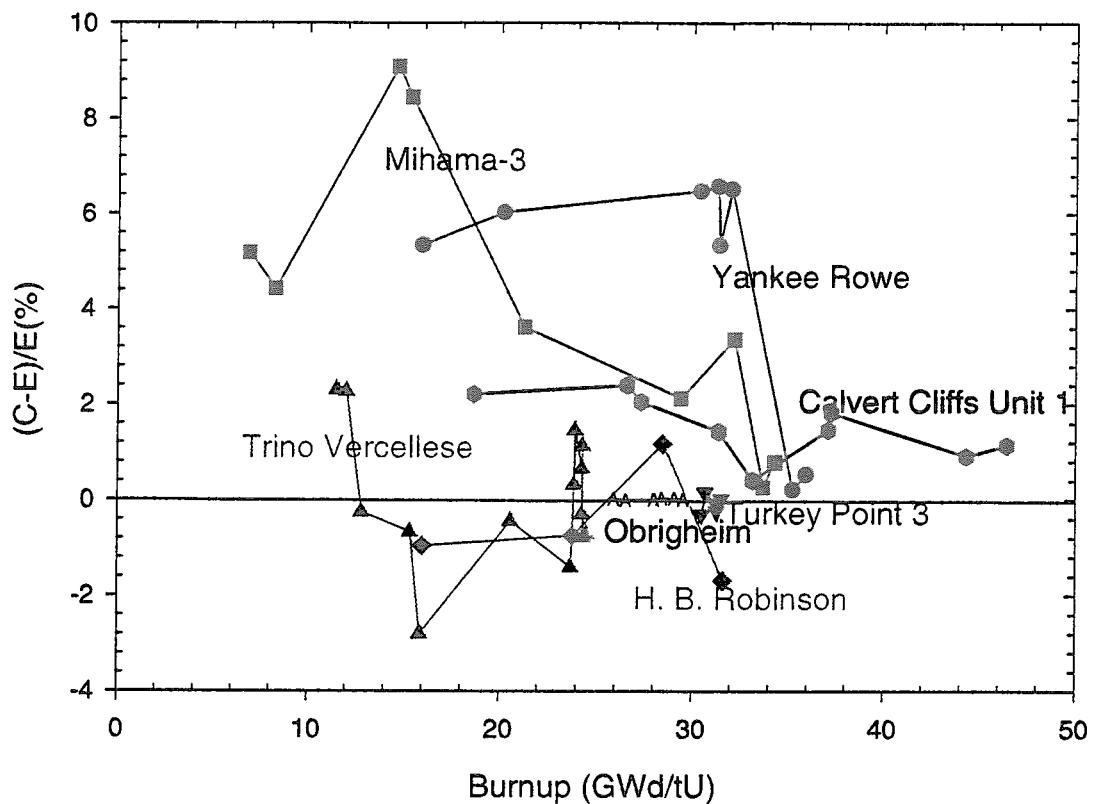


Fig. 2.1. Relative Errors of Total Depleted Actinide Amounts against Burnup except Effects of U-238.

3. Characteristics of SAS2H Module and SWAT Code System

3.1. SAS2H

SCALE(Modular Code System for Performing Standardized Computer Analysis for Licensing Evaluation) is a well-established code system that has been widely used in away-from-reactor (AFR) applications for spent fuel characterization via the SAS2H(Shielding Analysis Sequence No.2) analysis sequence. SAS2H is a multicode sequence that determines the isotopic composition of spent fuel using the ORIGEN-S code[22] for depletion and decay calculations and a 1-D neutronics model of an LWR fuel assembly to prepare burnup-dependent cross sections for ORIGEN-S.

The process used by SAS2H in calculation of spent fuel isotopes is illustrated schematically in Fig. 3.1. The calculation starts with input-specified data describing a fuel assembly as it is initially loaded into a reactor. The initial composition, average temperatures, geometry, and time-dependent specific power of the fuel assembly are required. The SAS2H sequence performs 1-D neutron transport analysis of the reactor fuel assembly using XSDRNPM and a two-part procedure with two separate unit-cell-lattice models.

As shown in Fig. 3.1, the first model is a unit fuel-pin cell from which cell-weighted cross sections are obtained. The second model represents a larger unit cell (e.g., an assembly) within an infinite lattice. The larger unit cell zones can be structured for different assembly designs to account for assembly-specific attributes (i.e., water holes, burnable poison rods, etc.). Problem-dependent resonance self-shielding of cross sections is performed prior to each XSDRNPM calculation using the BONAMI and NITAWL-II codes. The neutron flux spectrum obtained from the second (assembly) unit-cell model is used to determine the appropriate nuclide cross sections for the burnup-dependent fuel composition. The cross sections derived from XSDRNPM calculations at each time step are used in an ORIGEN-S point-depletion computation that produces the burnup-dependent fuel compositions to be used in the next spectrum calculation.

This sequence is repeated in user-specified burnup steps for a complete assembly operating history. The buildup and decay of nuclides in the fuel assembly is then computed by ORIGEN-S in the final pass based on the assembly's cooling time (i.e., the period of time after final exposure time). The neutron flux used to produce the ORIGEN-S cross sections is based on a radial average of an infinitely long uniform assembly with characteristics per input specifications. These specifications (e.g., burnup, specific power, moderator temperature, etc.) can be representative of any axial location along the fuel assembly or an axial average of the fuel assembly.

3.2. SWAT

SWAT is an integrated burnup code system, which are developed for analysis of post irradiation examination, transmutation of radioactive waste, and burnup credit problem. Fig. 3.2 shows the flow of analysis by SWAT. In SWAT calculation, the total burnup history is divided into burnup steps. SWAT calculates the neutron spectrum and effective cross sections with the SRAC code system[24] for each burnup step, prepares a one grouped cross section library for ORIGEN2, and performs burnup calculation with ORIGEN2 using that new library. SWAT consists of four codes: SRAC, ORIGEN2, TABMAK, and LIBMAK.

SRAC is a neutronics code widely used in Japanese research institutes. ORIGEN2 is one of the most famous point burnup codes. LIBMAK and TABMAK prepares libraries for ORIGEN2 using a calculated result of SRAC. TABMAK prepares input data for SRAC and ORIGEN2 from the result of ORIGEN2 for the next burnup step. Moreover, SWAT contains cross section library based on JENDL-3.2 [25], and decay and fission yield libraries based on JNDC FP library second version[26]. This means that we can carry out burnup calculation of more than thousands of isotopes by ORIGEN2 using the latest cross section libraries prepared by SRAC considering changes in the neutron spectrum and effective cross sections during the burnup.

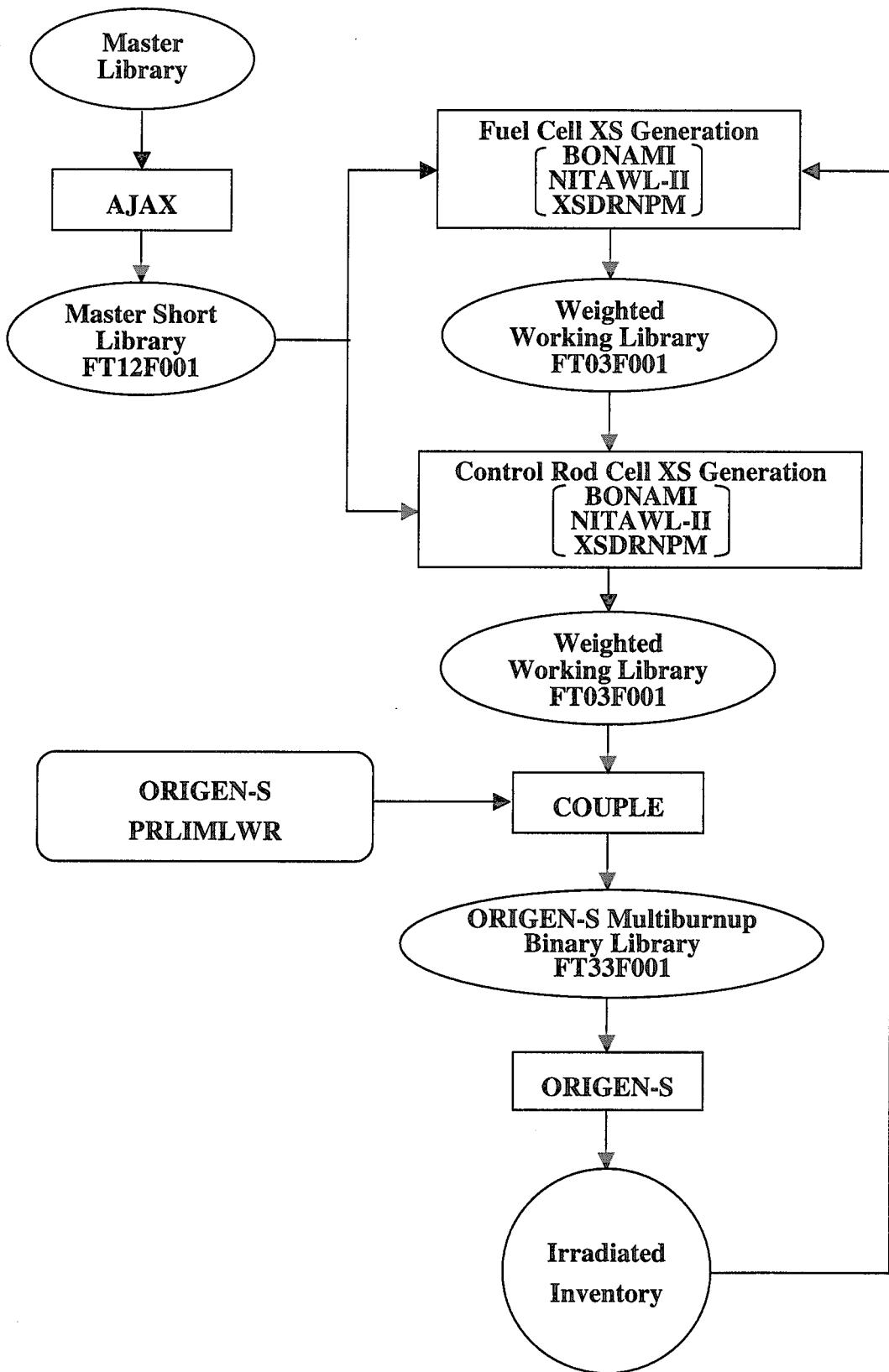


Fig. 3.1. Computational Flowchart of SAS2H Procedure.

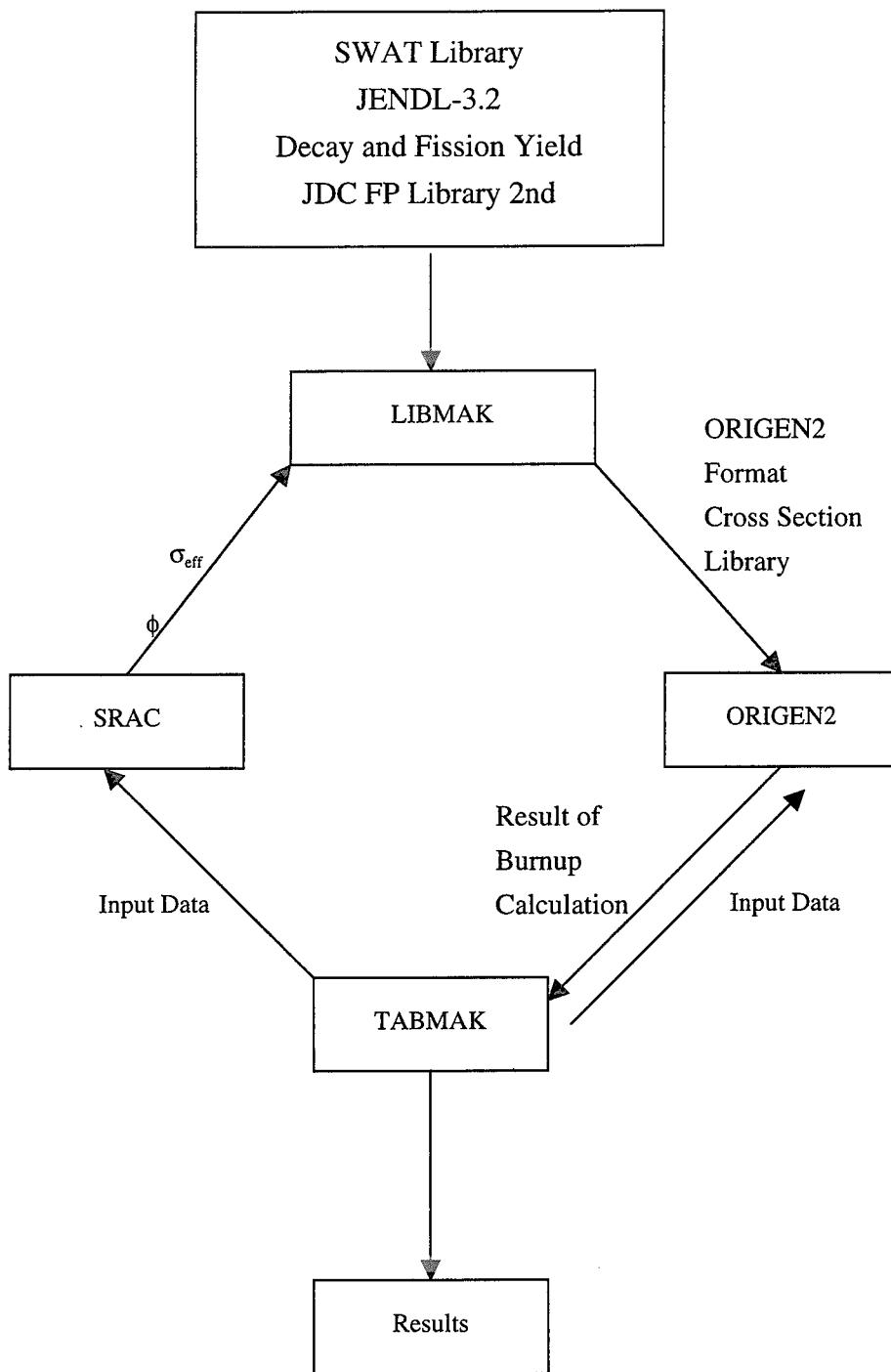


Fig. 3.2. Flow of Calculation in SWAT

4. Methods of Correction Factor Determination

The correction factors are determined on the basis of ratios of the calculated and measured data. Tolerance limit method and linear regression method are taken into account in this work.

4.1. Tolerance Limit Method[27-29]

Differences between calculated and measured isotopic compositions for any given fuel sample can be assumed to result from both the random fashion relative to modeled parameters and the random error associated with experimental measurements.

Given the measured isotopic composition and the corresponding calculated composition for an isotope, the ratio of the measured composition to the calculated isotopic composition for the isotope may be defined as

$$x_{ij} = \left[\frac{E_{ij}}{C_{ij}} \right] \quad (1)$$

where E_{ij} and C_{ij} are experimental value and calculated value for the nuclide i and sample j of the different initial enrichment, burnup, or/and cooling, respectively.

It is necessary to estimate the population mean and variance in terms of the mean and variance of a subset of samples selected to represent the entire population. The mean and the sample variance of the sample set for the nuclide i are given as \bar{x}_i and s_i^2 , respectively, where for a sample set comprised of N_i samples,

$$\bar{x}_i = \sum_{j=1}^{N_i} \left[\frac{x_{ij}}{N_i} \right] \quad (2)$$

$$s_i^2 = \sum_{j=1}^{N_i} \left[\frac{(x_{ij} - \bar{x}_i)^2}{N_i - 1} \right] \quad (3)$$

For a set of normally distributed data points, one may use a tolerance interval approach to assign a tolerance factor $k_{N_i}^{\alpha,\gamma}$ value for N_i . Under this approach, for a given α and γ , there is a probability γ that a future value of $\frac{E'_i}{C'_i}$ will lie within the range $\bar{x} \pm k_{N_i}^{\alpha,\gamma} s_i$,

with an α confidence.

$$\bar{x}_i - k_{N_i}^{\alpha,\gamma} s_i \leq \left[\frac{E'_i}{C'_i} \right] \leq \bar{x}_i + k_{N_i}^{\alpha,\gamma} s_i \quad (4)$$

where C'_i is a calculation value and E'_i is the corresponding measured data, true value. References [27,28] provides tabulated values of $k_{N_i}^{\alpha,\gamma}$ for common values of α and γ and for a range of values of N_i . By multiplying C'_i to eq.(4), the upper bound and lower bound of the true value are expressed by the following.

$$C'_i \cdot (\bar{x}_i - k_{N_i}^{\alpha,\gamma} s_i) \leq E'_i \leq C'_i \cdot (\bar{x}_i + k_{N_i}^{\alpha,\gamma} s_i) \quad (5)$$

In a spent fuel criticality calculation, a conservative approach in the prediction of the neutron multiplication factor, k_{eff} , is to assume the maximum concentration of fissile isotopes combined with the minimum concentration of non-fissile isotopes, to set an uppermost expected limit on k_{eff} . Thus for a set of isotopes present in a criticality calculation, one can determine the limiting isotopic composition by using a correction factor appropriate for each isotope. These correction factor may be written for each isotope i as

$$f_i(\text{fissile}) = \bar{x}_i + k_{N_i}^{\alpha,\gamma} s_i, \text{ or} \quad (6)$$

$$f_i(\text{non-fissile}) = \bar{x}_i - k_{N_i}^{\alpha,\gamma} s_i \quad (7)$$

The correction factors are applied conservatively to ensure that criticality safety evaluations employing the burnup credit method result in an overestimated value of the neutron multiplication factor for the system being evaluated.

As the number of experimental measurements increases, the terms s_i and $k_{N_i}^{\alpha,\gamma}$ will generally decrease. Isotopic correction factors based on a limited number of experimental measurements are, therefore, excessively conservative, though the conservatism is statistically justified.

4.2. Linear Regression Method[19,27]

Having established the trends associated with the isotopic data, the correction factor for each isotope can now be determined. The correction factor for each isotope is determined to assure that the isotopic concentration is conservative. This implies adding an appropriate uncertainty to the fissile isotopes and subtracting the uncertainty in the absorber isotopes. The appropriate uncertainty is found using the prediction interval technique. This technique establishes an interval around the mean prediction in which there is 95 % confidence that the next observation will be within the interval. For this application only one side of the interval is of interest. Therefore, the uncertainty is established in a way that there is a 95% confidence that the next observation being above (absorbers) or below (fissile isotopes) the corrected isotopic concentration.

The generic correction factor formula for isotopes which exhibit trends with respect to one or more parameters such as burnup, initial enrichment, specific power and a multiplication value of the nuclear parameters is also determined based on a prediction interval. Therefore, the 95%-confidence correction factor is:

$$f_{buc} = 1.0 + \sum_{j=1}^m b_j * H_j - t_{95,n-m} \sqrt{\left(1 + \sum_{j=1}^m \frac{H_j^2}{\sum_{i=1}^n h_{ji}^2}\right) \frac{SS_R}{n-m}} \quad (8)$$

Where

$$SS_r = \sum_{i=1}^n (x_i - \sum_{j=1}^m b_j * h_{ji})^2$$

m = number of parameters against which the specific isotope exhibited trends

b_j = the linear slope for the trending parameter j

H_j = the value of trending parameter variable j

h_{ij} = the value for trending parameter j for the i th sample (The h_{ji} values are predetermined by the samples set.)

n = number of data points

4.3. Statistical Tests

Two methods mentioned above can be used to determine the correction factor when the samples data pass the statistical tests. Although only normality test is required for application of tolerance limit method, in the case of linear regression method, additionally constant variance and power of $s=0.05$ test in the case of 95 % confidence level are required.

On the basis of the calculation value of SAS2H with 44 group cross-section library for 55 experimental samples, statistical tests have been preliminarily carried out. A few nuclides passed all three tests, which seemed to be resulted from the lack of experimental data. In this work, therefore, only tolerance limit method is applied to the determination of correction factors under the assumption of an approximate normal distribution.

5. Isotopic Composition Calculation for 26 Obrigheim Spent Fuel Samples

Using SAS2H and SWAT, isotopic compositions were calculated for 26 Obrigheim spent fuel samples.

5.1. Input Preparation

SWAT input was prepared using a fortran program which can read SFCOMPO data file. The basic nuclear parameters, cited from SFCOMPO database, such as fuel pellet and cladding radii, pitch, inlet and outlet temperatures, etc. were inputted in the program. The temperature at the axial location of the sample was also calculated in the program under the assumption of sine-curve power distribution. The depletion time step number per cycle was chosen to be 12 for the ORIGEN2 calculation. For the SRAC calculation, the cross section updating number per cycle was chosen to be 12. Two numbers were fixed for all SWAT calculations of 26 samples. The fuel design specifications and nuclear parameters which were used in the SWAT input were presented in Table 2.3.

A fortran program was made to generate SAS2H input on the basis of SWAT input and additional specification data such as assembly pitch, guide tube inner and outer diameters.

5.2. Comparison of Calculation Results with Experimental Data

5.2.1. Comparison of U-235 Measured-to-Calculated Ratio

Trend of U-235 measured-to-calculated ratio against each sample is shown in Fig. 5.1. The ratio is much higher than 1.0 in the case of samples 4 and 10. On the other hand, the ratios of samples 20-22 and 26 are much lower than 1.0. Although four kinds of calculation resulted different values on each sample, the trend patterns are similar to each other. It means that calculation mechanism and cross-section data are similar to each other. As shown in Fig. 5.1, any SWAT-calculated composition values except sample No 4 is a value between the minimum and maximum of three composition value which were calculated using SAS2H with 27, 44 and 238 group cross-section libraries.

5.2.2. Comparison of the Relative Errors

The relative errors of the calculated U-235 concentration are shown in Fig. 5.2. Maximum errors appeared to be about -25% at sample No 4 and about 30 % at sample No 26, respectively. The effects of axial location of the sample position are compared in Fig.5.3. As unexpected, the relative errors of the end point samples appeared to be rather smaller than the results of the fuel center area. It means that SAS2H and SWAT can take into account the spectrum hardening effect at the end of fuel rod very well. The big error of U-235 composition seems to be resulted from the inaccuracy of experimental data.

The relative errors of 16 nuclides which are separated into two initial enrichments and sorted against burnup in each part are shown in Figs. 5.4 – 5.19. The trend of the relative errors against burnup does not seem to be shown clearly in the Figs. The results of SWAT are under-estimated for all nuclides except U-235, U-238 and Pu-240 in comparison with three results of SAS2H. Specially, it is outstanding that the Pu-239 and Pu-241 relative errors of four calculations are over-estimated.

The relative error predictions of higher actinides such as americium and curium are much larger than the expected. It is necessary to certificate the validation of the experiment data. Uranium, plutonium and actinide compositions are compared in Figs. 5.20 – 5.22. In the cases of uranium and actinides, the U-238 composition is not included. If the composition was included, other nuclide trend could not be observed because U-238 composition is much larger than others. The actinide relative error is much lower, which means the basic condition is correct. But the detailed inspection of the experimental data seems to be required.

5.2.3. Selection of Available Samples

The sorted U-235 relative errors against burnup are presented in Table 5.1. As investigated above, in the cases of samples or4, or10 and almost all samples of the initial enrichment of 2.83 wt%, the relative errors are very large in comparison with others. The big errors seem to be resulted from burnup measuring errors. As shown in the

reference[12], the measurements were carried out by both Karlsruhe and Ispra using Nd-148, Cs-137 destructive and non-destructive methods. In this work, sample or4 was assumed to be 35.1 GWd/tU which were measured using Nd-148 method. But as shown in Table 3.3-4 of the reference, the measured burnup using Cs-137 non-destructive method was 29.35 GWd/tU. As considering an inverse proportion of U-235 composition to burnup and comparing with others, the value of 29.35 GWd/tU seems to be correct rather than 35.1 GWd/tU. In the case of sample or10 and some samples of 2.83 wt%, the measured burnup values seem to be incorrect because of the similar reason. Excepting 10 samples which seem to have some errors in measurement of burnup, 16 available samples are selected: samples or1-or3, or5-or9 and or11-or18.

5.2.4. Comparison of the Means and Standard Deviations of the Measured-to-Calculated Ratios

The means and standard deviations of the measured-to-calculated ratio for the 16 available samples are shown in the Fig. 5.23. Since Am-241, Am-242, Cm-242 and Eu-154 ratios are very larger than others, those are separately presented in Fig. 5.24.

The ratio of the measured to calculated values was used as a parameter. When the ratio is less than unity, the calculation overestimates the measurement, and the ratio becomes closer to unity, they have a better agreement. For many important nuclides for burnup credit criticality safety evaluation, the four methods applied in this study showed good coincidence with measurements in general. As shown in Fig. 5.23, by more precise observations, SWAT results for Pu-239, Pu-241, Am-243 and Cm-244 appear to be closer to unity than the SAS2H results.

It is strange that in the cases of Pu-242, Am-243 and Cm-244, the result of SAS2H with 27 group cross-section library is better than the results of SAS2H with 44 and 238 group cross-section library. It is found that the results of SAS2H with 44 and 238 group cross-section libraries are much improved in the case of Eu-154. The improvement must result from the updating libraries from ENDF/V to ENDF/VI.

Table 5.1. U-235 Relative errors of SAS2H and SWAT Calculated Compositions
in the Case of 26 Obrigheim Spent Fuel Samples

Sample Id	Enrichment (wt%)	Axial Location (cm)	Burnup (GWd/tU)	Exp. Data (g/tU,initial)	(Cal.-Exp.)/Exp.			
					SAS2H		SWAT	
					27 G	44 G	238 G	107 G
or23	2.830	254.7	24.220	8.940E+03	9.351	9.620	11.454	11.857
or24	2.830	15.00	25.450	1.000E+04	-7.880	-8.110	-6.470	-8.830
or22	2.830	242.6	30.160	6.270E+03	16.571	16.938	19.569	19.522
or26	2.830	220.6	32.900	5.040E+03	26.369	26.369	30.099	28.849
or21	2.830	220.6	35.640	4.950E+03	11.576	11.576	15.374	13.798
or25	2.830	132.8	36.670	4.860E+03	7.840	6.872	10.741	6.008
or20	2.830	132.8	36.880	4.410E+03	17.234	16.712	20.975	15.488
or19	2.830	132.8	38.100	5.050E+03	-3.663	-4.594	-0.871	-5.743
or16	3.000	15.00	15.600	1.570E+04	1.338	1.338	1.911	1.720
or9	3.000	15.00	17.130	1.520E+04	-1.974	-1.842	-1.184	-1.645
or3	3.000	15.00	20.180	1.280E+04	2.109	2.109	2.969	2.031
or1	3.000	15.00	21.170	1.370E+04	-8.759	-8.759	-7.737	-8.832
or10	3.000	15.00	22.700	1.440E+04	18.889	18.889	17.917	19.167
or8	3.000	258.0	22.860	1.190E+04	-2.437	-2.269	-1.092	-0.420
or18	3.000	231.0	24.900	1.030E+04	2.718	2.913	4.466	4.757
or15	3.000	258.0	25.810	1.010E+04	0.495	0.792	2.376	2.772
or11	3.000	31.00	25.830	1.080E+04	-6.204	-6.389	-4.907	-6.944
or14	3.000	231.0	27.710	1.010E+04	-8.089	-7.861	-6.228	-6.099
or17	3.000	143.0	29.360	8.780E+03	-2.301	-2.301	-0.159	-1.970
or6	3.000	231.0	30.890	7.480E+03	6.818	6.818	9.332	9.064
or7	3.000	231.0	30.940	7.840E+03	1.620	1.620	4.018	3.814
or13	3.000	143.0	31.140	7.500E+03	5.280	4.973	7.480	5.147
or12	3.000	143.0	31.500	7.610E+03	1.905	1.603	4.074	1.787
or2	3.000	143.0	33.750	6.930E+03	0.043	-0.303	2.756	-0.216
or4	3.000	31.00	35.100	8.440E+03	23.152	23.709	21.481	25.616
or5	3.000	143.5	36.260	6.090E+03	0.722	-0.049	3.415	-0.263

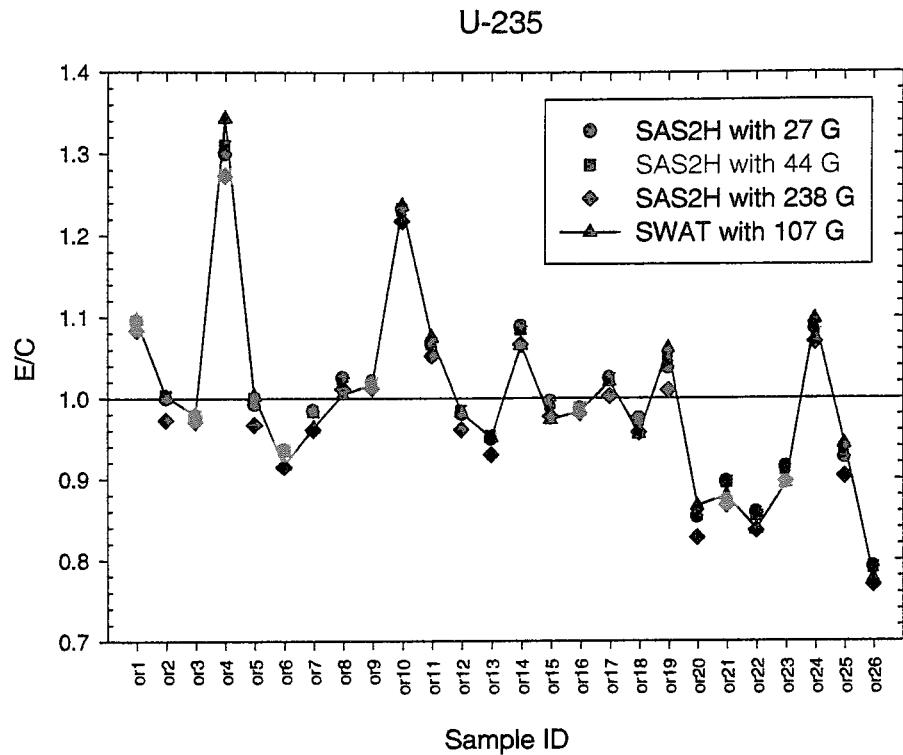


Fig. 5.1. Comparison of U-235 Measured-to-Calculated Ratios.

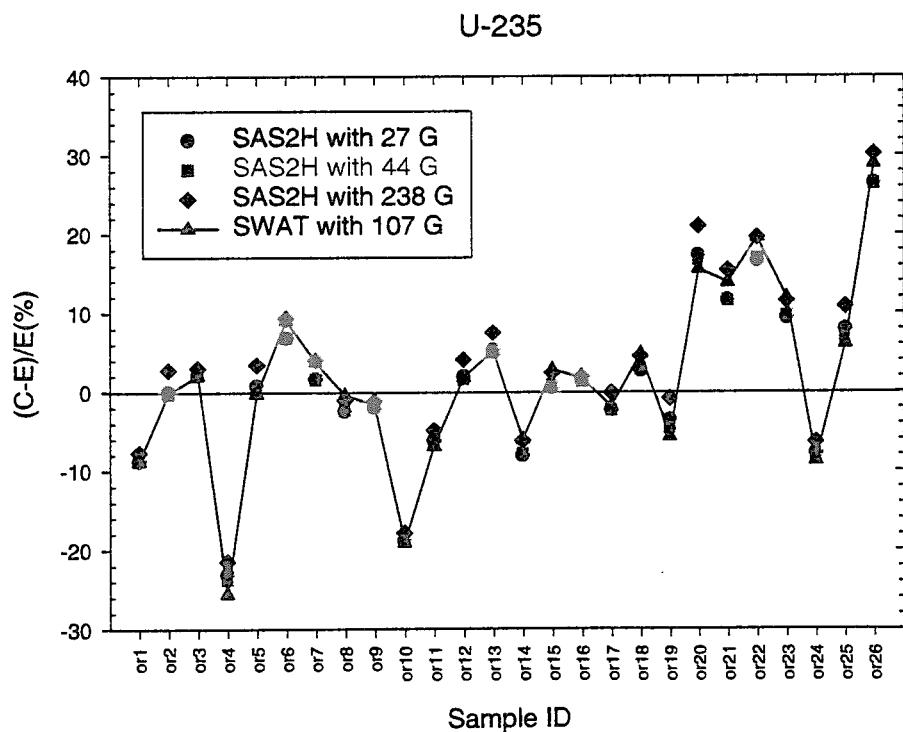


Fig. 5.2. Relative Errors of U-235 Calculated Compositions against Sample ID.

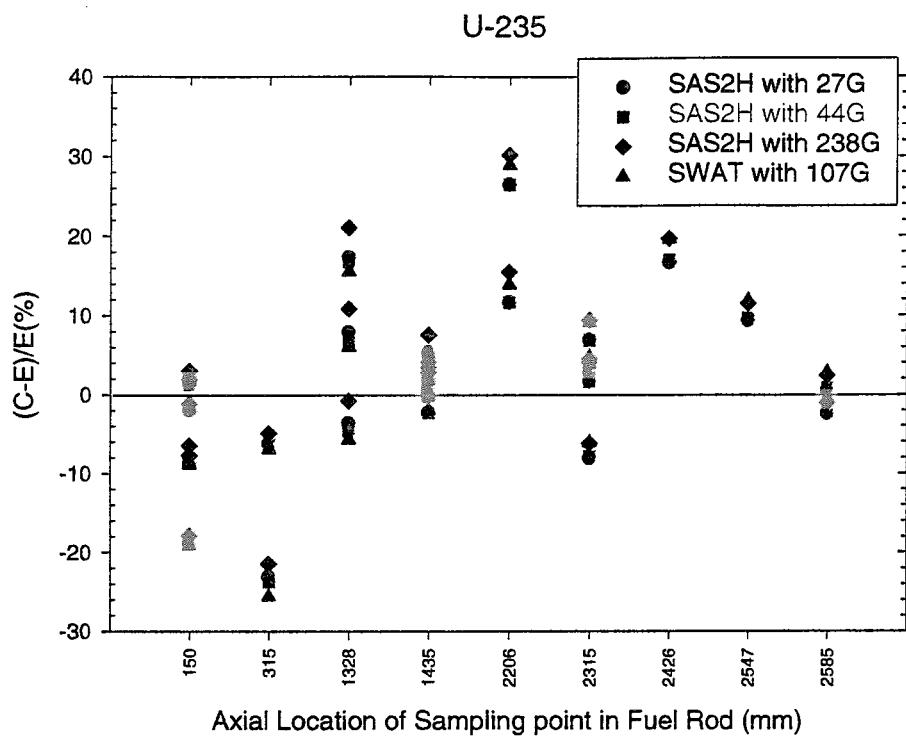


Fig. 5.3. Relative Errors of U-235 Calculated Compositions against Axial Location.

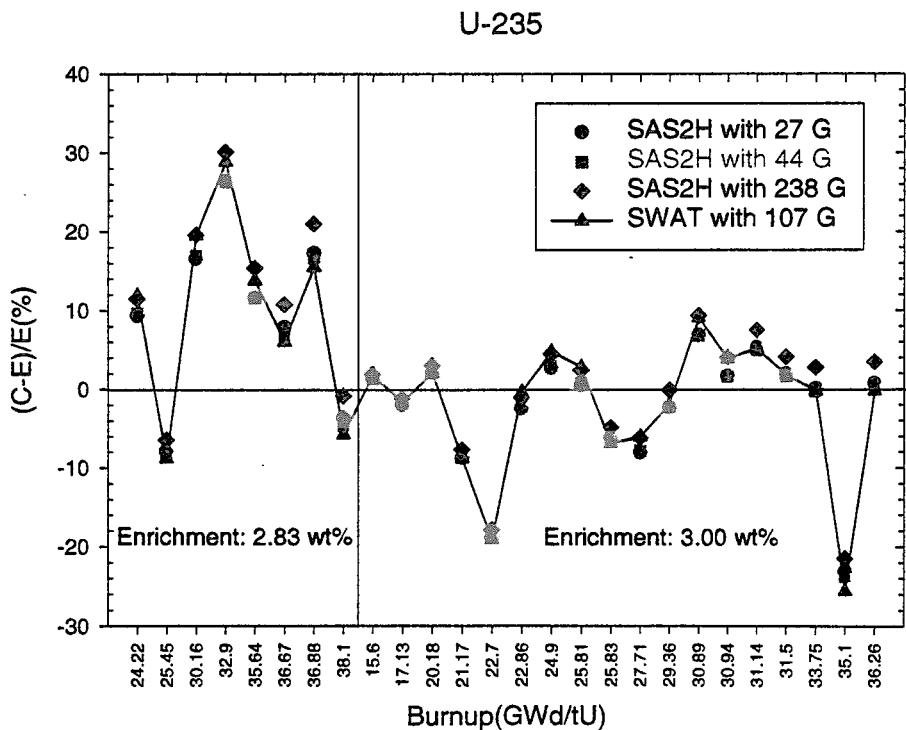


Fig. 5.4. Relative Errors of U-235 Calculated Compositions.

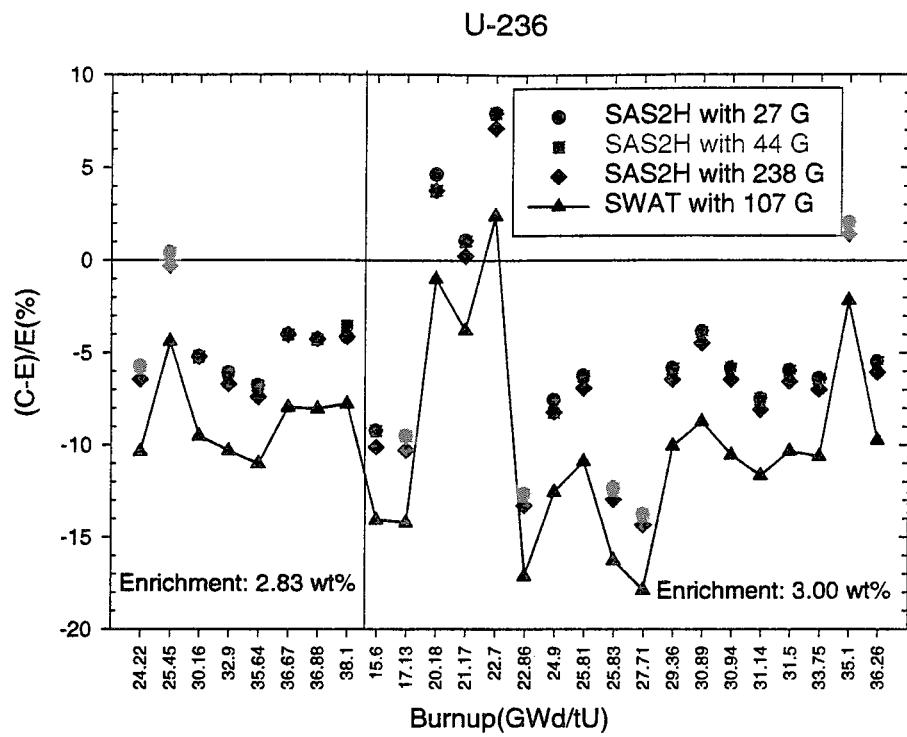


Fig. 5.5. Relative Errors of U-236 Calculated Compositions.

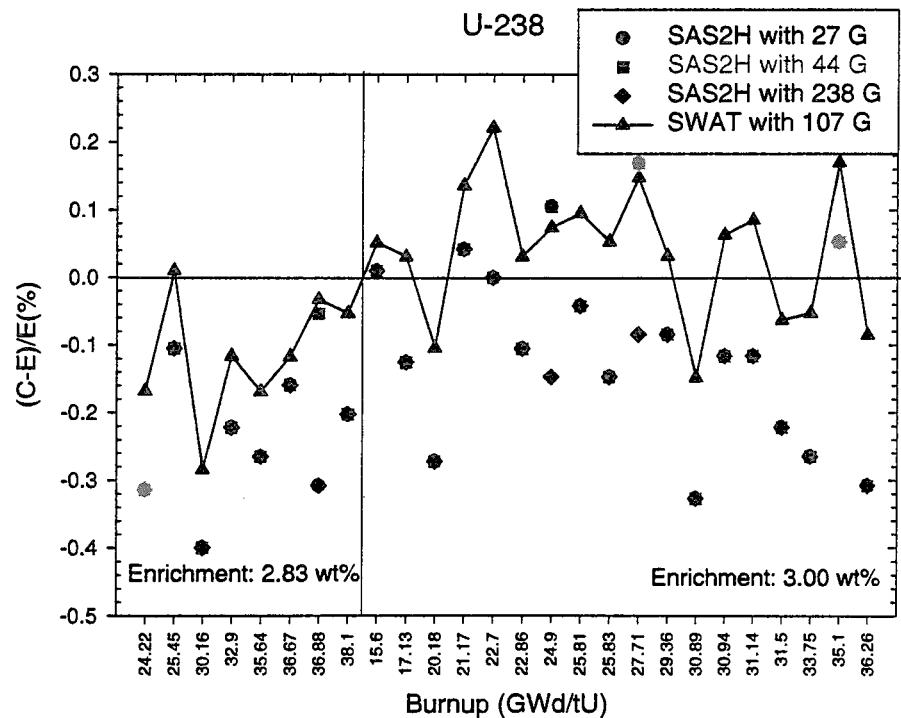


Fig. 5.6. Relative Errors of U-238 Calculated Compositions.

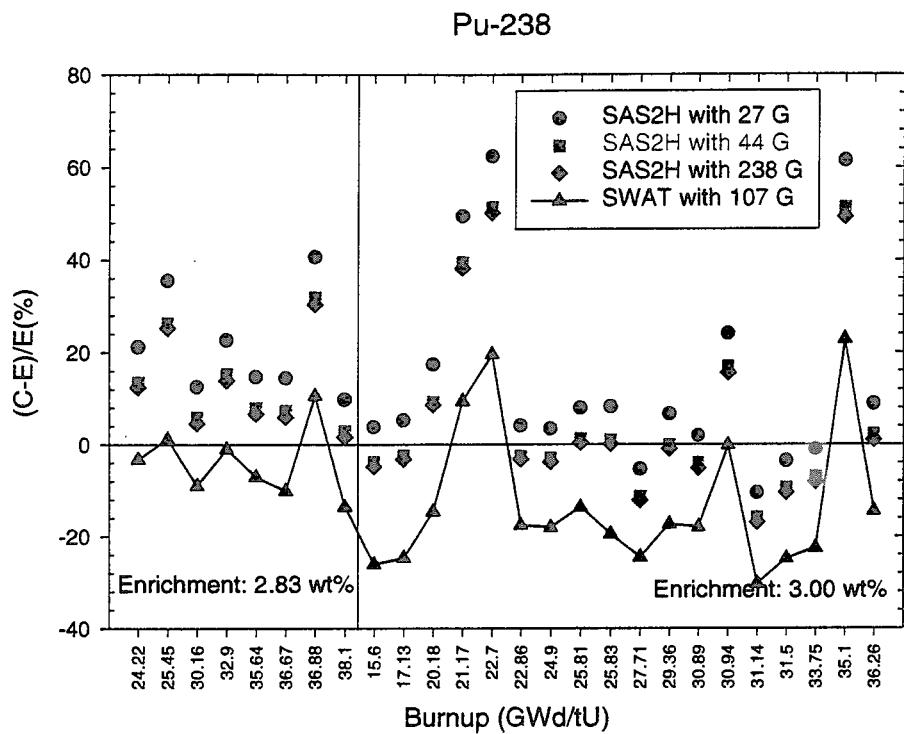


Fig. 5.7. Relative Errors of Pu-238 Calculated Compositions.

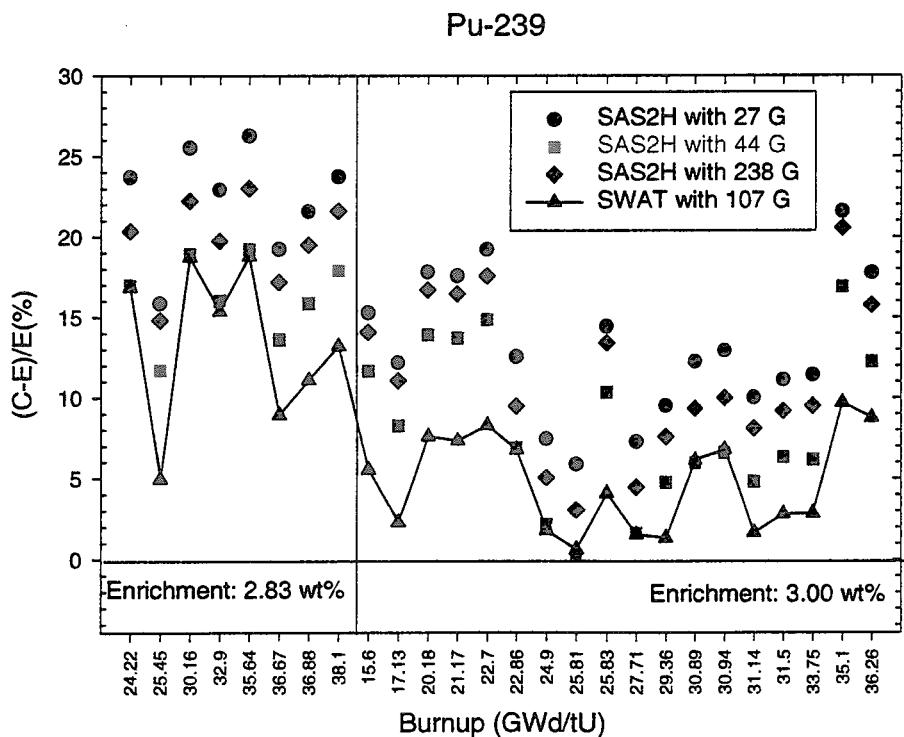


Fig. 5.8. Relative Errors of Pu-239 Calculated Compositions.

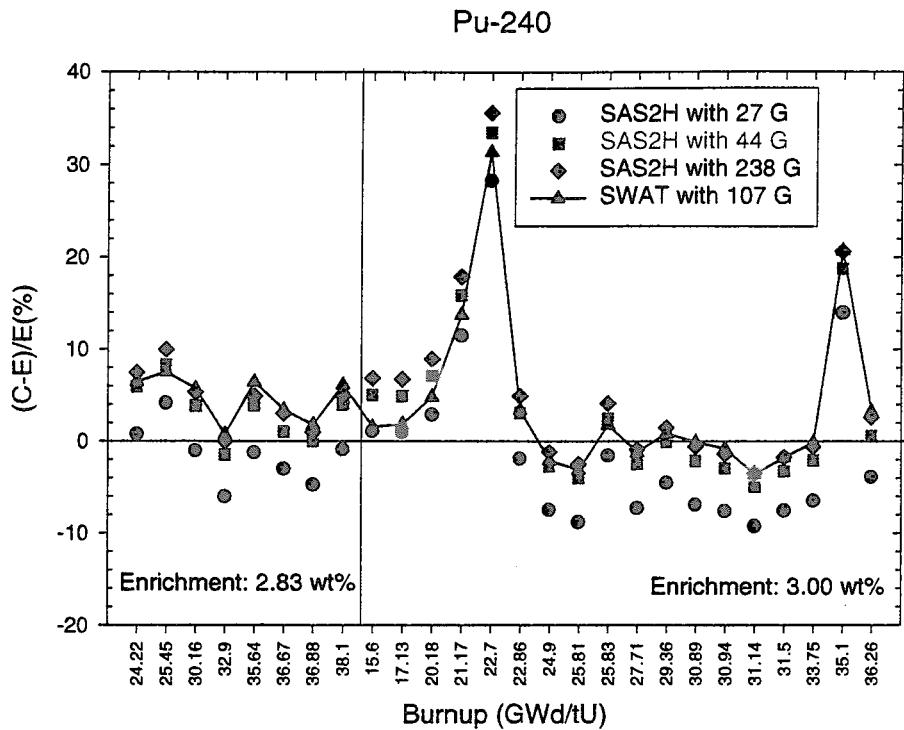


Fig. 5.9. Relative Errors of Pu-240 Calculated Compositions.

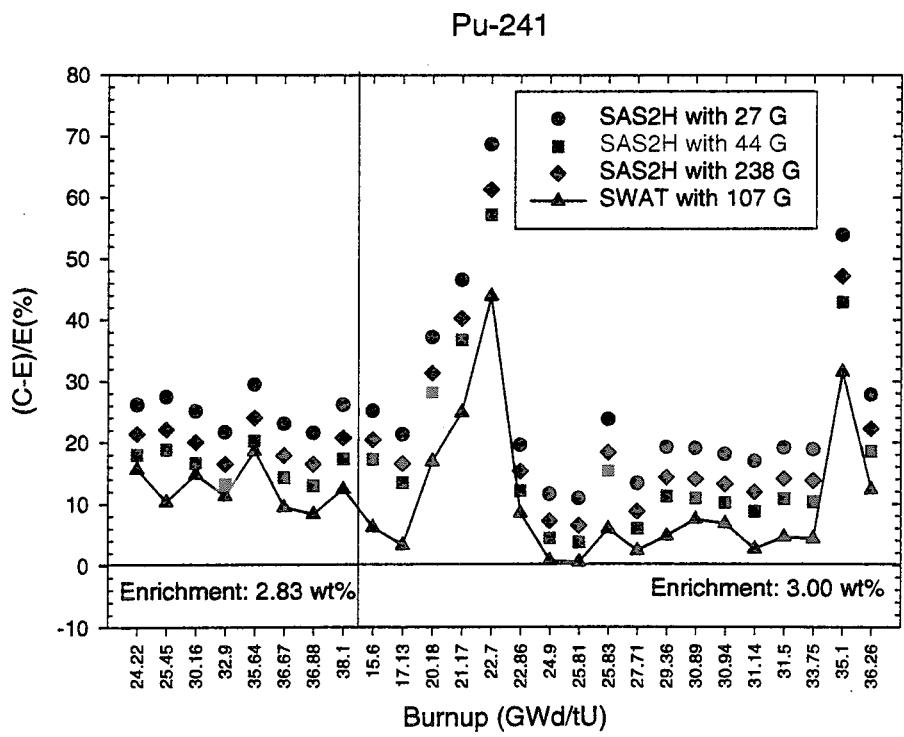


Fig. 5.10. Relative Errors of Pu-241 Calculated Compositions.

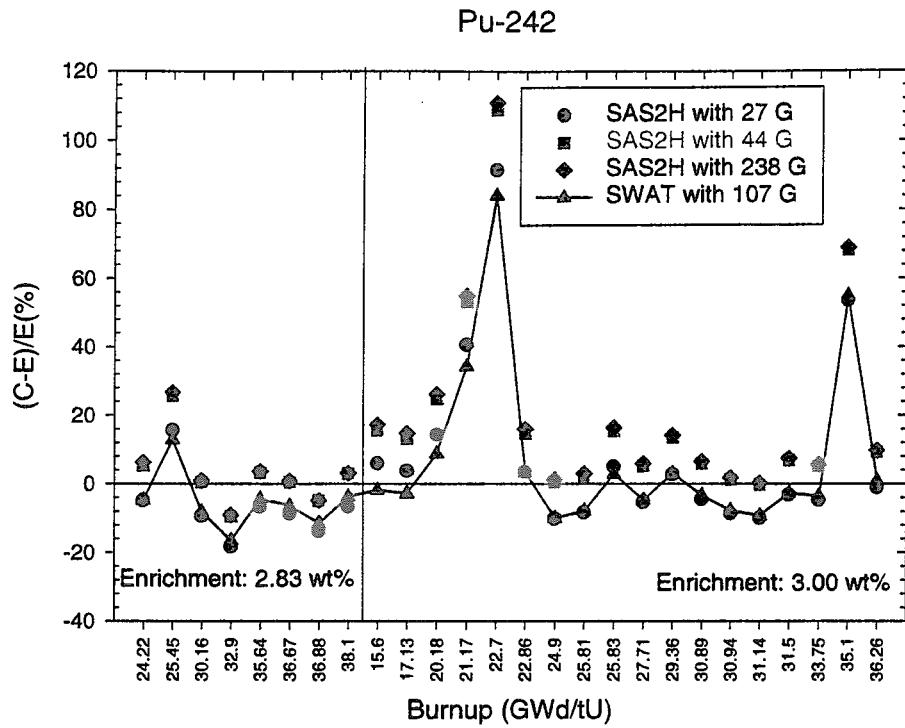


Fig. 5.11. Relative Errors of Pu-242 Calculated Compositions.

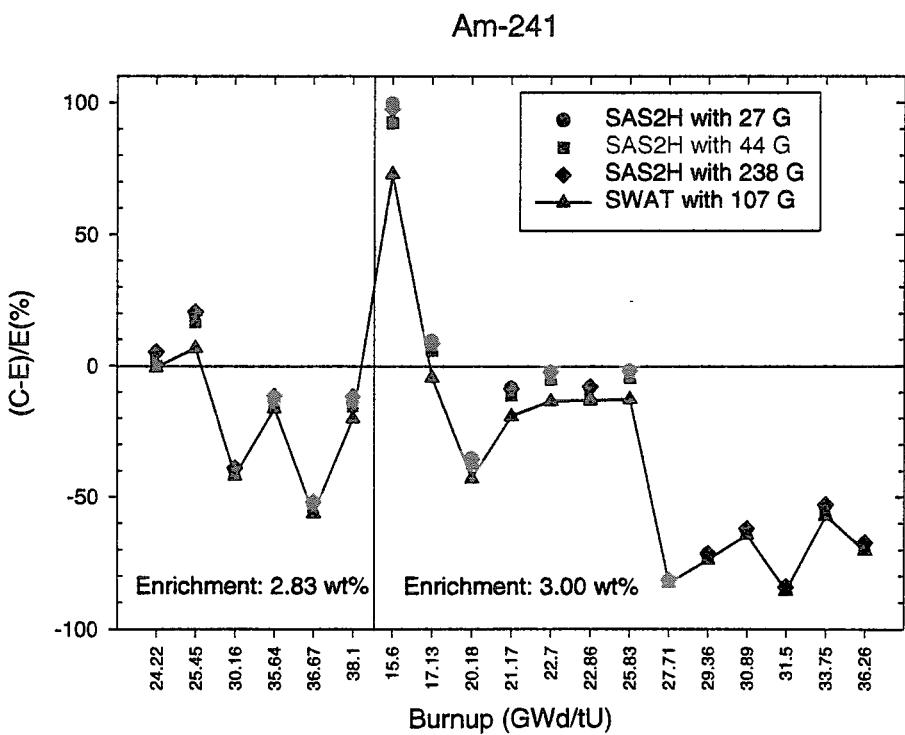


Fig. 5.12. Relative Errors of Am-241 Calculated Compositions.

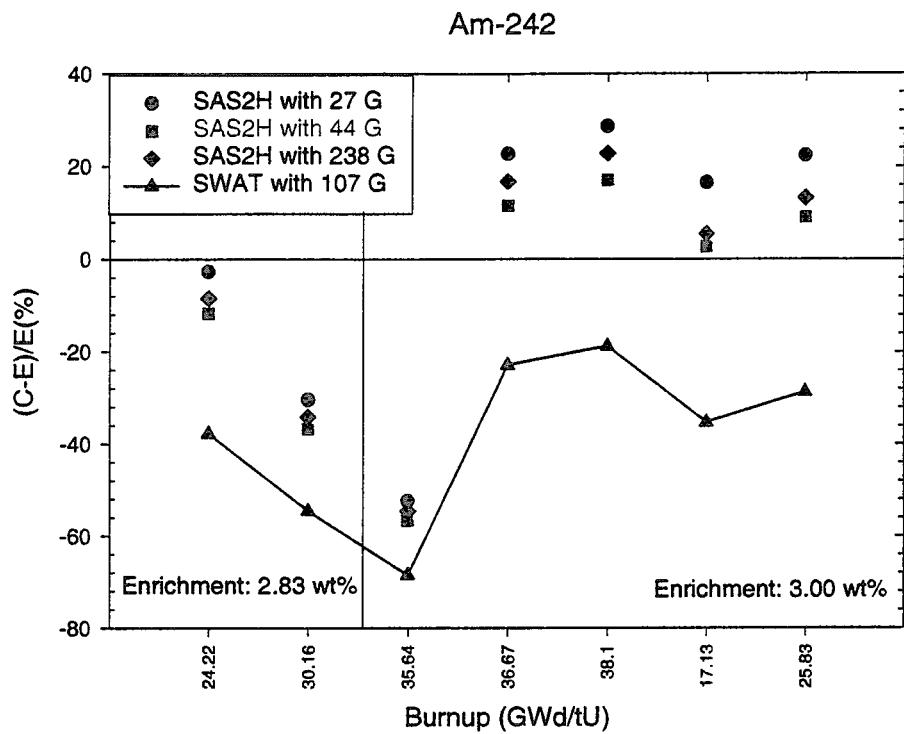


Fig. 5.13. Relative Errors of Am-242 Calculated Compositions.

