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# FBR燃料サイクル安全性の調査 報告書 (図表集)

(受託研究)

1980年6月

住友原子力工業株式会社

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本図表集は FBR 燃料サイクル安全性の調査，報告書の図表を収録したものである。図表は次のように 9 区分し，各区分毎に一連の図表番号を付して配列されている。

- 2.1 CRBR の概要
- 2.2 CRBR のソース・ターム
- 2.3 CRBR の環境影響
- 3.1 SNR-300 の概要
- 3.2 SNR-300 のソース・ターム
- 3.3 SNR-300 の環境影響
- 4.1 ソース・タームに関する評価
- 4.2 環境影響に関する評価
- 5. 「NUJEEP」

各区分毎に独立して図表をまとめたので，同じ図表で異なった番号を持ったものが数例あることを御承知置き願いたい。

図表の大部分は CRBRP 環境報告書（DOCKET-50537-2）からの引用である。原文との対比の便を考慮し，原文の図表番号を併記した。

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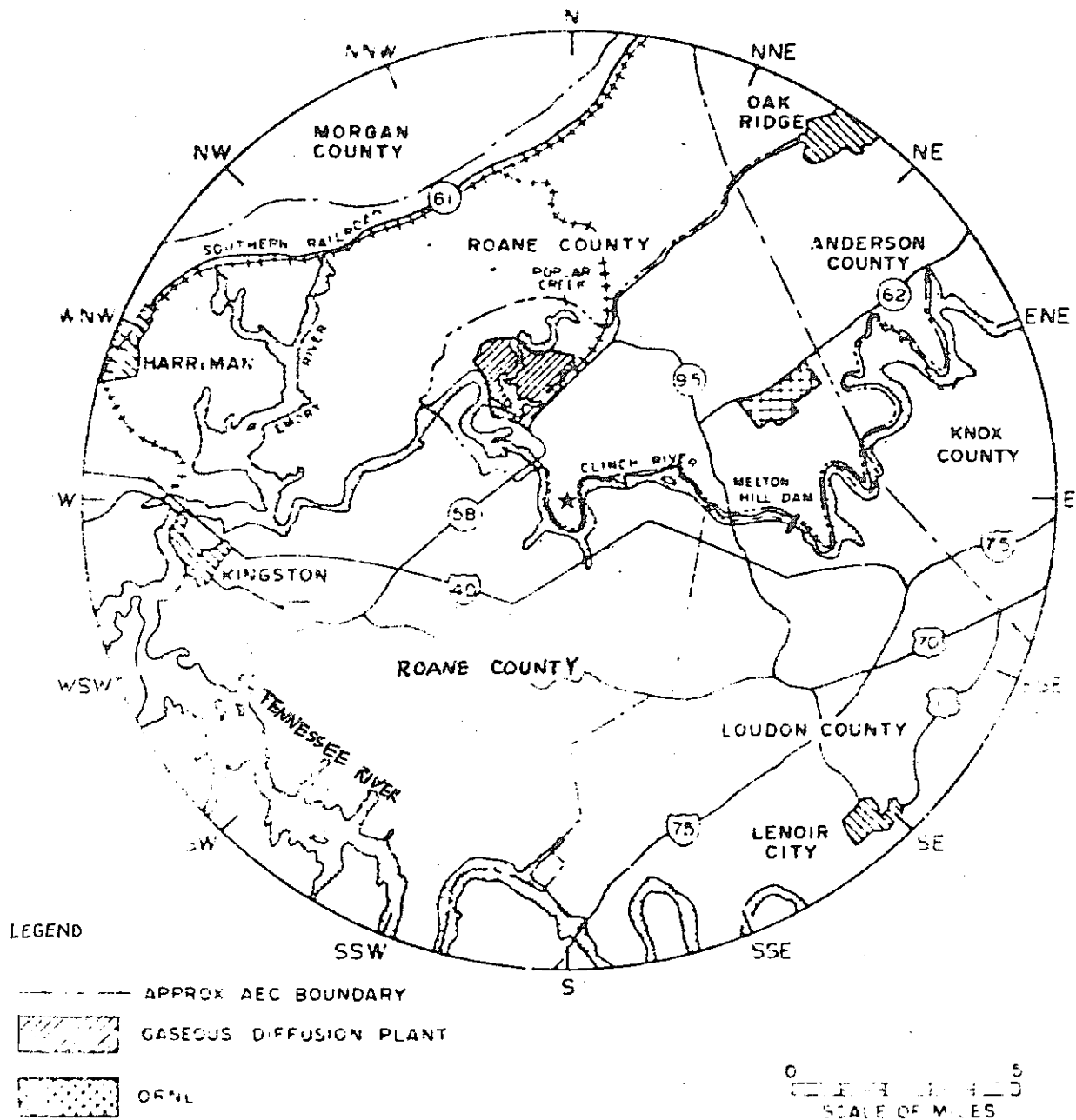
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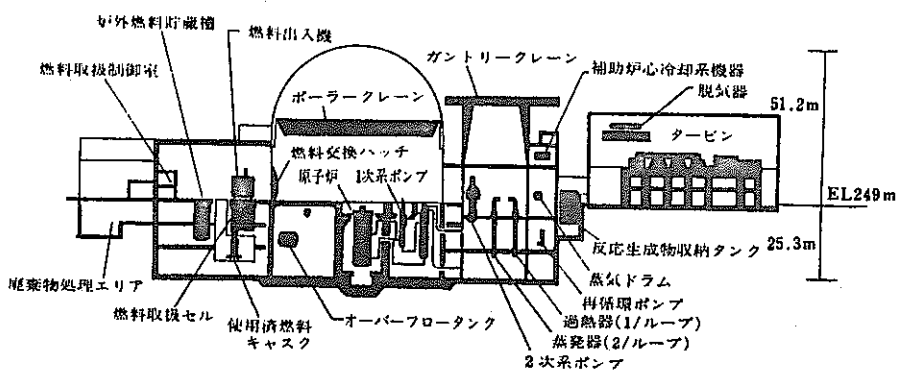
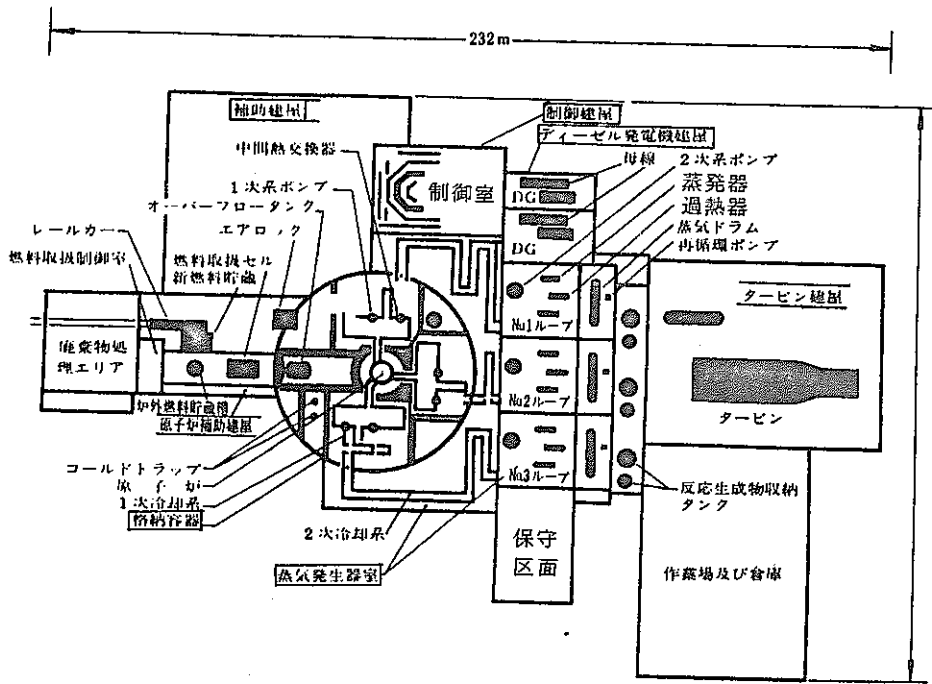
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# 図 関 係

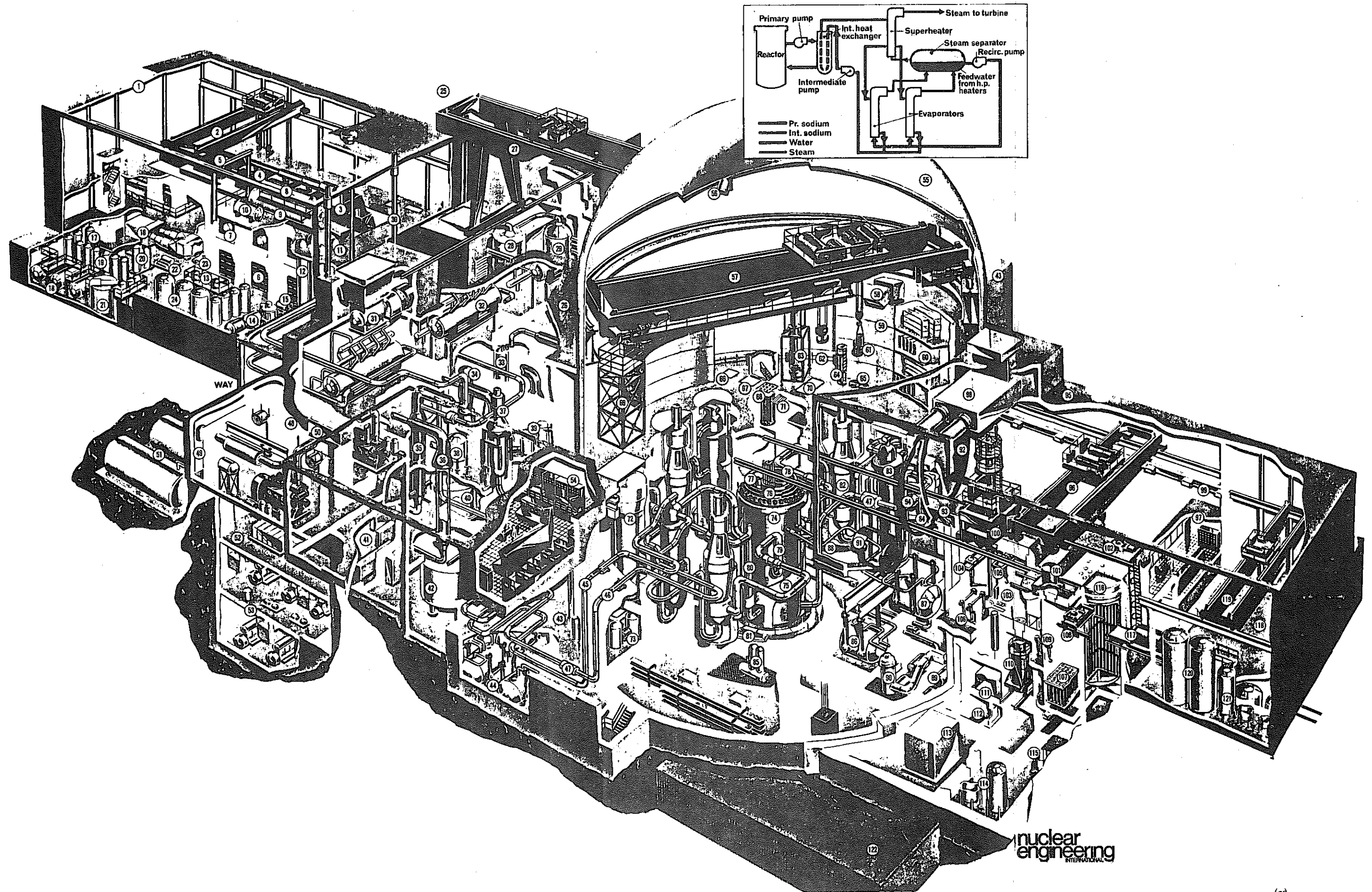


第 2.1 - 1 ☒ LOCATION OF SITE WITH RESPECT TO URBAN CENTERS, RAILROADS AND HIGHWAYS WITHIN A 10-MILE RADIUS OF THE SITE (1)



第 2.1 - 2 図 プラント配置図 (CRBRP) <sup>(68)</sup>

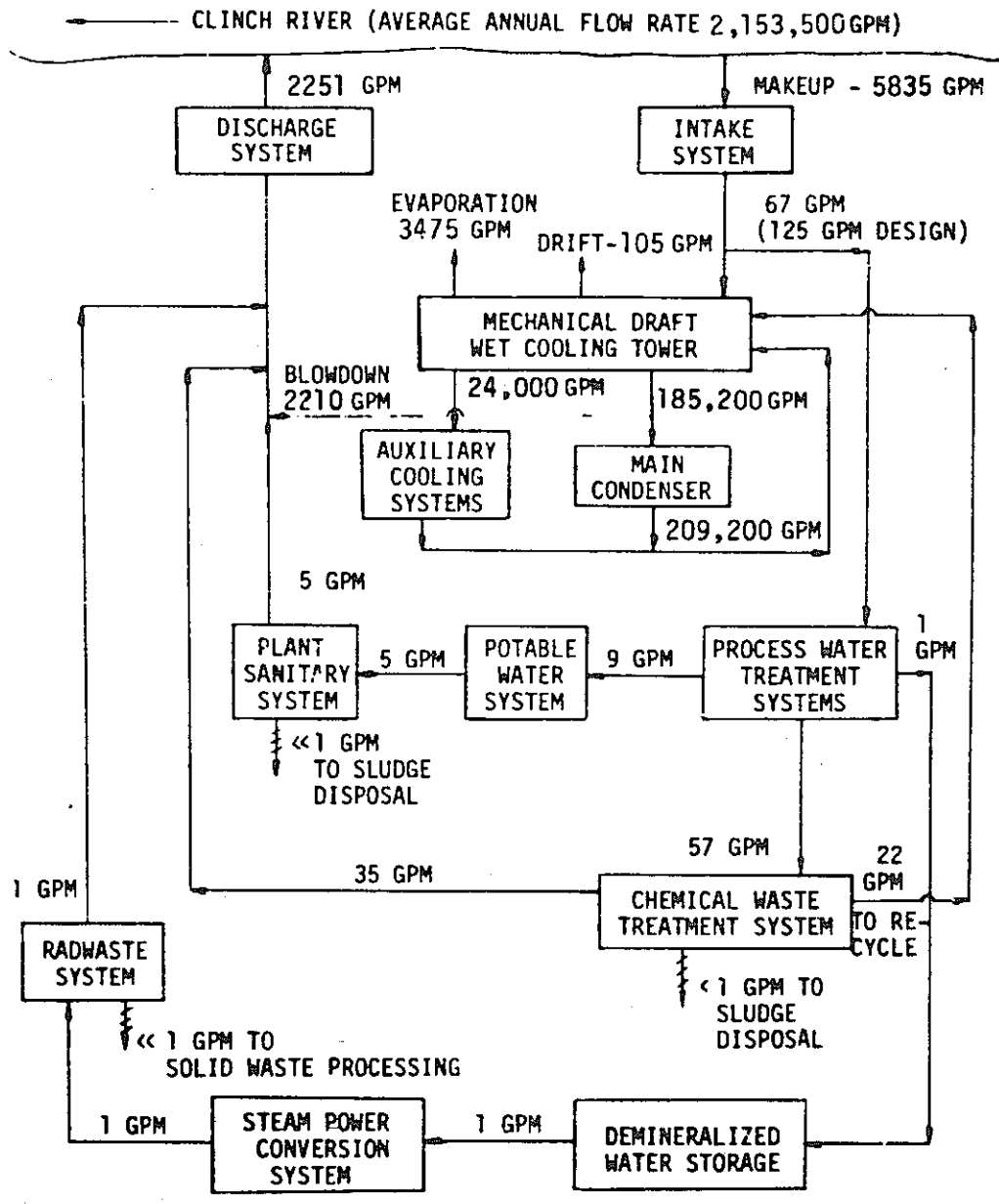




第 2.1-3 図 プラント鳥瞰図 (CRBRP) <sup>(68)</sup>

nuclear  
engineering  
INTERNATIONAL

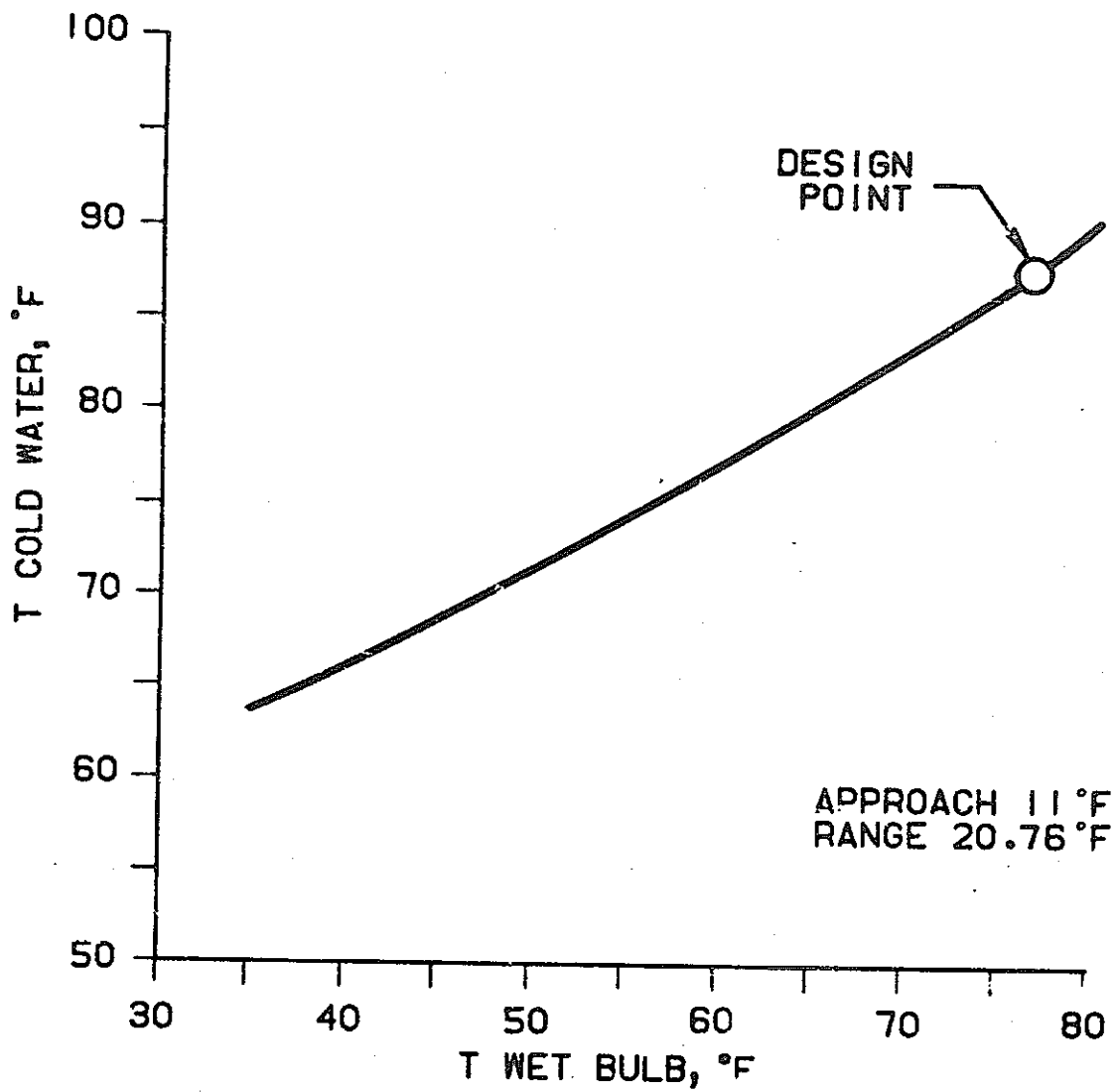
1. Turbine building.
2. Turbine building bridge crane.
3. High-pressure turbine.
4. Low-pressure turbines.
5. Generator.
6. Condenser.
7. Low-pressure heaters.
8. De-aerator heater.
9. Storage tank.
10. Surge tank.
11. High-pressure feedwater heaters.
12. Low-pressure feedwater heaters.
13. Condensate pumps.
14. Steam generator feed pumps.
15. Vacuum pumps.
16. Heating, ventilation and air conditioning equipment.
17. Chemical mix tanks.
18. Ammonia, caustic, and acid storage tanks.
19. Demineralizers.
20. Filters.
21. Clarifiers.
22. Stator winding cooler unit.
23. Condenser drain pumps.
24. Condensate polishing tanks.
25. Warehouse and shop building.
26. Steam generator building.
27. Steam generator building gantry crane.
28. Centrifugal separation tank.
29. Reaction products tank.
30. Igniter.
31. Steam generator auxiliary heat removal system air-cooled condenser.
32. Steam drum.
33. Water dump tank.
34. Recirculating pump.
35. Superheater.
36. Evaporators.
37. Intermediate pump.
38. Expansion tank.
39. Cold traps.
40. Steam generator auxiliary heat removal system water tank.
41. Auxiliary bay.
42. Sodium dump tank.
43. Intermediate bay.
44. Primary sodium storage tanks (shown on opposite side of plant for clarity).
45. Cold return to heat exchanger.
46. Steam feed from heat exchanger.
47. Flow meter.
48. Diesel generator building.
49. Diesel exhaust structure.
50. Air intake plenum.
51. Diesel fuel storage tanks.
52. Switchgear.
53. Chilled liquid rooms (water and dowsing spray)
54. Control room.
55. Containment vessel.
56. Re circulating fans.
57. Reactor building polar crane.
58. Primary pump unit cooler.
59. Electrical equipment rooms.
60. Instrumentation and control cabinets.
61. Plug handling machine.
62. Cable trays.
63. Auxiliary handling machine.
64. In-vessel transfer machine drive mechanism storage.
65. In-vessel transfer machine port adaptors.
66. Equipment hatch.
67. In-vessel transfer machine storage.
68. Plug and sleeve storage.
69. Large maintenance stand.
70. Primary heat transfer system cell access hatch.
71. Electrical, instrumentation and control embedded conduits.
72. Large component cleaning and inspection vessel.
73. Large component cleaning and inspection vessel process equipment.
74. Reactor vessel.
75. Reactor guard vessel.
76. Rotating head plugs.
77. Ex-vessel transport machine plug.
78. In-vessel transfer machine plug.
79. Sodium from reactor to primary pump (hot leg).
80. Sodium from intermediate heat exchanger to reactor (cold leg).
81. Reactor cavity cooling duct.
82. Primary pump.
83. Intermediate heat exchanger.
84. Primary sodium cold traps.
85. Primary heat transfer system fan cooler unit.
86. Primary sodium storage vessel.
87. Reactor sodium overflow vessel.
88. Sodium drain pipe.
89. Primary sodium make-up pumps.
90. Primary sodium overflow and storage cell cooler unit.
91. Primary personnel access air lock.
92. Reactor containment building refuelling hatch.
93. Refuelling hatch floor tilting mechanism.
94. Primary check valve.
95. Reactor service building.
96. Reactor service building bridge crane.
97. Fuel handling control room.
98. Reactor containment air conditioning unit.
99. Reactor service building air ducts.
100. Ex-vessel transport machine.
101. Transfer dolly.
102. Floor valve.
103. Fuel handling cell.
104. Cell handling machine.
105. Cell bridge crane.
106. Fuel handling cell operating gallery.
107. New core component storage.
108. New core component cell bridge crane.
109. New core component cell operating gallery.
110. Spent fuel cask and transport dolly.
111. Fuel handling cell argon purification unit.
112. Mass spectrometer.
113. Radioactive argon processing system cold box.
114. Liquid nitrogen storage vessels.
115. Cell atmospheric processing system liquid collection tank.
116. Ex-vessel storage tank.
117. Spent fuel shipping cask on railroad car.
118. Decontamination area.
119. Decontamination area bridge crane.
120. Condensate storage tanks (liquid radwaste).
121. Monitoring tanks (liquid radwaste).
122. Plant service building.



NOTE: COOLING TOWER FLOWRATES ARE ANNUAL AVERAGES AT MAX. POWER OPERATION

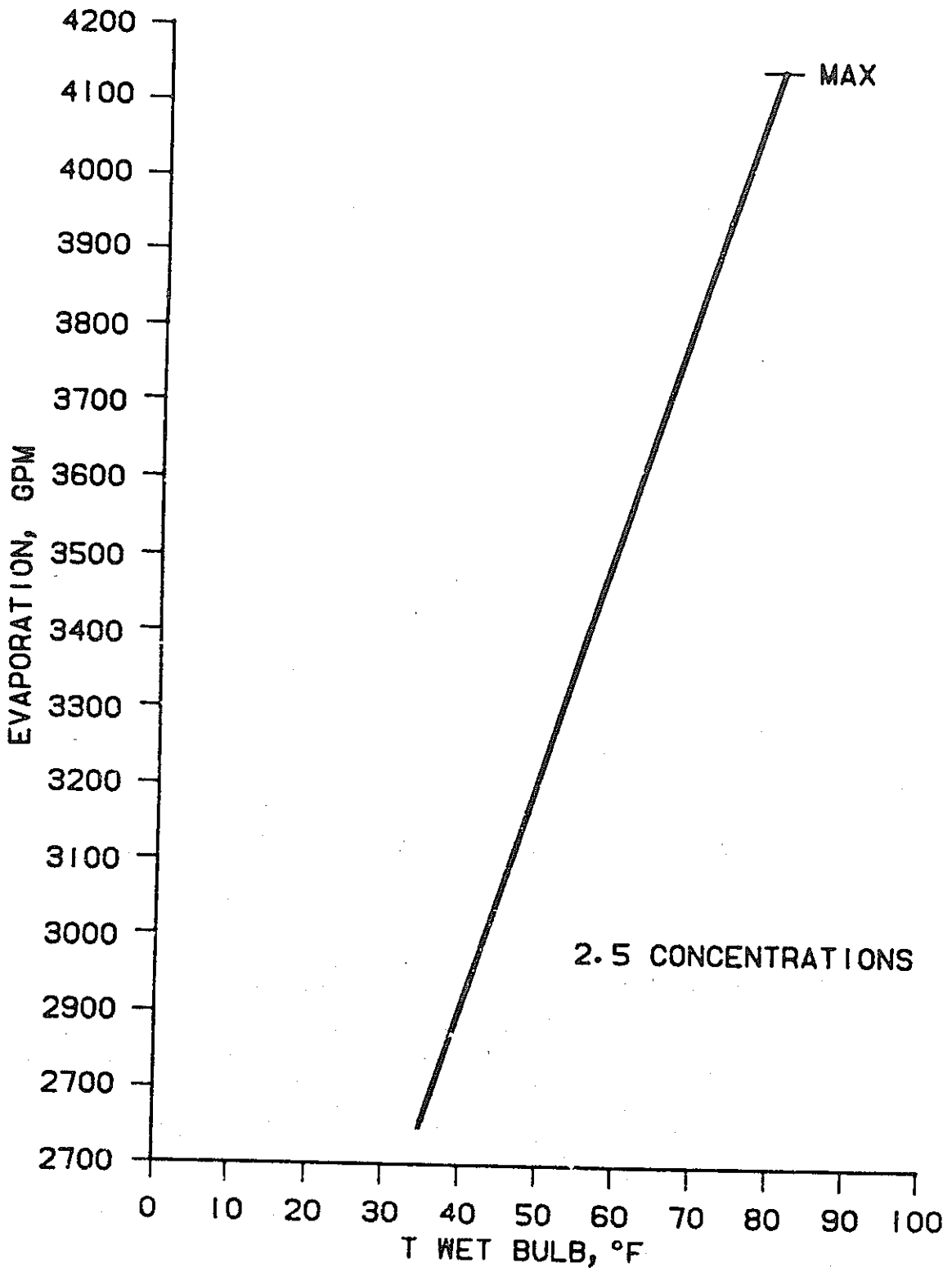
第 2.2 - 1 ☒ WATER USAGE DIAGRAM FOR THE CRBRP

Ref. (1) AMENDMENT VI Figure 3.3-1



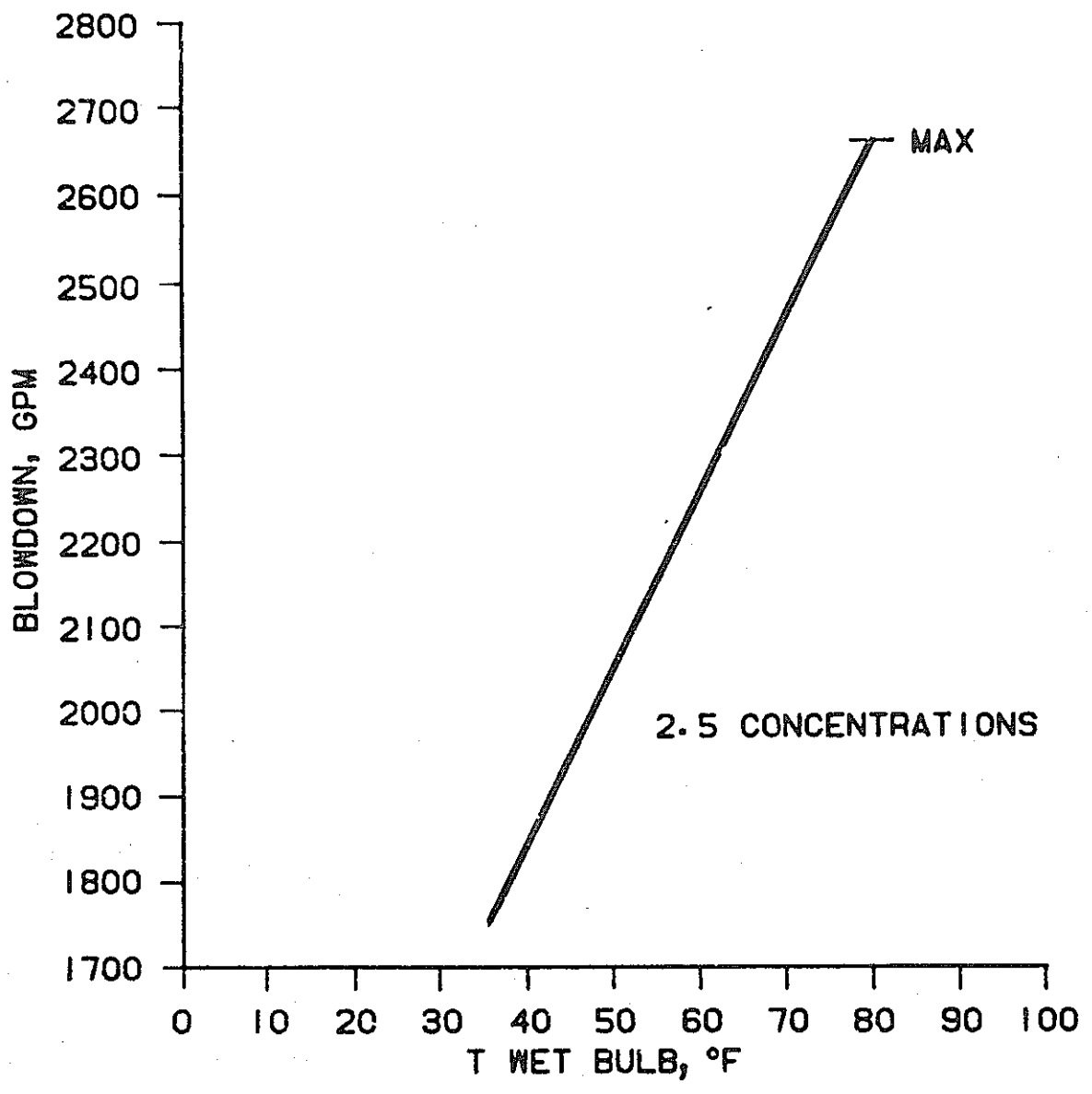
第 2.2 - 2 图 COOLING SYSTEM PERFORMANCE - MECHANICAL DRAFT WET TOWER

Ref.(1) AMENDMENT VI Figure 3.4-2



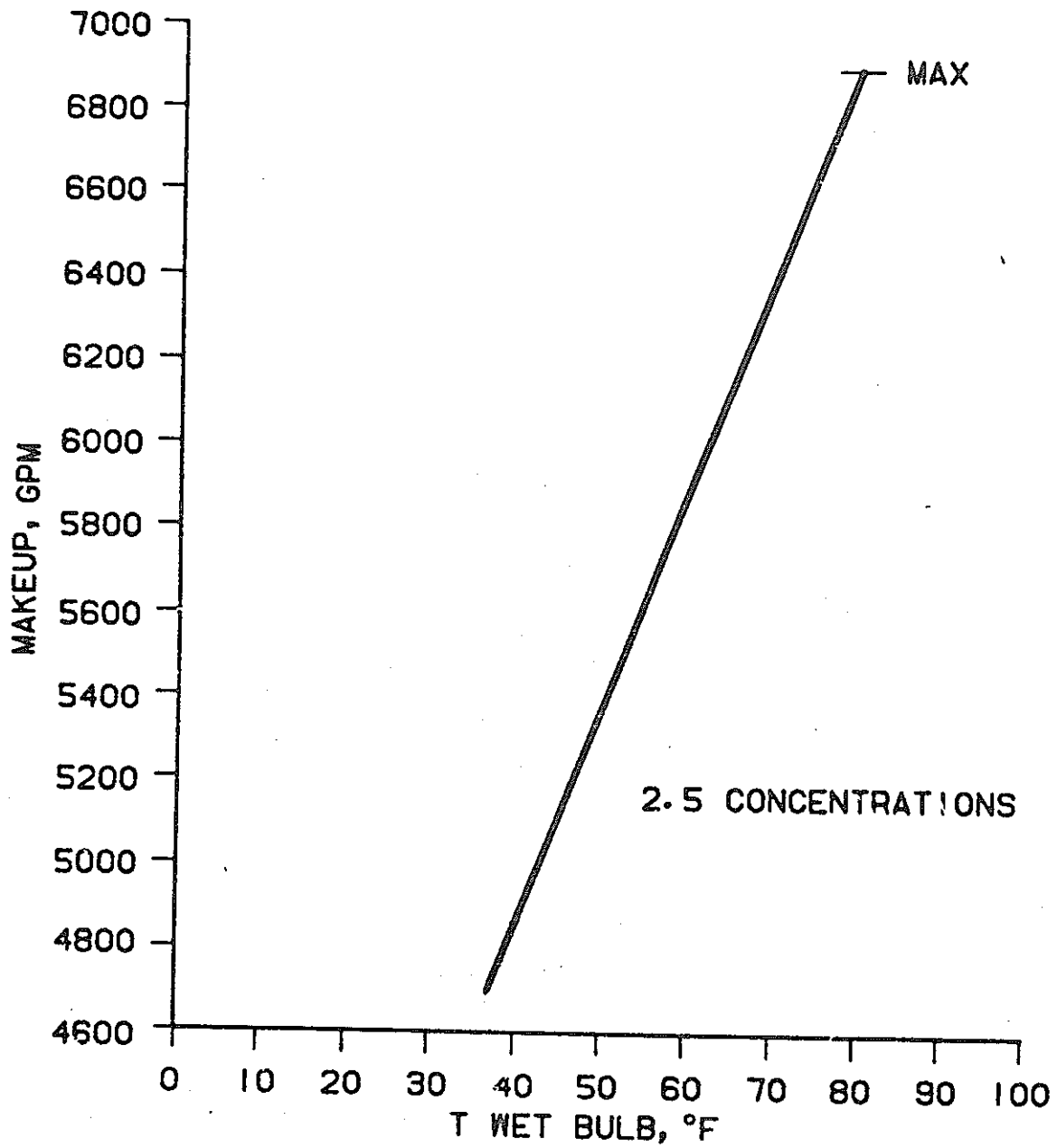
第 2.2 - 3 图 MECHANICAL DRAFT WET TOWER EVAPORATION

Ref. (1) AMENDMENT VI Figure 3.4-3



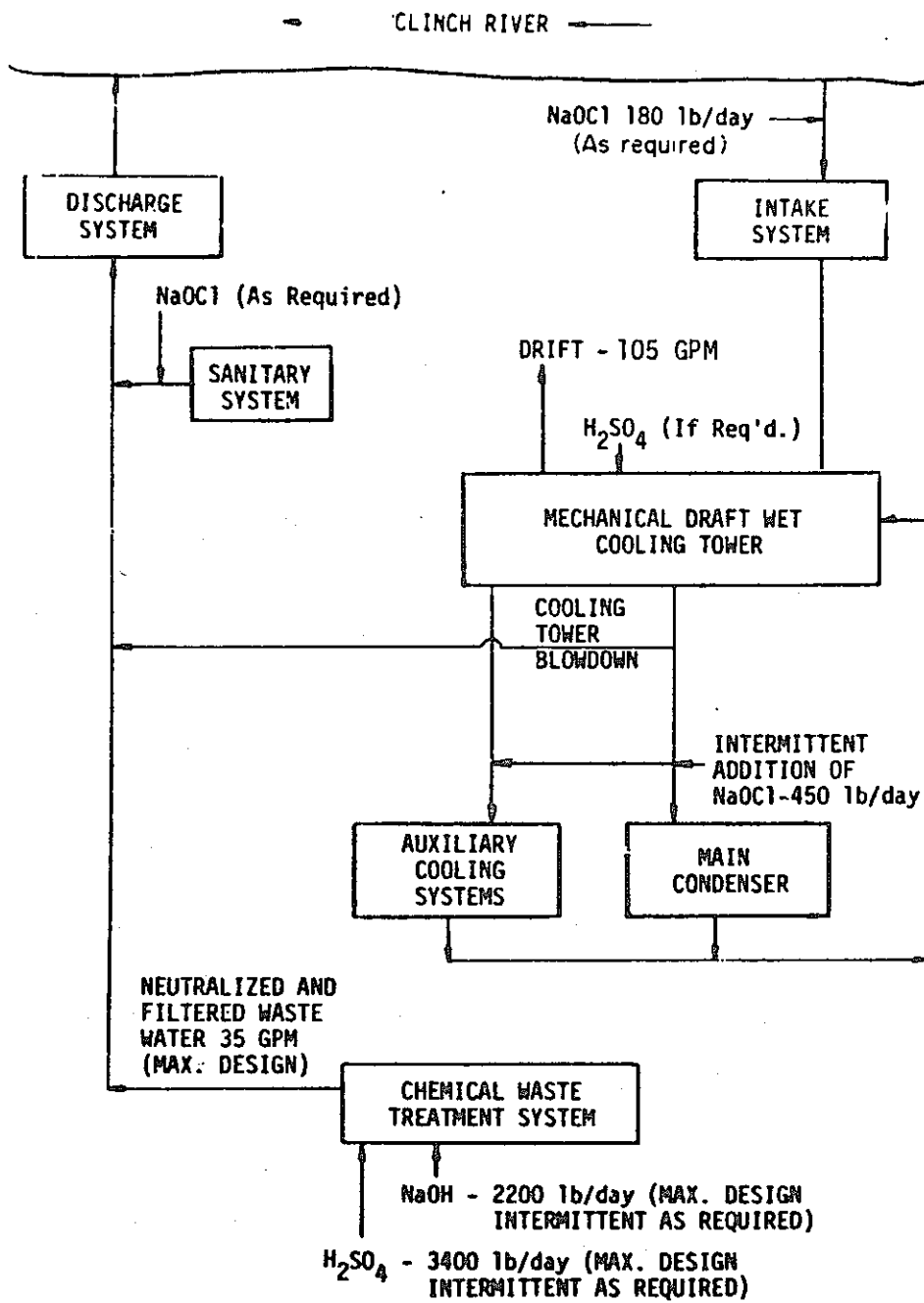
第 2.2 - 4 ☒ MECHANICAL DRAFT WET TOWER BLOWDOWN