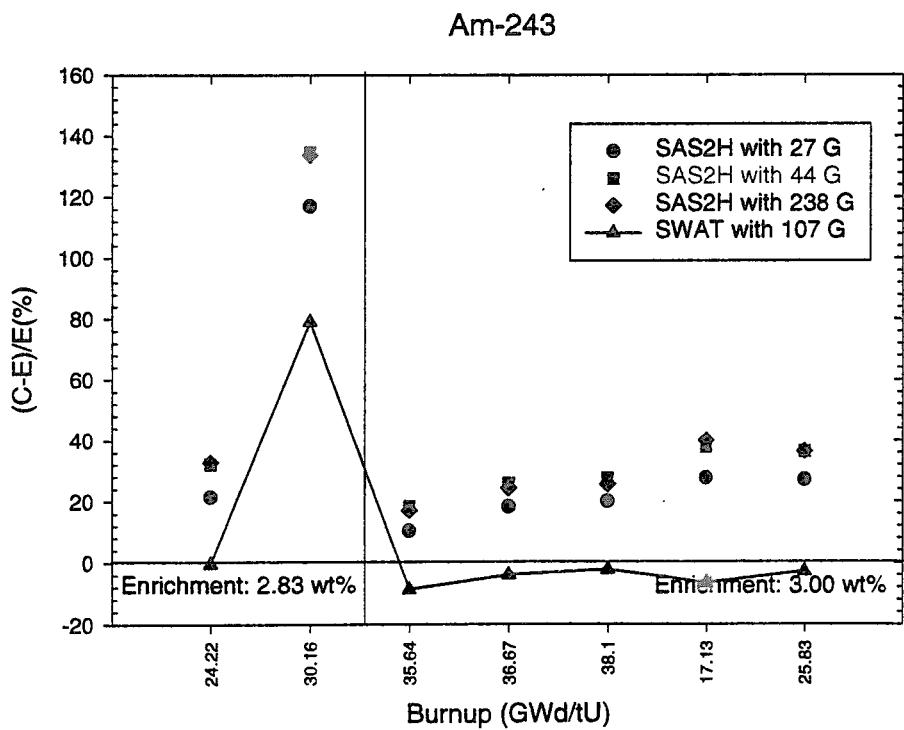


Fig. 5.14. Relative Errors of Am-243 Calculated Compositions.

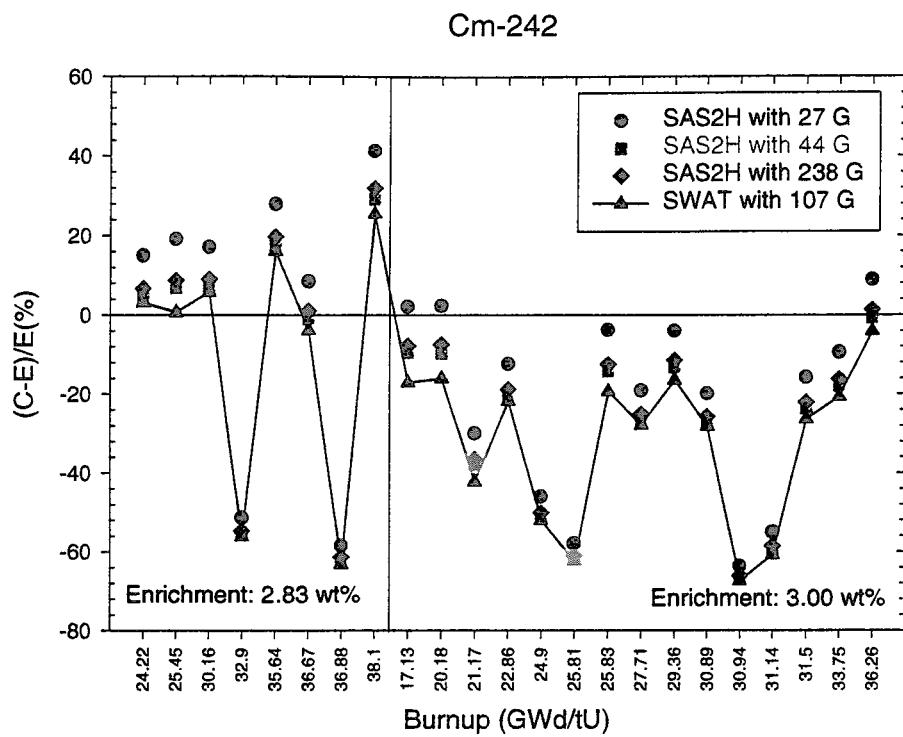


Fig. 5.15. Relative Errors of Cm-242 Calculated Compositions.

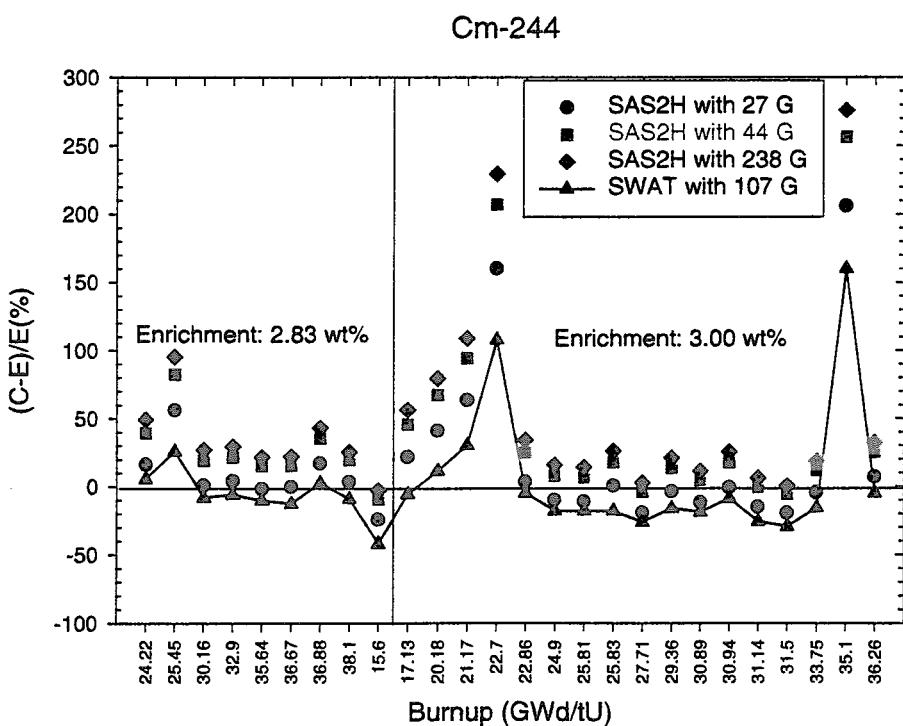


Fig. 5.16. Relative Errors of Cm-244 Calculated Compositions.

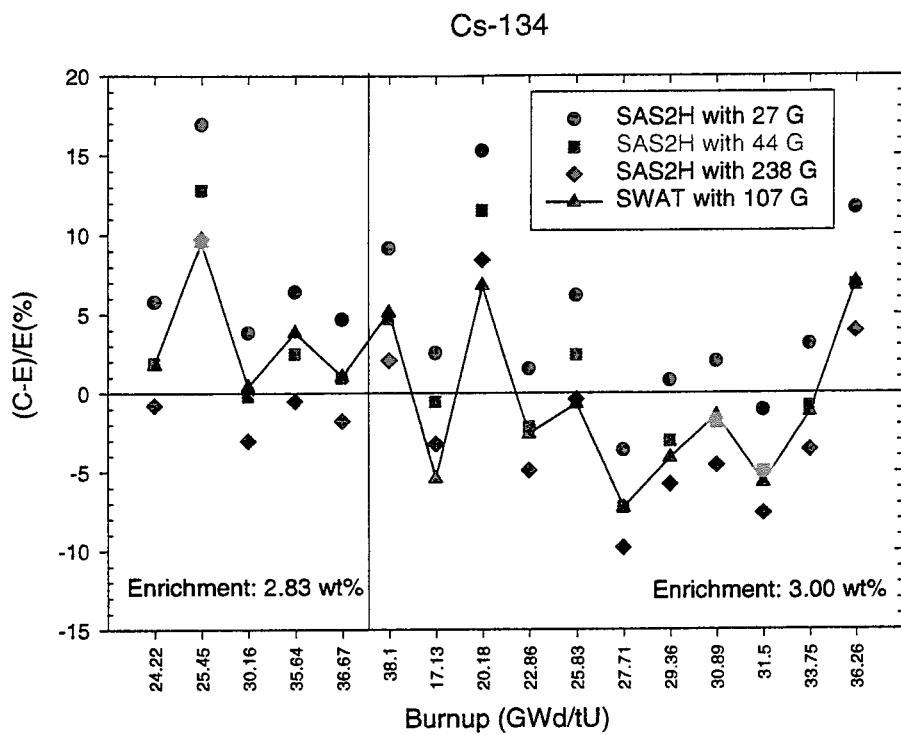


Fig. 5.17. Relative Errors of Cs-134 Calculated Compositions.

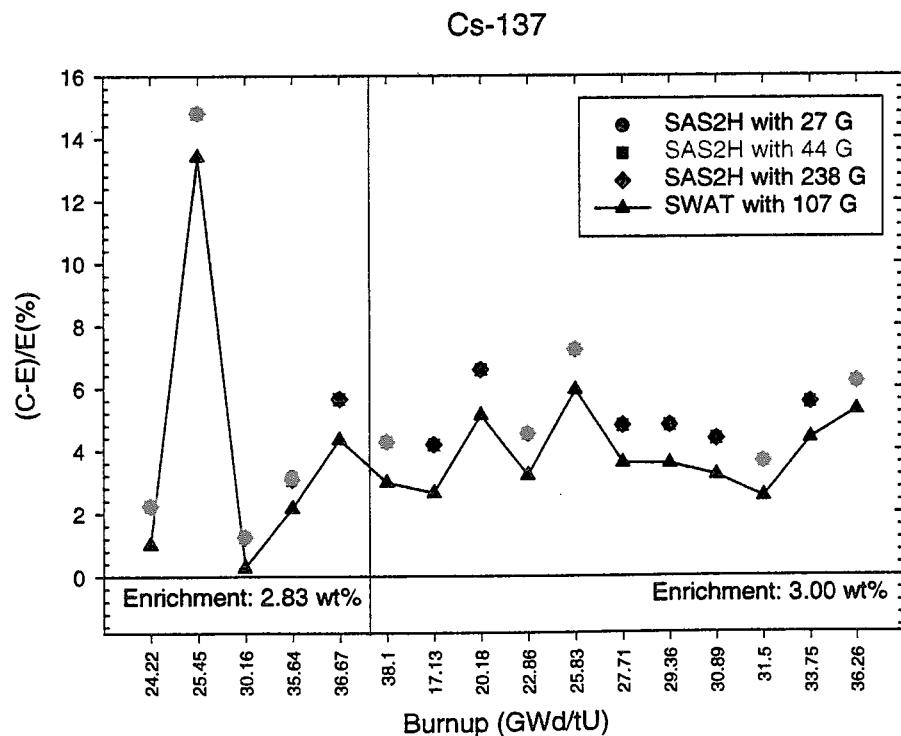


Fig. 5.18. Relative Errors of Cs-137 Calculated Compositions.

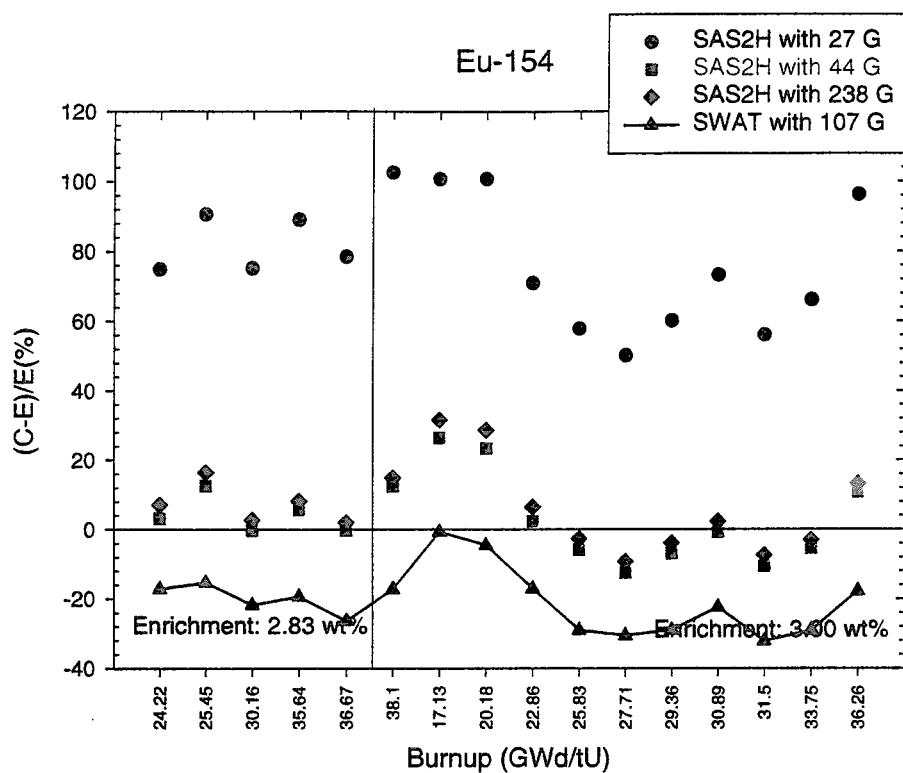


Fig. 5.19. Relative Errors of Eu-154 Calculated Compositions.

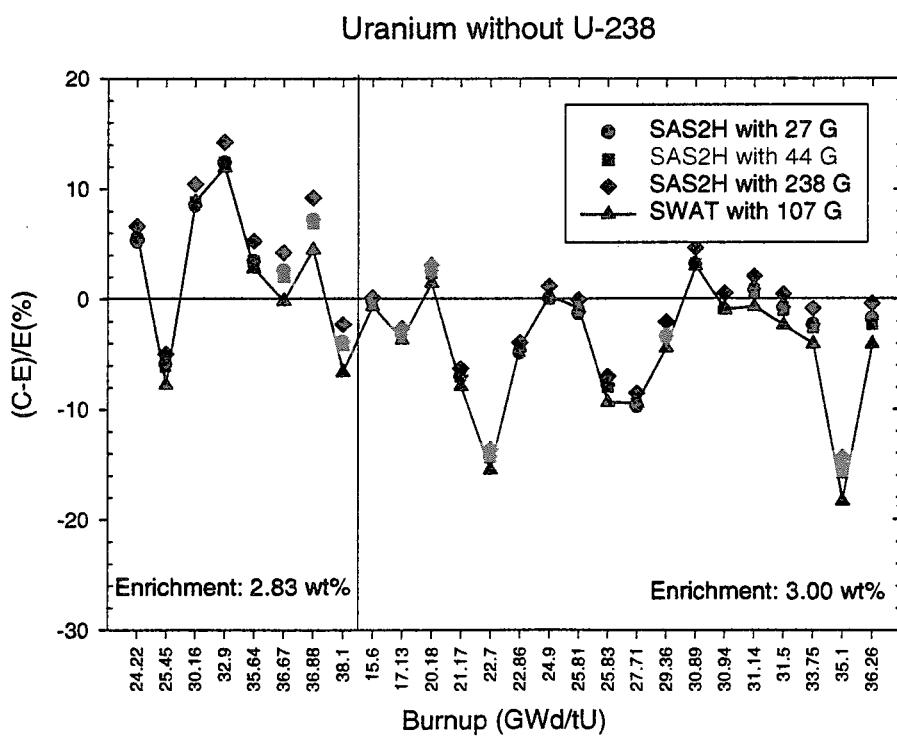


Fig. 5.20. Relative Errors of Uranium Calculated Compositions without U-238.

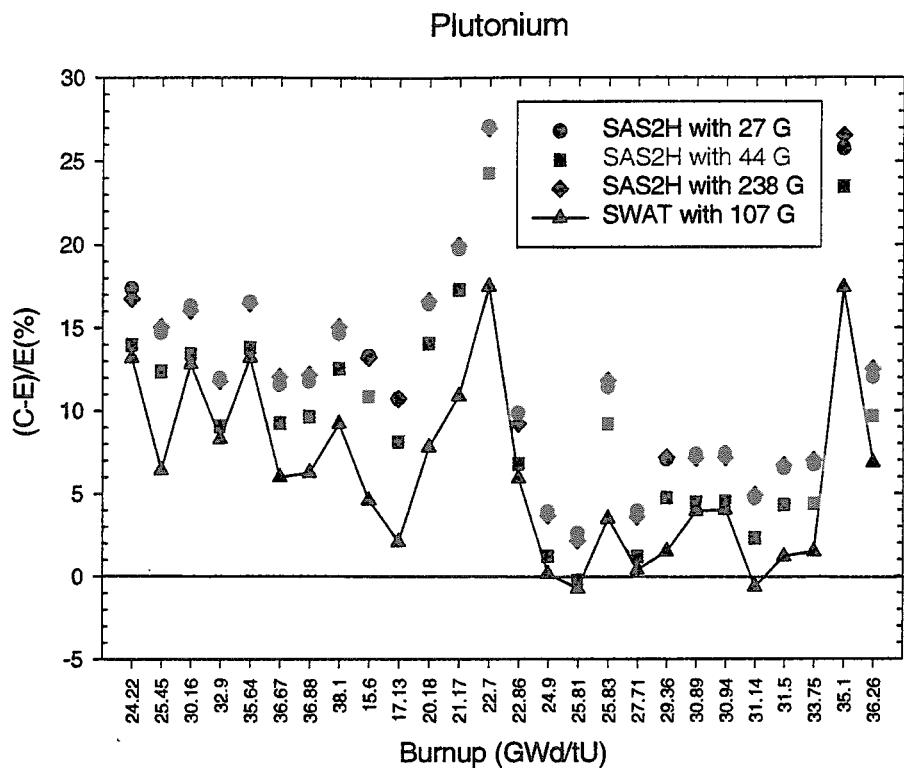


Fig. 5.21. Relative Errors of Plutonium Calculated Compositions.

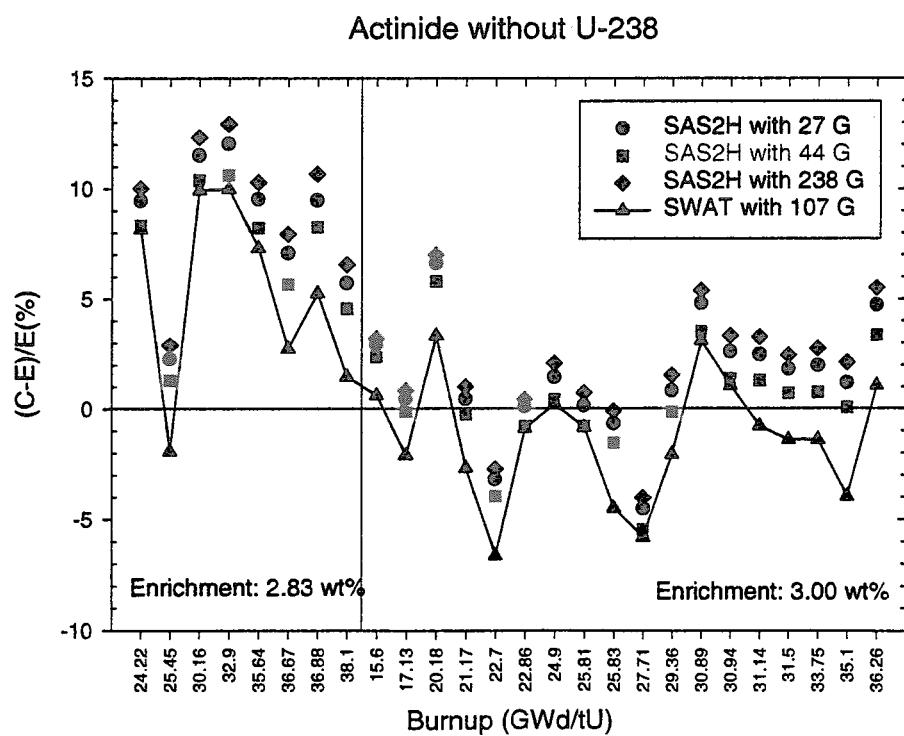


Fig. 5.22. Relative Errors of Actinide Calculated Compositions without U-238.

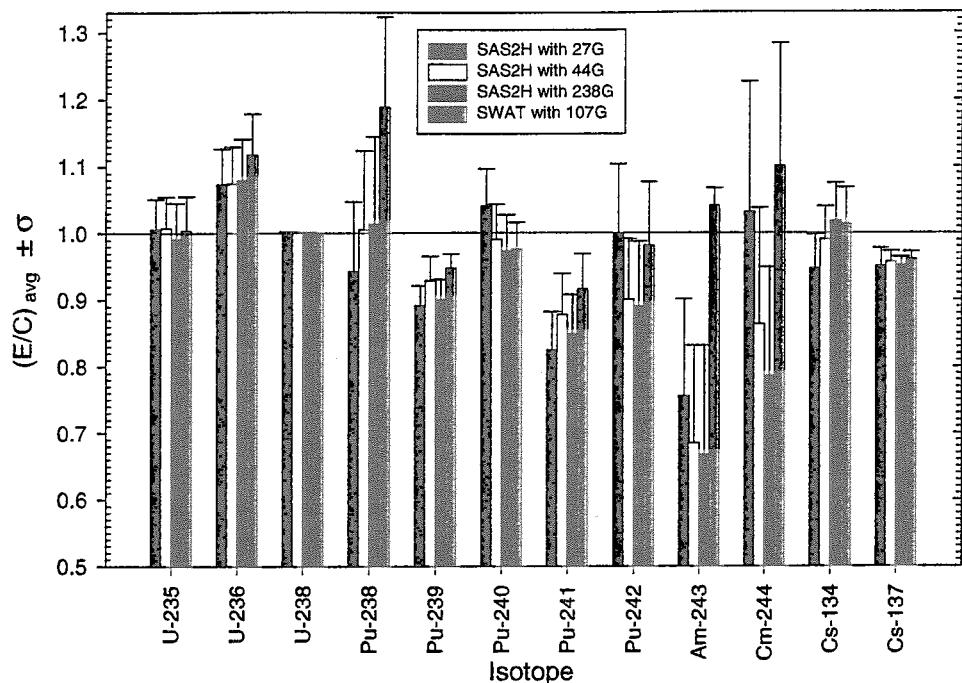


Fig. 5.23. Comparison of the Average Measured-to-calculated Ratios and Standard Deviations.

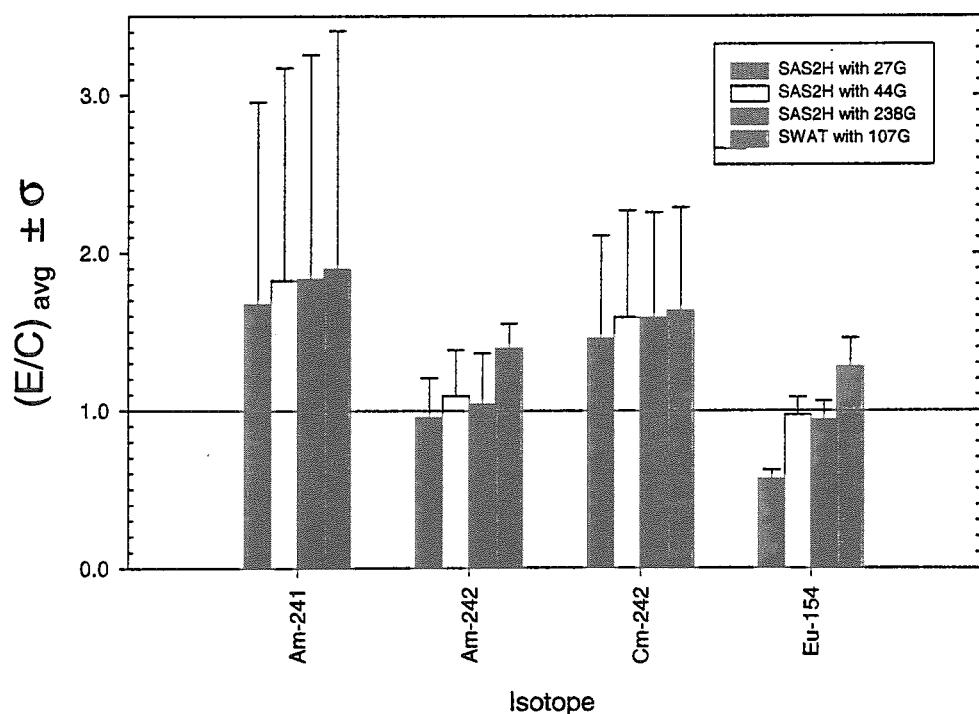


Fig.5.24. Comparison of the Average Measured-to-calculated Ratios and Standard Deviations for the large deviation nuclides.

6. Isotopic Composition Calculation for 55 Spent Fuel Samples

6.1. Input Preparation

Modeling optimization for SAS2H input for 55 samples were carried out in ORNL and DOE reports[18,19]. In this work, in the case of 27 group calculation the inputs listed in DOE report [19] were used without changing parameter values. In cases of calculation with 44 and 238 group libraries, neutron cross-section library and cladding material names were replaced by appropriate names. In the case of the calculation with 238 group library, some nuclides which were included in the fuel region to generate new cross-section library were excluded in order to reduce computer running time.

Fifty-five SWAT inputs were prepared by a fortran program which can extract fuel design specifications and operating parameters from the SAS2H inputs for 55 PWR samples and transform the data to SWAT input form. In the 55 samples some samples are different from modern PWR fuel. Some reactors have cross-form control devices and two kinds of enrichment fuel rods in the same assembly. However, in this work, the only simple modeling for SWAT calculation was carried out.

6.2. Comparison of Calculation Results with Experimental Data

Four measured-to-calculated ratios of U-235 against each sample are presented in Fig. 6.1. In two samples, ca8 and ca9, the ratios of SWAT calculation result are about 17 % difference, which is much lower than 26 Obrigheim samples. As shown in Fig. 6.1, the results of SWAT seem to be not much different from SAS2H results. In Fig. 6.2 the relative errors of U-235 composition are presented against the axis location of sampling point in the fuel rod. A special trend of the relative error against the axial location was not observed.

The relative errors of 21 nuclides against each sample were presented in Fig. 6.3 - 6.23. SWAT results are similar to SAS2H results in the cases of U-234, U-235 and U-238. Especially for U-234, the SWAT result is very close to SAS2H, as shown in Fig. 6.4. However in general, SWAT results seemed to be under-estimated in comparison to SAS2H results for all nuclides except Pu-240, Cs-134 and Nd148. In the cases of Am-242, Am-243,

Sm-149 and Eu-154, SWAT results are much different from SAS2H results and under-estimated.

The relative errors of uranium, plutonium and actinide calculation to experimental data are shown in Figs. 6.24-6.26. The trends of the materials are almost similar to the cases of 26 samples (see Figs. 5.20 - 5.22).

The mean and standard deviation of the measured-to-calculated ratios for actinide and fission products, respectively, are presented in Figs. 6.27 and 6.28, respectively, which indicate the bias and uncertainties in estimates of actinides and fission products using SAS2H with 27, 44 and 238 group cross-section libraries, and SWAT with the 107 group cross section library. Large biases are therefore required when these combinations are applied to the estimates of Am-241, Cm-242, Sn-126 and Sm-149. When SWAT with the 107 group cross section library is applied, further biasses are necessary for Am-242, -243 and Cm-244.

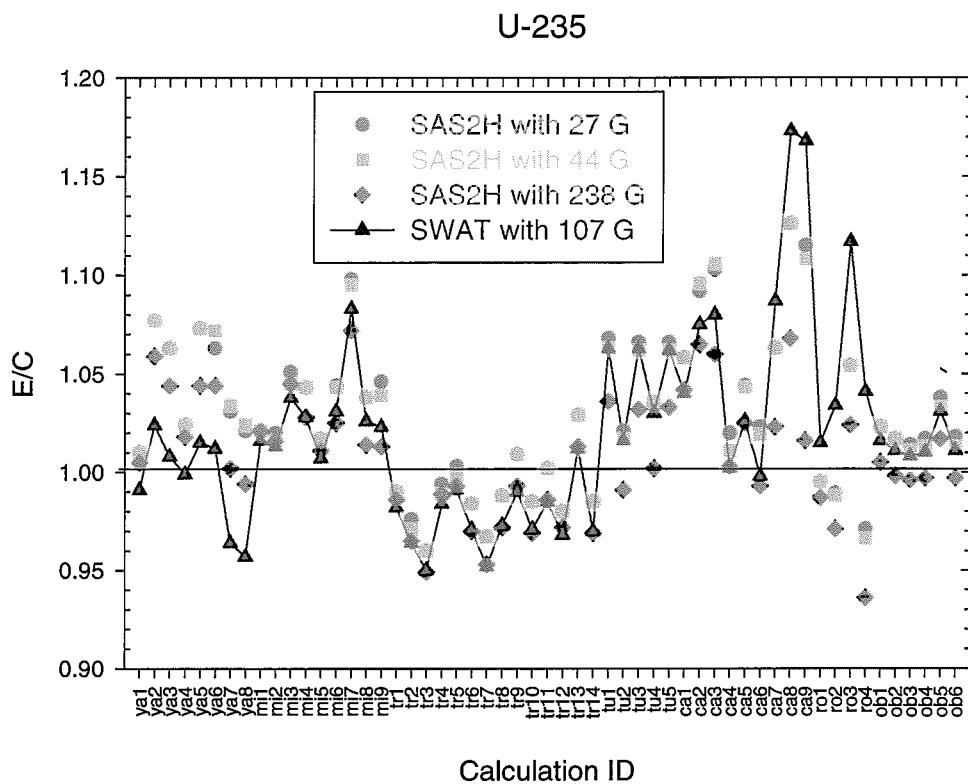


Fig. 6.1. Comparison of U-235 Measured-to-Calculated Ratios.

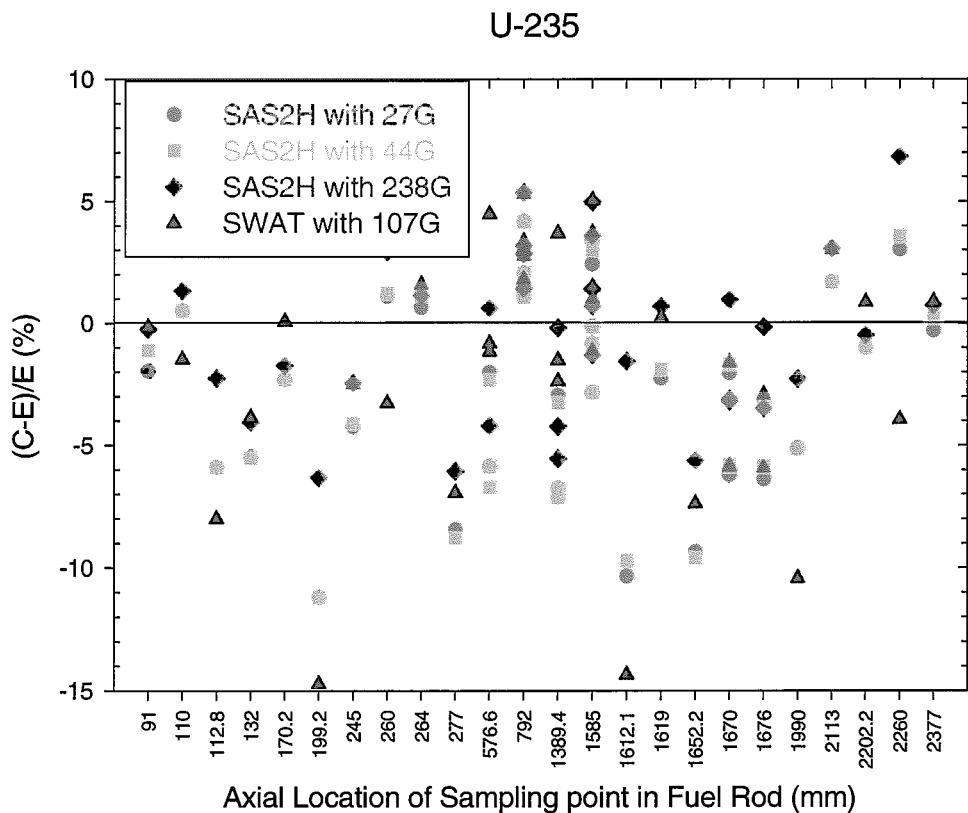


Fig. 6.2. Relative Errors of U-235 Calculated Compositions.

U-235

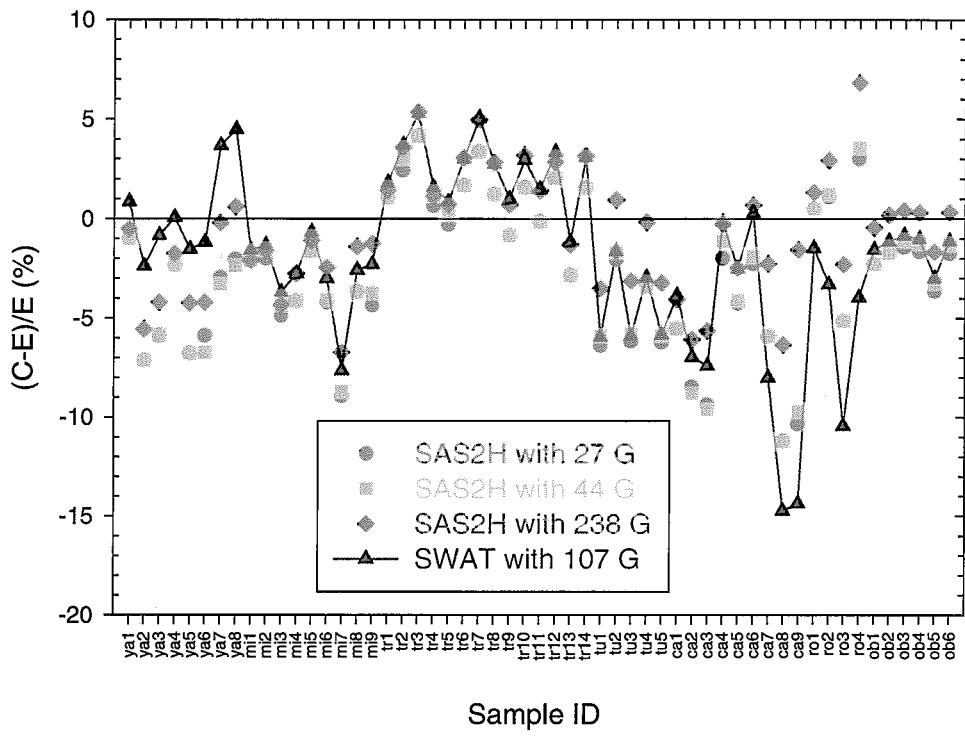


Fig. 6.3. Relative Errors of U-235 Calculated Compositions.

U-234

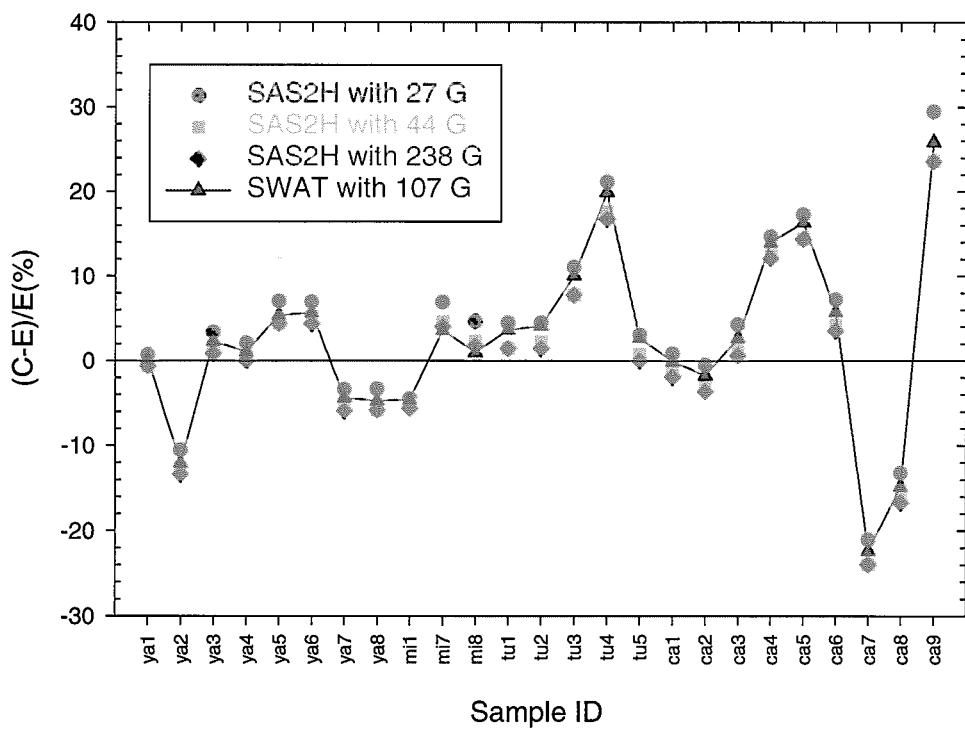


Fig. 6.4. Relative Errors of U-234 Calculated Compositions.

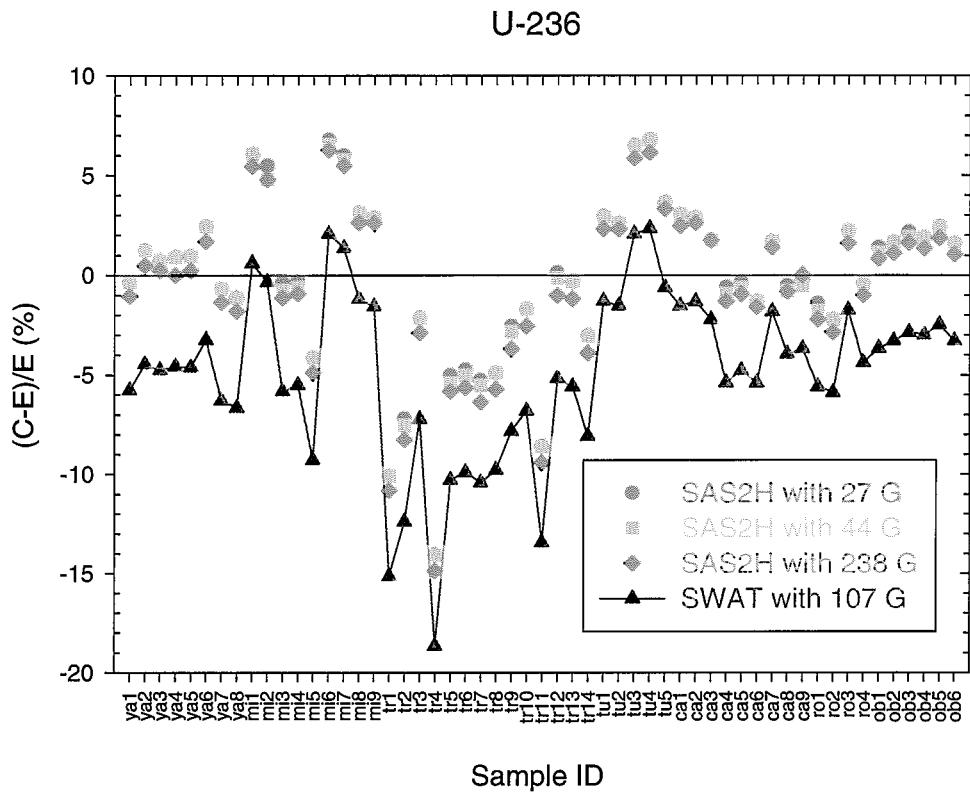


Fig. 6.5. Relative Errors of U-236 Calculated Compositions.

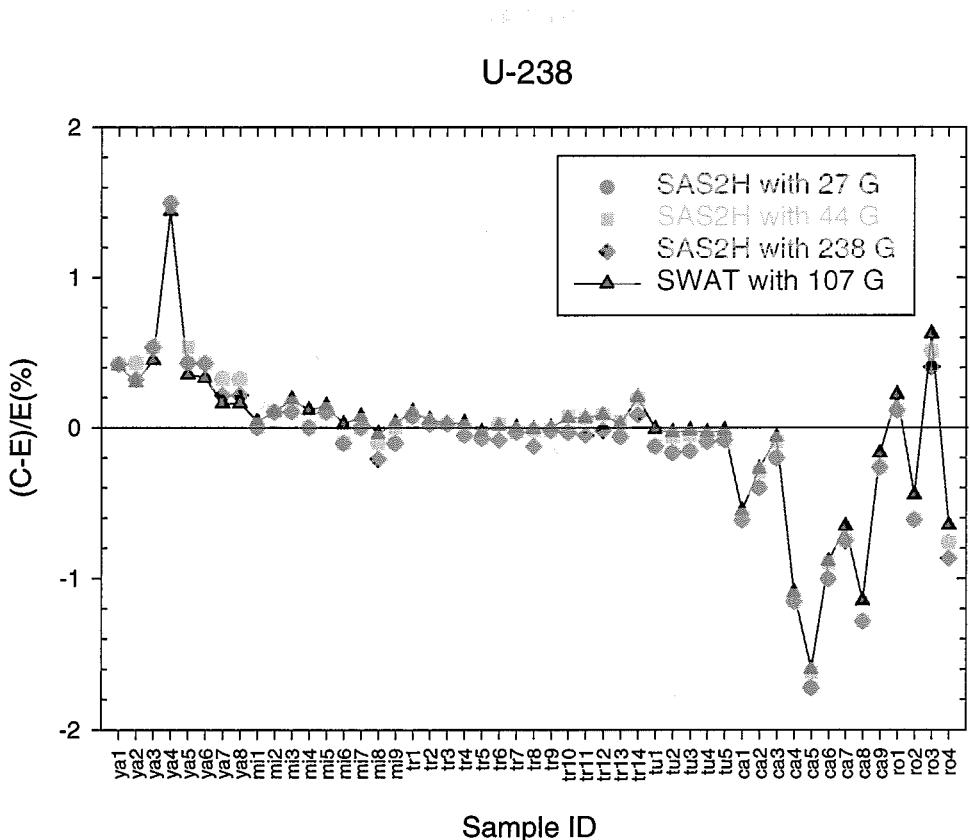


Fig. 6.6. Relative Errors of U-238 Calculated Compositions.

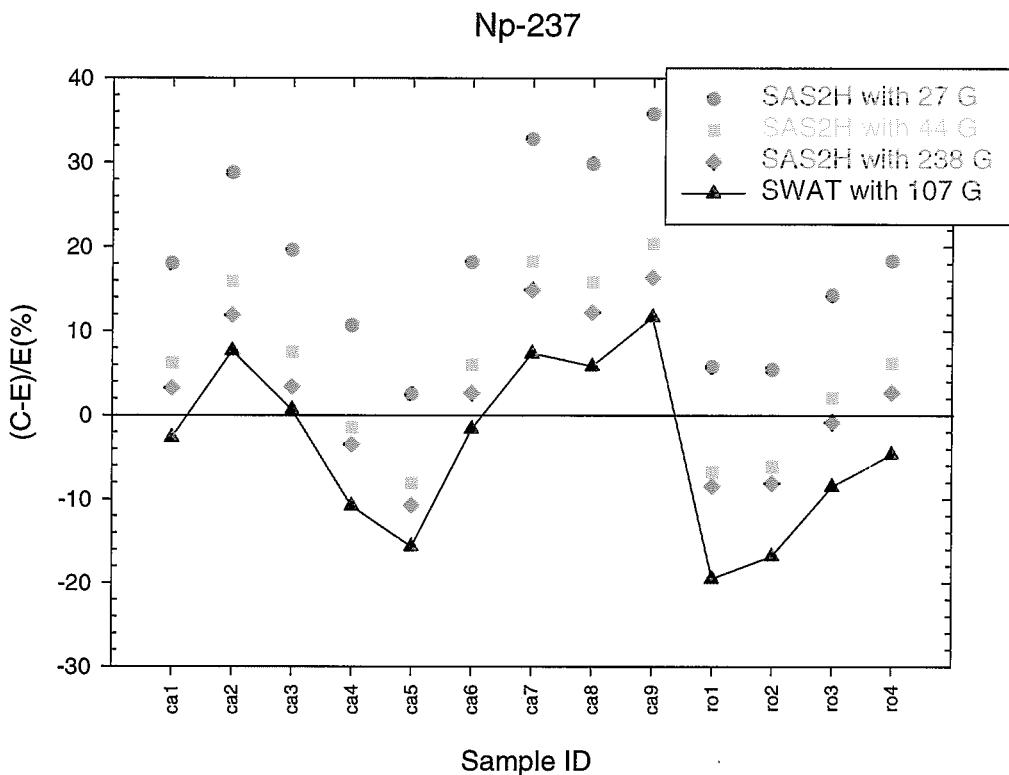


Fig. 6.7. Relative Errors of Np-237 Calculated Compositions.

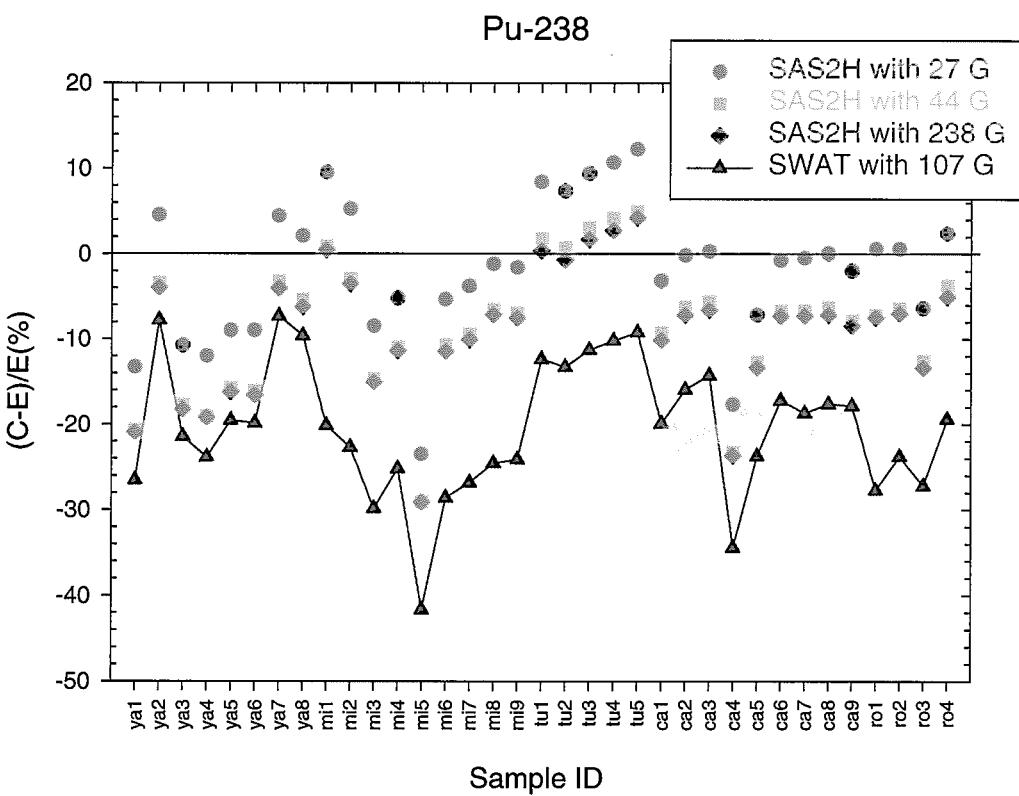


Fig. 6.8. Relative Errors of Pu-238 Calculated Compositions.

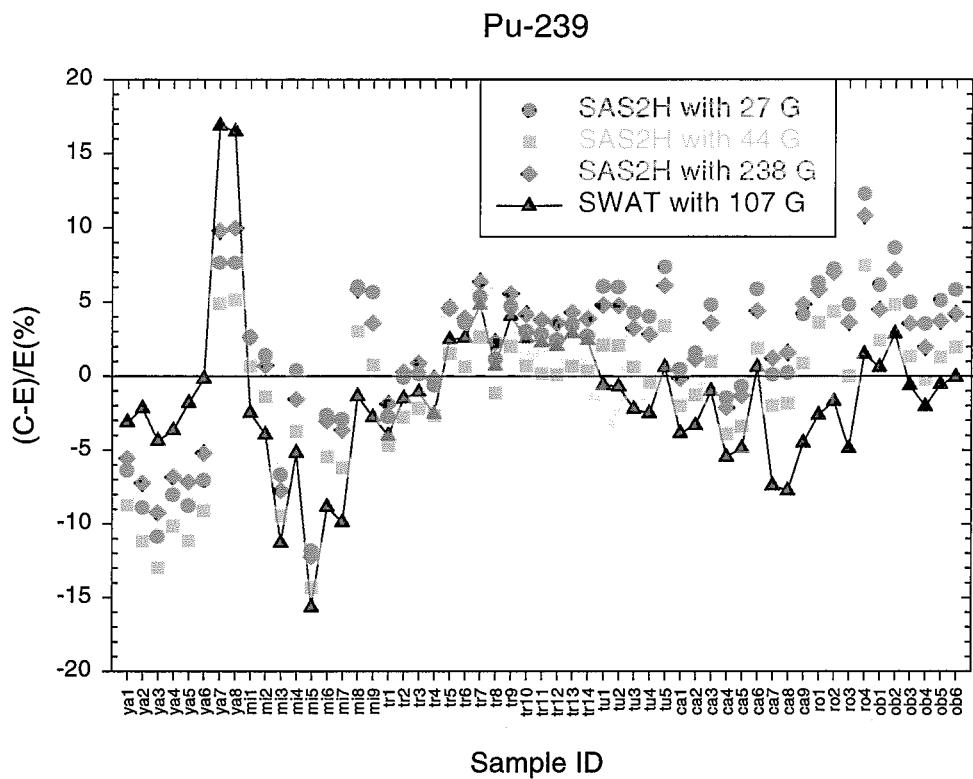


Fig. 6.9. Relative Errors of Pu-239 Calculated Compositions.

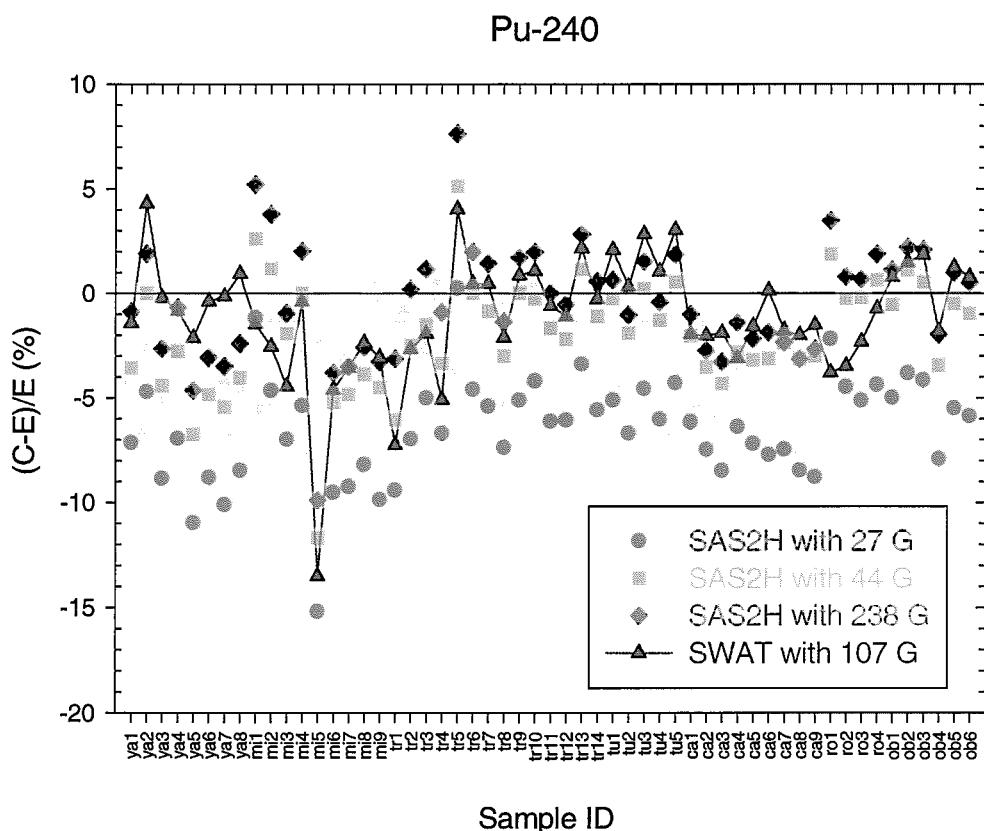


Fig. 6.10. Relative Errors of Pu-240 Calculated Compositions.

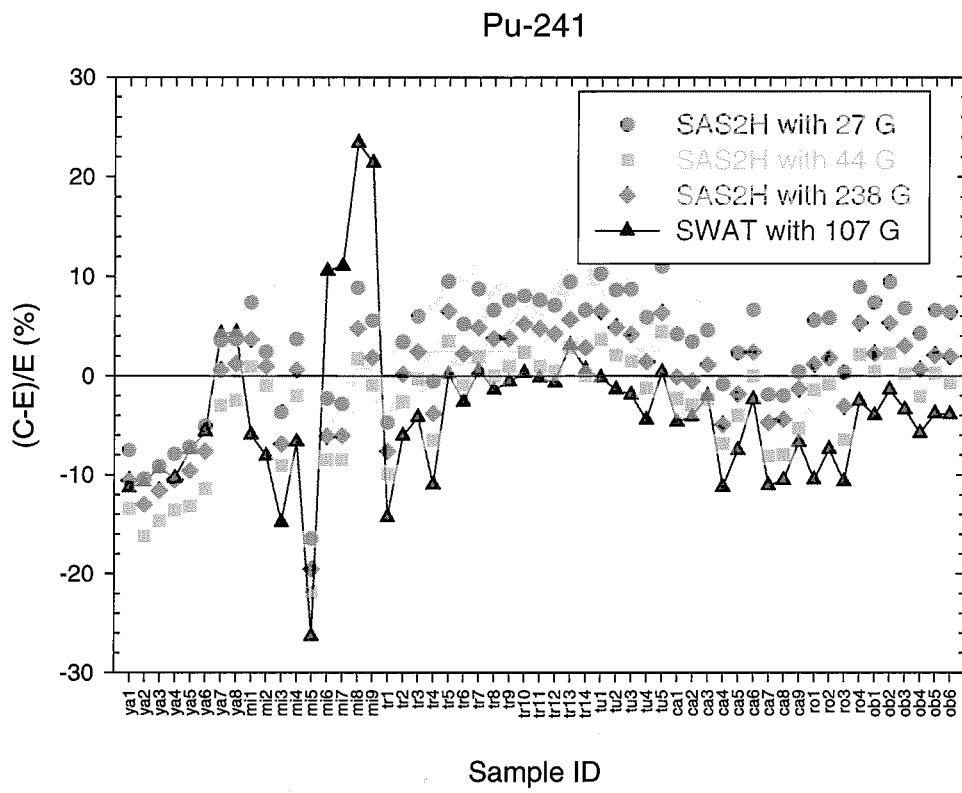


Fig. 6.11. Relative Errors of Pu-241 Calculated Compositions.

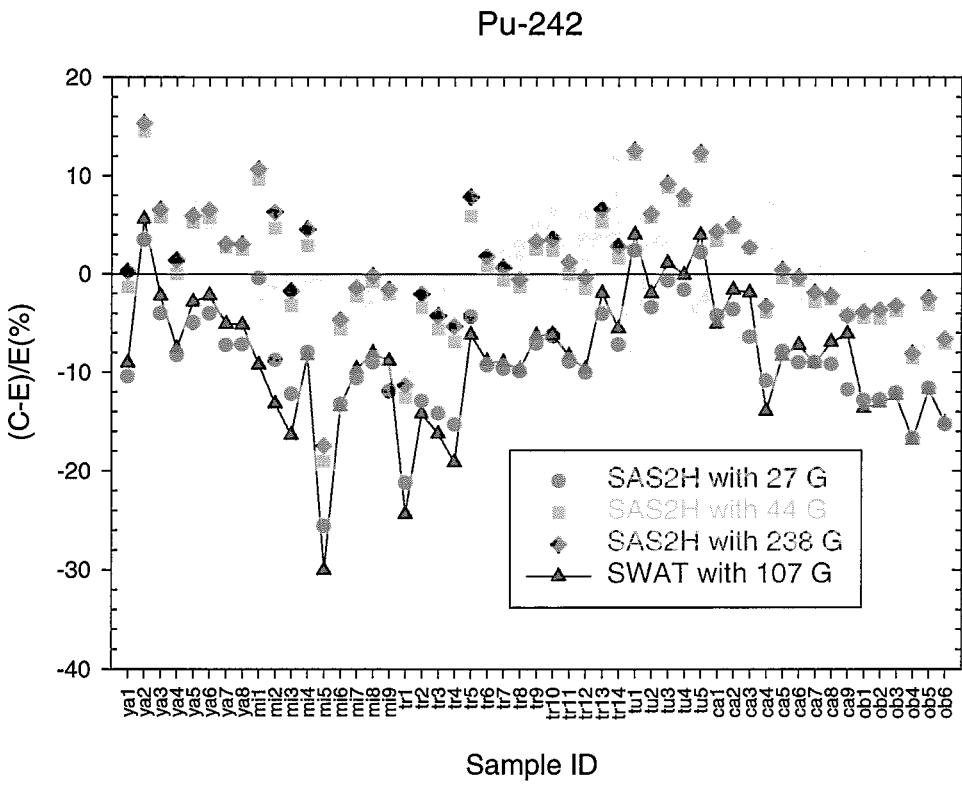


Fig. 6.12. Relative Errors of Pu-242 Calculated Compositions.

Am-241

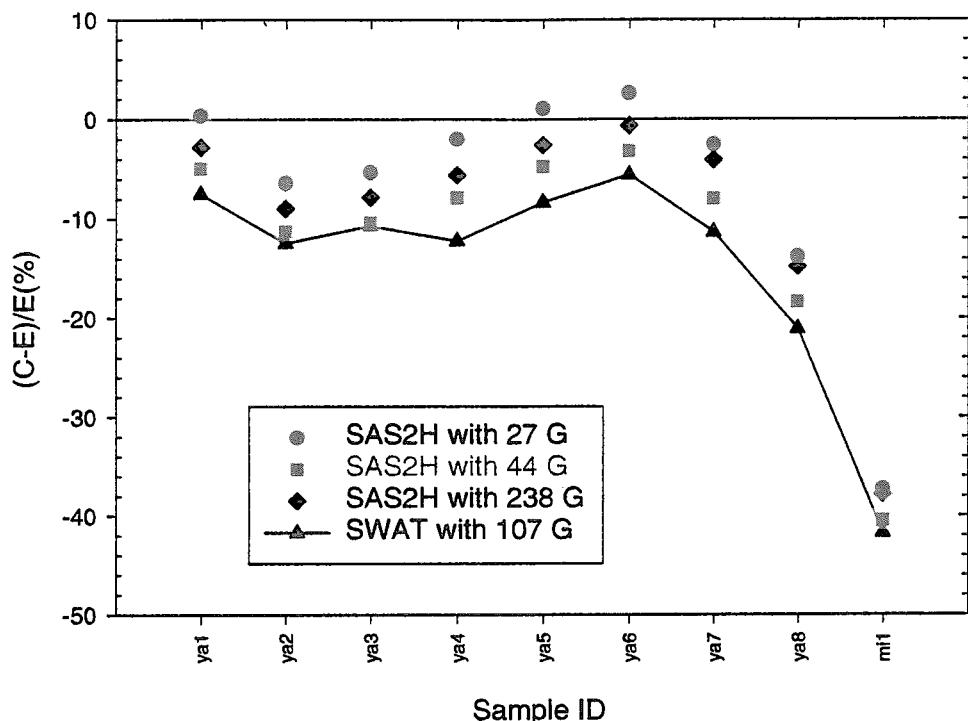


Fig. 6.13. Relative Errors of Am-241 Calculated Compositions.

Am-242

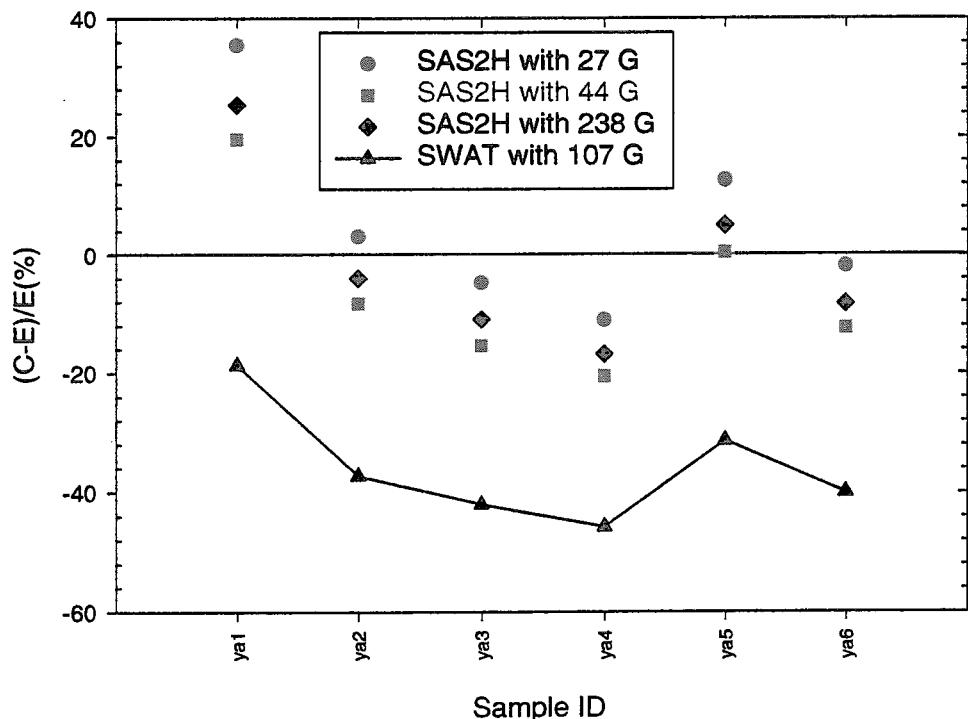


Fig. 6.14. Relative Errors of Am-242 Calculated Compositions.

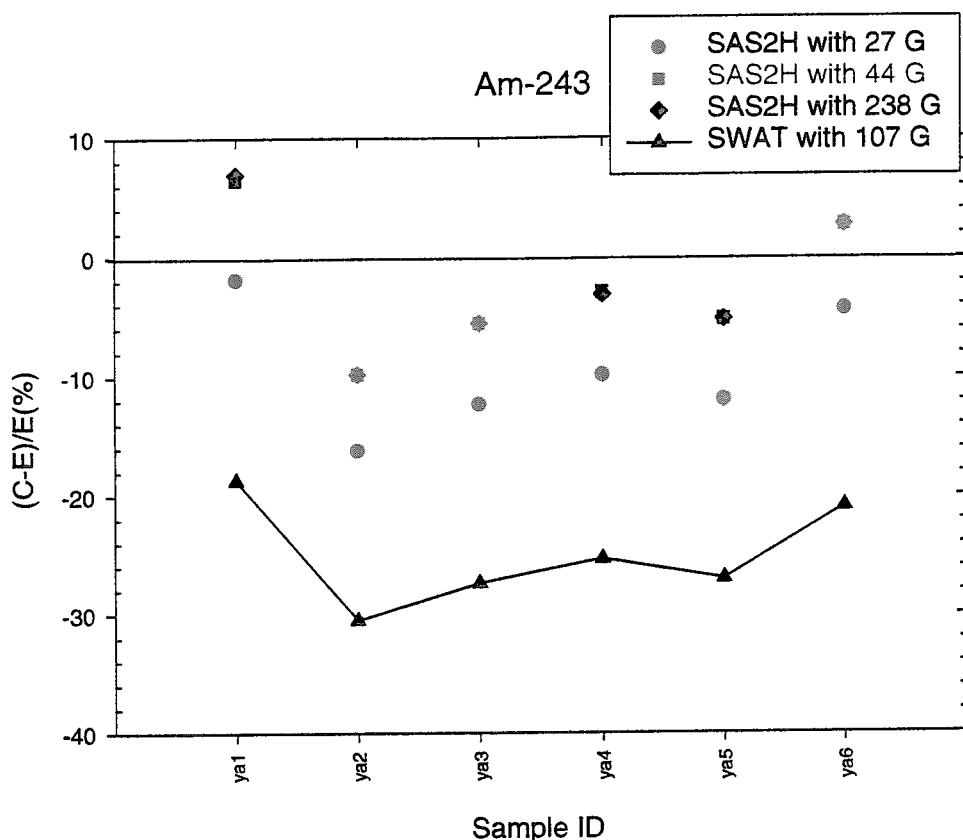


Fig. 6.15. Relative Errors of Am-243 Calculated Compositions.

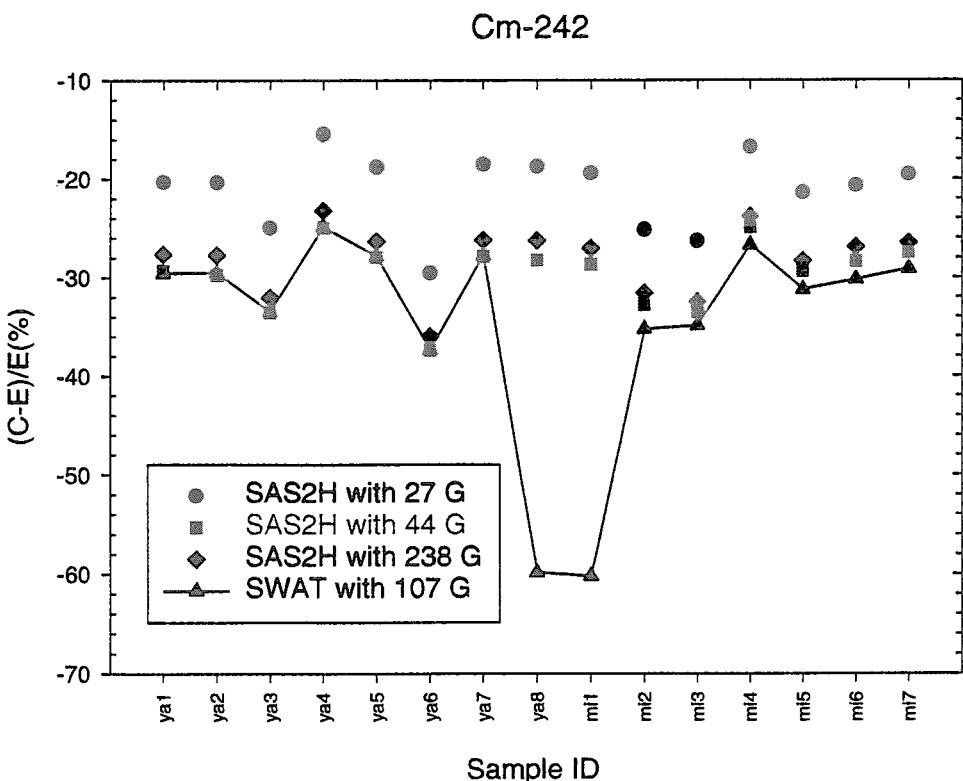


Fig. 6.16. Relative Errors of Cm-242 Calculated Compositions.

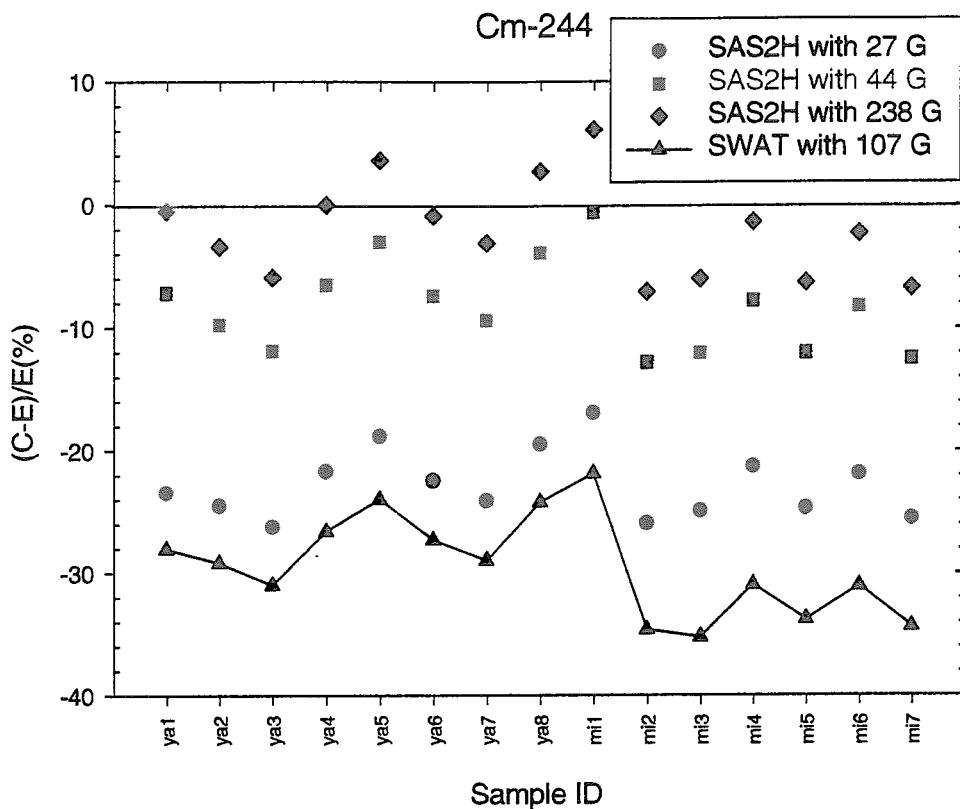


Fig. 6.17. Relative Errors of Cm-244 Calculated Compositions.

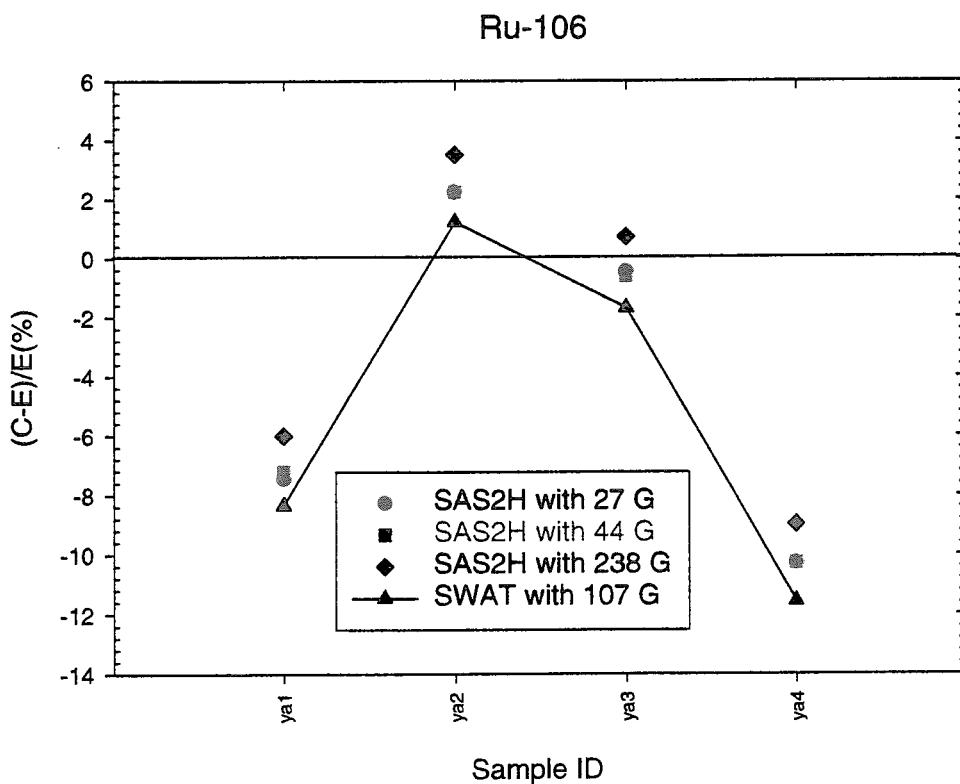


Fig. 6.18. Relative Errors of Ru-106 Calculated Compositions.

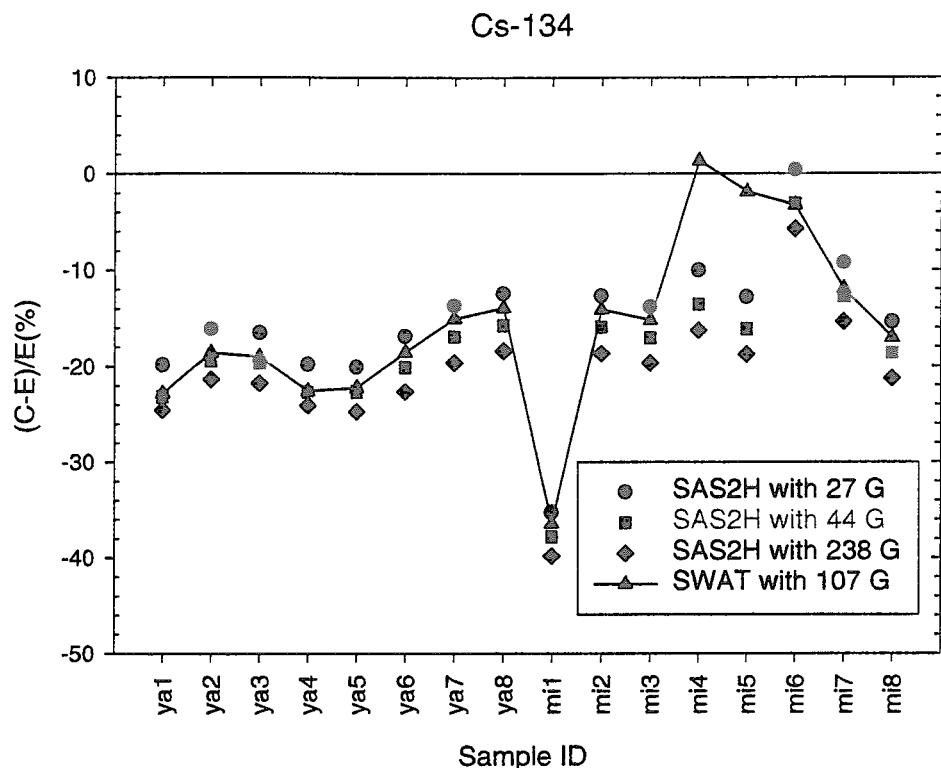


Fig. 6.19. Relative Errors of Cs-134 Calculated Compositions.

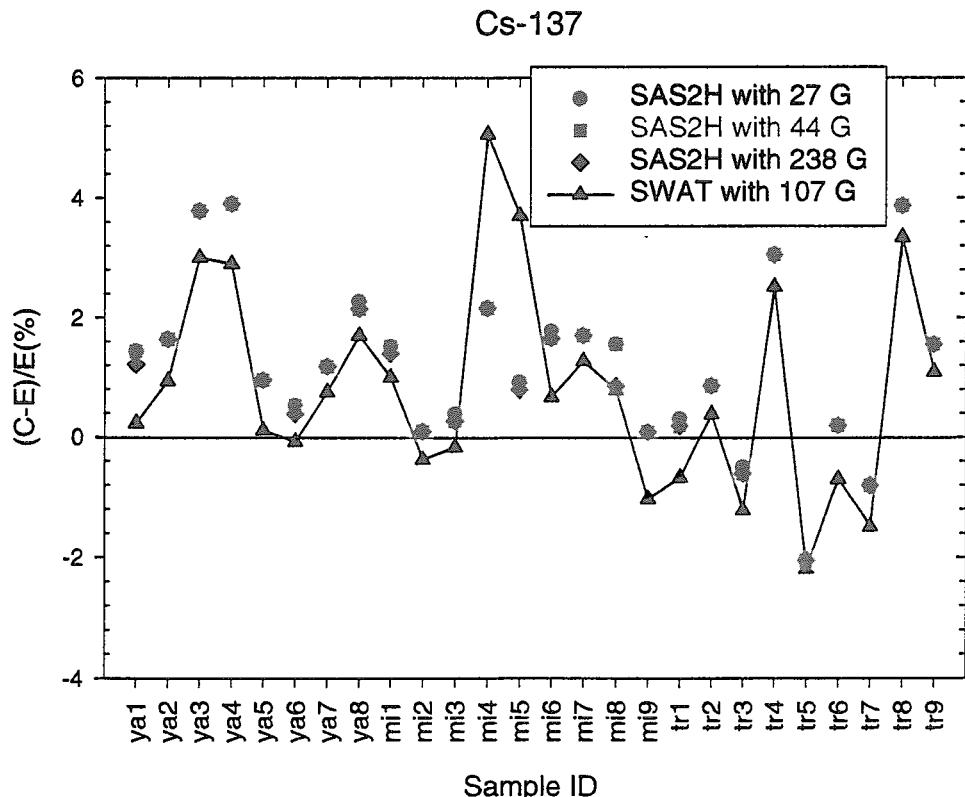


Fig. 6.20. Relative Errors of Cs-137 Calculated Compositions.

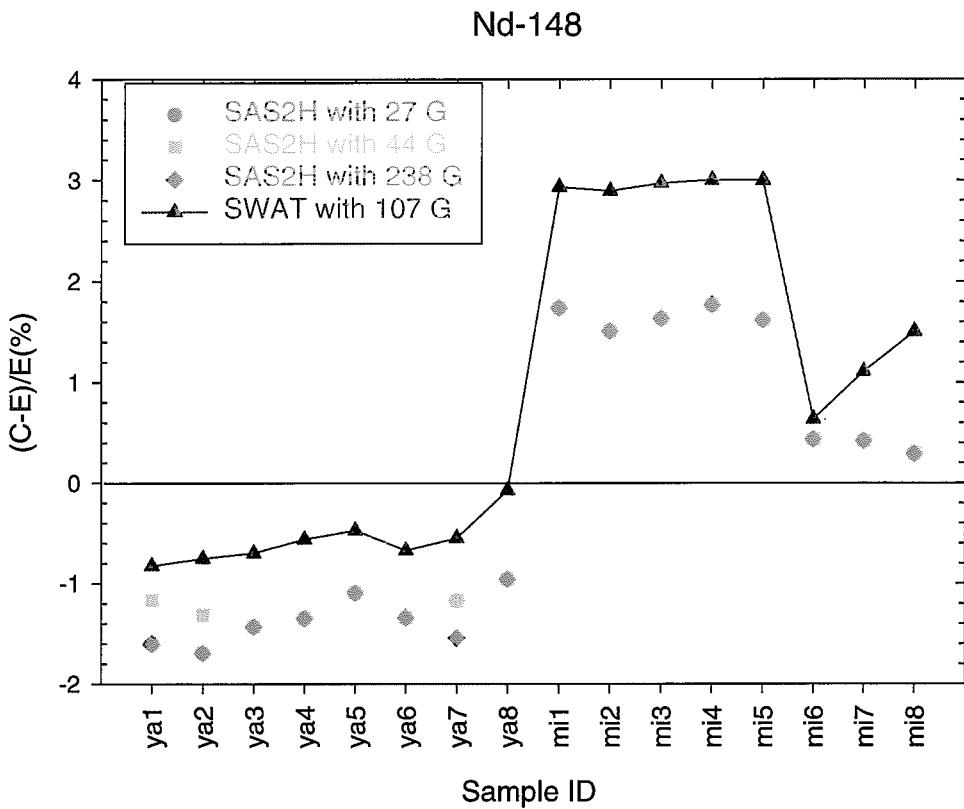


Fig. 6.21. Relative Errors of Nd-148 Calculated Compositions.

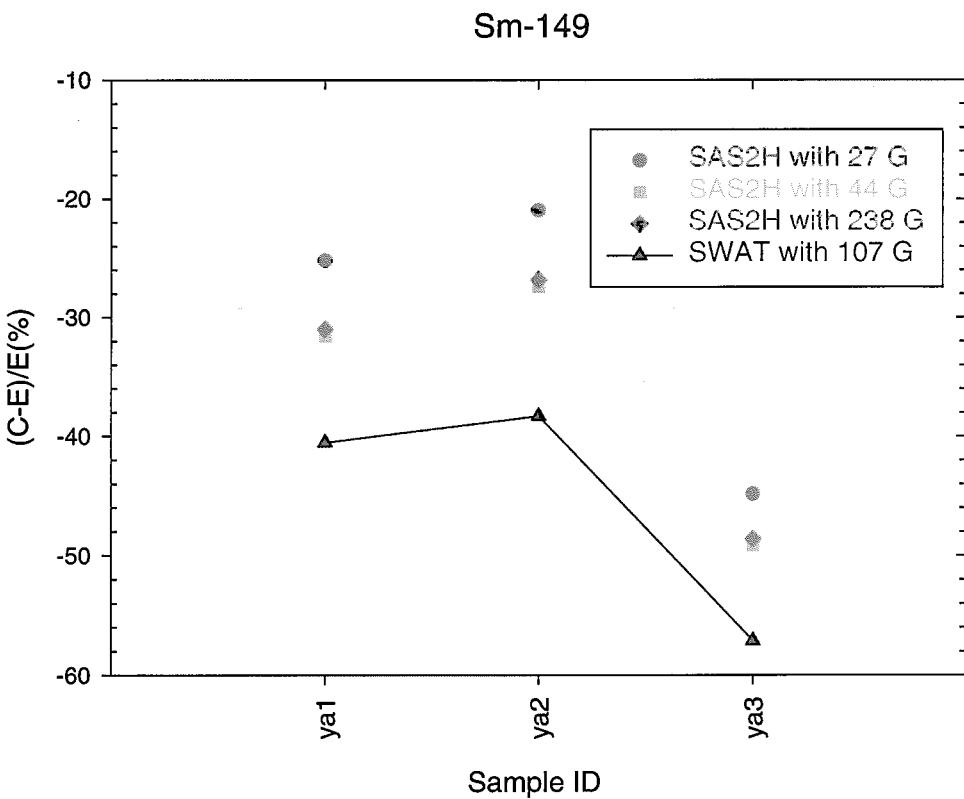


Fig. 6.22. Relative Errors of Sm-149 Calculated Compositions.

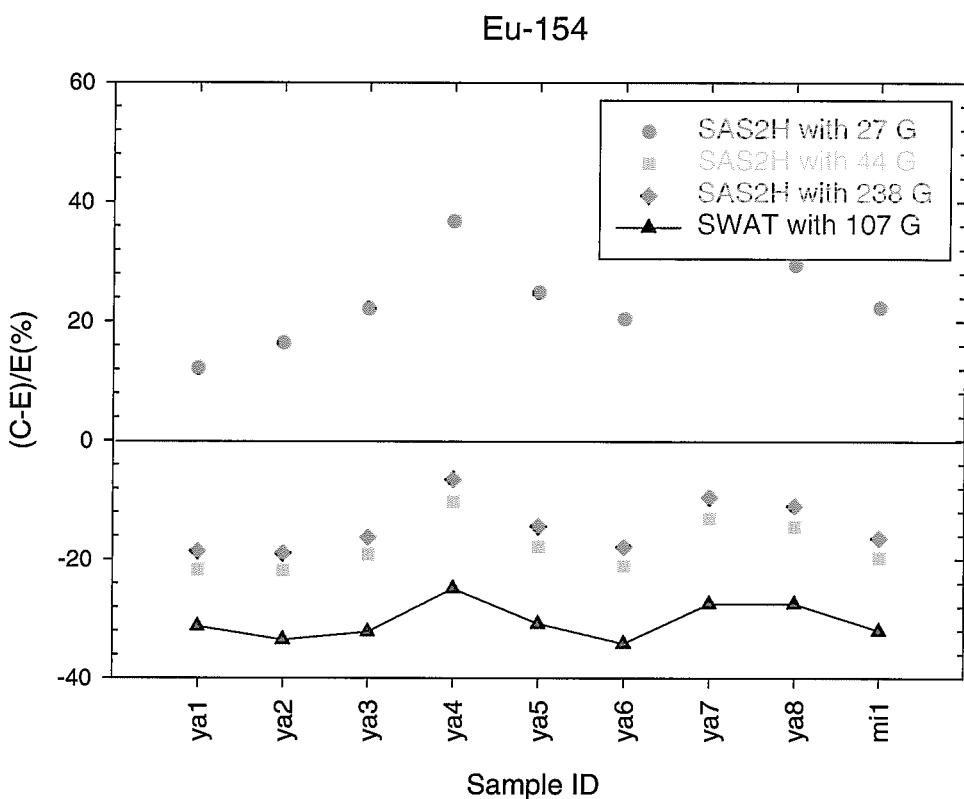
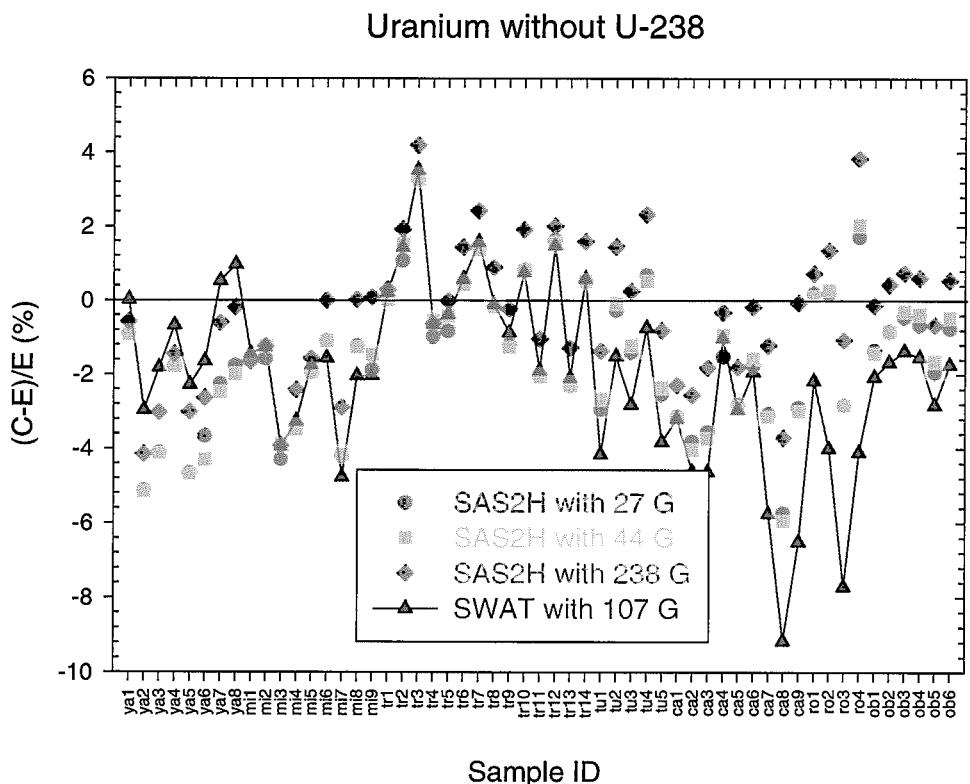


Fig. 6.23. Relative Errors of Eu-154 Calculated Compositions.



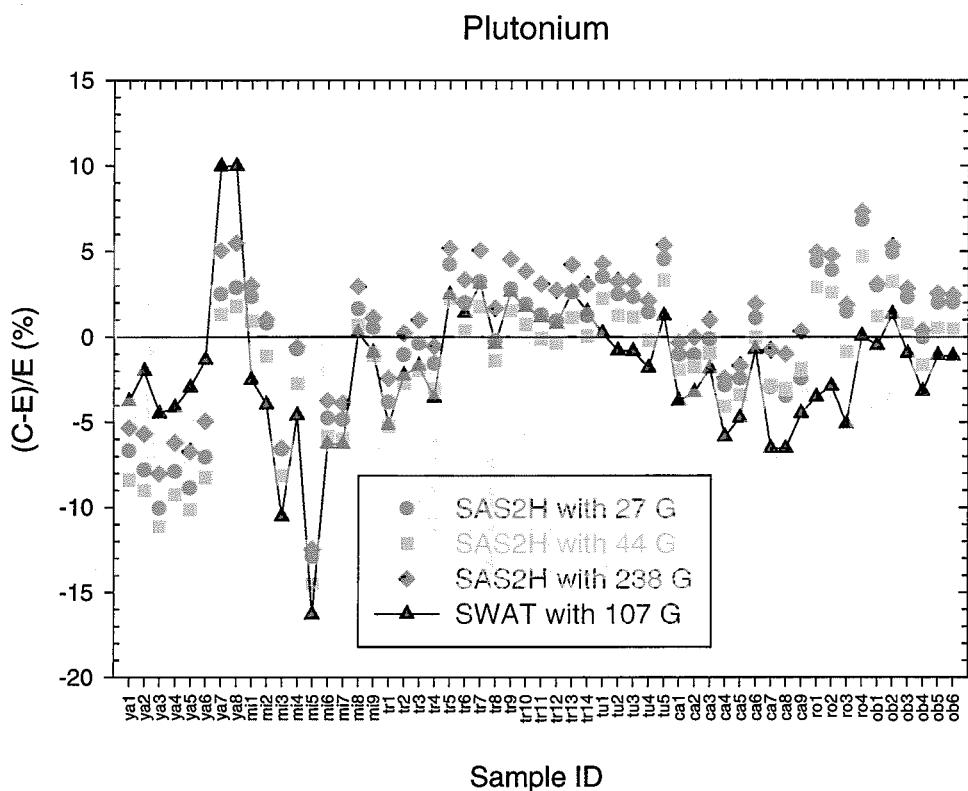


Fig. 6.25. Relative Errors of Plutonium Calculated Compositions.

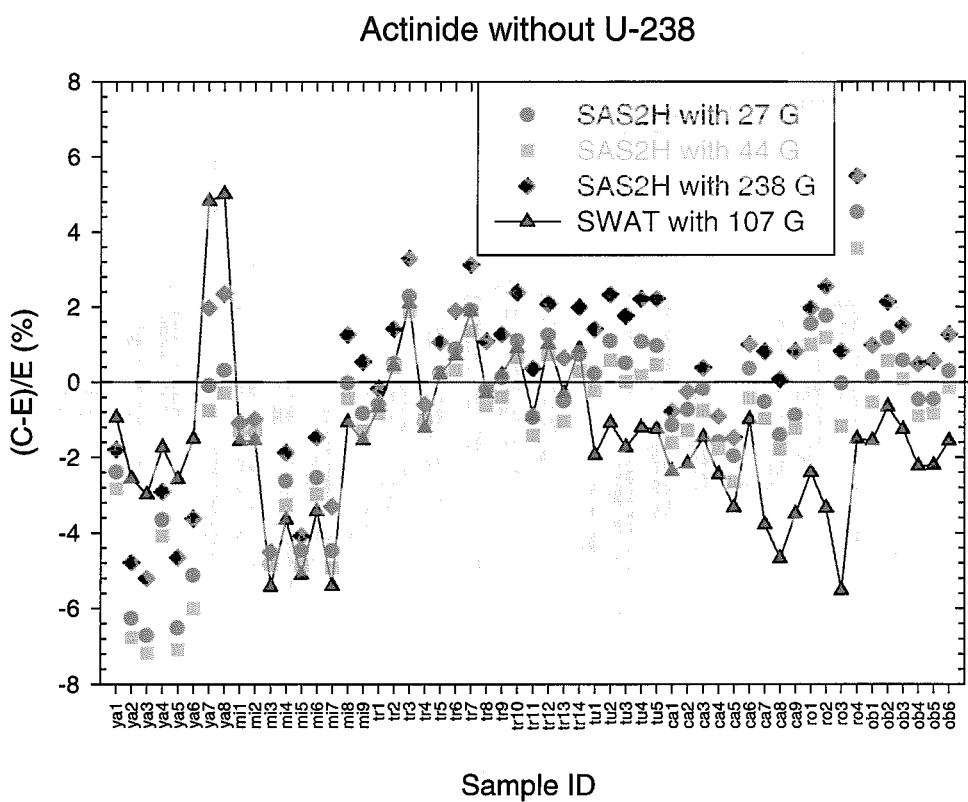


Fig. 6.26. Relative Errors of Actinide Calculated Compositions without U-238.

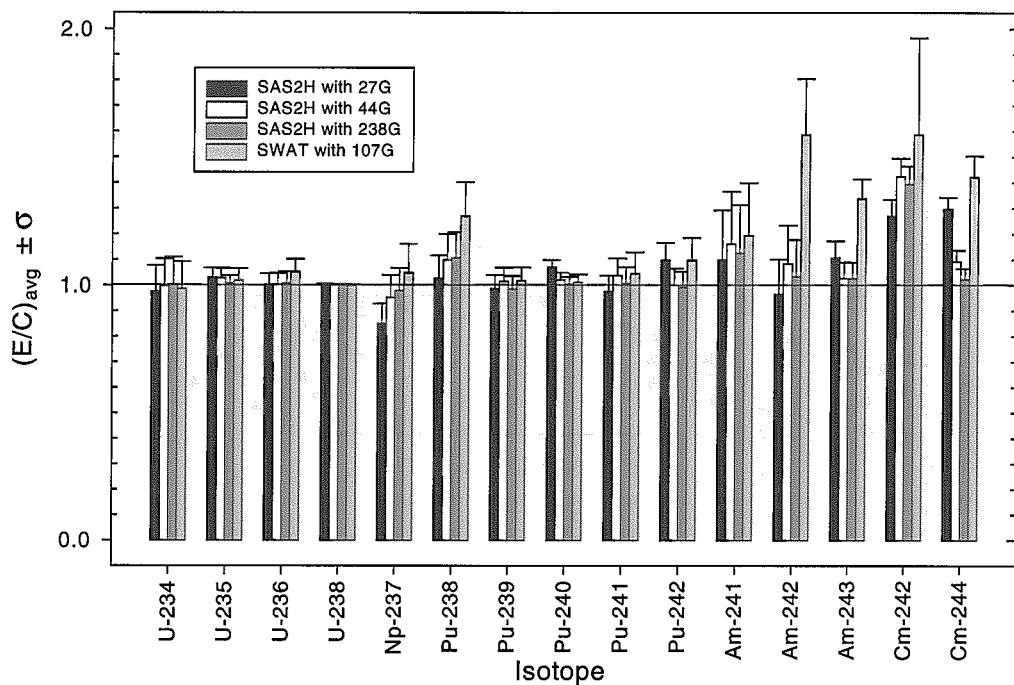


Fig. 6.27. Comparison of the Average Measured-to-Calculated Ratios and Standard Deviations for Actinides.

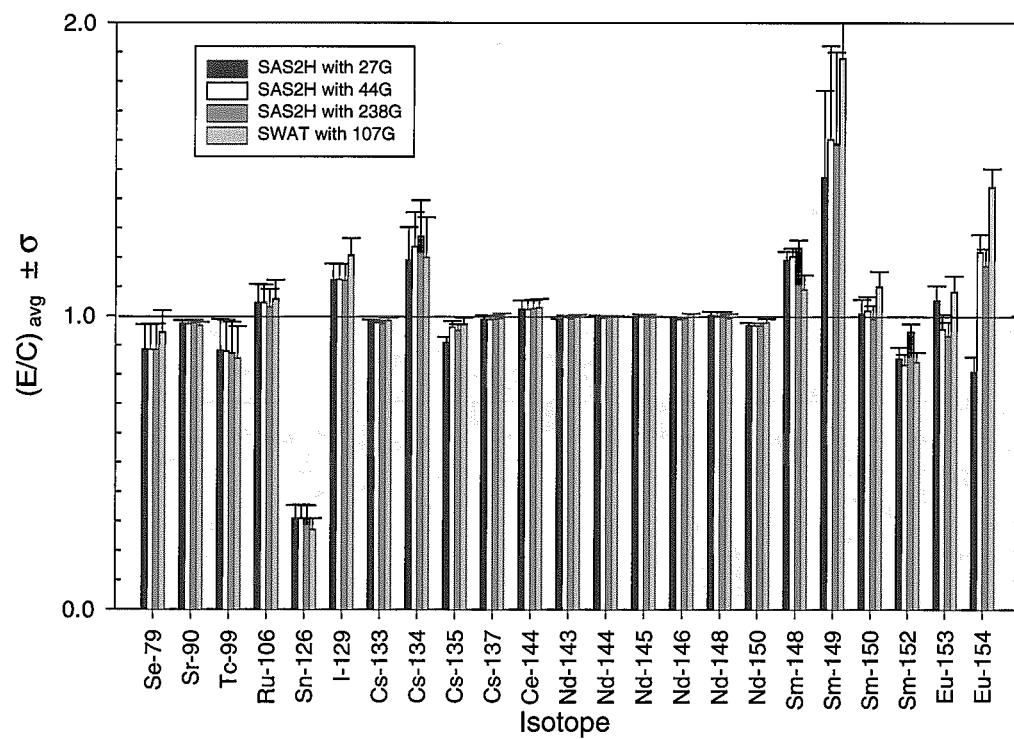


Fig. 6.28. Comparison of the Average Measured-to-Calculated Ratios and Standard Deviations for Fission Products.

7. Correction Factors

7.1. Selection of Samples

The correction factors of PWR spent fuel composition will be determined on the basis of the ratios of four calculated compositions to the experimental composition for 16 and 55 samples. Normality test have been carried out for 38 nuclides using the combined measured-to-calculated ratios. But some actinides didn't pass the normality test because the combined set consisted of 16 and 55 samples which were obtained from several different PWR types of 7 reactors. Therefore, it is necessary that some kinds of selection should be done before correction factors were generated.

A study on sample selection has been carried out to find the condition that the calculated composition ratios of all actinide nuclides can pass the normality test through selection of experimental data. There are a lot of ways to select experimental samples. Among them, the most important factors which affect experimental data, calculation method or the effective one-group cross-section are considered in selection of experimental data in this work. That is, the initial enrichment and/or burnup, axial location of sampling position in the fuel rod, burnup interval and experimental institute are taken into account in the selection. Although various selections have been tried to do changing the ranges of those factors, the sample sets have not been found that the ratios of all actinide nuclides can passed the normality test at a level of significance of $\alpha = 0.05$.

7.2. Determination of Correction Factors

Although further study is needed to get a sample set which can pass the normality test, it is out of scope of this work. More detailed analysis and application of high-level statistical methods are required to get the optimum sample set. In this work temporary correction factors will be generated on the basis of 71 samples which are slightly unsatisfied with normality. The correction factors may be used for an approximate burnup credit criticality analysis such as a preliminary calculation or feasibility study.

The correction factors have been determined at a level of significance of $\alpha = 0.05$ on

the basis of 71 samples of the combined set in which 16 and 55 samples are included, applying tolerance limit method shown in eqs.(4)-(7). The correction factors for 38 isotopes are determined and presented in Table 7.1. As shown in Table 7.1, four kinds of the correction factor for each nuclide are not much different except Pu-238, Am-242, Am-243, Cm-244, Sm-148, Eu-153 and Eu-154.

7.3. Conservative Prediction of Isotopic Composition

As shown in Table 7.1, in the case of Am-241 and Sm-149, all four kinds of the correction factors are determined to be zero because the standard deviations are very large. It means that Am-241 and Sm-149 are to be neglected in the burnup credit criticality calculation. The correction factors for fissile materials, U-235, Pu-239 and Pu-241 are determined to be larger than 1.0 and those for non-fissile materials are determined to be below 1.0. Therefore, the burnup credit criticality analysis will be conservative if k_{eff} is calculated on the basis of the corrected compositions which are obtained from the multiplication of the calculated composition by the correction factor.

Table 7.1. Correction Factors for 38 nuclides

Nuclide	Tolerance Limit Factor	Data#	Correction Factor			
			SAS2H			SWAT
			27 G	44 G	238 G	
U-234	2.292	25	0.7386	0.7548	0.7581	0.7472
U-235	1.987	71	1.1057	1.1047	1.0749	1.1091
U-236	1.987	71	0.9103	0.9116	0.9140	0.9519
U-238	2.005	65	0.9919	0.9918	0.9923	0.9920
Np-237	2.671	13	0.6435	0.7173	0.7485	0.7462
Pu-238	2.060	51	0.7905	0.8404	0.8516	0.9830
Pu-239	1.987	71	1.0901	1.1166	1.0819	1.1104
Pu-240	1.987	71	0.9864	0.9433	0.9274	0.9407
Pu-241	1.987	71	1.1145	1.1858	1.1484	1.1984
Pu-242	1.999	67	0.8986	0.8166	0.8113	0.8882
Am-241	2.371	21	0.0000	0.0000	0.0000	0.0000
Am-242	3.187	8	0.5196	0.5946	0.5793	0.9371
Am-243	3.187	8	0.5205	0.4822	0.4727	0.7937
Cm-242	2.220	30	0.4265	0.4974	0.4863	0.4665
Cm-244	2.208	31	0.7302	0.6135	0.5742	0.8561
Se-79	3.031	9	0.6218	0.6204	0.6197	0.7174
Sr-90	3.031	9	0.9387	0.9371	0.9406	0.9308
Tc-99	2.671	13	0.5931	0.5919	0.5820	0.5623
Ru-106	5.144	4	0.7161	0.7200	0.7140	0.7180
Sn-126	3.708	6	0.1405	0.1396	0.1392	0.1279
I-129	7.656	3	0.6838	0.7162	0.6845	0.7592
Cs-133	7.656	3	0.9399	0.9177	0.9027	0.9092
Cs-134	2.275	26	0.7727	0.8013	0.8238	0.8056
Cs-135	3.031	9	0.8513	0.9019	0.8883	0.9036
Cs-137	2.158	36	0.9318	0.9317	0.9317	0.9394
Ce-144	5.144	4	0.8669	0.8669	0.8773	0.8759
Nd-143	7.656	3	0.9591	0.9719	0.9576	0.9759
Nd-144	7.656	3	0.9869	0.9690	0.9869	0.9863
Nd-145	7.656	3	0.9845	0.9774	0.9807	0.9828
Nd-146	7.656	3	0.9884	0.9797	0.9873	0.9955
Nd-148	2.524	16	0.9661	0.9671	0.9658	0.9519
Nd-150	7.656	3	0.8992	0.8992	0.8992	0.8855
Sm-148	7.656	3	0.9619	0.9862	1.0248	0.7183
Sm-149	7.656	3	0.0000	0.0000	0.0000	0.0000
Sm-150	7.656	3	0.6426	0.6403	0.6436	0.6965
Sm-152	7.656	3	0.5571	0.5620	0.7353	0.6010
Eu-153	7.656	3	0.6654	0.5664	0.5699	0.6714
Eu-154	2.423	19	0.3806	0.7385	0.7168	1.0064

8. Conclusions

In ideal situation, the burnup code predicts precisely the measurement. However, the reality is different. The code usually overestimates or underestimates the nuclide concentrations obtained by measurement. For a conservative estimate in burnup credit criticality application a correction factor is introduced for each nuclide based on the comparison of calculation results with measurements.

Four kinds of methods, i.e., SCALE4.4/SAS2H with 27, 44 and 238 group cross-section libraries and SWAT with 107 group library, were applied and the results were compared on the basis of 26 Obrigheim spent fuel samples and 55 spent fuel samples of 7 reactors. For convenience, the ratio of the measured to calculated values was used as a parameter. When the ratio is less than unity, the calculation overestimates the measurement, and the ratio becomes closer to unity, they have a better agreement. For many important nuclides for burnup credit criticality safety evaluation, the four methods applied in this study showed good coincidence with measurements in general. More precise observations showed, however: (1) Less unity ratios were found for Pu-239 and -241 for selected 16 samples out of the 26 samples from the Obrigheim reactor (10 samples were deselected because their burnups were measured with Cs-137 non-destructive method, less reliable than Nd-148 method the rest 16 samples were measured with); (2) Larger than unity ratios were found for Am-241 and Cm-242 for both the 16 and 55 samples; (3) Larger than unity ratios were found for Sm-149 for the 55 samples; (4) SWAT was generally accompanied by larger ratios than those of SAS2H with some exceptions.

Based on the measured-to-calculated ratios for 71 samples of a combined set in which 16 selected samples and 55 samples were included, the correction factors that should be multiplied to the calculated isotopic compositions were determined for a conservative estimate of the neutron multiplication factor of a system containing PWR spent fuel, taking burnup credit into account. However, some nuclides did not pass the normality test. Although, various sample selections were tried, the sample sets were not found that the ratios of all nuclides passed the normality test at a level of significance of $\alpha=0.05$.

It is necessary to investigate deeply the main reason of the big differences between calculations and experiments in several cases of 26 Obrigheim samples. In the case of the combined 71 samples, further study is required to find the set which pass normality test. The calculation results of SAS2H and SWAT are expected to be improved through modeling optimization.

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Appendix : Input and Output Listings

- A.1 SAS2H Input for One of 26 Obrigheim Samples
- A.2 SWAT Input for One of 26 Obrigheim Samples
- A.3 SWAT Inputs for 55 Samples
- A.4 Calculation Results for 26 Obrigheim Samples
- A.5 Calculation Results for 55 Samples

A.1. SAS2H Input for Sample Or1 of 26 Obriegheim samples, 44 group,
 =sas2h parm='halt03,skipshipdata'
 'id arr frd burnup enrich pitch actlgth zposit h2oden gdia1 gdia2 dtemp voi
 ob1 18 308 21.17 3.000 1.4300 295.60 0.00 0.7283 0.6413 0.6845 300. 0.
 44group latticecell
 uo2 1 den=10.4215 1 900.0000
 92234 0.0055
 92235 3.0000
 92238 96.9945
 Np-237 1 0 1-20 900.0000 end
 Pu-238 1 0 1-20 900.0000 end
 Pu-239 1 0 1-20 900.0000 end
 Pu-240 1 0 1-20 900.0000 end
 Pu-241 1 0 1-20 900.0000 end
 Pu-242 1 0 1-20 900.0000 end
 Am-241 1 0 1-20 900.0000 end
 Am-243 1 0 1-20 900.0000 end
 Cm-244 1 0 1-20 900.0000 end
 Gd-154 1 0 1-20 900.0000 end
 Gd-155 1 0 1-20 900.0000 end
 Gd-156 1 0 1-20 900.0000 end
 Gd-157 1 0 1-20 900.0000 end
 Gd-158 1 0 1-20 900.0000 end
 Gd-160 1 0 1-20 900.0000 end
 Xe-135 1 0 1-20 900.0000 end
 Nd-143 1 0 1-20 900.0000 end
 Rh-103 1 0 1-20 900.0000 end
 Xe-131 1 0 1-20 900.0000 end
 Cs-133 1 0 1-20 900.0000 end
 Sm-149 1 0 1-20 900.0000 end
 Tc-99 1 0 1-20 900.0000 end
 Sm-152 1 0 1-20 900.0000 end
 Sm-151 1 0 1-20 900.0000 end
 Pm-147 1 0 1-20 900.0000 end
 Eu-153 1 0 1-20 900.0000 end
 Nd-145 1 0 1-20 900.0000 end
 Eu-155 1 0 1-20 900.0000 end
 Eu-154 1 0 1-20 900.0000 end
 Sm-150 1 0 1-20 900.0000 end
 Mo-95 1 0 1-20 900.0000 end
 Ag-109 1 0 1-20 900.0000 end
 Ru-101 1 0 1-20 900.0000 end
 Cs-134 1 0 1-20 900.0000 end
 Pd-105 1 0 1-20 900.0000 end
 Pm-148 1 0 1-20 900.0000 end
 Rh-105 1 0 1-20 900.0000 end
 Pr-141 1 0 1-20 900.0000 end
 Kr-83 1 0 1-20 900.0000 end
 Pd-108 1 0 1-20 900.0000 end
 Sm-147 1 0 1-20 900.0000 end
 Pd-107 1 0 1-20 900.0000 end
 Mo-97 1 0 1-20 900.0000 end
 Cd-113 1 0 1-20 900.0000 end
 Cs-135 1 0 1-20 900.0000 end
 Mo-98 1 0 1-20 900.0000 end
 Xe-133 1 0 1-20 900.0000 end
 In-115 1 0 1-20 900.0000 end
 Pr-143 1 0 1-20 900.0000 end
 Eu-156 1 0 1-20 900.0000 end
 Ru-103 1 0 1-20 900.0000 end
 Sm-148 1 0 1-20 900.0000 end
 Nd-147 1 0 1-20 900.0000 end
 Pm-149 1 0 1-20 900.0000 end
 O-16 1 0 1-20 900.0000 end
 zircalloy 2 1 600.0000 end
 h2o 3 den= 0.7283 1 556.3400 end
 arbm-bormod 0.7283 1 1 0 0 5000 100 3 0.50E-03 556.3400 end
 end comp
 squarepitch 1.43000 0.90400 1 3 1.07600 2 0.93180 0 end
 fuellnght= 550.654 npin/assm= 308 ncycles= 3
 nlib/cyc= 1 printlevel= 10 lightel= 0
 inplevel= 2 numztotal= 5
 3 0.6413 2 0.6845 3 0.8068 500 3.6306 3 3.6446 end
 power= 18.674 burn= 258.000 down= 370.000 end
 power= 30.954 burn= 283.000 down= 23.000 bfrac=2.000 end
 power= 33.153 burn= 229.000 bfrac=1.000 end
 end

A.2. SWAT Input for Sample Or1 of 26 Obrigheim samples

```
===== PDS FILE ALOCATION ======
FASTP : pfast
THERMP : pthml
FASTU : fastu
THERMU : thermalu
MACWRK : macrowrk
FLUX : flux
MACRO : macro
MCROSSP: pmcrs
MICREF : micref
UMCROS : umcros
===== for libmak =====
usacti ./home5/codes/swat9906/xslib/acti.j32.v2.1
usfp ./home5/codes/swat9906/xslib/fp.j32.v2.4
ori2ori:/home5/codes/swat9906/ori2origlib/decaydat.fp-j3.v7
===== for origen2 =====
photo ./home5/codes/swat9906/ori2origlib/photodat
***** global data lists *****
Template of SWAT Input Data for The Obrigheim Reactor By SHIN, Hee Sung
ob1 18 308 21.170 3.0000 1.4300 295.60 15.00 0.7283 0.9318 0.6413 0.6845
1 1 1 0 0 0 0 1 1 1 / Library Control
1 1 1 1 2 1 4 3 -2 1 0 0 0 0 2 0 1 0 0 0 / SRAC General Control
1.0000E-25
63 44 1 /fast thermal letherry
3 3 3 3 3 0 3 0 0 0 0 0 8 15 0 0 30 0 1 /COL.PROB.CONT
1 2 3
0.00000 0.45200 0.53800 0.83806
1
3
67 1 0 0 0 4 4(0) 1.0 0.904 0.0 10.42150 3.000 0.0 4(0.0) / UO2 (3.000wt%)
922340 2 1 0 0 1 2 / U -234
922350 2 1 0 0 1 2 / U -235
922360 2 1 0 0 1 2 / U -236
922380 2 1 0 0 1 2 / U -238
932370 2 1 0 0 1 0
942380 2 1 0 0 1 0
942390 2 1 0 0 1 0
942400 2 1 0 0 1 0
942410 2 1 0 0 1 0
942420 2 1 0 0 1 0
952410 2 1 0 0 1 0
952421 2 1 3 0 1 0
952420 2 1 2 0 1 0
952430 2 1 0 0 1 0
962420 2 1 0 0 1 0
962430 2 1 0 0 1 0
962440 2 1 0 0 1 0
962450 2 1 0 0 1 0
962460 2 1 0 0 1 0
641520 2 1 0 0 1 0
641540 2 1 0 0 1 0
641550 2 1 0 0 1 0
641560 2 1 0 0 1 0
641570 2 1 0 0 1 0
641580 2 1 0 0 1 0
641600 2 1 0 0 1 0
541350 2 1 0 0 1 0
601430 2 1 0 0 1 0
451030 2 1 0 0 1 0
541310 2 1 0 0 1 0
551330 2 1 0 0 1 0
621490 2 1 0 0 1 0
430990 2 1 0 0 1 0
621520 2 1 0 0 1 0
621510 2 1 0 0 1 0
611470 2 1 0 0 1 0
631530 2 1 0 0 1 0
601450 2 1 0 0 1 0
631550 2 1 0 0 1 0
631540 2 1 0 0 1 0
621500 2 1 0 0 1 0
420950 2 1 0 0 1 0
471090 2 1 0 0 1 0
611481 2 1 3 0 1 0
441010 2 1 0 0 1 0
551340 2 1 0 0 1 0
```

461050 2 1 0 0 1 0
 611480 2 1 2 0 1 0
 451050 2 1 0 0 1 0
 591410 2 1 0 0 1 0
 360830 2 1 0 0 1 0
 461080 2 1 0 0 1 0
 621470 2 1 0 0 1 0
 461070 2 1 0 0 1 0
 420970 2 1 0 0 1 0
 481130 2 1 0 0 1 0
 551350 2 1 0 0 1 0
 420980 2 1 0 0 1 0
 541330 2 1 0 0 1 0
 491150 2 1 0 0 1 0
 591430 2 1 0 0 1 0
 631560 2 1 0 0 1 0
 441030 2 1 0 0 1 0
 621480 2 1 0 0 1 0
 601470 2 1 0 0 1 0
 611490 2 1 0 0 1 0
 80160 0 0 0 0 0 1
 922340 55.00
 922350 30000.00
 922360 0.00
 922380 969945.00
 4.64956E-02 / O-16 constant density
 3 9(0) 0.0 0.31651 8(0.0)
 400000 2 1 1 0 0 1 / Zr
 260000 2 1 1 0 0 1 / Fe
 240000 2 1 1 0 0 1 / Cr
 4.2982E-02 1.4838E-04 7.5891E-05 / Zr,Fe,Cr
 4 0 1 7(0) 0.0 0.94891 8(0.0)
 10010 2 1 0 9 0 1 / H-1
 80160 2 1 0 0 0 1 / O-16
 50100 2 1 0 0 0 1 / B-10
 50110 2 1 0 0 0 1 / B-11
 4(1.0E-2) /
 1 0
 1
 38 12
 12(2) 1 12(2) 1 12(2)
 3 4 / 1
 3 4 / 2
 3 4 / 3
 3 4 / 4
 3 4 / 5
 3 4 / 6
 3 4 / 7
 3 4 / 8
 3 4 / 9
 3 4 / 10
 3 4 / 11
 3 4 / 12
 4 / 13
 3 4 / 14
 3 4 / 15
 3 4 / 16
 3 4 / 17
 3 4 / 18
 3 4 / 19
 3 4 / 20
 3 4 / 21
 3 4 / 22
 3 4 / 23
 3 4 / 24
 3 4 / 25
 4 / 26
 3 4 / 27
 3 4 / 28
 3 4 / 29
 3 4 / 30
 3 4 / 31
 3 4 / 32
 3 4 / 33
 3 4 / 34
 3 4 / 35
 3 4 / 36
 3 4 / 37
 3 4 / 38