Ref.(1) AMENDMENT VI Figure 3.4-4



第 2.2 - 5 图 MECHANICAL DRAFT WET TOWER MAKEUP

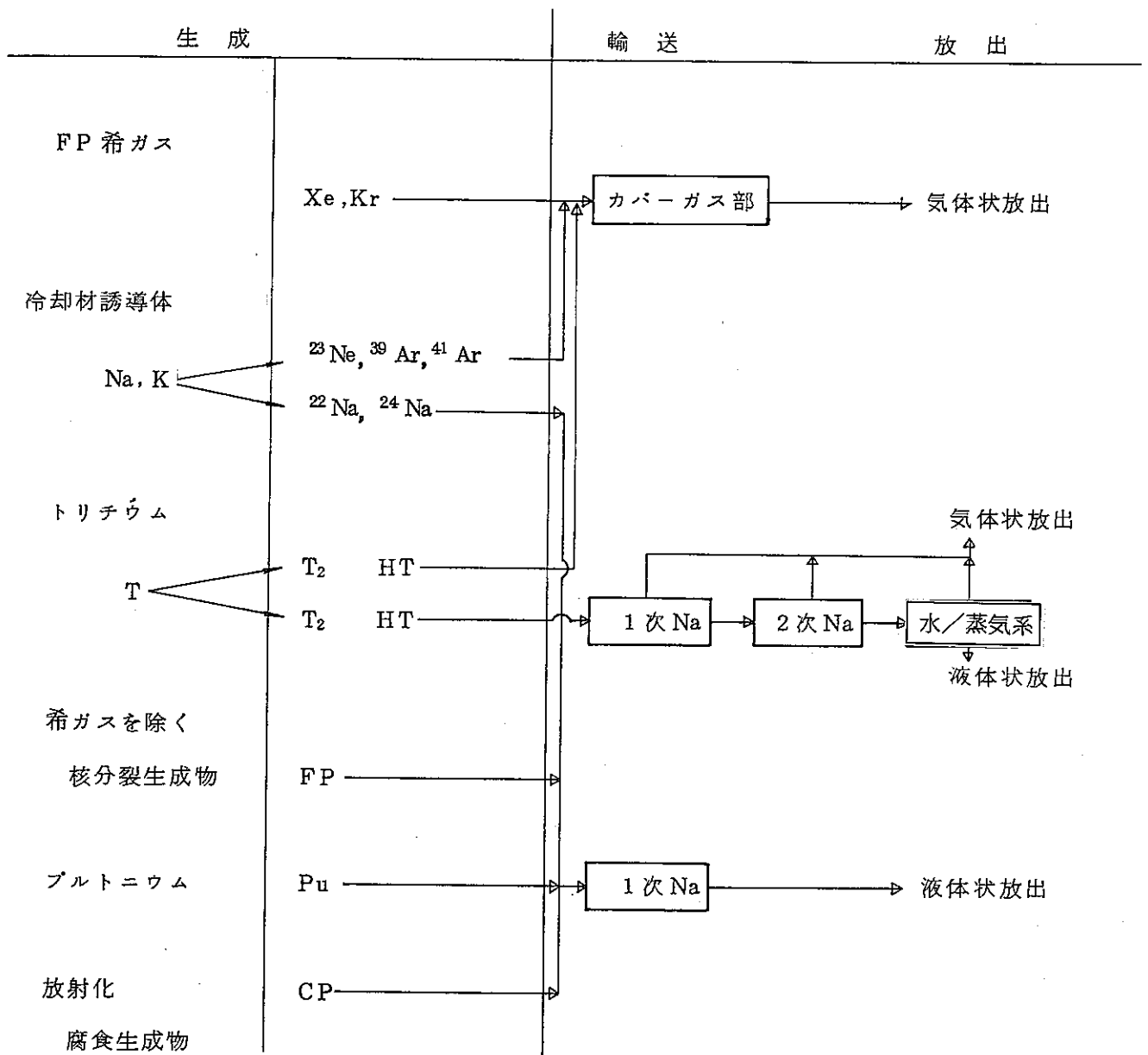
Ref. (1) AMENDMENT VI Figure 3.4-5



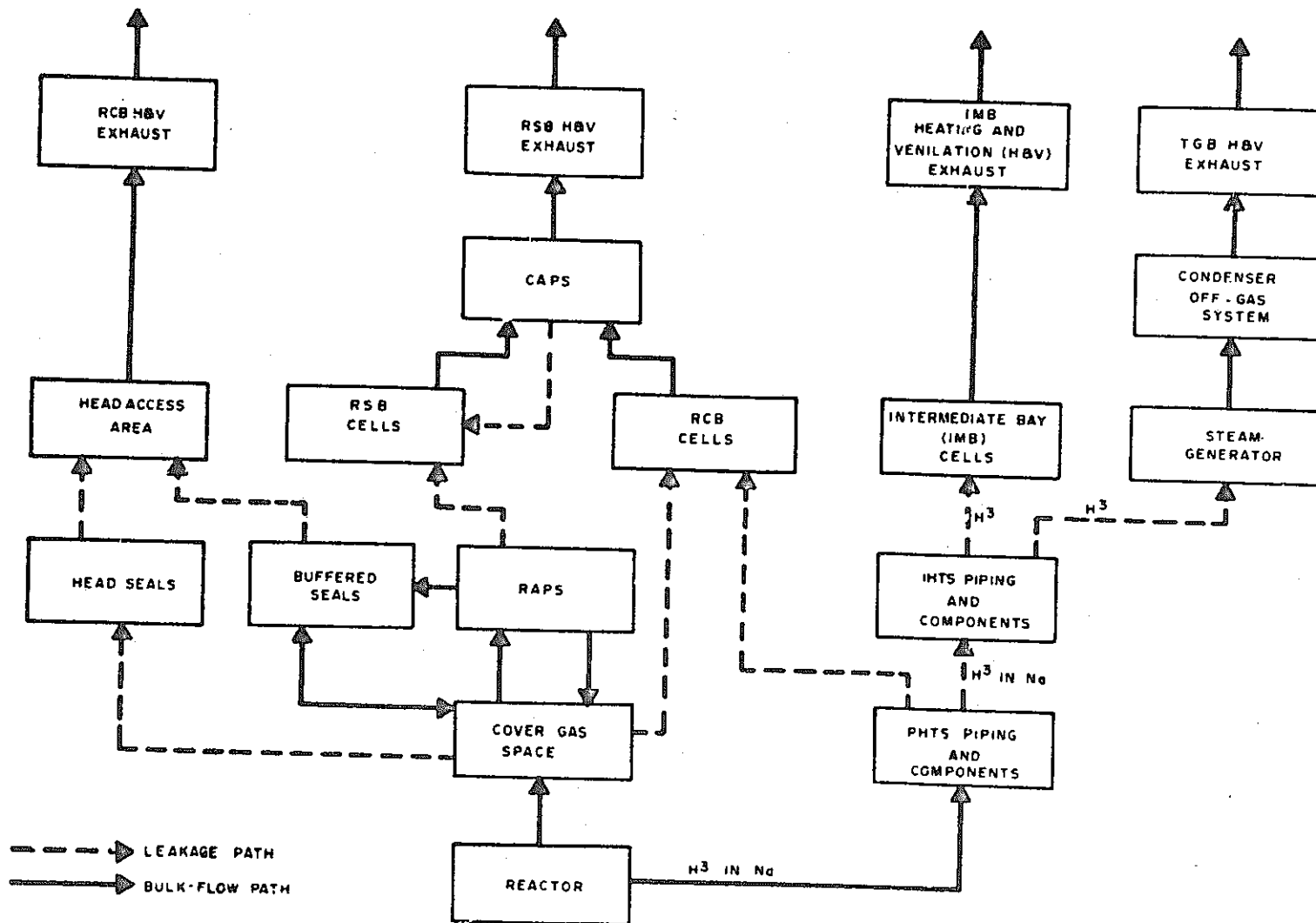
第 2.2 - 6 图 CHEMICAL AND BIOCIDES ADDITIONS AND DISCHARGES AT MAXIMUM POWER OPERATION

Ref. (1) Figure 3.6-1



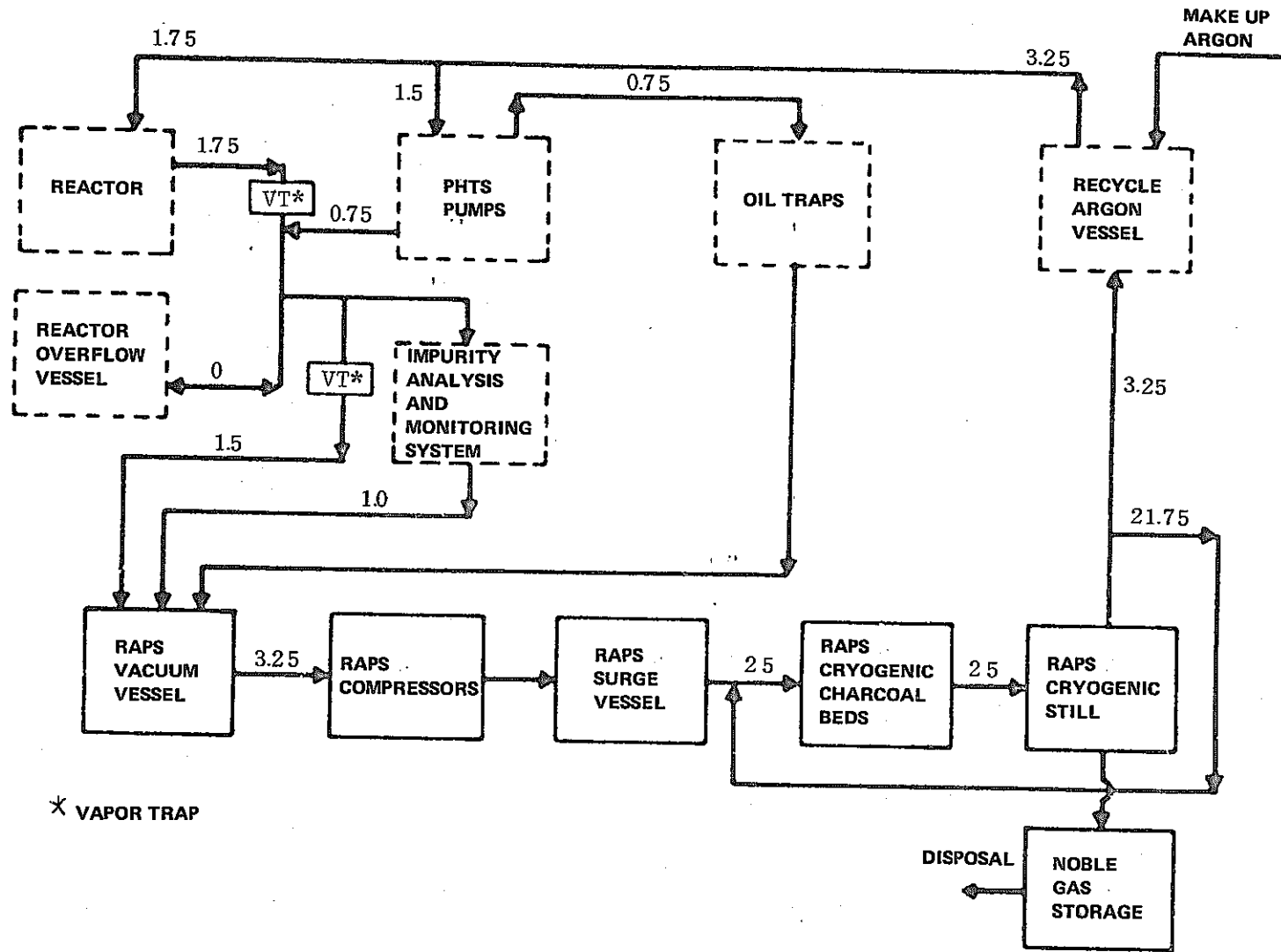


第 2.2 - 7 図 放射性物質の生成，輸送，放出過程



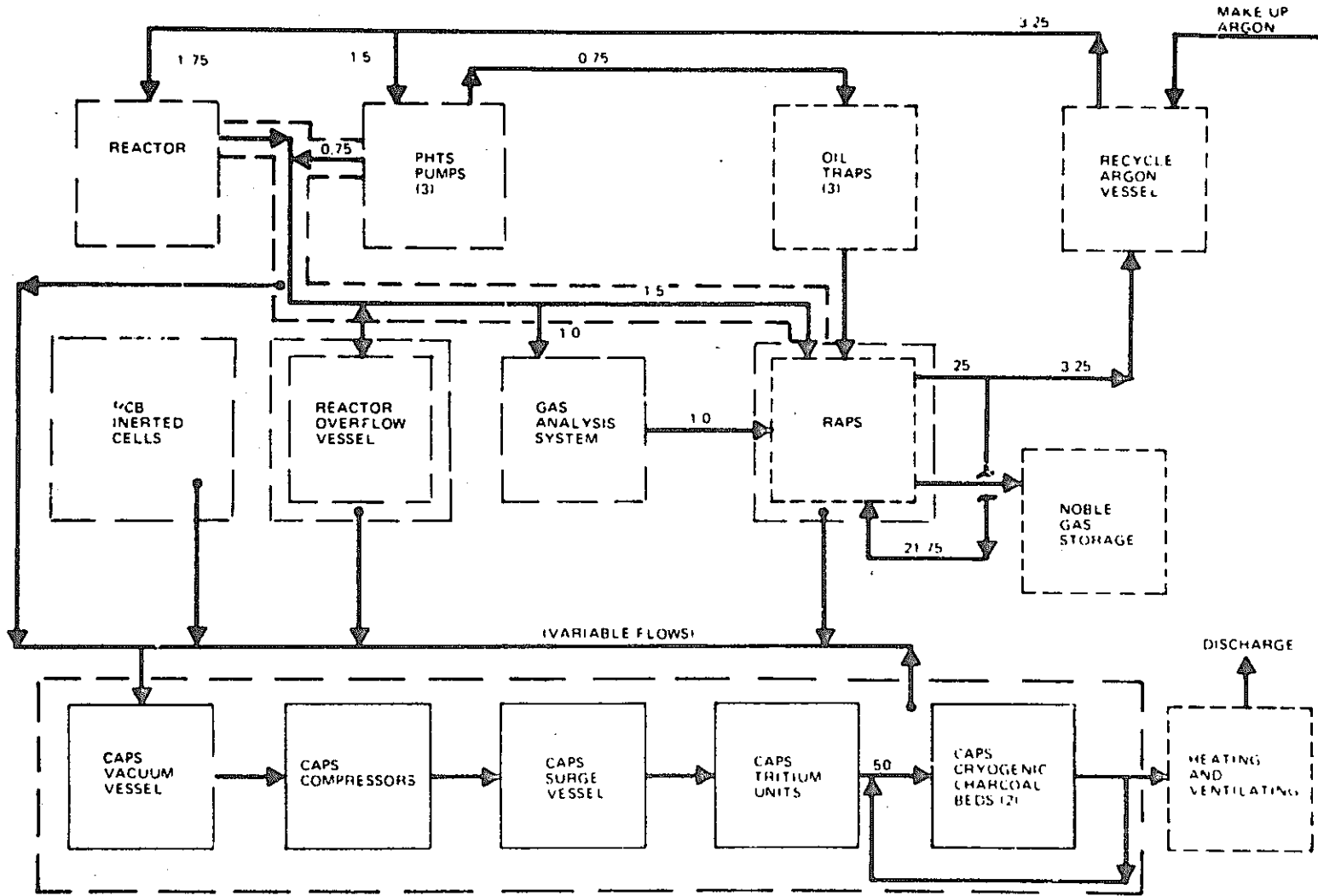
第 2.2 - 8 图 RADIOACTIVE GAS FLOW PATHS

Ref. (1) AMENDMENT VI Figure 3.5-4



第 2.2 - 9 ☒ SCHEMATIC DIAGRAM OF THE RAPS SYSTEM

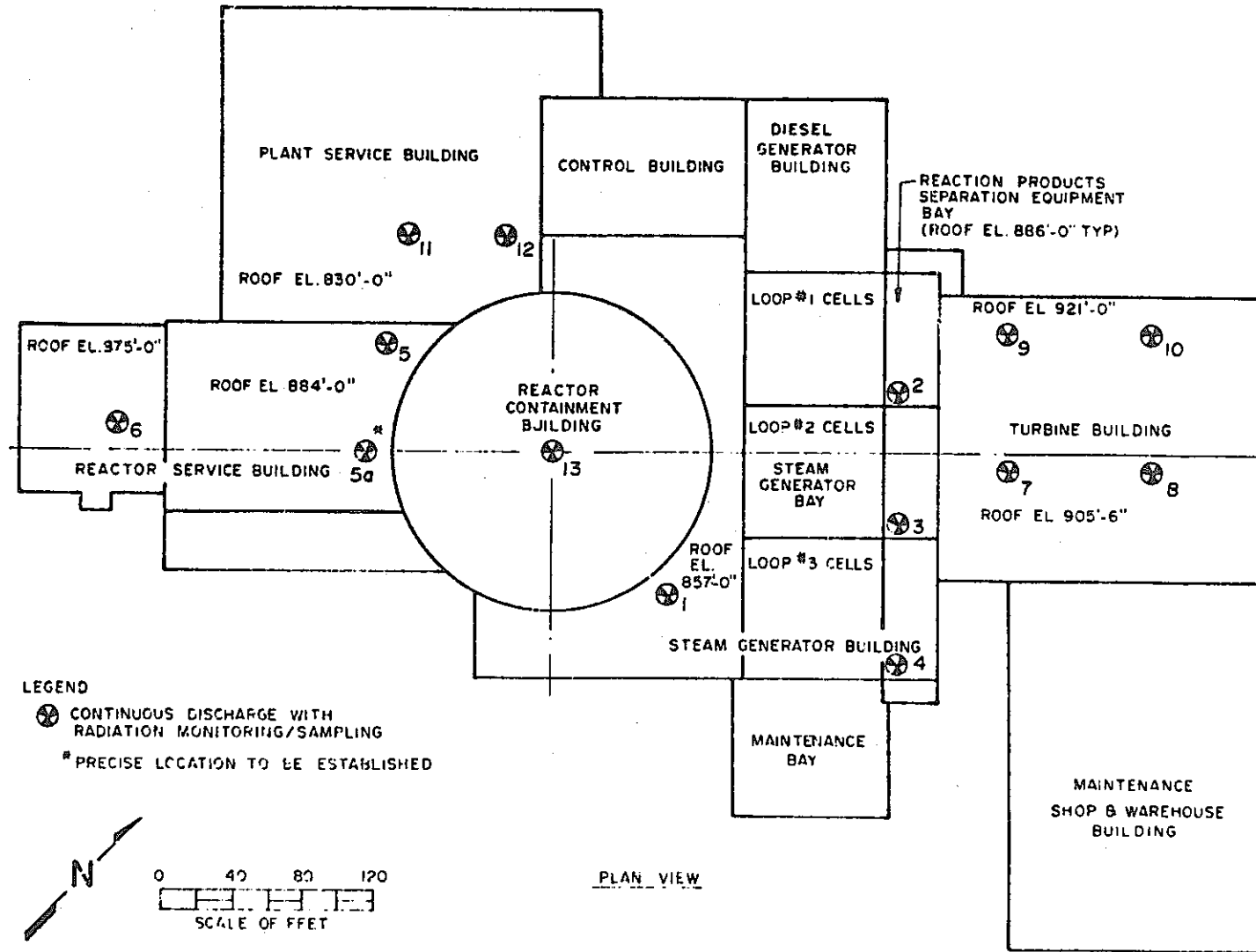
Ref. (1) AMENDMENT VI Figure 3.5-2



VALUES SHOWN ARE FLOW RATES (lcc/min)

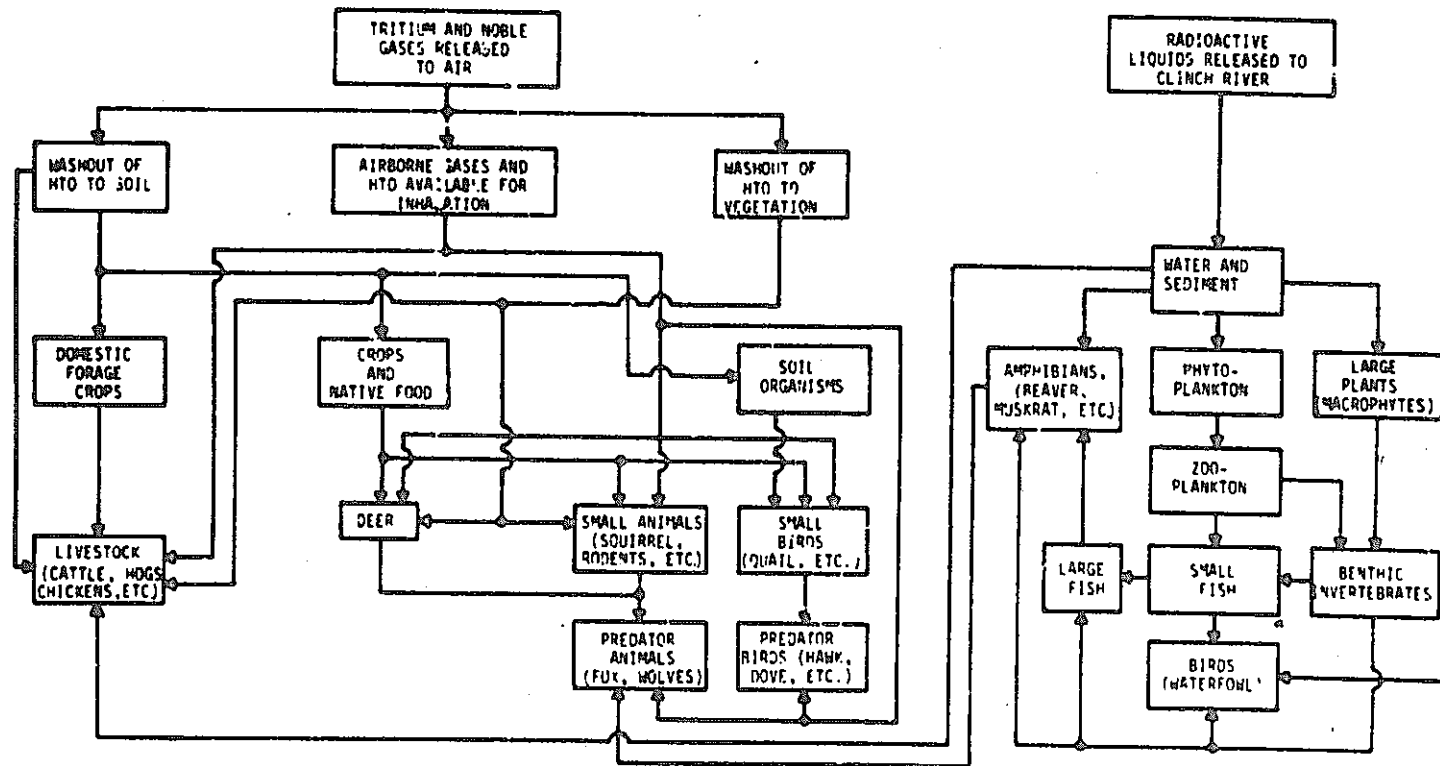
第 2.2 - 1 0 图 SCHEMATIC DIAGRAM OF THE CAPS SYSTEM

Ref.(1) AMENDMENT VIII Figure 3.5-3



第 2.2 - 1 1 ☒ CRBRP RELEASE POINTS

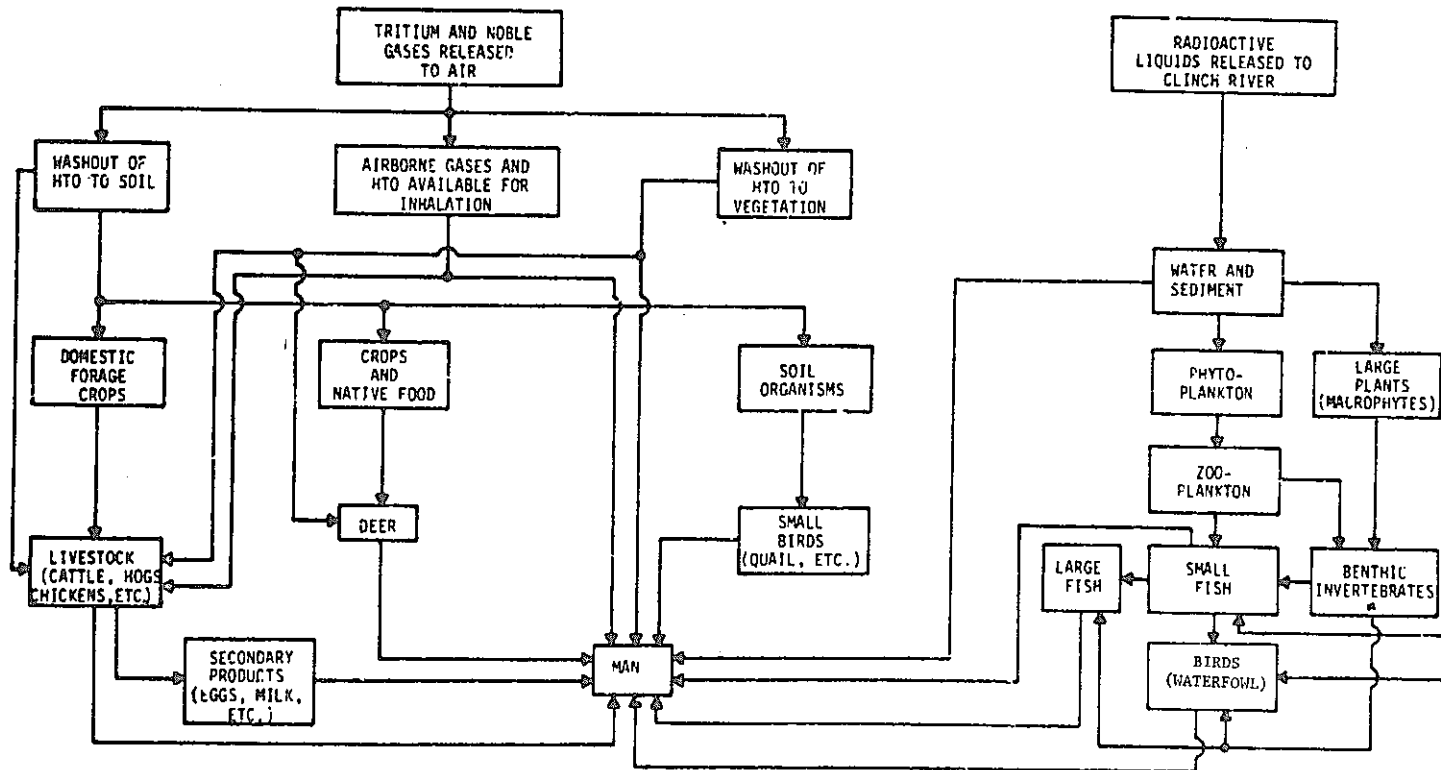
Ref. (1) AMENDMENT VII Figure 1 (Item 010.7)



第 2.3 - 1 ☒

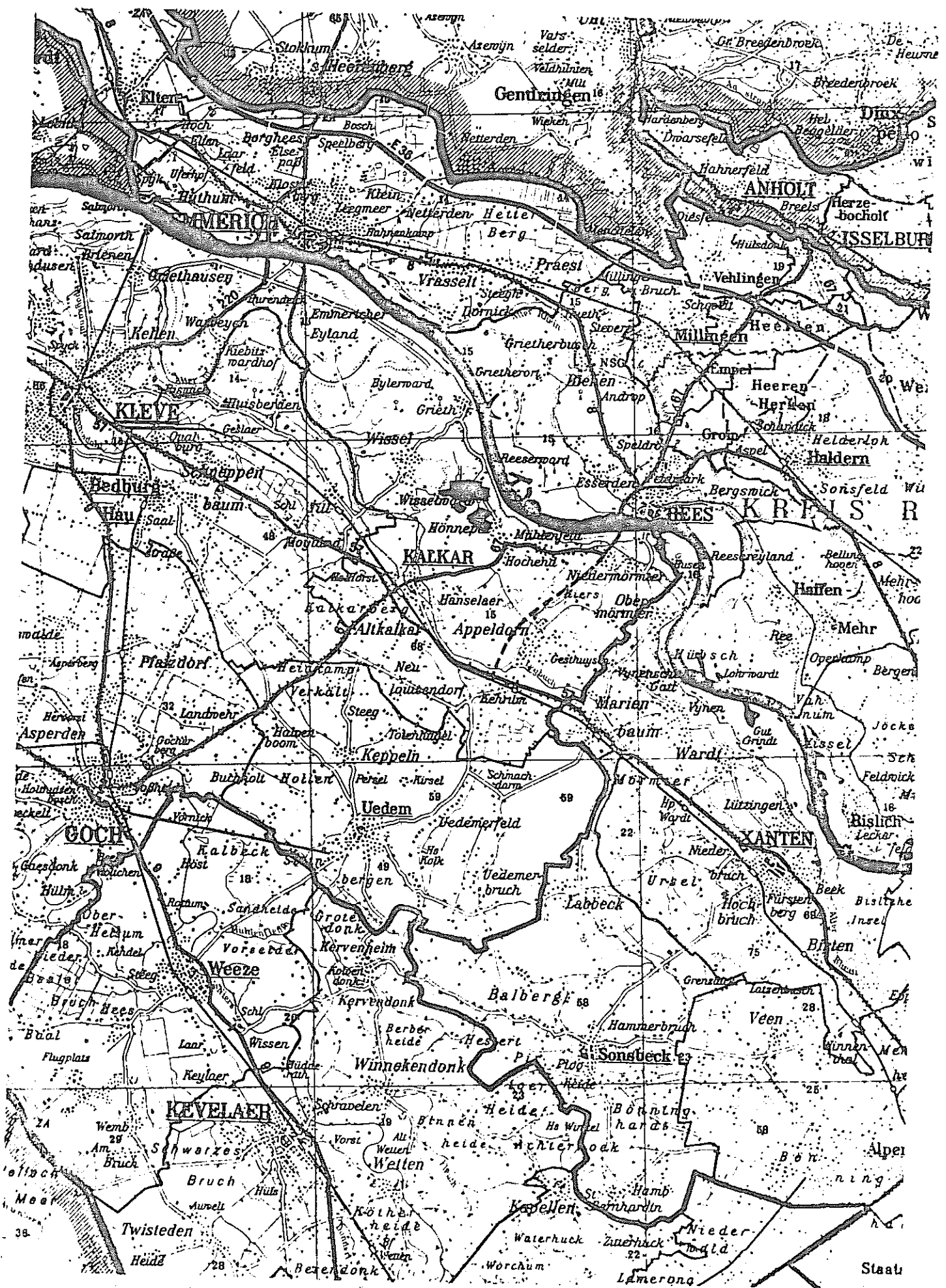
POTENTIAL RADIATION EXPOSURE PATHWAYS TO BIOTA OTHER THAN MAN FROM THE CRBRP RADWASTE SYSTEMS

Ref. (1) FIGURE 5.2-1



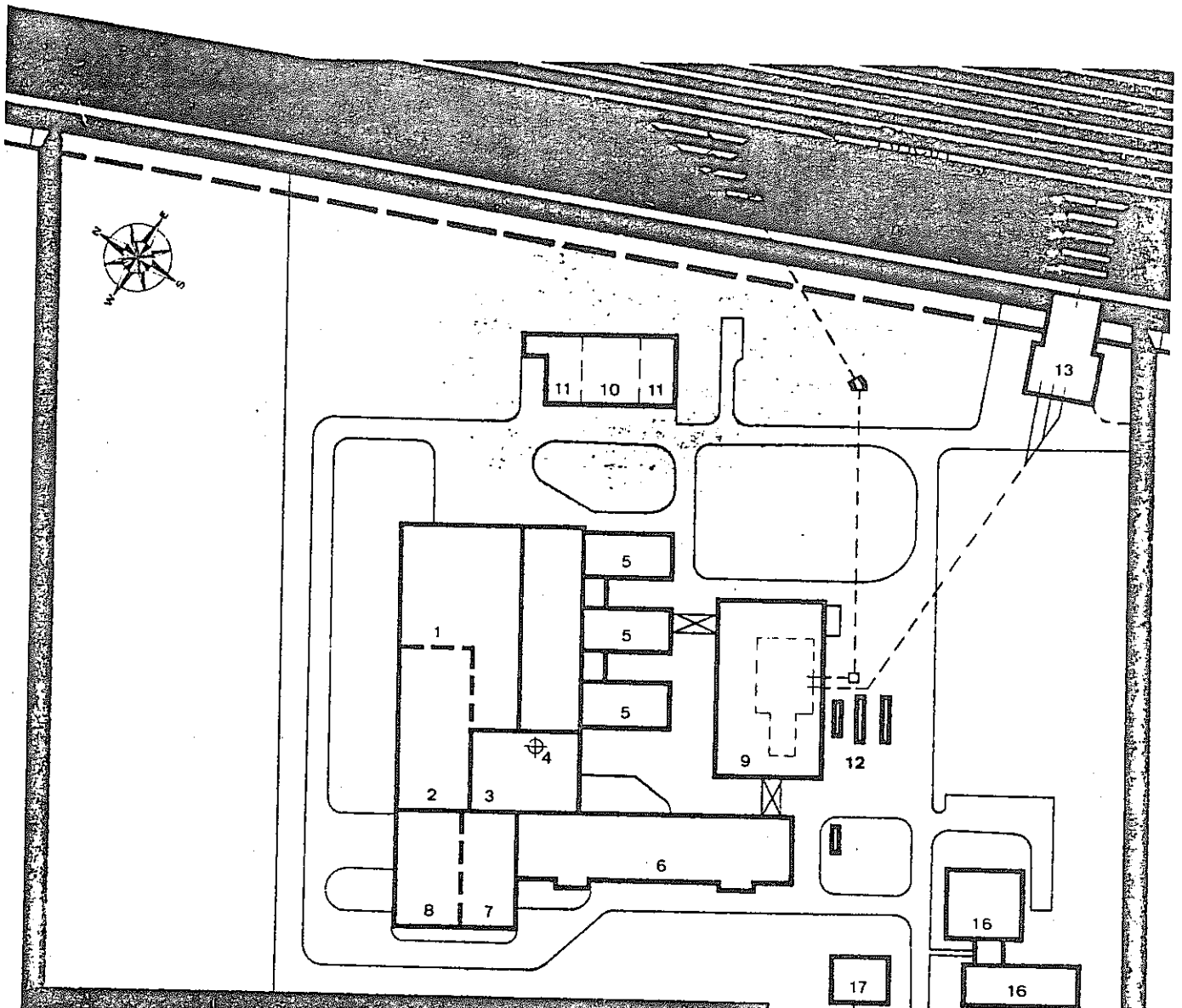
第 2.3 - 2 ☒ POTENTIAL RADIATION EXPOSURE PATHWAYS TO MAN FROM THE CRBRP RADWASTE SYSTEMS

Ref. (1) FIGURE 5.3-1



第 3.1-1 図 SNR-300 のサイト

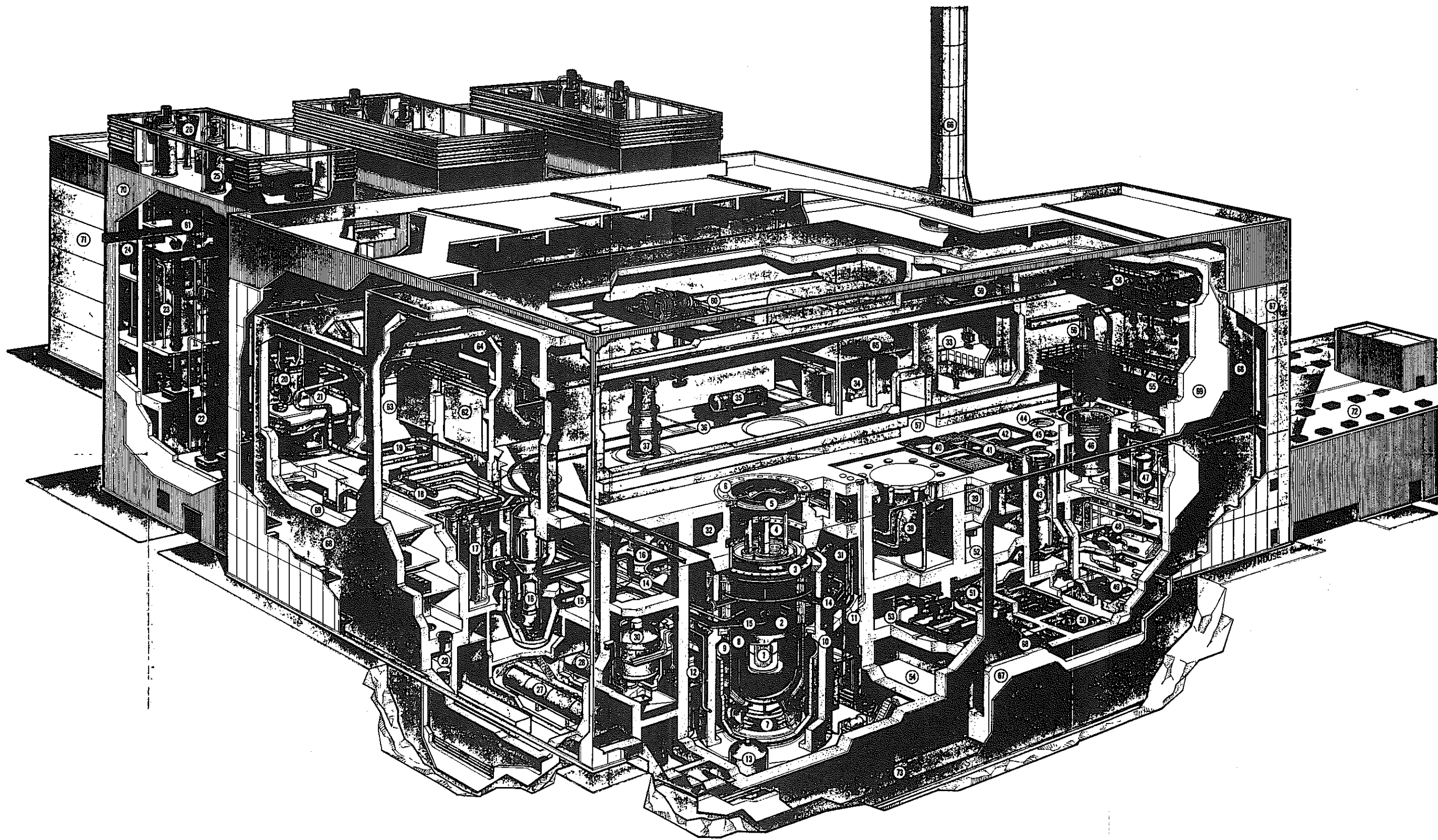




Site Plan

- |                                |   |
|--------------------------------|---|
| 1 Reactor building             | 9 Turbine generator building                    |
| 2 Handling area                | 10 Water treatment system                       |
| 3 Auxiliary equipment area     | 11 Standby diesel set                           |
| 4 Stack                        | 12 Transformers                                 |
| 5 Steam generator buildings    | 13 Cooling water pump building                  |
| 6 Service and control building | 14 Seal pit                                     |
| 7 Workshop                     | 15 Outlet structure                             |
| 8 Storeroom                    | 16 Administration building and social buildings |
|                                | 17 Information centre                           |

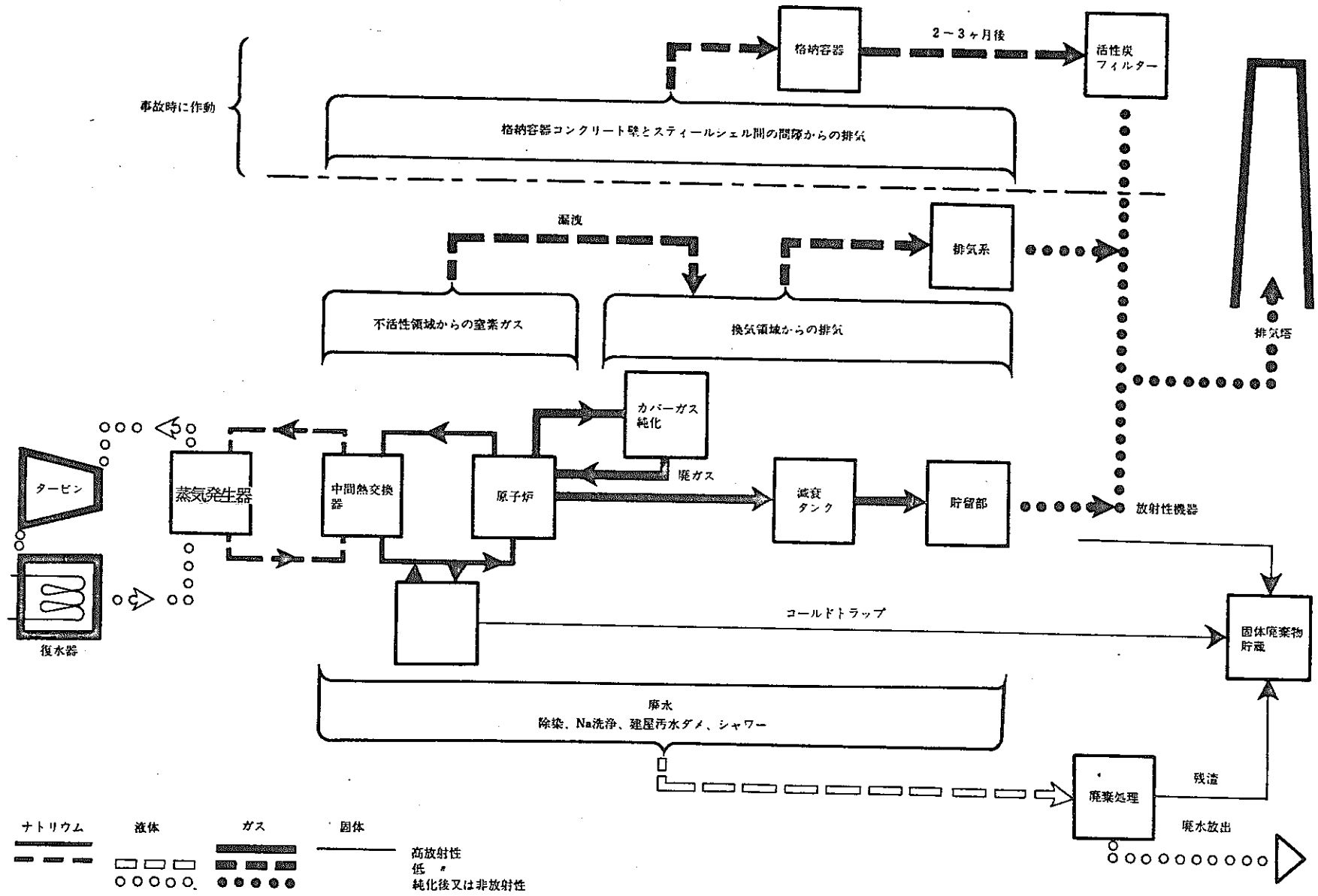
第 3.1 - 2 図 SNR-300 プラント配置図 <sup>(68)</sup>



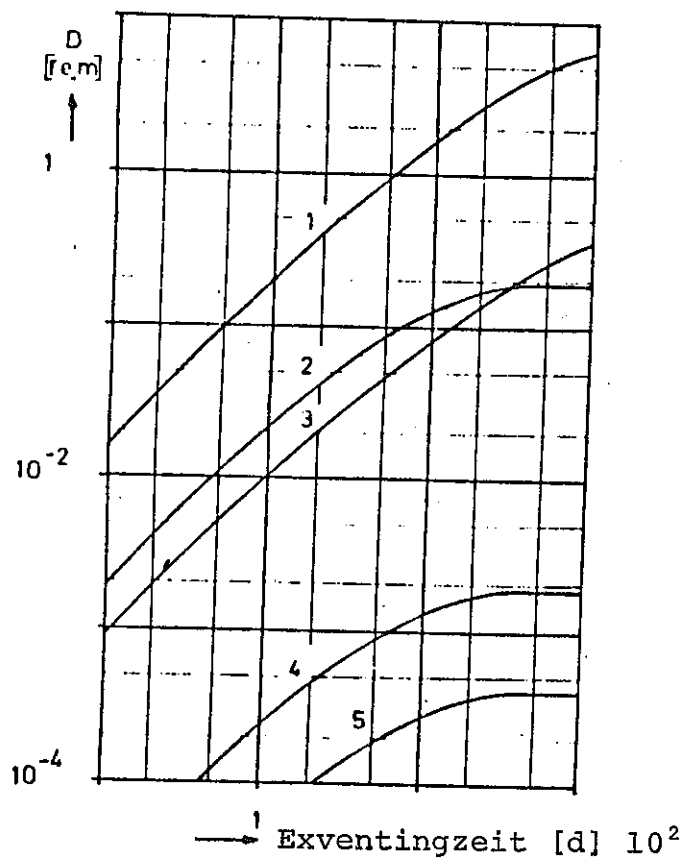
第 3.1-3 図 SNR-300 プラント鳥瞰図 <sup>(68)</sup>