12(1)	0	12(1)	0	12(1)
21.500	18.674 /	1	21.500=	258.000/ 12.000
21.500	18.674 /	2	18.674=	6600.0/ 258.000* 21.170/ 29.000
21.500	18.674 /	3		
21.500	18.674 /	4		
21.500	18.674 /	5		
21.500	18.674 /	6		
21.500	18.674 /	7		
21.500	18.674 /	8		
21.500	18.674 /	9		
21.500	18.674 /	10		
21.500	18.674 /	11		
21.500	18.674 /	12		
370.000	/	13		
23.583	30.954 /	14	23.583=	283.000/ 12.000
23.583	30.954 /	15	30.954=	12000.0/ 283.000* 21.170/ 29.000
23.583	30.954 /	16		
23.583	30.954 /	17		
23.583	30.954 /	18		
23.583	30.954 /	19		
23.583	30.954 /	20		
23.583	30.954 /	21		
23.583	30.954 /	22		
23.583	30.954 /	23		
23.583	30.954 /	24		
23.583	30.954 /	25		
23.000	/	26		
19.083	33.153 /	27	19.083=	229.000/ 12.000
19.083	33.153 /	28	33.153=	10400.0/ 229.000* 21.170/ 29.000
19.083	33.153 /	29		
19.083	33.153 /	30		
19.083	33.153 /	31		
19.083	33.153 /	32		
19.083	33.153 /	33		
19.083	33.153 /	34		
19.083	33.153 /	35		
19.083	33.153 /	36		
19.083	33.153 /	37		
19.083	33.153 /	38		
900.000	600.000	556.340 /	1	
900.000	600.000	556.340 /	2	
900.000	600.000	556.340 /	3	
900.000	600.000	556.340 /	4	
900.000	600.000	556.340 /	5	
900.000	600.000	556.340 /	6	
900.000	600.000	556.340 /	7	
900.000	600.000	556.340 /	8	
900.000	600.000	556.340 /	9	
900.000	600.000	556.340 /	10	
900.000	600.000	556.340 /	11	
900.000	600.000	556.340 /	12	
3(300.0)	/	13		
900.000	600.000	556.340 /	14	
900.000	600.000	556.340 /	15	
900.000	600.000	556.340 /	16	
900.000	600.000	556.340 /	17	
900.000	600.000	556.340 /	18	
900.000	600.000	556.340 /	19	
900.000	600.000	556.340 /	20	
900.000	600.000	556.340 /	21	
900.000	600.000	556.340 /	22	
900.000	600.000	556.340 /	23	
900.000	600.000	556.340 /	24	
900.000	600.000	556.340 /	25	
3(300.0)	/	26		
900.000	600.000	556.340 /	27	
900.000	600.000	556.340 /	28	
900.000	600.000	556.340 /	29	
900.000	600.000	556.340 /	30	
900.000	600.000	556.340 /	31	
900.000	600.000	556.340 /	32	
900.000	600.000	556.340 /	33	
900.000	600.000	556.340 /	34	
900.000	600.000	556.340 /	35	
900.000	600.000	556.340 /	36	
900.000	600.000	556.340 /	37	
900.000	600.000	556.340 /	38	
1 0 0 0 0 0 14(0.0)	/	1	result control	
1 0 0 0 0 0 14(0.0)	/	2	result control	

```

1 0 0 0 0 0 0 14( 0.0) / 3 result control
1 0 0 0 0 0 0 14( 0.0) / 4 result control
1 0 0 0 0 0 0 14( 0.0) / 5 result control
1 0 0 0 0 0 0 14( 0.0) / 6 result control
1 0 0 0 0 0 0 14( 0.0) / 7 result control
1 0 0 0 0 0 0 14( 0.0) / 8 result control
1 0 0 0 0 0 0 14( 0.0) / 9 result control
1 0 0 0 0 0 0 14( 0.0) / 10 result control
1 0 0 0 0 0 0 14( 0.0) / 11 result control
1 0 0 0 0 0 0 14( 0.0) / 12 result control
1 0 0 0 0 0 0 14( 0.0) / 13 result control
1 0 0 0 0 0 0 14( 0.0) / 14 result control
1 0 0 0 0 0 0 14( 0.0) / 15 result control
1 0 0 0 0 0 0 14( 0.0) / 16 result control
1 0 0 0 0 0 0 14( 0.0) / 17 result control
1 0 0 0 0 0 0 14( 0.0) / 18 result control
1 0 0 0 0 0 0 14( 0.0) / 19 result control
1 0 0 0 0 0 0 14( 0.0) / 20 result control
1 0 0 0 0 0 0 14( 0.0) / 21 result control
1 0 0 0 0 0 0 14( 0.0) / 22 result control
1 0 0 0 0 0 0 14( 0.0) / 23 result control
1 0 0 0 0 0 0 14( 0.0) / 24 result control
1 0 0 0 0 0 0 14( 0.0) / 25 result control
1 0 0 0 0 0 0 14( 0.0) / 26 result control
1 0 0 0 0 0 0 14( 0.0) / 27 result control
1 0 0 0 0 0 0 14( 0.0) / 28 result control
1 0 0 0 0 0 0 14( 0.0) / 29 result control
1 0 0 0 0 0 0 14( 0.0) / 30 result control
1 0 0 0 0 0 0 14( 0.0) / 31 result control
1 0 0 0 0 0 0 14( 0.0) / 32 result control
1 0 0 0 0 0 0 14( 0.0) / 33 result control
1 0 0 0 0 0 0 14( 0.0) / 34 result control
1 0 0 0 0 0 0 14( 0.0) / 35 result control
1 0 0 0 0 0 0 14( 0.0) / 36 result control
1 0 0 0 0 0 0 14( 0.0) / 37 result control
1 0 0 0 0 0 0 14( 0.0) / 38 result control
0 / PWR
38( 0.000) / void ratio (%)
12( -500.0) 1(-1000.0) 12( -500.0) 1(-1000.0) 12( -500.0)
0 /xs val.
0 /branching
0 /weight factor

```

A.3.1. SWAT input for Sample NO 1 of Yankee Rowe.

```
===== PDS FILE ALOCATION =====
FASTP : pfast
THERMP : pthml
FASTU : fastu
THERMU : thermalu
MACWRK : macrowrk
FLUX : flux
MACRO : macro
MCROSSP: pmcrs
MICREF : micref
UMCROS : umcros
===== for libmak =====
usacti ./home5/codes/swat9906/xslib/acti.j32.v2.1
usfp ./home5/codes/swat9906/xslib/fp.j32.v2.4
ori2ori:/home5/codes/swat9906/origlib/decaydat.fp-j3.v7
===== for origen2 =====
photo ./home5/codes/swat9906/origlib/photodat
***** global data lists *****
Template of SWAT Input Data for The Obrigheim Reactor By SHIN, Hee Sung
yal 18 305 15.950 3.4000 1.0719 230.05 220.22 0.7702 0.7569 0.3785 0.4318
1 1 1 0 0 0 0 1 1 1 / Library Control
1 1 1 1 2 1 4 3 -2 1 0 0 0 0 2 0 1 0 0 0 / SRAC General Control
1.0000E-25
63 44 1 /fast thermal letherry
3 3 3 3 3 0 3 0 0 0 0 0 8 15 0 0 30 0 1 /COL.PROB.CONT
1 2 3
0.00000 0.37084 0.43180 0.62113
1
3
67 1 0 0 0 4 4(0) 1.0 0.742 0.0 10.18000 3.400 0.0 4(0.0) / UO2 (3.400wt%)
922340 2 1 0 0 1 2 / U -234
922350 2 1 0 0 1 2 / U -235
922360 2 1 0 0 1 2 / U -236
922380 2 1 0 0 1 2 / U -238
932370 2 1 0 0 1 0
942380 2 1 0 0 1 0
942390 2 1 0 0 1 0
942400 2 1 0 0 1 0
942410 2 1 0 0 1 0
942420 2 1 0 0 1 0
952410 2 1 0 0 1 0
952421 2 1 3 0 1 0
952420 2 1 2 0 1 0
952430 2 1 0 0 1 0
962420 2 1 0 0 1 0
962430 2 1 0 0 1 0
962440 2 1 0 0 1 0
962450 2 1 0 0 1 0
962460 2 1 0 0 1 0
641520 2 1 0 0 1 0
641540 2 1 0 0 1 0
641550 2 1 0 0 1 0
641560 2 1 0 0 1 0
641570 2 1 0 0 1 0
641580 2 1 0 0 1 0
641600 2 1 0 0 1 0
541350 2 1 0 0 1 0
601430 2 1 0 0 1 0
451030 2 1 0 0 1 0
541310 2 1 0 0 1 0
551330 2 1 0 0 1 0
621490 2 1 0 0 1 0
430990 2 1 0 0 1 0
621520 2 1 0 0 1 0
621510 2 1 0 0 1 0
611470 2 1 0 0 1 0
631530 2 1 0 0 1 0
601450 2 1 0 0 1 0
631550 2 1 0 0 1 0
631540 2 1 0 0 1 0
621500 2 1 0 0 1 0
420950 2 1 0 0 1 0
471090 2 1 0 0 1 0
611481 2 1 3 0 1 0
441010 2 1 0 0 1 0
551340 2 1 0 0 1 0
461050 2 1 0 0 1 0
```

611480 2 1 2 0 1 0
 451050 2 1 0 0 1 0
 591410 2 1 0 0 1 0
 360830 2 1 0 0 1 0
 461080 2 1 0 0 1 0
 621470 2 1 0 0 1 0
 461070 2 1 0 0 1 0
 420970 2 1 0 0 1 0
 481130 2 1 0 0 1 0
 551350 2 1 0 0 1 0
 420980 2 1 0 0 1 0
 541330 2 1 0 0 1 0
 491150 2 1 0 0 1 0
 591430 2 1 0 0 1 0
 631560 2 1 0 0 1 0
 441030 2 1 0 0 1 0
 621480 2 1 0 0 1 0
 601470 2 1 0 0 1 0
 611490 2 1 0 0 1 0
 80160 0 0 0 0 0 1
 922340 200.00
 922350 34000.00
 922360 200.00
 922380 965600.00
 4.64956E-02 / O-16 constant density
 3 9(0) 0.0 0.22663 8(0.0)
 260000 2 1 1 0 0 1 / Fe
 240000 2 1 1 0 0 1 / Cr
 280000 2 1 1 0 0 1 / Ni
 5.7872E-2 1.7408E-2 8.1116E-3 / Fe, Cr, Ni
 4 0 1 7(0) 0.0 0.64190 8(0.0)
 10010 2 1 0 9 0 1 / H-1
 80160 2 1 0 0 0 1 / O-16
 50100 2 1 0 0 0 1 / B-10
 50110 2 1 0 0 0 1 / B-11
 4(1.0E-2) /
 1 0
 1
 39 12
 12(2) 1 12(2) 1 12(2) 1
 3 4 / 1
 3 4 / 2
 3 4 / 3
 3 4 / 4
 3 4 / 5
 3 4 / 6
 3 4 / 7
 3 4 / 8
 3 4 / 9
 3 4 / 10
 3 4 / 11
 3 4 / 12
 4 / 13
 3 4 / 14
 3 4 / 15
 3 4 / 16
 3 4 / 17
 3 4 / 18
 3 4 / 19
 3 4 / 20
 3 4 / 21
 3 4 / 22
 3 4 / 23
 3 4 / 24
 3 4 / 25
 4 / 26
 3 4 / 27
 3 4 / 28
 3 4 / 29
 3 4 / 30
 3 4 / 31
 3 4 / 32
 3 4 / 33
 3 4 / 34
 3 4 / 35
 3 4 / 36
 3 4 / 37
 3 4 / 38
 4 / 39

12(1)	0	12(1)	0	12(1)	0
37.628	13.066	/	1		
37.628	13.066	/	2		
37.628	13.066	/	3		
37.628	13.066	/	4		
37.628	13.066	/	5		
37.628	13.066	/	6		
37.628	13.066	/	7		
37.628	13.066	/	8		
37.628	13.066	/	9		
37.628	13.066	/	10		
37.628	13.066	/	11		
37.628	13.066	/	12		
128.960		/	13		
27.760	13.004	/	14		
27.760	13.004	/	15		
27.760	13.004	/	16		
27.760	13.004	/	17		
27.760	13.004	/	18		
27.760	13.004	/	19		
27.760	13.004	/	20		
27.760	13.004	/	21		
27.760	13.004	/	22		
27.760	13.004	/	23		
27.760	13.004	/	24		
27.760	13.004	/	25		
369.960		/	26		
28.087	16.965	/	27		
28.087	16.965	/	28		
28.087	16.965	/	29		
28.087	16.965	/	30		
28.087	16.965	/	31		
28.087	16.965	/	32		
28.087	16.965	/	33		
28.087	16.965	/	34		
28.087	16.965	/	35		
28.087	16.965	/	36		
28.087	16.965	/	37		
28.087	16.965	/	38		
281.500		/	39		
771.310	559.090	548.650	/	1	
771.310	559.090	548.650	/	2	
771.310	559.090	548.650	/	3	
771.310	559.090	548.650	/	4	
771.310	559.090	548.650	/	5	
771.310	559.090	548.650	/	6	
771.310	559.090	548.650	/	7	
771.310	559.090	548.650	/	8	
771.310	559.090	548.650	/	9	
771.310	559.090	548.650	/	10	
771.310	559.090	548.650	/	11	
771.310	559.090	548.650	/	12	
3(300.0)		/	13		
771.310	559.090	548.650	/	14	
771.310	559.090	548.650	/	15	
771.310	559.090	548.650	/	16	
771.310	559.090	548.650	/	17	
771.310	559.090	548.650	/	18	
771.310	559.090	548.650	/	19	
771.310	559.090	548.650	/	20	
771.310	559.090	548.650	/	21	
771.310	559.090	548.650	/	22	
771.310	559.090	548.650	/	23	
771.310	559.090	548.650	/	24	
771.310	559.090	548.650	/	25	
3(300.0)		/	26		
771.310	559.090	548.650	/	27	
771.310	559.090	548.650	/	28	
771.310	559.090	548.650	/	29	
771.310	559.090	548.650	/	30	
771.310	559.090	548.650	/	31	
771.310	559.090	548.650	/	32	
771.310	559.090	548.650	/	33	
771.310	559.090	548.650	/	34	
771.310	559.090	548.650	/	35	
771.310	559.090	548.650	/	36	
771.310	559.090	548.650	/	37	
771.310	559.090	548.650	/	38	
3(300.0)		/	39		

```

1 0 0 0 0 0 14( 0.0) / 1 result control
1 0 0 0 0 0 14( 0.0) / 2 result control
1 0 0 0 0 0 14( 0.0) / 3 result control
1 0 0 0 0 0 14( 0.0) / 4 result control
1 0 0 0 0 0 14( 0.0) / 5 result control
1 0 0 0 0 0 14( 0.0) / 6 result control
1 0 0 0 0 0 14( 0.0) / 7 result control
1 0 0 0 0 0 14( 0.0) / 8 result control
1 0 0 0 0 0 14( 0.0) / 9 result control
1 0 0 0 0 0 14( 0.0) / 10 result control
1 0 0 0 0 0 14( 0.0) / 11 result control
1 0 0 0 0 0 14( 0.0) / 12 result control
1 0 0 0 0 0 14( 0.0) / 13 result control
1 0 0 0 0 0 14( 0.0) / 14 result control
1 0 0 0 0 0 14( 0.0) / 15 result control
1 0 0 0 0 0 14( 0.0) / 16 result control
1 0 0 0 0 0 14( 0.0) / 17 result control
1 0 0 0 0 0 14( 0.0) / 18 result control
1 0 0 0 0 0 14( 0.0) / 19 result control
1 0 0 0 0 0 14( 0.0) / 20 result control
1 0 0 0 0 0 14( 0.0) / 21 result control
1 0 0 0 0 0 14( 0.0) / 22 result control
1 0 0 0 0 0 14( 0.0) / 23 result control
1 0 0 0 0 0 14( 0.0) / 24 result control
1 0 0 0 0 0 14( 0.0) / 25 result control
1 0 0 0 0 0 14( 0.0) / 26 result control
1 0 0 0 0 0 14( 0.0) / 27 result control
1 0 0 0 0 0 14( 0.0) / 28 result control
1 0 0 0 0 0 14( 0.0) / 29 result control
1 0 0 0 0 0 14( 0.0) / 30 result control
1 0 0 0 0 0 14( 0.0) / 31 result control
1 0 0 0 0 0 14( 0.0) / 32 result control
1 0 0 0 0 0 14( 0.0) / 33 result control
1 0 0 0 0 0 14( 0.0) / 34 result control
1 0 0 0 0 0 14( 0.0) / 35 result control
1 0 0 0 0 0 14( 0.0) / 36 result control
1 0 0 0 0 0 14( 0.0) / 37 result control
1 0 0 0 0 0 14( 0.0) / 38 result control
1 0 0 0 0 0 14( 0.0) / 39 result control

```

0 / PWR

39(0.000) / void ratio (%)

12(-0.1E-05) 1(-0.1E-05)

12(-0.1E-05) 1(-0.1E-05)

12(-0.3E-03) 1(-0.3E-03)

0 /xs val.

0 /branching

0 /weight factor

A.3.2. SWAT input for Mihama-3 Sample NO 1.

```

===== PDS FILE ALOCATION =====
FASTP : pfast
THERMP : pthml
FASTU : fastu
THERMU : thermalu
MACWRK : macrowrk
FLUX : flux
MACRO : macro
MCROSSP: pmcrs
MICREF : micref
UMCROS : umcros
===== for libmak =====
usacti :/home5/codes/swat9906/xslib/acti.j32.v2.1
usfp :/home5/codes/swat9906/xslib/fp.j32.v2.4
ori2ori:/home5/codes/swat9906/ori2origlib/decaydat.fp-j3.v7
===== for origen2 =====
photo :/home5/codes/swat9906/ori2origlib/photodat
***** global data lists *****
Template of SWAT Input Data for The Obrigheim Reactor By SHIN, Hee Sung
mi1 15 204 8.301 3.2080 1.4300 365.76 -1.00 0.7518 0.9484 0.6502 0.6934
1 1 1 0 0 0 0 1 1 1 / Library Control
1 1 1 1 2 1 4 3 -2 1 0 0 0 0 2 0 1 0 0 0 / SRAC General Control
1.0000E-25
63 44 1 /fast thermal lethergy
3 3 3 3 3 0 3 0 0 0 0 0 8 15 0 0 30 0 1 /COL.PROB.CONT
1 2 3
0.00000 0.46470 0.53595 0.84350
1
3
67 1 0 0 0 4 4(0) 1.0 0.929 0.0 9.99600 3.208 0.0 4(0.0) / UO2 (3.208wt%)
922340 2 1 0 0 1 2 / U -234
922350 2 1 0 0 1 2 / U -235
922360 2 1 0 0 1 2 / U -236
922380 2 1 0 0 1 2 / U -238
932370 2 1 0 0 1 0
942380 2 1 0 0 1 0
942390 2 1 0 0 1 0
942400 2 1 0 0 1 0
942410 2 1 0 0 1 0
942420 2 1 0 0 1 0
952410 2 1 0 0 1 0
952421 2 1 3 0 1 0
952420 2 1 2 0 1 0
952430 2 1 0 0 1 0
962420 2 1 0 0 1 0
962430 2 1 0 0 1 0
962440 2 1 0 0 1 0
962450 2 1 0 0 1 0
962460 2 1 0 0 1 0
641520 2 1 0 0 1 0
641540 2 1 0 0 1 0
641550 2 1 0 0 1 0
641560 2 1 0 0 1 0
641570 2 1 0 0 1 0
641580 2 1 0 0 1 0
641600 2 1 0 0 1 0
541350 2 1 0 0 1 0
601430 2 1 0 0 1 0
451030 2 1 0 0 1 0
541310 2 1 0 0 1 0
551330 2 1 0 0 1 0
621490 2 1 0 0 1 0
430990 2 1 0 0 1 0
621520 2 1 0 0 1 0
621510 2 1 0 0 1 0
611470 2 1 0 0 1 0
631530 2 1 0 0 1 0
601450 2 1 0 0 1 0
631550 2 1 0 0 1 0
631540 2 1 0 0 1 0
621500 2 1 0 0 1 0
420950 2 1 0 0 1 0
471090 2 1 0 0 1 0
611481 2 1 3 0 1 0
441010 2 1 0 0 1 0
551340 2 1 0 0 1 0

```

461050 2 1 0 0 1 0
 611480 2 1 2 0 1 0
 451050 2 1 0 0 1 0
 591410 2 1 0 0 1 0
 360830 2 1 0 0 1 0
 461080 2 1 0 0 1 0
 621470 2 1 0 0 1 0
 461070 2 1 0 0 1 0
 420970 2 1 0 0 1 0
 481130 2 1 0 0 1 0
 551350 2 1 0 0 1 0
 420980 2 1 0 0 1 0
 541330 2 1 0 0 1 0
 491150 2 1 0 0 1 0
 591430 2 1 0 0 1 0
 631560 2 1 0 0 1 0
 441030 2 1 0 0 1 0
 621480 2 1 0 0 1 0
 601470 2 1 0 0 1 0
 611490 2 1 0 0 1 0
 80160 0 0 0 0 0 1
 922340 285.00
 922350 32080.00
 922360 208.00
 922380 967419.94
 4.64956E-02 / O-16 constant density
 3 9(0) 0.0 0.26606 8(0.0)
 400000 2 1 1 0 0 1 / Zr
 260000 2 1 1 0 0 1 / Fe
 240000 2 1 1 0 0 1 / Cr
 4.2982E-02 1.4838E-04 7.5891E-05 / Zr,Fe,Cr
 4 0 1 7(0) 0.0 1.00593 8(0.0)
 10010 2 1 0 9 0 1 / H-1
 80160 2 1 0 0 0 1 / O-16
 50100 2 1 0 0 0 1 / B-10
 50110 2 1 0 0 0 1 / B-11
 4(1.0E-2) /
 1 0
 1
 13 12
 12(2) 1
 3 4 / 1
 3 4 / 2
 3 4 / 3
 3 4 / 4
 3 4 / 5
 3 4 / 6
 3 4 / 7
 3 4 / 8
 3 4 / 9
 3 4 / 10
 3 4 / 11
 3 4 / 12
 4 / 13
 12(1) 0
 17.917 38.610 / 1
 17.917 38.610 / 2
 17.917 38.610 / 3
 17.917 38.610 / 4
 17.917 38.610 / 5
 17.917 38.610 / 6
 17.917 38.610 / 7
 17.917 38.610 / 8
 17.917 38.610 / 9
 17.917 38.610 / 10
 17.917 38.610 / 11
 17.917 38.610 / 12
 1825.000 / 13
 923.000 600.400 560.400 / 1
 923.000 600.400 560.400 / 2
 923.000 600.400 560.400 / 3
 923.000 600.400 560.400 / 4
 923.000 600.400 560.400 / 5
 923.000 600.400 560.400 / 6
 923.000 600.400 560.400 / 7
 923.000 600.400 560.400 / 8
 923.000 600.400 560.400 / 9
 923.000 600.400 560.400 / 10
 923.000 600.400 560.400 / 11

923.000 600.400 560.400 / 12
3(300.0) / 13
1 0 0 0 0 0 14(0.0) / 1 result control
1 0 0 0 0 0 14(0.0) / 2 result control
1 0 0 0 0 0 14(0.0) / 3 result control
1 0 0 0 0 0 14(0.0) / 4 result control
1 0 0 0 0 0 14(0.0) / 5 result control
1 0 0 0 0 0 14(0.0) / 6 result control
1 0 0 0 0 0 14(0.0) / 7 result control
1 0 0 0 0 0 14(0.0) / 8 result control
1 0 0 0 0 0 14(0.0) / 9 result control
1 0 0 0 0 0 14(0.0) / 10 result control
1 0 0 0 0 0 14(0.0) / 11 result control
1 0 0 0 0 0 14(0.0) / 12 result control
1 0 0 0 0 0 14(0.0) / 13 result control
0 / PWR
13(-0.000) / void ratio (%)
12(-0.4E-03) 1(-0.4E-03)
0 /xs val.
0 /branching
0 /weight factor

A.3.3. SWAT input for Trino Vercellese Sample NO 1.

```
===== PDS FILE ALOCATION =====
FASTP : pfast
THERMP : pthml
FASTU : fastu
THERMU : thermalu
MACWRK : macrowrk
FLUX : flux
MACRO : macro
MCROSSP: pmcrs
MICREF : micref
UMCROS : umcros
===== for libmak =====
usacti ./home5/codes/swat9906/xslib/acti.j32.v2.1
usfp ./home5/codes/swat9906/xslib/fp.j32.v2.4
ori2ori:/home5/codes/swat9906/ori2origlib/decaydat.fp-j3.v7
===== for origen2 =====
photo ./home5/codes/swat9906/ori2origlib/photodat
***** global data lists *****
Template of SWAT Input Data for The Obrigheim Reactor By SHIN, Hee Sung
tr1 15 221 12.042 3.8970 1.3030 264.10 79.20 0.7795 0.9020 0.7351 *****
1 1 1 0 0 0 0 1 1 1 / Library Control
1 1 1 1 2 1 4 3 -2 1 0 0 0 0 2 0 1 0 0 0 / SRAC General Control
1.0000E-25
63 44 1 /fast thermal lethergy
3 3 3 3 3 0 3 0 0 0 0 0 8 15 0 0 30 0 1 /COL.PROB.CONT
1 2 3
0.00000 0.44500 0.48930 0.74132
1
3
67 1 0 0 0 4 4(0) 1.0 0.890 0.0 10.35300 3.897 0.0 4(0.0) / UO2 (3.897wt%)
922340 2 1 0 0 1 2 / U -234
922350 2 1 0 0 1 2 / U -235
922360 2 1 0 0 1 2 / U -236
922380 2 1 0 0 1 2 / U -238
932370 2 1 0 0 1 0
942380 2 1 0 0 1 0
942390 2 1 0 0 1 0
942400 2 1 0 0 1 0
942410 2 1 0 0 1 0
942420 2 1 0 0 1 0
952410 2 1 0 0 1 0
952421 2 1 3 0 1 0
952420 2 1 2 0 1 0
952430 2 1 0 0 1 0
962420 2 1 0 0 1 0
962430 2 1 0 0 1 0
962440 2 1 0 0 1 0
962450 2 1 0 0 1 0
962460 2 1 0 0 1 0
641520 2 1 0 0 1 0
641540 2 1 0 0 1 0
641550 2 1 0 0 1 0
641560 2 1 0 0 1 0
641570 2 1 0 0 1 0
641580 2 1 0 0 1 0
641600 2 1 0 0 1 0
541350 2 1 0 0 1 0
601430 2 1 0 0 1 0
451030 2 1 0 0 1 0
541310 2 1 0 0 1 0
551330 2 1 0 0 1 0
621490 2 1 0 0 1 0
430990 2 1 0 0 1 0
621520 2 1 0 0 1 0
621510 2 1 0 0 1 0
611470 2 1 0 0 1 0
631530 2 1 0 0 1 0
601450 2 1 0 0 1 0
631550 2 1 0 0 1 0
631540 2 1 0 0 1 0
621500 2 1 0 0 1 0
420950 2 1 0 0 1 0
471090 2 1 0 0 1 0
611481 2 1 3 0 1 0
441010 2 1 0 0 1 0
551340 2 1 0 0 1 0
461050 2 1 0 0 1 0
```

611480 2 1 2 0 1 0
 451050 2 1 0 0 1 0
 591410 2 1 0 0 1 0
 360830 2 1 0 0 1 0
 461080 2 1 0 0 1 0
 621470 2 1 0 0 1 0
 461070 2 1 0 0 1 0
 420970 2 1 0 0 1 0
 481130 2 1 0 0 1 0
 551350 2 1 0 0 1 0
 420980 2 1 0 0 1 0
 541330 2 1 0 0 1 0
 491150 2 1 0 0 1 0
 591430 2 1 0 0 1 0
 631560 2 1 0 0 1 0
 441030 2 1 0 0 1 0
 621480 2 1 0 0 1 0
 601470 2 1 0 0 1 0
 611490 2 1 0 0 1 0
 80160 0 0 0 0 0 1
 922340 350.00
 922350 38970.00
 922360 180.00
 922380 960500.00
 4.64956E-02 / O-16 constant density
 3 9(0) 0.0 0.16918 8(0.0)
 260000 2 1 1 0 0 1 / Fe
 240000 2 1 1 0 0 1 / Cr
 280000 2 1 1 0 0 1 / Ni
 5.7872E-2 1.7408E-2 8.1116E-3 / Fe, Cr, Ni
 4 0 1 7(0) 0.0 0.83673 8(0.0)
 10010 2 1 0 9 0 1 / H-1
 80160 2 1 0 0 0 1 / O-16
 50100 2 1 0 0 0 1 / B-10
 50110 2 1 0 0 0 1 / B-11
 4(1.0E-2) /
 1 0
 1
 39 12
 12(2) 1 12(2) 1 12(2) 1
 3 4 / 1
 3 4 / 2
 3 4 / 3
 3 4 / 4
 3 4 / 5
 3 4 / 6
 3 4 / 7
 3 4 / 8
 3 4 / 9
 3 4 / 10
 3 4 / 11
 3 4 / 12
 4 / 13
 3 4 / 14
 3 4 / 15
 3 4 / 16
 3 4 / 17
 3 4 / 18
 3 4 / 19
 3 4 / 20
 3 4 / 21
 3 4 / 22
 3 4 / 23
 3 4 / 24
 3 4 / 25
 4 / 26
 3 4 / 27
 3 4 / 28
 3 4 / 29
 3 4 / 30
 3 4 / 31
 3 4 / 32
 3 4 / 33
 3 4 / 34
 3 4 / 35
 3 4 / 36
 3 4 / 37
 3 4 / 38
 4 / 39

12(1)	0	12(1)	0	12(1)	0
18.833	10.390	/	1		
18.833	10.390	/	2		
18.833	10.390	/	3		
18.833	10.390	/	4		
18.833	10.390	/	5		
18.833	10.390	/	6		
18.833	10.390	/	7		
18.833	10.390	/	8		
18.833	10.390	/	9		
18.833	10.390	/	10		
18.833	10.390	/	11		
18.833	10.390	/	12		
86.000		/	13		
21.917	16.138	/	14		
21.917	16.138	/	15		
21.917	16.138	/	16		
21.917	16.138	/	17		
21.917	16.138	/	18		
21.917	16.138	/	19		
21.917	16.138	/	20		
21.917	16.138	/	21		
21.917	16.138	/	22		
21.917	16.138	/	23		
21.917	16.138	/	24		
21.917	16.138	/	25		
51.000		/	26		
24.333	18.663	/	27		
24.333	18.663	/	28		
24.333	18.663	/	29		
24.333	18.663	/	30		
24.333	18.663	/	31		
24.333	18.663	/	32		
24.333	18.663	/	33		
24.333	18.663	/	34		
24.333	18.663	/	35		
24.333	18.663	/	36		
24.333	18.663	/	37		
24.333	18.663	/	38		
10.000		/	39		
1001.000	570.000	543.000	/	1	
1001.000	570.000	543.000	/	2	
1001.000	570.000	543.000	/	3	
1001.000	570.000	543.000	/	4	
1001.000	570.000	543.000	/	5	
1001.000	570.000	543.000	/	6	
1001.000	570.000	543.000	/	7	
1001.000	570.000	543.000	/	8	
1001.000	570.000	543.000	/	9	
1001.000	570.000	543.000	/	10	
1001.000	570.000	543.000	/	11	
1001.000	570.000	543.000	/	12	
3(300.0)		/	13		
1001.000	570.000	543.000	/	14	
1001.000	570.000	543.000	/	15	
1001.000	570.000	543.000	/	16	
1001.000	570.000	543.000	/	17	
1001.000	570.000	543.000	/	18	
1001.000	570.000	543.000	/	19	
1001.000	570.000	543.000	/	20	
1001.000	570.000	543.000	/	21	
1001.000	570.000	543.000	/	22	
1001.000	570.000	543.000	/	23	
1001.000	570.000	543.000	/	24	
1001.000	570.000	543.000	/	25	
3(300.0)		/	26		
1001.000	570.000	543.000	/	27	
1001.000	570.000	543.000	/	28	
1001.000	570.000	543.000	/	29	
1001.000	570.000	543.000	/	30	
1001.000	570.000	543.000	/	31	
1001.000	570.000	543.000	/	32	
1001.000	570.000	543.000	/	33	
1001.000	570.000	543.000	/	34	
1001.000	570.000	543.000	/	35	
1001.000	570.000	543.000	/	36	
1001.000	570.000	543.000	/	37	
1001.000	570.000	543.000	/	38	
3(300.0)		/	39		

```

1 0 0 0 0 0 14( 0.0) / 1 result control
1 0 0 0 0 0 14( 0.0) / 2 result control
1 0 0 0 0 0 14( 0.0) / 3 result control
1 0 0 0 0 0 14( 0.0) / 4 result control
1 0 0 0 0 0 14( 0.0) / 5 result control
1 0 0 0 0 0 14( 0.0) / 6 result control
1 0 0 0 0 0 14( 0.0) / 7 result control
1 0 0 0 0 0 14( 0.0) / 8 result control
1 0 0 0 0 0 14( 0.0) / 9 result control
1 0 0 0 0 0 14( 0.0) / 10 result control
1 0 0 0 0 0 14( 0.0) / 11 result control
1 0 0 0 0 0 14( 0.0) / 12 result control
1 0 0 0 0 0 14( 0.0) / 13 result control
1 0 0 0 0 0 14( 0.0) / 14 result control
1 0 0 0 0 0 14( 0.0) / 15 result control
1 0 0 0 0 0 14( 0.0) / 16 result control
1 0 0 0 0 0 14( 0.0) / 17 result control
1 0 0 0 0 0 14( 0.0) / 18 result control
1 0 0 0 0 0 14( 0.0) / 19 result control
1 0 0 0 0 0 14( 0.0) / 20 result control
1 0 0 0 0 0 14( 0.0) / 21 result control
1 0 0 0 0 0 14( 0.0) / 22 result control
1 0 0 0 0 0 14( 0.0) / 23 result control
1 0 0 0 0 0 14( 0.0) / 24 result control
1 0 0 0 0 0 14( 0.0) / 25 result control
1 0 0 0 0 0 14( 0.0) / 26 result control
1 0 0 0 0 0 14( 0.0) / 27 result control
1 0 0 0 0 0 14( 0.0) / 28 result control
1 0 0 0 0 0 14( 0.0) / 29 result control
1 0 0 0 0 0 14( 0.0) / 30 result control
1 0 0 0 0 0 14( 0.0) / 31 result control
1 0 0 0 0 0 14( 0.0) / 32 result control
1 0 0 0 0 0 14( 0.0) / 33 result control
1 0 0 0 0 0 14( 0.0) / 34 result control
1 0 0 0 0 0 14( 0.0) / 35 result control
1 0 0 0 0 0 14( 0.0) / 36 result control
1 0 0 0 0 0 14( 0.0) / 37 result control
1 0 0 0 0 0 14( 0.0) / 38 result control
1 0 0 0 0 0 14( 0.0) / 39 result control

```

0 / PWR

39(0.000) / void ratio (%)

12(-0.1E-02) 1(-0.1E-02)

12(-0.8E-03) 1(-0.8E-03)

12(-0.3E-03) 1(-0.3E-03)

0 /xs val.

0 /branching

0 /weight factor

A.3.4. SWAT input for Turky Point Sample NO 1.

```
===== FILE ALOCATION =====
FASTP : pfast
THERMP : pthml
FASTU : fastu
THERMU : thermalu
MACWRK : macrowrk
FLUX : flux
MACRO : macro
MCROSSP: pmcrs
MICREF : micref
UMCROS : umcros
===== for libmak =====
usacti ./home5/codes/swat9906/xslib/acti.j32.v2.1
usfp ./home5/codes/swat9906/xslib/fp.j32.v2.4
ori2ori:/home5/codes/swat9906/origlib/decaydat.fp-j3.v7
===== for origin2 =====
photo ./home5/codes/swat9906/origlib/photodat
***** global data lists *****
Template of SWAT Input Data for The Obrigheim Reactor By SHIN, Hee Sung
tu1 15 204 30.720 2.5560 1.4300 365.80 167.60 0.7310 0.9484 0.6502 0.6934
1 1 1 0 0 0 0 1 1 1 / Library Control
1 1 1 1 2 1 4 3 -2 1 0 0 0 0 2 0 1 0 0 0 / SRAC General Control
1.0000E-25
63 44 1 /fast thermal lethergy
3 3 3 3 3 0 3 0 0 0 0 0 8 15 0 0 30 0 1 /COL.PROB.CONT
1 2 3
0.00000 0.46482 0.53595 0.84350
1
3
67 1 0 0 0 4 4(0) 1.0 0.930 0.0 10.23500 2.556 0.0 4(0.0) / UO2 (2.556wt%)
922340 2 1 0 0 1 2 / U -234
922350 2 1 0 0 1 2 / U -235
922360 2 1 0 0 1 2 / U -236
922380 2 1 0 0 1 2 / U -238
932370 2 1 0 0 1 0
942380 2 1 0 0 1 0
942390 2 1 0 0 1 0
942400 2 1 0 0 1 0
942410 2 1 0 0 1 0
942420 2 1 0 0 1 0
952410 2 1 0 0 1 0
952421 2 1 3 0 1 0
952420 2 1 2 0 1 0
952430 2 1 0 0 1 0
962420 2 1 0 0 1 0
962430 2 1 0 0 1 0
962440 2 1 0 0 1 0
962450 2 1 0 0 1 0
962460 2 1 0 0 1 0
641520 2 1 0 0 1 0
641540 2 1 0 0 1 0
641550 2 1 0 0 1 0
641560 2 1 0 0 1 0
641570 2 1 0 0 1 0
641580 2 1 0 0 1 0
641600 2 1 0 0 1 0
541350 2 1 0 0 1 0
601430 2 1 0 0 1 0
451030 2 1 0 0 1 0
541310 2 1 0 0 1 0
551330 2 1 0 0 1 0
621490 2 1 0 0 1 0
430990 2 1 0 0 1 0
621520 2 1 0 0 1 0
621510 2 1 0 0 1 0
611470 2 1 0 0 1 0
631530 2 1 0 0 1 0
601450 2 1 0 0 1 0
631550 2 1 0 0 1 0
631540 2 1 0 0 1 0
621500 2 1 0 0 1 0
420950 2 1 0 0 1 0
471090 2 1 0 0 1 0
611481 2 1 3 0 1 0
441010 2 1 0 0 1 0
551340 2 1 0 0 1 0
```

461050 2 1 0 0 1 0
 611480 2 1 2 0 1 0
 451050 2 1 0 0 1 0
 591410 2 1 0 0 1 0
 360830 2 1 0 0 1 0
 461080 2 1 0 0 1 0
 621470 2 1 0 0 1 0
 461070 2 1 0 0 1 0
 420970 2 1 0 0 1 0
 481130 2 1 0 0 1 0
 551350 2 1 0 0 1 0
 420980 2 1 0 0 1 0
 541330 2 1 0 0 1 0
 491150 2 1 0 0 1 0
 591430 2 1 0 0 1 0
 631560 2 1 0 0 1 0
 441030 2 1 0 0 1 0
 621480 2 1 0 0 1 0
 601470 2 1 0 0 1 0
 611490 2 1 0 0 1 0
 80160 0 0 0 0 0 1
 922340 230.00
 922350 25560.00
 922360 120.00
 922380 974089.94
 4.64956E-02 / O-16 constant density
 3 9(0) 0.0 0.26564 8(0.0)
 400000 2 1 1 0 0 1 / Zr
 260000 2 1 1 0 0 1 / Fe
 240000 2 1 1 0 0 1 / Cr
 4.2982E-02 1.4838E-04 7.5891E-05 / Zr,Fe,Cr
 4 0 1 7(0) 0.0 1.00593 8(0.0)
 10010 2 1 0 9 0 1 / H-1
 80160 2 1 0 0 0 1 / O-16
 50100 2 1 0 0 0 1 / B-10
 50110 2 1 0 0 0 1 / B-11
 4(1.0E-2) /
 1 0
 1
 39 12
 12(2) 1 12(2) 1 12(2) 1
 3 4 / 1
 3 4 / 2
 3 4 / 3
 3 4 / 4
 3 4 / 5
 3 4 / 6
 3 4 / 7
 3 4 / 8
 3 4 / 9
 3 4 / 10
 3 4 / 11
 3 4 / 12
 4 / 13
 3 4 / 14
 3 4 / 15
 3 4 / 16
 3 4 / 17
 3 4 / 18
 3 4 / 19
 3 4 / 20
 3 4 / 21
 3 4 / 22
 3 4 / 23
 3 4 / 24
 3 4 / 25
 4 / 26
 3 4 / 27
 3 4 / 28
 3 4 / 29
 3 4 / 30
 3 4 / 31
 3 4 / 32
 3 4 / 33
 3 4 / 34
 3 4 / 35
 3 4 / 36
 3 4 / 37
 3 4 / 38

4	/ 39
12(1)	0 12(1) 0 12(1) 0
26.167	32.235 / 1
26.167	32.235 / 2
26.167	32.235 / 3
26.167	32.235 / 4
26.167	32.235 / 5
26.167	32.235 / 6
26.167	32.235 / 7
26.167	32.235 / 8
26.167	32.235 / 9
26.167	32.235 / 10
26.167	32.235 / 11
26.167	32.235 / 12
58.000	/ 13
27.250	32.235 / 14
27.250	32.235 / 15
27.250	32.235 / 16
27.250	32.235 / 17
27.250	32.235 / 18
27.250	32.235 / 19
27.250	32.235 / 20
27.250	32.235 / 21
27.250	32.235 / 22
27.250	32.235 / 23
27.250	32.235 / 24
27.250	32.235 / 25
62.000	/ 26
26.000	32.235 / 27
26.000	32.235 / 28
26.000	32.235 / 29
26.000	32.235 / 30
26.000	32.235 / 31
26.000	32.235 / 32
26.000	32.235 / 33
26.000	32.235 / 34
26.000	32.235 / 35
26.000	32.235 / 36
26.000	32.235 / 37
26.000	32.235 / 38
927.000	/ 39
922.000	595.000 570.000 / 1
922.000	595.000 570.000 / 2
922.000	595.000 570.000 / 3
922.000	595.000 570.000 / 4
922.000	595.000 570.000 / 5
922.000	595.000 570.000 / 6
922.000	595.000 570.000 / 7
922.000	595.000 570.000 / 8
922.000	595.000 570.000 / 9
922.000	595.000 570.000 / 10
922.000	595.000 570.000 / 11
922.000	595.000 570.000 / 12
3(300.0)	/ 13
922.000	595.000 570.000 / 14
922.000	595.000 570.000 / 15
922.000	595.000 570.000 / 16
922.000	595.000 570.000 / 17
922.000	595.000 570.000 / 18
922.000	595.000 570.000 / 19
922.000	595.000 570.000 / 20
922.000	595.000 570.000 / 21
922.000	595.000 570.000 / 22
922.000	595.000 570.000 / 23
922.000	595.000 570.000 / 24
922.000	595.000 570.000 / 25
3(300.0)	/ 26
922.000	595.000 570.000 / 27
922.000	595.000 570.000 / 28
922.000	595.000 570.000 / 29
922.000	595.000 570.000 / 30
922.000	595.000 570.000 / 31
922.000	595.000 570.000 / 32
922.000	595.000 570.000 / 33
922.000	595.000 570.000 / 34
922.000	595.000 570.000 / 35
922.000	595.000 570.000 / 36
922.000	595.000 570.000 / 37
922.000	595.000 570.000 / 38

```

3( 300.0)      / 39
 1 0 0 0 0 0 14( 0.0) / 1 result control
 1 0 0 0 0 0 14( 0.0) / 2 result control
 1 0 0 0 0 0 14( 0.0) / 3 result control
 1 0 0 0 0 0 14( 0.0) / 4 result control
 1 0 0 0 0 0 14( 0.0) / 5 result control
 1 0 0 0 0 0 14( 0.0) / 6 result control
 1 0 0 0 0 0 14( 0.0) / 7 result control
 1 0 0 0 0 0 14( 0.0) / 8 result control
 1 0 0 0 0 0 14( 0.0) / 9 result control
 1 0 0 0 0 0 14( 0.0) / 10 result control
 1 0 0 0 0 0 14( 0.0) / 11 result control
 1 0 0 0 0 0 14( 0.0) / 12 result control
 1 0 0 0 0 0 14( 0.0) / 13 result control
 1 0 0 0 0 0 14( 0.0) / 14 result control
 1 0 0 0 0 0 14( 0.0) / 15 result control
 1 0 0 0 0 0 14( 0.0) / 16 result control
 1 0 0 0 0 0 14( 0.0) / 17 result control
 1 0 0 0 0 0 14( 0.0) / 18 result control
 1 0 0 0 0 0 14( 0.0) / 19 result control
 1 0 0 0 0 0 14( 0.0) / 20 result control
 1 0 0 0 0 0 14( 0.0) / 21 result control
 1 0 0 0 0 0 14( 0.0) / 22 result control
 1 0 0 0 0 0 14( 0.0) / 23 result control
 1 0 0 0 0 0 14( 0.0) / 24 result control
 1 0 0 0 0 0 14( 0.0) / 25 result control
 1 0 0 0 0 0 14( 0.0) / 26 result control
 1 0 0 0 0 0 14( 0.0) / 27 result control
 1 0 0 0 0 0 14( 0.0) / 28 result control
 1 0 0 0 0 0 14( 0.0) / 29 result control
 1 0 0 0 0 0 14( 0.0) / 30 result control
 1 0 0 0 0 0 14( 0.0) / 31 result control
 1 0 0 0 0 0 14( 0.0) / 32 result control
 1 0 0 0 0 0 14( 0.0) / 33 result control
 1 0 0 0 0 0 14( 0.0) / 34 result control
 1 0 0 0 0 0 14( 0.0) / 35 result control
 1 0 0 0 0 0 14( 0.0) / 36 result control
 1 0 0 0 0 0 14( 0.0) / 37 result control
 1 0 0 0 0 0 14( 0.0) / 38 result control
 1 0 0 0 0 0 14( 0.0) / 39 result control

```

0 / PWR

39(0.000) / void ratio (%)

12(-0.4E-03) 1(-0.4E-03)

12(-0.4E-03) 1(-0.4E-03)

12(-0.4E-03) 1(-0.4E-03)

0 /xs val.

0 /branching

0 /weight factor

A.3.5. SWAT input for Calvert Cliffs Sample NO 1.

```
===== PDS FILE ALOCATION =====
FASTP : pfast
THERMP : pthml
FASTU : fastu
THERMU : thermalu
MACWRK : macrowrk
FLUX : flux
MACRO : macro
MCROSSP: pmers
MICREF : micref
UMCROS : umcros
===== for libmak =====
usacti :/home5/codes/swat9906/xslib/acti.j32.v2.1
usfp :/home5/codes/swat9906/xslib/fp.j32.v2.4
ori2ori:/home5/codes/swat9906/origlib/decaydat.fp-j3.v7
===== for origen2 =====
photo :/home5/codes/swat9906/origlib/photodat
***** global data lists *****
Template of SWAT Input Data for The Obrigheim Reactor By SHIN, Hee Sung
ca1 14 176 27.348 3.0380 1.4732 347.22 13.20 0.7575 0.9855 1.3140 1.4160
1 1 1 0 0 0 0 1 1 1 / Library Control
1 1 1 1 2 1 4 3 -2 1 0 0 0 0 2 0 1 0 0 0 / SRAC General Control
1.0000E-25
63 44 1 /fast thermal lethergy
3 3 3 3 3 0 3 0 0 0 0 0 8 15 0 0 30 0 1 /COL.PROB.CONT
1 2 3
0.00000 0.47815 0.55880 0.87261
1
3
67 1 0 0 0 4 4(0) 1.0 0.956 0.0 10.04500 3.038 0.0 4(0.0) / UO2 (3.038wt%)
922340 2 1 0 0 1 2 / U -234
922350 2 1 0 0 1 2 / U -235
922360 2 1 0 0 1 2 / U -236
922380 2 1 0 0 1 2 / U -238
932370 2 1 0 0 1 0
942380 2 1 0 0 1 0
942390 2 1 0 0 1 0
942400 2 1 0 0 1 0
942410 2 1 0 0 1 0
942420 2 1 0 0 1 0
952410 2 1 0 0 1 0
952421 2 1 3 0 1 0
952420 2 1 2 0 1 0
952430 2 1 0 0 1 0
962420 2 1 0 0 1 0
962430 2 1 0 0 1 0
962440 2 1 0 0 1 0
962450 2 1 0 0 1 0
962460 2 1 0 0 1 0
641520 2 1 0 0 1 0
641540 2 1 0 0 1 0
641550 2 1 0 0 1 0
641560 2 1 0 0 1 0
641570 2 1 0 0 1 0
641580 2 1 0 0 1 0
641600 2 1 0 0 1 0
541350 2 1 0 0 1 0
601430 2 1 0 0 1 0
451030 2 1 0 0 1 0
541310 2 1 0 0 1 0
551330 2 1 0 0 1 0
621490 2 1 0 0 1 0
430990 2 1 0 0 1 0
621520 2 1 0 0 1 0
621510 2 1 0 0 1 0
611470 2 1 0 0 1 0
631530 2 1 0 0 1 0
601450 2 1 0 0 1 0
631550 2 1 0 0 1 0
631540 2 1 0 0 1 0
621500 2 1 0 0 1 0
420950 2 1 0 0 1 0
471090 2 1 0 0 1 0
611481 2 1 3 0 1 0
441010 2 1 0 0 1 0
551340 2 1 0 0 1 0
461050 2 1 0 0 1 0
```

611480 2 1 2 0 1 0
 451050 2 1 0 0 1 0
 591410 2 1 0 0 1 0
 360830 2 1 0 0 1 0
 461080 2 1 0 0 1 0
 621470 2 1 0 0 1 0
 461070 2 1 0 0 1 0
 420970 2 1 0 0 1 0
 481130 2 1 0 0 1 0
 551350 2 1 0 0 1 0
 420980 2 1 0 0 1 0
 541330 2 1 0 0 1 0
 491150 2 1 0 0 1 0
 591430 2 1 0 0 1 0
 631560 2 1 0 0 1 0
 441030 2 1 0 0 1 0
 621480 2 1 0 0 1 0
 601470 2 1 0 0 1 0
 611490 2 1 0 0 1 0
 80160 0 0 0 0 0 1
 922340 270.00
 922350 30380.00
 922360 140.00
 922380 969210.00
 4.64956E-02 / O-16 constant density.
 3 9(0) 0.0 0.29932 8(0.0)
 400000 2 1 1 0 0 1 / Zr
 260000 2 1 1 0 0 1 / Fe
 240000 2 1 1 0 0 1 / Cr
 4.2982E-02 1.4838E-04 7.5891E-05 / Zr,Fe,Cr
 4 0 1 7(0) 0.0 1.02953 8(0.0)
 10010 2 1 0 9 0 1 / H-1
 80160 2 1 0 0 0 1 / O-16
 50100 2 1 0 0 0 1 / B-10
 50110 2 1 0 0 0 1 / B-11
 4(1.0E-2) /
 1 0
 1
 52 12
 12(2) 1 12(2) 1 12(2) 1 12(2) 1
 3 4 / 1
 3 4 / 2
 3 4 / 3
 3 4 / 4
 3 4 / 5
 3 4 / 6
 3 4 / 7
 3 4 / 8
 3 4 / 9
 3 4 / 10
 3 4 / 11
 3 4 / 12
 4 / 13
 3 4 / 14
 3 4 / 15
 3 4 / 16
 3 4 / 17
 3 4 / 18
 3 4 / 19
 3 4 / 20
 3 4 / 21
 3 4 / 22
 3 4 / 23
 3 4 / 24
 3 4 / 25
 4 / 26
 3 4 / 27
 3 4 / 28
 3 4 / 29
 3 4 / 30
 3 4 / 31
 3 4 / 32
 3 4 / 33
 3 4 / 34
 3 4 / 35
 3 4 / 36
 3 4 / 37
 3 4 / 38
 4 / 39

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3	4 / 40
3	4 / 41
3	4 / 42
3	4 / 43
3	4 / 44
3	4 / 45
3	4 / 46
3	4 / 47
3	4 / 48
3	4 / 49
3	4 / 50
3	4 / 51
4	/ 52
12(1)	0 12(1) 0 12(1) 0 12(1) 0
25.500	17.240 / 1
25.500	17.240 / 2
25.500	17.240 / 3
25.500	17.240 / 4
25.500	17.240 / 5
25.500	17.240 / 6
25.500	17.240 / 7
25.500	17.240 / 8
25.500	17.240 / 9
25.500	17.240 / 10
25.500	17.240 / 11
25.500	17.240 / 12
71.000	/ 13
31.808	19.426 / 14
31.808	19.426 / 15
31.808	19.426 / 16
31.808	19.426 / 17
31.808	19.426 / 18
31.808	19.426 / 19
31.808	19.426 / 20
31.808	19.426 / 21
31.808	19.426 / 22
31.808	19.426 / 23
31.808	19.426 / 24
31.808	19.426 / 25
81.300	/ 26
38.833	17.037 / 27
38.833	17.037 / 28
38.833	17.037 / 29
38.833	17.037 / 30
38.833	17.037 / 31
38.833	17.037 / 32
38.833	17.037 / 33
38.833	17.037 / 34
38.833	17.037 / 35
38.833	17.037 / 36
38.833	17.037 / 37
38.833	17.037 / 38
85.000	/ 39
38.425	14.570 / 40
38.425	14.570 / 41
38.425	14.570 / 42
38.425	14.570 / 43
38.425	14.570 / 44
38.425	14.570 / 45
38.425	14.570 / 46
38.425	14.570 / 47
38.425	14.570 / 48
38.425	14.570 / 49
38.425	14.570 / 50
38.425	14.570 / 51
1870.000	/ 52
790.000	620.000 557.000 / 1
790.000	620.000 557.000 / 2
790.000	620.000 557.000 / 3
790.000	620.000 557.000 / 4
790.000	620.000 557.000 / 5
790.000	620.000 557.000 / 6
790.000	620.000 557.000 / 7
790.000	620.000 557.000 / 8
790.000	620.000 557.000 / 9
790.000	620.000 557.000 / 10
790.000	620.000 557.000 / 11
790.000	620.000 557.000 / 12
3(300.0)	/ 13

790.000	620.000	557.000	/	14
790.000	620.000	557.000	/	15
790.000	620.000	557.000	/	16
790.000	620.000	557.000	/	17
790.000	620.000	557.000	/	18
790.000	620.000	557.000	/	19
790.000	620.000	557.000	/	20
790.000	620.000	557.000	/	21
790.000	620.000	557.000	/	22
790.000	620.000	557.000	/	23
790.000	620.000	557.000	/	24
790.000	620.000	557.000	/	25
3(300.0)			/	26
790.000	620.000	557.000	/	27
790.000	620.000	557.000	/	28
790.000	620.000	557.000	/	29
790.000	620.000	557.000	/	30
790.000	620.000	557.000	/	31
790.000	620.000	557.000	/	32
790.000	620.000	557.000	/	33
790.000	620.000	557.000	/	34
790.000	620.000	557.000	/	35
790.000	620.000	557.000	/	36
790.000	620.000	557.000	/	37
790.000	620.000	557.000	/	38
3(300.0)			/	39
790.000	620.000	557.000	/	40
790.000	620.000	557.000	/	41
790.000	620.000	557.000	/	42
790.000	620.000	557.000	/	43
790.000	620.000	557.000	/	44
790.000	620.000	557.000	/	45
790.000	620.000	557.000	/	46
790.000	620.000	557.000	/	47
790.000	620.000	557.000	/	48
790.000	620.000	557.000	/	49
790.000	620.000	557.000	/	50
790.000	620.000	557.000	/	51
3(300.0)			/	52
1 0 0 0 0 0 14(0.0)		/	1 result control
1 0 0 0 0 0 14(0.0)		/	2 result control
1 0 0 0 0 0 14(0.0)		/	3 result control
1 0 0 0 0 0 14(0.0)		/	4 result control
1 0 0 0 0 0 14(0.0)		/	5 result control
1 0 0 0 0 0 14(0.0)		/	6 result control
1 0 0 0 0 0 14(0.0)		/	7 result control
1 0 0 0 0 0 14(0.0)		/	8 result control
1 0 0 0 0 0 14(0.0)		/	9 result control
1 0 0 0 0 0 14(0.0)		/	10 result control
1 0 0 0 0 0 14(0.0)		/	11 result control
1 0 0 0 0 0 14(0.0)		/	12 result control
1 0 0 0 0 0 14(0.0)		/	13 result control
1 0 0 0 0 0 14(0.0)		/	14 result control
1 0 0 0 0 0 14(0.0)		/	15 result control
1 0 0 0 0 0 14(0.0)		/	16 result control
1 0 0 0 0 0 14(0.0)		/	17 result control
1 0 0 0 0 0 14(0.0)		/	18 result control
1 0 0 0 0 0 14(0.0)		/	19 result control
1 0 0 0 0 0 14(0.0)		/	20 result control
1 0 0 0 0 0 14(0.0)		/	21 result control
1 0 0 0 0 0 14(0.0)		/	22 result control
1 0 0 0 0 0 14(0.0)		/	23 result control
1 0 0 0 0 0 14(0.0)		/	24 result control
1 0 0 0 0 0 14(0.0)		/	25 result control
1 0 0 0 0 0 14(0.0)		/	26 result control
1 0 0 0 0 0 14(0.0)		/	27 result control
1 0 0 0 0 0 14(0.0)		/	28 result control
1 0 0 0 0 0 14(0.0)		/	29 result control
1 0 0 0 0 0 14(0.0)		/	30 result control
1 0 0 0 0 0 14(0.0)		/	31 result control
1 0 0 0 0 0 14(0.0)		/	32 result control
1 0 0 0 0 0 14(0.0)		/	33 result control
1 0 0 0 0 0 14(0.0)		/	34 result control
1 0 0 0 0 0 14(0.0)		/	35 result control
1 0 0 0 0 0 14(0.0)		/	36 result control
1 0 0 0 0 0 14(0.0)		/	37 result control
1 0 0 0 0 0 14(0.0)		/	38 result control
1 0 0 0 0 0 14(0.0)		/	39 result control
1 0 0 0 0 0 14(0.0)		/	40 result control

```

1 0 0 0 0 0 14( 0.0) / 41 result control
1 0 0 0 0 0 14( 0.0) / 42 result control
1 0 0 0 0 0 14( 0.0) / 43 result control
1 0 0 0 0 0 14( 0.0) / 44 result control
1 0 0 0 0 0 14( 0.0) / 45 result control
1 0 0 0 0 0 14( 0.0) / 46 result control
1 0 0 0 0 0 14( 0.0) / 47 result control
1 0 0 0 0 0 14( 0.0) / 48 result control
1 0 0 0 0 0 14( 0.0) / 49 result control
1 0 0 0 0 0 14( 0.0) / 50 result control
1 0 0 0 0 0 14( 0.0) / 51 result control
1 0 0 0 0 0 14( 0.0) / 52 result control
0 / PWR
52( 0.000) / void ratio (%)
12(-0.3E-03) 1(-0.3E-03)
12(-0.5E-03) 1(-0.5E-03)
12(-0.5E-03) 1(-0.5E-03)
12(-0.5E-03) 1(-0.5E-03)
0 /xs val.
0 /branching
0 /weight factor

comment statement
    0 h2ofrac
    9 light element inclued in fresh fuel
o      135.000
cr     5.90000
mn     0.330000
fe     12.9000
co     0.750000E-01
ni     9.90000
zr     221.000
nb     0.710000
sn     3.60000

```

A.3.6. SWAT input for H. B. Robinson Sample NO 1.

```
===== PDS FILE ALOCATION ======
FASTP : pfast
THERMP : pthml
FASTU : fastu
THERMU : thermalu
MACWRK : macrowrk
FLUX : flux
MACRO : macro
MCROSSP: pmcrs
MICREF : micref
UMCROS : umcros
===== for libmak =====
usacti ./home5/codes/swat9906/xslib/acti.j32.v2.1
usfp ./home5/codes/swat9906/xslib/fp.j32.v2.4
ori2ori:/home5/codes/swat9906/ori2origlib/decaydat.fp-j3.v7
===== for origen2 =====
photo ./home5/codes/swat9906/ori2origlib/photodat
***** global data lists *****
Template of SWAT Input Data for The Obrigheim Reactor By SHIN, Hee Sung
r01 15 204 16.020 2.5610 1.4300 365.80 11.00 0.7544 0.9484 0.2839 0.3004
1 1 1 0 0 0 0 1 1 1 / Library Control
1 1 1 1 2 1 4 3 -2 1 0 0 0 0 2 0 1 0 0 0 / SRAC General Control
1.0000E-25
63 44 1 /fast thermal lethurgy
3 3 3 3 3 0 3 0 0 0 0 0 8 15 0 0 30 0 1 /COL.PROB.CONT
1 2 3
0.00000 0.46470 0.53595 0.84350
1
3
67 1 0 0 0 4 4(0) 1.0 0.929 0.0 9.94400 2.561 0.0 4(0.0) / UO2 (2.561wt%)
922340 2 1 0 0 1 2 / U -234
922350 2 1 0 0 1 2 / U -235
922360 2 1 0 0 1 2 / U -236
922380 2 1 0 0 1 2 / U -238
932370 2 1 0 0 1 0
942380 2 1 0 0 1 0
942390 2 1 0 0 1 0
942400 2 1 0 0 1 0
942410 2 1 0 0 1 0
942420 2 1 0 0 1 0
952410 2 1 0 0 1 0
952421 2 1 3 0 1 0
952420 2 1 2 0 1 0
952430 2 1 0 0 1 0
962420 2 1 0 0 1 0
962430 2 1 0 0 1 0
962440 2 1 0 0 1 0
962450 2 1 0 0 1 0
962460 2 1 0 0 1 0
641520 2 1 0 0 1 0
641540 2 1 0 0 1 0
641550 2 1 0 0 1 0
641560 2 1 0 0 1 0
641570 2 1 0 0 1 0
641580 2 1 0 0 1 0
641600 2 1 0 0 1 0
541350 2 1 0 0 1 0
601430 2 1 0 0 1 0
451030 2 1 0 0 1 0
541310 2 1 0 0 1 0
551330 2 1 0 0 1 0
621490 2 1 0 0 1 0
430990 2 1 0 0 1 0
621520 2 1 0 0 1 0
621510 2 1 0 0 1 0
611470 2 1 0 0 1 0
631530 2 1 0 0 1 0
601450 2 1 0 0 1 0
631550 2 1 0 0 1 0
631540 2 1 0 0 1 0
621500 2 1 0 0 1 0
420950 2 1 0 0 1 0
471090 2 1 0 0 1 0
611481 2 1 3 0 1 0
441010 2 1 0 0 1 0
551340 2 1 0 0 1 0
461050 2 1 0 0 1 0
```

611480 2 1 2 0 1 0
 451050 2 1 0 0 1 0
 591410 2 1 0 0 1 0
 360830 2 1 0 0 1 0
 461080 2 1 0 0 1 0
 621470 2 1 0 0 1 0
 461070 2 1 0 0 1 0
 420970 2 1 0 0 1 0
 481130 2 1 0 0 1 0
 551350 2 1 0 0 1 0
 420980 2 1 0 0 1 0
 541330 2 1 0 0 1 0
 491150 2 1 0 0 1 0
 591430 2 1 0 0 1 0
 631560 2 1 0 0 1 0
 441030 2 1 0 0 1 0
 621480 2 1 0 0 1 0
 601470 2 1 0 0 1 0
 611490 2 1 0 0 1 0
 80160 0 0 0 0 0 1
 922340 230.00
 922350 25610.00
 922360 130.00
 922380 974030.00
 4.64956E-02 / O-16 constant density
 3 9(0) 0.0 0.26606 8(0.0)
 400000 2 1 1 0 0 1 / Zr
 260000 2 1 1 0 0 1 / Fe
 240000 2 1 1 0 0 1 / Cr
 4.2982E-02 1.4838E-04 7.5891E-05 / Zr,Fe,Cr
 4 0 1 7(0) 0.0 1.00593 8(0.0)
 10010 2 1 0 9 0 1 / H-1
 80160 2 1 0 0 0 1 / O-16
 50100 2 1 0 0 0 1 / B-10
 50110 2 1 0 0 0 1 / B-11
 4(1.0E-2) /
 1 0
 1
 52 12
 12(2) 1 12(2) 1 12(2) 1 12(2) 1
 3 4 / 1
 3 4 / 2
 3 4 / 3
 3 4 / 4
 3 4 / 5
 3 4 / 6
 3 4 / 7
 3 4 / 8
 3 4 / 9
 3 4 / 10
 3 4 / 11
 3 4 / 12
 4 / 13
 3 4 / 14
 3 4 / 15
 3 4 / 16
 3 4 / 17
 3 4 / 18
 3 4 / 19
 3 4 / 20
 3 4 / 21
 3 4 / 22
 3 4 / 23
 3 4 / 24
 3 4 / 25
 4 / 26
 3 4 / 27
 3 4 / 28
 3 4 / 29
 3 4 / 30
 3 4 / 31
 3 4 / 32
 3 4 / 33
 3 4 / 34
 3 4 / 35
 3 4 / 36
 3 4 / 37
 3 4 / 38
 4 / 39

3	4 / 40
3	4 / 41
3	4 / 42
3	4 / 43
3	4 / 44
3	4 / 45
3	4 / 46
3	4 / 47
3	4 / 48
3	4 / 49
3	4 / 50
3	4 / 51
4	/ 52
12(1)	0 12(1) 0 12(1) 0 12(1) 0
20.292	20.861 / 1
20.292	20.861 / 2
20.292	20.861 / 3
20.292	20.861 / 4
20.292	20.861 / 5
20.292	20.861 / 6
20.292	20.861 / 7
20.292	20.861 / 8
20.292	20.861 / 9
20.292	20.861 / 10
20.292	20.861 / 11
20.292	20.861 / 12
40.000	/ 13
20.292	20.150 / 14
20.292	20.150 / 15
20.292	20.150 / 16
20.292	20.150 / 17
20.292	20.150 / 18
20.292	20.150 / 19
20.292	20.150 / 20
20.292	20.150 / 21
20.292	20.150 / 22
20.292	20.150 / 23
20.292	20.150 / 24
20.292	20.150 / 25
64.000	/ 26
13.000	19.566 / 27
13.000	19.566 / 28
13.000	19.566 / 29
13.000	19.566 / 30
13.000	19.566 / 31
13.000	19.566 / 32
13.000	19.566 / 33
13.000	19.566 / 34
13.000	19.566 / 35
13.000	19.566 / 36
13.000	19.566 / 37
13.000	19.566 / 38
39.000	/ 39
13.000	19.111 / 40
13.000	19.111 / 41
13.000	19.111 / 42
13.000	19.111 / 43
13.000	19.111 / 44
13.000	19.111 / 45
13.000	19.111 / 46
13.000	19.111 / 47
13.000	19.111 / 48
13.000	19.111 / 49
13.000	19.111 / 50
13.000	19.111 / 51
3936.000	/ 52
743.000	595.000 559.000 / 1
743.000	595.000 559.000 / 2
743.000	595.000 559.000 / 3
743.000	595.000 559.000 / 4
743.000	595.000 559.000 / 5
743.000	595.000 559.000 / 6
743.000	595.000 559.000 / 7
743.000	595.000 559.000 / 8
743.000	595.000 559.000 / 9
743.000	595.000 559.000 / 10
743.000	595.000 559.000 / 11
743.000	595.000 559.000 / 12
3(300.0)	/ 13

743.000	595.000	559.000	/	14
743.000	595.000	559.000	/	15
743.000	595.000	559.000	/	16
743.000	595.000	559.000	/	17
743.000	595.000	559.000	/	18
743.000	595.000	559.000	/	19
743.000	595.000	559.000	/	20
743.000	595.000	559.000	/	21
743.000	595.000	559.000	/	22
743.000	595.000	559.000	/	23
743.000	595.000	559.000	/	24
743.000	595.000	559.000	/	25
3(300.0)			/	26
743.000	595.000	559.000	/	27
743.000	595.000	559.000	/	28
743.000	595.000	559.000	/	29
743.000	595.000	559.000	/	30
743.000	595.000	559.000	/	31
743.000	595.000	559.000	/	32
743.000	595.000	559.000	/	33
743.000	595.000	559.000	/	34
743.000	595.000	559.000	/	35
743.000	595.000	559.000	/	36
743.000	595.000	559.000	/	37
743.000	595.000	559.000	/	38
3(300.0)			/	39
743.000	595.000	559.000	/	40
743.000	595.000	559.000	/	41
743.000	595.000	559.000	/	42
743.000	595.000	559.000	/	43
743.000	595.000	559.000	/	44
743.000	595.000	559.000	/	45
743.000	595.000	559.000	/	46
743.000	595.000	559.000	/	47
743.000	595.000	559.000	/	48
743.000	595.000	559.000	/	49
743.000	595.000	559.000	/	50
743.000	595.000	559.000	/	51
3(300.0)			/	52
1 0 0 0 0 0 0 14(0.0)		/	1 result control
1 0 0 0 0 0 0 14(0.0)		/	2 result control
1 0 0 0 0 0 0 14(0.0)		/	3 result control
1 0 0 0 0 0 0 14(0.0)		/	4 result control
1 0 0 0 0 0 0 14(0.0)		/	5 result control
1 0 0 0 0 0 0 14(0.0)		/	6 result control
1 0 0 0 0 0 0 14(0.0)		/	7 result control
1 0 0 0 0 0 0 14(0.0)		/	8 result control
1 0 0 0 0 0 0 14(0.0)		/	9 result control
1 0 0 0 0 0 0 14(0.0)		/	10 result control
1 0 0 0 0 0 0 14(0.0)		/	11 result control
1 0 0 0 0 0 0 14(0.0)		/	12 result control
1 0 0 0 0 0 0 14(0.0)		/	13 result control
1 0 0 0 0 0 0 14(0.0)		/	14 result control
1 0 0 0 0 0 0 14(0.0)		/	15 result control
1 0 0 0 0 0 0 14(0.0)		/	16 result control
1 0 0 0 0 0 0 14(0.0)		/	17 result control
1 0 0 0 0 0 0 14(0.0)		/	18 result control
1 0 0 0 0 0 0 14(0.0)		/	19 result control
1 0 0 0 0 0 0 14(0.0)		/	20 result control
1 0 0 0 0 0 0 14(0.0)		/	21 result control
1 0 0 0 0 0 0 14(0.0)		/	22 result control
1 0 0 0 0 0 0 14(0.0)		/	23 result control
1 0 0 0 0 0 0 14(0.0)		/	24 result control
1 0 0 0 0 0 0 14(0.0)		/	25 result control
1 0 0 0 0 0 0 14(0.0)		/	26 result control
1 0 0 0 0 0 0 14(0.0)		/	27 result control
1 0 0 0 0 0 0 14(0.0)		/	28 result control
1 0 0 0 0 0 0 14(0.0)		/	29 result control
1 0 0 0 0 0 0 14(0.0)		/	30 result control
1 0 0 0 0 0 0 14(0.0)		/	31 result control
1 0 0 0 0 0 0 14(0.0)		/	32 result control
1 0 0 0 0 0 0 14(0.0)		/	33 result control
1 0 0 0 0 0 0 14(0.0)		/	34 result control
1 0 0 0 0 0 0 14(0.0)		/	35 result control
1 0 0 0 0 0 0 14(0.0)		/	36 result control
1 0 0 0 0 0 0 14(0.0)		/	37 result control
1 0 0 0 0 0 0 14(0.0)		/	38 result control
1 0 0 0 0 0 0 14(0.0)		/	39 result control
1 0 0 0 0 0 0 14(0.0)		/	40 result control

```
1 0 0 0 0 0 14( 0.0) / 41 result control
1 0 0 0 0 0 14( 0.0) / 42 result control
1 0 0 0 0 0 14( 0.0) / 43 result control
1 0 0 0 0 0 14( 0.0) / 44 result control
1 0 0 0 0 0 14( 0.0) / 45 result control
1 0 0 0 0 0 14( 0.0) / 46 result control
1 0 0 0 0 0 14( 0.0) / 47 result control
1 0 0 0 0 0 14( 0.0) / 48 result control
1 0 0 0 0 0 14( 0.0) / 49 result control
1 0 0 0 0 0 14( 0.0) / 50 result control
1 0 0 0 0 0 14( 0.0) / 51 result control
1 0 0 0 0 0 14( 0.0) / 52 result control
0 / PWR
52( 0.000) / void ratio (%)
12(-0.7E-03) 1(-0.7E-03)
12(-0.2E-03) 1(-0.2E-03)
12(-0.7E-03) 1(-0.7E-03)
12(-0.2E-03) 1(-0.2E-03)
0 /xs val.
0 /branching
0 /weight factor
```

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```
===== PDS FILE ALOCATION =====
FASTP : pfast
THERMP : pthml
FASTU : fastu
THERMU : thermalu
MACWRK : macrowrk
FLUX : flux
MACRO : macro
MCROSSP: pmcrs
MICREF : micref
UMCROS : umcros
===== for libmak =====
usacti ./home5/codes/swat9906/xslib/acti.j32.v2.1
usfp ./home5/codes/swat9906/xslib/fp.j32.v2.4
ori2ori./home5/codes/swat9906/origlib/decadaydat.fp-j3.v7
===== for origin2 =====
photo ./home5/codes/swat9906/origlib/photodat
***** global data lists *****
Template of SWAT Input Data for The Obrigheim Reactor By SHIN, Hee Sung
ob1 14 180 25.929 3.1300 1.4300 295.60 -1.00 0.7283 0.9300 0.6413 0.6845
1 1 1 0 0 0 0 1 1 1 / Library Control
1 1 1 1 2 1 4 3 -2 1 0 0 0 0 2 0 1 0 0 0 / SRAC General Control
1.0000E-25
63 44 1 /fast thermal letherry
3 3 3 3 3 0 3 0 0 0 0 0 8 15 0 0 30 0 1 /COL.PROB.CONT
1 2 3
0.00000 0.45650 0.53700 0.83807
1
3
67 1 0 0 0 4 4(0) 1.0 0.913 0.0 10.05000 3.130 0.0 4(0.0) / UO2 (3.130wt%)
922340 2 1 0 0 1 2 / U -234
922350 2 1 0 0 1 2 / U -235
922360 2 1 0 0 1 2 / U -236
922380 2 1 0 0 1 2 / U -238
932370 2 1 0 0 1 0
942380 2 1 0 0 1 0
942390 2 1 0 0 1 0
942400 2 1 0 0 1 0
942410 2 1 0 0 1 0
942420 2 1 0 0 1 0
952410 2 1 0 0 1 0
952421 2 1 3 0 1 0
952420 2 1 2 0 1 0
952430 2 1 0 0 1 0
962420 2 1 0 0 1 0
962430 2 1 0 0 1 0
962440 2 1 0 0 1 0
962450 2 1 0 0 1 0
962460 2 1 0 0 1 0
641520 2 1 0 0 1 0
641540 2 1 0 0 1 0
641550 2 1 0 0 1 0
641560 2 1 0 0 1 0
641570 2 1 0 0 1 0
641580 2 1 0 0 1 0
641600 2 1 0 0 1 0
541350 2 1 0 0 1 0
601430 2 1 0 0 1 0
451030 2 1 0 0 1 0
541310 2 1 0 0 1 0
551330 2 1 0 0 1 0
621490 2 1 0 0 1 0
430990 2 1 0 0 1 0
621520 2 1 0 0 1 0
621510 2 1 0 0 1 0
611470 2 1 0 0 1 0
631530 2 1 0 0 1 0
601450 2 1 0 0 1 0
631550 2 1 0 0 1 0
631540 2 1 0 0 1 0
621500 2 1 0 0 1 0
420950 2 1 0 0 1 0
471090 2 1 0 0 1 0
611481 2 1 3 0 1 0
441010 2 1 0 0 1 0
551340 2 1 0 0 1 0
461050 2 1 0 0 1 0
611480 2 1 2 0 1 0
451050 2 1 0 0 1 0
```

591410 2 1 0 0 0 1 0
 360830 2 1 0 0 1 0
 461080 2 1 0 0 1 0
 621470 2 1 0 0 1 0
 461070 2 1 0 0 1 0
 420970 2 1 0 0 1 0
 481130 2 1 0 0 1 0
 551350 2 1 0 0 1 0
 420980 2 1 0 0 1 0
 541330 2 1 0 0 1 0
 491150 2 1 0 0 1 0
 591430 2 1 0 0 1 0
 631560 2 1 0 0 1 0
 441030 2 1 0 0 1 0
 621480 2 1 0 0 1 0
 601470 2 1 0 0 1 0
 611490 2 1 0 0 1 0
 80160 0 0 0 0 0 1
 922340 300.00
 922350 31300.00
 922360 140.00
 922380 968259.94
 4.64956E-02 / O-16 constant density
 3 9(0) 0.0 0.29787 8(0.0)
 400000 2 1 1 0 0 1 / Zr
 260000 2 1 1 0 0 1 / Fe
 240000 2 1 1 0 0 1 / Cr
 4.2982E-02 1.4838E-04 7.5891E-05 / Zr,Fe,Cr
 4 0 1 7(0) 0.0 0.98796 8(0.0)
 10010 2 1 0 9 0 1 / H-1
 80160 2 1 0 0 0 1 / O-16
 50100 2 1 0 0 0 1 / B-10
 50110 2 1 0 0 0 1 / B-11
 4(1.0E-2) /
 1 0
 1
 39 12
 12(2) 1 12(2) 1 12(2) 1
 3 4 / 1
 3 4 / 2
 3 4 / 3
 3 4 / 4
 3 4 / 5
 3 4 / 6
 3 4 / 7
 3 4 / 8
 3 4 / 9
 3 4 / 10
 3 4 / 11
 3 4 / 12
 4 / 13
 3 4 / 14
 3 4 / 15
 3 4 / 16
 3 4 / 17
 3 4 / 18
 3 4 / 19
 3 4 / 20
 3 4 / 21
 3 4 / 22
 3 4 / 23
 3 4 / 24
 3 4 / 25
 4 / 26
 3 4 / 27
 3 4 / 28
 3 4 / 29
 3 4 / 30
 3 4 / 31
 3 4 / 32
 3 4 / 33
 3 4 / 34
 3 4 / 35
 3 4 / 36
 3 4 / 37
 3 4 / 38
 4 / 39
 12(1) 0 12(1) 0 12(1) 0
 24.000 20.929 / 1

24.000	20.929	/	2	
24.000	20.929	/	3	
24.000	20.929	/	4	
24.000	20.929	/	5	
24.000	20.929	/	6	
24.000	20.929	/	7	
24.000	20.929	/	8	
24.000	20.929	/	9	
24.000	20.929	/	10	
24.000	20.929	/	11	
24.000	20.929	/	12	
81.000		/	13	
25.750	37.468	/	14	
25.750	37.468	/	15	
25.750	37.468	/	16	
25.750	37.468	/	17	
25.750	37.468	/	18	
25.750	37.468	/	19	
25.750	37.468	/	20	
25.750	37.468	/	21	
25.750	37.468	/	22	
25.750	37.468	/	23	
25.750	37.468	/	24	
25.750	37.468	/	25	
396.000		/	26	
20.667	33.564	/	27	
20.667	33.564	/	28	
20.667	33.564	/	29	
20.667	33.564	/	30	
20.667	33.564	/	31	
20.667	33.564	/	32	
20.667	33.564	/	33	
20.667	33.564	/	34	
20.667	33.564	/	35	
20.667	33.564	/	36	
20.667	33.564	/	37	
20.667	33.564	/	38	
10.000		/	39	
846.000	605.000	572.000	/	1
846.000	605.000	572.000	/	2
846.000	605.000	572.000	/	3
846.000	605.000	572.000	/	4
846.000	605.000	572.000	/	5
846.000	605.000	572.000	/	6
846.000	605.000	572.000	/	7
846.000	605.000	572.000	/	8
846.000	605.000	572.000	/	9
846.000	605.000	572.000	/	10
846.000	605.000	572.000	/	11
846.000	605.000	572.000	/	12
3(300.0)		/	13	
846.000	605.000	572.000	/	14
846.000	605.000	572.000	/	15
846.000	605.000	572.000	/	16
846.000	605.000	572.000	/	17
846.000	605.000	572.000	/	18
846.000	605.000	572.000	/	19
846.000	605.000	572.000	/	20
846.000	605.000	572.000	/	21
846.000	605.000	572.000	/	22
846.000	605.000	572.000	/	23
846.000	605.000	572.000	/	24
846.000	605.000	572.000	/	25
3(300.0)		/	26	
846.000	605.000	572.000	/	27
846.000	605.000	572.000	/	28
846.000	605.000	572.000	/	29
846.000	605.000	572.000	/	30
846.000	605.000	572.000	/	31
846.000	605.000	572.000	/	32
846.000	605.000	572.000	/	33
846.000	605.000	572.000	/	34
846.000	605.000	572.000	/	35
846.000	605.000	572.000	/	36
846.000	605.000	572.000	/	37
846.000	605.000	572.000	/	38
3(300.0)		/	39	
1 0 0 0 0 0 0 14(0.0)		/	1 result control	
1 0 0 0 0 0 0 14(0.0)		/	2 result control	

```

1 0 0 0 0 0 14( 0.0) / 3 result control
1 0 0 0 0 0 14( 0.0) / 4 result control
1 0 0 0 0 0 14( 0.0) / 5 result control
1 0 0 0 0 0 14( 0.0) / 6 result control
1 0 0 0 0 0 14( 0.0) / 7 result control
1 0 0 0 0 0 14( 0.0) / 8 result control
1 0 0 0 0 0 14( 0.0) / 9 result control
1 0 0 0 0 0 14( 0.0) / 10 result control
1 0 0 0 0 0 14( 0.0) / 11 result control
1 0 0 0 0 0 14( 0.0) / 12 result control
1 0 0 0 0 0 14( 0.0) / 13 result control
1 0 0 0 0 0 14( 0.0) / 14 result control
1 0 0 0 0 0 14( 0.0) / 15 result control
1 0 0 0 0 0 14( 0.0) / 16 result control
1 0 0 0 0 0 14( 0.0) / 17 result control
1 0 0 0 0 0 14( 0.0) / 18 result control
1 0 0 0 0 0 14( 0.0) / 19 result control
1 0 0 0 0 0 14( 0.0) / 20 result control
1 0 0 0 0 0 14( 0.0) / 21 result control
1 0 0 0 0 0 14( 0.0) / 22 result control
1 0 0 0 0 0 14( 0.0) / 23 result control
1 0 0 0 0 0 14( 0.0) / 24 result control
1 0 0 0 0 0 14( 0.0) / 25 result control
1 0 0 0 0 0 14( 0.0) / 26 result control
1 0 0 0 0 0 14( 0.0) / 27 result control
1 0 0 0 0 0 14( 0.0) / 28 result control
1 0 0 0 0 0 14( 0.0) / 29 result control
1 0 0 0 0 0 14( 0.0) / 30 result control
1 0 0 0 0 0 14( 0.0) / 31 result control
1 0 0 0 0 0 14( 0.0) / 32 result control
1 0 0 0 0 0 14( 0.0) / 33 result control
1 0 0 0 0 0 14( 0.0) / 34 result control
1 0 0 0 0 0 14( 0.0) / 35 result control
1 0 0 0 0 0 14( 0.0) / 36 result control
1 0 0 0 0 0 14( 0.0) / 37 result control
1 0 0 0 0 0 14( 0.0) / 38 result control
1 0 0 0 0 0 14( 0.0) / 39 result control
0 / PWR
39( 0.000) / void ratio (%)
12(-0.4E-03) 1(-0.4E-03)
12(-0.4E-03) 1(-0.4E-03)
12(-0.4E-03) 1(-0.4E-03)
0 /xs val.
0 /branching
0 /weight factor

```

A.3.7. SWAT input for Obrigheim-b Sample NO 1.

```
===== PDS FILE ALOCATION =====
FASTP : pfast
THERMP : pthml
FASTU : fastu
THERMU : thermalu
MACWRK : macrowrk
FLUX : flux
MACRO : macro
MCROSSP: pmcrs
MICREF : micref
UMCROS : umcros
===== for libmak =====
usacti :/home5/codes/swat9906/xslib/acti.j32.v2.1
usfp :/home5/codes/swat9906/xslib/fp.j32.v2.4
ori2ori:/home5/codes/swat9906/ori2origlib/decaydat.fp-j3.v7
===== for origin2 =====
photo :/home5/codes/swat9906/ori2origlib/photodat
***** global data lists *****
Template of SWAT Input Data for The Obrigheim Reactor By SHIN, Hee Sung
ob1 14 180 25.929 3.1300 1.4300 295.60 -1.00 0.7283 0.9300 0.6413 0.6845
1 1 1 0 0 0 0 1 1 1 / Library Control
1 1 1 1 2 1 4 3 -2 1 0 0 0 0 2 0 1 0 0 0 / SRAC General Control
1.0000E-25
63 44 1 /fast thermal lethergy
3 3 3 3 3 0 3 0 0 0 0 0 8 15 0 0 30 0 1 /COL.PROB.CONT
1 2 3
0.00000 0.45650 0.53700 0.83807
1
3
67 1 0 0 0 4 4(0) 1.0 0.913 0.0 10.05000 3.130 0.0 4(0.0) / UO2 (3.130wt%)
922340 2 1 0 0 1 2 / U -234
922350 2 1 0 0 1 2 / U -235
922360 2 1 0 0 1 2 / U -236
922380 2 1 0 0 1 2 / U -238
932370 2 1 0 0 1 0
942380 2 1 0 0 1 0
942390 2 1 0 0 1 0
942400 2 1 0 0 1 0
942410 2 1 0 0 1 0
942420 2 1 0 0 1 0
952410 2 1 0 0 1 0
952421 2 1 3 0 1 0
952420 2 1 2 0 1 0
952430 2 1 0 0 1 0
962420 2 1 0 0 1 0
962430 2 1 0 0 1 0
962440 2 1 0 0 1 0
962450 2 1 0 0 1 0
962460 2 1 0 0 1 0
641520 2 1 0 0 1 0
641540 2 1 0 0 1 0
641550 2 1 0 0 1 0
641560 2 1 0 0 1 0
641570 2 1 0 0 1 0
641580 2 1 0 0 1 0
641600 2 1 0 0 1 0
541350 2 1 0 0 1 0
601430 2 1 0 0 1 0
451030 2 1 0 0 1 0
541310 2 1 0 0 1 0
551330 2 1 0 0 1 0
621490 2 1 0 0 1 0
430990 2 1 0 0 1 0
621520 2 1 0 0 1 0
621510 2 1 0 0 1 0
611470 2 1 0 0 1 0
631530 2 1 0 0 1 0
601450 2 1 0 0 1 0
631550 2 1 0 0 1 0
631540 2 1 0 0 1 0
621500 2 1 0 0 1 0
420950 2 1 0 0 1 0
471090 2 1 0 0 1 0
611481 2 1 3 0 1 0
441010 2 1 0 0 1 0
551340 2 1 0 0 1 0
461050 2 1 0 0 1 0
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611480 2 1 2 0 1 0
 451050 2 1 0 0 1 0
 591410 2 1 0 0 1 0
 360830 2 1 0 0 1 0
 461080 2 1 0 0 1 0
 621470 2 1 0 0 1 0
 461070 2 1 0 0 1 0
 420970 2 1 0 0 1 0
 481130 2 1 0 0 1 0
 551350 2 1 0 0 1 0
 420980 2 1 0 0 1 0
 541330 2 1 0 0 1 0
 491150 2 1 0 0 1 0
 591430 2 1 0 0 1 0
 631560 2 1 0 0 1 0
 441030 2 1 0 0 1 0
 621480 2 1 0 0 1 0
 601470 2 1 0 0 1 0
 611490 2 1 0 0 1 0
 80160 0 0 0 0 0 1
 922340 300.00
 922350 31300.00
 922360 140.00
 922380 968259.94
 4.64956E-02 / O-16 constant density
 3 9(0) 0.0 0.29787 8(0.0)
 400000 2 1 1 0 0 1 / Zr
 260000 2 1 1 0 0 1 / Fe
 240000 2 1 1 0 0 1 / Cr
 4.2982E-02 1.4838E-04 7.5891E-05 / Zr,Fe,Cr
 4 0 1 7(0) 0.0 0.98796 8(0.0)
 10010 2 1 0 9 0 1 / H-1
 80160 2 1 0 0 0 1 / O-16
 50100 2 1 0 0 0 1 / B-10
 50110 2 1 0 0 0 1 / B-11
 4(1.0E-2) /
 1 0
 1
 39 12
 12(2) 1 12(2) 1 12(2) 1
 3 4 / 1
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 3 4 / 37
 3 4 / 38
 4 / 39

12(1)	0	12(1)	0	12(1)	0
24.000	20.929	/	1		
24.000	20.929	/	2		
24.000	20.929	/	3		
24.000	20.929	/	4		
24.000	20.929	/	5		
24.000	20.929	/	6		
24.000	20.929	/	7		
24.000	20.929	/	8		
24.000	20.929	/	9		
24.000	20.929	/	10		
24.000	20.929	/	11		
24.000	20.929	/	12		
81.000	/	13			
25.750	37.468	/	14		
25.750	37.468	/	15		
25.750	37.468	/	16		
25.750	37.468	/	17		
25.750	37.468	/	18		
25.750	37.468	/	19		
25.750	37.468	/	20		
25.750	37.468	/	21		
25.750	37.468	/	22		
25.750	37.468	/	23		
25.750	37.468	/	24		
25.750	37.468	/	25		
396.000	/	26			
20.667	33.564	/	27		
20.667	33.564	/	28		
20.667	33.564	/	29		
20.667	33.564	/	30		
20.667	33.564	/	31		
20.667	33.564	/	32		
20.667	33.564	/	33		
20.667	33.564	/	34		
20.667	33.564	/	35		
20.667	33.564	/	36		
20.667	33.564	/	37		
20.667	33.564	/	38		
10.000	/	39			
846.000	605.000	572.000	/	1	
846.000	605.000	572.000	/	2	
846.000	605.000	572.000	/	3	
846.000	605.000	572.000	/	4	
846.000	605.000	572.000	/	5	
846.000	605.000	572.000	/	6	
846.000	605.000	572.000	/	7	
846.000	605.000	572.000	/	8	
846.000	605.000	572.000	/	9	
846.000	605.000	572.000	/	10	
846.000	605.000	572.000	/	11	
846.000	605.000	572.000	/	12	
3(-300.0)	/	13			
846.000	605.000	572.000	/	14	
846.000	605.000	572.000	/	15	
846.000	605.000	572.000	/	16	
846.000	605.000	572.000	/	17	
846.000	605.000	572.000	/	18	
846.000	605.000	572.000	/	19	
846.000	605.000	572.000	/	20	
846.000	605.000	572.000	/	21	
846.000	605.000	572.000	/	22	
846.000	605.000	572.000	/	23	
846.000	605.000	572.000	/	24	
846.000	605.000	572.000	/	25	
3(-300.0)	/	26			
846.000	605.000	572.000	/	27	
846.000	605.000	572.000	/	28	
846.000	605.000	572.000	/	29	
846.000	605.000	572.000	/	30	
846.000	605.000	572.000	/	31	
846.000	605.000	572.000	/	32	
846.000	605.000	572.000	/	33	
846.000	605.000	572.000	/	34	
846.000	605.000	572.000	/	35	
846.000	605.000	572.000	/	36	
846.000	605.000	572.000	/	37	
846.000	605.000	572.000	/	38	
3(-300.0)	/	39			

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1 0 0 0 0 0 14( 0.0) / 1 result control
1 0 0 0 0 0 14( 0.0) / 2 result control
1 0 0 0 0 0 14( 0.0) / 3 result control
1 0 0 0 0 0 14( 0.0) / 4 result control
1 0 0 0 0 0 14( 0.0) / 5 result control
1 0 0 0 0 0 14( 0.0) / 6 result control
1 0 0 0 0 0 14( 0.0) / 7 result control
1 0 0 0 0 0 14( 0.0) / 8 result control
1 0 0 0 0 0 14( 0.0) / 9 result control
1 0 0 0 0 0 14( 0.0) / 10 result control
1 0 0 0 0 0 14( 0.0) / 11 result control
1 0 0 0 0 0 14( 0.0) / 12 result control
1 0 0 0 0 0 14( 0.0) / 13 result control
1 0 0 0 0 0 14( 0.0) / 14 result control
1 0 0 0 0 0 14( 0.0) / 15 result control
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1 0 0 0 0 0 14( 0.0) / 17 result control
1 0 0 0 0 0 14( 0.0) / 18 result control
1 0 0 0 0 0 14( 0.0) / 19 result control
1 0 0 0 0 0 14( 0.0) / 20 result control
1 0 0 0 0 0 14( 0.0) / 21 result control
1 0 0 0 0 0 14( 0.0) / 22 result control
1 0 0 0 0 0 14( 0.0) / 23 result control
1 0 0 0 0 0 14( 0.0) / 24 result control
1 0 0 0 0 0 14( 0.0) / 25 result control
1 0 0 0 0 0 14( 0.0) / 26 result control
1 0 0 0 0 0 14( 0.0) / 27 result control
1 0 0 0 0 0 14( 0.0) / 28 result control
1 0 0 0 0 0 14( 0.0) / 29 result control
1 0 0 0 0 0 14( 0.0) / 30 result control
1 0 0 0 0 0 14( 0.0) / 31 result control
1 0 0 0 0 0 14( 0.0) / 32 result control
1 0 0 0 0 0 14( 0.0) / 33 result control
1 0 0 0 0 0 14( 0.0) / 34 result control
1 0 0 0 0 0 14( 0.0) / 35 result control
1 0 0 0 0 0 14( 0.0) / 36 result control
1 0 0 0 0 0 14( 0.0) / 37 result control
1 0 0 0 0 0 14( 0.0) / 38 result control
1 0 0 0 0 0 14( 0.0) / 39 result control

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0 / PWR
 39(0.000) / void ratio (%)

12(-0.4E-03) 1(-0.4E-03)
 12(-0.4E-03) 1(-0.4E-03)
 12(-0.4E-03) 1(-0.4E-03)

0 /xs val.

0 /branching

0 /weight factor

comment statement

0 h2ofrac

9 light element inclued in fresh fuel

o 135.000

cr 5.90000

mn 0.330000

fe 12.9000

co 0.750000E-01

ni 9.90000

zr 221.000

nb 0.710000

sn 3.60000

A.4. Relative Errors of the Calculated Compositions for 26 Obrigheim Samples Using SAS2H with 27, 44 and 238 g and SWAT with 107 g

26 U-235

exp. data	SAS-27G	SAS-44G	SAS-238G	SWAT	Enrich.	Burnup	z-locat.	Sample Id
1.370E+04	-8.759	-8.759	-7.737	-8.832	3.000	21.170	150.000	or1
6.930E+03	0.043	-0.303	2.756	-0.216	3.000	33.750	1435.000	or2
1.280E+04	2.109	2.109	2.969	2.031	3.000	20.180	150.000	or3
8.440E+03	-23.152	-23.709	-21.481	-25.616	3.000	35.100	315.000	or4
6.090E+03	0.722	-0.049	3.415	-0.263	3.000	36.260	1435.000	or5
7.480E+03	6.818	6.818	9.332	9.064	3.000	30.890	2315.000	or6
7.840E+03	1.620	1.620	4.018	3.814	3.000	30.940	2315.000	or7
1.190E+04	-2.437	-2.269	-1.092	-0.420	3.000	22.860	2585.000	or8
1.520E+04	-1.974	-1.842	-1.184	-1.645	3.000	17.130	150.000	or9
1.440E+04	-18.889	-18.889	-17.917	-19.167	3.000	22.700	150.000	or10
1.080E+04	-6.204	-6.389	-4.907	-6.944	3.000	25.830	315.000	or11
7.610E+03	1.905	1.603	4.074	1.787	3.000	31.500	1435.000	or12
7.500E+03	5.280	4.973	7.480	5.147	3.000	31.140	1435.000	or13
1.010E+04	-8.089	-7.861	-6.228	-6.099	3.000	27.710	2315.000	or14
1.010E+04	0.495	0.792	2.376	2.772	3.000	25.810	2585.000	or15
1.570E+04	1.338	1.338	1.911	1.720	3.000	15.600	150.000	or16
8.780E+03	-2.301	-2.301	-0.159	-1.970	3.000	29.360	1435.000	or17
1.030E+04	2.718	2.913	4.466	4.757	3.000	24.900	2315.000	or18
5.050E+03	-3.663	-4.594	-0.871	-5.743	2.830	38.100	1328.000	or19
4.410E+03	17.234	16.712	20.975	15.488	2.830	36.880	1328.000	or20
4.950E+03	11.576	11.576	15.374	13.798	2.830	35.640	2206.000	or21
6.270E+03	16.571	16.938	19.569	19.522	2.830	30.160	2426.000	or22
8.940E+03	9.351	9.620	11.454	11.857	2.830	24.220	2547.000	or23
1.000E+04	-7.880	-8.110	-6.470	-8.830	2.830	25.450	150.000	or24
4.860E+03	7.840	6.872	10.741	6.008	2.830	36.670	1328.000	or25
5.040E+03	26.369	26.369	30.099	28.849	2.830	32.900	2206.000	or26
err-avg	1.10	0.968	3.19	1.57				
err-sd	10.5	10.6	11.2	11.4				

26 U-236

exp. data	SAS-27G	SAS-44G	SAS-238G	SWAT	Enrich.	Burnup	z-locat.	Sample Id
2.990E+03	1.037	1.037	0.234	-3.779	3.000	21.170	150.000	or1
4.060E+03	-6.404	-6.404	-6.995	-10.616	3.000	33.750	1435.000	or2
2.820E+03	4.610	3.759	3.759	-0.993	3.000	20.180	150.000	or3
3.770E+03	2.042	2.042	1.406	-2.149	3.000	35.100	315.000	or4
4.120E+03	-5.485	-5.485	-6.068	-9.733	3.000	36.260	1435.000	or5
3.830E+03	-3.864	-3.864	-4.491	-8.721	3.000	30.890	2315.000	or6
3.910E+03	-5.831	-5.831	-6.445	-10.537	3.000	30.940	2315.000	or7
3.620E+03	-12.652	-12.652	-13.287	-17.127	3.000	22.860	2585.000	or8
2.920E+03	-9.486	-9.486	-10.274	-14.212	3.000	17.130	150.000	or9
2.930E+03	7.918	7.918	7.133	2.389	3.000	22.700	150.000	or10
3.850E+03	-12.338	-12.338	-12.961	-16.260	3.000	25.830	315.000	or11
3.940E+03	-5.964	-5.964	-6.548	-10.330	3.000	31.500	1435.000	or12
3.980E+03	-7.487	-7.487	-8.090	-11.658	3.000	31.140	1435.000	or13
4.050E+03	-13.753	-13.753	-14.346	-17.877	3.000	27.710	2315.000	or14
3.600E+03	-6.250	-6.250	-6.917	-10.889	3.000	25.810	2585.000	or15
2.730E+03	-9.231	-9.231	-10.110	-14.066	3.000	15.600	150.000	or16
3.810E+03	-5.853	-5.853	-6.457	-10.052	3.000	29.360	1435.000	or17
3.600E+03	-7.556	-8.222	-8.222	-12.556	3.000	24.900	2315.000	or18
3.890E+03	-4.139	-3.548	-4.139	-7.763	2.830	38.100	1328.000	or19
3.870E+03	-4.264	-4.264	-4.264	-8.036	2.830	36.880	1328.000	or20

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3.950E+03	-6.785	-6.785	-7.392	-11.013	2.830	35.640	2206.000	or21
3.660E+03	-5.219	-5.219	-5.219	-9.508	2.830	30.160	2426.000	or22
3.330E+03	-5.736	-5.736	-6.456	-10.360	2.830	24.220	2547.000	or23
3.220E+03	0.404	0.404	-0.311	-4.379	2.830	25.450	150.000	or24
3.860E+03	-4.016	-4.016	-4.016	-7.953	2.830	36.670	1328.000	or25
3.820E+03	-6.099	-6.099	-6.702	-10.314	2.830	32.900	2206.000	or26
err-avg	-5.09	-5.13	-5.66	-9.56				
err-sd	5.01	4.97	5.00	4.80				

26 U-238

exp. data	SAS-27G	SAS-44G	SAS-238G	SWAT	Enrich.	Burnup	z-locat.	Sample Id
9.540E+05	0.042	0.042	0.042	0.136	3.000	21.170	150.000	or1
9.450E+05	-0.265	-0.265	-0.265	-0.053	3.000	33.750	1435.000	or2
9.570E+05	-0.272	-0.272	-0.272	-0.104	3.000	20.180	150.000	or3
9.420E+05	0.053	0.053	0.053	0.170	3.000	35.100	315.000	or4
9.430E+05	-0.308	-0.308	-0.308	-0.085	3.000	36.260	1435.000	or5
9.480E+05	-0.327	-0.327	-0.327	-0.148	3.000	30.890	2315.000	or6
9.460E+05	-0.116	-0.116	-0.116	0.063	3.000	30.940	2315.000	or7
9.530E+05	-0.105	-0.105	-0.105	0.031	3.000	22.860	2585.000	or8
9.580E+05	-0.125	-0.125	-0.125	0.031	3.000	17.130	150.000	or9
9.520E+05	0.000	0.000	0.000	0.221	3.000	22.700	150.000	or10
9.510E+05	-0.147	-0.147	-0.147	0.053	3.000	25.830	315.000	or11
9.470E+05	-0.222	-0.222	-0.222	-0.063	3.000	31.500	1435.000	or12
9.460E+05	-0.116	-0.116	-0.116	0.085	3.000	31.140	1435.000	or13
9.480E+05	0.169	0.169	-0.084	0.148	3.000	27.710	2315.000	or14
9.500E+05	-0.042	-0.042	-0.042	0.095	3.000	25.810	2585.000	or15
9.590E+05	0.010	0.010	0.010	0.052	3.000	15.600	150.000	or16
9.480E+05	-0.084	-0.084	-0.084	0.032	3.000	29.360	1435.000	or17
9.510E+05	0.105	0.105	-0.147	0.074	3.000	24.900	2315.000	or18
9.420E+05	-0.202	-0.202	-0.202	-0.053	2.830	38.100	2328.000	or19
9.430E+05	-0.308	-0.053	-0.308	-0.032	2.830	36.880	2328.000	or20
9.450E+05	-0.265	-0.265	-0.265	-0.169	2.830	35.640	2206.000	or21
9.510E+05	-0.400	-0.400	-0.400	-0.284	2.830	30.160	2426.000	or22
9.550E+05	-0.314	-0.314	-0.314	-0.168	2.830	24.220	2547.000	or23
9.530E+05	-0.105	-0.105	-0.105	0.010	2.830	25.450	150.000	or24
9.440E+05	-0.159	-0.159	-0.159	-0.117	2.830	36.670	1328.000	or25
9.470E+05	-0.222	-0.222	-0.222	-0.116	2.830	32.900	2206.000	or26
err-avg	-0.143	-0.133	-0.163	-0.736E-02				
err-sd	0.147	0.144	0.122	0.121				

26 Pu-238

exp. data	SAS-27G	SAS-44G	SAS-238G	SWAT	Enrich.	Burnup	z-locat.	Sample Id
3.600E+01	49.417	39.500	38.167	9.333	3.000	21.170	150.000	or1
1.560E+02	-1.154	-6.923	-8.141	-22.564	3.000	33.750	1435.000	or2
4.100E+01	17.268	9.122	8.561	-14.634	3.000	20.180	150.000	or3
1.040E+02	61.346	51.250	49.231	22.788	3.000	35.100	315.000	or4
1.650E+02	8.788	2.242	0.970	-14.545	3.000	36.260	1435.000	or5
1.250E+02	1.840	-4.000	-5.200	-18.000	3.000	30.890	2315.000	or6
1.030E+02	24.078	16.893	15.534	-0.194	3.000	30.940	2315.000	or7
6.200E+01	4.032	-2.500	-3.258	-17.548	3.000	22.860	2585.000	or8
3.100E+01	5.194	-2.484	-3.258	-24.710	3.000	17.130	150.000	or9
3.900E+01	62.333	51.333	50.128	19.538	3.000	22.700	150.000	or10
7.900E+01	8.152	0.924	0.025	-19.481	3.000	25.830	315.000	or11
1.380E+02	-3.623	-9.493	-10.507	-24.855	3.000	31.500	1435.000	or12
1.450E+02	-10.552	-15.931	-16.966	-30.345	3.000	31.140	1435.000	or13
1.060E+02	-5.472	-11.311	-12.208	-24.566	3.000	27.710	2315.000	or14
7.900E+01	7.848	1.228	0.316	-13.671	3.000	25.810	2585.000	or15

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2.500E+01	3.760	-3.840	-4.800	-26.080	3.000	15.600	150.000	or16
1.070E+02	6.542	-0.093	-1.028	-17.374	3.000	29.360	1435.000	or17
7.600E+01	3.342	-2.921	-3.855	-18.079	3.000	24.900	2315.000	or18
1.900E+02	9.737	2.947	1.579	-13.579	2.830	38.100	1328.000	or19
1.390E+02	40.576	31.871	30.288	10.576	2.830	36.880	1328.000	or20
1.590E+02	14.654	7.925	6.604	-7.107	2.830	35.640	2206.000	or21
1.140E+02	12.544	5.877	4.561	-9.035	2.830	30.160	2426.000	or22
6.500E+01	21.200	13.508	12.415	-3.292	2.830	24.220	2547.000	or23
6.500E+01	35.477	26.323	25.231	1.169	2.830	25.450	150.000	or24
1.690E+02	14.379	7.337	5.917	-10.118	2.830	36.670	1328.000	or25
1.260E+02	22.619	15.238	13.889	-1.032	2.830	32.900	2206.000	or26
err-avg	15.9	8.62	7.47	-10.3				
err-sd	19.4	18.0	17.8	14.1				

26 Pu-239

exp. data	SAS-27G	SAS-44G	SAS-238G	SWAT	Enrich.	Burnup	z-locat.	Sample Id
4.350E+03	17.586	13.724	16.483	7.356	3.000	21.170	150.000	or1
5.020E+03	11.414	6.175	9.502	2.849	3.000	33.750	1435.000	or2
4.280E+03	17.827	13.925	16.706	7.617	3.000	20.180	150.000	or3
4.620E+03	21.580	16.905	20.541	9.697	3.000	35.100	315.000	or4
4.770E+03	17.757	12.243	15.744	8.763	3.000	36.260	1435.000	or5
4.940E+03	12.247	5.951	9.332	6.134	3.000	30.890	2315.000	or6
4.910E+03	12.933	6.599	10.000	6.802	3.000	30.940	2315.000	or7
4.650E+03	12.559	6.903	9.484	6.796	3.000	22.860	2585.000	or8
4.260E+03	12.207	8.286	11.080	2.300	3.000	17.130	150.000	or9
4.390E+03	19.226	14.875	17.585	8.314	3.000	22.700	150.000	or10
4.700E+03	14.426	10.340	13.404	4.085	3.000	25.830	315.000	or11
4.990E+03	11.122	6.333	9.198	2.806	3.000	31.500	1435.000	or12
5.040E+03	10.020	4.802	8.115	1.647	3.000	31.140	1435.000	or13
5.080E+03	7.264	1.614	4.449	1.516	3.000	27.710	2315.000	or14
5.080E+03	5.866	0.217	3.031	0.591	3.000	25.810	2585.000	or15
3.980E+03	15.302	11.683	14.095	5.553	3.000	15.600	150.000	or16
5.020E+03	9.502	4.741	7.590	1.315	3.000	29.360	1435.000	or17
4.960E+03	7.460	2.157	5.040	1.794	3.000	24.900	2315.000	or18
4.520E+03	23.739	17.920	21.615	13.230	2.830	38.100	1328.000	or19
4.600E+03	21.587	15.870	19.500	11.109	2.830	36.880	1328.000	or20
4.410E+03	26.281	19.229	23.016	18.821	2.830	35.640	2206.000	or21
4.360E+03	25.528	18.945	22.248	18.761	2.830	30.160	2426.000	or22
4.270E+03	23.700	16.979	20.351	16.862	2.830	24.220	2547.000	or23
4.600E+03	15.870	11.717	14.826	4.957	2.830	25.450	150.000	or24
4.690E+03	19.254	13.646	17.207	8.955	2.830	36.670	1328.000	or25
4.510E+03	22.949	16.053	19.756	15.388	2.830	32.900	2206.000	or26
err-avg	16.0	10.7	13.8	7.46				
err-sd	5.95	5.70	5.90	5.46				

26 Pu-240

exp. data	SAS-27G	SAS-44G	SAS-238G	SWAT	Enrich.	Burnup	z-locat.	Sample Id
1.320E+03	11.439	15.833	17.803	13.712	3.000	21.170	150.000	or1
2.360E+03	-6.525	-2.076	-0.636	-0.127	3.000	33.750	1435.000	or2
1.360E+03	2.868	7.132	8.897	4.779	3.000	20.180	150.000	or3
1.990E+03	13.970	18.794	20.603	20.704	3.000	35.100	315.000	or4
2.410E+03	-3.900	0.581	2.573	3.278	3.000	36.260	1435.000	or5
2.220E+03	-6.937	-2.162	-0.631	-0.090	3.000	30.890	2315.000	or6
2.240E+03	-7.634	-2.946	-1.429	-0.848	3.000	30.940	2315.000	or7
1.620E+03	-1.914	3.086	4.877	3.395	3.000	22.860	2585.000	or8
1.160E+03	0.948	4.914	6.724	1.810	3.000	17.130	150.000	or9
1.230E+03	28.211	33.496	35.610	31.382	3.000	22.700	150.000	or10

1.810E+03	-1.602	2.486	4.088	1.768	3.000	25.830	315.000	or11
2.270E+03	-7.577	-3.260	-1.762	-1.806	3.000	31.500	1435.000	or12
2.290E+03	-9.258	-4.934	-3.493	-3.624	3.000	31.140	1435.000	or13
2.040E+03	-7.304	-2.451	-0.931	-1.225	3.000	27.710	2315.000	or14
1.950E+03	-8.821	-4.000	-2.513	-3.128	3.000	25.810	2585.000	or15
1.040E+03	1.058	5.000	6.827	1.538	3.000	15.600	150.000	or16
2.080E+03	-4.567	-0.096	1.442	0.865	3.000	29.360	1435.000	or17
1.860E+03	-7.473	-2.688	-1.183	-2.097	3.000	24.900	2315.000	or18
2.470E+03	-0.891	3.968	4.939	6.113	2.830	38.100	1328.000	or19
2.520E+03	-4.762	0.000	0.952	1.746	2.830	36.880	1328.000	or20
2.380E+03	-1.261	3.866	4.874	6.429	2.830	35.640	2206.000	or21
2.110E+03	-1.043	3.839	5.308	5.687	2.830	30.160	2426.000	or22
1.720E+03	0.756	5.930	7.442	6.453	2.830	24.220	2547.000	or23
1.740E+03	4.138	8.276	9.943	7.529	2.830	25.450	150.000	or24
2.470E+03	-3.036	1.053	2.996	3.401	2.830	36.670	1328.000	or25
2.370E+03	-6.034	-1.477	-0.042	0.717	2.830	32.900	2206.000	or26
err-avg	-1.04	3.54	5.13	4.17				
err-sd	8.28	8.37	8.52	7.65				