### Key to drawing

- 1 Core (*Kern*)
- 2 Reactor vessel (*Reaktortank*)
- 3 Reactor top rotating shield (*Reaktordrehdeckel*)
- 4 Reactor pit (*Reaktorgrube*)
- 5 Rotating lid (*Drehdeckel der Zellenabdeckung*)
- 6 Cover (*Zellenabdeckung*)
- 7 Floor cooling and core retention system (*Bodenkühleinrichtung*)
- 8 Guard vessel (*Doppeltank*)
- 9 Primary shield (*Primärabschirmung*)
- 10 Biological shield (*Biologisches Schild*)
- 11 Neutron flux instrumentation (*Neutronenflußinstrumentierung*)
- 12 Sodium leak pan (*Natriumauffangwanne*)
- 13 Leak collector tank (*Leckauffangbehälter*)
- 14 Sodium inlet pipe (*Natriumeintrittsleitung*)
- 15 Sodium outlet pipe (*Natriumaustrittsleitung*)
- 16 Primary sodium pump (*Natriumprimärpumpe*)
- 17 Intermediate heat exchanger (*Zwischenwärmetauscher*)
- 18 Secondary circuit manifolds (*Sekundärleitungssammler*)
- 19 Main secondary pipes (*Sekundärhauptleitungen*)
- 20 Secondary sodium pumps (*Sekundärnatriumpumpe*)
- 21 Sodium expansion tank (*Stoßtank*)
- 22 Evaporators (*Verdampfer*)
- 23 Superheaters (*Überhitzer*)
- 24 Emergency feed water tank (*Notspeisewasserbehälter*)
- 25 Pressure release cyclone (*Druckentlastungszyklon*)
- 26 Silencers (*Schalldämpfer*)
- 27 Primary sodium dump tank (*Primärnatriumablaßtank*)
- 28 Leak collector tank (*Leckauffangbehälter*)
- 29 Primary sodium cold trap (*Primärnatriumkühlfalle*)
- 30 Sodium level tank (*Spiegelhaltebehälter*)
- 31 Hot gas pipes (*Heißgasleitung*)
- 32 Core instrumentation room (*Kerninstrumentierungsraum*)
- 33 Decontamination and maintenance area (*Wärmewerkstatt*)
- 34 Material airlock (*Materialschleuse*)
- 35 Used fuel shipping container (*Brennelementtransportbehälter*)
- 36 Transport trolley (*Transportwagen*)
- 37 Pump/IHX handling flask (*Komponentenwechsellvorrichtung*)
- 38 Sodium cooled fuel store (*Natriumgekühltes Brennelementlager*)
- 39 New fuel store (*Lager für neue Brennelemente*)
- 40 Irradiated fuel cell (*Zelle für bestrahlte Brennelemente*)
- 41 Maintenance pit and shipping container loading/unloading station (*Wartungsstand und Be- und Entladestation*)
- 42 Radioactive waste store (*Abfallager*)
- 43 Reactor component storage (*Lager für Reaktorkomponenten*)
- 44 Wash cell (*Waschzelle*)
- 45 Cold trap storage pit (*Kühlfallenlagerschacht*)
- 46 Gas cooled fuel store (*Gasgekühltes Brennelementlager*)
- 47 Gas cooled store filter (*Filter des gasgekühlten Lagers*)
- 48 Gas cooling loops (*Gaskühlkreisläufe*)
- 49 Waste water storage room (*Behälterraum für BE-Waschanlage*)
- 50 Cold trap for sodium cooled store (*Kühlfalle des natriumgekühlten Lagers*)
- 51 Main cooling loop of the sodium cooled store (*Betriebskühlkreislauf des natriumgekühlten Lagers*)
- 52 Auxiliary system of the irradiated fuel cell (*Nebenanlage der Zelle für bestrahlte Brennelemente*)
- 53 Emergency cooling loops of the sodium cooled store (*Notkühlkreislauf des natrium gekühlten Lagers*)
- 54 Spare room (*Reserveraum*)
- 55 Transfer machine transporter (*Wechselmaschinenfahrwerk*)
- 56 Handling flasks (*Wechselflaschen*)
- 57 Rail bridge (*Gleisbrücke*)
- 58 Handling hall crane (*Handhabungshallenkran*)
- 59 Shipping container lifting crane (*Kran für Brennelement-Transportbehälter*)
- 60 Component hall crane (*Komponentenhallenkran*)
- 61 Steam generator building crane (*Dampferzeugerhauskran*)
- 62 Heat absorbing blocks (*Wärmespeicherplatten*)
- 63 Pressure relief room (*Druckentlastungsraum*)
- 64 Primary argon system (*Primär-Argon-System*)
- 65 Handling control room (*Handhabungssteuerstelle*)
- 66 Vent stack (*Abgaskamin*)
- 67 Reactor building outer wall (*Reaktorgebäudeaußenwand*)
- 68 Steel liner (*Stahl liner*)
- 69 Reactor building inner wall (*Reaktorgebäudeinnenwand*)
- 70 Steam generator building (*Dampferzeugerhaus*)
- 71 Turbine generator building (*Maschinenhaus*)
- 72 Storage and workshop building (*Lager-Werkstattgebäude*)
- 73 Concrete base plate (*Bodenplatte*)



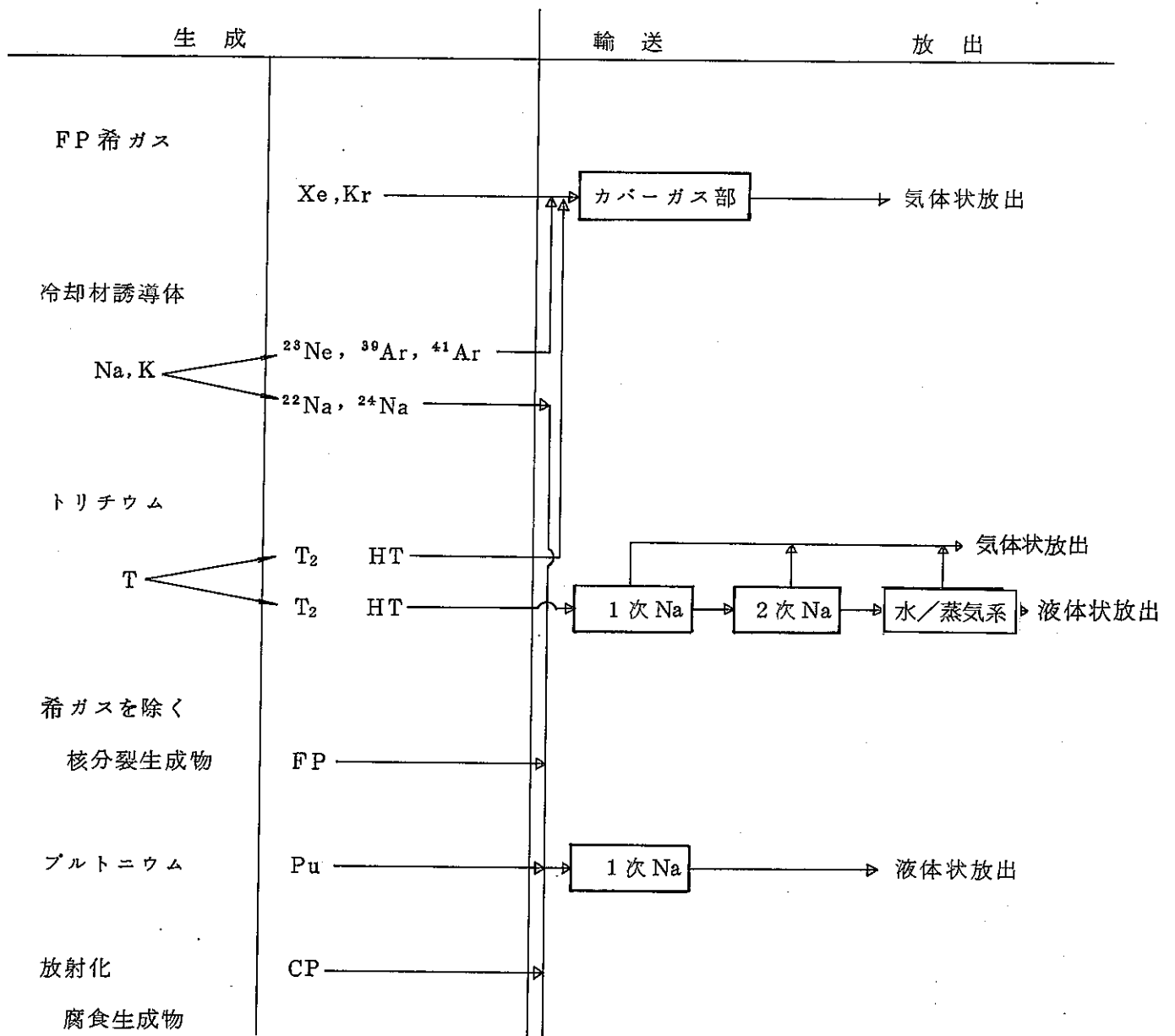
第3.1-4図 SNR-300 廃棄物処理系統図 (69)



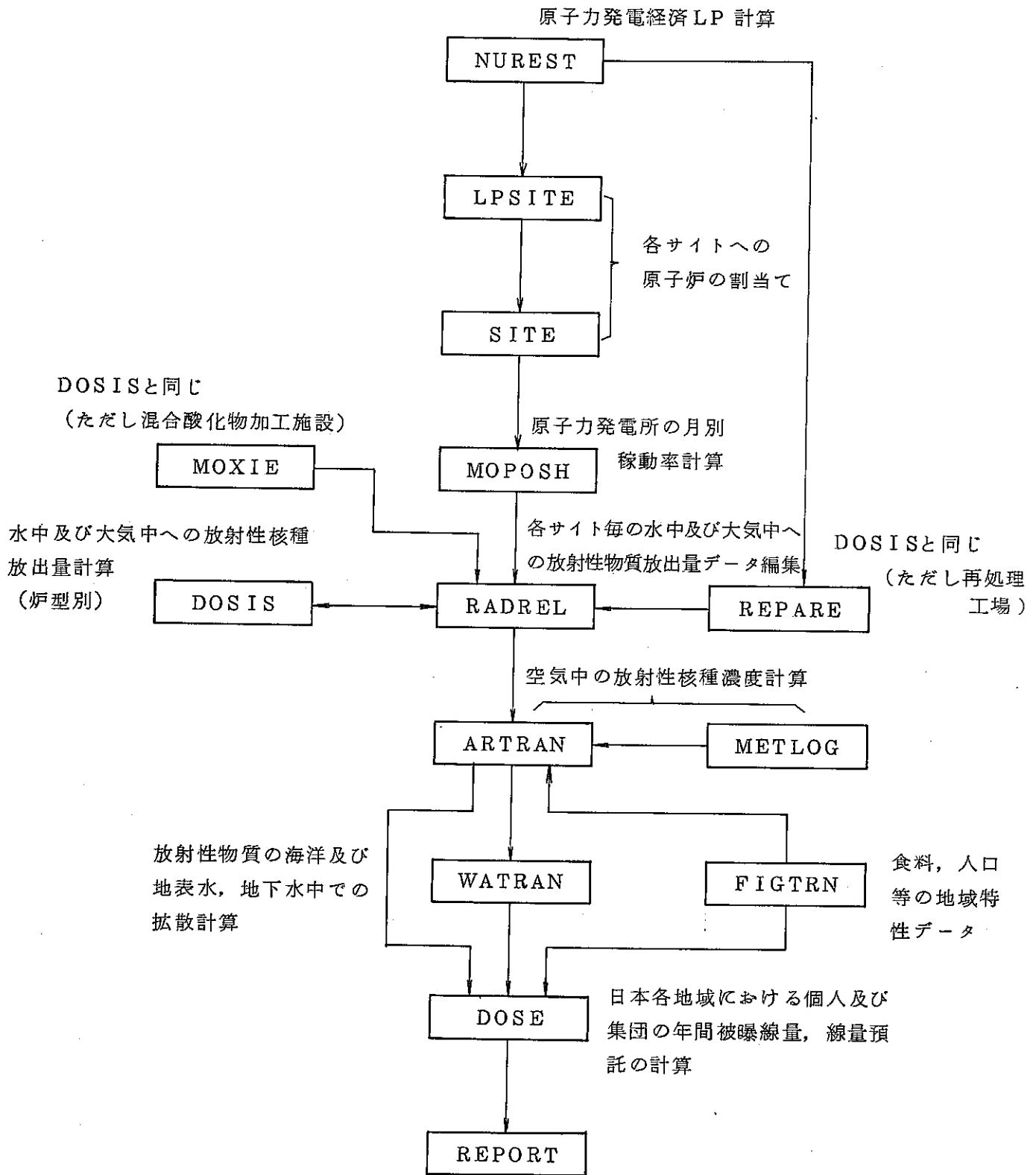
第 3.3 - 1 图 Dose at Point of Maximum Concentration Due to Fuel Element Melt; 3 Days Decay Time; 6 Days Reventing Period (12)

- 1 - Bone dose
- 2 - Thyroid
- 3 - Lung
- 4 - Whole body ( $\beta$ )
- 5 - Whole body ( $\gamma$ )

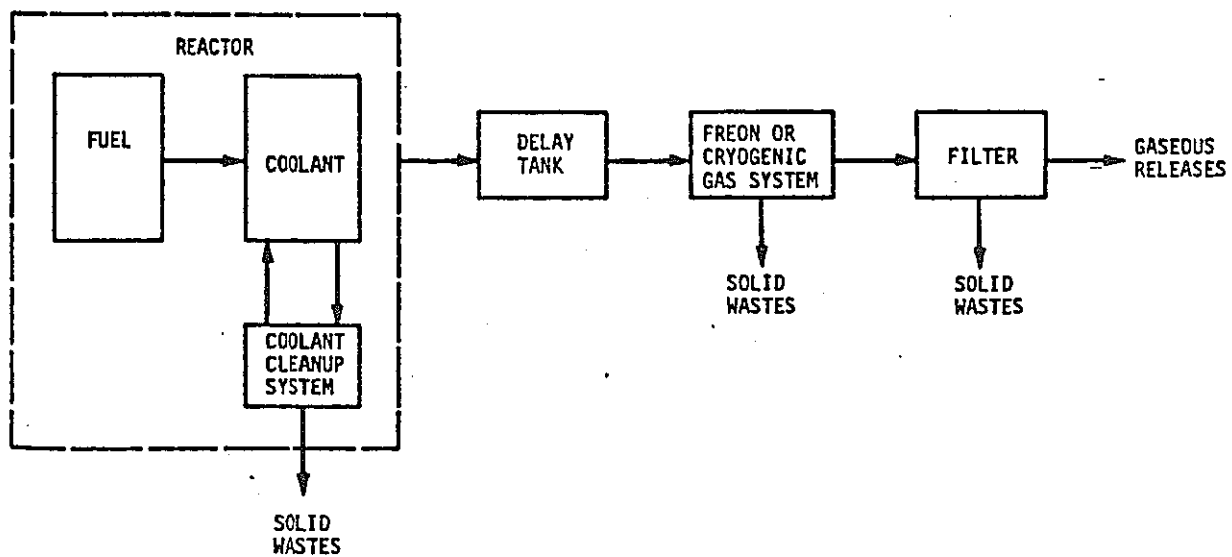
Ref. (11) Fig. 3



第 4.1 - 1 図 放射性物質の生成, 輸送, 放出過程

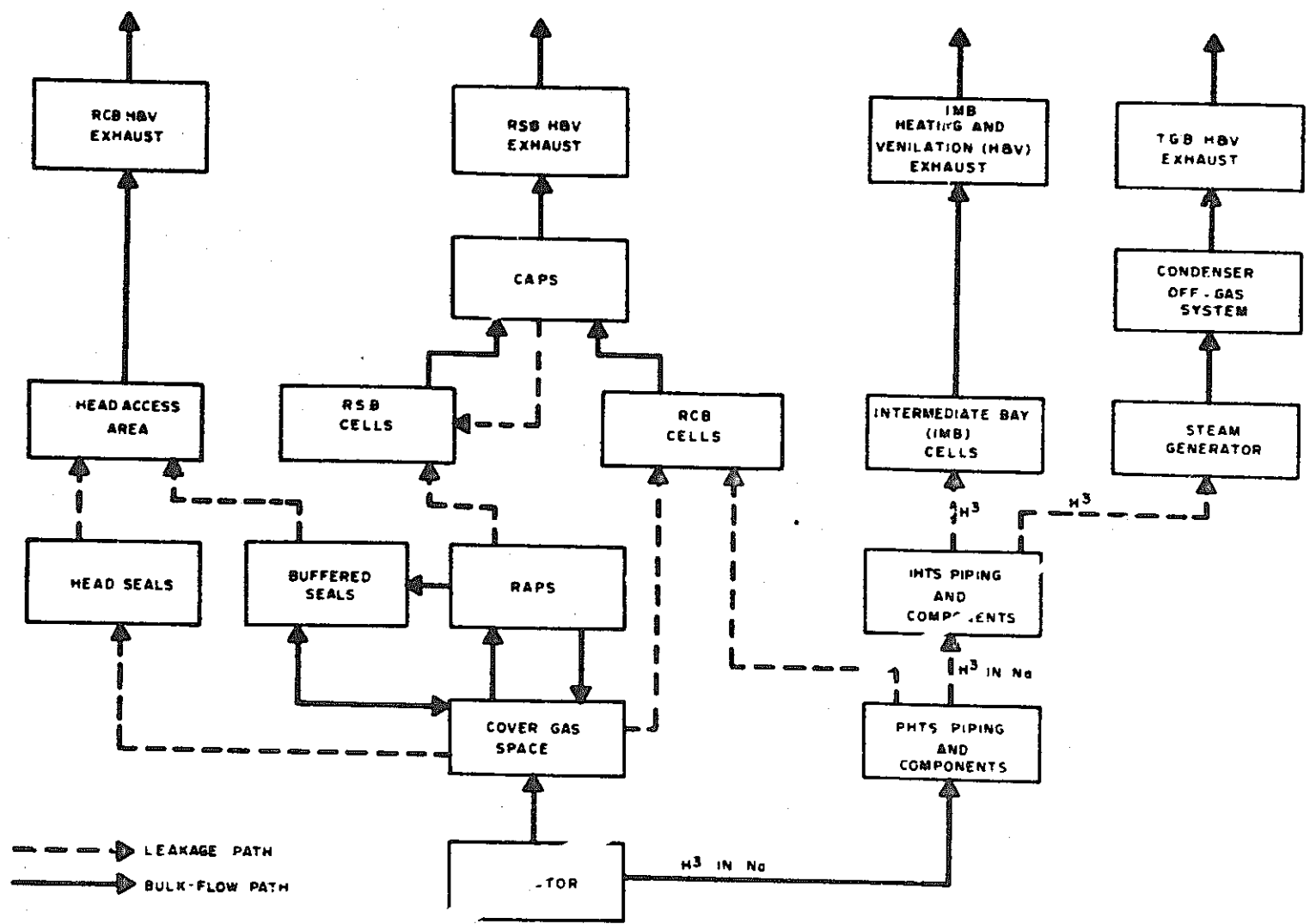


第5-1図 「NUJEEP」のコードエレメント  
相互関連図<sup>(3)</sup>

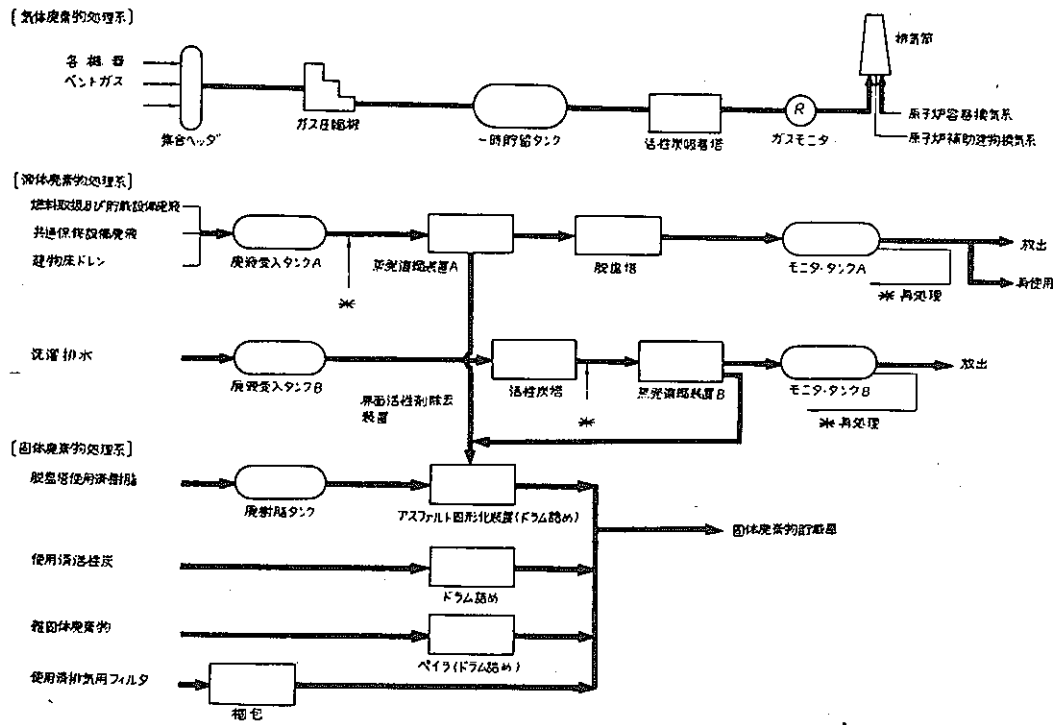


第 5 - 2 図 LMFBR 放射性廃棄物処理系計算モデル (NUJEEP) <sup>(33)</sup>

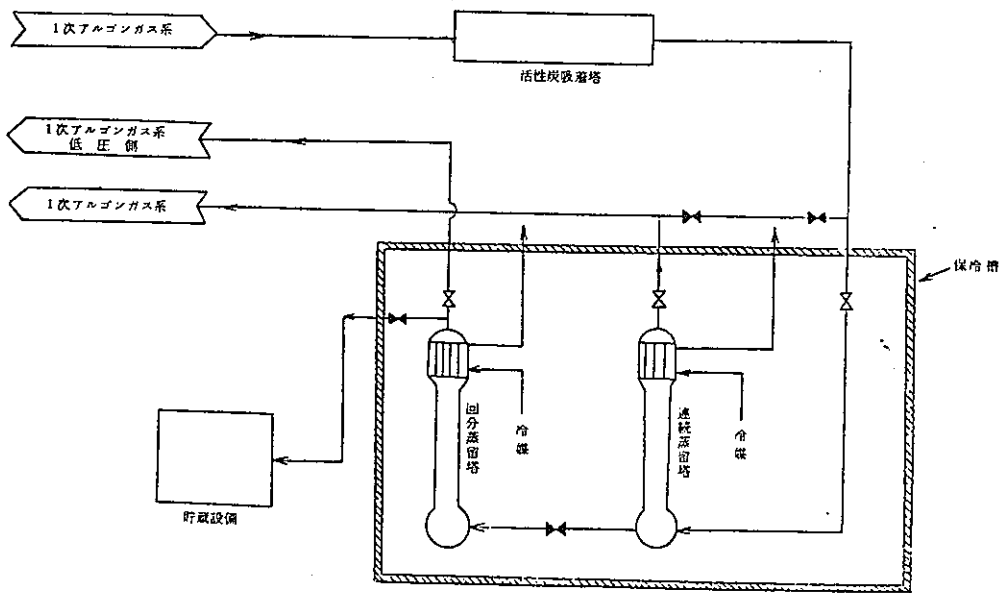




第 4 図 CRBRにおける放射性物質の大気放出経路 (1)



第5-5図 「もんじゅ」放射性廃棄物処理系説明図 (43)



第5-6図 「もんじゅ」の希ガス除去・回収設備系統図 (43)

# 表 関 係

第 2.1 - 1 表 C R B R 設計の主要項<sup>(69)</sup>

・原子炉型式	ループ型
・電気出力 (送電端)	3 5 0 M W e
・熱出力	9 7 5 M W t
・炉心燃料	( P u , U ) O <sub>2</sub>
・炉心寸法	
等価直径	1,870mm
高さ	915mm
・燃料インベントリー	
炉心 ( U m e t a l + P u m e t a l )	6,577 Kg
ブランケット ( U m e t a l )	21,720 Kg
・炉心燃料集合体本数 (内側 / 外側炉心)	108 / 90
・ブランケット燃料集合体本数	150
・炉心燃料集合体	
被覆材	SUS 316
被覆材外径	5.842 mm
被覆材肉厚	0.38 mm
・線出力	472.5 / 217 ( W / c m )
・軸方向ブランケット厚さ (上 / 下)	356.6mm / 356.6mm
・ガスプレナム長さ	1,219.2 mm
・ガスプレナム位置	炉心上部
・被覆材許容最高温度	732.2 °C
	(含むホットスポットファクタ)
・燃料中心最高温度	2,638 °C
・集合体当りピン本数 (炉心 / ブランケット)	217 / 61
・増殖比	~1.2
・取出し燃料燃焼度 (最大 / 平均)	15 / 10 ( × 10 <sup>4</sup> M W D / T )
・制御棒	
吸収材	B <sub>4</sub> C
調整棒本数 + 安全棒本数	15
後備炉停止棒本数	4
炉停止系ワース (1次 / 2次)	21.6 \$ / 6.84 \$
	(両系統共ワンロッドスタック時)

第 2.1-1 表 (つづき)

・原子炉容器寸法 (高さ/直径)	1 6.7 m/6.17 m
・ループ数	3
・クランピング構造	固定リング
・ポンプ位置 (1次系/2次系)	ホットレグ/コールドレグ
・1次冷却系流量	$6.23 \times 10^3 \text{ ton/hr} \cdot \text{ループ}$
・2次冷却系流量	$5.806 \times 10^3 \text{ ton/hr} \cdot \text{ループ}$
・原子炉出入口温度 (入口/出口)	388°C/535°C
・2次系中間熱交換器出入口温度 (入口/出口)	344°C/502°C
・中間熱交換器型式	縦型向流シェルアンドチューブ
・中間熱交換器基数	3
・蒸気発生器	
蒸気発生器型式	ホッキースティック
蒸発器基数 (ループ当り)	2
過熱器基数 (ループ当り)	1
蒸発器チューブ材	$2 \frac{1}{4} \text{ Cr-1Mo}$
過熱器チューブ材	$2 \frac{1}{4} \text{ Cr-1Mo}$
・給水温度	232°C
・主蒸気圧力	$102 \text{ Kg/cm}^2 \cdot \text{g}$
・主蒸気温度	482°C
・非常用炉心冷却系	
ループ数	3
除熱容量	1.2 MWt/ループ
ポンプ型式	縦型遠心式 (ボニーモータ付)
・炉内燃料交換方式	3 重回転プラグ
・燃料交換間隔	6ヶ月 (初期), 12ヶ月 (最終)
・格納容器	
型式	1 重鋼製容器
直径	5.67 m
高さ	7.71 m
設計条件 (温度/圧力)	121°C/0.703 Kg/cm <sup>2</sup> ・g

第 2.2 - 1 表

CRBRP WATER USAGE\* SEASONAL VARIATION  
(100% Load Factor)

Water Use	<u>Winter</u>	<u>Spring</u>	<u>Summer</u>	<u>Fall</u>	<u>Annual</u>
A. Plant Makeup	4,955	5,740	6,685	5,860	5,835
B. Consumptive Use					
1. Cooling Tower Evaporation	2,950	3,420	3,980	3,490	3,475
2. Cooling Tower Drift	105	105	105	105	105
3. Potable Water	<u>4</u>	<u>4</u>	<u>4</u>	<u>4</u>	<u>4</u>
Total Consumption	3,059	3,529	4,089	3,599	3,584
C. Discharge to Clinch River					
1. Cooling Tower Blowdown	1,855	2,170	2,545	2,220	2,210
2. Chemical Waste Treatment System	35	35	35	35	35
3. Sanitary Waste	5	5	5	5	5
4. Radwaste	<u>1</u>	<u>1</u>	<u>1</u>	<u>1</u>	<u>1</u>
Total Discharge	1,896	2,211	2,596	2,261	2,251

\*All values in gpm

第 2.2 - 2 表

ESTIMATED WET BULB TEMPERATURES BASED ON READILY AVAILABLE  
 DRY BULB TEMPERATURES AND RELATIVE HUMIDITIES AT KNOXVILLE, TENNESSEE

	Dry Bulb Temperature* (°F)	Relative Humidity* (%)	Wet Bulb Temperature** (°F)
January	41.4	70.8	40.0
February	43.1	67.0	42.0
March	49.6	63.3	48.0
April	58.9	62.5	56.5
May	67.7	67.3	64.5
June	75.7	73.5	73.5
July	78.4	75.8	75.5
August	77.4	76.0	74.5
September	72.2	74.3	69.5
October	60.9	71.0	58.5
November	48.7	71.3	48.0
December	41.6	71.5	41.0

\*Local Climate Copy Data, Annual Summary with Comparative Data,  
 Knoxville, Tennessee, 1931-1960, No. AA, U.S. Department of  
 Interior, 1971.

\*\*Psychrometric chart conversion of columns 1 and 2

Ref. (1) TABLE 3.4-3

第 2.2 - 3 表

WATER TEMPERATURES OF THE CLINCH RIVER  
AND THE COOLING TOWER BLOWDOWN\*

	<u>River Water**</u>			<u>Mechanical Wet Cooling Tower Blowdown</u>		
	<u>Average</u>	<u>Average Maximum</u>	<u>Average Minimum</u>	<u>Average</u>	<u>Daily Maximum</u>	<u>Daily Minimum</u>
January	42.7	48.0	37.9	66	68	61.5
February	42.1	48.0	37.6	67	68.5	61.5
March	47.0	54.9	40.9	70	72	63.5
April	55.1	62.3	48.1	74.5	77	66.5
May	60.9	66.4	56.0	79.5	83	70.5
June	63.5	69.9	58.5	85	88.5	75
July	64.4	69.4	60.3	86.5	90.5	77.5
August	65.7	70.1	61.9	86	90	77
September	66.9	70.4	63.4	82.5	87.5	73.5
October	64.6	68.7	60.2	76	80.5	68
November	57.0	63.4	50.4	70	72.5	63.5
December	47.7	53.8	43.0	66.5	68.5	61.5

\*All temperatures are in degrees Fahrenheit

\*\*June 1963 to October 1972, Whitewing Bridge Temperature Data from TVA

Ref.(1) AMENDMENT VI TABLE 3.4-4



第 2.2 - 4 表 PRELIMINARY ESTIMATES OF EFFLUENT WATER CONCENTRATIONS

	Clinch River (Background)*		Cooling Tower Blowdown**		CRRRP Waste Streams		Sanitary Wastes Based on the Design Loading (mg/l)	Discharge to River		
	Avg. Conc. (mg/l)	Max. Conc. (mg/l)	Neutralized Plant Wastes <sup>v</sup>		Based on Avg. Discharge -3.7 gpm (mg/l)	Based on Max. Discharge -35 gpm (mg/l)		Annual Quantity <sup>++</sup> (10 <sup>4</sup> lbs/yr)	Concentration	
			Based on Avg. River Conc. (mg/l)	Based on Max. River Conc. (mg/l)					Average (mg/l)	Maximum (mg/l)
Total Alkalinity (as CaCO <sub>3</sub> )	95	116	240	290	50	50	--	NA	239	296
Ammonia Nitrogen (as N)	0.28	1.00	0.70	2.50	--	--	0.5	0.47	0.70	2.50
BOD	2.1	6.0	5.3	15.0	--	--	12	3.5	5.3	15.0
Calcium	34	43	85	108	224	96	--	57	85	108
Chloride	4.7	13.0	11.8	32.5	43	21	--	7.8	11.8	32.3
Chlorine Residual	--VV	--VV	0.2	0.5	--	--	1	0.1	0.2	0.5
COD	6.7	16.0	16.8	40.0	--	--	25	11.2	16.8	40.0
Copper <sup>+</sup>	0.005	<0.01	0.20	0.93	--	--	--	0.13	0.20	0.93
Total Dissolved Solids (TDS)	142	174	355	435	13,738	11,920	--	249	377	614
Total Iron <sup>+</sup>	0.38	0.68	0.95	1.72	--	--	--	0.63	0.95	1.72
Lead	<0.03	<0.03	<0.03	<0.03	--	--	--	<0.01	<0.03	<0.03
Magnesium	7.8	8.5	19.5	21.3	75	32	--	13.0	19.6	21.4
Manganese <sup>+</sup>	0.05	0.07	0.13	0.18	1	0.4	--	0.09	0.13	0.18
Nickel <sup>+</sup>	<0.01	<0.01	0.02	0.14	--	--	--	0.01	0.02	0.11
Nitrate (NO <sub>3</sub> )	1.3	2.2	3.3	5.5	3.2	1	66	2.3	3.4	5.6
pH	7.9	8.3	7.9	8.3	6.5-8.5	6.5-8.5	6-9	NA	6.5-8.5	6.5-8.5
Total Phosphate	0.05	0.4	0.13	1.00	1	0.4	5	0.10	0.14	1.07
Potassium	1.4	1.9	3.5	4.8	15	7	--	2.3	3.5	4.8
Silica (SiO <sub>2</sub> )	3.9	6.1	9.8	15.3	27	12	--	6.5	9.8	15.3
Sodium	2.1	2.5	5.3	6.3	5,800	7,900	--	12.1	15.0	129
Sulfate (SO <sub>4</sub> )	15	23	38	58	7,500	3,800	--	29.4	50	116
Total Suspended Solids (TSS)	13	46	33	115	<30	<30	5	21.9	33	114
Zinc <sup>+</sup>	0.02	0.03	0.05	0.08	--	--	--	0.03	0.05	0.08

\* Based on the Aquatic Baseline Monitoring Program chemical data.

\*\* Includes several recycled waste streams (Make-Up Water System equipment rinses, Backwashes and blowdown; non-radioactive floor drains). These do not measurably affect the Cooling Tower Blowdown Chemical Concentrations.

+ Includes Make-Up Water Demineralizer and Steam Condensate Polisher regeneration wastes, Auxiliary Boiler blowdown and Non-Radioactive Lab and Sampling Wastes.

++ Computed as follows: Quantity from Cooling Tower Blowdown = (Avg. Conc.) (Annual Avg. Blowdown = 2,210 gpm) (Plant Load Factor = 68.5%)  
 Quantity from Neutralized Plant Wastes = (Conc.) (Flow = 35 gpm) (24 hr/day operation) (26 operation days/yr)  
 Quantity from Sanitary Wastes = (Conc.) (Flow = 5 gpm) (24 hr, any operation) (365 operation days/yr)

<sup>v</sup>  $\frac{(\text{Conc.})(\text{Flow})}{(\text{Flow})}$ , where Avg. Conc. is based on average river conc. (cooling tower blowdown) and average discharge flow (neutralized plant wastes) and Max. Conc. is based on max. river conc. and max. discharge flow.

VV Field measurements using the orthotolidine calorimetric method repeatedly showed the chlorine residual concentration to be below the limits of detection (0.05 mg/l). As there are no nearby sources of chlorine additions to the river. It can be assumed that the ambient level is zero.

+ Includes contribution to effluent quantities from condenser erosion/corrosion.

第 2.2 - 5 表

BOP CHEMICAL STORAGE TANKS

<u>Chemical</u>	<u>Tank Capacity</u>	<u>Location</u>
Sulfuric Acid	6,000 gallons	Turbine Building Basement
Sodium Hydroxide	6,000 gallons	Turbine Building Basement
Hydrazine (35% dilution)	300 gallons	Turbine Building Basement
Ammonia	3,000 gallons	Turbine Building Basement

Ref. (1) TABLE 7.2-1

第 2.2 - 6 表

ESTIMATED\* SODIUM HYDROXIDE RELEASES FOR REPRESENTATIVE POTENTIAL FIRE ACCIDENTS

<u>Accident No.**</u>	<u>Description</u>	<u>Duration</u>	<u>Average Concentration (mg/m<sup>3</sup>)</u>	<u>Peak Concentration (mg/m<sup>3</sup>)</u>
4.1	Failure of ex-containment primary sodium drain pipe during maintenance	2 minutes	1.73	2.54
5.2	Steam generator tube rupture	15 seconds	7.95	--
8.1	Primary sodium in-containment drain tank failure during maintenance	145 hours	$3 \times 10^{-7}$	$7.3 \times 10^{-5}$

\*Estimated sodium hydroxide levels at the closest Site boundary

\*\*Refer to accident numbering in Section 7.1

Ref. (1) AMENDMENT VII TABLE 7.2-2

第 2.2 - 7 表

FISSION PRODUCT ESCAPE FRACTIONS

Class	Element	Escape Fractions
1	Kr*, Xe*, Cs <sup>136</sup>	$EF = \frac{1}{(1.5E5)\lambda} (1 - e^{-(1.5E5)\lambda})^{**}$
2	Cs <sup>134, 137</sup>	EF = 1.0
3	Sb, Te, I	$EF = \frac{0.2}{(1.5E6)\lambda} (1 - e^{-(1.5E6)\lambda})^{**}$
4	Sr	EF = 0.005
5	All other Fission Products	EF = 0.001

\*Assumed released to cover gas

\*\*λ in (sec<sup>-1</sup>) decay constant of ith isotope

Ref.(1) AMENDMENT I TABLE 1 (Item 0105)

第 2.2 - 8 表

## PRODUCTION RATES OF RADIONUCLIDES

<u>Isotope</u>	<u>Half-Life</u>	<u>Cover Gas Input Rate (Ci/day)</u>
Xe-131m	11.96 days	$1.1 \times 10^2$
Xe-133m	2.26 days	$3.8 \times 10^3$
Xe-133	5.27 days	$6.5 \times 10^4$
Xe-135m	15.7 minutes	$9.6 \times 10^4$
Xe-135	9.16 hours	$3.4 \times 10^5$
Xe-138	14.2 minutes	$1.7 \times 10^5$
Kr-83m	1.86 hours	$1.6 \times 10^4$
Kr-85m	4.4 hours	$3.0 \times 10^4$
Kr-85	10.76 year	$2.0 \times 10^1$
Kr-87	76 minutes	$5.2 \times 10^4$
Kr-88	2.79 hours	$6.4 \times 10^4$
Ar-39	269 years	$1.3 \times 10^{-1}$
Ar-41	110 minutes	$4.0 \times 10^2$
Ne-23	38 seconds	$1.4 \times 10^9$
H-3	12.5 years	$3.4 \times 10^{-6}$

Ref. (1) AMENDMENT VII TABLE 3.5-6

第 2.2 - 9 表

EXPECTED CONCENTRATION OF LOW AND INTERMEDIATE ACTIVITY  
LEVEL INPUT STREAMS\*

Isotope	Half-Life	Concentration ( $\mu\text{Ci/cc}$ )		
		Low Level**	Intermediate, First Rinse <sup>+</sup>	Intermediate, Acid Etch <sup>++</sup>
H-3	12.3 years	$2.37 \times 10^{-6}$	$3.50 \times 10^{-4}$	$3.50 \times 10^{-4}$
Na-22	2.6 years	$1.99 \times 10^{-6}$	$2.83 \times 10^{-4}$	--
Na-24	15 hours	$5.69 \times 10^{-7}$	$8.99 \times 10^{-5}$	--
Cr-51	28 days	--	$1.30 \times 10^{-2}$	$1.31 \times 10^{-2}$
Mn-54	312 days	$2.24 \times 10^{-8}$	$9.15 \times 10^{-2}$	$9.21 \times 10^{-2}$
Co-58	71 days	$5.66 \times 10^{-9}$	$5.62 \times 10^{-2}$	$5.66 \times 10^{-2}$
Fe-59	45 days	--	$4.51 \times 10^{-4}$	$4.54 \times 10^{-4}$
Co-60	5.2 years	$3.03 \times 10^{-9}$	$8.58 \times 10^{-2}$	$9.03 \times 10^{-2}$
Sr-89	51 days	$1.03 \times 10^{-8}$	$5.16 \times 10^{-3}$	$5.19 \times 10^{-3}$
Sr-90	28.8 years	$7.37 \times 10^{-9}$	$3.71 \times 10^{-3}$	$3.73 \times 10^{-3}$
Y-90		$7.37 \times 10^{-9}$	$3.71 \times 10^{-3}$	$3.73 \times 10^{-3}$
Y-91	58 days	$3.01 \times 10^{-9}$	$1.52 \times 10^{-3}$	$1.53 \times 10^{-3}$
Zr-95	65 days	$5.70 \times 10^{-9}$	$2.85 \times 10^{-3}$	$2.87 \times 10^{-3}$
Nb-95		$5.70 \times 10^{-9}$	$2.85 \times 10^{-3}$	$2.87 \times 10^{-3}$
Mo-99	67 hours	--	$3.22 \times 10^{-4}$	$3.24 \times 10^{-4}$
Ru-103	40 days	$7.90 \times 10^{-9}$	$3.96 \times 10^{-3}$	$3.98 \times 10^{-3}$
Ru-106	1 year	$6.13 \times 10^{-9}$	$3.07 \times 10^{-3}$	$3.09 \times 10^{-3}$
Rh-106		$6.13 \times 10^{-9}$	$3.07 \times 10^{-3}$	$3.09 \times 10^{-3}$
Ag-111	7.5 days	--	$1.05 \times 10^{-4}$	$1.05 \times 10^{-4}$
Sb-125	2.7 years	$5.24 \times 10^{-8}$	$7.45 \times 10^{-6}$	--
Te-129m	34 days	$6.41 \times 10^{-8}$	$3.17 \times 10^{-2}$	--
Te-129		$6.41 \times 10^{-8}$	$3.17 \times 10^{-2}$	--
I-131	8.1 days	$2.44 \times 10^{-6}$	$3.46 \times 10^{-4}$	--
Te-132	78 hours	$4.57 \times 10^{-8}$	$2.61 \times 10^{-2}$	--
I-132		$4.57 \times 10^{-8}$	$2.61 \times 10^{-2}$	--

(Continued)

第 2.2 - 9 表 (Continued)

Isotope	Half-Life	Concentration ( $\mu\text{Ci/cc}$ )		
		Low Level**	Intermediate, First Rinse*	Intermediate, Acid Etch**
Cs-134	2.1 years	$2.46 \times 10^{-7}$	$3.50 \times 10^{-5}$	--
Cs-136	13 days	$1.11 \times 10^{-6}$	$1.57 \times 10^{-4}$	--
Cs-137	30 years	$9.03 \times 10^{-6}$	$8.44 \times 10^{-4}$	$2.68 \times 10^{-4}$
Ba-140	12.8 days	$4.13 \times 10^{-9}$	$2.07 \times 10^{-3}$	$2.08 \times 10^{-3}$
La-140		$4.13 \times 10^{-9}$	$2.07 \times 10^{-3}$	$2.08 \times 10^{-3}$
Ce-141	32.5 days	$6.81 \times 10^{-9}$	$3.41 \times 10^{-3}$	$3.43 \times 10^{-3}$
Fr-143	13.7 days	$3.57 \times 10^{-9}$	$1.79 \times 10^{-3}$	$1.80 \times 10^{-3}$
Ce-144	285 days	$4.84 \times 10^{-9}$	$2.43 \times 10^{-3}$	$2.45 \times 10^{-3}$
Pr-144		$4.84 \times 10^{-9}$	$2.43 \times 10^{-3}$	$2.45 \times 10^{-3}$
Nd-147	11.1 days	$1.49 \times 10^{-9}$	$7.50 \times 10^{-4}$	$7.54 \times 10^{-4}$
Pm-147	2.7 days	$2.78 \times 10^{-9}$	$1.39 \times 10^{-3}$	$1.40 \times 10^{-3}$
Eu-155	1.8 years	--	$1.37 \times 10^{-4}$	$1.37 \times 10^{-4}$
Ta-182	115 days	--	$1.07 \times 10^{-2}$	$1.08 \times 10^{-2}$
Pu-238	86 years	$8.55 \times 10^{-9}$	$3.59 \times 10^{-5}$	$3.46 \times 10^{-5}$
Pu-239	$2 \times 10^4$ years	$2.37 \times 10^{-9}$	$7.95 \times 10^{-6}$	$7.66 \times 10^{-6}$
Pu-240	$6.7 \times 10^3$ years	$3.09 \times 10^{-9}$	$1.94 \times 10^{-5}$	$9.98 \times 10^{-6}$
Pu-241	13 years	$2.59 \times 10^{-7}$	$8.71 \times 10^{-4}$	$8.39 \times 10^{-4}$
Pu-242	$3.8 \times 10^5$ years	$6.56 \times 10^{-12}$	$5.21 \times 10^{-8}$	$2.13 \times 10^{-8}$

\*0.1 percent failed fuel for solid fission products and 50 ppb Pu in sodium, 30-year irradiation and 10 days decay. Decay times during collection, processing and holdup are neglected.