26 Pu-241

exp. data	SAS-27G	SAS-44G	SAS-238G	SWAT	Enrich.	Burnup	z-locat.	Sample Id
6.200E+02	46.548	36.823	40.323	24.952	3.000	21.170	150.000	or1
1.280E+03	18.828	10.313	13.750	4.297	3.000	33.750	1435.000	or2
6.200E+02	37.210	28.274	31.387	16.935	3.000	20.180	150.000	or3
1.020E+03	53.824	42.941	47.157	31.569	3.000	35.100	315.000	or4
1.260E+03	27.778	18.571	22.222	12.302	3.000	36.260	1435.000	or5
1.180E+03	19.068	10.932	13.983	7.458	3.000	30.890	2315.000	or6
1.190E+03	18.067	10.168	13.193	6.723	3.000	30.940	2315.000	or7
8.400E+02	19.643	12.179	15.333	8.476	3.000	22.860	2585.000	or8
5.500E+02	21.382	13.491	16.564	3.291	3.000	17.130	150.000	or9
5.900E+02	68.695	57.254	61.356	43.983	3.000	22.700	150.000	or10
9.400E+02	23.830	15.426	18.404	5.904	3.000	25.830	315.000	or11
1.200E+03	19.083	10.833	14.083	4.583	3.000	31.500	1435.000	or12
1.210E+03	16.942	8.760	11.901	2.645	3.000	31.140	1435.000	or13
1.110E+03	13.333	5.946	8.739	2.342	3.000	27.710	2315.000	or14
1.050E+03	10.857	3.714	6.476	0.476	3.000	25.810	2585.000	or15
4.600E+02	25.217	17.348	20.500	6.217	3.000	15.600	150.000	or16
1.120E+03	19.196	11.250	14.286	4.732	3.000	29.360	1435.000	or17
1.000E+03	11.600	4.400	7.200	0.700	3.000	24.900	2315.000	or18
1.300E+03	26.231	17.385	20.846	12.462	2.830	38.100	1328.000	or19
1.320E+03	21.591	13.030	16.515	8.333	2.830	36.880	1328.000	or20
1.210E+03	29.504	20.331	24.050	18.678	2.830	35.640	2206.000	or21
1.090E+03	25.138	16.697	20.092	14.862	2.830	30.160	2426.000	or22
8.600E+02	26.163	18.023	21.395	15.651	2.830	24.220	2547.000	or23
9.000E+02	27.444	18.889	22.111	10.333	2.830	25.450	150.000	or24
1.300E+03	23.077	14.385	17.923	9.538	2.830	36.670	1328.000	or25
1.210E+03	21.736	13.306	16.529	11.322	2.830	32.900	2206.000	or26
err-avg	25.8	17.3	20.6	11.1				
err-sd	13.0	12.0	12.3	9.96				

26 Pu-242

exp. data	SAS-27G	SAS-44G	SAS-238G	SWAT	Enrich.	Burnup	z-locat.	Sample Id
1.280E+02	40.469	53.125	54.844	34.219	3.000	21.170	150.000	or1
5.640E+02	-4.752	5.124	5.550	-3.741	3.000	33.750	1435.000	or2
1.390E+02	14.245	24.676	26.043	8.705	3.000	20.180	150.000	or3
3.800E+02	53.474	68.132	68.763	54.763	3.000	35.100	315.000	or4
6.290E+02	-1.129	9.269	9.650	0.827	3.000	36.260	1435.000	or5

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4.640E+02	-4.547	5.884	6.401	-3.405	3.000	30.890	2315.000	or6
4.880E+02	-8.750	1.168	1.660	-7.828	3.000	30.940	2315.000	or7
2.110E+02	3.460	14.692	15.829	3.270	3.000	22.860	2585.000	or8
9.900E+01	3.636	13.131	14.646	-2.899	3.000	17.130	150.000	or9
1.120E+02	91.429	108.929	110.893	84.196	3.000	22.700	150.000	or10
2.790E+02	4.946	15.376	16.237	2.796	3.000	25.830	315.000	or11
4.780E+02	-3.305	6.820	7.322	-2.699	3.000	31.500	1435.000	or12
5.000E+02	-9.980	-0.300	0.180	-9.380	3.000	31.140	1435.000	or13
3.660E+02	-5.437	5.137	5.792	-4.809	3.000	27.710	2315.000	or14
3.200E+02	-8.500	2.094	2.844	-8.000	3.000	25.810	2585.000	or15
7.500E+01	5.840	15.520	17.133	-1.907	3.000	15.600	150.000	or16
3.840E+02	2.734	13.438	14.063	2.969	3.000	29.360	1435.000	or17
2.990E+02	-10.167	0.368	1.171	-10.033	3.000	24.900	2315.000	or18
7.730E+02	-6.701	3.001	3.001	-3.777	2.830	38.100	1328.000	or19
7.870E+02	-13.901	-4.981	-4.981	-11.576	2.830	36.880	1328.000	or20
6.800E+02	-6.765	3.206	3.559	-4.412	2.830	35.640	2206.000	or21
4.940E+02	-9.372	0.425	0.911	-8.198	2.830	30.160	2426.000	or22
2.850E+02	-4.912	5.298	6.140	-4.772	2.830	24.220	2547.000	or23
2.640E+02	15.492	25.568	26.515	12.879	2.830	25.450	150.000	or24
7.350E+02	-8.803	0.422	0.748	-6.435	2.830	36.670	1328.000	or25
6.580E+02	-18.359	-9.529	-9.164	-16.626	2.830	32.900	2206.000	or26
err-avg	4.24	14.8	15.6	3.62				
err-sd	23.8	25.5	25.9	22.0				

19 Am-241

exp. data	SAS-27G	SAS-44G	SAS-238G	SWAT	Enrich.	Burnup	z-locat.	Sample Id
2.190E+01	-8.539	-11.187	-8.767	-19.269	3.000	21.170	150.000	or1
6.080E+01	-53.618	-54.408	-52.829	-57.007	3.000	33.750	1435.000	or2
2.930E+01	-35.256	-37.235	-35.597	-43.072	3.000	20.180	150.000	or3
9.000E+01	-68.133	-68.667	-67.333	-70.400	3.000	36.260	1435.000	or4
7.300E+01	-62.699	-63.356	-62.027	-64.411	3.000	30.890	2315.000	or5
2.370E+01	-8.397	-10.422	-7.890	-13.249	3.000	22.860	2585.000	or6
1.400E+01	9.500	5.857	8.429	-4.571	3.000	17.130	150.000	or7
2.210E+01	-2.398	-5.023	-2.398	-13.529	3.000	22.700	150.000	or8
2.480E+01	-1.855	-4.395	-1.855	-12.702	3.000	25.830	315.000	or9
1.760E+02	-84.392	-84.665	-84.114	-85.563	3.000	31.500	1435.000	or10
1.400E+02	-81.750	-82.100	-81.579	-82.671	3.000	27.710	2315.000	or11
6.700E+00	99.701	92.388	97.463	72.836	3.000	15.600	150.000	or12
9.390E+01	-71.768	-72.279	-71.512	-73.951	3.000	29.360	1435.000	or13
4.100E+01	-14.171	-15.366	-11.829	-20.195	2.830	38.100	1328.000	or14
4.030E+01	-13.300	-14.491	-11.489	-16.352	2.830	35.640	2206.000	or15
5.530E+01	-39.855	-40.723	-38.987	-42.098	2.830	30.160	2426.000	or16
2.770E+01	4.404	1.805	5.271	-0.758	2.830	24.220	2547.000	or17
2.520E+01	19.563	16.667	20.516	6.706	2.830	25.450	150.000	or18
7.490E+01	-53.017	-53.672	-52.056	-56.409	2.830	36.670	1328.000	or19
err-avg	-24.5	-26.4	-24.1	-31.4				
err-sd	44.5	42.9	44.0	38.7				

7 Am-242

exp. data	SAS-27G	SAS-44G	SAS-238G	SWAT	Enrich.	Burnup	z-locat.	Sample Id
2.880E-01	16.458	2.674	5.382	-35.347	3.000	17.130	150.000	or1
4.940E-01	22.328	9.008	13.158	-28.725	3.000	25.830	315.000	or2
7.290E-01	28.601	17.010	22.730	-18.848	2.830	38.100	1328.000	or3
1.930E+00	-52.430	-56.617	-54.611	-68.539	2.830	35.640	2206.000	or4
1.210E+00	-30.397	-36.719	-34.157	-54.554	2.830	30.160	2426.000	or5
7.100E-01	-2.690	-11.718	-8.479	-37.775	2.830	24.220	2547.000	or6
7.570E-01	22.629	11.506	16.658	-22.946	2.830	36.670	1328.000	or7

err-avg	0.643	-9.27	-5.62	-38.1					
err-sd	31.0	27.7	28.9	17.8					
7 Am-243									
exp. data	SAS-27G	SAS-44G	SAS-238G	SWAT	Enrich.	Burnup	z-locat.	Sample	Id
8.600E+00	27.674	37.907	39.884	-6.640	3.000	17.130	150.000	or1	
3.900E+01	27.103	36.462	36.462	-2.923	3.000	25.830	315.000	or2	
1.540E+02	20.065	27.662	25.584	-2.273	2.830	38.100	1328.000	or3	
1.380E+02	10.435	18.478	17.101	-8.696	2.830	35.640	2206.000	or4	
4.200E+01	116.976	134.905	133.738	79.167	2.830	30.160	2426.000	or5	
3.620E+01	21.492	32.238	32.901	-0.497	2.830	24.220	2547.000	or6	
1.400E+02	18.357	26.000	24.286	-4.000	2.830	36.670	1328.000	or7	
err-avg	34.6	44.8	44.3	7.73					
err-sd	36.8	40.3	40.2	31.6					
23 Cm-242									
exp. data	SAS-27G	SAS-44G	SAS-238G	SWAT	Enrich.	Burnup	z-locat.	Sample	Id
7.400E+00	-30.014	-37.865	-36.554	-42.324	3.000	21.170	150.000	or1	
1.570E+01	-9.490	-17.834	-16.306	-20.701	3.000	33.750	1435.000	or2	
4.500E+00	2.178	-9.644	-7.511	-16.111	3.000	20.180	150.000	or3	
1.480E+01	8.919	-0.743	1.216	-4.122	3.000	36.260	1435.000	or4	
1.500E+01	-20.000	-27.067	-25.800	-28.333	3.000	30.890	2315.000	or5	
3.320E+01	-63.765	-66.988	-66.325	-67.500	3.000	30.940	2315.000	or6	
7.100E+00	-12.408	-20.577	-18.873	-21.817	3.000	22.860	2585.000	or7	
2.940E+00	2.075	-9.456	-7.823	-17.143	3.000	17.130	150.000	or8	
8.580E+00	-3.823	-14.254	-12.564	-19.382	3.000	25.830	315.000	or9	
1.480E+01	-15.811	-23.649	-22.162	-26.419	3.000	31.500	1435.000	or10	
2.720E+01	-55.147	-59.412	-58.640	-60.882	3.000	31.140	1435.000	or11	
1.190E+01	-19.269	-26.588	-25.160	-28.000	3.000	27.710	2315.000	or12	
1.960E+01	-58.020	-61.847	-61.107	-62.429	3.000	25.810	2585.000	or13	
1.130E+01	-4.071	-13.265	-11.549	-16.566	3.000	29.360	1435.000	or14	
1.410E+01	-46.106	-51.085	-50.227	-52.149	3.000	24.900	2315.000	or15	
1.450E+01	41.172	29.172	31.862	25.517	2.830	38.100	1328.000	or16	
4.700E+01	-58.553	-62.106	-61.383	-63.255	2.830	36.880	1328.000	or17	
1.440E+01	27.917	17.500	19.653	16.042	2.830	35.640	2206.000	or18	
1.170E+01	17.094	6.923	8.974	5.726	2.830	30.160	2426.000	or19	
7.560E+00	14.921	4.669	6.601	3.095	2.830	24.220	2547.000	or20	
8.130E+00	19.065	6.863	8.647	0.578	2.830	25.450	150.000	or21	
1.780E+01	8.371	-0.899	1.011	-3.876	2.830	36.670	1328.000	or22	
3.310E+01	-51.450	-55.559	-54.743	-56.133	2.830	32.900	2206.000	or23	
err-avg	-13.3	-21.5	-19.9	-24.2					
err-sd	30.4	27.6	28.2	26.8					
26 Cm-244									
exp. data	SAS-27G	SAS-44G	SAS-238G	SWAT	Enrich.	Burnup	z-locat.	Sample	Id
2.220E+00	63.784	94.550	108.829	30.270	3.000	21.170	150.000	or1	
3.400E+01	-4.559	11.941	18.412	-15.824	3.000	33.750	1435.000	or2	
2.040E+00	41.127	67.451	79.412	11.275	3.000	20.180	150.000	or3	
1.260E+01	205.952	256.349	275.714	160.000	3.000	35.100	315.000	or4	
4.160E+01	6.755	24.928	31.971	-5.216	3.000	36.260	1435.000	or5	
2.480E+01	-11.935	4.274	11.169	-19.153	3.000	30.890	2315.000	or6	
2.220E+01	-0.991	17.613	25.315	-9.054	3.000	30.940	2315.000	or7	
5.130E+00	3.216	25.088	34.133	-4.971	3.000	22.860	2585.000	or8	
1.040E+00	21.731	45.673	56.250	-5.827	3.000	17.130	150.000	or9	
1.970E+00	160.102	207.157	229.442	108.071	3.000	22.700	150.000	or10	
9.490E+00	0.274	17.808	26.027	-18.240	3.000	25.830	315.000	or11	
2.970E+01	-19.663	-5.522	0.236	-29.630	3.000	31.500	1435.000	or12	
2.670E+01	-15.206	-0.375	5.993	-25.768	3.000	31.140	1435.000	or13	

1.650E+01	-19.697	-4.000	2.485	-26.606	3.000	27.710	2315.000	or14
1.070E+01	-11.290	6.729	14.019	-18.224	3.000	25.810	2585.000	or15
1.040E+00	-24.452	-9.442	-2.885	-42.202	3.000	15.600	150.000	or16
1.800E+01	-3.889	13.611	20.889	-16.222	3.000	29.360	1435.000	or17
8.910E+00	-10.180	7.901	15.600	-18.204	3.000	24.900	2315.000	or18
5.980E+01	3.227	19.548	25.268	-9.465	2.830	38.100	1328.000	or19
4.590E+01	16.950	35.556	43.007	2.527	2.830	36.880	1328.000	or20
4.720E+01	-1.780	15.275	21.483	-10.614	2.830	35.640	2206.000	or21
2.210E+01	0.814	19.231	26.968	-8.235	2.830	30.160	2426.000	or22
6.950E+00	16.201	39.381	49.209	5.439	2.830	24.220	2547.000	or23
6.530E+00	56.202	82.389	95.100	25.727	2.830	25.450	150.000	or24
5.260E+01	-0.266	15.513	21.996	-12.719	2.830	36.670	1328.000	or25
3.170E+01	3.912	21.609	29.306	-6.278	2.830	32.900	2206.000	or26
err-avg	18.3	39.6	48.7	1.57				
err-sd	53.4	62.3	66.3	42.7				

16 Cs-134

exp. data	SAS-27G	SAS-44G	SAS-238G	SWAT	Enrich.	Burnup	z-locat.	Sample Id
1.300E+02	3.077	-0.846	-3.615	-1.231	3.000	33.750	1435.000	or1
4.290E+01	15.268	11.515	8.392	6.807	3.000	20.180	150.000	or2
1.380E+02	11.667	6.812	3.913	6.957	3.000	36.260	1435.000	or3
1.110E+02	1.982	-1.892	-4.595	-1.441	3.000	30.890	2315.000	or4
6.230E+01	1.525	-2.135	-4.928	-2.616	3.000	22.860	2585.000	or5
3.490E+01	2.521	-0.544	-3.238	-5.415	3.000	17.130	150.000	or6
7.550E+01	6.146	2.411	-0.424	-0.702	3.000	25.830	315.000	or7
1.190E+02	-1.092	-4.958	-7.647	-5.714	3.000	31.500	1435.000	or8
9.540E+01	-3.637	-7.285	-9.822	-7.306	3.000	27.710	2315.000	or9
1.020E+02	0.784	-3.039	-5.804	-4.147	3.000	29.360	1435.000	or10
1.510E+02	9.139	4.702	2.053	5.099	2.830	38.100	1328.000	or11
1.360E+02	6.397	2.500	-0.515	3.824	2.830	35.640	2206.000	or12
1.020E+02	3.824	-0.196	-3.039	0.392	2.830	30.160	2426.000	or13
6.550E+01	5.771	1.893	-0.779	1.786	2.830	24.220	2547.000	or14
6.520E+01	16.948	12.837	9.755	9.555	2.830	25.450	150.000	or15
1.460E+02	4.658	0.959	-1.781	1.027	2.830	36.670	1328.000	or16
err-avg	5.31	1.42	-1.38	0.430				
err-sd	5.62	5.45	5.33	4.98				

16 Cs-137

exp. data	SAS-27G	SAS-44G	SAS-238G	SWAT	Enrich.	Burnup	z-locat.	Sample Id
1.210E+03	5.537	5.537	5.537	4.380	3.000	33.750	1435.000	or1
7.160E+02	6.578	6.578	6.578	5.126	3.000	20.180	150.000	or2
1.290E+03	6.202	6.202	6.202	5.271	3.000	36.260	1435.000	or3
1.120E+03	4.375	4.375	4.375	3.214	3.000	30.890	2315.000	or4
8.270E+02	4.534	4.534	4.534	3.192	3.000	22.860	2585.000	or5
6.220E+02	4.180	4.180	4.180	2.637	3.000	17.130	150.000	or6
9.110E+02	7.223	7.223	7.223	5.928	3.000	25.830	315.000	or7
1.150E+03	3.652	3.652	3.652	2.522	3.000	31.500	1435.000	or8
1.000E+03	4.800	4.800	4.800	3.600	3.000	27.710	2315.000	or9
1.060E+03	4.811	4.811	4.811	3.585	3.000	29.360	1435.000	or10
1.380E+03	4.275	4.275	4.275	2.971	2.830	38.100	1328.000	or11
1.300E+03	3.154	3.077	3.077	2.154	2.830	35.640	2206.000	or12
1.120E+03	1.250	1.250	1.250	0.268	2.830	30.160	2426.000	or13
8.910E+02	2.245	2.245	2.245	1.010	2.830	24.220	2547.000	or14
8.340E+02	14.820	14.820	14.820	13.417	2.830	25.450	150.000	or15
1.310E+03	5.649	5.649	5.649	4.351	2.830	36.670	1328.000	or16
err-avg	5.21	5.20	5.20	3.98				
err-sd	2.99	2.99	2.99	2.93				

16 Eu-154

exp. data	SAS-27G	SAS-44G	SAS-238G	SWAT	Enrich.	Burnup	z-locat.	Sample	Id
2.590E+01	65.907	-5.444	-3.089	-29.189	3.000	33.750	1435.000	or1	
7.750E+00	100.645	23.394	28.568	-4.581	3.000	20.180	150.000	or2	
2.490E+01	96.064	10.723	13.173	-17.871	3.000	36.260	1435.000	or3	
2.110E+01	72.986	-0.758	2.180	-22.464	3.000	30.890	2315.000	or4	
1.180E+01	70.932	2.288	6.356	-17.102	3.000	22.860	2585.000	or5	
5.460E+00	100.549	26.355	31.429	-0.769	3.000	17.130	150.000	or6	
1.630E+01	57.791	-5.890	-2.699	-29.080	3.000	25.830	315.000	or7	
2.430E+01	55.885	-10.658	-7.490	-32.263	3.000	31.500	1435.000	or8	
1.970E+01	50.102	-12.437	-9.340	-30.660	3.000	27.710	2315.000	or9	
2.070E+01	59.952	-7.005	-4.010	-29.082	3.000	29.360	1435.000	or10	
2.670E+01	102.434	12.472	14.794	-17.303	2.830	38.100	1328.000	or11	
2.550E+01	89.020	5.686	8.118	-19.373	2.830	35.640	2206.000	or12	
2.040E+01	75.147	-0.343	2.647	-21.814	2.830	30.160	2426.000	or13	
1.330E+01	74.812	3.158	7.068	-17.218	2.830	24.220	2547.000	or14	
1.350E+01	90.519	12.593	16.370	-15.333	2.830	25.450	150.000	or15	
2.840E+01	78.415	-0.211	1.937	-26.408	2.830	36.670	1328.000	or16	
err-avg	77.6	3.37	6.63	-20.7					
err-sd	17.2	11.3	11.9	9.00					

26 U

exp. data	SAS-27G	SAS-44G	SAS-238G	SWAT	Enrich.	Burnup	z-locat.	Sample	Id
1.669E+04	-7.004	-7.004	-6.309	-7.927	3.000	21.170	150.000	or1	
1.099E+04	-2.338	-2.557	-0.846	-4.058	3.000	33.750	1435.000	or2	
1.562E+04	2.561	2.407	3.111	1.485	3.000	20.180	150.000	or3	
1.221E+04	-15.373	-15.758	-14.414	-18.370	3.000	35.100	315.000	or4	
1.021E+04	-1.783	-2.243	-0.411	-4.084	3.000	36.260	1435.000	or5	
1.131E+04	3.201	3.201	4.651	3.042	3.000	30.890	2315.000	or6	
1.175E+04	-0.860	-0.860	0.536	-0.962	3.000	30.940	2315.000	or7	
1.552E+04	-4.820	-4.691	-3.937	-4.317	3.000	22.860	2585.000	or8	
1.812E+04	-3.184	-3.074	-2.649	-3.670	3.000	17.130	150.000	or9	
1.733E+04	-14.357	-14.357	-13.681	-15.522	3.000	22.700	150.000	or10	
1.465E+04	-7.816	-7.952	-7.024	-9.392	3.000	25.830	315.000	or11	
1.155E+04	-0.779	-0.978	0.450	-2.346	3.000	31.500	1435.000	or12	
1.148E+04	0.854	0.653	2.082	-0.679	3.000	31.140	1435.000	or13	
1.415E+04	-9.710	-9.548	-8.551	-9.470	3.000	27.710	2315.000	or14	
1.370E+04	-1.277	-1.058	-0.066	-0.818	3.000	25.810	2585.000	or15	
1.843E+04	-0.228	-0.228	0.130	-0.619	3.000	15.600	150.000	or16	
1.259E+04	-3.376	-3.376	-2.065	-4.416	3.000	29.360	1435.000	or17	
1.390E+04	0.058	0.029	1.180	0.273	3.000	24.900	2315.000	or18	
8.940E+03	-3.870	-4.139	-2.293	-6.622	2.830	38.100	1328.000	or19	
8.280E+03	7.186	6.908	9.179	4.493	2.830	36.880	1328.000	or20	
8.900E+03	3.427	3.427	5.270	2.787	2.830	35.640	2206.000	or21	
9.930E+03	8.540	8.771	10.433	8.822	2.830	30.160	2426.000	or22	
1.227E+04	5.257	5.452	6.593	5.827	2.830	24.220	2547.000	or23	
1.322E+04	-5.862	-6.036	-4.970	-7.746	2.830	25.450	150.000	or24	
8.720E+03	2.592	2.053	4.209	-0.172	2.830	36.670	1328.000	or25	
8.860E+03	12.370	12.370	14.233	11.964	2.830	32.900	2206.000	or26	
err-avg	-1.41	-1.48	-0.198	-2.40					
err-sd	6.46	6.48	6.74	6.81					

26 Pu

exp. data	SAS-27G	SAS-44G	SAS-238G	SWAT	Enrich.	Burnup	z-locat.	Sample	Id
6.454E+03	19.743	17.300	19.925	10.890	3.000	21.170	150.000	or1	
9.380E+03	6.731	4.383	7.000	1.479	3.000	33.750	1435.000	or2	
6.440E+03	16.453	14.074	16.620	7.797	3.000	20.180	150.000	or3	

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8.114E+03	25.770	23.480	26.528	17.424	3.000	35.100	315.000	or4
9.234E+03	12.025	9.682	12.511	6.857	3.000	36.260	1435.000	or5
8.929E+03	7.360	4.450	7.114	3.928	3.000	30.890	2315.000	or6
8.931E+03	7.402	4.502	7.167	3.993	3.000	30.940	2315.000	or7
7.383E+03	9.858	6.810	9.213	5.936	3.000	22.860	2585.000	or8
6.100E+03	10.718	8.138	10.731	2.075	3.000	17.130	150.000	or9
6.361E+03	27.087	24.286	26.973	17.488	3.000	22.700	150.000	or10
7.808E+03	11.440	9.217	11.812	3.482	3.000	25.830	315.000	or11
9.076E+03	6.514	4.314	6.704	1.177	3.000	31.500	1435.000	or12
9.185E+03	4.712	2.291	4.892	-0.641	3.000	31.140	1435.000	or13
8.702E+03	3.934	1.204	3.588	0.395	3.000	27.710	2315.000	or14
8.479E+03	2.583	-0.240	2.151	-0.736	3.000	25.810	2585.000	or15
5.580E+03	13.285	10.887	13.225	4.617	3.000	15.600	150.000	or16
8.711E+03	7.054	4.747	7.162	1.490	3.000	29.360	1435.000	or17
8.195E+03	3.894	1.219	3.668	0.162	3.000	24.900	2315.000	or18
9.253E+03	14.684	12.567	15.089	9.251	2.830	38.100	1328.000	or19
9.366E+03	11.798	9.685	12.192	6.284	2.830	36.880	1328.000	or20
8.839E+03	16.555	13.807	16.480	13.211	2.830	35.640	2206.000	or21
8.168E+03	16.320	13.440	16.047	12.845	2.830	30.160	2426.000	or22
7.200E+03	17.358	13.971	16.758	13.192	2.830	24.220	2547.000	or23
7.569E+03	14.704	12.387	15.067	6.431	2.830	25.450	150.000	or24
9.364E+03	11.615	9.275	12.062	6.019	2.830	36.670	1328.000	or25
8.874E+03	11.975	9.088	11.801	8.309	2.830	32.900	2206.000	or26
err-avg	12.0	9.42	12.0	6.28				
err-sd	6.28	6.29	6.39	5.31				

19 Am

exp. data	SAS-27G	SAS-44G	SAS-238G	SWAT	Enrich.	Burnup	z-locat.	Sample Id
2.190E+01	-8.539	-11.187	-8.767	-19.269	3.000	21.170	150.000	or1
6.080E+01	-53.618	-54.408	-52.829	-57.007	3.000	33.750	1435.000	or2
2.930E+01	-35.256	-37.235	-35.597	-43.072	3.000	20.180	150.000	or3
9.000E+01	-68.133	-68.667	-67.333	-70.400	3.000	36.260	1435.000	or4
7.300E+01	-62.699	-63.356	-62.027	-64.411	3.000	30.890	2315.000	or5
2.370E+01	-8.397	-10.422	-7.890	-13.249	3.000	22.860	2585.000	or6
2.289E+01	16.416	17.860	20.209	-5.736	3.000	17.130	150.000	or7
2.210E+01	-2.398	-5.023	-2.398	-13.529	3.000	22.700	150.000	or8
6.429E+01	15.896	20.491	21.503	-6.893	3.000	25.830	315.000	or9
1.760E+02	-84.392	-84.665	-84.114	-85.563	3.000	31.500	1435.000	or10
1.400E+02	-81.750	-82.100	-81.579	-82.671	3.000	27.710	2315.000	or11
6.700E+00	99.701	92.388	97.463	72.836	3.000	15.600	150.000	or12
9.390E+01	-71.768	-72.279	-71.512	-73.951	3.000	29.360	1435.000	or13
1.957E+02	12.925	18.609	17.737	-6.089	2.830	38.100	1328.000	or14
1.802E+02	4.454	10.302	9.941	-11.049	2.830	35.640	2206.000	or15
9.851E+01	27.126	34.205	34.714	9.451	2.830	30.160	2426.000	or16
6.461E+01	13.900	18.707	20.600	-1.019	2.830	24.220	2547.000	or17
2.520E+01	19.563	16.667	20.516	6.706	2.830	25.450	150.000	or18
2.157E+02	-6.417	-1.722	-2.255	-22.269	2.830	36.670	1328.000	or19
err-avg	-14.4	-13.8	-12.3	-25.6				
err-sd	47.1	47.4	48.0	39.6				

26 Cm

exp. data	SAS-27G	SAS-44G	SAS-238G	SWAT	Enrich.	Burnup	z-locat.	Sample Id
9.620E+00	-8.368	-7.308	-3.004	-25.572	3.000	21.170	150.000	or1
4.970E+01	-6.117	2.535	7.445	-17.364	3.000	33.750	1435.000	or2
6.540E+00	14.327	14.404	19.602	-7.569	3.000	20.180	150.000	or3
1.260E+01	205.952	256.349	275.714	160.000	3.000	35.100	315.000	or4
5.640E+01	7.323	18.191	23.901	-4.929	3.000	36.260	1435.000	or5

3.980E+01	-14.975	-7.538	-2.764	-22.613	3.000	30.890	2315.000	or6
5.540E+01	-38.610	-33.087	-29.603	-44.079	3.000	30.940	2315.000	or7
1.223E+01	-5.854	-1.423	3.361	-14.751	3.000	22.860	2585.000	or8
3.980E+00	7.211	4.950	8.920	-14.186	3.000	17.130	150.000	or9
1.970E+00	160.102	207.157	229.442	108.071	3.000	22.700	150.000	or10
1.807E+01	-1.671	2.584	7.703	-18.783	3.000	25.830	315.000	or11
4.450E+01	-18.382	-11.551	-7.213	-28.562	3.000	31.500	1435.000	or12
5.390E+01	-35.362	-30.167	-26.623	-43.488	3.000	31.140	1435.000	or13
2.840E+01	-19.518	-13.465	-9.099	-27.190	3.000	27.710	2315.000	or14
3.030E+01	-41.518	-37.630	-34.578	-46.818	3.000	25.810	2585.000	or15
1.040E+00	-24.452	-9.442	-2.885	-42.202	3.000	15.600	150.000	or16
2.930E+01	-3.959	3.246	8.379	-16.355	3.000	29.360	1435.000	or17
2.301E+01	-32.195	-28.244	-24.737	-39.005	3.000	24.900	2315.000	or18
7.430E+01	10.633	21.427	26.555	-2.638	2.830	38.100	1328.000	or19
9.290E+01	-21.249	-13.854	-9.806	-30.753	2.830	36.880	1328.000	or20
6.160E+01	5.162	15.795	21.055	-4.383	2.830	35.640	2206.000	or21
3.380E+01	6.450	14.970	20.740	-3.402	2.830	30.160	2426.000	or22
1.451E+01	15.534	21.296	27.009	4.218	2.830	24.220	2547.000	or23
1.466E+01	35.607	40.505	47.156	11.780	2.830	25.450	150.000	or24
7.040E+01	1.918	11.364	16.690	-10.483	2.830	36.670	1328.000	or25
6.480E+01	-24.367	-17.809	-13.627	-31.744	2.830	32.900	2206.000	or26
err-avg	6.68	16.3	22.3	-8.18				
err-sd	55.5	66.6	70.9	45.3				

16 Cs

exp. data	SAS-27G	SAS-44G	SAS-238G	SWAT	Enrich.	Burnup	z-locat.	Sample Id
1.340E+03	5.299	4.918	4.649	3.836	3.000	33.750	1435.000	or1
7.589E+02	7.069	6.857	6.681	5.221	3.000	20.180	150.000	or2
1.428E+03	6.730	6.261	5.980	5.434	3.000	36.260	1435.000	or3
1.231E+03	4.159	3.810	3.566	2.794	3.000	30.890	2315.000	or4
8.893E+02	4.324	4.067	3.872	2.785	3.000	22.860	2585.000	or5
6.569E+02	4.092	3.929	3.786	2.209	3.000	17.130	150.000	or6
9.865E+02	7.140	6.855	6.638	5.420	3.000	25.830	315.000	or7
1.269E+03	3.207	2.845	2.593	1.749	3.000	31.500	1435.000	or8
1.095E+03	4.065	3.747	3.527	2.650	3.000	27.710	2315.000	or9
1.162E+03	4.458	4.122	3.880	2.906	3.000	29.360	1435.000	or10
1.531E+03	4.755	4.317	4.056	3.181	2.830	38.100	1328.000	or11
1.436E+03	3.461	3.022	2.737	2.312	2.830	35.640	2206.000	or12
1.222E+03	1.465	1.129	0.892	0.278	2.830	30.160	2426.000	or13
9.565E+02	2.486	2.221	2.038	1.063	2.830	24.220	2547.000	or14
8.992E+02	14.974	14.676	14.453	13.137	2.830	25.450	150.000	or15
1.456E+03	5.549	5.179	4.904	4.018	2.830	36.670	1328.000	or16
err-avg	5.20	4.87	4.64	3.69				
err-sd	3.04	3.05	3.05	2.92				

16 Eu

exp. data	SAS-27G	SAS-44G	SAS-238G	SWAT	Enrich.	Burnup	z-locat.	Sample Id
2.590E+01	65.907	-5.444	-3.089	-29.189	3.000	33.750	1435.000	or1
7.750E+00	100.645	23.394	28.568	-4.581	3.000	20.180	150.000	or2
2.490E+01	96.064	10.723	13.173	-17.871	3.000	36.260	1435.000	or3
2.110E+01	72.986	-0.758	2.180	-22.464	3.000	30.890	2315.000	or4
1.180E+01	70.932	2.288	6.356	-17.102	3.000	22.860	2585.000	or5
5.460E+00	100.549	26.355	31.429	-0.769	3.000	17.130	150.000	or6
1.630E+01	57.791	-5.890	-2.699	-29.080	3.000	25.830	315.000	or7
2.430E+01	55.885	-10.658	-7.490	-32.263	3.000	31.500	1435.000	or8
1.970E+01	50.102	-12.437	-9.340	-30.660	3.000	27.710	2315.000	or9
2.070E+01	59.952	-7.005	-4.010	-29.082	3.000	29.360	1435.000	or10

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2.670E+01	102.434	12.472	14.794	-17.303	2.830	38.100	1328.000	or11
2.550E+01	89.020	5.686	8.118	-19.373	2.830	35.640	2206.000	or12
2.040E+01	75.147	-0.343	2.647	-21.814	2.830	30.160	2426.000	or13
1.330E+01	74.812	3.158	7.068	-17.218	2.830	24.220	2547.000	or14
1.350E+01	90.519	12.593	16.370	-15.333	2.830	25.450	150.000	or15
2.840E+01	78.415	-0.211	1.937	-26.408	2.830	36.670	1328.000	or16
err-avg	77.6	3.37	6.63	-20.7				
err-sd	17.2	11.3	11.9	9.00				

26 TO

exp. data	SAS-27G	SAS-44G	SAS-238G	SWAT	Enrich.	Burnup	z-locat.	Sample Id
2.318E+04	0.442	-0.240	0.996	-2.705	3.000	21.170	150.000	or1
2.185E+04	1.954	0.745	2.731	-1.404	3.000	33.750	1435.000	or2
2.286E+04	6.612	5.801	6.999	3.325	3.000	20.180	150.000	or3
2.034E+04	1.180	0.066	2.101	-3.978	3.000	35.100	315.000	or4
2.104E+04	4.710	3.353	5.488	1.061	3.000	36.260	1435.000	or5
2.160E+04	4.786	3.503	5.366	3.094	3.000	30.890	2315.000	or6
2.074E+04	2.598	1.364	3.312	1.057	3.000	30.940	2315.000	or7
2.384E+04	0.100	-0.803	0.432	-0.898	3.000	22.860	2585.000	or8
2.491E+04	0.455	-0.117	0.828	-2.111	3.000	17.130	150.000	or9
2.372E+04	-3.215	-3.965	-2.746	-6.656	3.000	22.700	150.000	or10
2.354E+04	-0.688	-1.551	-0.112	-4.516	3.000	25.830	315.000	or11
2.214E+04	1.801	0.713	2.441	-1.414	3.000	31.500	1435.000	or12
2.072E+04	2.470	1.299	3.253	-0.774	3.000	31.140	1435.000	or13
2.414E+04	-4.546	-5.495	-4.051	-5.826	3.000	27.710	2315.000	or14
2.221E+04	0.141	-0.796	0.733	-0.849	3.000	25.810	2585.000	or15
2.402E+04	2.938	2.380	3.200	0.617	3.000	15.600	150.000	or16
2.261E+04	0.819	-0.141	1.519	-2.091	3.000	29.360	1435.000	or17
2.212E+04	1.446	0.440	2.075	0.191	3.000	24.900	2315.000	or18
2.002E+04	5.724	4.568	6.552	1.469	2.830	38.100	1328.000	or19
1.774E+04	9.472	8.266	10.670	5.254	2.830	36.880	1328.000	or20
1.944E+04	9.525	8.222	10.276	7.311	2.830	35.640	2206.000	or21
1.947E+04	11.519	10.380	12.322	9.923	2.830	30.160	2426.000	or22
2.052E+04	9.453	8.342	10.007	8.152	2.830	24.220	2547.000	or23
2.174E+04	2.277	1.304	2.887	-1.921	2.830	25.450	150.000	or24
1.985E+04	7.072	5.677	7.934	2.741	2.830	36.670	1328.000	or25
1.780E+04	12.040	10.624	12.919	9.982	2.830	32.900	2206.000	or26
err-avg	3.50	2.46	4.16	0.732				
err-sd	4.33	4.20	4.44	4.49				

26 T2

exp. data	SAS-27G	SAS-44G	SAS-238G	SWAT	Enrich.	Burnup	z-locat.	Sample Id
9.785E+05	-0.122	-0.139	-0.109	-0.197	3.000	21.170	150.000	or1
9.663E+05	0.096	0.069	0.113	0.020	3.000	33.750	1435.000	or2
9.789E+05	0.257	0.238	0.266	0.180	3.000	20.180	150.000	or3
9.639E+05	-0.141	-0.165	-0.122	-0.250	3.000	35.100	315.000	or4
9.632E+05	0.186	0.156	0.203	0.106	3.000	36.260	1435.000	or5
9.682E+05	0.251	0.223	0.264	0.214	3.000	30.890	2315.000	or6
9.673E+05	-0.006	-0.033	0.009	-0.039	3.000	30.940	2315.000	or7
9.771E+05	-0.028	-0.050	-0.020	-0.053	3.000	22.860	2585.000	or8
9.832E+05	-0.019	-0.033	-0.010	-0.084	3.000	17.130	150.000	or9
9.778E+05	-0.293	-0.311	-0.281	-0.376	3.000	22.700	150.000	or10
9.750E+05	-0.068	-0.089	-0.054	-0.160	3.000	25.830	315.000	or11
9.685E+05	0.103	0.078	0.118	0.030	3.000	31.500	1435.000	or12
9.675E+05	-0.030	-0.055	-0.013	-0.099	3.000	31.140	1435.000	or13
9.735E+05	-0.257	-0.280	-0.244	-0.288	3.000	27.710	2315.000	or14
9.731E+05	-0.089	-0.111	-0.076	-0.112	3.000	25.810	2585.000	or15

9.835E+05	0.021	0.007	0.027	-0.036	3.000	15.600	150.000	or16
9.709E+05	-0.012	-0.034	0.004	-0.080	3.000	29.360	1435.000	or17
9.738E+05	-0.039	-0.062	-0.025	-0.068	3.000	24.900	2315.000	or18
9.615E+05	0.171	0.147	0.188	0.083	2.830	38.100	1328.000	or19
9.604E+05	0.206	0.184	0.228	0.128	2.830	36.880	1328.000	or20
9.628E+05	0.359	0.332	0.374	0.314	2.830	35.640	2206.000	or21
9.678E+05	0.511	0.488	0.527	0.479	2.830	30.160	2426.000	or22
9.739E+05	0.363	0.340	0.375	0.336	2.830	24.220	2547.000	or23
9.748E+05	0.041	0.019	0.054	-0.053	2.830	25.450	150.000	or24
9.628E+05	0.260	0.231	0.278	0.171	2.830	36.670	1328.000	or25
9.637E+05	0.337	0.310	0.353	0.299	2.830	32.900	2206.000	or26
err-avg	0.791E-01	0.562E-01	0.934E-01	0.178E-01				
err-sd	0.200	0.198	0.201	0.206				

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exp. data	SAS-27G	SAS-44G	SAS-238G	SWAT	Enrich.	Burnup	z-locat.	Sample Id
9.720E+05	-0.254	-0.254	-0.242	-0.270	3.000	21.170	150.000	or1
9.555E+05	0.025	0.023	0.043	0.006	3.000	33.750	1435.000	or2
9.716E+05	0.144	0.142	0.153	0.127	3.000	20.180	150.000	or3
9.558E+05	-0.364	-0.369	-0.352	-0.402	3.000	35.100	315.000	or4
9.524E+05	0.065	0.060	0.080	0.040	3.000	36.260	1435.000	or5
9.579E+05	0.184	0.184	0.201	0.182	3.000	30.890	2315.000	or6
9.584E+05	-0.073	-0.073	-0.056	-0.074	3.000	30.940	2315.000	or7
9.688E+05	-0.108	-0.106	-0.094	-0.100	3.000	22.860	2585.000	or8
9.764E+05	-0.090	-0.088	-0.080	-0.099	3.000	17.130	150.000	or9
9.714E+05	-0.472	-0.472	-0.460	-0.493	3.000	22.700	150.000	or10
9.662E+05	-0.170	-0.172	-0.158	-0.194	3.000	25.830	315.000	or11
9.580E+05	0.053	0.051	0.068	0.034	3.000	31.500	1435.000	or12
9.583E+05	-0.073	-0.076	-0.059	-0.092	3.000	31.140	1435.000	or13
9.636E+05	-0.288	-0.286	-0.271	-0.284	3.000	27.710	2315.000	or14
9.646E+05	-0.111	-0.108	-0.094	-0.105	3.000	25.810	2585.000	or15
9.779E+05	-0.055	-0.055	-0.049	-0.063	3.000	15.600	150.000	or16
9.609E+05	-0.075	-0.075	-0.058	-0.089	3.000	29.360	1435.000	or17
9.656E+05	-0.072	-0.072	-0.056	-0.069	3.000	24.900	2315.000	or18
9.504E+05	0.016	0.014	0.031	-0.010	2.830	38.100	1328.000	or19
9.510E+05	0.094	0.092	0.111	0.071	2.830	36.880	1328.000	or20
9.523E+05	0.200	0.200	0.217	0.194	2.830	35.640	2206.000	or21
9.582E+05	0.370	0.373	0.390	0.373	2.830	30.160	2426.000	or22
9.657E+05	0.232	0.235	0.249	0.240	2.830	24.220	2547.000	or23
9.663E+05	-0.091	-0.093	-0.078	-0.116	2.830	25.450	150.000	or24
9.516E+05	0.139	0.134	0.154	0.114	2.830	36.670	1328.000	or25
9.548E+05	0.230	0.230	0.247	0.226	2.830	32.900	2206.000	or26
err-avg	-0.209E-01	-0.217E-01	-0.622E-02	-0.328E-01				
err-sd	0.196	0.196	0.197	0.200				

A.5. Relative Errors of the Calculated Compositions for 38 Nuclides Using SAS2H with 27,
44 and 238 g and SWAT with 107 g

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exp. data	SAS-27G	SAS-44G	SAS-238G	SWAT	Enrich.	Burnup	z-locat.	Sample Id
1.550E+02	0.645	-0.645	-0.645	0.129	3.400	15.950	220.220	ya1
1.420E+02	-10.563	-12.676	-13.380	-12.113	3.400	30.390	138.940	ya2
1.190E+02	3.361	1.681	0.840	2.269	3.400	31.330	57.660	ya3
1.440E+02	2.083	0.694	0.000	1.042	3.400	20.190	17.020	ya4
1.140E+02	7.018	4.386	4.386	5.351	3.400	32.030	138.940	ya5
1.150E+02	6.957	5.217	4.348	5.652	3.400	31.410	57.660	ya6
1.180E+02	-3.390	-5.085	-5.932	-4.407	3.400	35.970	138.940	ya7
1.200E+02	-3.333	-5.833	-5.833	-4.750	3.400	35.260	57.660	ya8
2.670E+02	-4.494	-5.243	-5.618	-4.607	3.208	8.300	-1.000	mi1
1.740E+02	6.897	4.598	4.023	3.563	3.210	32.200	-1.000	mi2
1.740E+02	4.598	2.299	1.724	0.977	3.210	33.710	-1.000	mi3
1.321E+02	4.466	1.438	1.438	3.634	2.556	30.720	167.600	mi4
1.321E+02	4.466	2.195	1.438	4.088	2.556	30.510	167.000	mi5
1.225E+02	11.020	7.755	7.755	10.041	2.556	31.560	167.000	mi6
1.131E+02	21.132	17.595	16.711	19.894	2.556	31.260	167.600	mi7
1.320E+02	3.030	0.758	0.000	2.652	2.556	31.310	167.000	mi8
1.815E+02	0.826	-1.377	-1.928	-0.110	3.038	27.350	13.200	mi9
1.588E+02	-0.504	-3.023	-3.652	-1.763	3.038	37.120	27.700	tr1
1.362E+02	4.258	1.322	0.587	2.643	3.038	44.340	165.220	tr2
1.588E+02	14.610	12.720	12.091	13.980	2.720	18.680	9.100	tr3
1.373E+02	17.261	14.348	14.348	16.315	2.720	26.620	24.500	tr4
1.362E+02	7.195	4.258	3.524	5.727	2.720	33.170	161.900	tr5
1.736E+02	-21.083	-23.963	-23.963	-22.408	2.453	31.400	11.280	tr6
1.441E+02	-13.255	-16.031	-16.725	-14.851	2.453	37.270	19.920	tr7
8.497E+01	29.457	23.573	23.573	25.809	2.453	46.460	161.210	tr8
err-avg	3.71	1.24	0.764	2.35				
err-sd	10.6	10.1	10.1	10.4				

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exp. data	SAS-27G	SAS-44G	SAS-238G	SWAT	Enrich.	Burnup	z-locat.	Sample Id
1.980E+04	-1.010	-1.010	-0.505	0.859	3.400	15.950	220.220	ya1
1.260E+04	-7.143	-7.143	-5.556	-2.381	3.400	30.390	138.940	ya2
1.190E+04	-5.882	-5.882	-4.202	-0.840	3.400	31.330	57.660	ya3
1.720E+04	-2.326	-2.326	-1.744	0.058	3.400	20.190	17.020	ya4
1.180E+04	-6.780	-6.780	-4.237	-1.525	3.400	32.030	138.940	ya5
1.190E+04	-5.882	-6.723	-4.202	-1.176	3.400	31.410	57.660	ya6
9.780E+03	-2.965	-3.272	-0.204	3.681	3.400	35.970	138.940	ya7
9.840E+03	-2.033	-2.337	0.610	4.472	3.400	35.260	57.660	ya8
2.390E+04	-2.092	-2.092	-2.092	-1.548	3.208	8.300	-1.000	mi1
2.520E+04	-1.984	-1.587	-1.587	-1.310	3.208	6.900	-1.000	mi2
1.850E+04	-4.865	-4.324	-4.324	-3.676	3.203	15.360	-1.000	mi3
1.450E+04	-4.138	-4.138	-2.759	-2.759	3.203	21.290	-1.000	mi4
1.840E+04	-1.630	-1.630	-1.087	-0.652	3.203	14.660	-1.000	mi5
9.790E+03	-4.188	-4.086	-2.451	-2.983	3.210	29.500	-1.000	mi6
9.070E+03	-8.931	-8.710	-6.725	-7.641	3.210	32.200	-1.000	mi7
7.890E+03	-3.676	-3.676	-1.394	-2.573	3.210	33.710	-1.000	mi8
8.040E+03	-4.353	-3.731	-1.244	-2.276	3.210	34.320	-1.000	mi9
2.662E+04	1.052	1.052	1.427	1.803	3.897	12.040	79.200	tr1
1.728E+04	2.431	3.009	3.588	3.704	3.130	15.380	158.500	tr2
1.661E+04	4.154	4.154	5.358	5.298	3.130	15.900	79.200	tr3
2.017E+04	0.645	1.140	1.140	1.587	3.130	11.530	26.400	tr4
1.946E+04	-0.308	0.206	0.719	0.874	3.130	12.860	237.700	tr5

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1.436E+04	1.671	1.671	3.064	2.994	3.130	20.600	211.300	tr6
1.248E+04	3.365	3.365	4.968	5.048	3.130	23.720	158.500	tr7
1.235E+04	1.215	1.215	2.834	2.753	3.130	4.300	79.200	tr8
1.291E+04	-0.852	-0.852	0.697	1.007	3.130	23.870	158.500	tr9
1.221E+04	1.556	1.556	3.194	2.948	3.130	24.550	79.200	tr10
1.282E+04	-0.156	-0.156	1.404	1.482	3.130	23.930	158.500	tr11
1.225E+04	2.041	2.041	2.857	3.347	3.130	24.360	79.200	tr12
1.297E+04	-2.853	-2.853	-1.311	-1.157	3.130	24.330	158.500	tr13
1.231E+04	1.543	1.543	3.168	3.087	3.130	24.310	79.200	tr14
5.865E+03	-6.394	-5.882	-3.495	-5.934	2.556	30.720	167.600	tu1
5.676E+03	-2.044	-1.691	0.951	-1.621	2.556	30.510	167.000	tu2
5.584E+03	-6.160	-5.802	-3.116	-5.892	2.556	31.560	167.000	tu3
5.509E+03	-3.249	-3.431	-0.163	-2.941	2.556	31.260	167.600	tu4
5.662E+03	-6.217	-5.864	-3.214	-5.828	2.556	31.310	167.000	tu5
9.610E+03	-5.515	-5.515	-4.058	-3.861	3.038	27.350	13.200	ca1
5.866E+03	-8.456	-8.796	-6.069	-6.955	3.038	37.120	27.700	ca2
4.016E+03	-9.363	-9.612	-5.627	-7.395	3.038	44.340	165.220	ca3
1.163E+04	-1.978	-1.118	-0.258	-0.172	2.720	18.680	9.100	ca4
7.874E+03	-4.242	-4.115	-2.464	-2.515	2.720	26.620	24.500	ca5
5.423E+03	-2.268	-1.899	0.682	0.240	2.720	33.170	161.900	ca6
4.379E+03	-5.915	-5.915	-2.261	-8.016	2.453	31.400	11.280	ca7
3.075E+03	-11.220	-11.220	-6.341	-14.732	2.453	37.270	19.920	ca8
1.595E+03	-10.345	-9.718	-1.567	-14.357	2.453	46.460	161.210	ca9
1.214E+04	0.494	0.494	1.318	-1.483	2.561	16.020	11.000	ro1
8.180E+03	1.100	1.222	2.934	-3.289	2.561	23.810	26.000	ro2
7.011E+03	-5.149	-5.149	-2.296	-10.441	2.561	28.470	199.000	ro3
5.514E+03	3.011	3.555	6.819	-3.954	2.561	31.660	226.000	ro4
1.095E+04	-2.283	-2.283	-0.457	-1.553	3.130	25.930	-1.000	ob1
1.058E+04	-1.701	-1.701	0.189	-1.134	3.130	26.540	-1.000	ob2
9.850E+03	-1.421	-1.117	0.406	-0.832	3.130	27.990	-1.000	ob3
9.680E+03	-1.653	-1.240	0.310	-0.992	3.130	28.400	-1.000	ob4
9.580E+03	-3.653	-3.236	-1.670	-2.985	3.130	29.040	-1.000	ob5
9.180E+03	-1.743	-1.307	0.327	-1.111	3.130	29.520	-1.000	ob6
err-avg	-2.74	-2.61	-0.722	-1.73				
err-sd	3.59	3.63	3.06	4.28				

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exp. data	SAS-27G	SAS-44G	SAS-238G	SWAT	Enrich.	Burnup	z-locat.	Sample Id
2.880E+03	-0.347	-0.347	-1.042	-5.764	3.400	15.950	220.220	ya1
4.080E+03	1.225	1.225	0.490	-4.461	3.400	30.390	138.940	ya2
4.150E+03	0.723	0.723	0.241	-4.747	3.400	31.330	57.660	ya3
3.300E+03	0.909	0.909	0.000	-4.576	3.400	20.190	17.020	ya4
4.180E+03	0.957	0.957	0.239	-4.617	3.400	32.030	138.940	ya5
4.090E+03	2.445	2.445	1.711	-3.227	3.400	31.410	57.660	ya6
4.450E+03	-0.674	-0.674	-1.348	-6.270	3.400	35.970	138.940	ya7
4.440E+03	-1.126	-1.126	-1.802	-6.644	3.400	35.260	57.660	ya8
1.650E+03	6.061	6.061	5.455	0.606	3.208	8.300	-1.000	mi1
1.460E+03	5.479	4.795	4.795	-0.342	3.208	6.900	-1.000	mi2
2.650E+03	-0.377	-0.755	-1.132	-5.811	3.203	15.360	-1.000	mi3
3.270E+03	-0.306	-0.612	-0.917	-5.505	3.203	21.290	-1.000	mi4
2.660E+03	-4.135	-4.135	-4.887	-9.286	3.203	14.660	-1.000	mi5
3.830E+03	6.789	6.527	6.266	2.063	3.210	29.500	-1.000	mi6
4.000E+03	6.000	5.750	5.500	1.375	3.210	32.200	-1.000	mi7
4.180E+03	3.110	3.110	2.632	-1.172	3.210	33.710	-1.000	mi8
4.200E+03	2.857	2.857	2.619	-1.571	3.210	34.320	-1.000	mi9
2.736E+03	-10.088	-10.088	-10.819	-15.132	3.897	12.040	79.200	tr1
2.834E+03	-7.198	-7.551	-8.257	-12.385	3.130	15.380	158.500	tr2

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2.739E+03	-2.154	-2.154	-2.884	-7.229	3.130	15.900	79.200	tr3
2.502E+03	-14.069	-14.069	-14.868	-18.665	3.130	11.530	26.400	tr4
2.453E+03	-5.014	-5.422	-5.830	-10.273	3.130	12.860	237.700	tr5
3.317E+03	-4.733	-5.035	-5.638	-9.888	3.130	20.600	211.300	tr6
3.610E+03	-5.263	-5.540	-6.371	-10.416	3.130	23.720	158.500	tr7
3.638E+03	-4.893	-4.893	-5.717	-9.786	3.130	4.300	79.200	tr8
3.520E+03	-2.557	-2.841	-3.693	-7.813	3.130	23.870	158.500	tr9
3.540E+03	-1.695	-1.695	-2.542	-6.808	3.130	24.550	79.200	tr10
3.753E+03	-8.606	-8.606	-9.406	-13.429	3.130	23.930	158.500	tr11
3.465E+03	0.144	-0.144	-1.010	-5.166	3.130	24.360	79.200	tr12
3.471E+03	-0.317	-0.317	-1.181	-5.589	3.130	24.330	158.500	tr13
3.569E+03	-3.054	-3.054	-3.895	-8.069	3.130	24.310	79.200	tr14
3.254E+03	2.950	2.950	2.336	-1.291	2.556	30.720	167.600	tu1
3.255E+03	2.611	2.611	2.304	-1.536	2.556	30.510	167.000	tu2
3.174E+03	6.490	6.490	5.860	2.079	2.556	31.560	167.000	tu3
3.156E+03	6.781	6.781	6.147	2.345	2.556	31.260	167.600	tu4
3.252E+03	3.629	3.629	3.321	-0.615	2.556	31.310	167.000	tu5
3.562E+03	3.032	3.032	2.471	-1.544	3.038	27.350	13.200	ca1
4.005E+03	2.871	2.871	2.622	-1.323	3.038	37.120	27.700	ca2
4.187E+03	1.743	1.743	1.743	-2.221	3.038	44.340	165.220	ca3
2.837E+03	-0.599	-0.952	-1.304	-5.393	2.720	18.680	9.100	ca4
3.392E+03	-0.354	-0.649	-0.943	-4.776	2.720	26.620	24.500	ca5
3.699E+03	-1.325	-1.325	-1.595	-5.407	2.720	33.170	161.900	ca6
3.245E+03	1.695	1.695	1.387	-1.818	2.453	31.400	11.280	ca7
3.438E+03	-0.524	-0.814	-0.814	-3.956	2.453	37.270	19.920	ca8
3.449E+03	-0.261	-0.551	0.029	-3.682	2.453	46.460	161.210	ca9
2.485E+03	-1.408	-1.811	-2.213	-5.594	2.561	16.020	11.000	ro1
3.109E+03	-2.219	-2.219	-2.863	-5.886	2.561	23.810	26.000	ro2
3.199E+03	2.219	2.219	1.594	-1.751	2.561	28.470	199.000	ro3
3.404E+03	-0.411	-0.411	-0.999	-4.377	2.561	31.660	226.000	ro4
3.590E+03	1.393	1.114	0.836	-3.677	3.130	25.930	-1.000	ob1
3.620E+03	1.657	1.657	1.105	-3.287	3.130	26.540	-1.000	ob2
3.700E+03	2.162	1.892	1.622	-2.865	3.130	27.990	-1.000	ob3
3.730E+03	1.877	1.877	1.340	-2.976	3.130	28.400	-1.000	ob4
3.750E+03	2.400	2.400	1.867	-2.480	3.130	29.040	-1.000	ob5
3.810E+03	1.575	1.575	1.050	-3.281	3.130	29.520	-1.000	ob6
err-avg	-0.350E-01	-0.144	-0.662	-4.83				
err-sd	4.13	4.14	4.24	4.24				

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exp. data	SAS-27G	SAS-44G	SAS-238G	SWAT	Enrich.	Burnup	z-locat.	Sample Id
9.490E+05	0.421	0.421	0.421	0.411	3.400	15.950	220.220	ya1
9.370E+05	0.427	0.427	0.320	0.299	3.400	30.390	138.940	ya2
9.350E+05	0.535	0.535	0.535	0.449	3.400	31.330	57.660	ya3
9.360E+05	1.496	1.496	1.496	1.442	3.400	20.190	17.020	ya4
9.350E+05	0.428	0.535	0.428	0.353	3.400	32.030	138.940	ya5
9.360E+05	0.427	0.427	0.427	0.331	3.400	31.410	57.660	ya6
9.330E+05	0.322	0.322	0.214	0.161	3.400	35.970	138.940	ya7
9.340E+05	0.321	0.321	0.214	0.161	3.400	35.260	57.660	ya8
9.620E+05	0.000	0.000	0.000	0.042	3.208	8.300	-1.000	mi1
9.620E+05	0.104	0.104	0.104	0.104	3.208	6.900	-1.000	mi2
9.560E+05	0.105	0.105	0.105	0.188	3.203	15.360	-1.000	mi3
9.520E+05	0.000	0.000	0.000	0.116	3.203	21.290	-1.000	mi4
9.570E+05	0.104	0.104	0.104	0.146	3.203	14.660	-1.000	mi5
9.470E+05	-0.106	-0.106	-0.106	0.021	3.210	29.500	-1.000	mi6
9.440E+05	0.000	0.000	0.000	0.074	3.210	32.200	-1.000	mi7
9.440E+05	-0.106	-0.106	-0.212	-0.042	3.210	33.710	-1.000	mi8

9.420E+05	-0.106	0.000	-0.106	0.032	3.210	34.320	-1.000	mi9
9.513E+05	0.074	0.074	0.074	0.105	3.897	12.040	79.200	tr1
9.558E+05	0.021	0.021	0.021	0.052	3.130	15.380	158.500	tr2
9.558E+05	0.021	0.021	0.021	0.031	3.130	15.900	79.200	tr3
9.595E+05	-0.052	-0.052	-0.052	0.031	3.130	11.530	26.400	tr4
9.587E+05	-0.073	-0.073	-0.073	-0.031	3.130	12.860	237.700	tr5
9.518E+05	0.021	0.021	-0.084	0.011	3.130	20.600	211.300	tr6
9.493E+05	-0.032	-0.032	-0.032	0.000	3.130	23.720	158.500	tr7
9.492E+05	-0.021	-0.021	-0.126	-0.011	3.130	4.300	79.200	tr8
9.492E+05	-0.021	-0.021	-0.021	0.000	3.130	23.870	158.500	tr9
9.483E+05	-0.032	0.074	-0.032	0.063	3.130	24.550	79.200	tr10
9.485E+05	0.053	0.053	-0.053	0.063	3.130	23.930	158.500	tr11
9.482E+05	0.084	0.084	-0.021	0.084	3.130	24.360	79.200	tr12
9.486E+05	-0.063	0.042	-0.063	0.021	3.130	24.330	158.500	tr13
9.472E+05	0.190	0.190	0.084	0.201	3.130	24.310	79.200	tr14
9.502E+05	-0.126	-0.126	-0.126	-0.011	2.556	30.720	167.600	tu1
9.506E+05	-0.168	-0.063	-0.168	-0.032	2.556	30.510	167.000	tu2
9.495E+05	-0.158	-0.053	-0.158	-0.021	2.556	31.560	167.000	tu3
9.499E+05	-0.095	-0.095	-0.095	-0.032	2.556	31.260	167.600	tu4
9.498E+05	-0.084	-0.084	-0.084	-0.021	2.556	31.310	167.000	tu5
9.559E+05	-0.617	-0.617	-0.617	-0.554	3.038	27.350	13.200	ca1
9.448E+05	-0.402	-0.296	-0.402	-0.275	3.038	37.120	27.700	ca2
9.359E+05	-0.203	-0.096	-0.203	-0.064	3.038	44.340	165.220	ca3
9.702E+05	-1.154	-1.154	-1.154	-1.093	2.720	18.680	9.100	ca4
9.687E+05	-1.724	-1.621	-1.724	-1.600	2.720	26.620	24.500	ca5
9.556E+05	-1.005	-0.900	-1.005	-0.889	2.720	33.170	161.900	ca6
9.582E+05	-0.751	-0.751	-0.751	-0.657	2.453	31.400	11.280	ca7
9.573E+05	-1.285	-1.285	-1.285	-1.149	2.453	37.270	19.920	ca8
9.385E+05	-0.266	-0.266	-0.266	-0.170	2.453	46.460	161.210	ca9
9.609E+05	0.114	0.114	0.114	0.219	2.561	16.020	11.000	ro1
9.609E+05	-0.614	-0.614	-0.614	-0.447	2.561	23.810	26.000	ro2
9.462E+05	0.507	0.507	0.402	0.624	2.561	28.470	199.000	ro3
9.553E+05	-0.764	-0.764	-0.869	-0.649	2.561	31.660	226.000	ro4
err-avg	-0.868E-01	-0.653E-01	-0.111	-0.391E-01				
err-sd	0.515	0.506	0.508	0.472				

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exp. data	SAS-27G	SAS-44G	SAS-238G	SWAT	Enrich.	Burnup	z-locat.	Sample Id
3.041E+02	18.053	6.215	3.256	-2.664	3.038	27.350	13.200	ya1
4.039E+02	28.745	15.870	11.909	7.650	3.038	37.120	27.700	ya2
5.310E+02	19.586	7.533	3.390	0.640	3.038	44.340	165.220	ya3
1.979E+02	10.662	-1.465	-3.487	-10.814	2.720	18.680	9.100	ya4
3.395E+02	2.504	-8.100	-10.751	-15.670	2.720	26.620	24.500	ya5
3.877E+02	18.133	6.010	2.657	-1.625	2.720	33.170	161.900	ya6
2.960E+02	32.770	18.243	14.865	7.365	2.453	31.400	11.280	ya7
3.636E+02	29.813	15.787	12.211	5.831	2.453	37.270	19.920	ya8
4.280E+02	35.748	20.327	16.355	11.636	2.453	46.460	161.210	mi1
1.759E+02	5.742	-6.765	-8.471	-19.500	2.561	16.020	11.000	mi2
2.950E+02	5.424	-6.102	-8.136	-16.814	2.561	23.810	26.000	mi3
3.449E+02	14.236	2.059	-0.841	-8.524	2.561	28.470	199.000	mi4
3.778E+02	18.317	6.141	2.700	-4.685	2.561	31.660	226.000	mi5
err-avg	18.4	5.83	2.74	-3.63				
err-sd	10.8	9.70	9.06	10.2				

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exp. data	SAS-27G	SAS-44G	SAS-238G	SWAT	Enrich.	Burnup	z-locat.	Sample Id
4.730E+01	-13.319	-20.719	-20.930	-26.575	3.400	15.950	220.220	ya1
1.760E+02	4.545	-3.409	-3.977	-7.784	3.400	30.390	138.940	ya2

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2.140E+02	-10.748	-17.757	-18.224	-21.449	3.400	31.330	57.660	ya3
7.910E+01	-12.010	-19.090	-19.216	-23.881	3.400	20.190	17.020	ya4
2.220E+02	-9.009	-15.766	-16.216	-19.550	3.400	32.030	138.940	ya5
2.110E+02	-9.005	-16.114	-16.588	-19.905	3.400	31.410	57.660	ya6
2.470E+02	4.453	-3.239	-4.049	-7.328	3.400	35.970	138.940	ya7
2.400E+02	2.083	-5.417	-6.250	-9.625	3.400	35.260	57.660	ya8
4.510E+00	9.534	0.887	0.443	-20.177	3.208	8.300	-1.000	mi1
3.410E+00	5.279	-2.933	-3.519	-22.727	3.208	6.900	-1.000	mi2
2.590E+01	-8.494	-14.672	-15.058	-29.884	3.203	15.360	-1.000	mi3
5.720E+01	-5.245	-11.014	-11.364	-25.210	3.203	21.290	-1.000	mi4
2.680E+01	-23.507	-29.104	-29.104	-41.679	3.203	14.660	-1.000	mi5
1.310E+02	-5.344	-10.687	-11.450	-28.626	3.210	29.500	-1.000	mi6
1.590E+02	-3.774	-9.434	-10.063	-26.855	3.210	32.200	-1.000	mi7
1.680E+02	-1.190	-6.548	-7.143	-24.583	3.210	33.710	-1.000	mi8
1.860E+02	-1.613	-6.989	-7.527	-24.140	3.210	34.320	-1.000	mi9
1.365E+02	8.425	1.832	0.366	-12.381	2.556	30.720	167.600	tr1
1.360E+02	7.353	0.735	-0.735	-13.309	2.556	30.510	167.000	tr2
1.426E+02	9.397	3.086	1.683	-11.290	2.556	31.560	167.000	tr3
1.382E+02	10.709	4.197	2.750	-10.203	2.556	31.260	167.600	tr4
1.372E+02	12.245	4.956	4.227	-9.257	2.556	31.310	167.000	tr5
1.146E+02	-3.141	-9.250	-10.122	-19.948	3.038	27.350	13.200	tr6
2.144E+02	-0.187	-6.250	-7.183	-15.951	3.038	37.120	27.700	tr7
3.052E+02	0.262	-5.636	-6.619	-14.286	3.038	44.340	165.220	tr8
5.503E+01	-17.681	-23.315	-23.678	-34.472	2.720	18.680	9.100	tr9
1.099E+02	-7.188	-12.739	-13.376	-23.758	2.720	26.620	24.500	tr10
1.683E+02	-0.772	-6.714	-7.308	-17.231	2.720	33.170	161.900	tr11
1.618E+02	-0.494	-6.675	-7.293	-18.727	2.453	31.400	11.280	tr12
2.209E+02	0.045	-6.292	-7.198	-17.655	2.453	37.270	19.920	tr13
3.224E+02	-1.985	-7.878	-8.499	-17.866	2.453	46.460	161.210	tr14
3.211E+01	0.592	-7.194	-7.505	-27.748	2.561	16.020	11.000	tu1
7.885E+01	0.571	-6.405	-7.039	-23.817	2.561	23.810	26.000	tu2
1.293E+02	-6.419	-12.606	-13.380	-27.247	2.561	28.470	199.000	tu3
1.475E+02	2.373	-3.729	-5.085	-19.458	2.561	31.660	226.000	tu4
err-avg	-1.81	-8.34	-9.04	-20.4				
err-sd	8.14	7.85	7.58	7.75				

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exp. data	SAS-27G	SAS-44G	SAS-238G	SWAT	Enrich.	Burnup	z-locat.	Sample Id
5.950E+03	-6.387	-8.739	-5.546	-3.109	3.400	15.950	220.220	ya1
7.870E+03	-8.895	-11.182	-7.243	-2.186	3.400	30.390	138.940	ya2
8.010E+03	-10.861	-12.984	-9.238	-4.370	3.400	31.330	57.660	ya3
6.600E+03	-8.030	-10.152	-6.818	-3.667	3.400	20.190	17.020	ya4
7.980E+03	-8.772	-11.153	-7.143	-1.817	3.400	32.030	138.940	ya5
7.680E+03	-7.031	-9.115	-5.208	-0.182	3.400	31.410	57.660	ya6
6.950E+03	7.626	4.892	9.784	16.878	3.400	35.970	138.940	ya7
6.820E+03	7.625	5.132	9.971	16.481	3.400	35.260	57.660	ya8
3.020E+03	2.649	0.662	2.649	-2.483	3.208	8.300	-1.000	mi1
2.830E+03	1.413	-1.413	0.707	-3.958	3.208	6.900	-1.000	mi2
4.650E+03	-6.667	-9.462	-7.742	-11.290	3.203	15.360	-1.000	mi3
5.080E+03	0.394	-3.740	-1.575	-5.197	3.203	21.290	-1.000	mi4
4.740E+03	-11.814	-14.346	-12.236	-15.675	3.203	14.660	-1.000	mi5
5.300E+03	-2.642	-5.472	-3.019	-8.849	3.210	29.500	-1.000	mi6
5.470E+03	-2.925	-6.216	-3.656	-9.890	3.210	32.200	-1.000	mi7
4.970E+03	6.036	3.018	5.835	-1.368	3.210	33.710	-1.000	mi8
5.320E+03	5.639	0.752	3.571	-2.782	3.210	34.320	-1.000	mi9
4.586E+03	-2.747	-4.710	-1.875	-4.012	3.897	12.040	79.200	tr1
5.266E+03	-0.114	-2.773	0.266	-1.519	3.130	15.380	158.500	tr2

5.234E+03	0.115	-2.178	0.879	-1.089	3.130	15.900	79.200	tr3
4.418E+03	-0.634	-2.671	-0.181	-2.558	3.130	11.530	26.400	tr4
4.580E+03	4.585	1.528	4.585	2.467	3.130	12.860	237.700	tr5
5.755E+03	3.562	0.608	3.910	2.572	3.130	20.600	211.300	tr6
5.895E+03	5.344	2.629	6.361	4.801	3.130	23.720	158.500	tr7
6.070E+03	1.153	-1.153	2.306	0.675	3.130	4.300	79.200	tr8
5.950E+03	4.706	2.017	5.546	4.067	3.130	23.870	158.500	tr9
5.980E+03	3.010	0.669	4.181	2.542	3.130	24.550	79.200	tr10
6.060E+03	2.805	0.165	3.795	2.277	3.130	23.930	158.500	tr11
5.995E+03	2.419	0.083	3.586	2.018	3.130	24.360	79.200	tr12
6.060E+03	3.465	0.660	4.290	2.888	3.130	24.330	158.500	tr13
5.970E+03	2.680	0.335	3.853	2.412	3.130	24.310	79.200	tr14
4.838E+03	6.036	2.108	4.795	-0.620	2.556	30.720	167.600	tu1
4.840E+03	5.992	2.066	4.752	-0.723	2.556	30.510	167.000	tu2
4.930E+03	4.260	0.609	3.245	-2.231	2.556	31.560	167.000	tu3
4.941E+03	4.028	-0.425	2.813	-2.530	2.556	31.260	167.600	tu4
4.788E+03	7.352	3.383	6.099	0.585	2.556	31.310	167.000	tu5
4.838E+03	0.455	-2.026	-0.165	-3.865	3.038	27.350	13.200	ca1
4.943E+03	1.558	-1.275	1.153	-3.338	3.038	37.120	27.700	ca2
4.943E+03	4.795	0.951	3.581	-1.012	3.038	44.340	165.220	ca3
4.476E+03	-1.475	-3.932	-2.145	-5.474	2.720	18.680	9.100	ca4
4.824E+03	-0.705	-3.400	-1.327	-4.892	2.720	26.620	24.500	ca5
4.751E+03	5.872	1.873	4.399	0.610	2.720	33.170	161.900	ca6
4.327E+03	0.069	-2.011	1.225	-7.419	2.453	31.400	11.280	ca7
4.351E+03	0.207	-1.862	1.586	-7.768	2.453	37.270	19.920	ca8
4.273E+03	4.142	0.866	4.844	-4.517	2.453	46.460	161.210	ca9
4.130E+03	6.295	3.632	5.811	-2.639	2.561	16.020	11.000	ro1
4.561E+03	7.213	4.363	6.994	-1.710	2.561	23.810	26.000	ro2
4.980E+03	4.819	0.000	3.614	-4.900	2.561	28.470	199.000	ro3
4.765E+03	12.277	7.450	10.808	1.469	2.561	31.660	226.000	ro4
4.805E+03	6.139	2.393	4.475	0.583	3.130	25.930	-1.000	ob1
4.713E+03	8.636	4.816	7.150	2.843	3.130	26.540	-1.000	ob2
4.925E+03	4.975	1.320	3.553	-0.650	3.130	27.990	-1.000	ob3
5.013E+03	3.531	-0.259	1.935	-2.055	3.130	28.400	-1.000	ob4
4.957E+03	5.104	1.271	3.692	-0.565	3.130	29.040	-1.000	ob5
4.943E+03	5.806	1.962	4.188	-0.061	3.130	29.520	-1.000	ob6
err-avg	1.73	-1.28	1.67	-1.40				
err-sd	5.29	4.87	4.94	5.26				

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exp. data	SAS-27G	SAS-44G	SAS-238G	SWAT	Enrich.	Burnup	z-locat.	Sample	Id
1.120E+03	-7.143	-3.571	-0.893	-1.429	3.400	15.950	220.220	ya1	
2.120E+03	-4.717	0.000	1.887	4.292	3.400	30.390	138.940	ya2	
2.260E+03	-8.850	-4.425	-2.655	-0.221	3.400	31.330	57.660	ya3	
1.440E+03	-6.944	-2.778	-0.694	-0.833	3.400	20.190	17.020	ya4	
2.370E+03	-10.970	-6.751	-4.641	-2.152	3.400	32.030	138.940	ya5	
2.270E+03	-8.811	-4.846	-3.084	-0.396	3.400	31.410	57.660	ya6	
2.570E+03	-10.117	-5.447	-3.502	-0.156	3.400	35.970	138.940	ya7	
2.480E+03	-8.468	-4.032	-2.419	0.927	3.400	35.260	57.660	ya8	
4.220E+02	-1.185	2.607	5.213	-1.469	3.208	8.300	-1.000	mi1	
3.440E+02	-4.651	1.163	3.779	-2.558	3.208	6.900	-1.000	mi2	
1.030E+03	-6.990	-1.942	-0.971	-4.456	3.203	15.360	-1.000	mi3	
1.490E+03	-5.369	0.000	2.013	-0.403	3.203	21.290	-1.000	mi4	
1.060E+03	-15.189	-11.698	-9.906	-13.519	3.203	14.660	-1.000	mi5	
2.100E+03	-9.524	-5.238	-3.810	-4.619	3.210	29.500	-1.000	mi6	
2.270E+03	-9.251	-4.846	-3.524	-3.568	3.210	32.200	-1.000	mi7	
2.320E+03	-8.190	-3.879	-2.586	-2.371	3.210	33.710	-1.000	mi8	

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2.430E+03	-9.877	-4.527	-3.292	-3.086	3.210	34.320	-1.000	mi9
7.165E+02	-9.421	-6.071	-3.140	-7.258	3.897	12.040	79.200	tr1
1.118E+03	-6.977	-2.504	0.179	-2.683	3.130	15.380	158.500	tr2
1.137E+03	-5.013	-1.495	1.143	-1.935	3.130	15.900	79.200	tr3
7.750E+02	-6.710	-3.355	-0.903	-5.097	3.130	11.530	26.400	tr4
8.400E+02	0.238	5.119	7.619	4.024	3.130	12.860	237.700	tr5
1.520E+03	-4.605	0.000	1.974	0.461	3.130	20.600	211.300	tr6
1.755E+03	-5.413	-0.855	1.425	0.456	3.130	23.720	158.500	tr7
1.825E+03	-7.397	-3.014	-1.370	-2.137	3.130	4.300	79.200	tr8
1.760E+03	-5.114	0.000	1.705	0.852	3.130	23.870	158.500	tr9
1.785E+03	-4.202	-0.280	1.961	1.064	3.130	24.550	79.200	tr10
1.790E+03	-6.145	-1.676	0.000	-0.615	3.130	23.930	158.500	tr11
1.810E+03	-6.077	-2.210	-0.552	-1.105	3.130	24.360	79.200	tr12
1.770E+03	-3.390	1.130	2.825	2.147	3.130	24.330	158.500	tr13
1.790E+03	-5.587	-1.117	0.559	-0.279	3.130	24.310	79.200	tr14
2.266E+03	-5.119	-0.265	0.618	2.074	2.556	30.720	167.600	tu1
2.294E+03	-6.713	-1.918	-1.046	0.305	2.556	30.510	167.000	tu2
2.295E+03	-4.575	0.218	1.525	2.832	2.556	31.560	167.000	tu3
2.320E+03	-6.034	-1.293	-0.431	1.034	2.556	31.260	167.600	tu4
2.278E+03	-4.302	0.527	1.844	3.029	2.556	31.310	167.000	tu5
1.950E+03	-6.154	-2.051	-1.026	-1.949	3.038	27.350	13.200	ca1
2.540E+03	-7.480	-3.543	-2.756	-2.047	3.038	37.120	27.700	ca2
2.885E+03	-8.492	-4.333	-3.293	-1.906	3.038	44.340	165.220	ca3
1.410E+03	-6.383	-2.837	-1.418	-3.121	2.720	18.680	9.100	ca4
2.004E+03	-7.186	-3.194	-2.196	-1.597	2.720	26.620	24.500	ca5
2.395E+03	-7.724	-3.132	-1.879	0.125	2.720	33.170	161.900	ca6
2.345E+03	-7.463	-2.345	-2.345	-1.791	2.453	31.400	11.280	ca7
2.633E+03	-8.469	-3.152	-3.152	-2.013	2.453	37.270	19.920	ca8
2.949E+03	-8.783	-3.018	-2.679	-1.526	2.453	46.460	161.210	ca9
1.237E+03	-2.183	1.859	3.476	-3.800	2.561	16.020	11.000	ro1
1.895E+03	-4.485	-0.264	0.792	-3.483	2.561	23.810	26.000	ro2
2.235E+03	-5.145	-0.224	0.671	-2.327	2.561	28.470	199.000	ro3
2.405E+03	-4.366	0.624	1.871	-0.748	2.561	31.660	226.000	ro4
1.800E+03	-5.000	-0.556	1.111	0.778	3.130	25.930	-1.000	ob1
1.830E+03	-3.825	1.093	2.186	1.475	3.130	26.540	-1.000	ob2
1.920E+03	-4.167	0.521	2.083	1.823	3.130	27.990	-1.000	ob3
2.020E+03	-7.921	-3.465	-1.980	-1.832	3.130	28.400	-1.000	ob4
2.000E+03	-5.500	-0.500	1.000	1.250	3.130	29.040	-1.000	ob5
2.040E+03	-5.882	-0.980	0.490	0.784	3.130	29.520	-1.000	ob6
err-avg	-6.46	-1.98	-0.404	-1.10				
err-sd	2.53	2.69	2.81	2.85				

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exp. data	SAS-27G	SAS-44G	SAS-238G	SWAT	Enrich.	Burnup	z-locat.	Sample Id
6.630E+02	-7.541	-13.424	-10.558	-11.312	3.400	15.950	220.220	ya1
1.540E+03	-10.390	-16.234	-12.987	-10.714	3.400	30.390	138.940	ya2
1.640E+03	-9.146	-14.634	-11.585	-9.329	3.400	31.330	57.660	ya3
9.150E+02	-7.869	-13.552	-10.492	-10.317	3.400	20.190	17.020	ya4
1.670E+03	-7.186	-13.174	-9.581	-7.425	3.400	32.030	138.940	ya5
1.580E+03	-5.063	-11.392	-7.595	-5.633	3.400	31.410	57.660	ya6
1.680E+03	3.571	-2.976	0.595	4.286	3.400	35.970	138.940	ya7
1.620E+03	3.704	-2.469	1.235	4.383	3.400	35.260	57.660	ya8
1.090E+02	7.339	0.917	3.670	-5.963	3.208	8.300	-1.000	mi1
8.280E+01	2.415	-0.966	0.966	-8.068	3.208	6.900	-1.000	mi2
4.080E+02	-3.676	-9.069	-6.863	-14.779	3.203	15.360	-1.000	mi3
6.510E+02	3.687	-1.997	0.614	-6.651	3.203	21.290	-1.000	mi4
4.250E+02	-16.471	-21.882	-19.529	-26.329	3.203	14.660	-1.000	mi5

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9.550E+02	-2.304	-8.482	-6.073	10.576	3.210	29.500	-1.000	mi6
1.060E+03	-2.830	-8.491	-6.038	11.038	3.210	32.200	-1.000	mi7
9.830E+02	8.850	1.729	4.781	23.398	3.210	33.710	-1.000	mi8
1.080E+03	5.556	-0.926	1.852	21.389	3.210	34.320	-1.000	mi9
3.475E+02	-4.748	-9.928	-7.626	-14.273	3.897	12.040	79.200	tr1
6.140E+02	3.420	-2.606	0.163	-6.042	3.130	15.380	158.500	tr2
6.180E+02	5.987	-0.324	2.427	-4.191	3.130	15.900	79.200	tr3
3.690E+02	-0.542	-6.504	-3.794	-11.003	3.130	11.530	26.400	tr4
4.000E+02	9.500	3.500	6.500	0.175	3.130	12.860	237.700	tr5
8.850E+02	5.198	-0.904	2.260	-2.655	3.130	20.600	211.300	tr6
1.030E+03	8.738	1.942	4.854	0.583	3.130	23.720	158.500	tr7
1.060E+03	6.604	0.000	3.774	-1.415	3.130	4.300	79.200	tr8
1.050E+03	7.619	0.952	3.810	-0.571	3.130	23.870	158.500	tr9
1.055E+03	8.057	2.370	5.213	0.284	3.130	24.550	79.200	tr10
1.050E+03	7.619	0.952	4.762	-0.190	3.130	23.930	158.500	tr11
1.055E+03	7.109	0.474	4.265	-0.664	3.130	24.360	79.200	tr12
1.060E+03	9.434	2.830	5.660	3.113	3.130	24.330	158.500	tr13
1.060E+03	6.604	0.000	2.830	0.660	3.130	24.310	79.200	tr14
1.061E+03	10.273	3.676	6.503	-0.189	2.556	30.720	167.600	tu1
1.068E+03	8.614	2.060	4.869	-1.404	2.556	30.510	167.000	tu2
1.104E+03	8.696	1.449	4.167	-1.902	2.556	31.560	167.000	tu3
1.124E+03	5.872	-1.246	1.423	-4.448	2.556	31.260	167.600	tu4
1.072E+03	11.007	4.478	6.343	0.373	2.556	31.310	167.000	tu5
7.727E+02	4.180	-2.291	-0.091	-4.633	3.038	27.350	13.200	ca1
1.025E+03	3.415	-2.927	-0.488	-4.098	3.038	37.120	27.700	ca2
1.157E+03	4.581	-2.334	1.124	-1.988	3.038	44.340	165.220	ca3
5.153E+02	-0.834	-6.850	-4.910	-11.217	2.720	18.680	9.100	ca4
7.740E+02	2.326	-4.005	-1.809	-7.481	2.720	26.620	24.500	ca5
9.219E+02	6.628	0.011	2.397	-2.397	2.720	33.170	161.900	ca6
8.237E+02	-1.906	-8.098	-4.698	-11.060	2.453	31.400	11.280	ca7
9.224E+02	-1.995	-7.958	-4.380	-10.538	2.453	37.270	19.920	ca8
1.006E+03	0.398	-5.268	-1.292	-6.670	2.453	46.460	161.210	ca9
3.449E+02	5.538	-1.421	1.189	-10.496	2.561	16.020	11.000	ro1
5.718E+02	5.806	-0.839	1.784	-7.398	2.561	23.810	26.000	ro2
7.726E+02	0.311	-6.420	-3.055	-10.691	2.561	28.470	199.000	ro3
7.851E+02	8.903	2.153	5.337	-2.522	2.561	31.660	226.000	ro4
9.780E+02	7.362	0.409	2.249	-3.978	3.130	25.930	-1.000	ob1
9.780E+02	9.407	2.249	5.317	-1.411	3.130	26.540	-1.000	ob2
1.058E+03	6.805	0.189	3.025	-3.403	3.130	27.990	-1.000	ob3
1.103E+03	4.261	-2.085	0.635	-5.802	3.130	28.400	-1.000	ob4
1.107E+03	6.594	0.271	2.078	-3.794	3.130	29.040	-1.000	ob5
1.128E+03	6.383	-0.709	1.950	-3.901	3.130	29.520	-1.000	ob6
err-avg	3.02	-3.27	-0.415	-3.61				
err-sd	6.12	5.78	5.76	7.99				

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exp. data	SAS-27G	SAS-44G	SAS-238G	SWAT	Enrich.	Burnup	z-locat.	Sample Id
8.030E+01	-10.461	-1.370	0.249	-9.054	3.400	15.950	220.220	ya1
3.460E+02	3.468	14.451	15.318	5.578	3.400	30.390	138.940	ya2
3.980E+02	-4.020	5.779	6.533	-2.236	3.400	31.330	57.660	ya3
1.450E+02	-8.276	0.000	1.379	-7.586	3.400	20.190	17.020	ya4
4.220E+02	-4.976	5.213	5.924	-2.867	3.400	32.030	138.940	ya5
4.000E+02	-4.000	5.750	6.500	-2.200	3.400	31.410	57.660	ya6
5.520E+02	-7.246	2.717	3.080	-5.109	3.400	35.970	138.940	ya7
5.290E+02	-7.183	2.457	3.025	-5.198	3.400	35.260	57.660	ya8
9.490E+00	-0.421	9.589	10.643	-9.231	3.208	8.300	-1.000	mi1
6.040E+00	-8.775	4.636	6.291	-13.195	3.208	6.900	-1.000	mi2

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7.390E+01	-12.179	-3.248	-1.759	-16.387	3.203	15.360	-1.000	mi3
1.760E+02	-7.955	2.841	4.545	-8.295	3.203	21.290	-1.000	mi4
7.510E+01	-25.566	-19.041	-17.443	-30.053	3.203	14.660	-1.000	mi5
4.080E+02	-13.235	-5.637	-4.657	-13.505	3.210	29.500	-1.000	mi6
4.900E+02	-10.612	-2.245	-1.429	-9.673	3.210	32.200	-1.000	mi7
5.340E+02	-8.989	-0.749	-0.187	-8.052	3.210	33.710	-1.000	mi8
5.700E+02	-11.930	-2.105	-1.579	-8.842	3.210	34.320	-1.000	mi9
3.135E+01	-21.212	-12.600	-11.324	-24.370	3.897	12.040	79.200	tr1
8.638E+01	-12.943	-3.450	-2.061	-14.228	3.130	15.380	158.500	tr2
9.487E+01	-14.198	-5.660	-4.290	-16.264	3.130	15.900	79.200	tr3
3.803E+01	-15.330	-6.916	-5.338	-19.169	3.130	11.530	26.400	tr4
4.600E+01	-4.348	5.870	7.826	-6.196	3.130	12.860	237.700	tr5
1.720E+02	-9.302	0.581	1.744	-8.895	3.130	20.600	211.300	tr6
2.435E+02	-9.651	-0.616	0.616	-8.994	3.130	23.720	158.500	tr7
2.575E+02	-9.903	-1.359	-0.583	-9.709	3.130	4.300	79.200	tr8
2.400E+02	-7.083	2.500	3.333	-6.250	3.130	23.870	158.500	tr9
2.540E+02	-6.299	2.362	3.543	-6.181	3.130	24.550	79.200	tr10
2.470E+02	-8.907	0.000	1.215	-8.340	3.130	23.930	158.500	tr11
2.590E+02	-10.039	-1.544	-0.386	-9.691	3.130	24.360	79.200	tr12
2.440E+02	-4.098	5.328	6.557	-1.967	3.130	24.330	158.500	tr13
2.500E+02	-7.200	1.600	2.800	-5.560	3.130	24.310	79.200	tr14
5.020E+02	2.390	12.151	12.550	3.984	2.556	30.720	167.600	tu1
5.248E+02	-3.392	5.755	6.136	-2.020	2.556	30.510	167.000	tu2
5.477E+02	-0.676	8.819	9.184	1.095	2.556	31.560	167.000	tu3
5.428E+02	-1.621	7.406	7.959	-0.092	2.556	31.260	167.600	tu4
5.235E+02	2.197	11.939	12.321	3.954	2.556	31.310	167.000	tu5
3.279E+02	-4.239	3.385	4.300	-5.093	3.038	27.350	13.200	ca1
6.535E+02	-3.596	4.667	4.973	-1.622	3.038	37.120	27.700	ca2
9.531E+02	-6.411	2.613	2.717	-1.910	3.038	44.340	165.220	ca3
1.582E+02	-10.872	-3.919	-3.287	-13.970	2.720	18.680	9.100	ca4
3.745E+02	-7.877	-0.401	0.401	-8.358	2.720	26.620	24.500	ca5
6.211E+02	-9.032	-0.660	-0.338	-7.245	2.720	33.170	161.900	ca6
6.198E+02	-9.003	-2.872	-1.904	-9.116	2.453	31.400	11.280	ca7
8.796E+02	-9.163	-2.569	-2.228	-6.958	2.453	37.270	19.920	ca8
1.326E+03	-11.765	-4.223	-4.223	-6.109	2.453	46.460	161.210	ca9
3.120E+02	-12.821	-4.487	-3.846	-13.622	3.130	25.930	-1.000	ro1
3.280E+02	-12.805	-4.573	-3.659	-13.171	3.130	26.540	-1.000	ro2
3.720E+02	-12.097	-3.763	-3.226	-12.392	3.130	27.990	-1.000	ro3
4.070E+02	-16.708	-8.600	-8.108	-16.929	3.130	28.400	-1.000	ro4
4.050E+02	-11.605	-3.210	-2.469	-11.753	3.130	29.040	-1.000	ob1
4.380E+02	-15.297	-7.078	-6.621	-15.137	3.130	29.520	-1.000	ob2
err-avg	-8.57	0.304	1.19	-8.40				
err-sd	5.53	6.19	6.11	6.76				

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exp. data	SAS-27G	SAS-44G	SAS-238G	SWAT	Enrich.	Burnup	z-locat.	Sample Id
2.829E+02	0.389	-4.913	-2.793	-7.494	3.038	27.350	13.200	ya1
3.900E+02	-6.410	-11.282	-8.974	-12.462	3.038	37.120	27.700	ya2
4.330E+02	-5.312	-10.393	-7.852	-10.716	3.038	44.340	165.220	ya3
2.204E+02	-1.996	-7.895	-5.626	-12.250	2.720	18.680	9.100	ya4
3.275E+02	1.069	-4.733	-2.595	-8.366	2.720	26.620	24.500	ya5
3.966E+02	2.622	-3.177	-0.656	-5.572	2.720	33.170	161.900	ya6
3.900E+02	-2.564	-7.949	-4.103	-11.333	2.453	31.400	11.280	ya7
4.825E+02	-13.782	-18.342	-14.819	-21.078	2.453	37.270	19.920	ya8
7.205E+02	-37.266	-40.458	-37.821	-41.721	2.453	46.460	161.210	mi1
err-avg	-7.03	-12.1	-9.47	-14.6				
err-sd	12.4	11.5	11.4	11.1				

6 Am-242

exp. data	SAS-27G	SAS-44G	SAS-238G	SWAT	Enrich.	Burnup	z-locat.	Sample	Id
1.388E+00	35.447	19.597	25.360	-18.660	3.130	20.600	211.300	ya1	
2.125E+00	3.059	-8.235	-4.000	-37.271	3.130	23.720	158.500	ya2	
2.257E+00	-4.741	-15.374	-10.944	-42.047	3.130	4.300	79.200	ya3	
2.440E+00	-11.066	-20.492	-16.803	-45.779	3.130	24.550	79.200	ya4	
1.962E+00	12.640	0.408	4.995	-31.346	3.130	23.930	158.500	ya5	
2.191E+00	-1.871	-12.369	-8.261	-40.119	3.130	24.360	79.200	ya6	
err-avg	5.58	-6.08	-1.61	-35.9					
err-sd	16.7	14.4	15.1	9.73					

6 Am-243

exp. data	SAS-27G	SAS-44G	SAS-238G	SWAT	Enrich.	Burnup	z-locat.	Sample	Id
2.394E+01	-1.838	6.516	6.934	-18.713	3.130	20.600	211.300	ya1	
4.533E+01	-16.170	-9.773	-9.773	-30.488	3.130	23.720	158.500	ya2	
4.584E+01	-12.304	-5.541	-5.541	-27.378	3.130	4.300	79.200	ya3	
4.615E+01	-9.859	-2.925	-3.142	-25.330	3.130	24.550	79.200	ya4	
4.452E+01	-11.950	-5.211	-5.211	-27.022	3.130	23.930	158.500	ya5	
4.247E+01	-4.403	2.661	2.661	-20.956	3.130	24.360	79.200	ya6	
err-avg	-9.42	-2.38	-2.35	-25.0					
err-sd	5.35	5.96	6.09	4.38					

15 Cm-242

exp. data	SAS-27G	SAS-44G	SAS-238G	SWAT	Enrich.	Burnup	z-locat.	Sample	Id
1.769E+01	-20.294	-29.339	-27.643	-29.565	3.130	20.600	211.300	ya1	
2.435E+01	-20.329	-29.774	-27.721	-29.487	3.130	23.720	158.500	ya2	
2.664E+01	-24.925	-33.559	-32.057	-33.483	3.130	4.300	79.200	ya3	
2.318E+01	-15.444	-24.935	-23.210	-24.849	3.130	23.870	158.500	ya4	
2.512E+01	-18.790	-27.946	-26.354	-27.826	3.130	24.550	79.200	ya5	
2.796E+01	-29.542	-37.411	-35.980	-37.339	3.130	23.930	158.500	ya6	
2.466E+01	-18.491	-27.818	-26.196	-27.737	3.130	24.360	79.200	ya7	
2.522E+01	-18.715	-28.232	-26.249	-59.833	3.130	24.330	158.500	ya8	
2.481E+01	-19.387	-28.658	-27.046	-60.210	3.130	24.310	79.200	mi1	
1.710E+01	-25.146	-32.749	-31.579	-35.263	3.130	25.930	-1.000	mi2	
1.940E+01	-26.289	-33.505	-32.474	-34.897	3.130	26.540	-1.000	mi3	
1.850E+01	-16.757	-24.865	-23.784	-26.703	3.130	27.990	-1.000	mi4	
2.010E+01	-21.393	-29.353	-28.358	-31.244	3.130	28.400	-1.000	mi5	
2.080E+01	-20.673	-28.365	-26.923	-30.240	3.130	29.040	-1.000	mi6	
2.150E+01	-19.535	-27.442	-26.512	-29.163	3.130	29.520	-1.000	mi7	
err-avg	-21.0	-29.6	-28.1	-34.5					
err-sd	3.82	3.39	3.45	10.9					

15 Cm-244

exp. data	SAS-27G	SAS-44G	SAS-238G	SWAT	Enrich.	Burnup	z-locat.	Sample	Id
4.675E+00	-23.422	-7.166	-0.535	-28.021	3.130	20.600	211.300	ya1	
9.017E+00	-24.476	-9.726	-3.405	-29.167	3.130	23.720	158.500	ya2	
9.904E+00	-26.191	-11.854	-5.897	-30.977	3.130	4.300	79.200	ya3	
8.960E+00	-21.652	-6.473	0.000	-26.585	3.130	23.870	158.500	ya4	
9.422E+00	-18.807	-2.993	3.587	-23.965	3.130	24.550	79.200	ya5	
9.155E+00	-22.447	-7.373	-0.928	-27.286	3.130	23.930	158.500	ya6	
9.734E+00	-24.081	-9.390	-3.123	-28.981	3.130	24.360	79.200	ya7	
9.524E+00	-19.467	-3.927	2.688	-24.234	3.130	24.330	158.500	ya8	
8.786E+00	-16.913	-0.637	6.078	-21.876	3.130	24.310	79.200	mi1	
1.030E+01	-25.922	-12.816	-7.087	-34.631	3.130	25.930	-1.000	mi2	
1.160E+01	-24.914	-12.069	-6.034	-35.250	3.130	26.540	-1.000	mi3	
1.410E+01	-21.277	-7.801	-1.418	-30.965	3.130	27.990	-1.000	mi4	
1.580E+01	-24.684	-12.025	-6.329	-33.797	3.130	28.400	-1.000	mi5	
1.690E+01	-21.893	-8.284	-2.367	-31.065	3.130	29.040	-1.000	mi6	
1.920E+01	-25.521	-12.500	-6.771	-34.375	3.130	29.520	-1.000	mi7	

err-avg	-22.8	-8.34	-2.10	-29.4					
err-sd	2.77	3.72	4.04	4.15					
9 Se-79									
exp. data	SAS-27G	SAS-44G	SAS-238G	SWAT	Enrich.	Burnup	z-locat.	Sample	Id
3.765E+00	8.898	8.898	8.632	4.223	3.038	27.350	13.200	ya1	
4.995E+00	8.909	8.909	8.709	1.842	3.038	37.120	27.700	ya2	
5.370E+00	18.808	18.808	18.808	9.237	3.038	44.340	165.220	ya3	
2.838E+00	0.070	-0.282	-0.282	-2.819	2.720	18.680	9.100	ya4	
3.798E+00	4.529	4.529	4.265	-0.184	2.720	26.620	24.500	ya5	
4.584E+00	6.021	6.021	6.021	-0.218	2.720	33.170	161.900	ya6	
3.459E+00	32.986	32.986	32.986	24.371	2.453	31.400	11.280	ya7	
4.659E+00	15.261	15.261	15.261	5.752	2.453	37.270	19.920	ya8	
4.957E+00	31.935	31.935	31.935	17.369	2.453	46.460	161.210	mi1	
err-avg	14.2	14.1	14.0	6.62					
err-sd	11.8	11.8	11.9	9.01					
9 Sr-90									
exp. data	SAS-27G	SAS-44G	SAS-238G	SWAT	Enrich.	Burnup	z-locat.	Sample	Id
3.815E+02	5.374	5.374	5.111	5.505	3.038	27.350	13.200	ya1	
4.904E+02	2.569	2.569	2.365	3.079	3.038	37.120	27.700	ya2	
5.470E+02	3.473	3.656	3.291	4.205	3.038	44.340	165.220	ya3	
2.793E+02	1.683	1.683	1.325	1.719	2.720	18.680	9.100	ya4	
3.665E+02	2.592	2.592	2.319	2.701	2.720	26.620	24.500	ya5	
4.347E+02	1.219	1.219	0.989	1.610	2.720	33.170	161.900	ya6	
3.857E+02	2.670	2.930	2.411	3.759	2.453	31.400	11.280	ya7	
4.305E+02	3.368	3.600	3.136	4.599	2.453	37.270	19.920	ya8	
5.021E+02	2.171	2.171	1.972	3.366	2.453	46.460	161.210	mi1	
err-avg	2.79	2.87	2.55	3.39					
err-sd	1.21	1.24	1.22	1.29					
13 Tc-99									
exp. data	SAS-27G	SAS-44G	SAS-238G	SWAT	Enrich.	Burnup	z-locat.	Sample	Id
6.415E+02	4.131	4.443	5.066	7.825	3.038	27.350	13.200	ya1	
8.228E+02	5.372	5.858	6.952	10.112	3.038	37.120	27.700	ya2	
9.033E+02	10.594	11.812	12.919	16.462	3.038	44.340	165.220	ya3	
4.730E+02	-0.423	-0.211	0.211	2.262	2.720	18.680	9.100	ya4	
6.268E+02	3.542	3.861	4.499	6.892	2.720	26.620	24.500	ya5	
7.560E+02	3.571	4.101	5.026	7.659	2.720	33.170	161.900	ya6	
5.151E+02	44.438	44.826	45.991	50.320	2.453	31.400	11.280	ya7	
5.994E+02	42.976	43.477	45.145	49.683	2.453	37.270	19.920	ya8	
7.292E+02	39.879	39.879	42.622	47.422	2.453	46.460	161.210	mi1	
3.639E+02	11.569	11.844	12.119	12.091	2.561	16.020	11.000	mi2	
5.412E+02	7.908	8.093	8.832	8.962	2.561	23.810	26.000	mi3	
5.987E+02	13.913	14.415	15.250	15.600	2.561	28.470	199.000	mi4	
6.756E+02	10.568	11.012	12.049	12.493	2.561	31.660	226.000	mi5	
err-avg	15.2	15.6	16.7	19.1					
err-sd	16.0	16.0	16.5	17.6					
4 Ru-106									
exp. data	SAS-27G	SAS-44G	SAS-238G	SWAT	Enrich.	Burnup	z-locat.	Sample	Id
4.192E+01	-7.443	-7.204	-6.011	-8.349	3.897	12.040	79.200	ya1	
6.328E+01	2.244	2.244	3.508	1.233	3.130	15.380	158.500	ya2	
6.761E+01	-0.459	-0.606	0.725	-1.686	3.130	15.900	79.200	ya3	
4.637E+01	-10.287	-10.287	-8.993	-11.581	3.130	11.530	26.400	ya4	
err-avg	-3.99	-3.96	-2.69	-5.10					
err-sd	5.86	5.78	5.80	5.90					
6 Sn-126									
exp. data	SAS-27G	SAS-44G	SAS-238G	SWAT	Enrich.	Burnup	z-locat.	Sample	Id
3.438E+00	179.232	178.650	180.396	220.244	2.720	18.680	9.100	ya1	

5.437E+00	181.405	179.566	181.405	220.765	2.720	26.620	24.500	ya2
6.756E+00	201.954	201.954	203.434	244.435	2.720	33.170	161.900	ya3
5.637E+00	247.703	247.703	249.477	293.294	2.453	31.400	11.280	ya4
6.397E+00	282.992	281.429	284.555	333.172	2.453	37.270	19.920	ya5
8.396E+00	285.898	285.898	287.089	338.423	2.453	46.460	161.210	ya6
err-avg	230.	229.	231.	275.				
err-sd	48.9	49.1	49.3	54.1				

3 I-129

exp. data	SAS-27G	SAS-44G	SAS-238G	SWAT	Enrich.	Burnup	z-locat.	Sample Id
1.124E+02	-11.655	-11.655	-11.477	-17.749	2.720	18.680	9.100	ya1
1.548E+02	-5.685	-6.331	-5.685	-12.662	2.720	26.620	24.500	ya2
2.159E+02	-14.775	-14.775	-14.775	-20.704	2.720	33.170	161.900	ya3
err-avg	-10.7	-10.9	-10.6	-17.0				
err-sd	4.62	4.27	4.60	4.07				

3 Cs-133

exp. data	SAS-27G	SAS-44G	SAS-238G	SWAT	Enrich.	Burnup	z-locat.	Sample Id
9.644E+02	1.203	1.514	1.825	0.601	3.038	27.350	13.200	ya1
1.237E+03	1.859	2.668	2.668	1.536	3.038	37.120	27.700	ya2
1.407E+03	2.345	3.056	3.767	2.630	3.038	44.340	165.220	ya3
err-avg	1.80	2.41	2.75	1.59				
err-sd	0.573	0.802	0.974	1.02				

16 Cs-134

exp. data	SAS-27G	SAS-44G	SAS-238G	SWAT	Enrich.	Burnup	z-locat.	Sample Id
2.108E+01	-19.829	-23.150	-24.573	-22.818	3.897	12.040	79.200	ya1
3.598E+01	-16.064	-19.400	-21.345	-18.566	3.130	15.380	158.500	ya2
3.808E+01	-16.492	-19.643	-21.744	-18.986	3.130	15.900	79.200	ya3
2.095E+01	-19.809	-22.673	-24.105	-22.578	3.130	11.530	26.400	ya4
1.927E+01	-20.083	-22.678	-24.754	-22.263	3.130	12.860	237.700	ya5
4.682E+01	-16.916	-20.120	-22.683	-18.582	3.130	20.600	211.300	ya6
5.877E+01	-13.731	-16.964	-19.687	-15.110	3.130	23.720	158.500	ya7
6.022E+01	-12.488	-15.809	-18.466	-13.999	3.130	4.300	79.200	ya8
7.943E+01	-35.289	-37.807	-39.821	-36.409	3.130	23.870	158.500	mi1
6.151E+01	-12.697	-15.949	-18.712	-14.128	3.130	24.550	79.200	mi2
6.138E+01	-13.816	-17.074	-19.681	-15.233	3.130	24.360	79.200	mi3
5.925E+01	-10.042	-13.586	-16.287	1.367	3.130	24.330	158.500	mi4
6.046E+01	-12.835	-16.143	-18.789	-1.886	3.130	24.310	79.200	mi5
1.135E+01	0.441	-3.084	-5.727	-3.260	3.038	27.350	13.200	mi6
2.269E+01	-9.211	-12.737	-15.381	-11.944	3.038	37.120	27.700	mi7
3.404E+01	-15.394	-18.625	-21.269	-17.039	3.038	44.340	165.220	mi8
err-avg	-15.3	-18.5	-20.8	-15.7				
err-sd	7.33	7.08	6.84	9.15				

9 Cs-135

exp. data	SAS-27G	SAS-44G	SAS-238G	SWAT	Enrich.	Burnup	z-locat.	Sample Id
4.085E+02	9.425	3.794	4.774	4.137	3.038	27.350	13.200	ya1
4.538E+02	8.197	2.027	3.129	1.697	3.038	37.120	27.700	ya2
4.879E+02	7.399	1.250	2.480	0.615	3.038	44.340	165.220	ya3
2.748E+02	9.534	4.076	4.803	5.022	2.720	18.680	9.100	ya4
3.073E+02	9.990	3.807	4.784	4.100	2.720	26.620	24.500	ya5
3.270E+02	11.315	4.893	6.116	4.832	2.720	33.170	161.900	ya6
3.979E+02	12.088	5.805	7.565	3.242	2.453	31.400	11.280	ya7
4.087E+02	14.754	8.148	9.861	4.698	2.453	37.270	19.920	ya8
4.718E+02	7.885	1.738	3.646	-1.823	2.453	46.460	161.210	mi1
err-avg	10.1	3.95	5.24	2.95				
err-sd	2.34	2.18	2.31	2.33				

26 Cs-137

exp. data	SAS-27G	SAS-44G	SAS-238G	SWAT	Enrich.	Burnup	z-locat.	Sample Id
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4.476E+02	1.430	1.430	1.206	0.223	3.897	12.040	79.200	ya1
5.687E+02	1.635	1.635	1.635	0.932	3.130	15.380	158.500	ya2
5.762E+02	3.783	3.783	3.783	3.002	3.130	15.900	79.200	ya3
4.177E+02	3.902	3.902	3.902	2.897	3.130	11.530	26.400	ya4
4.527E+02	0.950	0.950	0.950	0.110	3.130	12.860	237.700	ya5
7.282E+02	0.522	0.522	0.385	-0.082	3.130	20.600	211.300	ya6
8.322E+02	1.178	1.178	1.178	0.745	3.130	23.720	158.500	ya7
8.449E+02	2.261	2.142	2.142	1.693	3.130	4.300	79.200	ya8
8.354E+02	1.508	1.508	1.389	0.994	3.130	23.870	158.500	mi1
8.712E+02	0.092	0.092	0.092	-0.379	3.130	24.550	79.200	mi2
8.627E+02	0.383	0.267	0.267	-0.174	3.130	24.360	79.200	mi3
8.458E+02	2.152	2.152	2.152	5.060	3.130	24.330	158.500	mi4
8.562E+02	0.911	0.911	0.794	3.702	3.130	24.310	79.200	mi5
8.736E+02	1.763	1.648	1.648	0.664	3.038	27.350	13.200	mi6
1.180E+03	1.695	1.695	1.695	1.271	3.038	37.120	27.700	mi7
1.418E+03	1.551	1.551	0.846	0.776	3.038	44.340	165.220	mi8
5.985E+02	0.084	0.084	0.084	-1.036	2.720	18.680	9.100	mi9
8.514E+02	0.305	0.188	0.188	-0.681	2.720	26.620	24.500	tr1
1.051E+03	0.856	0.856	0.856	0.381	2.720	33.170	161.900	tr2
9.739E+02	-0.503	-0.606	-0.606	-1.222	2.453	31.400	11.280	tr3
1.116E+03	3.047	3.047	3.047	2.509	2.453	37.270	19.920	tr4
1.460E+03	-2.055	-2.055	-2.055	-2.192	2.453	46.460	161.210	tr5
4.681E+02	0.192	0.192	0.192	-0.705	2.561	16.020	11.000	tr6
7.027E+02	-0.811	-0.811	-0.811	-1.494	2.561	23.810	26.000	tr7
8.174E+02	3.866	3.866	3.866	3.340	2.561	28.470	199.000	tr8
9.296E+02	1.549	1.549	1.549	1.086	2.561	31.660	226.000	tr9
err-avg	1.24	1.22	1.17	0.824				
err-sd	1.43	1.43	1.43	1.75				

4 Ce-144

exp. data	SAS-27G	SAS-44G	SAS-238G	SWAT	Enrich.	Burnup	z-locat.	Sample Id
1.810E+02	-2.210	-2.210	-2.762	-3.094	3.897	12.040	79.200	ya1
2.245E+02	-3.341	-3.341	-3.786	-4.009	3.130	15.380	158.500	ya2
2.197E+02	1.957	1.957	1.502	1.365	3.130	15.900	79.200	ya3
1.746E+02	-4.926	-4.926	-4.926	-5.212	3.130	11.530	26.400	ya4
err-avg	-2.13	-2.13	-2.49	-2.74				
err-sd	2.94	2.94	2.81	2.87				

3 Nd-143

exp. data	SAS-27G	SAS-44G	SAS-238G	SWAT	Enrich.	Burnup	z-locat.	Sample Id
6.955E+02	1.222	0.503	0.791	-0.129	3.038	27.350	13.200	ya1
8.124E+02	1.059	-0.172	0.566	-0.517	3.038	37.120	27.700	ya2
8.657E+02	1.767	0.266	1.421	0.150	3.038	44.340	165.220	ya3
err-avg	1.35	0.199	0.926	-0.165				
err-sd	0.371	0.343	0.443	0.335				

3 Nd-144

exp. data	SAS-27G	SAS-44G	SAS-238G	SWAT	Enrich.	Burnup	z-locat.	Sample Id
1.070E+03	0.000	0.935	0.000	0.000	3.038	27.350	13.200	ya1
1.518E+03	0.132	0.791	0.132	0.264	3.038	37.120	27.700	ya2
1.864E+03	-0.215	0.322	-0.215	-0.054	3.038	44.340	165.220	ya3
err-avg	-0.276E-01	0.682	-0.276E-01	0.700E-01				
err-sd	0.175	0.320	0.175	0.170				

3 Nd-145

exp. data	SAS-27G	SAS-44G	SAS-238G	SWAT	Enrich.	Burnup	z-locat.	Sample Id
5.787E+02	0.570	0.052	0.052	0.242	3.038	27.350	13.200	ya1
7.409E+02	0.283	-0.391	-0.391	0.243	3.038	37.120	27.700	ya2
8.441E+02	0.344	-0.604	-0.486	0.557	3.038	44.340	165.220	ya3
err-avg	0.399	-0.315	-0.275	0.347				

err-sd	0.151	0.335	0.287	0.182							
3 Nd-146											
exp. data	SAS-27G	SAS-44G	SAS-238G	SWAT	Enrich.	Burnup	z-locat.	Sample	Id		
5.560E+02	0.540	1.079	0.899	-0.809	3.038	27.350	13.200	ya1			
7.738E+02	0.414	1.189	0.930	-0.685	3.038	37.120	27.700	ya2			
9.417E+02	0.350	1.306	0.988	-0.520	3.038	44.340	165.220	ya3			
err-avg	0.435	1.19	0.939	-0.672							
err-sd	0.963E-01	0.114	0.448E-01	0.145							
16 Nd-148											
exp. data	SAS-27G	SAS-44G	SAS-238G	SWAT	Enrich.	Burnup	z-locat.	Sample	Id		
2.307E+02	-1.604	-1.170	-1.604	-0.824	3.130	20.600	211.300	ya1			
2.655E+02	-1.695	-1.318	-1.695	-0.753	3.130	23.720	158.500	ya2			
2.719E+02	-1.434	-1.434	-1.434	-0.699	3.130	4.300	79.200	ya3			
2.666E+02	-1.350	-1.350	-1.350	-0.563	3.130	23.870	158.500	ya4			
2.740E+02	-1.095	-1.095	-1.095	-0.474	3.130	24.550	79.200	ya5			
2.676E+02	-1.345	-1.345	-1.345	-0.673	3.130	23.930	158.500	ya6			
2.722E+02	-1.176	-1.176	-1.543	-0.551	3.130	24.360	79.200	ya7			
2.706E+02	-0.961	-0.961	-0.961	-0.074	3.130	24.330	158.500	ya8			
3.342E+02	1.735	1.735	1.735	2.932	2.556	30.720	167.600	mi1			
3.320E+02	1.506	1.506	1.506	2.892	2.556	30.510	167.000	mi2			
3.434E+02	1.631	1.631	1.631	2.970	2.556	31.560	167.000	mi3			
3.400E+02	1.765	1.765	1.765	3.000	2.556	31.260	167.600	mi4			
3.405E+02	1.615	1.615	1.615	2.996	2.556	31.310	167.000	mi5			
3.007E+02	0.432	0.432	0.432	0.632	3.038	27.350	13.200	mi6			
4.073E+02	0.417	0.417	0.417	1.105	3.038	37.120	27.700	mi7			
4.856E+02	0.288	0.288	0.288	1.503	3.038	44.340	165.220	mi8			
err-avg	-0.794E-01	-0.287E-01	-0.102	0.839							
err-sd	1.38	1.33	1.40	1.62							
3 Nd-150											
exp. data	SAS-27G	SAS-44G	SAS-238G	SWAT	Enrich.	Burnup	z-locat.	Sample	Id		
1.407E+02	2.345	2.345	2.345	0.995	3.038	27.350	13.200	ya1			
1.952E+02	3.484	3.484	3.484	2.305	3.038	37.120	27.700	ya2			
2.360E+02	4.237	4.237	4.237	3.517	3.038	44.340	165.220	ya3			
err-avg	3.36	3.36	3.36	2.27							
err-sd	0.952	0.952	0.952	1.26							
3 Sm-148											
exp. data	SAS-27G	SAS-44G	SAS-238G	SWAT	Enrich.	Burnup	z-locat.	Sample	Id		
1.203E+02	-16.874	-17.706	-19.867	-12.801	3.038	27.350	13.200	ya1			
1.861E+02	-13.487	-14.562	-16.711	-5.373	3.038	37.120	27.700	ya2			
2.519E+02	-17.428	-18.222	-19.809	-6.511	3.038	44.340	165.220	ya3			
err-avg	-15.9	-16.8	-18.8	-8.23							
err-sd	2.13	1.98	1.81	4.00							
3 Sm-149											
exp. data	SAS-27G	SAS-44G	SAS-238G	SWAT	Enrich.	Burnup	z-locat.	Sample	Id		
3.290E+00	-25.228	-31.611	-31.003	-40.547	3.038	27.350	13.200	ya1			
3.404E+00	-20.975	-27.438	-26.851	-38.337	3.038	37.120	27.700	ya2			
5.333E+00	-44.872	-49.184	-48.622	-57.135	3.038	44.340	165.220	ya3			
err-avg	-30.4	-36.1	-35.5	-45.3							
err-sd	12.7	11.5	11.6	10.3							
3 Sm-150											
exp. data	SAS-27G	SAS-44G	SAS-238G	SWAT	Enrich.	Burnup	z-locat.	Sample	Id		
2.349E+02	-2.086	-2.512	-0.809	-9.706	3.038	27.350	13.200	ya1			
3.075E+02	4.715	3.740	6.667	-4.130	3.038	37.120	27.700	ya2			
4.096E+02	-4.541	-5.762	-2.100	-12.842	3.038	44.340	165.220	ya3			
err-avg	-0.637	-1.51	1.25	-8.89							
err-sd	4.80	4.83	4.73	4.41							