\*\*Low activity concentration computed by assuming that listed isotopes are present in 3.5 pounds of primary sodium per year diluted by  $3.1 \times 10^5$  gallons per year.

\*Intermediate activity annual concentrations for first rinse are computed assuming 40 percent of deposited activity and 100 percent of sodium activity adhering to processed components is dissolved in 37,000 gallons of water per year. The solution is present in the input stream to the collection tanks.

\*\*The average annual acid etch solution consists of 20 percent of the plated activity from processed components in an average annual volume of 14,700 gallons. All sodium activity is assumed to have been removed in the first water rinse.

<sup>v</sup>Isotope pairs in secular equilibrium

Ref. (1) AMENDMENT IV TABLE 3.5-1

第 2.2 - 1 0 表

PARAMETERS ASSUMED FOR PLUTONIUM RELEASE TO PRIMARY COOLANT\*

Parameter	Data	
1. Equilibrium core (MOL)** Pu inventories	Isotope	Weight (kgm)
	Pu <sup>239</sup>	$1.026 \times 10^3$
	Pu <sup>240</sup>	$3.65 \times 10^2$
	Pu <sup>241</sup>	$1.31 \times 10^2$
	Pu <sup>242</sup>	$4.66 \times 10^1$
	Pu <sup>238</sup>	$1.4 \times 10^1$
2. Total number of fuel rods	42,966	
3. Failed fuel rods containing a postulated 0.03 in. dia. hole in the fuel zone	43	
4. Plutonium escape rate coefficient	$9.71 \times 10^{14} \frac{\text{atoms}}{\text{cm}^2\text{-sec}}$	

\*For conservatism, 95% deposition in primary Na, 5% on wetted surfaces and 100% in cold traps is assumed in analyses.

\*\*MOL = Middle of Life

Ref. (1) AMENDMENT I TABLE 1A... ITEM 010.4



第 2.2 - 1 1 表

ISOTOPIC ATOM DENSITIES FOR STAINLESS STEEL-316  
(Stainless Steel-316 = 7.98 gm/cc)

Isotope	Material Weight-%	Density gm/cc	(NA) Natural Abundance (%)	(AW) Atomic Weight	Atoms/cm <sup>3</sup> Atom Density*
Cr <sup>50</sup> (n,γ)Cr <sup>51</sup>	18.00 (Cr)	1.436 (Cr)	4.31 (Cr <sup>50</sup> )	52.0569 (Cr)	7.162E20 (Cr <sup>50</sup> )
Fe <sup>54</sup> (n,p)Mn <sup>54</sup>	65.17 (Fe)	5.201 (Fe)	5.82 (Fe <sup>54</sup> )	55.9121 (Fe)	3.261E21 (Fe <sup>54</sup> )
Fe <sup>58</sup> (n,γ)Fe <sup>59</sup>	65.17 (Fe)	5.201 (Fe)	0.33 (Fe <sup>58</sup> )	55.9121 (Fe)	1.849E20 (Fe <sup>58</sup> )
Ni <sup>58</sup> (n,p)Co <sup>58</sup>	14.00 (Ni)	1.17 (Ni)	67.88 (Ni <sup>58</sup> )	58.7947 (Ni)	7.769E21 (Ni <sup>58</sup> )
Co <sup>59</sup> (n,γ)Co <sup>60</sup>	0.05 (Co)	0.004 (Co)	100.00 (Co <sup>59</sup> )	59.0000 (Co)	4.08E19 (Co <sup>59</sup> )
Ta <sup>181</sup> (n,γ)Ta <sup>182</sup>	0.02 (Ta)**	0.0016 (Ta)	99.99 (Ta <sup>181</sup> )	181.0000 (Ta)	5.32E19 (Ta <sup>181</sup> )

\*Atom density of target isotope

\*\*The nominal tantalum - columbium material weight of 0.02 is assumed to be 100% tantalum - the more significant component.

第 2.2 - 1 2 表

## ACTIVATION CROSS-SECTION (BARNS/ATOM)

Group	Energy Max/Group	Cr-50 (n, $\gamma$ )	Fe-54 (n,p)	Fl-58 (n, $\gamma$ )	Ni-58 (n,p)	Co-59 (n, $\gamma$ )	Ta-181 (n, $\gamma$ )
1	10.5 Mev	0	0.54	0	0.435	0.002	0.01
2	6.5		0.43		0.356	0.002	0.03
3	4.0		0.20		0.162	0.002	0.04
4	2.5		0.04		0.03	0.0031	0.10
5	1.4		0	0.001897	0.0017	0.0046	0.14
6	0.8			0.00237	0	0.0051	0.20
7	0.4			0.00285		0.008	0.27
8	0.2			0.00285		0.008	0.32
9	0.1	0.01		0.00332		0.056	0.45
10	46.5 kev	0.03		0.00806		0.038	0.80
11	21.1	0.065		0.00237		0.46	1.5
12	10.0	0.025		0.001897		1.2	2.9
13	4.65	0.14		0.00522		4.83	5.3
14	2.15	0.09		0.0503		2.81	9.6
15	1.0	0.11		0.00711		0.4	16.7
16	465 ev	0.15		0.0133		3.5	22.0
17	125	0.23		0.0175		24.8	32.0
18	100	0.33		0.025		49.1	32.0
19	46.5	0.48		0.034		1.15	104
20	21.5	0.70		0.049		1.56	111
21	10.0	1.00		0.073		2.19	16
22	4.65	1.50		0.104		3.5	483
23	2.15	2.20		0.156		4.63	4.2
24	1.0	3.20		0.232		6.75	4.9
25	0.465	4.70		0.342		10.2	6.4
26	0.0252	17.0		1.2		37.2	21.0

Ref. (1) AMENDMENT I TABLE 3 ... ITEM 0104

第 2.2 - 1 3 表

RADIAL ZONE PARAMETERS

Radial Zone	Description	$\Delta T^*$ Effective Temperature Rise ( $^{\circ}F$ )	Velocity (ft/sec)	Fraction Replaced/yr, f	Max. Assem. Residence Years (m)
1	1 Control Assemblies	110	8.0	1	1
2	24 Fuel Assemblies	318	24.6	1/3	3
3	6 Control Assemblies	110	8.0	1	1
4	52 Fuel Assemblies	327	22.9	1/3	3
5	6 Control Assemblies	110	8.0	1	1
6	24 Fuel Assemblies	312	19.3	1/3	3
7	6 Control Assemblies	110	8.0	1	1
8	90 Fuel Assemblies	309	20.0	1/3	3
9	150 Blanket Assemblies	271	5.19	1/5	5
10	72 Reflector Assemblies	260	1.0	1/7	7

\* $T_{inlet} = 740^{\circ}F$  for all zones

Ref.(1) AMENDMENT I TABLE 4... ITEM 010.4

第 2.2 - 1 4 表

TOTAL ACTIVATED CORROSION PRODUCTS RELEASED TO THE  
PRIMARY SODIUM - CURIES

<u>Isotope</u>	<u>Reactor Operating Time - Years</u>			
	<u>5</u>	<u>10</u>	<u>20</u>	<u>30</u>
Co-50	525	795	1,004	1,060
Co-58	729	729	729	729
Mn-54	1,080	1,100	1,100	1,100
Fe-59	6.2	6.2	6.2	6.2
Cr-51	195	195	195	195
Ta-182	141	141	141	141

Ref. (1) AMENDMENT TABLE 5 ... ITEM 0104

第 2.2 - 1 5 表

EXPECTED WEIGHT, VOLUME AND ACTIVITY OF SOLID RADWASTE  
IN TERMS OF ANNUAL QUANTITIES

	Volume (ft <sup>3</sup> )	Weight (lbs)	Activity (Ci)	Comment.**
Compactible Solids*	284	1.6 x 10 <sup>4</sup>	<1.0	Rags, paper and seals
Non-Compactible Solids				
Scrapped Components	705	5.7 x 10 <sup>4</sup>	82	Scrapped IHX after decontamination, valves, vapor traps
Resins	450 5	2.0 x 10 <sup>4</sup> 2.5 x 10 <sup>2</sup>	3.0 <1.0	Tritium; BOP* FP + CP; RWS
Filters	340 <sup>++</sup>	9.0 x 10 <sup>3</sup> *	25	Na + CP + FP
Solidified Liquid Radwaste	1	1.4 x 10 <sup>5</sup>	1.4 x 10 <sup>3</sup>	Concentrated evaporator bottoms
Solidified Tritiated Water	33	2.1 x 10 <sup>3</sup>	66	--
Metallic Sodium	42	2.5 x 10 <sup>3</sup>	9	Ex-vessel storage tank sodium
Sodium Bearing Solids	235	1.4 x 10 <sup>4</sup>	4.2 x 10 <sup>4</sup> 2.2 x 10 <sup>4</sup>	Tritium in sodium CP + FP
<b>Total</b>	<b>3,094</b>	<b>2.6 x 10<sup>5</sup></b>	<b>6.6 x 10<sup>4</sup></b>	

\*Assume compaction has decreased in volume by factor of 10

\*\*Average buildup of activities  $\frac{\text{Activity at end-of-life}}{\text{Total years operation}}$

\* H&V = Heating and Ventilation  
RWS = Radwaste System  
BOP = Balance of Plant  
FP = Fission products  
CP = Corrosion products

++Includes H&V and RWS

Ref. (1) AMENDMENT VIII TABLE 3.5-10

第 2.2 - 1 6 表

EXPECTED SOLID RADWASTE SHIPMENTS PER YEAR

<u>Material</u>	<u>Shipments Per Year</u>	<u>Volume (ft<sup>3</sup>)</u>	<u>Containers Per Year*</u>
Compactible Solids	0.2	284	28
Non-Compactible Solids			
Scrapped Components	6	705	82
Filters and Resins	0.6	795	120
Solidified Liquid Radwaste	9	1,000	170
Metallic Sodium	0.4	42	6
Sodium Bearing Solids	TBD	235	TBD

\*55-gallon drums

Ref. (1) AMENDMENT VII TABLE 3.5-11

第 2.2 - 1 7 表

CAPS PERFORMANCE SUMMARY DATA

<u>Isotope</u>	<u>Decontamination Factor<sup>a</sup></u>
Xe-131m	$2.89 \times 10^1$
Xe-132m	$1.9 \times 10^7$
Xe-133	$1.7 \times 10^3$
Xe-135m	$\gg 1.0 \times 10^{10}$
Xe-135	$\gg 1.0 \times 10^{10}$
Xe-138	$\gg 1.0 \times 10^{10}$
Kr-83m	$9.7 \times 10^9$
Kr-85m	$1.1 \times 10^5$
Kr-85	$1.0 \times 10^0$
Kr-87	$\gg 1.0 \times 10^{10}$
Kr-88	$1.5 \times 10^7$
Ar-39	$1.0 \times 10^0$
Ar-41	$4.5 \times 10^2$
Ne-23	$\gg 1.0 \times 10^{10}$
H-3	$1.0 \times 10^3$

<sup>a</sup> Includes cell delay effects

Ref. (1) AMENDMENT VII TABLE 3.5-5

第 2.2 - 1 8 表

## RAPS DELAY BED SYSTEM PERFORMANCE SUMMARY DATA

Isotope	Effective Delay Holdup Times (days)	Cover Gas Inventory* (Curies)	Cover Gas* Concentration ( $\mu\text{Ci/cc}$ )	RAPS Output Concentration** ( $\mu\text{Ci/cc}$ )	Decontamination Factor
Xe-131m	570	$8.8 \times 10^0$	$1.6 \times 10^0$	$\ll 10^{-10}$	$\gg 10^{11}$
Xe-133m	570	$5.8 \times 10^2$	$5.2 \times 10^1$	$\ll 10^{-10}$	$\gg 10^{11}$
Xe-133	570	$4.8 \times 10^3$	$9.1 \times 10^2$	$\ll 10^{-10}$	$\gg 10^{11}$
Xe-135m	570	$1.3 \times 10^3$	$1.2 \times 10^2$	$\ll 10^{-10}$	$\gg 10^{11}$
Xe-135	570	$4.2 \times 10^4$	$3.6 \times 10^3$	$\ll 10^{-10}$	$\gg 10^{11}$
Xe-138	570	$2.2 \times 10^3$	$1.9 \times 10^2$	$\ll 10^{-10}$	$\gg 10^{11}$
Kr-83m	7.44	$1.1 \times 10^3$	$9.3 \times 10^2$	$\ll 10^{-10}$	$\gg 10^{11}$
Kr-85m	7.44	$3.0 \times 10^3$	$2.6 \times 10^2$	$\ll 10^{-10}$	$\gg 10^{11}$
Kr-85	7.44	$3.3 \times 10^{-1}$	$2.8 \times 10^{-2}$	$2.0 \times 10^{-5}$	1.0
Kr-87	7.44	$2.7 \times 10^3$	$2.3 \times 10^2$	$\ll 10^{-10}$	$\gg 10^{11}$
Kr-88	7.44	$5.3 \times 10^3$	$4.6 \times 10^2$	$\ll 10^{-10}$	$\gg 10^{11}$
Ar-39**	0.235	$1.4 \times 10^0$	$1.2 \times 10^{-1}$	$1.2 \times 10^{-1}$	1.0
Ar-41**	0.235	$2.7 \times 10^1$	$2.3 \times 10^0$	$7.5 \times 10^{-4}$	6.5
Ne-23**	$6.1 \times 10^{-2}$	$8.9 \times 10^5$	$7.7 \times 10^4$	$\ll 10^{-10}$	$\gg 10^{11}$
H-3**	$2.5 \times 10^{-4}$	$3.0 \times 10^{-3}$	$2.6 \times 10^{-4}$	$2.6 \times 10^{-4}$	1.0

\*After 1 year of operation and with 1 percent failed fuel (equilibrium or maximum values are quoted).

\*\*Concentration in recycle tank

\*The purge factor used for the cover gas space is  $6.14 \text{ day}^{-1}$ .

\*\*Inventories independent of failed-fuel percentage

Ref. (1) AMENDMENT IV TABLE 3.5-4



第 2.2 - 1 9 表

RADIONUCLIDE RELEASE RATES AND RELEASE PATHS FOR THE DESIGN VALUE SERVICE CONDITION

Isotope	Cover Gas Leakage: RCB H&V Exhaust (Ci/day)	Buffer Seal Leakage: RCB H&V Exhaust (Ci/day)	Primary Piping Leakage: RCB Cells to CAPS to RSB H&V Exhaust (Ci/day)	RAPS/CAPS Components Leakage: RSB Cells to CAPS to RSB H&V Exhaust (Ci/day)	Intermediate Cells Leakage: Natural Con- vection to Environment (Ci/day)	Total Leakage (Ci/day)
Xe-131m	$2.7 \times 10^{-5}$	++	$7.8 \times 10^{-5}$	$4.2 \times 10^{-5}$	0	$1.5 \times 10^{-4}$
Xe-133m	$8.7 \times 10^{-4}$	++	$3.8 \times 10^{-9}$	$1.9 \times 10^{-9}$	0	$8.7 \times 10^{-4}$
Xe-133	$1.5 \times 10^{-2}$	++	$7.6 \times 10^{-4}$	$4.0 \times 10^{-4}$	0	$1.7 \times 10^{-2}$
Xe-135m	$2.1 \times 10^{-3}$	++	++	++	0	$2.1 \times 10^{-3}$
Xe-135	$6.3 \times 10^{-2}$	++	++	++	0	$6.3 \times 10^{-2}$
Xe-138	$3.3 \times 10^{-3}$	++	++	++	0	$3.3 \times 10^{-3}$
Kr-83m	$1.6 \times 10^{-3}$	++	$1.4 \times 10^{-11}$	++	*	$1.6 \times 10^{-3}$
Kr-85m	$4.5 \times 10^{-3}$	++	$3.4 \times 10^{-6}$	$1.2 \times 10^{-6}$	0	$4.5 \times 10^{-3}$
Kr-85	$4.8 \times 10^{-7}$	$2.0 \times 10^{-7}$	$4.0 \times 10^{-5}$	$2.2 \times 10^{-5}$	0	$6.2 \times 10^{-5}$
Kr-87	$4.0 \times 10^{-3}$	++	++	++	0	$4.0 \times 10^{-3}$
Kr-88	$7.9 \times 10^{-3}$	++	$4.4 \times 10^{-8}$	$1.4 \times 10^{-8}$	0	$7.9 \times 10^{-3}$
Ar-39**	$2.0 \times 10^{-6}$	$1.2 \times 10^{-3}$	$1.7 \times 10^{-4}$	$1.7 \times 10^{-4}$	0	$1.5 \times 10^{-3}$
Ar-41**	$4.0 \times 10^{-5}$	$7.6 \times 10^{-5}$	$7.3 \times 10^{-6}$	$2.0 \times 10^{-6}$	0	$5.7 \times 10^{-5}$
He-23**	$5.5 \times 10^{-3}$	++	$1.1 \times 10^{-8}$	$6.8 \times 10^{-9}$	0	$5.5 \times 10^{-3}$
H-3***, †	$4.5 \times 10^{-9}$	$2.6 \times 10^{-6}$	$3.8 \times 10^{-10}$	$3.8 \times 10^{-10}$	$1.7 \times 10^{-3}$	$1.7 \times 10^{-3}$
Total	$1.1 \times 10^{-1}$	$1.2 \times 10^{-3}$	$1.0 \times 10^{-3}$	$6.4 \times 10^{-4}$	$1.7 \times 10^{-3}$	$1.1 \times 10^{-1}$

\*One percent failed fuel

\*\*Release rates independent of failed fuel fraction.

†BOP tritium release ( $6.9 \times 10^{-3}$  Ci/day) from TG Building Exhaust not included

\*\*Less than  $10^{-15}$

第 2.2 - 2 0 表

ANNUAL ACTIVITY RELEASE RATES FOR THE  
EXPECTED SERVICE CONDITION<sup>†</sup>

Radionuclide	Main RCB H&V Exhaust (Ci/yr)	RSB H&V Exhaust (Ci/yr)	Intermediate Bay Leakage (Ci/yr)	Total Release (Ci/yr)
Xe-131m	$9.9 \times 10^{-4}$	$4.4 \times 10^{-3}$	0	$5.4 \times 10^{-3}$
Xe-133m	$3.2 \times 10^{-2}$	$2.1 \times 10^{-6}$	0	$3.2 \times 10^{-2}$
Xe-133	$5.5 \times 10^{-1}$	$4.4 \times 10^{-2}$	0	$5.9 \times 10^{-1}$
Xe-135m	$7.7 \times 10^{-2}$	++	0	$7.7 \times 10^{-2}$
Xe-135	$2.3 \times 10^0$	++	0	$2.3 \times 10^0$
Xe-138	$1.2 \times 10^{-1}$	++	0	$1.2 \times 10^{-1}$
Kr-83m	$5.8 \times 10^{-2}$	++	0	$5.8 \times 10^{-2}$
Kr-85m	$1.6 \times 10^{-1}$	$1.7 \times 10^{-4}$	0	$1.6 \times 10^{-1}$
Kr-85	$2.5 \times 10^{-5}$	$2.3 \times 10^{-3}$	0	$2.3 \times 10^{-3}$
Kr-87	$1.5 \times 10^{-1}$	++	0	$1.5 \times 10^{-1}$
Kr-88	$2.9 \times 10^{-1}$	$2.1 \times 10^{-6}$	0	$2.9 \times 10^{-1}$
Ar-39*	$0.44 \times 10^0$	$1.2 \times 10^{-1}$	0	$0.56 \times 10^0$
Ar-41*	$1.7 \times 10^{-2}$	$3.4 \times 10^{-3}$	0	$2.0 \times 10^{-2}$
Ne-23*	$2.0 \times 10^0$	$6.6 \times 10^{-6}$	0	$2.0 \times 10^0$
H-3*,**	$9.5 \times 10^{-4}$	$2.8 \times 10^{-7}$	$6.2 \times 10^{-1}$	$6.2 \times 10^{-1}$
Total	$6.2 \times 10^0$	$0.17 \times 10^0$	$0.62 \times 10^0$	$7.0 \times 10^0$

\*Release rates independent of failed fuel fraction

\*\*BOP tritium release ( $2.5 \times 10^0$  Ci/yr) from TG Building exhaust not included

<sup>†</sup>0.1 percent failed fuel

++ Less than  $10^{-13}$

Ref.(1) AMENDMENT IV TABLE 3.5-8

第 2.2-21 表 気体状放射性物質の放出位置

放 出 源	流 量 (Sft <sup>3</sup> /min)	高 さ	放出速度	温 度
IB	50,000	857'	未 定	-**
RSB fuel handling area radwaste area	35,000	884'0"	未 定	65~120°F
RSB CAPS	3,000	884'0"	750ft/min	65~120°F
RSB RCB からの排気	未 定	未 定	未 定	未 定
SGB 3つのSG loop cell から	57,000	886'0"	2280ft/min	65~120°F
RCS*	415,000	RCS の頂上	-**	-**

\* Design Basis Accident 及び正常運転時にはこの点からの放出はない。CDA 等の  
大事故の場合にのみ使用される。

\*\* 記述なし

略 記

RSB Reactor Service Building  
 SGB Steam Generator Building  
 RCS Reactor Confinement Structures  
 RCB Reactor Containment Building  
 IB Intermediate Bay of SGB

第 2.2 - 2 2 表

DEPOSITION OF ACTIVATION, FISSION, FUEL AND CORROSION PRODUCTS  
IN SODIUM, ON WETTED SURFACES AND ON COLD TRAPS

Isotope	In Na	Percent Deposition	
		On Wetted Plant Surfaces *	In Cold Traps
Na <sup>24</sup>	100	0	0
Na <sup>22</sup>	100	0	0
Cs <sup>137</sup>	20	0	80
Cs <sup>136</sup>	95	0	5
Cs <sup>134</sup>	40	0	60
Sb <sup>125</sup>	10	0	90
I <sup>132</sup>	95	0	5
I <sup>131</sup>	95	0	5
Remaining Fission Prod.	10	100	10 (Except Ba <sup>140</sup> , La <sup>140</sup> , Te <sup>132-5</sup> )
H <sup>3</sup>	2	0	47% Primary, 51% Intermediate
Corrosion Products (Co, Fe, Mn, Cr, and Ta)	<1	100	10 (50 for Mn <sup>54</sup> )
*Pu	95	5	100

\*See Pu source discussion in Section 11.1.

Ref. (5) TABLE 1 2.1-7

第 2.2 - 2 3 表

ACTIVATION, FISSION PRODUCT AND PLUTONIUM ISOTOPE  
CONCENTRATIONS IN THE PRIMARY SODIUM COOLANT DURING  
30 YEAR PLANT LIFETIME - DESIGN VALUES

<u>Isotope</u>	<u>µci/gm<sup>*,†</sup> of Sodium</u>	<u>Percentage** of Isotope Inventory in Sodium Coolant</u>	<u>Source for Isotope</u>
Na <sup>24</sup>	2.94 x 10 <sup>4</sup>	100	Na Activation
Na <sup>22</sup>	1.52	100	Na Activation
Cs <sup>137</sup>	68.7	20	Failed Fuel- Fission Product Release
Cs <sup>136</sup>	16.62	95	Failed Fuel- Fission Product Release
Cs <sup>134</sup>	1.88	40	Failed Fuel- Fission Product Release
Sb <sup>125</sup>	0.401	10	Failed Fuel- Fission Product Release
I <sup>131</sup>	43.7	95	Failed Fuel- Fission Product Release
Te <sup>132</sup>	2.78	10	Failed Fuel- Fission Product Release
I <sup>132</sup>	27.8	95	Failed Fuel- Fission Product Release
Te <sup>129m</sup>	0.597	10	Failed Fuel- Fission Product Release
Te <sup>129</sup>	0.597	10	Failed Fuel- Fission Product Release
Sr <sup>89</sup>	0.090	10	Failed Fuel- Fission Product Release
Sr <sup>90</sup>	0.056	10	Failed Fuel- Fission Product Release
Y <sup>90</sup>	0.056	10	Failed Fuel- Fission Product Release
Y <sup>91</sup>	0.0258	10	Failed Fuel- Fission Product Release
Zr <sup>95</sup>	0.0481	10	Failed Fuel- Fission Product Release

第 2.2 - 2 3 表 (CONTINUED)

<u>Isotope</u>	<u><math>\mu\text{Ci/gm}^{*+}</math> of Sodium</u>	<u>Percentage** of Isotope Inventory in Sodium Coolant</u>	<u>Source for Isotope</u>
Nb <sup>95</sup>	0.0481	10	Failed Fuel- Fission Product Release
Ru <sup>103</sup>	0.0714	10	Failed Fuel- Fission Product Release
Ru <sup>106</sup>	0.0475	10	Failed Fuel- Fission Product Release
Rh <sup>106</sup>	0.0475	10	Failed Fuel- Fission Product Release
Ba <sup>140</sup>	0.054	10	Failed Fuel- Fission Product Release
La <sup>140</sup>	0.054	10	Failed Fuel- Fission Product Release
Ce <sup>141</sup>	0.064	10	Failed Fuel- Fission Product Release
Ce <sup>144</sup>	0.0377	10	Failed Fuel- Fission Product Release
Pr <sup>144</sup>	0.0377	10	Failed Fuel- Fission Product Release
Ce <sup>143</sup>	0.0451	10	Failed Fuel- Fission Product Release
Pr <sup>143</sup>	0.0451	10	Failed Fuel- Fission Product Release
Nd <sup>147</sup>	0.0211	10	Failed Fuel- Fission Product Release
Pm <sup>147</sup>	0.0213	10	Failed Fuel- Fission Product Release
Co <sup>60</sup>	$2.3 \times 10^{-3}$	<1	Activated Corrosion Product
Co <sup>58</sup>	$4.3 \times 10^{-3}$	<1	Activated Corrosion Product
Mn <sup>54</sup>	$1.7 \times 10^{-2}$	<1	Activated Corrosion Product
Pu <sup>238</sup>	$1.3 \times 10^{-2}$	95	Released Fuel

第 2.2 - 2 3 表 (CONTINUED)

<u>Isotope</u>	<u><math>\mu\text{ci/gm}^{*},+</math> of Sodium</u>	<u>Percentage** of Isotope Inventory in Sodium Coolant</u>	<u>Source for Isotope</u>
Pu <sup>239</sup>	$3.6 \times 10^{-3}$	95	Released Fuel
Pu <sup>240</sup>	$4.7 \times 10^{-3}$	95	Released Fuel
Pu <sup>241</sup>	0.394	95	Released Fuel
Pu <sup>242</sup>	$1.0 \times 10^{-5}$	95	Released Fuel
H <sup>3</sup>	1.86	~2	B and K Activation, Ternary Fission

\*The above concentrations are based on a primary sodium mass of  $7.1 \times 10^8$  grams.  
+ Zero decay time

\*\*Percentage based on isotopic solubility in sodium, cold trap efficiency for isotope and tendency for plating out.

Ref. (5) TABLE 1 1.1-7

第 2.2 - 2 4 表

SIGNIFICANT CORROSION, FISSION PRODUCT AND RELEASED  
FUEL ACTIVITIES ON WETTED SURFACES  
AT REACTOR SHUTDOWN

<u>Fission Products</u>	<u>Surface* Activity <math>\mu\text{ci}/\text{cm}^2</math></u>	<u>Corrosion Products</u>	<u>Surface Activity <math>\mu\text{ci}/\text{cm}^2</math></u>	<u>Released Fuel</u>	<u>Surface Activity <math>\mu\text{ci}/\text{cm}^2</math></u>
Sr <sup>89</sup>	7.35	Co <sup>60</sup>	11.2	Pu <sup>238</sup>	$8.53 \times 10^{-3}$
Sr <sup>90</sup>	4.6	Co <sup>58</sup>	7.7	Pu <sup>239</sup>	$1.89 \times 10^{-3}$
Y <sup>90</sup>	4.6	Mn <sup>54</sup>	11.6	Pu <sup>240</sup>	$2.46 \times 10^{-3}$
Y <sup>91</sup>	2.12	Fe <sup>59</sup>	0.065	Pu <sup>241</sup>	0.204
Zr <sup>95</sup>	3.94	Cr <sup>51</sup>	2.1	Pu <sup>242</sup>	$5.25 \times 10^{-6}$
Nb <sup>95</sup>	3.94	Ta <sup>182</sup>	1.4		
Mo <sup>99</sup>	4.82				
Ru <sup>103</sup>	5.61				
Ru <sup>106</sup>	3.88				
Rh <sup>106</sup>	3.88				
Ag <sup>111</sup>	0.32				
Te <sup>128</sup>	238				
Te <sup>129m</sup>	48.4				
Te <sup>129</sup>	48.4				
Ba <sup>140</sup>	4.42				
La <sup>140</sup>	4.42				
Ce <sup>141</sup>	5.23				
Ce <sup>143</sup>	3.70				
Pr <sup>143</sup>	3.70				
Ce <sup>144</sup>	3.10				
Pr <sup>144</sup>	3.10				
Nd <sup>147</sup>	1.74				
Pm <sup>147</sup>	1.74				
Eu <sup>155</sup>	0.17				

(第 2.2 - 2 3 表)

\*Some isotopes shown in Table 11.1-7 are soluble in sodium and are not considered as surface sources. A residual film of sodium on a drained component will remain and act as a residual source for these isotopes. Analysis to calculate doses include a source due to a 1 mil sodium film on components prior to cleaning.

Ref. (5) TABLE 1.1.1-8



第 2.2 - 2 5 表

EXPECTED ACTIVITY INVENTORY STORED AFTER PROCESSING\*

<u>Isotope</u>	<u>Half-Life</u>	<u>Low-Level Activity** Monitor Tank (Ci)</u>	<u>Intermediate Activity* Storage Tank (Ci)</u>
H-3	12.3 years	$2.22 \times 10^{-5}$	$4.8 \times 10^{-2}$
Na-22	2.6 years	$1.86 \times 10^{-10}$	$3.96 \times 10^{-7}$
Na-24	15 hours	$5.32 \times 10^{-11}$	$1.13 \times 10^{-7}$
Cr-51	28 days	--	$1.82 \times 10^{-5}$
Mn-54	312 days	$2.09 \times 10^{-12}$	$1.28 \times 10^{-4}$
Co-58	71 days	$5.30 \times 10^{-13}$	$7.87 \times 10^{-5}$
Fe-59	45 days	--	$6.32 \times 10^{-7}$
Co-60	5.2 years	$2.83 \times 10^{-13}$	$1.26 \times 10^{-4}$
Sr-89	51 days	$9.61 \times 10^{-13}$	$7.22 \times 10^{-6}$
Sr-90		$6.90 \times 10^{-13}$	$5.19 \times 10^{-6}$
Y-90		$6.90 \times 10^{-13}$	$5.19 \times 10^{-6}$
Y-91	58 days	$2.82 \times 10^{-13}$	$2.12 \times 10^{-6}$
Zr-95	65 days	$5.33 \times 10^{-13}$	$3.99 \times 10^{-6}$
Nb-95		$5.33 \times 10^{-13}$	$3.99 \times 10^{-6}$
Mo-99	67 hours	--	$4.51 \times 10^{-7}$
Ru-103	40 days	$7.39 \times 10^{-13}$	$5.54 \times 10^{-6}$
Ru-106	1 year	$5.74 \times 10^{-13}$	$4.30 \times 10^{-6}$
Rh-106		$5.74 \times 10^{-13}$	$4.30 \times 10^{-6}$

(Continued)

第 2.2 - 2 5 表 (Continued)

<u>Isotope</u>	<u>Half-Life</u>	<u>Low-Level Activity** Monitor Tank (Ci)</u>	<u>Intermediate Activity+ Storage Tank (Ci)</u>
Ag-111	7.5 days	--	$1.47 \times 10^{-7}$
Sb-125	2.7 years	$4.90 \times 10^{-12}$	$1.04 \times 10^{-8}$
Te-129m } ++	34 days	$6.00 \times 10^{-12}$	$4.43 \times 10^{-5}$
Te-129 }		$6.00 \times 10^{-12}$	$4.43 \times 10^{-5}$
I-131	8.1 days	$2.28 \times 10^{-10}$	$4.85 \times 10^{-7}$
Te-132 } ++	78 hours	$4.28 \times 10^{-12}$	$3.65 \times 10^{-5}$
I-132 }		$4.28 \times 10^{-12}$	$3.65 \times 10^{-5}$
Cs-134	2.1 years	$2.30 \times 10^{-11}$	$4.90 \times 10^{-8}$
Cs-136	13 days	$1.04 \times 10^{-10}$	$2.28 \times 10^{-7}$
Cs-137	30 years	$8.45 \times 10^{-10}$	$1.18 \times 10^{-6}$
Ba-140 } ++	12.8 days	$3.87 \times 10^{-13}$	$2.90 \times 10^{-6}$
La-140 }		$3.87 \times 10^{-13}$	$2.90 \times 10^{-6}$
Ce-141	32.5 days	$6.37 \times 10^{-13}$	$4.77 \times 10^{-6}$
Pr-143	13.7 days	$3.34 \times 10^{-13}$	$2.51 \times 10^{-6}$
Ce-144 } ++	285 days	$4.53 \times 10^{-13}$	$3.41 \times 10^{-6}$
Pr-144 }		$4.53 \times 10^{-13}$	$3.41 \times 10^{-6}$
Nd-147	11.1 days	$1.39 \times 10^{-13}$	$1.05 \times 10^{-6}$
Pm-147	2.7 days	$2.60 \times 10^{-13}$	$1.94 \times 10^{-6}$
Eu-155	1.8 years	--	$1.92 \times 10^{-7}$
Ta-182	115 days	--	$1.50 \times 10^{-5}$

(Continued)

第 2.2 - 2 5 表 (Continued)

<u>Isotope</u>	<u>Half-Life</u>	<u>Low-Level Activity** Monitor Tank (Ci)</u>	<u>Intermediate Activity+ Storage Tank (Ci)</u>
Pu-238	86 years	$8.00 \times 10^{-13}$	$5.02 \times 10^{-8}$
Pu-239	$2.0 \times 10^4$ years	$2.22 \times 10^{-13}$	$1.11 \times 10^{-8}$
Pu-240	$6.7 \times 10^3$ years	$2.90 \times 10^{-13}$	$1.45 \times 10^{-8}$
Pu-241	13 years	$2.42 \times 10^{-11}$	$1.22 \times 10^{-6}$
Pu-242	$3.8 \times 10^5$ years	$6.16 \times 10^{-15}$	$3.09 \times 10^{-11}$

\*0.1 percent failed fuel, 50 ppb Pu in sodium. 30-year irradiation, 10-day decay. Decay due to collection, processing and holdup is neglected.

\*\*Low activity based on Table 3.5-1, with DF =  $10^5$ , except tritium DF = 1, 2,500 gallon monitoring tank volume (第 2.2 - 9 表)

+ Intermediate Activity is based on a 40,000 gallon storage capacity containing 40 percent of all plated activity on processed components including 100 percent of all plated sodium adhering to processed components. A decontamination factor of  $10^5$  is applied to all isotopes except tritium (DF = 1).

++ Isotope pairs in secular equilibrium

Ref. (1) AMENDMENT IV TABLE 3.5-2

第 2.2 - 2 6 表

CONCENTRATION OF RADIONUCLIDES AT DISCHARGE TO  
CLINCH RIVER: EXPECTED VALUES

Isotope	Half-Life	Low-Level Activity* Concentration at the Discharge Point ( $\mu\text{Ci/cc}$ )	Intermediate Level Activity** Concentration at the Discharge Point ( $\mu\text{Ci/cc}$ )	Total Activity ( $\mu\text{Ci/cc}$ ) <sup>V</sup>
H-3 <sup>†</sup>	12.3 years	$9.12 \times 10^{-10}$	$1.59 \times 10^{-9}$	$2.52 \times 10^{-9}$
Na-22	2.6 years	$7.65 \times 10^{-15}$	$1.31 \times 10^{-14}$	$2.09 \times 10^{-14}$
Na-24	15 hours	$2.19 \times 10^{-16}$	$3.78 \times 10^{-15}$	$4.01 \times 10^{-15}$
Cr-51	28 days	--	$6.07 \times 10^{-13}$	$6.07 \times 10^{-13}$
Mn-54	312 days	$8.61 \times 10^{-17}$	$4.29 \times 10^{-12}$	$4.29 \times 10^{-12}$
Co-58	71 days	$2.18 \times 10^{-17}$	$2.63 \times 10^{-12}$	$2.63 \times 10^{-12}$
Fe-59	45 days	--	$2.11 \times 10^{-14}$	$2.11 \times 10^{-14}$
Co-60	5.2 years	$1.17 \times 10^{-17}$	$4.20 \times 10^{-12}$	$4.20 \times 10^{-12}$
Sr-89	51 days	$3.95 \times 10^{-17}$	$2.41 \times 10^{-13}$	$2.42 \times 10^{-13}$
Sr-90	28.8 years	$2.84 \times 10^{-17}$	$1.74 \times 10^{-13}$	$1.74 \times 10^{-13}$
Y-90	--	$2.84 \times 10^{-17}$	$1.74 \times 10^{-13}$	$1.74 \times 10^{-13}$
Y-91	58 days	$1.16 \times 10^{-17}$	$7.09 \times 10^{-14}$	$7.09 \times 10^{-14}$
Zr-95	65 days	$2.19 \times 10^{-17}$	$1.34 \times 10^{-13}$	$1.34 \times 10^{-13}$
Nb-95	--	$2.19 \times 10^{-17}$	$1.34 \times 10^{-13}$	$1.34 \times 10^{-13}$
Mo-99	67 hours	--	$1.51 \times 10^{-14}$	$1.51 \times 10^{-14}$
Ru-103	40 days	$3.04 \times 10^{-17}$	$1.85 \times 10^{-13}$	$1.85 \times 10^{-13}$
Ru-106	1 year	$2.36 \times 10^{-17}$	$1.44 \times 10^{-13}$	$1.44 \times 10^{-13}$
Rh-106	--	$2.36 \times 10^{-17}$	$1.44 \times 10^{-13}$	$1.44 \times 10^{-13}$
Ag-111	7.5 days	--	$4.90 \times 10^{-15}$	$4.90 \times 10^{-15}$
Sb-125	2.7 years	$2.02 \times 10^{-11}$	$3.49 \times 10^{-16}$	$5.52 \times 10^{-16}$
Te-129 <sup>m</sup>	34 days	$2.47 \times 10^{-16}$	$1.48 \times 10^{-12}$	$1.48 \times 10^{-12}$
Te-129	--	$2.47 \times 10^{-16}$	$1.48 \times 10^{-12}$	$1.48 \times 10^{-12}$
I-131	8.1 days	$9.37 \times 10^{-15}$	$1.62 \times 10^{-14}$	$2.57 \times 10^{-14}$
Te-132	78 hours	$1.76 \times 10^{-16}$	$1.22 \times 10^{-12}$	$1.22 \times 10^{-12}$
I-132	--	$1.76 \times 10^{-16}$	$1.22 \times 10^{-12}$	$1.22 \times 10^{-12}$

(Continued)

第 2.2 - 2 6 表 (Continued)

Isotope	Half-Life	Low-Level Activity* Concentration at the Discharge Point ( $\mu\text{Ci}/\text{cc}$ )	Intermediate Level Activity** Concentration at the Discharge Point ( $\mu\text{Ci}/\text{cc}$ )	Total Activity ( $\mu\text{Ci}/\text{cc}$ ) <sup>†</sup>
Cs-134	2.1 years	$9.47 \times 10^{-16}$	$1.64 \times 10^{-15}$	$2.57 \times 10^{-15}$
Cs-136	13 days	$4.26 \times 10^{-15}$	$7.37 \times 10^{-15}$	$1.17 \times 10^{-14}$
Cs-137	30 years	$3.48 \times 10^{-14}$	$3.95 \times 10^{-14}$	$7.46 \times 10^{-14}$
Ba-140	12.8 days	$1.57 \times 10^{-17}$	$9.70 \times 10^{-14}$	$9.70 \times 10^{-14}$
La-140	--	$1.59 \times 10^{-17}$	$9.70 \times 10^{-14}$	$9.70 \times 10^{-14}$
Ce-141	32.9 days	$2.62 \times 10^{-17}$	$1.60 \times 10^{-13}$	$1.60 \times 10^{-13}$
Pr-143	13.7 days	$1.37 \times 10^{-17}$	$8.38 \times 10^{-14}$	$8.38 \times 10^{-14}$
Ce-144	285 days	$1.66 \times 10^{-17}$	$1.14 \times 10^{-13}$	$1.14 \times 10^{-13}$
Pr-144	--	$1.66 \times 10^{-17}$	$1.14 \times 10^{-13}$	$1.14 \times 10^{-13}$
Nd-147	11.1 days	$5.73 \times 10^{-18}$	$3.51 \times 10^{-14}$	$3.51 \times 10^{-14}$
Pm-147	2.7 days	$1.07 \times 10^{-17}$	$6.49 \times 10^{-14}$	$6.49 \times 10^{-14}$
Eu-155	1.8 years	--	$6.41 \times 10^{-15}$	$6.41 \times 10^{-15}$
Ta-182	115 days	--	$5.02 \times 10^{-14}$	$5.02 \times 10^{-14}$
Pu-238	86 years	$3.29 \times 10^{-17}$	$1.68 \times 10^{-15}$	$1.71 \times 10^{-15}$
Pu-239	$2.0 \times 10^4$ years	$9.12 \times 10^{-18}$	$3.72 \times 10^{-16}$	$3.81 \times 10^{-16}$
Pu-240	$6.7 \times 10^3$ years	$1.20 \times 10^{-17}$	$4.84 \times 10^{-16}$	$4.96 \times 10^{-16}$
Pu-241	13 years	$1.00 \times 10^{-15}$	$4.08 \times 10^{-14}$	$4.18 \times 10^{-14}$
Pu-242	$3.8 \times 10^5$ years	$2.55 \times 10^{-20}$	$1.04 \times 10^{-18}$	$1.06 \times 10^{-18}$

\* Low Activity Liquid Waste System Assumptions

- 0.1 percent failed fuel, 50 ppb Pu in sodium, 30-year irradiation, 10 days decay. Decay times during collection, processing and holdup are neglected.
- 850 gal/day containing  $\sim 10^{-4}$   $\mu\text{Ci}/\text{cc}$  is decontaminated by a factor of  $10^5$  and released into the coolant water blowdown stream of  $3.0 \times 10^{12}$  cc/year.
- The activity level of  $10^{-6}$   $\mu\text{Ci}/\text{cc}$  comes from spillage of 3.5 pounds per year of primary sodium into the drainage stream of 850 gal/day.

\*\* Intermediate Activity Level Stream Assumptions

- 0.1 percent failed fuel, 50 ppb Pu in sodium, 30-year irradiation, 10 days decay. Decay times during collection, processing and holdup are neglected.
- 4,000 gal/year discharged into the coolant water blowdown stream after (DF) of  $10^5$ .
- 50 percent of the annual plated activity on the processed components is released into the annual decontaminating liquids. 100 percent of the annual plated sodium activity is released into the same volume.

† BOP discharge tritium concentration of  $1.5 \times 10^{-4}$   $\mu\text{Ci}/\text{cc}$  not included in table.

\*\* Isotope pairs in secular equilibrium

† Sum of columns 3 and 4

Ref. (1) AMENDMENT VII TABLE 3.5-3

第 2.2 - 2 7 表

ESTIMATED CLEANING PROCESS DATA - INTERMEDIATE LEVEL SYSTEM

Number of Components	Volume(1) Requirement Gallons (30 years)	Type of Process	Concentration ppm Na	Concentration* $\mu\text{Ci/cc}$
308 <sup>(2)</sup>	$1.1 \times 10^6$	1st rinse	282	1.84
294 <sup>(3)</sup>	674,000	1st rinse	300	$6 \times 10^{-5}$
14 <sup>(4)</sup>	436,000	1st rinse	244	3.7
14	436,000	Acid etch	18,000 <sup>+</sup>	1.84
4 <sup>(5)</sup>	160,000	1st rinse	592	20
1 <sup>(6)</sup>	40,000	1st rinse	2580	$1.6 \times 10^{-1}$
303 <sup>(7)</sup>	900,000	1st rinse	135	$4.6 \times 10^{-1}$

(1) Volumes for process described does not include subsequent rinses

(2) Total first rinses

(3) Total of non-acid etch first rinses

(4) Acid etch first rinses

(5) IHX

(6) IRP - Intermediate Rotating Plug

(7) Low sodium first rinses

\*1.0% failed fuel assumed, 30 year irradiation and 10 day cooling. First rinse removes 40% of total activity deposited and 100% of Na. Acid etch removes 20% of total activity deposited and 0% of Na.

<sup>+</sup>Neutralized 5%  $\text{HNO}_3$  with NaOH.

Ref. (5) AMENDMENT 6 TABLE 1 1.2-8

第 2.2 - 2 8 表

LIQUID RADWASTE RADIOISOTOPE ANNUAL INVENTORY - DESIGN VALUES

Isotope	Half-life <sup>++</sup>	Solidified, (Ci) <sup>(1)</sup>	Released, (Ci)	Intermediate Stored, (Ci)
H-3 <sup>+</sup>	12.3 Y	5.1136 E-03	7.5504 E-03	4.8000 E-02
Na-22	2.6 Y	4.1233 E-03	6.2624 E-08	3.9562 E-07
Na-24	15 H	1.1812 E-03	1.1978 E-08	1.1318 E-07
Cr-51	28 D	1.7896 E+00	1.8161 E-06	1.8161 E-05
Mn-54	312 D	1.2518 E+00	1.2815 E-05	1.2815 E-04
C. -58	71 D	7.7500 E-01	7.8736 E-06	7.8736 E-05
Fe-59	45 D	6.2150 E-03	6.3168 E-08	6.3168 E-07
Co-60	5.2 Y	1.2393 E+00	1.2566 E-05	1.2566 E-04
Sr-89	51 D	7.1145 E-00	7.2224 E-06	7.2210 E-05
* { Sr-90	28.8 Y	5.1105 E+00	5.1910 E-06	5.1900 E-05
Y-90		5.1105 E+00	5.1910 E-06	5.1900 E-05
Y-91	58 D	2.0592 E+00	2.1215 E-06	2.1212 E-05
* { Zr-95	65 D	3.9313 E+00	3.9834 E-06	3.9943 E-05
Nb-95		3.9313 E+00	3.9834 E-06	3.9943 E-05
Mo-99	67 D	4.4554 E-01	4.5120 E-07	4.5120 E-06
Ru-103	40 D	5.4663 E+00	5.5412 E-06	5.5401 E-05
* { Ru-106	1 Y	4.2308 E+00	4.2995 E-06	4.2989 E-05
Rh-106		4.2308 E+00	4.2995 E-06	4.2989 E-05
Ag-111	7.5 D	1.4452 E-01	1.4664 E-07	1.4664 E-06
Sb-125	2.7 Y	1.0863 E-02	1.6506 E-08	1.0427 E-07
* { Te-129M	34 D	4.3691 E+01	4.4323 E-05	4.4316 E-04
Te-129		4.3691 E+01	4.4323 E-05	4.4316 E-04
I-131	8.1 D	6.8923 E+00	7.6730 E-07	4.8470 E-06
* { Te-132	78 H	3.5998 E+01	3.6470 E-05	3.6464 E-04
I-132		3.6002 E+02	3.6470 E-05	3.6434 E-04
Cs-134	2.1 Y	5.1105 E-02	7.7558 E-08	4.8994 E-07
Cs-136	13 D	2.2988 E-01	3.4880 E-07	2.2034 E-06
Cs-137	30 Y	2.6645 E-00	2.2296 E-06	1.1818 E-05
* { Ba-140	12.8 D	2.8567 E-00	2.9003 E-06	2.8998 E-05
La-140		2.8567 E-00	2.9003 E-06	2.8998 E-05
Ce-141	32.5 D	4.7175 E-00	4.7734 E-06	4.7728 E-05
Pr-143	13.7 D	2.4673 E-00	2.5053 E-06	2.5049 E-05
* { Ce-144	285 D	3.3584 E-00	3.4080 E-06	3.4075 E-05
Pr-144		3.3584 E-00	3.4080 E-06	3.4075 E-05
Nd-147	11.1 D	1.0333 E-00	1.0495 E-06	1.0493 E-05
Pm-147	2.7 D	1.9132 E-00	1.9410 E-06	1.9407 E-05
Eu-155	1.8 Y	1.8907 E-01	1.9176 E-07	1.9176 E-06

(1) The solidified activity includes contributions from all rinses of the component cleaning process.

<sup>+</sup>Does not include BOP design release rate of 1.5Ci per day.

<sup>++</sup>Y = Years, D = Days, H = Hours

EX=10<sup>x</sup>

第 2.2 - 2 8 表 (Continued)

Isotope	Half-life <sup>++</sup>	Solidified, (Ci) <sup>(1)</sup>	Released, (Ci)	Intermediate Storec, (Ci)
Ta-182	115 D	1.4789 E-01	1.5002 E-05	1.5002 E-05
Pu-238	86 Y	9.9204 E-03	1.0245 E-08	1.0047 E-07
Pu-239	2E4 Y	2.1994 E-03	2.2812 E-09	2.2262 E-08
Pu-240	6.7E3 Y	2.8638 E-03	2.9698 E-09	2.8980 E-08
Pu-241	13 Y	2.4096 E-01	2.4980 E-07	2.4379 E-06
Pu-242	3.8E5 Y	6.1179 E-06	6.3366 E-12	6.1340 E-11

(1) The solidified activity includes contributions from all rinses of the component cleaning process.

+Does not include BOP design release rate of 1.5Ci per day.

<sup>++</sup>Y = Years, D = Days, H = Hours

EX=10<sup>x</sup>

Ref. (5) TABLE 1 1.2-6



第 2.2 - 2 9 表

PARAMETERS USED IN THE CALCULATION OF  
HYDROGEN-TRITIUM TRANSPORT IN CRBRP

Primary Circuit System Parameters

Total Weight of Sodium in Primary Circuit	1.7E + 6 lbs	3.35E + 7g mole Na
Temperature of Piping	950°F	783°K
Area of Primary Piping (Excluding IHX)	6,190 ft <sup>2</sup>	5.75E + 6 cm <sup>2</sup>
Thickness of Primary Piping	0.625 in.	1.59 cm
Total Cold Trap Flow Rate (based on 250°F)	60 gpm	151.7 g moles Na/sec
Minimum Cold Trap Temperature	250°F	394°K
Cold Trap Efficiency for Hydrogen Removal	70%	0.70
Hydrogen Flux to Primary Circuit (not including IHX)	0	0
Tritium Flux to Primary Circuit	89 Ci/day	0.0362 μgm at T/sec
Total Volume of Nitrogen in Primary Cells	698,000 ft <sup>3</sup>	7.74E + 5g mole N <sub>2</sub>
Exchange Rate of Nitrogen in Primary Cells	10%/day	0.996 g mole N <sub>2</sub> /sec

IHX Parameters

Log Mean Total Diffusional Area of IHX	43,270 ft <sup>2</sup>	4.02E + 7 cm <sup>2</sup>
Wall Thickness of IHX Tubing	0.047 in.	0.119 cm

第 2.2 - 2 9 表 (Continued)

IHX Parameters

Hydrogen and Tritium Diffusion Coefficient for IHX	---	$1.083E - 6 \text{ cm}^2/\text{sec}$
--	-----	--------------------------------------

Intermediate System Parameters

Total Weight of Sodium in Intermediate Circuit	$7.92E + 5 \text{ lbs}$	$1.56E + 7 \text{ g mole Na}$
Temperature of Piping	$900^\circ\text{F}$	$756^\circ\text{K}$
Area of Intermediate Piping (Excluding IHX)	$8,130 \text{ ft}^2$	$7.55E + 6 \text{ cm}^2$
Thickness of Intermediate Piping	$0.5 \text{ in.}$	$1.27 \text{ cm}$
Total Cold Trap Flow Rate (based on $250^\circ\text{F}$ )	$180 \text{ gpm}$	$455.1 \text{ g mole Na/sec}$
Minimum Cold Trap Temperature	$250^\circ\text{F}$	$394^\circ\text{K}$
Cold Trap Efficiency for Hydrogen Removal	$70\%$	$0.70$
Total Volume of Air in Intermediate Cells	$386,000 \text{ ft}^3$	$4.28E + 5 \text{ g mole air}$
Hydrogen Content in Intermediate Cell Air	$0.5 \text{ vppm}$	---
Exchange Rate of Air in Intermediate Cell	$1\%/\text{day}$	$0.049 \text{ g mole N}_2/\text{sec}$

Steam Generator Parameters

Total Inside Area	$40,630 \text{ ft}^2$	$3.78E + 7 \text{ cm}^2$
Total Outside Area	$61,740 \text{ ft}^2$	$5.74E + 7 \text{ cm}^2$

(Continued)

第 2.2 - 2 9 表 (Continued)

Steam Generator Parameters

Wall Thickness of Tube	0.109 in.	0.277 cm
Hydrogen Flux	1.92E - 11 lb H/sec-ft <sup>2</sup> inside tube area	354.6 μgm at. H/sec
Tritium-Diffusion Coefficient	---	1.384E - 6 cm <sup>2</sup> /sec

Ref.(1) AMENDMENT I TABLE 1... ITEM 010.6

第 2.2 - 3 0 表

HYDROGEN-TRITIUM TRANSPORT

Concentration Vector	Hydrogen		Tritium	
	$\mu\text{gm at H/mole}$	wppm	$\mu\text{gm at T/mole}^*$	$\mu\text{Ci T/gm Na}^*$
Sodium Side of Primary Piping (SS)	0.261	--	4.00E-4	--
Sodium Side of Intermediate Piping (SS)	0.483	--	2.60E-5	--
Nitrogen Side of Primary Piping (SS)	0.181	--	3.28E-4	--
Primary Sodium (Na)	0.979	0.043	1.50E-3	1.86
Sodium Side of Steam Generator Piping (SS)	0	--	1.30E-5	--
Air Side of Intermediate Piping (SS)	0.455	--	2.53E-5	--
Intermediate Sodium (Na)	1.952	0.085	1.05E-4	0.13
Primary Cell Atmosphere (N <sub>2</sub> )	7.87E-3	--	1.22E-4	--
Intermediate Cell Atmosphere (Air)	4.23E-2**	--	2.81E-5	--

(Continued)

第 2.2 - 3 0 表 (Continued)

Flux Vector	Hydrogen	Tritium	
	$\mu\text{gm at H/sec}$	$\mu\text{gm at T/sec}$	Ci/day
Through IHX	11.25	0.0189	46.5
To Primary Cold Trap	11.19	0.0171	42.1
To Primary Cell	6.09E-2	5.43E-5	0.13
By R/A Decay in Primary	--	8.73E-5	0.21
To (or From) Steam Generator	354.6	4.24E-4	1.04
To Intermediate Cold Trap	343.3	0.0185	45.5
To Intermediate Cell	0.0248	6.98E-7	0.0017
By R/A Decay in Intermediate	--	2.86E-6	0.0070

\*Mole sodium, stainless steel, nitrogen or air, as applicable

\*\*Including the 0.5 ppm nominal content

第 2.2 - 3 1 表

SUMMARY OF TRITIUM DISTRIBUTION CALCULATION

Pri. Q <sub>p</sub> <sup>ε</sup> <sub>p</sub> GPM	Inter. Q <sub>i</sub> <sup>ε</sup> <sub>i</sub> GPM	Tritium					Hydrogen					Tritium	
		CT <sub>p</sub> *	CT <sub>i</sub> *	J <sub>SG</sub> *	T <sub>c,p</sub> **	T <sub>c,i</sub> **	CT <sub>p</sub> *	CT <sub>i</sub> *	J <sub>IHX</sub> *	H <sub>c,p</sub> ***	H <sub>c,i</sub> ***	ε CT *	% CT
20	90	2.4E-2	2.3E-2	9.1E-4	196	19	20.5	411	20.6	0.056	0.116	4.7E-2	97.7
20	150	1.9E-2	2.8E-2	8.0E-4	229	17	12.2	419	12.3	0.049	0.086	4.7E-2	97.9
20	300	1.2E-2	3.4E-2	7.1E-4	278	15	5.8	425	5.9	0.043	0.062	4.7E-2	98.1
60	90	2.9E-2	1.8E-2	7.3E-4	157	16	24.6	406	24.6	0.045	0.115	4.7E-2	98.1
60	150	2.3E-2	2.4E-2	6.9E-4	198	15	14.7	416	14.8	0.042	0.086	4.7E-2	98.3
60	300	1.5E-2	3.2E-2	6.6E-4	258	14	7.0	424	7.1	0.042	0.062	4.7E-2	98.3
100	90	3.0E-2	1.7E-2	6.9E-4	148	15	25.6	405	25.7	0.043	0.115	4.7E-2	98.3
100	150	2.4E-2	2.3E-2	6.7E-4	191	14	15.3	416	15.4	0.041	0.086	4.7E-2	98.3
100	300	1.6E-2	3.1E-2	6.5E-4	252	14	7.3	424	7.4	0.039	0.063	4.7E-2	98.3
200	90	3.1E-2	1.6E-2	6.5E-4	140	14	26.4	405	26.5	0.040	0.115	4.7E-2	98.3
200	150	2.5E-2	2.2E-2	6.4E-4	184	14	15.8	415	15.9	0.039	0.085	4.7E-2	98.3
200	300	1.6E-2	3.1E-2	6.4E-4	248	14	7.6	424	7.6	0.039	0.062	4.7E-2	98.3
400	90	3.1E-2	1.6E-2	6.3E-4	136	13	26.8	404	26.9	0.039	0.115	4.7E-2	98.5
400	150	2.5E-2	2.2E-2	6.3E-4	181	13	16.1	415	16.2	0.039	0.085	4.7E-2	98.3
400	300	1.6E-2	3.0E-2	6.3E-4	246	13	7.7	423	7.7	0.038	0.062	4.7E-2	98.3

\*Flux in units of μgm atom/sec

\*\*Concentration in units of parts per million million, ppmm

\*\*\*Concentration in units of parts per million, ppm

Ref. (1) AMENDMENT I TABLE... ITEM 010.6

第2.2-32表 トリチウムの放出

漏洩位置	BOP		2次系	1次系
	コンデンサーオフガス	ブローダウン		
漏洩量	$1.08 \times 10^{-3} \text{ Ci/day}$	1.14 Ci/d	$1.7 \times 10^{-3} \text{ Ci/d}$	0.13 Ci/d
放出量	$1.08 \times 10^{-3} \text{ Ci/day}$	$1.5 \times 10^{-4} \mu\text{Ci/cc}$	$1.7 \times 10^{-3} \text{ Ci/d}$	$1.3 \times 10^{-4} \text{ Ci/d}$
放出位置	TGB 排気系	Clinch川	IB 排気系	RSB 排気系

第 2.2 - 3.3 表 Isotopical Released Activity on Accident Conditions \*1

Released Activity [Ci]

ISOTOPE	AC. 2-1	AC. 2-2 * (2)	AC. 3-1	AC. 3-2	AC. 3-3
H 3	5.10 x 10	9.50 x 10 <sup>-3</sup>	2.70 x 10 <sup>-4</sup>	1.08 x 10 <sup>-3</sup>	1.78 x 10 <sup>-4</sup>
NE 23	--	--	--	--	2.30 x 10 <sup>-1</sup>
NA 22	--	--	--	--	--
NA 24	--	--	--	--	--
AR 39	--	--	--	--	1.04 x 10
AR 41	--	--	--	--	6.69 x 10 <sup>-1</sup>
MN 54	--	--	--	--	--
CO 58	--	--	--	--	--
CO 60	--	--	--	--	--
KR 83M	--	--	--	--	1.20
KR 85M	--	--	--	--	8.97
KR 85	--	--	--	--	7.44 x 10 <sup>-1</sup>
KR 87	--	--	--	--	1.90
KR 88	--	--	--	--	9.40
SR 89	--	--	--	--	--
SR 90	--	--	--	--	--
Y 90	--	--	--	--	--
Y 91	--	--	--	--	--
ZR 95	--	--	--	--	--
NB 95	--	--	--	--	--
RU 103	--	--	--	--	--
RU 106	--	--	--	--	--
SB 125	--	--	--	--	--
TE 129M	--	--	--	--	--
TE 129	--	--	--	--	--
TE 132	--	--	--	--	--
I 130	--	--	--	--	--
I 131	--	--	--	--	--
I 132	--	--	--	--	--
I 133	--	--	--	--	--
I 135	--	--	--	--	--
XE 131M	--	--	--	--	2.44
XE 133M	--	--	--	--	6.10
XE 133	--	--	--	--	1.60 x 10 <sup>2</sup>
XE 135M	--	--	--	--	8.20 x 10 <sup>-2</sup>
XE 135	--	--	--	--	2.10 x 10 <sup>2</sup>
XE 138	--	--	--	--	1.10 x 10 <sup>-1</sup>
CS 134	--	--	--	--	--
CS 136	--	--	--	--	--
CS 137	--	--	--	--	--
BA 140	--	--	--	--	--
LA 140	--	--	--	--	--
CE 141	--	--	--	--	--
CE 143	--	--	--	--	--
CE 144	--	--	--	--	--
PR 143	--	--	--	--	--
PR 144	--	--	--	--	--
ND 147	--	--	--	--	--
PM 147	--	--	--	--	--
PU 238	--	--	--	--	--
PU 239	--	--	--	--	--
PU 240	--	--	--	--	--
PU 241	--	--	--	--	--
PU 242	--	--	--	--	--
AM 241	--	--	--	--	--
AM 243	--	--	--	--	--
CM 242	--	--	--	--	--
CM 244	--	--	--	--	--
MO 99	--	--	--	--	--



第 2.2 - 3.3 表 (Continued)

ISOTOPE	AC. 3-4	AC. 4-1	AC. 4-2	AC. 5-1	AC. 5-2
H 3	$7.00 \times 10^{-3}$	$1.29 \times 10^{-3}$	$2.42 \times 10^{-2}$	--	$6.10 \times 10^{-1}$
NE 23	$1.80 \times 10^{-1}$	--	--	--	--
NA 22	--	$2.39 \times 10^{-3}$	$2.07 \times 10^{-2}$	--	--
NA 24	--	$2.98 \times 10^{-4}$	$4.67 \times 10^{-1}$	--	--
AR 39	4.55	--	--	--	--
AR 41	$1.00 \times 10^{-3}$	--	--	--	--
MN 54	--	$1.17 \times 10^{-5}$	--	--	--
CO 58	--	$2.97 \times 10^{-6}$	--	--	--
CO 60	--	$1.59 \times 10^{-6}$	--	--	--
KR 83M	$2.40 \times 10^{-2}$	--	--	$4.99 \times 10^{-5}$	--
KR 85M	$1.82 \times 10^{-1}$	--	--	$2.07 \times 10^{-4}$	--
KR 85	$2.24 \times 10^{-1}$	--	--	$2.08 \times 10^{-5}$	--
KR 87	$3.80 \times 10^{-2}$	--	--	$9.94 \times 10^{-5}$	--
KR 88	$1.89 \times 10^{-1}$	--	--	$3.05 \times 10^{-4}$	--
SR 89	--	$2.76 \times 10^{-5}$	--	--	--
SR 90	--	$1.93 \times 10^{-5}$	--	--	--
Y 90	--	$1.93 \times 10^{-5}$	--	--	--
Y 91	--	$8.29 \times 10^{-6}$	--	--	--
ZR 95	--	$1.52 \times 10^{-5}$	--	--	--
NB 95	--	$1.52 \times 10^{-5}$	--	--	--
RU 103	--	$2.07 \times 10^{-5}$	--	--	--
RU 106	--	$1.59 \times 10^{-5}$	--	--	--
SB 125	--	$1.37 \times 10^{-4}$	--	--	--
TE 129M	--	$1.69 \times 10^{-4}$	--	--	--
TE 129	--	$1.69 \times 10^{-4}$	--	--	--
TE 132	--	$1.13 \times 10^{-4}$	--	--	--
I 130	--	--	--	--	--
I 131	--	$6.36 \times 10^{-3}$	$2.13 \times 10^{-2}$	--	--
I 132	--	$1.13 \times 10^{-3}$	--	--	--
I 133	--	--	--	--	--
I 135	--	--	--	--	--
XE 131M	$1.06 \times 10^{-1}$	--	--	$2.03 \times 10^{-6}$	--
XE 133M	$6.11 \times 10^{-1}$	--	--	$6.16 \times 10^{-5}$	--
XE 138	$2.58 \times 10$	--	--	$1.13 \times 10^{-3}$	--
XE 135M	$4.00 \times 10^{-3}$	--	--	$1.35 \times 10^{-5}$	--
XE 135	4.25	--	--	$3.61 \times 10^{-3}$	--
XE 138	$6.00 \times 10^{-3}$	--	--	$1.97 \times 10^{-5}$	--
CS 134	--	$6.43 \times 10^{-4}$	$6.04 \times 10^{-4}$	--	--
CS 136	--	$3.47 \times 10^{-3}$	$9.53 \times 10^{-3}$	--	--
CS 137	--	$2.38 \times 10^{-2}$	$6.07 \times 10^{-1}$	--	--
BA 140	--	$1.11 \times 10^{-5}$	--	--	--
LA 140	--	$1.11 \times 10^{-5}$	--	--	--
CE 141	--	$1.80 \times 10^{-5}$	--	--	--
CE 143	--	--	--	--	--
CE 144	--	$1.24 \times 10^{-5}$	--	--	--
PR 143	--	$9.67 \times 10^{-6}$	--	--	--
PR 144	--	$1.24 \times 10^{-5}$	--	--	--
ND 147	--	$4.15 \times 10^{-6}$	--	--	--
PM 147	--	$7.60 \times 10^{-6}$	--	--	--
PU 238	--	$4.49 \times 10^{-6}$	$1.27 \times 10^{-4}$	--	--
PU 239	--	$1.24 \times 10^{-6}$	$3.18 \times 10^{-5}$	--	--
PU 240	--	$1.66 \times 10^{-6}$	$4.45 \times 10^{-6}$	--	--
PU 241	--	$1.36 \times 10^{-4}$	$2.92 \times 10^{-3}$	--	--
PU 242	--	$3.45 \times 10^{-9}$	$9.53 \times 10^{-8}$	--	--
AM 241	--	--	--	--	--
AM 243	--	--	--	--	--
CM 242	--	--	--	--	--
CM 244	--	--	--	--	--
MO 99	--	--	--	--	--

第 2.2-3 表 (Continued)

ISOTOPE	AC. 6-1	AC. 6-2	AC. 6-3	AC. 7-1	AC. 8-1
H 3	$2.00 \times 10^{-12}$	$2.90 \times 10^{-12}$	$1.43 \times 10^{-6}$	--	$9.70 \times 10^{-5}$
NE 23	--	--	--	--	--
NA 22	--	--	--	--	$1.81 \times 10^{-4}$
NA 24	--	--	--	--	$2.25 \times 10^{-4}$
AR 39	$6.51 \times 10^{-10}$	$6.51 \times 10^{-10}$	$6.39 \times 10^{-4}$	--	--
AR 41	--	--	$1.52 \times 10^{-8}$	--	--
MN 54	--	--	--	--	$8.87 \times 10^{-7}$
CO 58	--	--	--	--	$2.24 \times 10^{-7}$
CO 60	--	--	--	--	$1.20 \times 10^{-7}$
KR 83M	--	--	$3.44 \times 10^{-6}$	--	--
KR 85M	$6.66 \times 10^{-11}$	$6.66 \times 10^{-9}$	$6.35 \times 10^{-3}$	--	--
KR 85	$1.24 \times 10^{-8}$	$1.24 \times 10^{-6}$	$7.65 \times 10^{-5}$	$3.80 \times 10$	--
KR 87	--	--	$5.00 \times 10^{-8}$	--	--
KR 88	$4.75 \times 10^{-16}$	$4.75 \times 10^{-14}$	$7.45 \times 10^{-4}$	--	--
SR 89	--	--	--	--	$2.09 \times 10^{-6}$
SR 90	--	--	--	--	$1.46 \times 10^{-6}$
Y 90	--	--	--	--	$1.46 \times 10^{-6}$
Y 91	--	--	--	--	$6.26 \times 10^{-7}$
ZR 95	--	--	--	--	$1.15 \times 10^{-6}$
NB 95	--	--	--	--	$1.15 \times 10^{-6}$
RU 103	--	--	--	--	$1.57 \times 10^{-6}$
RU 106	--	--	--	--	$1.20 \times 10^{-6}$
SB 125	--	--	--	--	$1.04 \times 10^{-5}$
TE 129M	--	--	--	--	$1.27 \times 10^{-5}$
TE 129	--	--	--	--	$1.27 \times 10^{-5}$
TE 132	--	--	--	--	$8.56 \times 10^{-6}$
I 130	$3.79 \times 10^{-10}$	$3.79 \times 10^{-8}$	--	--	--
I 131	$3.25 \times 10^{-6}$	$3.25 \times 10^{-4}$	--	--	$4.80 \times 10^{-4}$
I 132	$1.69 \times 10^{-6}$	$1.69 \times 10^{-4}$	--	--	$8.56 \times 10^{-5}$
I 133	$3.74 \times 10^{-7}$	$3.74 \times 10^{-5}$	--	--	--
I 135	$8.42 \times 10^{-10}$	$8.42 \times 10^{-8}$	--	--	--
XE 131M	$2.41 \times 10^{-8}$	$2.41 \times 10^{-6}$	$4.05 \times 10^{-3}$	$2.11 \times 10^{-1}$	--
XE 133M	$9.71 \times 10^{-8}$	$9.71 \times 10^{-6}$	$9.35 \times 10^{-2}$	$3.61 \times 10^{-11}$	--
XE 133	$5.12 \times 10^{-6}$	$5.12 \times 10^{-4}$	2.08	$4.05 \times 10^{-2}$	--
XE 135M	$3.81 \times 10^{-11}$	$3.81 \times 10^{-9}$	--	--	--
XE 135	$3.32 \times 10^{-8}$	$3.31 \times 10^{-6}$	1.06	--	--
XE 138	--	--	--	--	--
CS 134	--	--	--	--	$4.85 \times 10^{-6}$
CS 136	--	--	--	--	$2.62 \times 10^{-4}$
CS 137	--	--	--	--	$1.79 \times 10^{-3}$
BA 140	--	--	--	--	$8.35 \times 10^{-7}$
LA 140	--	--	--	--	$8.35 \times 10^{-7}$
CE 141	--	--	--	--	$1.36 \times 10^{-6}$
CE 143	--	--	--	--	--
CE 144	--	--	--	--	$9.39 \times 10^{-7}$
PR 143	--	--	--	--	$7.30 \times 10^{-7}$
PR 144	--	--	--	--	$9.39 \times 10^{-7}$
ND 147	--	--	--	--	$3.13 \times 10^{-7}$
PM 147	--	--	--	--	$5.74 \times 10^{-7}$
PU 238	--	--	--	--	$3.39 \times 10^{-7}$
PU 239	--	--	--	--	$9.39 \times 10^{-8}$
PU 240	--	--	--	--	$1.25 \times 10^{-7}$
PU 241	--	--	--	--	$1.03 \times 10^{-5}$
PU 242	--	--	--	--	$2.61 \times 10^{-10}$
AM 241	--	--	--	--	--
AM 243	--	--	--	--	--
CM 242	--	--	--	--	--
CM 244	--	--	--	--	--
MO 99	--	--	--	--	--

第 2. 2 - 3 3 表 (Continued)

ISOTOPE	AC. 8-2	AC. 8-3	AC. 8-4	AC. 8-5
H 3	$5.98 \times 10^{-6}$	$1.80 \times 10^{-4}$	$3.98 \times 10^{-6}$	$5.50 \times 10^{-6}$
NE 23	--	--	--	--
NA 22	$1.12 \times 10^{-5}$	$3.34 \times 10^{-4}$	$3.39 \times 10^{-5}$	--
NA 24	$9.46 \times 10^{-2}$	$4.17 \times 10^{-5}$	$7.67 \times 10^{-4}$	--
AR 39	--	--	--	--
AR 41	--	--	--	--
MN 54	$5.47 \times 10^{-8}$	$1.64 \times 10^{-6}$	--	--
CO 58	$1.38 \times 10^{-8}$	$4.15 \times 10^{-7}$	--	--
CO 60	$7.40 \times 10^{-9}$	$2.22 \times 10^{-7}$	--	--
KR 83M	--	--	--	--
KR 85M	--	--	--	--
KR 85	--	--	--	--
KR 87	--	--	--	--
KR 88	--	--	--	--
SR 89	$1.45 \times 10^{-7}$	$3.86 \times 10^{-6}$	--	--
SR 90	$9.01 \times 10^{-8}$	$2.70 \times 10^{-6}$	--	--
Y 90	$9.01 \times 10^{-8}$	$2.70 \times 10^{-6}$	--	--
Y 91	$4.18 \times 10^{-8}$	$1.16 \times 10^{-6}$	--	--
ZR 95	$7.72 \times 10^{-8}$	$2.12 \times 10^{-6}$	--	--
NB 95	$7.72 \times 10^{-8}$	$2.12 \times 10^{-6}$	--	--
RU 103	$1.16 \times 10^{-7}$	$2.90 \times 10^{-6}$	--	--
RU 106	$7.72 \times 10^{-8}$	$2.22 \times 10^{-6}$	--	--
SB 125	$6.47 \times 10^{-7}$	$1.92 \times 10^{-5}$	--	--
TE 129M	$9.62 \times 10^{-7}$	$2.36 \times 10^{-5}$	--	--
TE 129	$9.62 \times 10^{-7}$	$2.36 \times 10^{-5}$	--	--
TE 132	$4.47 \times 10^{-6}$	$1.58 \times 10^{-5}$	--	--
I 130	--	--	--	--
I 131	$7.05 \times 10^{-6}$	$8.88 \times 10^{-4}$	$3.50 \times 10^{-5}$	--
I 132	$4.47 \times 10^{-6}$	$1.58 \times 10^{-4}$	--	--
I 133	--	--	--	--
I 135	--	--	--	--
XE 131M	--	--	--	--
XE 133M	--	--	--	--
XE 133	--	--	--	--
XE 135M	--	--	--	--
XE 135	--	--	--	--
XE 138	--	--	--	--
CS 134	$3.02 \times 10^{-6}$	$8.98 \times 10^{-5}$	$9.91 \times 10^{-6}$	--
CS 136	$2.68 \times 10^{-5}$	$4.85 \times 10^{-4}$	$1.57 \times 10^{-5}$	--
CS 137	$1.11 \times 10^{-4}$	$3.32 \times 10^{-3}$	$9.97 \times 10^{-4}$	--
BA 140	$8.69 \times 10^{-8}$	$1.54 \times 10^{-6}$	--	--
LA 140	$8.69 \times 10^{-8}$	$1.54 \times 10^{-6}$	--	--
CE 141	$1.03 \times 10^{-7}$	$2.51 \times 10^{-6}$	--	--
CE 143	--	--	--	--
CE 144	$6.11 \times 10^{-8}$	$1.74 \times 10^{-6}$	--	--
PR 143	$7.40 \times 10^{-8}$	$1.35 \times 10^{-6}$	--	--
PR 144	$6.11 \times 10^{-8}$	$1.74 \times 10^{-6}$	--	--
ND 147	$3.54 \times 10^{-8}$	$5.79 \times 10^{-7}$	--	--
PM 147	$3.54 \times 10^{-8}$	$1.06 \times 10^{-6}$	--	--
PU 238	$2.09 \times 10^{-8}$	$6.27 \times 10^{-7}$	$2.09 \times 10^{-7}$	--
PU 239	$5.79 \times 10^{-9}$	$1.74 \times 10^{-7}$	$5.22 \times 10^{-8}$	--
PU 240	$7.72 \times 10^{-9}$	$2.32 \times 10^{-7}$	$7.30 \times 10^{-8}$	--
PU 241	$6.34 \times 10^{-7}$	$1.90 \times 10^{-6}$	$4.80 \times 10^{-6}$	--
PU 242	$1.61 \times 10^{-11}$	$4.83 \times 10^{-10}$	$1.57 \times 10^{-10}$	--
AM 241	--	--	--	--
AM 243	--	--	--	--
CM 242	--	--	--	--
CM 244	--	--	--	--
MO 99	--	--	--	--

\*1 0.5% of failed fuel is assumed during normal operation.

\*2 Tritium is released to Clinch River at  $9.5 \times 10^{-8}$  [Ci/min]

第 2.2-34 表 Summary of Source Terms on Accident Condition \*1

Accident Index Number	Release Point *2	RI Group	Total Release
2-1	1	Tritium	5.1 E 1
2-2	to Clinch River	Tritium	9.5 E-3 *3
3-1	5	Tritium	2.7 E-4
3-2	5	Tritium	1.1 E-3
3-3	5	Rare Gas	4.1 E 2
3-4	5a	Rare Gas	3.6 E 1
4-1	1	Sodium Fire	4.0 E-2
4-2	5	Sodium Fire	1.2 E 0
5-1	5,5a	Rare Gas	5.5 E-3
5-2	2/3/4 and 1	Tritium	6.1 E-1
6-1	5,5a	Rare Gas, Iodine	1.1 E-5
6-2	5,5a	Rare Gas, Iodine	1.1 E-3
6-3	5,5a	Rare Gas	3.3 E 0
7-1	5	Rare Gas	3.8 E 1
8-1	5a	Sodium Fire	3.2 E-3
8-2	5a	Sodium Fire	9.5 E-2
8-3	1	Sodium Fire	5.6 E-3
8-4	5,5a	Sodium Fire	1.9 E-3
8-5	1	Tritium	5.5 E 1

\* 1 0.5% of failed fuel is assumed during normal operation.

\* 2 Release point index numbers are shown in Ref[1]

Am.VIII, Fig.1 (Item 010.7). (第 2.2-11 图)

\* 3 Tritium is released to Clinch River at 9.5E-3 (Ci/min).

第 2.2 - 3 5 表

RELEASE OF RADIOACTIVITY FROM THE RAPS SURGE TANK CELL TO  
RSB FOLLOWING RAPS SURGE TANK RUPTURE

Isotope	Concentration RAPS Surge Tank Before Rupture (.Ci/cc)	Concentration In Cell After Tank Rupture (.Ci/cc)	Concentration In Cell After 20 Minutes Delay (.Ci/cc)	Out-leakage First 20 Minutes Following Tank Rupture (Curies)	Out-leakage 20 Minutes to 39 Minutes Following Tank Rupture (Curies)	Total Out-leakage To Cell Over Pressure (Curies)
H-3	$2.6 \times 10^{-4}$	$4.4 \times 10^{-5}$	$4.4 \times 10^{-5}$	$1.1 \times 10^{-4}$	$4.4 \times 10^{-5}$	$1.5 \times 10^{-4}$
He-23	$5.2 \times 10^{-1}$	$8.7 \times 10^{-2}$	$2.4 \times 10^{-11}$	$2.3 \times 10^{-1}$	$2.4 \times 10^{-11}$	$2.3 \times 10^{-1}$
Ar-39	$1.2 \times 10^{-1}$	$2.0 \times 10^{-2}$	$2.0 \times 10^{-2}$	$5.3 \times 10^{-2}$	$2.0 \times 10^{-2}$	$7.3 \times 10^{-2}$
Ar-41	$1.0 \times 10^{-1}$	$1.7 \times 10^{-2}$	$1.5 \times 10^{-2}$	$4.1 \times 10^{-2}$	$1.5 \times 10^{-2}$	$5.9 \times 10^{-2}$
Kr-83m	$2.1 \times 10^0$	$3.5 \times 10^{-1}$	$3.1 \times 10^{-1}$	$8.7 \times 10^{-1}$	$3.1 \times 10^{-1}$	$1.2 \times 10^0$
Kr-85m	$1.5 \times 10^1$	$2.5 \times 10^0$	$2.4 \times 10^0$	$6.2 \times 10^0$	$2.4 \times 10^0$	$8.6 \times 10^0$
Kr-85	$7.5 \times 10^{-3}$	$1.2 \times 10^{-3}$	$1.2 \times 10^{-3}$	$3.0 \times 10^{-3}$	$1.2 \times 10^{-3}$	$4.2 \times 10^{-3}$
Kr-87	$3.3 \times 10^0$	$5.6 \times 10^{-1}$	$4.7 \times 10^{-1}$	$1.4 \times 10^0$	$4.7 \times 10^{-1}$	$1.9 \times 10^0$
Kr-88	$1.6 \times 10^1$	$2.7 \times 10^0$	$2.5 \times 10^0$	$6.9 \times 10^0$	$2.5 \times 10^0$	$9.4 \times 10^0$
Xe-131m	$4.1 \times 10^{-1}$	$6.8 \times 10^{-2}$	$6.8 \times 10^{-2}$	$1.7 \times 10^{-1}$	$6.7 \times 10^{-2}$	$2.4 \times 10^{-1}$
Xe-133m	$1.1 \times 10^1$	$1.7 \times 10^0$	$1.7 \times 10^0$	$4.4 \times 10^0$	$1.7 \times 10^0$	$6.1 \times 10^0$
Xe-133	$2.2 \times 10^2$	$3.8 \times 10^1$	$3.8 \times 10^1$	$9.4 \times 10^1$	$3.8 \times 10^1$	$1.3 \times 10^2$
Xe-135m	$1.7 \times 10^{-1}$	$2.8 \times 10^{-2}$	$1.2 \times 10^{-2}$	$7.0 \times 10^{-2}$	$1.2 \times 10^{-2}$	$8.2 \times 10^{-2}$
Xe-135	$3.7 \times 10^2$	$6.4 \times 10^1$	$6.2 \times 10^1$	$1.6 \times 10^2$	$6.1 \times 10^1$	$2.1 \times 10^2$
Xe-138	$2.3 \times 10^{-1}$	$4.0 \times 10^{-2}$	$1.5 \times 10^{-2}$	$9.9 \times 10^{-2}$	$1.5 \times 10^{-2}$	$1.1 \times 10^{-1}$
Total				$2.7 \times 10^2$	$1.1 \times 10^2$	$3.7 \times 10^2$

Ref. (1) AMENDMENT IV TABLE 7.1-14

第 2.2 - 3 6 表

CLEANUP OF RADIOACTIVE GAS FROM RAPS SURGE TANK CELL  
FOLLOWING RAPS SURGE TANK RUPTURE

Isotope	Inventory in RAPS Surge Tank Before Rupture (Curies)	Radioactivity After 500 Minutes Delay (Curies)	Radioactivity As Released From RAPS (Curies)
H-3	$2.0 \times 10^{-2}$	$2.0 \times 10^{-2}$	$2.5 \times 10^{-5}$
Ne-23	$4.0 \times 10^1$	$<1.0 \times 10^{-20}$	$<1.0 \times 10^{-20}$
Ar-39	$8.9 \times 10^0$	$8.9 \times 10^0$	$8.9 \times 10^0$
Ar-41	$7.7 \times 10^0$	$3.3 \times 10^{-1}$	$1.3 \times 10^{-1}$
Kr-83m	$1.6 \times 10^2$	$7.8 \times 10^0$	$1.1 \times 10^{-7}$
Kr-85m	$1.1 \times 10^3$	$3.0 \times 10^2$	$1.6 \times 10^{-1}$
Kr-85	$5.8 \times 10^{-1}$	$5.8 \times 10^{-1}$	$5.8 \times 10^{-1}$
Kr-87	$2.5 \times 10^2$	$2.6 \times 10^0$	$1.1 \times 10^{-11}$
Kr-88	$1.2 \times 10^3$	$1.6 \times 10^2$	$1.1 \times 10^{-3}$
Xe-131m	$3.1 \times 10^1$	$3.0 \times 10^1$	$1.7 \times 10^0$
Xe-133m	$8.2 \times 10^2$	$7.4 \times 10^2$	$1.7 \times 10^{-4}$
Xe-133	$1.7 \times 10^4$	$1.6 \times 10^4$	$2.3 \times 10^1$
Xe-135m	$1.3 \times 10^1$	$3.3 \times 10^{-9}$	0
Xe-135	$2.8 \times 10^4$	$1.5 \times 10^4$	0
Xe-138	$1.7 \times 10^1$	$4.5 \times 10^{-10}$	0
Total	$4.8 \times 10^4$	$3.2 \times 10^4$	$3.4 \times 10^1$

Ref. (1) AMENDMENT VII TABLE 7.1-15

第 2.2 - 3 7 表

CLEANUP OF RADIOACTIVE REACTOR COVER GAS IN CAPS  
FOLLOWING RAPS SURGE TANK RUPTURE

Isotope	Inventory In Reactor At Shutdown (Curies)	Radioactivity After 500 Minutes Delay (Curies)	Radioactivity As Released From CAPS (Curies)
H-3	$3.4 \times 10^{-3}$	$3.4 \times 10^{-3}$	$3.4 \times 10^{-6}$
Ne-23	$8.9 \times 10^5$	$<1.0 \times 10^{-20}$	$<1.0 \times 10^{-20}$
Ar-39	$1.4 \times 10^0$	$1.4 \times 10^0$	$1.4 \times 10^0$
Ar-41	$2.7 \times 10^1$	$1.2 \times 10^0$	$4.8 \times 10^{-1}$
Kr-83m	$5.5 \times 10^2$	$2.5 \times 10^1$	$3.9 \times 10^{-7}$
Kr-85m	$1.5 \times 10^3$	$4.0 \times 10^2$	$2.1 \times 10^{-1}$
Kr-85	$1.6 \times 10^{-1}$	$1.6 \times 10^{-1}$	$1.6 \times 10^{-1}$
Kr-87	$1.4 \times 10^3$	$1.4 \times 10^1$	$6.0 \times 10^{-11}$
Kr-88	$2.7 \times 10^3$	$3.3 \times 10^2$	$2.2 \times 10^{-3}$
Xe-131m	$9.2 \times 10^0$	$9.0 \times 10^0$	$5.0 \times 10^{-1}$
Xe-133m	$2.9 \times 10^2$	$2.5 \times 10^2$	$5.8 \times 10^{-5}$
Xe-133	$5.2 \times 10^3$	$4.8 \times 10^3$	$7.2 \times 10^0$
Xe-135m	$6.9 \times 10^2$	$1.9 \times 10^{-7}$	0
Xe-135	$2.1 \times 10^4$	$1.1 \times 10^4$	0
Xe-138	$1.1 \times 10^3$	$2.8 \times 10^{-8}$	0
Total	$9.2 \times 10^5$	$1.6 \times 10^4$	$1.0 \times 10^1$

Ref.(1) AMENDMENT VIII TABLE 7.1-16

第 2.2 - 3 8 表

RADIOACTIVITY RELEASE FOLLOWING POSTULATED COVER GAS  
EQUALIZATION LINE RUPTURE (CURIES)

<u>Isotope</u>	(1) <u>Inventory In Reactor Cover Gas</u>	(2) <u>Inventory In Overflow Vessel Cover Gas</u>	(3) <u>Inventory In Primary Pumps Cover Gas</u>	(4) <u>Total Primary System Inventory</u>	(5) <u>Total Activity Released To Environment</u>
Xe-131m	9.2	10.5	*	19.7	0.106
Xe-133m	292	301	*	593	0.611
Xe-133	5,000	5,750	*	10,750	25.82
Xe-135m	690	27.6	*	718	0.004
Xe-135	10,575	13,700	*	24,275	4.25
Xe-138	1,115	40.5	*	1,156	0.006
Kr-83m	545	127	*	672	0.024
Kr-85m	1,515	662	*	2,177	0.182
Kr-85	0.16	0.19	$9.3 \times 10^{-6}$	0.35	0.224
Kr-87	1,355	233	*	1,588	0.038
Kr-88	2,655	852	*	3,507	0.189
Ar-39	1.36	3.18	0.11	4.65	4.55
Ar-41	26.6	6.18	$3.9 \times 10^{-4}$	32.78	0.001
Ne-23	$8.98 \times 10^5$	1,497	*	$8.99 \times 10^5$	0.180
H-3	0.003	0.007	0.0002	0.0102	0.007

\*Less than  $10^{-13}$ . Based on continuous operation with 0.5% failed fuel.