3 Sm-152

exp. data	SAS-27G	SAS-44G	SAS-238G	SWAT	Enrich.	Burnup	z-locat.	Sample Id
9.871E+01	11.438	14.477	3.333	13.970	3.038	27.350	13.200	ya1
1.180E+02	21.186	23.729	9.322	22.627	3.038	37.120	27.700	ya2
1.373E+02	19.446	22.360	4.880	19.665	3.038	44.340	165.220	ya3
err-avg	17.4	20.2	5.84	18.8				
err-sd	5.20	4.99	3.11	4.40				

3 Eu-153

exp. data	SAS-27G	SAS-44G	SAS-238G	SWAT	Enrich.	Burnup	z-locat.	Sample Id
8.963E+01	-5.724	0.971	5.099	-9.885	3.038	27.350	13.200	ya1
1.237E+02	0.243	11.560	13.985	-2.021	3.038	37.120	27.700	ya2
1.679E+02	-8.874	2.442	3.633	-10.482	3.038	44.340	165.220	ya3
err-avg	-4.79	4.99	7.57	-7.46				
err-sd	4.63	5.74	5.60	4.72				

9 Eu-154

exp. data	SAS-27G	SAS-44G	SAS-238G	SWAT	Enrich.	Burnup	z-locat.	Sample Id
5.074E+00	12.140	-21.758	-18.605	-31.297	3.130	12.860	237.700	ya1
1.357E+01	16.433	-21.887	-18.939	-33.552	3.130	20.600	211.300	ya2
1.720E+01	22.093	-19.186	-16.279	-32.209	3.130	23.720	158.500	ya3
1.594E+01	36.763	-10.289	-6.524	-24.906	3.130	4.300	79.200	ya4
1.706E+01	24.853	-17.937	-14.420	-30.832	3.130	23.870	158.500	ya5
1.852E+01	20.410	-21.166	-17.927	-34.179	3.130	24.550	79.200	ya6
1.658E+01	32.690	-13.148	-9.530	-27.503	3.130	24.360	79.200	ya7
1.708E+01	29.391	-14.520	-11.007	-27.459	3.130	24.330	158.500	ya8
1.783E+01	22.266	-19.798	-16.433	-32.025	3.130	24.310	79.200	mi1
err-avg	24.1	-17.7	-14.4	-30.4				
err-sd	7.79	4.16	4.41	3.13				

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exp. data	SAS-27G	SAS-44G	SAS-238G	SWAT	Enrich.	Burnup	z-locat.	Sample Id
9.718E+05	0.390	0.390	0.398	0.402	3.400	15.950	220.220	ya1
9.538E+05	0.329	0.328	0.241	0.241	3.400	30.390	138.940	ya2
9.512E+05	0.456	0.455	0.474	0.411	3.400	31.330	57.660	ya3
9.566E+05	1.425	1.425	1.432	1.397	3.400	20.190	17.020	ya4
9.511E+05	0.342	0.446	0.370	0.308	3.400	32.030	138.940	ya5
9.521E+05	0.358	0.347	0.375	0.298	3.400	31.410	57.660	ya6
9.473E+05	0.282	0.279	0.202	0.166	3.400	35.970	138.940	ya7
9.484E+05	0.290	0.286	0.208	0.173	3.400	35.260	57.660	ya8
9.878E+05	-0.042	-0.042	-0.043	0.003	3.208	8.300	-1.000	mi1
9.887E+05	0.059	0.068	0.068	0.067	3.208	6.900	-1.000	mi2
9.772E+05	0.009	0.018	0.017	0.099	3.203	15.360	-1.000	mi3
9.698E+05	-0.063	-0.064	-0.044	0.054	3.203	21.290	-1.000	mi4
9.781E+05	0.060	0.060	0.069	0.106	3.203	14.660	-1.000	mi5
9.606E+05	-0.120	-0.120	-0.104	-0.001	3.210	29.500	-1.000	mi6
9.572E+05	-0.058	-0.058	-0.040	0.007	3.210	32.200	-1.000	mi7
9.562E+05	-0.120	-0.121	-0.209	-0.068	3.210	33.710	-1.000	mi8
9.542E+05	-0.129	-0.019	-0.104	0.005	3.210	34.320	-1.000	mi9
9.807E+05	0.072	0.072	0.080	0.109	3.897	12.040	79.200	tr1
9.759E+05	0.043	0.052	0.060	0.081	3.130	15.380	158.500	tr2
9.751E+05	0.085	0.085	0.104	0.101	3.130	15.900	79.200	tr3
9.822E+05	-0.074	-0.063	-0.065	0.016	3.130	11.530	26.400	tr4
9.806E+05	-0.090	-0.081	-0.072	-0.039	3.130	12.860	237.700	tr5
9.695E+05	0.029	0.028	-0.056	0.021	3.130	20.600	211.300	tr6
9.654E+05	-0.007	-0.008	0.009	0.026	3.130	23.720	158.500	tr7
9.652E+05	-0.024	-0.024	-0.110	-0.012	3.130	4.300	79.200	tr8
9.656E+05	-0.041	-0.042	-0.025	-0.015	3.130	23.870	158.500	tr9
9.641E+05	-0.018	0.086	0.000	0.075	3.130	24.550	79.200	tr10

9.651E+05	0.016	0.016	-0.070	0.030	3.130	23.930	158.500	tr11
9.639E+05	0.109	0.108	0.012	0.107	3.130	24.360	79.200	tr12
9.650E+05	-0.102	0.002	-0.084	-0.015	3.130	24.330	158.500	tr13
9.631E+05	0.195	0.195	0.109	0.207	3.130	24.310	79.200	tr14
9.595E+05	-0.154	-0.151	-0.138	-0.051	2.556	30.720	167.600	tu1
9.597E+05	-0.169	-0.063	-0.153	-0.045	2.556	30.510	167.000	tu2
9.584E+05	-0.170	-0.063	-0.154	-0.047	2.556	31.560	167.000	tu3
9.587E+05	-0.088	-0.089	-0.073	-0.038	2.556	31.260	167.600	tu4
9.588E+05	-0.107	-0.106	-0.091	-0.057	2.556	31.310	167.000	tu5
9.693E+05	-0.652	-0.653	-0.640	-0.591	3.038	27.350	13.200	ca1
9.548E+05	-0.438	-0.336	-0.425	-0.321	3.038	37.120	27.700	ca2
9.442E+05	-0.233	-0.128	-0.217	-0.104	3.038	44.340	165.220	ca3
9.848E+05	-1.160	-1.151	-1.142	-1.092	2.720	18.680	9.100	ca4
9.801E+05	-1.737	-1.635	-1.725	-1.616	2.720	26.620	24.500	ca5
9.649E+05	-1.012	-0.906	-0.997	-0.900	2.720	33.170	161.900	ca6
9.660E+05	-0.770	-0.771	-0.755	-0.699	2.453	31.400	11.280	ca7
9.640E+05	-1.316	-1.317	-1.302	-1.204	2.453	37.270	19.920	ca8
9.436E+05	-0.281	-0.281	-0.265	-0.205	2.453	46.460	161.210	ca9
9.755E+05	0.115	0.114	0.124	0.183	2.561	16.020	11.000	ro1
9.722E+05	-0.605	-0.604	-0.591	-0.489	2.561	23.810	26.000	ro2
9.564E+05	0.472	0.472	0.386	0.534	2.561	28.470	199.000	ro3
9.642E+05	-0.741	-0.738	-0.825	-0.681	2.561	31.660	226.000	ro4
1.454E+04	-1.376	-1.444	-0.138	-2.077	3.130	25.930	-1.000	ob1
1.420E+04	-0.845	-0.845	0.423	-1.683	3.130	26.540	-1.000	ob2
1.355E+04	-0.443	-0.295	0.738	-1.387	3.130	27.990	-1.000	ob3
1.341E+04	-0.671	-0.373	0.597	-1.544	3.130	28.400	-1.000	ob4
1.333E+04	-1.950	-1.650	-0.675	-2.843	3.130	29.040	-1.000	ob5
1.299E+04	-0.770	-0.462	0.539	-1.747	3.130	29.520	-1.000	ob6
err-avg	-0.208	-0.170	-0.782E-01	-0.261				
err-sd	0.578	0.552	0.510	0.741				

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exp. data	SAS-27G	SAS-44G	SAS-238G	SWAT	Enrich.	Burnup	z-locat.	Sample Id
3.041E+02	18.053	6.215	3.256	-2.664	3.038	27.350	13.200	ya1
4.039E+02	28.745	15.870	11.909	7.650	3.038	37.120	27.700	ya2
5.310E+02	19.586	7.533	3.390	0.640	3.038	44.340	165.220	ya3
1.979E+02	10.662	-1.465	-3.487	-10.814	2.720	18.680	9.100	ya4
3.395E+02	2.504	-8.100	-10.751	-15.670	2.720	26.620	24.500	ya5
3.877E+02	18.133	6.010	2.657	-1.625	2.720	33.170	161.900	ya6
2.960E+02	32.770	18.243	14.865	7.365	2.453	31.400	11.280	ya7
3.636E+02	29.813	15.787	12.211	5.831	2.453	37.270	19.920	ya8
4.280E+02	35.748	20.327	16.355	11.636	2.453	46.460	161.210	mi1
1.759E+02	5.742	-6.765	-8.471	-19.500	2.561	16.020	11.000	mi2
2.950E+02	5.424	-6.102	-8.136	-16.814	2.561	23.810	26.000	mi3
3.449E+02	14.236	2.059	-0.841	-8.524	2.561	28.470	199.000	mi4
3.778E+02	18.317	6.141	2.700	-4.685	2.561	31.660	226.000	mi5
err-avg	18.4	5.83	2.74	-3.63				
err-sd	10.8	9.70	9.06	10.2				

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exp. data	SAS-27G	SAS-44G	SAS-238G	SWAT	Enrich.	Burnup	z-locat.	Sample Id
7.861E+03	-6.675	-8.395	-5.339	-3.764	3.400	15.950	220.220	ya1
1.205E+04	-7.800	-9.011	-5.675	-1.995	3.400	30.390	138.940	ya2
1.252E+04	-10.054	-11.140	-8.010	-4.494	3.400	31.330	57.660	ya3
9.179E+03	-7.882	-9.250	-6.201	-4.121	3.400	20.190	17.020	ya4
1.266E+04	-8.852	-10.131	-6.720	-2.965	3.400	32.030	138.940	ya5
1.214E+04	-7.042	-8.245	-4.934	-1.341	3.400	31.410	57.660	ya6
1.200E+04	2.509	1.308	5.059	9.957	3.400	35.970	138.940	ya7

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1.169E+04	2.883	1.797	5.484	9.987	3.400	35.260	57.660	ya8
3.565E+03	2.339	0.924	3.002	-2.510	3.208	8.300	-1.000	mi1
3.266E+03	0.785	-1.121	1.043	-3.951	3.208	6.900	-1.000	mi2
6.188E+03	-6.597	-8.132	-6.516	-10.521	3.203	15.360	-1.000	mi3
7.454E+03	-0.711	-2.741	-0.597	-4.592	3.203	21.290	-1.000	mi4
6.327E+03	-12.905	-14.527	-12.469	-16.310	3.203	14.660	-1.000	mi5
8.894E+03	-4.756	-5.824	-3.733	-6.269	3.210	29.500	-1.000	mi6
9.449E+03	-4.847	-5.990	-3.884	-6.298	3.210	32.200	-1.000	mi7
8.975E+03	1.638	0.691	2.942	0.253	3.210	33.710	-1.000	mi8
9.586E+03	0.511	-1.095	1.116	-0.911	3.210	34.320	-1.000	mi9
5.681E+03	-3.813	-5.244	-2.439	-5.161	3.897	12.040	79.200	tr1
7.084E+03	-1.047	-2.724	0.215	-2.250	3.130	15.380	158.500	tr2
7.084E+03	-0.388	-1.953	0.987	-1.699	3.130	15.900	79.200	tr3
5.600E+03	-1.568	-3.047	-0.554	-3.578	3.130	11.530	26.400	tr4
5.866E+03	4.228	2.211	5.176	2.466	3.130	12.860	237.700	tr5
8.332E+03	1.980	0.336	3.337	1.395	3.130	20.600	211.300	tr6
8.924E+03	3.211	1.776	5.060	3.083	3.130	23.720	158.500	tr7
9.213E+03	-0.223	-1.395	1.666	-0.412	3.130	4.300	79.200	tr8
9.000E+03	2.811	1.511	4.533	2.622	3.130	23.870	158.500	tr9
9.074E+03	1.918	0.727	3.846	1.745	3.130	24.550	79.200	tr10
9.147E+03	1.290	-0.109	3.094	1.141	3.130	23.930	158.500	tr11
9.119E+03	0.921	-0.373	2.731	0.756	3.130	24.360	79.200	tr12
9.134E+03	2.628	1.128	4.226	2.641	3.130	24.330	158.500	tr13
9.070E+03	1.235	0.044	3.054	1.456	3.130	24.310	79.200	tr14
8.804E+03	3.504	2.255	4.299	0.206	2.556	30.720	167.600	tu1
8.863E+03	2.485	1.232	3.263	-0.809	2.556	30.510	167.000	tu2
9.019E+03	2.336	1.150	3.256	-0.844	2.556	31.560	167.000	tu3
9.066E+03	1.445	-0.210	2.118	-1.827	2.556	31.260	167.600	tu4
8.799E+03	4.550	3.311	5.368	1.239	2.556	31.310	167.000	tu5
8.003E+03	-1.040	-1.939	-0.327	-3.753	3.038	27.350	13.200	ca1
9.376E+03	-1.087	-1.769	-0.010	-3.240	3.038	37.120	27.700	ca2
1.024E+04	-0.149	-0.950	0.983	-1.853	3.038	44.340	165.220	ca3
6.615E+03	-2.831	-4.087	-2.412	-5.864	2.720	18.680	9.100	ca4
8.086E+03	-2.441	-3.395	-1.672	-4.740	2.720	26.620	24.500	ca5
8.857E+03	1.103	-0.015	1.939	-0.724	2.720	33.170	161.900	ca6
8.277E+03	-2.951	-2.867	-0.777	-6.535	2.453	31.400	11.280	ca7
9.007E+03	-3.474	-3.041	-0.998	-6.533	2.453	37.270	19.920	ca8
9.876E+03	-2.434	-1.887	0.320	-4.493	2.453	46.460	161.210	ca9
5.744E+03	4.392	2.886	4.956	-3.501	2.561	16.020	11.000	ro1
7.107E+03	3.907	2.591	4.765	-2.886	2.561	23.810	26.000	ro2
8.117E+03	1.467	-0.873	1.899	-5.098	2.561	28.470	199.000	ro3
8.103E+03	6.830	4.707	7.336	0.043	2.561	31.660	226.000	ro4
7.895E+03	3.002	1.203	3.103	-0.499	3.130	25.930	-1.000	ob1
7.849E+03	4.931	3.236	5.313	1.325	3.130	26.540	-1.000	ob2
8.275E+03	2.320	0.761	2.840	-0.956	3.130	27.990	-1.000	ob3
8.543E+03	-0.047	-1.650	0.363	-3.194	3.130	28.400	-1.000	ob4
8.469E+03	1.996	0.508	2.550	-1.093	3.130	29.040	-1.000	ob5
8.549E+03	2.012	0.444	2.456	-1.138	3.130	29.520	-1.000	ob6
err-avg	-0.445	-1.75	0.735	-1.86				
err-sd	4.22	4.12	4.11	4.13				

15 Am

exp. data	SAS-27G	SAS-44G	SAS-238G	SWAT	Enrich.	Burnup	z-locat.	Sample Id
2.533E+01	0.205	7.233	7.944	-18.711	3.130	20.600	211.300	ya1
4.746E+01	-15.309	-9.704	-9.514	-30.791	3.130	23.720	158.500	ya2
4.810E+01	-11.949	-6.002	-5.795	-28.066	3.130	4.300	79.200	ya3
4.859E+01	-9.920	-3.807	-3.828	-26.357	3.130	24.550	79.200	ya4

4.648E+01	-10.912	-4.974	-4.780	-27.204	3.130	23.930	158.500	ya5
4.466E+01	-4.279	1.923	2.125	-21.896	3.130	24.360	79.200	ya6
2.829E+02	0.389	-4.913	-2.793	-7.494	3.038	27.350	13.200	ya7
3.900E+02	-6.410	-11.282	-8.974	-12.462	3.038	37.120	27.700	ya8
4.330E+02	-5.312	-10.393	-7.852	-10.716	3.038	44.340	165.220	mi1
2.204E+02	-1.996	-7.895	-5.626	-12.250	2.720	18.680	9.100	mi2
3.275E+02	1.069	-4.733	-2.595	-8.366	2.720	26.620	24.500	mi3
3.966E+02	2.622	-3.177	-0.656	-5.572	2.720	33.170	161.900	mi4
3.900E+02	-2.564	-7.949	-4.103	-11.333	2.453	31.400	11.280	mi5
4.825E+02	-13.782	-18.342	-14.819	-21.078	2.453	37.270	19.920	mi6
7.205E+02	-37.266	-40.458	-37.821	-41.721	2.453	46.460	161.210	mi7
err-avg	-7.69	-8.30	-6.61	-18.9				
err-sd	9.97	10.6	10.1	10.4				

15 Cm

exp. data	SAS-27G	SAS-44G	SAS-238G	SWAT	Enrich.	Burnup	z-locat.	Sample Id
2.237E+01	-20.948	-24.704	-21.976	-29.242	3.130	20.600	211.300	ya1
3.337E+01	-21.449	-24.356	-21.150	-29.400	3.130	23.720	158.500	ya2
3.654E+01	-25.268	-27.676	-24.967	-32.804	3.130	4.300	79.200	ya3
3.214E+01	-17.175	-19.788	-16.739	-25.333	3.130	23.870	158.500	ya4
3.454E+01	-18.795	-21.139	-18.187	-26.773	3.130	24.550	79.200	ya5
3.711E+01	-27.792	-30.001	-27.334	-34.859	3.130	23.930	158.500	ya6
3.439E+01	-20.073	-22.603	-19.666	-28.089	3.130	24.360	79.200	ya7
3.474E+01	-18.921	-21.569	-18.317	-50.075	3.130	24.330	158.500	ya8
3.360E+01	-18.740	-21.330	-18.383	-50.185	3.130	24.310	79.200	mi1
2.740E+01	-25.438	-25.255	-22.372	-35.026	3.130	25.930	-1.000	mi2
3.100E+01	-25.774	-25.484	-22.581	-35.029	3.130	26.540	-1.000	mi3
3.260E+01	-18.712	-17.485	-14.110	-28.546	3.130	27.990	-1.000	mi4
3.590E+01	-22.841	-21.727	-18.663	-32.368	3.130	28.400	-1.000	mi5
3.770E+01	-21.220	-19.363	-15.915	-30.610	3.130	29.040	-1.000	mi6
4.070E+01	-22.359	-20.393	-17.199	-31.622	3.130	29.520	-1.000	mi7
err-avg	-21.7	-22.9	-19.8	-33.3				
err-sd	3.16	3.35	3.55	7.43				

9 Se

exp. data	SAS-27G	SAS-44G	SAS-238G	SWAT	Enrich.	Burnup	z-locat.	Sample Id
3.765E+00	8.898	8.898	8.632	4.223	3.038	27.350	13.200	ya1
4.995E+00	8.909	8.909	8.709	1.842	3.038	37.120	27.700	ya2
5.370E+00	18.808	18.808	18.808	9.237	3.038	44.340	165.220	ya3
2.838E+00	0.070	-0.282	-0.282	-2.819	2.720	18.680	9.100	ya4
3.798E+00	4.529	4.529	4.265	-0.184	2.720	26.620	24.500	ya5
4.584E+00	6.021	6.021	6.021	-0.218	2.720	33.170	161.900	ya6
3.459E+00	32.986	32.986	32.986	24.371	2.453	31.400	11.280	ya7
4.659E+00	15.261	15.261	15.261	5.752	2.453	37.270	19.920	ya8
4.957E+00	31.935	31.935	31.935	17.369	2.453	46.460	161.210	mi1
err-avg	14.2	14.1	14.0	6.62				
err-sd	11.8	11.8	11.9	9.01				

9 Sr

exp. data	SAS-27G	SAS-44G	SAS-238G	SWAT	Enrich.	Burnup	z-locat.	Sample Id
3.815E+02	5.374	5.374	5.111	5.505	3.038	27.350	13.200	ya1
4.904E+02	2.569	2.569	2.365	3.079	3.038	37.120	27.700	ya2
5.470E+02	3.473	3.656	3.291	4.205	3.038	44.340	165.220	ya3
2.793E+02	1.683	1.683	1.325	1.719	2.720	18.680	9.100	ya4
3.665E+02	2.592	2.592	2.319	2.701	2.720	26.620	24.500	ya5
4.347E+02	1.219	1.219	0.989	1.610	2.720	33.170	161.900	ya6
3.857E+02	2.670	2.930	2.411	3.759	2.453	31.400	11.280	ya7
4.305E+02	3.368	3.600	3.136	4.599	2.453	37.270	19.920	ya8
5.021E+02	2.171	2.171	1.972	3.366	2.453	46.460	161.210	mi1

err-avg	2.79	2.87	2.55	3.39							
err-sd	1.21	1.24	1.22	1.29							
13 Tc											
exp. data	SAS-27G	SAS-44G	SAS-238G	SWAT	Enrich.	Burnup	z-locat.	Sample	Id		
6.415E+02	4.131	4.443	5.066	7.825	3.038	27.350	13.200	ya1			
8.228E+02	5.372	5.858	6.952	10.112	3.038	37.120	27.700	ya2			
9.033E+02	10.594	11.812	12.919	16.462	3.038	44.340	165.220	ya3			
4.730E+02	-0.423	-0.211	0.211	2.262	2.720	18.680	9.100	ya4			
6.268E+02	3.542	3.861	4.499	6.892	2.720	26.620	24.500	ya5			
7.560E+02	3.571	4.101	5.026	7.659	2.720	33.170	161.900	ya6			
5.151E+02	44.438	44.826	45.991	50.320	2.453	31.400	11.280	ya7			
5.994E+02	42.976	43.477	45.145	49.683	2.453	37.270	19.920	ya8			
7.292E+02	39.879	39.879	42.622	47.422	2.453	46.460	161.210	mi1			
3.639E+02	11.569	11.844	12.119	12.091	2.561	16.020	11.000	mi2			
5.412E+02	7.908	8.093	8.832	8.962	2.561	23.810	26.000	mi3			
5.987E+02	13.913	14.415	15.250	15.600	2.561	28.470	199.000	mi4			
6.756E+02	10.568	11.012	12.049	12.493	2.561	31.660	226.000	mi5			
err-avg	15.2	15.6	16.7	19.1							
err-sd	16.0	16.0	16.5	17.6							
4 Ru											
exp. data	SAS-27G	SAS-44G	SAS-238G	SWAT	Enrich.	Burnup	z-locat.	Sample	Id		
4.192E+01	-7.443	-7.204	-6.011	-8.349	3.897	12.040	79.200	ya1			
6.328E+01	2.244	2.244	3.508	1.233	3.130	15.380	158.500	ya2			
6.761E+01	-0.459	-0.606	0.725	-1.686	3.130	15.900	79.200	ya3			
4.637E+01	-10.287	-10.287	-8.993	-11.581	3.130	11.530	26.400	ya4			
err-avg	-3.99	-3.96	-2.69	-5.10							
err-sd	5.86	5.78	5.80	5.90							
6 Sn											
exp. data	SAS-27G	SAS-44G	SAS-238G	SWAT	Enrich.	Burnup	z-locat.	Sample	Id		
3.438E+00	179.232	178.650	180.396	220.244	2.720	18.680	9.100	ya1			
5.437E+00	181.405	179.566	181.405	220.765	2.720	26.620	24.500	ya2			
6.756E+00	201.954	201.954	203.434	244.435	2.720	33.170	161.900	ya3			
5.637E+00	247.703	247.703	249.477	293.294	2.453	31.400	11.280	ya4			
6.397E+00	282.992	281.429	284.555	333.172	2.453	37.270	19.920	ya5			
8.396E+00	285.898	285.898	287.089	338.423	2.453	46.460	161.210	ya6			
err-avg	230.	229.	231.	275.							
err-sd	48.9	49.1	49.3	54.1							
3 I											
exp. data	SAS-27G	SAS-44G	SAS-238G	SWAT	Enrich.	Burnup	z-locat.	Sample	Id		
1.124E+02	-11.655	-11.655	-11.477	-17.749	2.720	18.680	9.100	ya1			
1.548E+02	-5.685	-6.331	-5.685	-12.662	2.720	26.620	24.500	ya2			
2.159E+02	-14.775	-14.775	-14.775	-20.704	2.720	33.170	161.900	ya3			
err-avg	-10.7	-10.9	-10.6	-17.0							
err-sd	4.62	4.27	4.60	4.07							
26 Cs											
exp. data	SAS-27G	SAS-44G	SAS-238G	SWAT	Enrich.	Burnup	z-locat.	Sample	Id		
4.687E+02	0.474	0.324	0.047	-0.813	3.897	12.040	79.200	ya1			
6.047E+02	0.582	0.384	0.268	-0.228	3.130	15.380	158.500	ya2			
6.143E+02	2.527	2.331	2.201	1.639	3.130	15.900	79.200	ya3			
4.387E+02	2.770	2.633	2.565	1.680	3.130	11.530	26.400	ya4			
4.720E+02	0.091	-0.015	-0.100	-0.803	3.130	12.860	237.700	ya5			
7.750E+02	-0.532	-0.725	-1.009	-1.200	3.130	20.600	211.300	ya6			
8.910E+02	0.194	-0.019	-0.199	-0.301	3.130	23.720	158.500	ya7			
9.051E+02	1.279	0.948	0.771	0.649	3.130	4.300	79.200	ya8			
9.148E+02	-1.687	-1.905	-2.189	-2.254	3.130	23.870	158.500	mi1			
9.327E+02	-0.752	-0.966	-1.148	-1.286	3.130	24.550	79.200	mi2			

9.241E+02	-0.561	-0.885	-1.058	-1.174	3.130	24.360	79.200	mi3
9.050E+02	1.354	1.121	0.945	4.819	3.130	24.330	158.500	mi4
9.167E+02	0.004	-0.214	-0.497	3.334	3.130	24.310	79.200	mi5
2.258E+03	2.903	1.955	2.252	1.246	3.038	27.350	13.200	mi6
2.893E+03	2.700	2.050	2.202	1.348	3.038	37.120	27.700	mi7
3.347E+03	2.565	1.935	2.087	1.350	3.038	44.340	165.220	mi8
8.733E+02	3.057	1.340	1.569	0.870	2.720	18.680	9.100	mi9
1.159E+03	2.874	1.148	1.407	0.587	2.720	26.620	24.500	tr1
1.378E+03	3.338	1.814	2.104	1.437	2.720	33.170	161.900	tr2
1.372E+03	3.149	1.254	1.764	0.073	2.453	31.400	11.280	tr3
1.525E+03	6.185	4.414	4.873	3.096	2.453	37.270	19.920	tr4
1.932E+03	0.373	-1.128	-0.663	-2.102	2.453	46.460	161.210	tr5
4.681E+02	0.192	0.192	0.192	-0.705	2.561	16.020	11.000	tr6
7.027E+02	-0.811	-0.811	-0.811	-1.494	2.561	23.810	26.000	tr7
8.174E+02	3.866	3.866	3.866	3.340	2.561	28.470	199.000	tr8
9.296E+02	1.549	1.549	1.549	1.086	2.561	31.660	226.000	tr9
err-avg	1.45	0.869	0.884	0.546				
err-sd	1.84	1.54	1.67	1.80				

4 Ce

exp. data	SAS-27G	SAS-44G	SAS-238G	SWAT	Enrich.	Burnup	z-locat.	Sample Id
1.810E+02	-2.210	-2.210	-2.762	-3.094	3.897	12.040	79.200	ya1
2.245E+02	-3.341	-3.341	-3.786	-4.009	3.130	15.380	158.500	ya2
2.197E+02	1.957	1.957	1.502	1.365	3.130	15.900	79.200	ya3
1.746E+02	-4.926	-4.926	-4.926	-5.212	3.130	11.530	26.400	ya4
err-avg	-2.13	-2.13	-2.49	-2.74				
err-sd	2.94	2.94	2.81	2.87				

16 Nd

exp. data	SAS-27G	SAS-44G	SAS-238G	SWAT	Enrich.	Burnup	z-locat.	Sample Id
2.307E+02	-1.604	-1.170	-1.604	-0.824	3.130	20.600	211.300	ya1
2.655E+02	-1.695	-1.318	-1.695	-0.753	3.130	23.720	158.500	ya2
2.719E+02	-1.434	-1.434	-1.434	-0.699	3.130	4.300	79.200	ya3
2.666E+02	-1.350	-1.350	-1.350	-0.563	3.130	23.870	158.500	ya4
2.740E+02	-1.095	-1.095	-1.095	-0.474	3.130	24.550	79.200	ya5
2.676E+02	-1.345	-1.345	-1.345	-0.673	3.130	23.930	158.500	ya6
2.722E+02	-1.176	-1.176	-1.543	-0.551	3.130	24.360	79.200	ya7
2.706E+02	-0.961	-0.961	-0.961	-0.074	3.130	24.330	158.500	ya8
3.342E+02	1.735	1.735	1.735	2.932	2.556	30.720	167.600	mi1
3.320E+02	1.506	1.506	1.506	2.892	2.556	30.510	167.000	mi2
3.434E+02	1.631	1.631	1.631	2.970	2.556	31.560	167.000	mi3
3.400E+02	1.765	1.765	1.765	3.000	2.556	31.260	167.600	mi4
3.405E+02	1.615	1.615	1.615	2.996	2.556	31.310	167.000	mi5
3.342E+03	0.581	0.730	0.461	-0.021	3.038	27.350	13.200	mi6
4.448E+03	0.549	0.571	0.436	0.119	3.038	37.120	27.700	mi7
5.237E+03	0.552	0.514	0.475	0.300	3.038	44.340	165.220	mi8
err-avg	-0.454E-01	0.136E-01	-0.877E-01	0.661				
err-sd	1.40	1.34	1.41	1.63				

3 Sm

exp. data	SAS-27G	SAS-44G	SAS-238G	SWAT	Enrich.	Burnup	z-locat.	Sample Id
4.572E+02	-3.224	-3.051	-5.147	-5.631	3.038	27.350	13.200	ya1
6.150E+02	2.225	1.864	-0.084	0.438	3.038	37.120	27.700	ya2
8.041E+02	-4.750	-5.151	-6.764	-5.602	3.038	44.340	165.220	ya3
err-avg	-1.92	-2.11	-4.00	-3.60				
err-sd	3.67	3.60	3.49	3.50				

12 Eu

exp. data	SAS-27G	SAS-44G	SAS-238G	SWAT	Enrich.	Burnup	z-locat.	Sample Id
5.074E+00	12.140	-21.758	-18.605	-31.297	3.130	12.860	237.700	ya1

1.357E+01	16.433	-21.887	-18.939	-33.552	3.130	20.600	211.300	ya2
1.720E+01	22.093	-19.186	-16.279	-32.209	3.130	23.720	158.500	ya3
1.594E+01	36.763	-10.289	-6.524	-24.906	3.130	4.300	79.200	ya4
1.706E+01	24.853	-17.937	-14.420	-30.832	3.130	23.870	158.500	ya5
1.852E+01	20.410	-21.166	-17.927	-34.179	3.130	24.550	79.200	ya6
1.658E+01	32.690	-13.148	-9.530	-27.503	3.130	24.360	79.200	ya7
1.708E+01	29.391	-14.520	-11.007	-27.459	3.130	24.330	158.500	ya8
1.783E+01	22.266	-19.798	-16.433	-32.025	3.130	24.310	79.200	mi1
8.963E+01	-5.724	0.971	5.099	-9.885	3.038	27.350	13.200	mi2
1.237E+02	0.243	11.560	13.985	-2.021	3.038	37.120	27.700	mi3
1.679E+02	-8.874	2.442	3.633	-10.482	3.038	44.340	165.220	mi4
err-avg	16.9	-12.1	-8.91	-24.7				
err-sd	14.8	11.1	10.9	10.9				

55 TO

exp.	data	SAS-27G	SAS-44G	SAS-238G	SWAT	Enrich.	Burnup	z-locat.	Sample	Id
9.797E+05	0.333	0.319	0.352	0.368	3.400	15.950	220.220	ya1		
9.659E+05	0.227	0.212	0.167	0.213	3.400	30.390	138.940	ya2		
9.637E+05	0.319	0.305	0.364	0.347	3.400	31.330	57.660	ya3		
9.658E+05	1.337	1.323	1.360	1.344	3.400	20.190	17.020	ya4		
9.638E+05	0.221	0.307	0.276	0.265	3.400	32.030	138.940	ya5		
9.642E+05	0.265	0.239	0.309	0.277	3.400	31.410	57.660	ya6		
9.593E+05	0.310	0.292	0.263	0.289	3.400	35.970	138.940	ya7		
9.601E+05	0.321	0.304	0.272	0.292	3.400	35.260	57.660	ya8		
9.914E+05	-0.033	-0.038	-0.032	-0.006	3.208	8.300	-1.000	mi1		
9.919E+05	0.061	0.064	0.071	0.054	3.208	6.900	-1.000	mi2		
9.833E+05	-0.032	-0.033	-0.024	0.032	3.203	15.360	-1.000	mi3		
9.772E+05	-0.068	-0.084	-0.049	0.018	3.203	21.290	-1.000	mi4		
9.844E+05	-0.023	-0.033	-0.012	0.000	3.203	14.660	-1.000	mi5		
9.695E+05	-0.162	-0.172	-0.137	-0.059	3.210	29.500	-1.000	mi6		
9.667E+05	-0.105	-0.116	-0.078	-0.055	3.210	32.200	-1.000	mi7		
9.652E+05	-0.104	-0.113	-0.180	-0.065	3.210	33.710	-1.000	mi8		
9.638E+05	-0.123	-0.030	-0.092	-0.004	3.210	34.320	-1.000	mi9		
9.870E+05	0.049	0.041	0.065	0.077	3.897	12.040	79.200	tr1		
9.839E+05	0.034	0.031	0.061	0.063	3.130	15.380	158.500	tr2		
9.831E+05	0.084	0.072	0.112	0.089	3.130	15.900	79.200	tr3		
9.884E+05	-0.082	-0.080	-0.068	-0.006	3.130	11.530	26.400	tr4		
9.870E+05	-0.064	-0.067	-0.041	-0.025	3.130	12.860	237.700	tr5		
9.789E+05	0.045	0.029	-0.029	0.030	3.130	20.600	211.300	tr6		
9.756E+05	0.021	0.006	0.053	0.051	3.130	23.720	158.500	tr7		
9.757E+05	-0.026	-0.038	-0.094	-0.018	3.130	4.300	79.200	tr8		
9.759E+05	-0.017	-0.031	0.014	0.006	3.130	23.870	158.500	tr9		
9.744E+05	-0.001	0.089	0.033	0.086	3.130	24.550	79.200	tr10		
9.746E+05	0.026	0.013	-0.042	0.037	3.130	23.930	158.500	tr11		
9.743E+05	0.116	0.102	0.035	0.109	3.130	24.360	79.200	tr12		
9.754E+05	-0.075	0.012	-0.044	0.012	3.130	24.330	158.500	tr13		
9.731E+05	0.205	0.192	0.135	0.219	3.130	24.310	79.200	tr14		
9.686E+05	-0.120	-0.128	-0.097	-0.047	2.556	30.720	167.600	tu1		
9.689E+05	-0.144	-0.051	-0.121	-0.051	2.556	30.510	167.000	tu2		
9.677E+05	-0.146	-0.052	-0.122	-0.053	2.556	31.560	167.000	tu3		
9.681E+05	-0.073	-0.090	-0.051	-0.054	2.556	31.260	167.600	tu4		
9.680E+05	-0.064	-0.074	-0.041	-0.044	2.556	31.310	167.000	tu5		
9.850E+05	-0.633	-0.647	-0.622	-0.608	3.038	27.350	13.200	ca1		
9.744E+05	-0.412	-0.326	-0.398	-0.333	3.038	37.120	27.700	ca2		
9.665E+05	-0.202	-0.117	-0.185	-0.109	3.038	44.340	165.220	ca3		
9.936E+05	-1.165	-1.169	-1.149	-1.125	2.720	18.680	9.100	ca4		
9.912E+05	-1.729	-1.644	-1.718	-1.639	2.720	26.620	24.500	ca5		

9.773E+05	-0.974	-0.890	-0.960	-0.892	2.720	33.170	161.900	ca6
9.772E+05	-0.747	-0.756	-0.721	-0.718	2.453	31.400	11.280	ca7
9.764E+05	-1.287	-1.294	-1.258	-1.218	2.453	37.270	19.920	ca8
9.578E+05	-0.279	-0.286	-0.244	-0.238	2.453	46.460	161.210	ca9
9.823E+05	0.146	0.134	0.155	0.161	2.561	16.020	11.000	ro1
9.808E+05	-0.566	-0.578	-0.550	-0.507	2.561	23.810	26.000	ro2
9.663E+05	0.496	0.472	0.410	0.496	2.561	28.470	199.000	ro3
9.743E+05	-0.661	-0.680	-0.745	-0.666	2.561	31.660	226.000	ro4
2.246E+04	0.134	-0.543	0.974	-1.563	3.130	25.930	-1.000	ob1
2.208E+04	1.173	0.571	2.129	-0.661	3.130	26.540	-1.000	ob2
2.186E+04	0.576	0.079	1.512	-1.265	3.130	27.990	-1.000	ob3
2.199E+04	-0.465	-0.904	0.474	-2.235	3.130	28.400	-1.000	ob4
2.184E+04	-0.453	-0.844	0.550	-2.213	3.130	29.040	-1.000	ob5
2.158E+04	0.291	-0.140	1.265	-1.562	3.130	29.520	-1.000	ob6
err-avg	-0.772E-01	-0.124		0.274E-01	-0.238			
err-sd	0.504	0.483		0.631	0.674			

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exp. data	SAS-27G	SAS-44G	SAS-238G	SWAT	Enrich.	Burnup	z-locat.	Sample	Id
2.680E+04	26.744	26.232	27.427	28.021	3.400	15.950	220.220	ya1	
2.607E+04	19.157	18.586	16.940	18.641	3.400	30.390	138.940	ya2	
2.449E+04	29.705	29.141	31.473	30.799	3.400	31.330	57.660	ya3	
1.632E+04	161.792	161.010	163.147	162.237	3.400	20.190	17.020	ya4	
2.546E+04	21.317	24.597	23.427	23.009	3.400	32.030	138.940	ya5	
2.515E+04	22.481	21.494	24.163	22.953	3.400	31.410	57.660	ya6	
2.485E+04	18.018	17.310	16.179	17.187	3.400	35.970	138.940	ya7	
2.459E+04	18.638	17.988	16.731	17.515	3.400	35.260	57.660	ya8	
2.898E+04	0.246	0.065	0.283	1.167	3.208	8.300	-1.000	mi1	
2.893E+04	5.551	5.647	5.891	5.310	3.208	6.900	-1.000	mi2	
2.554E+04	5.802	5.783	6.135	8.282	3.203	15.360	-1.000	mi3	
2.412E+04	1.811	1.143	2.593	5.296	3.203	21.290	-1.000	mi4	
2.599E+04	4.516	4.121	4.930	5.391	3.203	14.660	-1.000	mi5	
2.231E+04	-6.153	-6.579	-5.073	-1.661	3.210	29.500	-1.000	mi6	
2.199E+04	-1.437	-1.901	-0.227	0.787	3.210	32.200	-1.000	mi7	
2.162E+04	-6.499	-6.911	-9.866	-4.753	3.210	33.710	-1.000	mi8	
2.153E+04	-4.093	0.070	-2.708	1.225	3.210	34.320	-1.000	mi9	
3.473E+04	4.268	4.032	4.717	5.067	3.897	12.040	79.200	tr1	
2.759E+04	3.042	2.933	3.975	4.060	3.130	15.380	158.500	tr2	
2.703E+04	4.154	3.739	5.172	4.341	3.130	15.900	79.200	tr3	
2.863E+04	-1.785	-1.727	-1.308	0.857	3.130	11.530	26.400	tr4	
2.856E+04	-3.271	-3.378	-2.454	-1.901	3.130	12.860	237.700	tr5	
2.698E+04	1.994	1.431	-0.690	1.450	3.130	20.600	211.300	tr6	
2.627E+04	0.773	0.224	1.983	1.883	3.130	23.720	158.500	tr7	
2.658E+04	-1.317	-1.755	-3.817	-1.051	3.130	4.300	79.200	tr8	
2.666E+04	-0.628	-1.142	0.512	0.208	3.130	23.870	158.500	tr9	
2.553E+04	2.297	5.761	3.618	5.623	3.130	24.550	79.200	tr10	
2.547E+04	3.361	2.866	0.762	3.780	3.130	23.930	158.500	tr11	
2.533E+04	7.610	7.070	4.512	7.358	3.130	24.360	79.200	tr12	
2.660E+04	-2.003	1.201	-0.854	1.197	3.130	24.330	158.500	tr13	
2.402E+04	16.200	15.707	13.383	16.789	3.130	24.310	79.200	tr14	
1.849E+04	-6.809	-7.263	-5.640	-3.014	2.556	30.720	167.600	tu1	
1.856E+04	-9.160	-4.278	-7.948	-4.304	2.556	30.510	167.000	tu2	
1.844E+04	-8.720	-3.791	-7.478	-3.885	2.556	31.560	167.000	tu3	
1.848E+04	-5.432	-6.320	-4.318	-4.441	2.556	31.260	167.600	tu4	
1.839E+04	-4.483	-4.983	-3.243	-3.412	2.556	31.310	167.000	tu5	
3.442E+04	-33.517	-33.908	-33.211	-32.809	3.038	27.350	13.200	ca1	
3.220E+04	-20.557	-17.951	-20.112	-18.146	3.038	37.120	27.700	ca2	

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3.116E+04	-8.197	-5.557	-7.655	-5.292	3.038	44.340	165.220	ca3
3.400E+04	-65.206	-65.344	-64.744	-64.043	2.720	18.680	9.100	ca4
3.797E+04	-85.960	-83.736	-85.673	-83.611	2.720	26.620	24.500	ca5
3.020E+04	-59.689	-56.940	-59.228	-57.012	2.720	33.170	161.900	ca6
2.534E+04	-53.666	-54.001	-52.663	-52.560	2.453	31.400	11.280	ca7
3.008E+04	-78.362	-78.598	-77.427	-76.118	2.453	37.270	19.920	ca8
2.093E+04	-20.403	-20.732	-18.830	-18.525	2.453	46.460	161.210	ca9
1.928E+04	18.314	17.705	18.778	19.123	2.561	16.020	11.000	ro1
2.423E+04	-40.637	-41.118	-39.993	-38.246	2.561	23.810	26.000	ro2
1.419E+04	75.369	73.755	69.526	75.343	2.561	28.470	199.000	ro3
2.520E+04	-50.150	-50.884	-53.396	-50.337	2.561	31.660	226.000	ro4
-9.266E+05	0.666	0.682	0.645	0.707	3.130	25.930	-1.000	ob1
-9.270E+05	0.641	0.655	0.618	0.685	3.130	26.540	-1.000	ob2
-9.272E+05	0.655	0.667	0.633	0.698	3.130	27.990	-1.000	ob3
-9.271E+05	0.680	0.690	0.657	0.722	3.130	28.400	-1.000	ob4
-9.273E+05	0.679	0.689	0.656	0.721	3.130	29.040	-1.000	ob5
-9.275E+05	0.662	0.672	0.639	0.705	3.130	29.520	-1.000	ob6
err-avg	-1.84	-1.55	-1.79	-0.472				
err-sd	35.2	34.9	35.0	34.8				

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exp. data	SAS-27G	SAS-44G	SAS-238G	SWAT	Enrich.	Burnup	z-locat.	Sample Id
1.894E+04	40.618	40.607	41.030	41.216	3.400	15.950	220.220	ya1
1.402E+04	42.326	42.305	36.379	36.377	3.400	30.390	138.940	ya2
1.197E+04	71.301	71.284	72.780	67.722	3.400	31.330	57.660	ya3
7.144E+03	379.801	379.773	380.739	375.987	3.400	20.190	17.020	ya4
1.279E+04	51.180	58.973	53.267	48.719	3.400	32.030	138.940	ya5
1.301E+04	50.042	49.258	51.326	45.632	3.400	31.410	57.660	ya6
1.285E+04	32.503	32.254	26.564	23.940	3.400	35.970	138.940	ya7
1.290E+04	32.915	32.659	26.922	24.336	3.400	35.260	57.660	ya8
2.542E+04	-0.047	-0.055	-0.098	1.683	3.208	8.300	-1.000	mi1
2.566E+04	6.157	6.508	6.508	6.489	3.208	6.900	-1.000	mi2
1.935E+04	9.767	10.233	10.181	14.295	3.203	15.360	-1.000	mi3
1.667E+04	2.939	2.879	4.019	9.718	3.203	21.290	-1.000	mi4
1.966E+04	10.122	10.122	10.529	12.375	3.203	14.660	-1.000	mi5
1.342E+04	-7.079	-7.079	-5.961	1.393	3.210	29.500	-1.000	mi6
1.254E+04	1.132	1.180	2.527	6.124	3.210	32.200	-1.000	mi7
1.264E+04	-12.275	-12.306	-18.958	-8.307	3.210	33.710	-1.000	mi8
1.194E+04	-7.789	1.005	-5.779	2.940	3.210	34.320	-1.000	mi9
2.836E+04	6.009	6.009	6.291	7.286	3.897	12.040	79.200	tr1
1.961E+04	4.670	5.129	5.537	6.572	3.130	15.380	158.500	tr2
1.905E+04	5.937	5.937	6.882	6.730	3.130	15.900	79.200	tr3
2.237E+04	-1.886	-1.439	-1.529	2.025	3.130	11.530	26.400	tr4
2.221E+04	-5.326	-4.921	-4.515	-3.070	3.130	12.860	237.700	tr5
1.758E+04	2.179	2.122	-2.543	1.718	3.130	20.600	211.300	tr6
1.609E+04	-0.435	-0.497	0.559	1.579	3.130	23.720	158.500	tr7
1.609E+04	-2.039	-2.039	-7.198	-1.343	3.130	4.300	79.200	tr8
1.643E+04	-2.435	-2.495	-1.461	-0.883	3.130	23.870	158.500	tr9
1.515E+04	2.838	9.439	3.960	8.706	3.130	24.550	79.200	tr10
1.597E+04	4.739	4.739	-0.457	5.547	3.130	23.930	158.500	tr11
1.492E+04	12.437	12.370	6.135	12.276	3.130	24.360	79.200	tr12
1.624E+04	-4.809	1.348	-3.762	0.345	3.130	24.330	158.500	tr13
1.398E+04	27.048	27.048	21.110	27.842	3.130	24.310	79.200	tr14
9.351E+03	-16.823	-16.545	-15.262	-6.259	2.556	30.720	167.600	tu1
9.363E+03	-20.561	-9.699	-18.895	-7.867	2.556	30.510	167.000	tu2
9.081E+03	-20.093	-8.904	-18.485	-7.166	2.556	31.560	167.000	tu3
9.078E+03	-12.570	-12.724	-10.973	-7.331	2.556	31.260	167.600	tu4

9.246E+03	-13.303	-13.119	-11.616	-8.074	2.556	31.310	167.000	tu5
1.865E+04	-62.297	-62.318	-61.680	-59.111	3.038	27.350	13.200	ca1
1.263E+04	-53.697	-45.969	-52.707	-44.845	3.038	37.120	27.700	ca2
8.939E+03	-31.291	-20.261	-29.669	-17.746	3.038	44.340	165.220	ca3
2.523E+04	-87.307	-86.962	-86.609	-84.639	2.720	18.680	9.100	ca4
2.690E+04	-120.886	-117.184	-120.455	-116.482	2.720	26.620	24.500	ca5
1.776E+04	-102.838	-97.117	-102.022	-96.740	2.720	33.170	161.900	ca6
1.410E+04	-97.468	-97.503	-96.439	-92.561	2.453	31.400	11.280	ca7
1.766E+04	-134.122	-134.201	-133.358	-128.053	2.453	37.270	19.920	ca8
6.729E+03	-63.145	-63.219	-60.990	-52.521	2.453	46.460	161.210	ca9
1.253E+04	25.749	25.669	26.387	30.986	2.561	16.020	11.000	ro1
1.559E+04	-65.296	-65.232	-64.462	-58.067	2.561	23.810	26.000	ro2
4.310E+03	241.531	241.531	222.506	255.499	2.561	28.470	199.000	ro3
1.512E+04	-88.292	-88.094	-93.650	-84.449	2.561	31.660	226.000	ro4
-9.346E+05	0.685	0.686	0.666	0.696	3.130	25.930	-1.000	ob1
-9.349E+05	0.676	0.676	0.657	0.689	3.130	26.540	-1.000	ob2
-9.356E+05	0.669	0.667	0.652	0.683	3.130	27.990	-1.000	ob3
-9.357E+05	0.672	0.668	0.654	0.685	3.130	28.400	-1.000	ob4
-9.358E+05	0.690	0.686	0.672	0.703	3.130	29.040	-1.000	ob5
-9.361E+05	0.673	0.669	0.655	0.687	3.130	29.520	-1.000	ob6
err-avg	0.616	2.08	-0.625E-01	3.72				
err-sd	75.3	74.9	74.1	74.1				

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国際単位系(SI)と換算表

表1 SI基本単位および補助単位

量	名称	記号
長さ	メートル	m
質量	キログラム	kg
時間	秒	s
電流	アンペア	A
熱力学温度	ケルビン	K
物質量	モル	mol
光度	カンデラ	cd
平面角	ラジアン	rad
立体角	ステラジアン	sr

表3 固有の名称をもつSI組立単位

量	名称	記号	他のSI単位による表現
周波数	ヘルツ	Hz	s ⁻¹
圧力、応力	ニュートン	N	m·kg/s ²
エネルギー、仕事、熱量	パスカル	Pa	N/m ²
工率、放射束	ジュール	J	N·m
電気量、電荷	ワット	W	J/s
電位、電圧、起電力	クーロン	C	A·s
静電容量	ボルト	V	W/A
電気抵抗	アード	F	C/V
コンダクタンス	ジーメンス	S	A/V
磁束密度	ウェーバ	Wb	V·s
磁密	テスラ	T	Wb/m ²
インダクタンス	ヘンリー	H	Wb/A
セルシウス温度	セルシウス度	°C	
光束度	ルーメン	lm	cd·sr
照度	ルクス	lx	lm/m ²
放射能	ベクレル	Bq	s ⁻¹
吸収線量	グレイ	Gy	J/kg
線量等量	シーベルト	Sv	J/kg

表2 SIと併用される単位

名 称	記 号
分、時、日	min, h, d
度、分、秒	°, ', "
リットル	l, L
ト	t
電子ボルト	eV
原子質量単位	u

$$1 \text{ eV} = 1.60218 \times 10^{-19} \text{ J}$$

$$1 \text{ u} = 1.66054 \times 10^{-27} \text{ kg}$$

表5 SI接頭語

倍数	接頭語	記号
10 ¹⁸	エクサ	E
10 ¹⁵	ペタ	P
10 ¹²	テラ	T
10 ⁹	ギガ	G
10 ⁶	メガ	M
10 ³	キロ	k
10 ²	ヘクト	h
10 ¹	デカ	da
10 ⁻¹	デシ	d
10 ⁻²	センチ	c
10 ⁻³	ミリ	m
10 ⁻⁶	マイクロ	μ
10 ⁻⁹	ナノ	n
10 ⁻¹²	ピコ	p
10 ⁻¹⁵	フェムト	f
10 ⁻¹⁸	アト	a

(注)

- 表1~5は「国際単位系」第5版、国際度量衡局1985年刊行による。ただし、1eVおよび1uの値はCODATAの1986年推奨値によった。
- 表4には海里、ノット、アール、ヘクタールも含まれているが日常の単位なのでここでは省略した。
- barは、JISでは流体の圧力を表わす場合に限り表2のカテゴリーに分類されている。
- E C閣僚理事会指令ではbar、barnおよび「血圧の単位」mmHgを表2のカテゴリーに入れている。

換 算 表

圧	MPa(=10bar)	kgf/cm ²	atm	mmHg(Torr)	lbf/in ² (psi)
力	1	10.1972	9.86923	7.50062×10 ³	145.038
	0.0980665	1	0.967841	735.559	14.2233
力	0.101325	1.03323	1	760	14.6959
	1.33322×10 ⁻⁴	1.35951×10 ⁻³	1.31579×10 ⁻³	1	1.93368×10 ⁻²
	6.89476×10 ⁻³	7.03070×10 ⁻²	6.80460×10 ⁻²	51.7149	1

$$\text{粘度 } 1 \text{ Pa}\cdot\text{s} (\text{N}\cdot\text{s}/\text{m}^2) = 10 \text{ P} (\text{ポアズ}) (\text{g}/(\text{cm}\cdot\text{s}))$$

$$\text{動粘度 } 1 \text{ m}^2/\text{s} = 10^4 \text{ St} (\text{ストークス}) (\text{cm}^2/\text{s})$$

エネルギー・仕事・熱量	J(=10 ⁷ erg)	kgf·m	kW·h	cal(計量法)	Btu	ft·lbf	eV	1 cal = 4.18605J (計量法)	
								= 4.184J (熱化学)	= 4.1855J (15°C)
1	0.101972	2.77778×10 ⁻⁷	0.238889	9.47813×10 ⁻⁴	0.737562	6.24150×10 ¹⁸			= 4.1868J (国際蒸気表)
9.80665	1	2.72407×10 ⁻⁶	2.34270	9.29487×10 ⁻³	7.23301	6.12082×10 ¹⁹			仕事率 1 PS(仏馬力)
3.6×10 ⁶	3.67098×10 ⁵	1	8.59999×10 ⁵	3412.13	2.65522×10 ⁶	2.24694×10 ²⁵			= 75 kgf·m/s
4.18605	0.426858	1.16279×10 ⁻⁶	1	3.96759×10 ⁻³	3.08747	2.61272×10 ¹⁹			= 735.499W
1055.06	107.586	2.93072×10 ⁻⁴	252.042	1	778.172	6.58515×10 ²¹			
1.35582	0.138255	3.76616×10 ⁻⁷	0.323890	1.28506×10 ⁻³	1	8.46233×10 ¹⁸			
1.60218×10 ⁻¹⁹	1.63377×10 ⁻²⁰	4.45050×10 ⁻²⁰	3.82743×10 ⁻²⁰	1.51857×10 ⁻²²	1.18171×10 ⁻¹⁹	1			

放射能	Bq	Ci	Gy	rad	照射線量	C/kg	R	1 Sv = 100 rem	
								1	100
	1	2.70270×10 ⁻¹¹						0.01	1
	3.7×10 ¹⁰	1	0.01	1					

線量当量	Sv	rem	C/kg	R	照射線量	1	1 Sv = 100 rem	
							1	100
	1	100					0.01	1
	0.01	1						