## 第 2.2 - 3 9 表

## RADIOACTIVE CONTENT OF PRIMARY SODIUM COOLANT\*

<u>Isotope</u>	<u><math>\mu\text{Ci/gm}</math></u>	
	<u>0</u>	<u>10</u>
H-3	1.86	1.86
Na-22	3.49	3.46
Na-24	29400.	0.432
Mn-54	0.017	0.017
Co-58	0.0043	0.0043
Co-60	0.0023	0.0023
Sr-89	0.045	0.040
Sr-90	0.028	0.028
Y-90	0.028	0.028
Y-91	0.013	0.012
Zr-95	0.024	0.022
Nb-95	0.024	0.022
Ru-103	0.036	0.030
Ru-106	0.024	0.023
Sb-125	0.201	0.199
Te-129m	0.299	0.244
Te-129	0.299	0.244
Te-132	1.39	.164
I-131	21.9	9.20
I-132	13.9	1.64
Cs-134	0.94	0.93
Cs-136	8.32	5.02
Cs-137	34.4	34.4
Ba-140	0.027	0.016
La-140	0.027	0.016
Ce-141	0.032	0.026
Ce-144	0.019	0.018
Pr-143	0.023	0.014

第 2.2 - 3 9 表 (Continued)

<u>Isotope</u>	<u>μCi/gm</u> <u>Days After Shutdown</u>	
	<u>0</u>	<u>10</u>
Pr-144	0.019	0.018
Nd-147	0.011	0.006
Pm-147	0.011	0.011
Pu-238	0.0065	0.0065
Pu-239	0.0018	0.0018
Pu-240	0.0024	0.0024
Pu-241	0.197	0.197
Pu-242	$5.0 \times 10^{-6}$	$5.0 \times 10^{-6}$

---

\* 30 years of plant operation, 0.5 percent failed fuel

Ref. (1) AMENDMENT VII TABLE 7.1-18

第 2.2 - 4 0 表

RADIOACTIVE CONTENT OF EVST SODIUM\*

<u>Isotope</u>	<u>Sodium (<math>\mu\text{Ci/g}</math>)</u>
H-3	0.763
Na-22	0.65
Na-24	14.7
I-131	$6.7 \times 10^{-1}$
Cs-134	0.19
Cs-136	0.30
Cs-137	19.1
Pu-238	$4.0 \times 10^{-3}$
Pu-239	$1.0 \times 10^{-3}$
Pu-240	$1.4 \times 10^{-3}$
Pu-241	$9.2 \times 10^{-2}$
Pu-242	$3.0 \times 10^{-6}$

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\*30 years plant operation, 0.5 percent failed fuel, maximum value during refueling

Ref.(1) AMENDMENT VII TABLE 7.1-19

第 2.2 - 4 1 表

FUEL ASSEMBLY NOBLE GAS AND IODINE INVENTORIES 87 HOURS  
AFTER SHUTDOWN

<u>Isotope</u>	<u>Inventory (Curies)</u>	<u>Half-Life</u>
Kr-83m	$1.08 \times 10^{-10}$	1.86 hr
Kr-85m	$2.88 \times 10^{-2}$	4.4 hr
Kr-85	$4.30 \times 10^2$	10.76 yr
Kr-87	$9.74 \times 10^{-17}$	76 min
Kr-88	$2.35 \times 10^{-5}$	2.8 hr
I-130	$1.15 \times 10^1$	12.6 hr
I-131	$9.16 \times 10^4$	8.1 d
I-132	$7.13 \times 10^4$	2.4 hr
I-133	$1.10 \times 10^4$	20.3 hr
I-135	$2.75 \times 10^1$	6.68 hr
Xe-131m	$6.74 \times 10^2$	11.8 d
Xe-133m	$2.76 \times 10^3$	2.26 d
Xe-133	$1.44 \times 10^5$	5.27 d
Xe-135m	$8.58 \times 10^0$	15.7 min
Xe-135	$1.04 \times 10^3$	9.14 hr

Ref. (1) AMENDMENT IV TABLE 7.1-20

第 2.2 - 4 2 表

EVTM GAS ACTIVITY 87 HOURS AFTER SHUTDOWN

<u>Isotope</u>	<u>1% Release From Fuel Assembly (<math>\mu\text{Ci}/\text{cc}</math>)</u>	<u>100% Release From Fuel Assembly (<math>\mu\text{Ci}/\text{cc}</math>)</u>
H-3	$1.39 \times 10^{-4}$	$1.39 \times 10^{-4}$
Ar-39	$1.45 \times 10^{-1}$	$1.45 \times 10^{-1}$
Kr-85m	$1.45 \times 10^{-4}$	$1.45 \times 10^{-2}$
Kr-85	$2.16 \times 10^0$	$2.16 \times 10^2$
Kr-88	$1.18 \times 10^{-7}$	$1.18 \times 10^{-5}$
I-130	$5.79 \times 10^{-2}$	$5.79 \times 10^0$
I-131	$4.61 \times 10^2$	$4.61 \times 10^4$
I-132	$3.59 \times 10^2$	$3.59 \times 10^4$
I-133	$5.54 \times 10^1$	$5.54 \times 10^3$
I-135	$1.38 \times 10^{-1}$	$1.38 \times 10^1$
Xe-131m	$3.39 \times 10^0$	$3.39 \times 10^2$
Xe-133m	$1.39 \times 10^1$	$1.39 \times 10^3$
Xe-133	$7.25 \times 10^2$	$7.25 \times 10^4$
Xe-135m	$4.32 \times 10^{-2}$	$4.32 \times 10^0$
Xe-135	$5.24 \times 10^0$	$5.24 \times 10^2$
Total	$1.63 \times 10^3$	$1.63 \times 10^5$

Ref.(1) AMENDMENT IV TABLE 7.1-2.1

第 2.2 - 4 3 表

INITIAL LEAKAGE RATE THROUGH EVTM SEALS TO RCB/RSB ATMOSPHERE  
87 HOURS AFTER SHUTDOWN

<u>Isotope</u>	<u>1% Release From Fuel Assembly (<math>\mu\text{Ci}/\text{sec}</math>)</u>	<u>100% Release From Fuel Assembly (<math>\mu\text{Ci}/\text{sec}</math>)</u>
H-3	$9.48 \times 10^{-7}$	$9.48 \times 10^{-7}$
Ar-39	$2.13 \times 10^{-4}$	$2.13 \times 10^{-4}$
Kr-85m	$2.75 \times 10^{-7}$	$2.75 \times 10^{-5}$
Kr-85	$4.06 \times 10^{-3}$	$4.06 \times 10^{-1}$
Kr-88	$2.22 \times 10^{-10}$	$2.22 \times 10^{-8}$
I-130	$1.35 \times 10^{-4}$	$1.35 \times 10^{-2}$
I-131	$1.07 \times 10^0$	$1.07 \times 10^2$
I-132	$8.36 \times 10^{-1}$	$8.36 \times 10^1$
I-133	$1.29 \times 10^{-1}$	$1.29 \times 10^1$
I-135	$3.22 \times 10^{-4}$	$3.22 \times 10^{-2}$
Xe-131m	$7.90 \times 10^{-3}$	$7.90 \times 10^{-1}$
Xe-133m	$3.24 \times 10^{-2}$	$3.24 \times 10^0$
Xe-133	$1.69 \times 10^0$	$1.69 \times 10^2$
Xe-135m	$1.01 \times 10^{-4}$	$1.01 \times 10^{-2}$
Xe-135	$1.22 \times 10^{-2}$	$1.22 \times 10^0$
<b>Total</b>	<b><math>3.78 \times 10^0</math></b>	<b><math>3.78 \times 10^2</math></b>

Ref. (1) AMENDMENT VII TABLE 7.1-2.2

第 2.2 - 4 4 表

REACTOR COVER GAS INVENTORY 30 HOURS AFTER SHUTDOWN

<u>Isotope</u>	<u>Inventory (Curies)</u>
H-3	$1.43 \times 10^{-6}$
Ar-39	$6.39 \times 10^{-4}$
Ar-41	$1.52 \times 10^{-8}$
Kr-83m	$3.44 \times 10^{-6}$
Kr-85m	$6.35 \times 10^{-3}$
Kr-85	$7.65 \times 10^{-5}$
Kr-87	$5.00 \times 10^{-8}$
Kr-88	$7.45 \times 10^{-4}$
Xe-131m	$4.05 \times 10^{-3}$
Xe-133m	$9.35 \times 10^{-2}$
Xe-133	2.08
Xe-135m	0
Xe-135	1.06
Xe-138	0
<b>Total</b>	<b>3.25</b>

Ref. (1) AMENDMENT IV TABLE 7.1-23

第 2.3 - 1 表

## ACCLIMATION AND LETHAL TEMPERATURES OF SELECTED CLINCH RIVER FISH

<u>Genus and Species</u>	<u>Common Name</u>	<u>Acclimation Temperature</u>		<u>Lethal Temperature</u>		<u>Reference Number</u>
		<u>°F</u>	<u>(°C)</u>	<u>°F</u>	<u>(°C)</u>	
<u>Lepomis macrochirus</u>	Bluegill	45	(7.2)	89	(31.7)	26
		52	(11.1)	95	(35.0)	26
		59	(15.0)	*87.8	(31.0)	27
		70	(21.1)	101.5	(38.6)	26
		76	(24.4)	97-99	(36.1-37.2)	26
		79	(26.1)	103	(39.4)	28
		86	(30.0)	*93.2	(34.0)	27
<u>Cyprinus carpio</u>	Carp	68	(20.0)	87.8-93.2	(31.0-34.0)	29
		78.8	(26.0)	96.3	(35.7)	29
<u>Ictalurus punctatus</u>	Channel catfish	45	(7.2)	91	(32.8)	26
		52	(10.0)	95	(35.0)	26
		71.6	(22.0)	95	(35.0)	30
		86	(30.0)	>95	(>35.0)	30
<u>Dorosoma cepedianum</u>	Gizzard shad	77	(25.0)	94	(34.3)	31
		77	(25.0)	*95	(35.0)	27
		86	(30.0)	96.6	(35.9)	31
		95	(35.0)	98.6	(37.0)	27
<u>Micropterus salmoides</u>	Largemouth bass	45	(7.2)	87	(30.6)	26
		52	(11.1)	95	(35.0)	26
		68	(20.0)	90.5	(32.5)	31
		77	(25.0)	99	(37.2)	28
		77	(25.0)	94.1	(34.5)	31
		80	(26.7)	100-102	(37.8-38.9)	28
		86	(30.0)	97.5	(36.4)	31

\*Lethal temperature refers to the temperature at which mortality was first observed. Other lethal temperatures are reported as LD<sub>50</sub> - temperature which is lethal to 50 percent of a test group of organisms. Duration of temperature trials for LD<sub>50</sub> values varied from 10-43 hours.



第 2.3 - 2 表

## SPAWNING TEMPERATURES OF SELECTED CLINCH RIVER FISH

<u>Genus and Species</u>	<u>Common Name</u>	<u>Spawning Temperatures</u>	<u>Reference Number</u>
<u>Lepomis macrochirus</u>	Bluegill	80°F (26.7°C)	34
<u>Cyprinus carpio</u>	Carp	60-68°F (15.6 - 20°C) 59°F (15°C)	35 36
<u>Ictalms punctatus</u>	Channel catfish	70-85°F (21.1 - 29.4°C)	35
<u>Dorosoma cepedianum</u>	Gizzard shad	73.4 -84.2°F (23 - 29°C)	37
<u>Micropterus salmoides</u>	Largemouth bass	60.7°F (15.9°C)	36
<u>Percina caprodes</u>	Logperch	71.6 - 80.6°F (22 - 27°C)	36
<u>Ictiobus bubalus</u>	Smallmouth buffalo	57.2 - 69.8°F (14.21°C)	38
<u>Dorosoma petenense</u>	Threadfin shad	62.6°F (17°C)	39

Ref. (1) AMENDMENT II Table 5.1-8

第 2.3 - 3 表

MEAN LENGTH OF VISIBLE PLUME\* FOR CRBRP COOLING TOWER\*\*

Stability Class	Relative Humidity (percent)			
	100	95	85	75
A	1.6	0.6	0.4	0.2
B	3.4	1.1	0.8	0.7
C	5.1	1.8	1.3	0.9
D	6.0	3.7	2.9	2.2
E	8.3	5.5	5.0	4.1
F	10.3	8.0	6.9	6.4

\*Plume length in miles

\*\*From following Table

Ref. (1) AMENDMENT II Table 5.1-14

MEAN LENGTH OF VISIBLE PLUME FOR VARIOUS COOLING SYSTEMS  
AND STABILITY CLASSES

	Stability Class	No. of Ground Fog and Icing Hours		Mean Length of Visible Plume, (m) For Relative Humidities			
		100% Rel. Hum.	Severe Fog	100%	95%	85%	75%
Natural Draft Wet Cooling Tower	A	--	--	9,871	2,550	1,800	1,200
	B	--	--	11,228	2,775	2,475	1,830
	C	--	--	13,201	4,700	3,150	2,100
	D	--	--	19,220	10,500	4,600	3,150
	E	--	--	23,061	13,650	10,800	7,350
	F	--	--	27,617	18,018	15,660	11,172
Mechanical Draft Wet Cooling Tower, Linear Array	A	99.35	91.57	2,550	950	600	400
	B	8.80	--	5,500	1,783	1,250	1,100
	C	38.27	--	8,200	2,900	2,100	1,450
	D	--	--	9,600	6,000	4,600	3,600
	E	--	--	13,400	8,800	8,000	6,600
	F	--	--	16,500	12,800	11,100	10,233
Mechanical Draft Wet Cooling Tower, Circular Array	A	99.35	74.81	3,600	1,000	700	500
	B	8.80	--	7,000	1,850	1,450	1,200
	C	38.27	--	9,000	3,100	2,300	1,600
	D	--	--	10,400	7,000	5,000	3,800
	E	--	--	13,500	9,000	8,300	6,900
	F	--	--	16,600	13,000	11,300	10,467
Mechanical Draft Wet/Dry Cooling Tower, 30% Plume Severity	A	99.35	--	2,000	700	500	300
	B	8.54	--	5,000	1,650	1,050	700
	C	29.69	--	7,700	2,400	1,750	1,200
	D	--	--	8,400	5,100	3,100	2,775
	E	--	--	9,600	7,350	6,300	5,325
	F	--	--	10,400	9,275	8,700	8,075
Mechanical Draft Wet/Dry Cooling Tower, 0% Plume Severity	A	99.35	--	2,200	825	650	400
	B	8.54	--	5,150	1,700	1,225	850
	C	29.69	--	7,975	2,600	2,075	1,425
	D	--	--	8,750	5,275	3,500	2,950
	E	--	--	10,250	7,525	6,700	5,400
	F	--	--	11,300	10,300	9,350	8,400

第 2.3 - 4 表

GROUND FOG POTENTIAL FOR CRBRP COOLING TOWER

<u>Horizontal Visibility Through Fog (miles)</u>	<u>Ground Fog (hrs/yr)*</u>
<1/2	146
<1/4	145
<1/10	100

\*Ground fog values from following table

Ref.(1) AMENDMENT II Table 5.1-15

POTENTIAL GROUND FOGGING FOR MECHANICAL DRAFT WET COOLING TOWER, LINEAR ARRAY

	Ground Interception		Max. Intensity		Minimum Horiz. Visibility		Hours of Temp. at 100% R.H.	Hours of Ground Fog or Icing			
	Begin (m)	End (m)	Distance (m)	Density (g/m <sup>3</sup> )	Feet	Miles		Horiz. Visibility 1/2 Mile or Less	Horiz. Visibility 1/4 Mile or Less	Horiz. Visibility 1/10 Mile or Less	
10°F	A	700	2,000	800	0.14	718	0.14	8.77	1.53	1.53	--
	B	2,200	4,200	3,200	0.08	1,017	0.19	8.77	0.14	0.14	--
	C	--	--	--	--	--	--	--	--	--	--
	D	--	--	--	--	--	--	--	--	--	--
	E	--	--	--	--	--	--	--	--	--	--
	F	--	--	--	--	--	--	--	--	--	--
20°F	A	700	1,900	800	0.15	685	0.13	7.88	1.37	1.37	--
	B	2,100	4,000	2,400	0.09	933	0.18	7.88	0.12	0.12	--
	C	--	--	--	--	--	--	--	--	--	--
	D	--	--	--	--	--	--	--	--	--	--
	E	--	--	--	--	--	--	--	--	--	--
	F	--	--	--	--	--	--	--	--	--	--
30°F	A	700	1,800	800	0.20	520	0.10	28.03	4.88	4.88	4.88
	B	1,800	4,900	2,400	0.12	784	0.15	28.03	0.43	0.43	--
	C	4,800	7,200	5,000	0.08	1,017	0.19	28.03	1.93	1.93	--
	D	--	--	--	--	--	--	--	--	--	--
	E	--	--	--	--	--	--	--	--	--	--
	F	--	--	--	--	--	--	--	--	--	--
40°F	A	500	1,800	800	0.25	460	0.09	96.36	16.76	16.76	16.76
	B	1,400	4,800	2,400	0.15	685	0.13	96.36	1.48	1.48	--
	C	3,400	7,200	4,800	0.09	933	0.18	96.36	6.65	6.65	--
	D	--	--	--	--	--	--	--	--	--	--
	E	--	--	--	--	--	--	--	--	--	--
	F	--	--	--	--	--	--	--	--	--	--
50°F	A	500	1,800	800	0.31	398	0.08	169.94	29.56	29.56	29.56
	B	1,400	4,800	2,400	0.19	553	0.10	169.94	2.62	2.62	--
	C	2,900	7,200	4,000	0.11	817	0.15	169.94	11.73	11.73	--
	D	--	--	--	--	--	--	--	--	--	--
	E	--	--	--	--	--	--	--	--	--	--
	F	--	--	--	--	--	--	--	--	--	--
60°F	A	500	1,800	800	0.35	391	0.07	260.17	45.25	45.25	45.25
	B	1,100	5,800	2,400	0.20	520	0.10	260.17	4.01	4.01	--
	C	2,000	7,200	4,000	0.16	652	0.12	260.17	17.96	17.96	--
	D	--	--	--	--	--	--	--	--	--	--
	E	--	--	--	--	--	--	--	--	--	--
	F	--	--	--	--	--	--	--	--	--	--
Total Hours								146.30	146.30	100.46	

第 2.3 - 5 表

DRIFT DEPOSITION FOR CRBRP COOLING TOWER\*

	Direction from Site							
	<u>N</u>	<u>NNE</u>	<u>NE</u>	<u>ENE</u>	<u>E</u>	<u>ESE</u>	<u>SE</u>	<u>SSE</u>
Typical Drift Deposition (lb/acre-month)	34	84	43	59	29	29	13	6

	Direction from Site							
	<u>S</u>	<u>SSW</u>	<u>SW</u>	<u>WSW</u>	<u>W</u>	<u>WNW</u>	<u>NW</u>	<u>NNW</u>
Typical Drift Deposition (lb/acre-month)	26	89	42	39	10	13	7	23

\*Based on following Table with assumption of 375 mg/l TDS in circulating cooling water  
(equivalent to 150 mg/l TDS in Clinch River)

Ref. (1) AMENDMENT II Table 5.1-17

DRIFTED DEPOSITION FROM A MECHANICAL DRAFT WET TOWER. LINEAR ARRAY

Stability Class	Drift Deposition Rate for Various Directions from the Site (lb/acre-month)*															
	N	NNE	NE	ENE	E	ESE	SE	SSE	S	SSW	SW	WSW	W	WNW	NW	NNW
C	34.22	83.71	43.10	57.07	29.19	29.19	12.67	6.34	17.11	88.75	41.86	39.31	8.88	10.13	5.09	22.85
D	23.49	75.31	36.25	58.94	23.07	20.71	7.96	5.18	26.27	49.38	24.59	29.89	9.56	12.76	6.78	11.53

\* C Stability  $0.710 \text{ kg/m}^2\text{-yr} = (527.89 \text{ lb/acre-month}) \left(\frac{7.57}{7.38}\right) = 541.48 \text{ lb/acre-month at } 326.5 \text{ m}$

D Stability  $0.522 \text{ kg/m}^2\text{-yr} = (410.41 \text{ lb/acre-month}) \left(\frac{7.57}{7.38}\right) = 420.98 \text{ lb/acre-month at } 360.7 \text{ m}$

Ref. (1) TABLE 10.1A-16

第 2.3 - 6 表

AVERAGE AND MAXIMUM VALUES OF SOME CHEMICAL  
CONSTITUENTS IN CLINCH RIVER\*

	Avg. Conc. (mg/l)	Max. Conc. (mg/l)
Total Alkalinity (as CaCO <sub>3</sub> )	96	116
Ammonia Nitrogen (as N)	0.28	1.00
BOD	2.1	6.0
Calcium	34	43
Chloride	4.7	13.0
Chlorine Residual	**	**
COD	6.7	16.0
Copper <sup>+</sup>	<0.005	<0.01
Total Dissolved Solids (TDS)	142	174
Total Iron <sup>+</sup>	0.38	0.68
Lead <sup>+</sup>	<0.03	<0.03
Magnesium	7.8	8.5
Manganese <sup>+</sup>	0.05	0.07
Nickel <sup>+</sup>	<0.01	<0.01
Nitrate (NO <sub>3</sub> )	1.3	2.2
pH	8.1	8.3
Total Phosphate	0.05	0.4
Potassium	1.4	1.9
Silica (SiO <sub>2</sub> )	3.9	6.1
Sodium	2.1	2.5
Sulfate (SO <sub>4</sub> )	15	23
Total Suspended Solids (TSS)	13	46
Zinc <sup>+</sup>	0.02	0.03

\*Based on Aquatic Baseline Survey Data (March, 1974-April, 1975)

\*\*Field measurements using the orthotolidine calorimetric method repeatedly showed the chlorine residual concentration to be below the limits of detection (<0.05 mg/l). As there are no nearby sources of chlorine additions to the river, it can be assumed that the ambient level is zero.

<sup>+</sup>Includes contribution to effluent quantities from condenser erosion/corrosion.

Ref. (1) AMENDMENT II Table 5.4-7



第 2.3 - 7 表

CONCENTRATIONS OF CHEMICAL CONSTITUENTS IN THE CRBRP DISCHARGE AND THE SIX PERCENT ISOPLETH OF THE SUMMER SHORT DURATION NO-FLOW PLUME\*

	Concentrations in CRBRP Discharge**		Concentrations in Six Percent Isopleth	
	Average (mg/l)	Maximum (mg/l)	Average (mg/l)	Maximum (mg/l)
Total Alkalinity (as CaCO <sub>3</sub> )	239	286	104.58	126.20
Ammonia Nitrogen (as N)	0.7	2.5	0.31	1.09
BOD	5.3	15.0	2.29	6.54
Calcium	85	108	37.06	46.90
Chloride	11.8	32.3	5.13	14.16
Chlorine Residual	0.2	0.5	0.01	0.03
COD	16.8	40.0	7.31	17.44
Copper <sup>+</sup>	0.2	0.93	0.02	0.07
Total Dissolved Solids (TDS)	373	582	155.86	198.48
Total Iron <sup>+</sup>	0.95	1.72	0.41	0.74
Lead <sup>+</sup>	<0.03	<0.03	<0.03	<0.03
Magnesium	19.6	21.4	8.51	9.27
Manganese	0.13	0.18	0.05	0.08
Nickel	0.02	0.11	0.01	0.02
Nitrate (NO <sub>3</sub> )	3.4	5.6	1.43	2.40

(Continued)

第 2.3 - 7 表 (Continued)

	Concentrations in CRBRP Discharge**		Concentrations in Six Percent Isopleth	
	Average (mg/l)	Maximum (mg/l)	Average (mg/l)	Maximum (mg/l)
pH	6.5 - 8.5	6.5 - 8.5		
Total Phosphate	0.14	1.0	0.06	0.44
Potassium	3.5	4.8	1.53	2.07
Silica (SiO <sub>2</sub> )	9.8	15.3	4.25	6.65
Sodium	13.2	107.3	2.77	8.79
Sulfate (SO <sub>4</sub> )	48	106	16.98	27.98
Total Suspended Solids (TSS)	33	114	14.20	50.08
Zinc <sup>+</sup>	0.05	0.08	0.02	0.03

\*Based on Iowa Institute physical model study

\*\*From Table 10.3A-2 (第 2.2 - 4 表)

<sup>+</sup>Includes contribution to effluent quantities from condenser erosion/corrosion.

第 2.3 - 8 表

DRINKING WATER QUALITY STANDARDS OF THE U.S. PUBLIC HEALTH SERVICE (44)

<u>Substance</u>	<u>Recommended Limits of Concentrations (mg/l)</u>	<u>Mandatory Limits of Concentrations (mg/l)</u>
Alkyl benzene sulfonate (ABS)	0.5	--
Arsenic (As)	0.01	0.05
Barium (Ba)	--	1.0
Cadmium (Cd)	--	0.01
Carbon chloroform extract (CCE)	0.2	--
Chloride (Cl)	250	--
Chromium (hexavalent) (Cr <sup>+6</sup> )	--	0.05
Copper (Cu)	1.0	--
Cyanide (CN)	0.01	0.2
Fluoride (F)	0.6 - 1.7	--
Iron (Fe)	0.3	--
Lead (Pb)	--	0.05
Manganese (Mn)	0.05	--
Nitrate (NO <sub>3</sub> )*	45	--
Phenols	0.001	--
Selenium (Se)	--	0.01
Silver (Ag)	--	0.05
Sulfate (SO <sub>4</sub> )	250	--
Total dissolved solids (TDS)	500	--
Zinc (Zn)	5	--

\*In areas in which the nitrate content of water is known to be in excess of the listed concentration, the public should be warned of the potential dangers of using the water for infant feeding.

Ref. (1) AMENDMENT II Table 5.4-1

第 2.3 - 9 表

RECOMMENDED SURFACE WATER CRITERIA FOR PUBLIC WATER SUPPLIES (45)

Constituent, or Characteristic	Permissible Criteria (mg/l)	Desirable Criteria (mg/l)
Ammonia	0.5 (as N)	< 0.01
Arsenic*	0.05	Absent
Barium*	1.0	Absent
Boron*	1.0	Absent
Cadmium*	0.01	Absent
Chloride*	250	< 25
Chromium,* hexavalent	0.05	Absent
Copper*	1.0	Virtually absent
Dissolved Oxygen	≥ 4 (monthly mean) > 3 (individual sample)	Near saturation
Iron (filterable)	0.3	Virtually absent
Lead*	0.05	Absent
Manganese* (filterable)	0.05	Absent
Nitrates plus nitrites*	10 (as N)	Virtually absent
pH (range)	6.0 - 8.5	
Selenium*	0.01	Absent
Silver*	0.05	Absent
Sulfate*	250	< 50
Total dissolved solids* (filterable residue)	500	< 200
Zinc*	5	Virtually absent
Cyanide*	0.2	Absent
Oil and grease	Virtually absent	Absent
Total carbon*	0.15	< 0.04
DDT*	0.042	Absent

(Continued)

第 2.3 - 9 表 (Continued)

<u>Constituent or Characteristics</u>	<u>Permissible Criteria (mg/l)</u>	<u>Desirable Criteria (mg/l)</u>
Dieldrin*	0.017	Absent
Heptaepoxide	0.018	Absent
2-4-D	0.1	Absent

\*The defined treatment process has little effect on this constituent.

Ref.(1) AMENDMENT II Table 5.4-2

第 2.3 - 1 0 表

GUIDES FOR EVALUATING THE QUALITY OF WATER USED BY LIVESTOCK<sup>(46)</sup>

Quality Factor	Threshold Concentration* (mg/l)	Limiting Concentration** (mg/l)
Total Dissolved Solids (TDS)	2,500	5,000
Cadmium	5	--
Calcium	500	1,000
Magnesium	250	500 <sup>+</sup>
Sodium	1,000	2,000 <sup>+</sup>
Arsenic	1	
Bicarbonate	500	500
Chloride	1,500	3,000
Fluoride	1	6
Nitrate	200	400
Nitrite	None	None
Sulfate	500	1,000 <sup>+</sup>
Range of pH	6.0 - 8.5	5.6 - 9.0

\*Threshold values represent concentrations at which poultry or sensitive animals might show slight effects from prolonged use of such water. Lower concentrations are of little or no concern.

\*\*Limiting concentrations based on interim criteria, South Africa. Animals in lactation or production might show definite adverse reactions.

+Total magnesium compounds plus sodium sulfate should not exceed 50 percent of the total dissolved solids.

Ref. (1) AMENDMENT II Table 5.4-3

第 2.3 - 1 1 表

TRACE ELEMENT TOLERANCES FOR IRRIGATION WATER (47)

<u>Element</u>	<u>For Water Used Continuously on All Soils (mg/l)</u>	<u>For Short-Term Use on Fine Textured Soils Only (mg/l)</u>
Aluminum	1.0	20.0
Arsenic	1.0	10.0
Beryllium	0.5	1.0
Boron	0.75	2.0
Cadmium	0.005	0.05
Chromium	5.0	20.0
Cobalt	0.2	10.0
Copper	0.2	5.0
Lead	5.0	20.0
Lithium	5.0	5.0
Manganese	2.0	20.0
Molybdenum	0.005	0.05
Nickel	0.5	2.0
Selenium	0.05	0.05
Vanadium	10.0	10.0
Zinc	5.0	10.0

Ref. (1) AMENDMENT II Table 5.4-4

第 2.3 - 1 2 表

CRITERIA FOR WATER QUALITY: FRESHWATER CONSTITUENTS  
FOR AQUATIC AND WILD LIFE\*

Parameter	Maximum Acceptable Concentrations, mg/l		
pH	6.0 - 9.0		
Alkalinity	Decreases not <25% of natural value.		
Acidity	Additions of weak dissociated acids - unacceptable.		
NH <sub>3</sub>	0.02		
Cl <sub>2</sub>	Up to 0.05 residual chlorine in 30 minutes of any 24 hours.		
DO	Temp. °C	Saturation	Min.
	36.0	7	5.8
	27.5	8	5.8
	21.0	9	6.2
	16.0	10	6.5
	7.7	12	6.8
	1.5	14	6.8
	Under extreme conditions <24 hour minimum of 4.00 for temp. >31 °C		
N <sub>2</sub> and gas bubbles	110% of existing atmospheric pressure		
Cd	0.03, total hardness >100 (as CaCO <sub>3</sub> )		
	0.004, total hardness <100 (as CaCO <sub>3</sub> )		
	0.003 crustacea, and larvae of salmonid, <100 CaCO <sub>3</sub>		
	0.004 (crustacea, eggs and larvae of salmonid, >100 CaCO <sub>3</sub> )		
Cr (total)	0.05		
Cu	0.10 of 95-hour LC50 of most sensitive important species.**		
Pb	0.03		

(Continued)



第 2.3 - 1 2 表 (Continued)

Parameter	Maximum Acceptable Concentrations, mg/l
Hg organic or inorganic	Maximum total unfiltered: 0.2 µg/l Average unfiltered: 0.05 µg/l Maximum total in aquatic organism: 0.5 µg/g wet weight
Ni	0.02 of 96-hour LC <sub>50</sub> of most sensitive important species.**
S <sup>=</sup>	Total Sulfides: 0.002
Zn	0.005 of 95-hour LC <sub>50</sub> of most sensitive important species.**
CN	0.005
Detergent	Linear alkylate sulfonates LAS: 0.2
Oils	1. No visible oil on surface 2. Hexane extracted (excluding S) in air dried sediment <1,000 mg/kg 3. <0.05 of 96-hour LC <sub>50</sub> of most sensitive important species.
Polychlorinated Biphenyls (PCB)	0.002 µg/l in water 0.5 µg/g in tissue of aquatic organisms
Phenols	0.10
Color	<10% of seasonally established normal
Turbidity	<10% of seasonally established normal
TDS	Bioassays
Suspended solids	Maximum: 80.00 Accepted: <10% of seasonally established normal

\*Water Quality Criteria, 1972, A report of the Committee on Water Quality Criteria, Environmental Studies Board, National Academy of Sciences - National Academy of Engineering, Washington, D. C., 1972; EPA R3-73-033, March 1973.

\*\*LC<sub>50</sub> lethal concentration to 50% of the tested animals.

Ref. (1) AMENDMENT II Table 5.4-5

第 2.3 - 1 3 表

PERMISSIBLE CHLORINE CONCENTRATIONS IN EFFLUENTS  
FROM NEW SOURCES\*

<u>Effluent Characteristic</u>	<u>Maximum Concentration</u>	<u>Average Concentration</u>
Free available chlorine	0.5 mg/l	0.2 mg/l

The quantity of pollutants discharged in cooling tower blowdown shall not exceed the quantity determined by multiplying the flow of cooling tower blowdown sources times the concentration listed in the above table.

Neither free available chlorine nor total residual chlorine may be discharged from any unit for more than two hours in any one day and not more than one unit in any plant may discharge free available or total residual chlorine at any one time unless the utility can demonstrate to the regional administrator or state, if the state has NPDES permit issuing authority, that the units in a particular location cannot operate at or below this level of chlorination.

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\*Federal Register, Vol 39, No. 196, October 8, 1974.

Ref. (1) AMENDMENT II Table 5.4-6

第 2.3 - 1 4 表

HUD'S ACCEPTABILITY CATEGORIES FOR NON-AIRCRAFT NOISE<sup>(48)</sup>

- Acceptable - Noise level does not exceed 45 dBA more than 30 minutes per 24 hours
- Normally Acceptable - Noise level does not exceed 65 dBA more than 8 hours per 24 hours
- Normally Unacceptable - Noise level exceeds 65 dBA 8 hours per 24 hours
- Unacceptable - Noise level exceeds 75 dBA 8 hours per 24 hours and  
Noise level exceeds 80 dBA 60 minutes per 24 hours

HVD: Department of Housing and Urban Development

Ref.(1) AMENDMENT VI Table 5.7-3

第 2.3 - 1 5 表

EXPECTED RELEASE RATES OF RADIONUCLIDES FROM THE  
GASEOUS RADWASTE SYSTEM

<u>Isotope</u>	<u>Total Leakage*</u> <u>(Ci/day)</u>
H-3	$8.5 \times 10^{-3}$
Ne-23	$5.5 \times 10^{-3}$
Ar-39	$1.5 \times 10^{-3}$
Ar-41	$5.5 \times 10^{-5}$
Kr-83m	$1.6 \times 10^{-4}$
Kr-85	$6.3 \times 10^{-6}$
Kr-85m	$4.4 \times 10^{-4}$
Kr-87	$4.1 \times 10^{-4}$
Kr-88	$7.9 \times 10^{-4}$
Xe-131m	$1.5 \times 10^{-5}$
Xe-133	$1.6 \times 10^{-3}$
Xe-133m	$8.8 \times 10^{-5}$
Xe-135	$6.3 \times 10^{-3}$
Xe-135m	$2.1 \times 10^{-4}$
Xe-138	$3.3 \times 10^{-4}$

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\*Expected release rates based on 0.1 percent failed fuel

Ref. (1) AMENDMENT IV Table 5.2-1

第 2.3 - 1 6 表

BIOACCUMULATION FACTORS FOR FRESHWATER AQUATIC FOODS<sup>(49)</sup>

<u>Isotope</u>	<u>Fish</u>	<u>Crustacea- Mollusks</u>	<u>Algae</u>	<u>Plants*</u>
H-3	1	1	1	1
Na-22	100	200	500	50
Na-24	100	200	500	50
Ne-23	NA	NA	NA	NA
Ar-39	1	1	1	1
Ar-41	1	1	1	1
Cr-51	20	2,000	4,000	400
Mn-54	400	90,000	10,000	1,000
Fe-59	100	3,200	1,000	100
Co-58	50	200	200	20
Co-60	50	200	200	20
Kr-83m	1	1	1	1
Kr-85	1	1	1	1
Kr-85m	1	1	1	1
Kr-87	1	1	1	1
Kr-88	1	1	1	1
Sr-89	30	100	500	50
Sr-90	30	100	500	50
Y-90	25	1,000	5,000	500
Y-91	25	1,000	5,000	500
Zr-95	330	7	1,000	100
Nb-95	30,000	100	800	80
Mo-99	10	10	1,000	100
Ru-103	10	300	2,000	200
Ru-106	10	300	2,000	200
Rh-106	10	300	200	20

(Continued)

第 2.3 - 1 6 表 (Continued)

<u>Isotope</u>	<u>Fish</u>	<u>Crustacea- Mollusks</u>	<u>Algae</u>	<u>Plants*</u>
Ag-111	2	770	200	20
Sb-125	1	10	1,500	150
Te-129	400	75	100	10
Te-129m	400	75	100	10
Te-132	400	75	100	10
I-131	15	5	40	4
I-132	15	5	40	4
Xe-131m	1	1	1	1
Xe-133	1	1	1	1
Xe-133m	1	1	1	1
Xe-135	1	1	1	1
Xe-135m	1	1	1	1
Xe-138	1	1	1	1
Cs-134	2,000	100	500	50
Cs-136	2,000	100	500	50
Cs-137	2,000	100	500	50
Ba-140	4	200	500	50
La-140	25	1,000	5,000	500
Ce-141	1	1,000	4,000	400
Ce-144	1	1,000	4,000	400
Pr-143	25	1,000	5,000	500
Pr-144	25	1,000	5,000	500
Nd-147	25	1,000	5,000	500
Pm-147	25	1,000	5,000	500
Eu-155	25	1,000	5,000	500
Ta-182	NA	NA	NA	NA

(Continued)

第 2.3 - 1 6 表 (Continued)

<u>Isotope</u>	<u>Fish</u>	<u>Crustacea- Mollusks</u>	<u>Algae</u>	<u>Plants*</u>
Pu-238	4	100	350	35
Pu-239	4	100	350	35
Pu-240	4	100	350	35
Pu-241	4	100	350	35
Pu-242	4	100	350	35

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\*Plants are assumed to contain 1/10 as much radioactivity as would be predicted using bioaccumulation factors for algae.

Ref. (1) AMENDMENT IV Table 5.3A-12

第 2.3 - 1 7 表

EXPECTED RELEASE RATES OF RADIONUCLIDES IN THE  
LIQUID RADWASTE DISCHARGE

<u>Isotope</u>	<u>Low-Level Activity* Concentration at the Discharge Point (<math>\mu\text{Ci}/\text{cc}</math>)</u>	<u>Intermediate- Level Activity** Concentration at the Discharge Point (<math>\mu\text{Ci}/\text{cc}</math>)</u>
H-3 <sup>+</sup>	$9.12 \times 10^{-10}$	$1.59 \times 10^{-9}$
Na-22	$7.65 \times 10^{-15}$	$1.31 \times 10^{-14}$
Na-24	$2.19 \times 10^{-16}$	$3.78 \times 10^{-15}$
Cr-51	--	$6.07 \times 10^{-13}$
Mn-54	$8.61 \times 10^{-17}$	$4.29 \times 10^{-12}$
Co-58	$2.18 \times 10^{-17}$	$2.63 \times 10^{-12}$
Co-60	$1.17 \times 10^{-17}$	$4.20 \times 10^{-12}$
Fe-59	--	$2.11 \times 10^{-14}$
Sr-89	$3.95 \times 10^{-17}$	$2.41 \times 10^{-13}$
Sr-90	$2.84 \times 10^{-17}$	$1.74 \times 10^{-13}$
Y-90	$2.84 \times 10^{-17}$	$1.74 \times 10^{-13}$
Y-91	$1.16 \times 10^{-17}$	$7.09 \times 10^{-14}$
Zr-95	$2.19 \times 10^{-17}$	$1.34 \times 10^{-13}$
Nb-95	$2.19 \times 10^{-17}$	$1.34 \times 10^{-13}$
Mo-99	--	$1.51 \times 10^{-14}$
Ru-103	$3.04 \times 10^{-17}$	$1.85 \times 10^{-13}$
Ru-106	$2.36 \times 10^{-17}$	$1.44 \times 10^{-13}$
Rh-106	$2.36 \times 10^{-17}$	$1.44 \times 10^{-13}$
Ag-111	--	$4.90 \times 10^{-15}$
Sb-125	$2.02 \times 10^{-16}$	$3.49 \times 10^{-16}$
Te-129	$2.47 \times 10^{-16}$	$1.48 \times 10^{-12}$
Te-129m	$2.47 \times 10^{-16}$	$1.48 \times 10^{-12}$

(Continued)



第 2.3 - 1 7 表 (Continued)

<u>Isotope</u>	<u>Low-Level Activity* Concentration at the Discharge Point (<math>\mu\text{Ci/cc}</math>)</u>	<u>Intermediate- Level Activity** Concentration at the Discharge Point (<math>\mu\text{Ci/cc}</math>)</u>
Te-132	$1.76 \times 10^{-16}$	$1.22 \times 10^{-12}$
I-131	$9.37 \times 10^{-15}$	$1.62 \times 10^{-14}$
I-132	$1.76 \times 10^{-16}$	$1.22 \times 10^{-12}$
Cs-134	$9.47 \times 10^{-16}$	$1.64 \times 10^{-15}$
Cs-136	$4.26 \times 10^{-15}$	$7.37 \times 10^{-15}$
Cs-137	$3.48 \times 10^{-14}$	$3.95 \times 10^{-14}$
Ba-140	$1.57 \times 10^{-17}$	$9.70 \times 10^{-14}$
La-140	$1.59 \times 10^{-17}$	$9.70 \times 10^{-14}$
Ce-141	$2.62 \times 10^{-17}$	$1.60 \times 10^{-13}$
Ce-144	$1.86 \times 10^{-17}$	$1.14 \times 10^{-13}$
Pr-143	$1.37 \times 10^{-17}$	$8.38 \times 10^{-14}$
Pr-144	$1.86 \times 10^{-17}$	$1.14 \times 10^{-13}$
Nd-147	$5.73 \times 10^{-18}$	$3.51 \times 10^{-14}$
Pm-147	$1.07 \times 10^{-17}$	$6.49 \times 10^{-14}$
Eu-155	--	$6.11 \times 10^{-15}$
Ta-182	--	$5.02 \times 10^{-14}$
Pu-238	$3.29 \times 10^{-17}$	$1.68 \times 10^{-15}$
Pu-239	$9.12 \times 10^{-18}$	$3.72 \times 10^{-16}$
Pu-240	$1.20 \times 10^{-17}$	$4.84 \times 10^{-16}$
Pu-241	$1.00 \times 10^{-15}$	$4.08 \times 10^{-14}$
Pu-242	$2.55 \times 10^{-20}$	$1.04 \times 10^{-18}$

(Continued)

第 2.3 - 1 7 表 (Continued)

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**\*Low-Activity Liquid Waste System Assumptions**

1. 0.1 percent failed fuel, 50 ppb Pu in sodium, 30-year irradiation, 10 days decay
2. 850 gal/day containing  $10^{-4}$   $\mu\text{Ci/cc}$  is decontaminated by a factor of  $10^5$  and released into the coolant water blowdown stream of  $3.0 \times 10^{12}$  cc/yr
3. The activity level of  $10^{-4}$   $\mu\text{Ci/cc}$  comes from spillage of 3.5 pounds per year of primary sodium into the drainage stream of 850 gal/day.

**\*\*Intermediate-Activity Level Stream Assumptions**

1. 0.1 percent failed fuel, 50 ppb Pu in sodium, 30-year irradiation, 10 days decay. Decay times during collection, processing and holdup are neglected.
2. 4,000 gal/yr discharged into the coolant water blowdown stream after DF of  $10^5$
3. 40 percent of the annual plated activity on the processed components is released into the annual decontaminant liquids. 100 percent of the annual sodium plated activity is released into the same volume.

<sup>+</sup>Balance of plant tritium concentration of  $1.5 \times 10^{-4}$   $\mu\text{Ci/cc}$  not included in table. However, BOP tritium discharge has been included in all dose calculations.

Ref. (1) AMENDMENT VIII Table 5.2-2

第 2.3 - 1 8 表

EVALUATION OF DOSES TO BIOTA OTHER THAN MAN VIA EXPOSURE TO GASEOUS RELEASES FROM THE CRBRP

Biota	Pathway	Equations Used from Appendix to Sections 5.2 and 5.3	Assumptions	Dose
All terrestrial species	External dose from exposure to radioactive plume	1 and 2 (16, 17)	Exposure occurs at the site boundary in the prevailing wind direction where $\chi/Q = 4.33 \times 10^{-5} \text{ sec/m}^3$	Total Body Gamma - 0.020 mrad/yr Beta Skin - 0.043 mrad/yr
All terrestrial species	External dose from exposure to contaminated soil	14 and 15 (28, 29)	Exposure occurs at the site boundary in the prevailing wind direction where $\chi/Q = 4.33 \times 10^{-5} \text{ sec/m}^3$	Total Body Gamma - 0.0 mrad/yr Beta Skin - 0.0 mrad/yr
All terrestrial species	Internal dose due to inhalation of contaminated air	4 (19)	Exposure occurs at the site boundary in the prevailing wind direction where $\chi/Q = 4.33 \times 10^{-5} \text{ sec/m}^3$  Average breathing rate of all species is 2.3 m <sup>3</sup> /day.	Whole Body - $8.2 \times 10^{-4}$ mrad/yr
Rabbit Deer	Internal dose from ingestion of contaminated food crops	16 and 17 (30, 31)	Masses - Rabbit, 2.0 kg Deer, 50.0 kg Ingestion Rate - Rabbit, 100 g/day Deer, 1000 g/day  Food crops are ingested at the site boundary in the prevailing wind direction where $\chi/Q = 4.33 \times 10^{-5} \text{ sec/m}^3$  Duration of deposition - 365 days Period of ingestion - 60 days	Rabbit Whole Body - 0.27 mrad/yr  Deer Whole Body - 0.12 mrad/yr

(Continued)

第 2.3 - 1 8 表 (Continued)

Biota	Pathway	Equations Used from Appendix to Sections 5.2 and 5.3	Assumptions	Dose
Rabbit Deer	Internal dose from ingestion of food crops contaminated by uptake of radioactivity deposited on soil	18 and 19 (32, 33)	Masses - Rabbit, 2.0 kg Deer, 50.0 kg Ingestion Rate - Rabbit, 100 g/day Deer, 1000 g/day Food crops are ingested at the site boundary in the prevailing wind direction where $\chi/Q = 4.33 \times 10^{-5} \text{ sec/m}^3$ Duration of deposition - 365 days Period of ingestion - 60 days	Rabbit Whole Body - $1.0 \times 10^{-3}$ mrad/yr Deer Whole Body - $3.8 \times 10^{-4}$ mrad/yr

Ref. (1) AMENDMENT VIII Table 5.2-3

( )内の数字は本文中 ( 2.3.4 ) の式番号を示す。

第 2.3 - 1 9 表

EVALUATION OF DOSES TO BIOTA OTHER THAN MAN VIA EXPOSURE TO LIQUID RELEASES FROM THE CRBRP

Biota	Pathway	Equations Used from Appendix to Sections 5.2 and 5.3	Assumptions	Dose
All aquatic species except those which are buried in the sediment	External dose from exposure to contaminated river sediment	20 (34)	Water body width factor - 0.2 Dilution factor - 0.05 Elapsed time between isotope release and exposure - 0.5 days Operating lifetime of plant - 10,950 days	Total Body Gamma - $1.26 \times 10^{-6}$ mrad/yr Beta Skin - $1.48 \times 10^{-6}$ mrad/yr
Aquatic species which are buried in the sediment (mussels, fish eggs, worms, etc.)	External dose from exposure to contaminated river sediment	20 (34)	Water body width factor - 2.0 Dilution factor - 0.05 Elapsed time between isotope release and exposure - 0.5 days Operating lifetime of plant - 10,950 days	Total Body Gamma - $1.26 \times 10^{-5}$ mrad/yr Beta Skin - $1.48 \times 10^{-5}$ mrad/yr
All aquatic species	External dose from immersion in contaminated water	21 and 22 (35,36)	Time of exposure - 8,760 hr Dilution factor - 0.05 Elapsed time between isotope release and exposure - 0.5 days Operating lifetime of plant - 10,950 days	Total Body Gamma - $1.42 \times 10^{-5}$ mrad/yr Beta Skin - $1.76 \times 10^{-5}$ mrad/yr
Crustacea Aquatic Plant Fish Heron Raccoon	Internal dose from ingestion of contaminated water	30 (44)	Doses - Crustacea, 0.01 kg Aquatic Plant, 0.01 kg Fish, 1.0 kg Heron, 4.6 kg Raccoon, 12.0 kg  In the absence of data for bioaccumulation of radionuclide in Heron or Raccoon, data for Fish will be used Dilution factor - 0.05	Whole Body: Crustacea - 1.41 mrad/yr Aquatic Plant - 1.38 mrad/yr Fish - 1.38 mrad/yr Heron - 1.38 mrad/yr Raccoon - 1.38 mrad/yr

(Continued)

第 2.3 - 19 表 (Continued)

Biota	Pathway	Equations Used from Appendix to Sections 5.2 and 5.3	Assumptions	Dose
Fish	Internal dose from ingestion of aquatic foods	31	Masses - Fish, 1.0 kg Ducks, 1.0 kg Mink, 1.0 kg Heron, 4.6 kg Raccoon, 12.0 kg  Feeding Rates - Duck, 100 g fish/day Duck, 100 g plants/day Mink, 50 g fish/day 50 g crustacea/day Heron, 300 g fish/day Raccoon, 300 g fish/day 50 g crustacea/day 50 g plants/day  Period of ingestion, 365 days Dilution factor, 0.05	Fish, 1.93 mrad/yr
Fish-Feeding Ducks		(45)		Fish-Feeding Duck, 2.40 mrad/yr
Plant-Feeding Ducks				Plant-Feeding Duck, 2.40 mrad/yr
Mink				Mink, 2.40 mrad/yr
Heron				Heron, 1.56 mrad/yr
Raccoon			Raccoon, 0.81 mrad/yr	

Ref. (1) AMENDMENT VIII Table 5.2-4

( )内の数字は本文中(2.3.4)の式番号を示す。

SUMMARY OF DOSE RATES TO BIOTA OTHER THAN MAN FROM EXPOSURE TO RADIOACTIVE  
MATERIALS RELEASED FROM CRBRP RADWASTE SYSTEMS

mrads/yr

	Total External Dose		Total Internal Dose
	Total Body	Skin	
<u>Aquatic Species</u>			
Crustacea	$1.5 \times 10^{-5}$	$1.9 \times 10^{-5}$	1.41
Aquatic Plant	$1.5 \times 10^{-5}$	$1.9 \times 10^{-5}$	1.38
Fish	$1.5 \times 10^{-5}$	$1.9 \times 10^{-5}$	3.29
Fish-Feeding Duck	$1.5 \times 10^{-5}$	$1.9 \times 10^{-5}$	2.40
Plant-Feeding Duck	$1.5 \times 10^{-5}$	$1.9 \times 10^{-5}$	2.40
Mussels, Fish Eggs, Worms	$2.7 \times 10^{-5}$	$3.2 \times 10^{-5}$	--
<u>Terrestrial Species</u>			
Heron	$2.0 \times 10^{-2}$	$4.3 \times 10^{-2}$	2.94
Mink	$2.0 \times 10^{-2}$	$4.3 \times 10^{-2}$	2.40
Raccoon	$2.0 \times 10^{-2}$	$4.3 \times 10^{-2}$	2.19
Rabbit	$2.0 \times 10^{-2}$	$4.3 \times 10^{-2}$	0.27
Deer	$2.0 \times 10^{-2}$	$4.3 \times 10^{-2}$	< 0.12

第 2.3 - 2 1 表

ANNUAL AVERAGE  $\chi/Q$ 'S AT VARIOUS DOWNWIND DISTANCES FOR EACH WIND SECTOR  
ANNUAL AVERAGE  $\chi/Q$  (sec/m<sup>3</sup>)

Downwind Distance (Miles)	WIND DIRECTION															
	N	NNE	NE	ENE	E	ESE	SE	SSE	S	SSW	SW	WSW	W	WNW	NW	NNW
0.1	1.34E-4	1.14E-4	2.26E-4	3.84E-4	5.19E-4	7.28E-4	7.87E-4	3.02E-4	2.37E-4	2.18E-4	2.40E-4	1.60E-4	1.31E-4	1.47E-4	1.96E-4	2.66E-4
0.2	3.86E-5	3.23E-5	6.52E-5	1.11E-4	1.50E-4	2.11E-4	2.29E-4	8.75E-5	6.87E-5	6.31E-5	6.91E-5	4.59E-5	3.77E-5	4.22E-5	5.65E-5	7.71E-5
0.3	1.88E-5	1.59E-5	3.18E-5	5.41E-5	7.33E-5	1.03E-4	1.12E-4	4.27E-5	3.35E-5	3.08E-5	3.38E-5	2.25E-5	1.84E-5	2.06E-5	2.75E-5	3.76E-5
0.34	1.49E-5	1.26E-5	2.52E-5	4.27E-5	5.78E-5	8.12E-5	8.78E-5	3.36E-5	2.64E-5	2.43E-5	2.70E-5	1.81E-5	1.46E-5	1.64E-5	2.18E-5	2.93E-5
0.42	1.04E-5	8.89E-6	1.77E-5	3.00E-5	4.04E-5	5.68E-5	6.14E-5	2.35E-5	1.85E-5	1.71E-5	1.91E-5	1.28E-5	1.03E-5	1.16E-5	1.53E-5	2.09E-5
0.5	7.74E-6	6.61E-6	1.32E-5	2.23E-5	3.00E-5	4.22E-5	4.57E-5	1.75E-5	1.38E-5	1.27E-5	1.43E-5	9.65E-6	7.69E-6	8.68E-6	1.14E-5	1.55E-5
0.6	5.63E-6	4.87E-6	9.69E-6	1.63E-5	2.20E-5	3.10E-5	3.35E-5	1.28E-5	1.01E-5	9.35E-6	1.06E-5	7.16E-6	5.67E-6	6.41E-6	8.39E-6	1.14E-5
0.7	4.49E-6	3.92E-6	7.72E-6	1.28E-5	1.71E-5	2.40E-5	2.59E-5	1.00E-5	7.91E-6	7.43E-6	8.83E-6	6.01E-6	4.57E-6	5.22E-6	6.65E-6	8.92E-6
1.0	2.52E-6	2.19E-6	4.34E-6	7.21E-6	9.70E-6	1.37E-5	1.48E-5	5.67E-6	4.48E-6	4.19E-6	4.94E-6	3.35E-6	2.56E-6	2.92E-6	3.74E-6	5.01E-6
1.5	1.45E-6	1.27E-6	2.45E-6	3.98E-6	5.31E-6	7.37E-6	7.89E-6	3.11E-6	2.46E-6	2.33E-6	2.77E-6	1.89E-6	1.44E-6	1.66E-6	2.12E-6	2.91E-6
2.0	8.54E-7	7.33E-7	1.47E-6	2.45E-6	3.30E-6	4.67E-6	5.04E-6	1.93E-6	1.32E-6	1.42E-6	1.65E-6	1.11E-6	8.59E-7	9.80E-7	1.20E-6	1.63E-6
2.5	5.94E-7	5.16E-7	1.01E-6	1.69E-6	2.27E-6	3.18E-6	3.44E-6	1.33E-6	1.05E-6	9.77E-7	1.13E-6	7.55E-7	5.94E-7	6.75E-7	8.70E-7	1.17E-6
3.0	4.63E-7	4.00E-7	7.93E-7	1.32E-6	1.79E-6	2.52E-6	2.73E-6	1.05E-6	8.26E-7	7.67E-7	8.87E-7	5.91E-7	4.63E-7	5.26E-7	6.80E-7	9.12E-7
3.5	3.64E-7	3.15E-7	6.23E-7	1.04E-6	1.40E-6	1.93E-6	2.14E-6	8.20E-7	6.47E-7	6.01E-7	6.96E-7	4.63E-7	3.64E-7	4.14E-7	5.34E-7	7.17E-7
4.0	2.99E-7	2.58E-7	5.12E-7	8.55E-7	1.16E-6	1.63E-6	1.76E-6	8.76E-7	5.33E-7	4.95E-7	5.71E-7	3.79E-7	2.99E-7	3.40E-7	4.35E-7	5.83E-7
4.5	2.51E-7	2.17E-7	4.29E-7	7.17E-7	9.69E-7	1.36E-6	1.47E-6	5.66E-7	4.47E-7	4.15E-7	4.77E-7	3.16E-7	2.50E-7	2.84E-7	3.68E-7	4.94E-7
5.0	2.16E-7	1.86E-7	3.66E-7	6.16E-7	8.35E-7	1.18E-6	1.27E-6	4.88E-7	3.85E-7	3.56E-7	4.09E-7	2.70E-7	2.14E-7	2.44E-7	3.15E-7	4.24E-7
7.0	1.33E-7	1.14E-7	2.27E-7	3.81E-7	5.18E-7	7.33E-7	7.94E-7	3.03E-7	2.39E-7	2.20E-7	2.49E-7	1.63E-7	1.31E-7	1.49E-7	1.94E-7	2.61E-7
7.5	1.21E-7	1.03E-7	2.06E-7	3.46E-7	4.72E-7	6.67E-7	7.23E-7	2.76E-7	2.17E-7	2.00E-7	2.26E-7	1.48E-7	1.19E-7	1.35E-7	1.76E-7	2.33E-7
9.0	5.26E-8	4.53E-8	8.96E-8	1.45E-7	1.96E-7	2.73E-7	2.94E-7	1.16E-7	9.17E-8	8.60E-8	9.70E-8	6.40E-8	5.00E-8	5.70E-8	7.40E-8	9.80E-8
10.0	4.57E-8	3.97E-8	7.93E-8	1.26E-7	1.71E-7	2.37E-7	2.58E-7	1.00E-7	7.91E-8	7.43E-8	8.83E-8	6.01E-8	4.57E-8	5.22E-8	6.65E-8	8.92E-8
15.0	4.66E-8	3.95E-8	7.97E-8	1.35E-7	1.86E-7	2.64E-7	2.88E-7	1.00E-7	8.54E-8	7.78E-8	8.58E-8	5.47E-8	4.53E-8	5.11E-8	6.75E-8	9.00E-8
20.0	3.22E-8	2.71E-8	5.56E-8	9.35E-8	1.29E-7	1.84E-7	2.01E-7	7.54E-8	5.93E-8	5.38E-8	5.88E-8	3.71E-8	3.11E-8	3.50E-8	4.64E-8	6.20E-8
25.0	3.02E-8	2.55E-8	5.16E-8	8.76E-8	1.21E-7	1.73E-7	1.88E-7	7.07E-8	5.56E-8	5.04E-8	5.50E-8	3.47E-8	2.91E-8	3.27E-8	4.35E-8	5.84E-8
27.0	2.41E-8	2.02E-8	4.13E-8	7.03E-8	9.72E-8	1.33E-7	1.52E-7	5.68E-8	4.47E-8	4.04E-8	4.38E-8	2.75E-8	2.32E-8	2.61E-8	3.47E-8	4.67E-8
35.0	1.55E-8	1.32E-8	2.73E-8	4.67E-8	6.50E-8	9.41E-8	1.03E-7	3.81E-8	2.99E-8	2.68E-8	2.86E-8	1.78E-8	1.51E-8	1.71E-8	2.28E-8	3.06E-8
45.0	1.18E-8	9.67E-9	2.02E-8	3.47E-8	4.86E-8	7.07E-8	7.73E-8	2.85E-8	2.23E-8	2.00E-8	2.11E-8	1.29E-8	1.11E-8	1.25E-8	1.69E-8	2.26E-8
50.0	1.05E-8	8.55E-9	1.80E-8	3.10E-8	4.35E-8	6.35E-8	6.95E-8	2.55E-8	2.00E-8	1.78E-8	1.87E-8	1.14E-8	9.88E-9	1.11E-8	1.50E-8	2.01E-8



第 2.3 - 2 2 表

RADIOLOGICAL DATA FOR ISOTOPES RELEASED FROM CRBRP RADWASTE SYSTEMS

<u>Isotope</u>	<u>Radioactive Half-life<sup>(2)</sup> (Days)</u>	<u>Total Gamma Energy<sup>(2,3)</sup> (MeV/dis)</u>	<u>Average Beta Energy<sup>(2,4)</sup> (MeV/dis)</u>
H-3	$4.49 \times 10^3$	0.0	0.006
Na-22	$3.16 \times 10^2$	2.195	0.182
Na-24	$6.25 \times 10^{-1}$	4.123	0.463
Ne-23	$4.40 \times 10^{-4}$	0.160	1.460
Ar-39	$9.80 \times 10^4$	0.0	0.188
Ar-41	$7.60 \times 10^{-2}$	1.280	0.406
Cr-51	$2.78 \times 10^1$	0.029	0.105
Mn-54	$3.03 \times 10^2$	0.835	0.276
Fe-59	$4.56 \times 10^1$	1.190	0.116
Co-58	$7.13 \times 10^1$	0.977	0.024
Co-60	$1.92 \times 10^3$	2.510	0.105
Kr-83m	$7.80 \times 10^{-2}$	0.002	0.036
Kr-85	$3.93 \times 10^3$	0.002	0.230
Kr-85m	$1.82 \times 10^{-1}$	0.158	0.277
Kr-87	$5.30 \times 10^{-2}$	0.793	1.324
Kr-88	$1.16 \times 10^{-1}$	1.950	0.376
Sr-89	$5.27 \times 10^1$	$8.2 \times 10^{-5}$	0.488
Sr-90	$1.01 \times 10^4$	0.0	0.182
Y-90	$2.67 \times 10^0$	0.0	0.930
Y-91	$5.88 \times 10^1$	0.004	0.515
Zr-95	$6.55 \times 10^1$	0.725	0.130
Nb-95	$3.50 \times 10^1$	0.765	0.053
Mo-99	$2.80 \times 10^0$	0.137	0.410

(Continued)

第 2.3 - 2 2 表 (Continued)

<u>Isotope</u>	<u>Radioactive Half-life<sup>(2)</sup> (Days)</u>	<u>Total Gamma Energy<sup>(2,3)</sup> (MeV/dis)</u>	<u>Average Beta Energy<sup>(2,4)</sup> (MeV/dis)</u>
Ru-103	$3.95 \times 10^1$	0.474	0.077
Ru-106	$3.68 \times 10^2$	0.0	0.013
Rh-106	$3.50 \times 10^{-4}$	0.200	1.180
Ag-111	$7.50 \times 10^0$	0.023	0.350
Sb-125	$9.90 \times 10^2$	0.121	0.335
Te-129	$4.80 \times 10^{-2}$	0.098	0.499
Te-129m	$3.41 \times 10^1$	0.041	0.621
Te-132	$3.24 \times 10^0$	0.216	0.100
I-131	$8.05 \times 10^0$	0.371	0.197
I-132	$9.60 \times 10^{-2}$	2.400	0.448
Xe-131m	$1.18 \times 10^1$	0.020	0.143
Xe-133	$5.27 \times 10^0$	0.045	0.135
Xe-133m	$2.26 \times 10^0$	0.042	0.189
Xe-135	$0.38 \times 10^0$	0.247	0.316
Xe-135m	$1.08 \times 10^{-2}$	0.432	0.095
Xe-138	$1.21 \times 10^{-2}$	1.183	0.612
Cs-134	$7.47 \times 10^2$	1.590	0.166
Cs-136	$1.37 \times 10^1$	2.230	0.139
Cs-137	$1.10 \times 10^4$	0.563	0.246
Ba-140	$1.28 \times 10^1$	0.236	0.284
La-140	$1.70 \times 10^0$	2.120	0.397
Ce-141	$3.25 \times 10^1$	0.070	0.315
Ce-144	$2.84 \times 10^2$	0.016	0.101
Pr-143	$1.36 \times 10^1$	0.0	0.310
Pr-144	$1.19 \times 10^{-2}$	0.030	0.997
Nd-147	$1.11 \times 10^1$	0.122	0.335

(Continued)

第 2.3 - 2 2 表 (Continued)

<u>Isotope</u>	<u>Radioactive Half-life<sup>(2)</sup> (Days)</u>	<u>Total Gamma (2,3) Energy (MeV/dis)</u>	<u>Average Beta (2,4) Energy (MeV/dis)</u>
Pm-147	$9.56 \times 10^2$	0.0	0.070
Eu-155	$6.61 \times 10^2$	0.049	0.075
Ta-182	$1.15 \times 10^2$	1.133	0.877
Pu-238	$3.15 \times 10^4$	$3.8 \times 10^{-4}$	0.021
Pu-239*	$8.90 \times 10^6$	$2.9 \times 10^{-5}$	0.036
Pu-240*	$2.40 \times 10^6$	$1.3 \times 10^{-7}$	0.022
Pu-241	$4.80 \times 10^3$	$2.3 \times 10^{-7}$	0.007
Pu-242*	$1.38 \times 10^8$	0.0	0.0

\*Decay is primarily by alpha emission. Total alpha energies, MeV/dis, for the plutonium isotopes are as follows:

1. Pu-239 - 5.10
2. Pu-240 - 5.16
3. Pu-242 - 4.89

Ref. (1) AMENDMENT IV Table 5.3A-1

第 2.3 - 2 3 表

MAXIMUM INTERNAL WHOLE BODY DOSE RECEIVED BY AN INDIVIDUAL  
VIA EXPOSURE TO CRBRP GASEOUS EFFLUENTS

<u>Pathway</u>	<u>Location of Exposure</u>	<u>x/Q (sec/m<sup>3</sup>)</u>	<u>Dose (mrem/yr)</u>
Inhalation	Near side of river 2,500 feet NW of the Plant	$5.0 \times 10^{-5}$	$8.4 \times 10^{-3}$
Ingestion of milk	Closest dairy cow, 2 miles, WNW	$4.67 \times 10^{-6}$	$4.4 \times 10^{-1}$
Ingestion of leafy vegetables	Closest home garden, 0.6 mile, SSW	$9.69 \times 10^{-6}$	$3.5 \times 10^{-2}$
Ingestion of beef	Closest forage area 0.3 mile, S	$1.88 \times 10^{-5}$	$7.4 \times 10^{-2}$
Total			$5.6 \times 10^{-1}$

Ref.(1) AMENDMENT VII Table 5.3-1

第 2.3 - 2.4 表

SUMMARY OF VARIABLES USED IN RADIOLOGICAL DOSE EVALUATIONS  
WHICH ARE NOT SPECIFIC TO THE CRBRP

<u>Variable</u>	<u>Description</u>	<u>Measurement</u>
<u>Ingestion of Leafy Vegetables</u>		
VDW	Deposition velocity of isotope over water	Noble gases, $0.5 \times 10^{-7}$ cm/sec <sup>(52)</sup> H-3, 5 cm/sec <sup>(53, 54)</sup>
YC	Yield per unit of cultivated land area for leafy vegetables	1.5 kg/m <sup>2</sup> <sup>(55)</sup>
	Total acreage of leafy vegetable crops under cultivation within a 50-mile radius of the CRBRP	434 acres
TGS	Growing season of leafy vegetables	3 months <sup>(49)</sup>
VDL	Deposition velocity of isotope over land	Noble gases, $0.5 \times 10^{-7}$ cm/sec <sup>(52)</sup> H-3, 1.4 cm/sec <sup>(51)</sup>
TLV	Total daily intake of leafy vegetables	0.2 kg/day <sup>(49)</sup> for an individual or an average population
TDL	Elapsed time between harvest and ingestion	7 days <sup>(56)</sup>
T <sub>b</sub>	Weathering half-life of isotopes on leafy vegetables	14 days <sup>(55, 57)</sup>
FLI	Fractional retention of isotope on vegetation leaves	0.1 <sup>(56)</sup>
FA	Average fraction of the ground surface covered by leafy vegetables	0.25 <sup>(49)</sup>

(Continued)

第 2.3 - 2 4 表 (Continued)

<u>Variable</u>	<u>Description</u>	<u>Measurement</u>
FRI	Transfer coefficient for soil to plant via roots	<u>Element</u> <u>Coefficient</u> <sup>(55, 58)</sup>
		Fe $1.5 \times 10^{-4}$
		Sr $3.2 \times 10^{-3}$
		Ru $3.8 \times 10^{-3}$
		Cs $1.9 \times 10^{-2}$
		Ce $7.5 \times 10^{-4}$
		Pu $1.0 \times 10^{-4}$
FSI	Fraction of isotope which reaches soil	0.75 <sup>(49)</sup>
R	Rate of ingestion of vegetation	Rabbit, 100 g/day <sup>(55)</sup>
<u>Ingestion of Beef</u>		
G	Effective grazing area of cattle	20-80 m <sup>2</sup> /day <sup>(59)</sup> (45 m <sup>2</sup> /day used <sup>(62)</sup> )
SUMFT <sub>B</sub>	Total cumulative fraction of isotope transferred per kg of beef	$2 \times 10^{-3}$ /kg for H-3 <sup>(55)</sup> 0.2/kg for Cs <sup>(60)</sup> 0.05/kg for Sr <sup>(60)</sup>
TB	Total daily human intake of beef	0.04 kg/day for an individual <sup>(55)</sup> 0.14 kg/day for an average population <sup>(63)</sup>
TDB	Elapsed time between butchering and ingestion	20 days <sup>(55)</sup>
<u>Ingestion of Aquatic Foods</u>		
G <sub>F</sub>	Rate of ingestion of aquatic food for man	50 g/day - freshwater fish (max. for adult) <sup>(49)</sup>
P	Rate of ingestion of aquatic foods for biota other than man	Ducks, surface feeding - 100 g/day of plants <sup>(61)</sup>
		Ducks, diving - 100 g/day of fish <sup>(61)</sup>

第 2.3 - 2.4 表 (Continued)

<u>Variable</u>	<u>Description</u>	<u>Measurement</u>
		Mink - 50 g/day of fish and 50 g/day if invertebrates <sup>(61)</sup>
MS	Average mass of organism feeding on aquatic food	Ducks - 1 kg <sup>(49, 61)</sup> Mink - 1 kg <sup>(61)</sup> Muskrat - 1 kg <sup>(49)</sup> Raccoon - 12 kg <sup>(49)</sup> Heron - 4.6 kg <sup>(49)</sup>
TIM	Elapsed time between release and ingestion	0.5 days
	Average effective radius of organisms feeding on aquatic food	Ducks - 5 cm <sup>(49)</sup> Mink - 10 cm <sup>(61)</sup> Rabbit - 10 cm <sup>(61)</sup> Muskrat - 6 cm <sup>(49)</sup> Raccoon - 14 cm <sup>(49)</sup> Heron - 11 cm <sup>(49)</sup>
M	Average mass of aquatic organism	Fish - 1 kg <sup>(61)</sup> Invertebrates - 0.005 kg <sup>(61)</sup> Plant - 0.005 kg <sup>(61)</sup>
	Average effective radius of aquatic organism	Fish - 10 cm <sup>(61)</sup> Invertebrates - 2 cm <sup>(61)</sup> Plant - 2 cm <sup>(61)</sup>
<u>Exposure Via Above-Water Activities</u>		
TI	Time spent immersed in effluent water	100 hr/yr <sup>(49)</sup>
TAW	Time spent in above water activities	Boating - 100 hr/yr <sup>(49)</sup> Shoreline activities - 500 hr/yr <sup>(49)</sup>

第 2.3 - 2.4 表 (Continued)

<u>Variable</u>	<u>Description</u>	<u>Measurement</u>
SUMFT	Accumulative fractional intake of isotope per liter which is transferred to the milk each day	$2.0 \times 10^{-2}/l$ for H-3 <sup>(55)</sup>

Ref. (1) AMENDMENT VIII Table 5.3A-13



第 2.3 - 2 5 表

DOSE RATES RECEIVED BY AN INDIVIDUAL VIA  
EXPOSURE TO CRBRP LIQUID EFFLUENTS

mrem/yr

	<u>Pathway</u>			
	<u>Contaminated River Sediment</u>	<u>Immersion</u>	<u>Above-Water Activities</u>	<u>Ingestion of Aquatic Food</u>
Total Body Gamma	$7.20 \times 10^{-8}$	$1.62 \times 10^{-7}$	$4.87 \times 10^{-7}$	--
Total Skin	$8.48 \times 10^{-8}$	$2.01 \times 10^{-7}$	$6.04 \times 10^{-7}$	--
Whole Body Internal	--	--	--	$1.69 \times 10^{-2}$
Bone	--	--	--	$2.89 \times 10^{-5}$
GI Tract	--	--	--	$2.00 \times 10^{-4}$
Thyroid (Adult)	--	--	--	$6.51 \times 10^{-7}$
Kidney	--	--	--	$3.41 \times 10^{-5}$

Ref.(1) AMENDMENT VIII Table 5.3-2

第 2.3 - 2 6 表

BUILD-UP ACTIVITY OF AM-241 FROM PU-241 RELEASED  
FROM CRBRP LIQUID RADWASTE SYSTEM\*

<u>No. of Years After Pu-241 is Initially Released</u>	<u>Activity Am-241 (<math>\mu\text{Ci/cc}</math>)</u>
1	$7.11 \times 10^{-17}$
30	$2.11 \times 10^{-15}$
80	$5.38 \times 10^{-15}$
200	$1.23 \times 10^{-14}$
1,000	$3.66 \times 10^{-14}$

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\*Initial activity of Pu-241 is  $4.76 \times 10^{-14} \mu\text{Ci/cc}$

Ref. (1) AMENDMENT VI Table 5.3-3

第 2.3 - 27 表

DOSE CONVERSION FACTORS\* FOR EXPOSURE VIA INGESTION OF WATER  
TO RADIOACTIVE MATERIALS RELEASED FROM THE CRBRP RADWASTE SYSTEMS  
mrem/yr per  $\mu\text{Ci/cc}$

<u>Isotope</u>	<u>Whole Body</u>	<u>Bone</u>	<u>GI Tract**</u>	<u>Thyroid (adult)</u>	<u>Kidney</u>
H-3	$1.0 \times 10^5$	--	--	--	--
Na-22	$1.3 \times 10^7$	--	$5.0 \times 10^6$	--	--
Na-24	$1.3 \times 10^6$	--	$7.5 \times 10^6$	--	--
Cr-51	$2.5 \times 10^4$	--	$7.5 \times 10^5$	$3.0 \times 10^4$	$7.5 \times 10^3$
Mn-54	$6.3 \times 10^5$	--	$1.5 \times 10^7$	--	--
Fe-59	$2.5 \times 10^6$	$3.0 \times 10^6$	$3.0 \times 10^7$	--	--
Co-58	$1.3 \times 10^6$	--	$1.7 \times 10^7$	--	$2.1 \times 10^5$
Co-60	$5.0 \times 10^6$	--	$5.0 \times 10^7$	--	$5.0 \times 10^5$
Sr-89	$7.1 \times 10^6$	$1.7 \times 10^8$	$5.0 \times 10^7$	--	--
Sr-90	$1.3 \times 10^9$	$1.7 \times 10^9$	$3.8 \times 10^7$	--	--
Y-90	$1.7 \times 10^2$	$7.5 \times 10^3$	$7.5 \times 10^7$	--	--
Y-91	$2.5 \times 10^3$	$1.0 \times 10^5$	$5.0 \times 10^7$	--	--
Zr-95	$5.0 \times 10^3$	$1.5 \times 10^4$	$2.5 \times 10^7$	--	$7.5 \times 10^3$
Nb-95	$1.3 \times 10^3$	$4.3 \times 10^3$	$1.5 \times 10^7$	--	$2.5 \times 10^3$
Mo-99	$6.3 \times 10^5$	--	$3.8 \times 10^7$	--	$7.5 \times 10^6$

(Continued)

第 2.3 - 2 7 表 (Continued)

mrem/yr per  $\mu\text{Ci/cc}$

<u>Isotope</u>	<u>Whole Body</u>	<u>Bone</u>	<u>GI Tract**</u>	<u>Thyroid (adult)</u>	<u>Kidney</u>
Ru-103	$6.3 \times 10^4$	$1.5 \times 10^5$	$1.9 \times 10^7$	--	$5.0 \times 10^5$
Ru-106	$2.5 \times 10^5$	$3.0 \times 10^6$	$1.5 \times 10^8$	--	$3.8 \times 10^6$
Rh-106	NA	--	--	--	--
Ag-111	$1.0 \times 10^4$	$5.0 \times 10^4$	$3.8 \times 10^7$	--	$7.5 \times 10^4$
Sb-125	$2.5 \times 10^5$	$1.5 \times 10^6$	$1.5 \times 10^7$	$1.5 \times 10^3$	--
Te-129	$1.0 \times 10^4$	$3.0 \times 10^4$	$1.9 \times 10^7$	$3.0 \times 10^4$	$1.5 \times 10^5$
Te-129m	$2.5 \times 10^6$	$1.0 \times 10^7$	$7.5 \times 10^7$	$3.8 \times 10^6$	$3.8 \times 10^7$
Te-132	$1.0 \times 10^6$	$1.5 \times 10^6$	$7.5 \times 10^7$	$1.5 \times 10^6$	$7.5 \times 10^6$
I-131	$2.5 \times 10^6$	--	$1.5 \times 10^6$	$1.5 \times 10^9$	--
I-132	$1.3 \times 10^5$	--	$3.8 \times 10^6$	$5.0 \times 10^7$	--
Cs-134	$5.6 \times 10^7$	$4.3 \times 10^7$	$3.0 \times 10^6$	--	$3.8 \times 10^7$
Cs-136	$5.6 \times 10^6$	$3.0 \times 10^6$	$1.9 \times 10^6$	--	$5.0 \times 10^6$
Cs-137	$2.5 \times 10^7$	$6.0 \times 10^7$	$1.9 \times 10^6$	--	$3.0 \times 10^7$
Ba-140	$1.0 \times 10^6$	$1.5 \times 10^7$	$7.5 \times 10^7$	--	$5.0 \times 10^3$
La-140	$2.5 \times 10^2$	$1.5 \times 10^3$	$7.5 \times 10^7$	--	--
Ce-141	$5.0 \times 10^2$	$6.0 \times 10^3$	$1.7 \times 10^7$	--	$2.1 \times 10^3$
Ce-144	$1.7 \times 10^4$	$3.8 \times 10^5$	$1.5 \times 10^8$	--	$7.5 \times 10^4$

(Continued)

第 2.3 - 2 7 表 (Continued)

mrem/yr per  $\mu\text{Ci/cc}$

Isotope	Whole Body	Bone	GI Tract**	Thyroid (adult)	Kidney
Pr-143	$5.0 \times 10^2$	$7.5 \times 10^3$	$3.0 \times 10^7$	--	$1.7 \times 10^3$
Pr-144	NA	--	--	--	--
Nd-147	$5.0 \times 10^2$	$5.0 \times 10^3$	$2.5 \times 10^7$	--	$3.0 \times 10^3$
Pm-147	$2.5 \times 10^3$	$6.0 \times 10^4$	$7.5 \times 10^6$	--	$7.5 \times 10^3$
Eu-155	$5.0 \times 10^3$	$3.8 \times 10^4$	$7.5 \times 10^6$	--	$2.1 \times 10^4$
Ta-182	$7.1 \times 10^3$	$1.5 \times 10^4$	$3.8 \times 10^7$	--	$2.1 \times 10^4$
Pu-238	$1.3 \times 10^7$	$6.0 \times 10^8$	$5.0 \times 10^7$	--	$5.0 \times 10^7$
Pu-239	$1.7 \times 10^7$	$6.0 \times 10^8$	$5.0 \times 10^7$	--	$7.5 \times 10^7$
Pu-240	$1.7 \times 10^7$	$6.0 \times 10^8$	$5.0 \times 10^7$	--	$7.5 \times 10^7$
Pu-241	$2.5 \times 10^5$	$1.5 \times 10^7$	$1.5 \times 10^6$	--	$1.5 \times 10^6$
Pu-242	$1.3 \times 10^7$	$6.0 \times 10^8$	$5.0 \times 10^7$	--	$5.0 \times 10^7$

★ Calculated from data tabulated in Table 5.3 A - 4 (第 2.3 - 5 0 表), maximum permissible dose :  
 maximum permissible concentration in water,  $\left(\frac{MFD}{MPC_w}\right)$

\*\*MPC for insoluble compounds used for all elements except I<sub>2</sub>, Cs and Na. CRBRP releases of I<sub>2</sub>, Cs and Na will be in soluble form only.

NA - Not available

第 2.3 - 2 8 表

ESTIMATED RADIATION DOSE TO THE PUBLIC VIA  
DIRECT RADIATION FROM THE CRBRP

<u>Distance From Plant (miles)</u>	<u>Estimated Dose Rate (mrem/yr)</u>
0.4	$6.3 \times 10^{-1}$
0.6	$9.0 \times 10^{-2}$
1.0	$2.6 \times 10^{-3}$
2.0	$7.6 \times 10^{-7}$
3.0	$2.8 \times 10^{-10}$
4.0	$1.6 \times 10^{-13}$
5.0	$6.8 \times 10^{-17}$

Population Dose within 5 miles of Site =  
0.02 man-rem/year

Ref. (1) Table 5.3-4

第 2.3 - 2 9 表

ESTIMATED EXTERNAL TOTAL BODY DOSES TO TRANSPORT WORKERS AND THE GENERAL PUBLIC FROM SHIPPING UNIRRADIATED MATERIALS TO CRBRP SITE

<u>Material*</u>	<u>Total Miles Per Year</u>	<u>Man-rems Received Per Year</u>	
		<u>Transport Workers</u>	<u>General Population</u>
Fresh fuel			
Radial blanket	9,750	0.062	0.015
Fresh fuel			
Core and axial blanket	24,750	1.8	0.41
Total		1.9	0.43

\*These packages meet all DOT limits on external dose rates

Ref. (1) AMENDMENT VI Table 5.3-5

第 2.3 - 3 0 表

ESTIMATED EXTERNAL TOTAL BODY DOSES TO TRANSPORT WORKERS AND THE GENERAL PUBLIC FROM SHIPPING IRRADIATED MATERIALS FROM THE CRBRP SITE

<u>Material</u>	<u>Total Miles Per Year</u>	<u>Man-rem's Received Per Year</u>	
		<u>Transport Workers</u>	<u>General Population</u>
Spent fuel			
Core and axial blanket	9,000	1.02	0.15
Radial blanket	2,250	0.26	0.04
Radwaste	7,925	0.16	0.04
<b>Total</b>		<u>1.44</u>	<u>0.23</u>

Ref. (1) AMENDMENT VI Table 5.3-6



第 2.3 - 3 1 表

SUMMARY OF INDIVIDUAL AND POPULATION DOSES  
FROM EXPOSURE TO THE CRBRP

Exposure Pathway	Individual		Population*	
	External Total Body (mrem/yr)	Internal Whole Body (mrem/yr)	External Total Body (man-rem/yr)	Internal Whole Body (man-rem/yr)
Gaseous Effluents	$2.3 \times 10^{-2}$	$5.6 \times 10^{-1}$	$2.7 \times 10^{-2}$	
Liquid Effluents	$7.2 \times 10^{-7}$	$1.9 \times 10^{-2}$	$3.7 \times 10^{-8}$	$3.9 \times 10^{-3}$
Direct Radiation	$6.3 \times 10^{-1}$	--	$2.0 \times 10^{-2}$	--
Transportation of Fuel and Radwaste	--	--	$6.6 \times 10^{-1}$	--
Total	$6.5 \times 10^{-1}$	$5.8 \times 10^{-1}$	$7.1 \times 10^{-1}$	$3.9 \times 10^{-3}$
Percent of Natural Radiation**	$6.5 \times 10^{-1}$	$3.2 \times 10^0$	$7.2 \times 10^{-4}$	$2.2 \times 10^{-5}$

\*Population is 987,314 as projected for 2010 in Section 2.2

\*\*External natural background for Eastern Tennessee is 100 mrem/yr. Internal natural background is 18 mrem/yr.

+This value is very conservatively calculated since it does not include allowance for shielding provided by the four-foot thick concrete confinement structure.

第 2.3 - 3 2 表

SUMMARY OF POTENTIAL DOSES FROM PLANT ACCIDENTS  
 MINIMUM EXCLUSION DISTANCE - 2200 FEET\*  
 mrem/event

Accident Number	Skin	Whole Body	Bone	Lung	Thyroid
2.1	$5.24 \times 10^{-2}$	$1.77 \times 10^0$	--	$1.77 \times 10^0$	$1.77 \times 10^0$
3.1	$2.78 \times 10^7$	$9.35 \times 10^{-6}$	--	$9.35 \times 10^{-6}$	$9.35 \times 10^{-6}$
3.2	$1.11 \times 10^{-6}$	$3.74 \times 10^{-5}$	--	$3.74 \times 10^{-5}$	$3.74 \times 10^{-5}$
3.3	$1.73 \times 10^1$	$1.52 \times 10^1$	--	$6.18 \times 10^{-6}$	$6.18 \times 10^{-6}$
3.4	$1.08 \times 10^0$	$5.05 \times 10^{-1}$	--	$2.42 \times 10^{-4}$	$2.42 \times 10^{-4}$
4.1	$3.97 \times 10^{-2}$	$1.44 \times 10^1$	$2.05 \times 10^2$	$1.13 \times 10^1$	$6.32 \times 10^1$
4.2	$6.89 \times 10^{-2}$	$1.50 \times 10^1$	$2.19 \times 10^2$	$1.18 \times 10^1$	$9.13 \times 10^0$
5.1	$3.50 \times 10^{-4}$	$3.40 \times 10^{-4}$	--	--	--
5.2	$6.27 \times 10^{-4}$	$2.11 \times 10^{-2}$	--	$2.11 \times 10^{-2}$	$2.11 \times 10^{-2}$
6.1	$1.78 \times 10^{-3}$	$1.54 \times 10^{-2}$	$1.35 \times 10^{-2}$	--	$6.28 \times 10^0$
6.2	$1.78 \times 10^{-1}$	$1.54 \times 10^0$	$1.35 \times 10^0$	--	$6.28 \times 10^2$
6.3	$1.09 \times 10^{-1}$	$6.74 \times 10^{-2}$	--	--	--
7.1	$8.46 \times 10^{-1}$	$9.26 \times 10^{-3}$	--	--	--
8.1	$2.70 \times 10^{-3}$	$9.70 \times 10^{-1}$	$1.40 \times 10^1$	$7.60 \times 10^{-1}$	$4.30 \times 10^0$
8.2	$5.35 \times 10^{-2}$	$8.30 \times 10^{-1}$	$5.61 \times 10^{-1}$	$3.10 \times 10^{-1}$	$4.93 \times 10^{-1}$
8.3	$4.94 \times 10^{-3}$	$1.78 \times 10^0$	$2.54 \times 10^1$	$1.40 \times 10^0$	$7.85 \times 10^0$
8.4	$9.80 \times 10^{-4}$	$2.10 \times 10^{-1}$	$3.10 \times 10^0$	$1.70 \times 10^{-1}$	$1.30 \times 10^{-1}$
8.5	$5.70 \times 10^{-2}$	$1.90 \times 10^0$	--	$1.90 \times 10^0$	$1.90 \times 10^0$
10CFR20 (mrem/yr)	--	$5.00 \times 10^2$	--	--	$1.50 \times 10^3$
10CFR100 (mrem/event)	--	$2.50 \times 10^4$	$1.50 \times 10^{5**}$	$7.50 \times 10^{4**}$	$3.00 \times 10^5$

\* Shortest distance from containment to the far bank of the Clinch River (Site Boundary)

\*\* Not covered in 10CFR100; used as guideline values

Ref. (1) AMENDMENT VII Table 7.1-5

第 2.3 - 3 3 表

SUMMARY OF POTENTIAL DOSES FROM PLANT ACCIDENTS  
DOWNWIND DISTANCE - 0.6 MILE\*  
mrem/event

Accident Number	Skin	Whole Body	Bone	Lung	Thyroid
2.1	$2.98 \times 10^{-2}$	$1.01 \times 10^0$	--	$1.01 \times 10^0$	$1.01 \times 10^0$
3.1	$1.53 \times 10^{-7}$	$5.31 \times 10^{-6}$	--	$5.31 \times 10^{-6}$	$5.31 \times 10^{-6}$
3.2	$6.30 \times 10^{-7}$	$2.12 \times 10^{-5}$	--	$2.12 \times 10^{-5}$	$2.12 \times 10^{-5}$
3.3	$9.83 \times 10^0$	$8.63 \times 10^0$	--	$3.51 \times 10^{-5}$	$3.51 \times 10^{-6}$
3.4	$6.13 \times 10^{-1}$	$2.87 \times 10^{-1}$	--	$1.37 \times 10^{-4}$	$1.37 \times 10^{-4}$
4.1	$2.25 \times 10^{-2}$	$8.18 \times 10^0$	$1.16 \times 10^2$	$6.42 \times 10^0$	$3.59 \times 10^1$
4.2	$3.91 \times 10^{-2}$	$8.52 \times 10^0$	$1.24 \times 10^2$	$6.70 \times 10^0$	$5.19 \times 10^0$
5.1	$1.99 \times 10^{-4}$	$1.93 \times 10^{-4}$	--	--	--
5.2	$3.56 \times 10^{-4}$	$1.20 \times 10^{-2}$	--	$1.20 \times 10^{-2}$	$1.20 \times 10^{-2}$
6.1	$1.01 \times 10^{-3}$	$8.75 \times 10^{-3}$	$7.67 \times 10^{-3}$	--	$3.57 \times 10^0$
6.2	$1.01 \times 10^{-1}$	$8.75 \times 10^{-1}$	$7.67 \times 10^{-1}$	--	$3.57 \times 10^2$
6.3	$6.19 \times 10^{-2}$	$3.83 \times 10^{-2}$	--	--	--
7.1	$4.81 \times 10^{-1}$	$5.26 \times 10^{-3}$	--	--	--
8.1	$1.53 \times 10^{-3}$	$5.51 \times 10^{-1}$	$7.95 \times 10^0$	$4.32 \times 10^{-1}$	$2.44 \times 10^0$
8.2	$3.05 \times 10^{-2}$	$4.73 \times 10^{-1}$	$3.19 \times 10^{-1}$	$1.76 \times 10^{-1}$	$2.84 \times 10^{-1}$
8.3	$2.83 \times 10^{-3}$	$1.01 \times 10^0$	$1.44 \times 10^1$	$7.95 \times 10^{-1}$	$4.46 \times 10^0$
8.4	$5.57 \times 10^{-4}$	$1.19 \times 10^{-1}$	$1.76 \times 10^0$	$9.66 \times 10^{-2}$	$7.38 \times 10^{-2}$
8.5	$3.24 \times 10^{-2}$	$1.08 \times 10^0$	--	$1.08 \times 10^0$	$1.08 \times 10^0$
10CFR20 (mrem/yr)	--	$5.00 \times 10^2$	--	--	$1.50 \times 10^3$
10CFR100 (mrem/event)	--	$2.50 \times 10^4$	$1.50 \times 10^5$	$7.50 \times 10^4$	$3.00 \times 10^5$

\* Nearest Residence

Ref. (1) AMENDMENT VIII Table 7.1-6

第 2.3 - 3 4 表

SUMMARY OF POTENTIAL DOSES FROM PLANT ACCIDENTS  
DOWNWIND DISTANCE - 1 MILE\*  
mrem/event

Accident Number	Skin	Whole Body	Bone	Lung	Thyroid
2.1	$2.47 \times 10^{-2}$	$8.34 \times 10^{-1}$	--	$8.34 \times 10^{-1}$	$8.34 \times 10^{-1}$
3.1	$1.31 \times 10^{-7}$	$4.41 \times 10^{-6}$	--	$4.40 \times 10^{-6}$	$4.40 \times 10^{-6}$
3.2	$5.23 \times 10^{-7}$	$1.76 \times 10^{-5}$	--	$1.76 \times 10^{-5}$	$1.76 \times 10^{-5}$
3.3	$8.15 \times 10^0$	$7.16 \times 10^0$	--	$2.91 \times 10^{-6}$	$2.91 \times 10^{-5}$
3.4	$5.09 \times 10^{-1}$	$2.38 \times 10^{-1}$	--	$1.14 \times 10^{-4}$	$1.14 \times 10^{-4}$
4.1	$1.87 \times 10^{-2}$	$6.78 \times 10^0$	$9.66 \times 10^1$	$5.32 \times 10^0$	$2.98 \times 10^1$
4.2	$3.25 \times 10^{-2}$	$7.07 \times 10^0$	$1.03 \times 10^2$	$5.56 \times 10^0$	$4.30 \times 10^0$
5.1	$1.65 \times 10^{-4}$	$1.60 \times 10^{-4}$	--	--	--
5.2	$2.95 \times 10^{-4}$	$9.94 \times 10^{-3}$	--	$9.94 \times 10^{-3}$	$9.94 \times 10^{-3}$
6.1	$8.38 \times 10^{-4}$	$7.25 \times 10^{-3}$	$6.36 \times 10^{-3}$	--	$2.96 \times 10^0$
6.2	$8.38 \times 10^{-2}$	$7.25 \times 10^{-1}$	$6.36 \times 10^{-1}$	--	$2.96 \times 10^2$
6.3	$5.13 \times 10^{-2}$	$3.17 \times 10^{-2}$	--	--	--
7.1	$3.98 \times 10^{-1}$	$4.36 \times 10^{-3}$	--	--	--
8.1	$1.27 \times 10^{-3}$	$4.57 \times 10^{-1}$	$6.59 \times 10^0$	$3.58 \times 10^{-1}$	$2.03 \times 10^0$
8.2	$1.41 \times 10^{-2}$	$2.18 \times 10^{-1}$	$1.48 \times 10^{-1}$	$8.15 \times 10^{-2}$	$1.30 \times 10^{-1}$
8.3	$2.33 \times 10^{-3}$	$8.38 \times 10^{-1}$	$1.20 \times 10^1$	$6.59 \times 10^{-1}$	$3.70 \times 10^0$
8.4	$4.62 \times 10^{-4}$	$9.89 \times 10^{-2}$	$1.46 \times 10^0$	$8.01 \times 10^{-2}$	$6.12 \times 10^{-2}$
8.5	$2.68 \times 10^{-2}$	$8.95 \times 10^{-1}$	--	$8.95 \times 10^{-1}$	$8.95 \times 10^{-1}$
10CFR20 (mrem/yr)	--	$5.00 \times 10^2$	--	--	$1.50 \times 10^3$
10CFR100 (mrem/event)	--	$2.50 \times 10^4$	$1.50 \times 10^5$	$7.50 \times 10^4$	$3.00 \times 10^5$

\* Nearest Recreational Area

Ref. (1) AMENDMENT VIII Table 7.1-7

第 2.3 - 3 5 表

SUMMARY OF POTENTIAL DOSES FROM PLANT ACCIDENTS  
DOWNWIND DISTANCE - 2.5 MILES\*  
mrem/event

Accident Number	Skin	Whole Body	Bone	Lung	Thyroid
2.1	$1.38 \times 10^{-2}$	$4.67 \times 10^{-1}$	--	$4.67 \times 10^{-1}$	$4.67 \times 10^{-1}$
3.1	$7.34 \times 10^{-8}$	$2.47 \times 10^{-6}$	--	$2.47 \times 10^{-6}$	$2.47 \times 10^{-6}$
3.2	$2.93 \times 10^{-7}$	$9.87 \times 10^{-6}$	--	$9.87 \times 10^{-6}$	$9.87 \times 10^{-6}$
3.3	$4.57 \times 10^0$	$4.01 \times 10^0$	--	$1.63 \times 10^{-6}$	$1.63 \times 10^{-6}$
3.4	$2.85 \times 10^{-1}$	$1.33 \times 10^{-1}$	--	$6.39 \times 10^{-5}$	$6.39 \times 10^{-5}$
4.1	$1.05 \times 10^{-2}$	$3.80 \times 10^0$	$5.41 \times 10^1$	$2.98 \times 10^0$	$1.67 \times 10^1$
4.2	$1.82 \times 10^{-2}$	$3.96 \times 10^0$	$5.78 \times 10^1$	$3.12 \times 10^0$	$2.41 \times 10^0$
5.1	$9.24 \times 10^{-5}$	$8.98 \times 10^{-5}$	--	--	--
5.2	$1.66 \times 10^{-4}$	$5.57 \times 10^{-3}$	--	$5.57 \times 10^{-3}$	$5.57 \times 10^{-3}$
6.1	$4.70 \times 10^{-4}$	$4.07 \times 10^{-3}$	$3.56 \times 10^{-3}$	--	$1.66 \times 10^0$
6.2	$4.70 \times 10^{-2}$	$4.07 \times 10^{-1}$	$3.56 \times 10^{-1}$	--	$1.66 \times 10^2$
6.3	$2.88 \times 10^{-2}$	$1.78 \times 10^{-2}$	--	--	--
7.1	$2.23 \times 10^{-1}$	$2.44 \times 10^{-3}$	--	--	--
8.1	$7.13 \times 10^{-4}$	$2.56 \times 10^{-1}$	$3.70 \times 10^0$	$2.01 \times 10^{-1}$	$1.14 \times 10^0$
8.2	$3.63 \times 10^{-3}$	$5.64 \times 10^{-2}$	$3.80 \times 10^{-2}$	$2.10 \times 10^{-2}$	$3.34 \times 10^{-2}$
8.3	$1.30 \times 10^{-3}$	$4.70 \times 10^{-1}$	$6.71 \times 10^0$	$3.70 \times 10^{-1}$	$2.07 \times 10^0$
8.4	$2.59 \times 10^{-4}$	$5.54 \times 10^{-2}$	$8.18 \times 10^{-1}$	$4.49 \times 10^{-2}$	$3.43 \times 10^{-2}$
8.5	$1.50 \times 10^{-2}$	$5.02 \times 10^{-1}$	--	$5.02 \times 10^{-1}$	$5.02 \times 10^{-1}$
10CFR20 (mrem/yr)	--	$5.00 \times 10^2$	--	--	$1.50 \times 10^3$
10CFR100 (mrem/event)	--	$2.50 \times 10^4$	$1.50 \times 10^5$	$7.50 \times 10^4$	$3.00 \times 10^5$

\* Low Population Zone (LPZ)

Ref. (1) AMENDMENT VIII Table 7.1-8

第 2.3 - 3 6 表

SUMMARY OF POTENTIAL DOSES FROM PLANT ACCIDENTS  
DOWNWIND DISTANCE - 4 MILES\*  
mrem/event

Accident Number	Skin	Whole Body	Bone	Lung	Thyroid
2.1	$7.18 \times 10^{-3}$	$2.42 \times 10^{-1}$	--	$2.42 \times 10^{-1}$	$2.42 \times 10^{-1}$
3.1	$3.81 \times 10^{-8}$	$1.28 \times 10^{-6}$	--	$1.28 \times 10^{-6}$	$1.28 \times 10^{-6}$
3.2	$1.52 \times 10^{-7}$	$5.12 \times 10^{-6}$	--	$5.12 \times 10^{-6}$	$5.12 \times 10^{-6}$
3.3	$2.37 \times 10^0$	$2.08 \times 10^0$	--	$8.47 \times 10^{-7}$	$8.47 \times 10^{-7}$
3.4	$1.48 \times 10^{-1}$	$6.92 \times 10^{-2}$	--	$3.32 \times 10^{-5}$	$3.32 \times 10^{-5}$
4.1	$5.44 \times 10^{-3}$	$1.97 \times 10^0$	$2.81 \times 10^1$	$1.55 \times 10^0$	$8.66 \times 10^0$
4.2	$9.44 \times 10^{-3}$	$2.06 \times 10^0$	$3.00 \times 10^1$	$1.62 \times 10^0$	$1.25 \times 10^0$
5.1	$4.80 \times 10^{-5}$	$4.65 \times 10^{-5}$	--	--	--
5.2	$8.59 \times 10^{-5}$	$2.89 \times 10^{-3}$	--	$2.89 \times 10^{-3}$	$2.89 \times 10^{-3}$
6.1	$2.44 \times 10^{-4}$	$2.11 \times 10^{-3}$	$1.85 \times 10^{-3}$	--	$3.60 \times 10^{-1}$
6.2	$2.44 \times 10^{-2}$	$2.11 \times 10^{-1}$	$1.85 \times 10^{-1}$	--	$8.60 \times 10^1$
6.3	$1.49 \times 10^{-2}$	$9.23 \times 10^{-3}$	--	--	--
7.1	$1.16 \times 10^{-1}$	$1.27 \times 10^{-3}$	--	--	--
8.1	$3.70 \times 10^{-4}$	$1.33 \times 10^{-1}$	$1.92 \times 10^0$	$1.04 \times 10^{-1}$	$5.89 \times 10^{-1}$
8.2	$1.89 \times 10^{-3}$	$2.92 \times 10^{-2}$	$1.98 \times 10^{-2}$	$1.09 \times 10^{-2}$	$1.74 \times 10^{-2}$
8.3	$6.77 \times 10^{-4}$	$2.44 \times 10^{-1}$	$3.48 \times 10^0$	$1.92 \times 10^{-1}$	$1.08 \times 10^0$
8.4	$1.34 \times 10^{-4}$	$2.88 \times 10^{-2}$	$4.25 \times 10^{-1}$	$2.33 \times 10^{-2}$	$1.78 \times 10^{-2}$
8.5	$7.81 \times 10^{-3}$	$2.60 \times 10^{-1}$	--	$2.60 \times 10^{-1}$	$2.60 \times 10^{-1}$
10CFR20 (mrem/yr)	--	$5.00 \times 10^2$	--	--	$1.50 \times 10^3$
10CFR100 (mrem/event)	--	$2.50 \times 10^4$	$1.50 \times 10^5$	$7.50 \times 10^4$	$3.00 \times 10^5$

\* Nearest Dairy

Ref. (1) AMENDMENT VIII Table 7.1-9

第 2.3 - 3 7 表

SUMMARY OF POTENTIAL DOSES FROM PLANT ACCIDENTS  
DOWNWIND DISTANCE - 7 MILES\*  
mrem/event

Accident Number	Skin	Whole Body	Bone	Lung	Thyroid
2.1	$3.56 \times 10^{-3}$	$1.20 \times 10^{-1}$	--	$1.20 \times 10^{-1}$	$1.20 \times 10^{-1}$
3.1	$1.89 \times 10^{-8}$	$6.36 \times 10^{-7}$	--	$6.36 \times 10^{-7}$	$6.36 \times 10^{-7}$
3.2	$7.55 \times 10^{-8}$	$2.54 \times 10^{-6}$	--	$2.54 \times 10^{-6}$	$2.54 \times 10^{-6}$
3.3	$1.18 \times 10^0$	$1.03 \times 10^0$	--	$4.20 \times 10^{-7}$	$4.20 \times 10^{-7}$
3.4	$7.34 \times 10^{-2}$	$3.43 \times 10^{-2}$	--	$1.65 \times 10^{-5}$	$1.65 \times 10^{-5}$
4.1	$2.70 \times 10^{-3}$	$9.79 \times 10^{-1}$	$1.39 \times 10^{+1}$	$7.68 \times 10^{-1}$	$4.30 \times 10^0$
4.2	$4.69 \times 10^{-3}$	$1.02 \times 10^0$	$1.45 \times 10^{+1}$	$8.02 \times 10^{-1}$	$6.21 \times 10^{-1}$
5.1	$2.38 \times 10^{-5}$	$2.31 \times 10^{-5}$	--	--	--
5.2	$4.26 \times 10^{-5}$	$1.43 \times 10^{-3}$	--	$1.43 \times 10^{-3}$	$1.43 \times 10^{-3}$
6.1	$1.21 \times 10^{-4}$	$1.05 \times 10^{-3}$	$9.18 \times 10^{-4}$	--	$4.27 \times 10^{-3}$
6.2	$1.21 \times 10^{-2}$	$1.05 \times 10^{-1}$	$9.18 \times 10^{-2}$	--	$4.27 \times 10^{+1}$
6.3	$7.41 \times 10^{-3}$	$4.58 \times 10^{-2}$	--	--	--
7.1	$5.75 \times 10^{-2}$	$6.30 \times 10^{-4}$	--	--	--
8.1	$1.84 \times 10^{-4}$	$6.60 \times 10^{-2}$	$9.52 \times 10^{-1}$	$5.17 \times 10^{-2}$	$2.92 \times 10^{-1}$
8.2	$6.70 \times 10^{-4}$	$1.35 \times 10^{-2}$	$9.12 \times 10^{-3}$	$5.04 \times 10^{-3}$	$8.02 \times 10^{-3}$
8.3	$3.36 \times 10^{-4}$	$1.21 \times 10^{-1}$	$1.73 \times 10^0$	$9.52 \times 10^{-2}$	$5.34 \times 10^{-1}$
8.4	$6.66 \times 10^{-5}$	$1.43 \times 10^{-2}$	$2.11 \times 10^{-1}$	$1.16 \times 10^{-2}$	$8.84 \times 10^{-3}$
8.5	$3.88 \times 10^{-3}$	$1.29 \times 10^{-1}$	--	$1.29 \times 10^{-1}$	$1.29 \times 10^{-1}$
10CFR20 (mrem/yr)	--	$5.00 \times 10^{+2}$	--	--	$1.57 \times 10^{+3}$
10CFR100 (mrem/event)	--	$2.50 \times 10^{+4}$	$1.50 \times 10^{+5}$	$7.50 \times 10^{+4}$	$3.00 \times 10^{+5}$

\*Nearest Population Center > 2,500 (Kingston)

Ref. (1) AMENDMENT VII Table 7.1-10

第 2.3 - 3 8 表

SUMMARY OF POTENTIAL DOSES FROM PLANT ACCIDENTS  
DOWNWIND DISTANCE - 21 MILES\*  
mrem/event

Accident Number	Skin	Whole Body	Bone	Lung	Thyroid
2.1	$9.43 \times 10^{-4}$	$3.19 \times 10^{-2}$	--	$3.19 \times 10^{-2}$	$3.19 \times 10^{-2}$
3.1	$5.00 \times 10^{-9}$	$1.68 \times 10^{-7}$	--	$1.68 \times 10^{-7}$	$1.68 \times 10^{-7}$
3.2	$2.00 \times 10^{-8}$	$6.73 \times 10^{-7}$	--	$6.73 \times 10^{-7}$	$6.73 \times 10^{-7}$
3.3	$3.11 \times 10^{-1}$	$2.74 \times 10^{-1}$	--	$1.11 \times 10^{-7}$	$1.11 \times 10^{-7}$
3.4	$1.94 \times 10^{-2}$	$9.09 \times 10^{-3}$	--	$4.36 \times 10^{-6}$	$4.36 \times 10^{-6}$
4.1	$7.15 \times 10^{-4}$	$2.59 \times 10^{-1}$	$3.69 \times 10^0$	$2.03 \times 10^{-1}$	$1.14 \times 10^0$
4.2	$1.24 \times 10^{-3}$	$2.70 \times 10^{-1}$	$3.94 \times 10^0$	$2.12 \times 10^{-1}$	$1.64 \times 10^{-1}$
5.1	$6.30 \times 10^{-6}$	$6.12 \times 10^{-6}$	--	--	--
5.2	$1.13 \times 10^{-5}$	$3.80 \times 10^{-4}$	--	$3.80 \times 10^{-4}$	$3.80 \times 10^{-4}$
6.1	$3.20 \times 10^{-5}$	$2.77 \times 10^{-4}$	$2.43 \times 10^{-4}$	--	$1.13 \times 10^{-1}$
6.2	$3.20 \times 10^{-3}$	$2.77 \times 10^{-2}$	$2.43 \times 10^{-2}$	--	$1.13 \times 10^{+1}$
6.3	$1.96 \times 10^{-3}$	$1.21 \times 10^{-3}$	--	--	--
7.1	$1.52 \times 10^{-2}$	$1.57 \times 10^{-4}$	--	--	--
8.1	$4.86 \times 10^{-5}$	$1.75 \times 10^{-2}$	$2.52 \times 10^{-1}$	$1.37 \times 10^{-2}$	$7.74 \times 10^{-2}$
8.2	$2.14 \times 10^{-4}$	$3.33 \times 10^{-3}$	$2.25 \times 10^{-3}$	$1.24 \times 10^{-3}$	$1.98 \times 10^{-3}$
8.3	$8.89 \times 10^{-5}$	$3.20 \times 10^{-2}$	$4.57 \times 10^{-1}$	$2.52 \times 10^{-2}$	$1.41 \times 10^{-1}$
8.4	$1.76 \times 10^{-5}$	$3.78 \times 10^{-3}$	$5.58 \times 10^{-2}$	$3.06 \times 10^{-3}$	$2.34 \times 10^{-3}$
8.5	$1.03 \times 10^{-3}$	$3.42 \times 10^{-2}$	--	$3.42 \times 10^{-2}$	$3.42 \times 10^{-2}$
10CFR20 (mrem/yr)	--	$5.00 \times 10^{+2}$	--	--	$1.50 \times 10^{+3}$
10CFR100 (mrem/event)	--	$2.50 \times 10^{+4}$	$1.50 \times 10^{+5}$	$7.50 \times 10^{+4}$	$3.00 \times 10^{+5}$

\*Nearest Population Center > 100,000 (Knoxville)

Ref. (1) AMENDMENT VIII Table 7.1-11



第 2.3 - 3 9 表

SUMMARY OF POTENTIAL DOSES FROM PLANT ACCIDENTS  
DOWNWIND DISTANCE - 50 MILES  
mrem/event

<u>Accident Number</u>	<u>Skin</u>	<u>Whole Body</u>	<u>Bone</u>	<u>Lung</u>	<u>Thyroid</u>
2.1	$4.72 \times 10^{-4}$	$1.59 \times 10^{-2}$	--	$1.59 \times 10^{-2}$	$1.59 \times 10^{-2}$
3.1	$2.50 \times 10^{-9}$	$8.42 \times 10^{-8}$	--	$8.42 \times 10^{-8}$	$8.42 \times 10^{-8}$
3.2	$9.99 \times 10^{-9}$	$3.37 \times 10^{-7}$	--	$3.37 \times 10^{-7}$	$3.37 \times 10^{-7}$
3.3	$1.56 \times 10^{-1}$	$1.37 \times 10^{-1}$	--	$5.56 \times 10^{-8}$	$5.56 \times 10^{-8}$
3.4	$9.72 \times 10^{-3}$	$4.55 \times 10^{-3}$	--	$2.18 \times 10^{-6}$	$2.18 \times 10^{-6}$
4.1	$3.57 \times 10^{-4}$	$1.30 \times 10^{-1}$	$1.85 \times 10^0$	$1.02 \times 10^{-1}$	$5.69 \times 10^{-1}$
4.2	$6.20 \times 10^{-4}$	$1.35 \times 10^{-1}$	$1.97 \times 10^0$	$1.06 \times 10^{-1}$	$8.22 \times 10^{-2}$
5.1	$3.15 \times 10^{-6}$	$3.06 \times 10^{-6}$	--	--	--
5.2	$5.64 \times 10^{-6}$	$1.90 \times 10^{-4}$	--	$1.90 \times 10^{-4}$	$1.90 \times 10^{-4}$
6.1	$1.60 \times 10^{-5}$	$1.39 \times 10^{-4}$	$1.22 \times 10^{-4}$	--	$5.65 \times 10^{-2}$
6.2	$1.60 \times 10^{-3}$	$1.39 \times 10^{-2}$	$1.22 \times 10^{-2}$	--	$5.65 \times 10^0$
6.3	$9.81 \times 10^{-4}$	$6.07 \times 10^{-4}$	--	--	--
7.1	$7.61 \times 10^{-3}$	$8.33 \times 10^{-5}$	--	--	--
8.1	$2.43 \times 10^{-5}$	$8.73 \times 10^{-3}$	$1.26 \times 10^{-1}$	$6.84 \times 10^{-3}$	$3.87 \times 10^{-2}$
8.2	$8.48 \times 10^{-5}$	$1.32 \times 10^{-3}$	$8.89 \times 10^{-4}$	$4.91 \times 10^{-4}$	$7.81 \times 10^{-4}$
8.3	$4.45 \times 10^{-5}$	$1.60 \times 10^{-2}$	$2.29 \times 10^{-1}$	$1.26 \times 10^{-2}$	$7.07 \times 10^{-2}$
8.4	$8.82 \times 10^{-6}$	$1.89 \times 10^{-3}$	$2.79 \times 10^{-2}$	$1.53 \times 10^{-3}$	$1.17 \times 10^{-3}$
8.5	$5.13 \times 10^{-4}$	$1.71 \times 10^{-2}$	--	$1.71 \times 10^{-2}$	$1.71 \times 10^{-2}$
10CFR20 (mrem/yr)	--	$5.00 \times 10^{+2}$	--	--	$1.50 \times 10^{+3}$
10CFR100 (mrem/event)	--	$2.50 \times 10^{+4}$	$1.50 \times 10^{+5}$	$7.50 \times 10^{+4}$	$3.00 \times 10^{+5}$

Ref.(1) AMENDMENT VIII Table 7.1-12

第 2.3 - 4 0 表

ATMOSPHERIC DILUTION FACTORS  
50 PERCENT PROBABILITY  $\chi/Q$  VALUES ( $\text{sec}/\text{m}^3$ )\*

<u>Distance (miles)</u>	<u>TIME INTERVAL</u>			
	<u>0-8 Hours</u>	<u>8-24 Hours</u>	<u>1-4 Days</u>	<u>4-30 Days</u>
0.42	$7.45 \times 10^{-4}$	$3.79 \times 10^{-4}$	$2.51 \times 10^{-4}$	$1.52 \times 10^{-4}$
0.5	$5.55 \times 10^{-4}$	$2.85 \times 10^{-4}$	$1.82 \times 10^{-4}$	$1.20 \times 10^{-4}$
0.6	$4.23 \times 10^{-4}$	$2.00 \times 10^{-4}$	$1.29 \times 10^{-4}$	$8.85 \times 10^{-5}$
0.7	$3.95 \times 10^{-4}$	$1.56 \times 10^{-4}$	$1.01 \times 10^{-4}$	$6.80 \times 10^{-5}$
1.0	$3.51 \times 10^{-4}$	$9.00 \times 10^{-5}$	$5.63 \times 10^{-5}$	$3.93 \times 10^{-5}$
1.5	$3.29 \times 10^{-4}$	$4.78 \times 10^{-5}$	$3.28 \times 10^{-5}$	$2.04 \times 10^{-5}$
2.0	$2.88 \times 10^{-4}$	$3.07 \times 10^{-5}$	$2.00 \times 10^{-5}$	$1.35 \times 10^{-5}$
2.5	$1.97 \times 10^{-4}$	$2.10 \times 10^{-5}$	$1.33 \times 10^{-5}$	$9.00 \times 10^{-6}$
3.0	$1.61 \times 10^{-4}$	$2.70 \times 10^{-5}$	$1.07 \times 10^{-5}$	$7.30 \times 10^{-6}$
3.5	$1.28 \times 10^{-4}$	$1.29 \times 10^{-5}$	$8.15 \times 10^{-6}$	$5.78 \times 10^{-6}$
4.0	$1.02 \times 10^{-4}$	$1.08 \times 10^{-5}$	$6.90 \times 10^{-6}$	$4.67 \times 10^{-6}$
4.5	$9.05 \times 10^{-5}$	$8.85 \times 10^{-6}$	$5.75 \times 10^{-6}$	$3.93 \times 10^{-6}$
5.0	$7.90 \times 10^{-5}$	$7.80 \times 10^{-6}$	$5.00 \times 10^{-6}$	$3.39 \times 10^{-6}$
7.0	$5.05 \times 10^{-5}$	$4.83 \times 10^{-6}$	$3.09 \times 10^{-6}$	$2.12 \times 10^{-6}$
7.5	$4.50 \times 10^{-5}$	$4.35 \times 10^{-6}$	$2.80 \times 10^{-6}$	$1.93 \times 10^{-6}$
9.0	$3.66 \times 10^{-5}$	$3.41 \times 10^{-6}$	$2.26 \times 10^{-6}$	$1.49 \times 10^{-6}$
10.0	$3.25 \times 10^{-5}$	$2.98 \times 10^{-6}$	$1.99 \times 10^{-6}$	$1.31 \times 10^{-6}$
15.0	$2.00 \times 10^{-5}$	$1.75 \times 10^{-6}$	$1.15 \times 10^{-6}$	$7.70 \times 10^{-7}$
20.0	$1.51 \times 10^{-5}$	$1.23 \times 10^{-6}$	$7.85 \times 10^{-7}$	$5.42 \times 10^{-7}$
21.0	$1.37 \times 10^{-5}$	$1.16 \times 10^{-6}$	$7.40 \times 10^{-7}$	$5.10 \times 10^{-7}$
25.0	$1.17 \times 10^{-5}$	$9.25 \times 10^{-7}$	$5.99 \times 10^{-7}$	$4.12 \times 10^{-7}$
35.0	$8.55 \times 10^{-6}$	$6.40 \times 10^{-7}$	$4.15 \times 10^{-7}$	$2.78 \times 10^{-7}$
45.0	$7.05 \times 10^{-6}$	$4.85 \times 10^{-7}$	$3.10 \times 10^{-7}$	$2.11 \times 10^{-7}$
50.0	$6.50 \times 10^{-6}$	$4.28 \times 10^{-7}$	$2.73 \times 10^{-7}$	$1.91 \times 10^{-7}$

\* See Section 2.6.

Ref. (1) AMENDMENT VII Table 7.1-1

第 2.3 - 4 1 表

NINETY-FIFTY AND FIFTIETH PERCENTILE  $\chi/Q$  VALUES FOR VARIOUS DOWNWIND DISTANCES  
 33-FT WIND SPEED AND DIRECTION: 200-FT TO 75-FT DELTA T  
 WIND MEANDER FACTOR OF 4 USED WHEN APPLICABLE  
 BUILDING WAKE FACTOR USED WHEN APPLICABLE  
 DATA FROM JULY 1, 1975 THROUGH JUNE 30, 1976

Distance (Miles)	95th Percentile $\chi/Q$ Values (sec/m <sup>3</sup> )					50th Percentile $\chi/Q$ Values (sec/m <sup>3</sup> )				
	0-1 hr	0-8 hr	8-24 hr	1-4 day	4-30 day	0-1 hr	0-8 hr	8-24 hr	1-4 day	4-30 day
0.1	3.48E-2	1.25E-2	5.55E-3	3.00E-3	2.00E-3	1.71E-2	2.40E-3	1.21E-3	7.65E-4	8.40E-4
0.2	1.08E-2	3.85E-3	1.53E-3	8.70E-4	5.85E-4	5.45E-3	7.55E-4	3.55E-4	2.25E-4	2.45E-4
0.3	5.51E-3	2.00E-3	7.80E-4	4.30E-4	2.50E-4	2.78E-3	3.89E-4	1.70E-4	1.05E-4	1.19E-4
0.42	3.12E-3	1.11E-3	4.50E-4	2.30E-4	1.58E-4	1.56E-3	2.20E-4	9.60E-5	6.00E-5	6.45E-5
0.5	2.32E-3	8.40E-4	3.39E-4	1.75E-4	1.17E-4	1.17E-3	1.67E-4	7.10E-5	4.45E-5	4.95E-5
0.6	1.79E-3	6.40E-4	2.50E-4	1.30E-4	8.50E-5	8.50E-4	1.24E-4	5.30E-5	3.13E-5	3.58E-5
0.7	1.71E-3	5.90E-4	1.87E-4	9.90E-5	6.60E-5	8.50E-4	1.20E-4	4.30E-5	2.40E-5	2.70E-5
1.0	1.07E-3*	3.31E-4*	1.09E-4	5.65E-5	3.78E-5	7.60E-4*	1.10E-4*	2.25E-5	1.38E-5	1.53E-5
1.5	1.45E-4*	5.11E-4*	5.70E-5	2.97E-5	1.38E-5	7.20E-4*	1.04E-4*	1.26E-5	7.90E-6	8.55E-6
2.0	1.21E-4	4.26E-4	3.75E-5	1.91E-5	1.30E-5	6.11E-4	8.40E-5	7.50E-6	4.70E-6	5.15E-6
2.5	8.25E-4	2.65E-4	2.65E-5	1.30E-5	8.70E-6	4.11E-4	5.90E-5	5.35E-6	3.45E-6	3.70E-6
3.0	6.90E-4	2.47E-4	1.90E-5	1.4E-5	7.00E-6	3.38E-4	4.60E-5	4.30E-6	2.60E-6	2.95E-6
3.5	5.50E-4	1.87E-4	1.56E-5	8.70E-6	5.45E-6	2.60E-4	3.85E-5	2.30E-6	2.10E-6	2.32E-6
4.0	4.30E-4	1.48E-4	1.30E-5	6.65E-6	4.50E-6	2.22E-4	3.15E-5	2.75E-6	1.78E-6	1.94E-6
4.5	3.80E-4	1.40E-4	1.04E-5	5.60E-6	3.85E-6	1.88E-4	2.70E-5	2.30E-6	1.46E-6	1.60E-6
5.0	3.31E-4	1.18E-4	9.00E-6	4.90E-6	3.22E-6	1.66E-4	2.39E-5	2.02E-6	1.26E-6	1.40E-6
7.0	2.20E-4	7.30E-5	5.60E-6	3.10E-6	2.03E-6	1.06E-4	1.59E-5	1.25E-6	7.80E-7	8.45E-7
7.5	1.98E-4	7.10E-5	5.10E-6	2.78E-6	1.87E-6	9.50E-5	1.38E-5	1.17E-6	7.10E-7	8.10E-7
9.0	1.53E-4	5.25E-5	3.95E-6	2.19E-6	1.44E-6	7.60E-5	1.08E-5	8.80E-7	5.45E-7	6.15E-7
10.0	1.43E-4	5.10E-5	3.45E-6	1.88E-6	1.26E-6	5.75E-5	1.00E-5	7.75E-7	4.75E-7	5.33E-7
15.0	8.70E-5	2.92E-5	2.06E-6	1.14E-6	7.35E-7	4.20E-5	6.05E-6	4.40E-7	2.75E-7	3.17E-7
20.0	6.70E-5	2.11E-5	1.43E-6	7.75E-7	5.40E-7	3.07E-5	4.35E-6	3.27E-7	1.96E-7	2.20E-7
25.0	5.90E-5	1.98E-5	1.33E-6	7.25E-7	4.90E-7	2.86E-5	4.10E-6	2.91E-7	1.61E-7	2.05E-7
25.0	5.35E-5	1.69E-5	1.09E-6	5.80E-7	4.00E-7	2.48E-5	3.39E-6	2.38E-7	1.44E-7	1.64E-7
35.0	3.59E-5	1.24E-5	7.55E-7	4.00E-7	2.70E-7	1.84E-5	2.50E-6	1.55E-7	9.90E-8	1.14E-7
45.0	3.07E-5	1.00E-5	5.65E-7	3.02E-7	2.07E-7	1.49E-5	2.03E-6	1.19E-7	7.35E-8	8.55E-8
50.0	2.80E-5	9.30E-6	5.50E-7	2.77E-7	1.85E-7	1.38E-5	1.87E-6	1.06E-7	6.60E-8	7.60E-8

\*These  $\chi/Q$  values replace the ones in Table 2.6-38 to account for gradual change in  $\chi/Q$  values after wind meander factor is removed.

第 2.3 - 4 2 表

RATIOS OF 50 PERCENTILE  $\chi/Q$  VALUES FROM  
TABLE 7.1-1 (第 2.3 - 4 0 表) TO THE 50 PERCENTILE  
 $\chi/Q$  VALUES FROM TABLE 2.6-38A (第 2.3 - 4 1 表)

DISTANCE (Miles)	0-8 hr	8.24 hr	1-4 day	4-30 day
0.1	3.44	3.87	4.25	2.50
0.2	3.40	3.92	4.09	2.49
0.3	3.36	3.90	4.28	2.49
0.42	3.39	3.95	4.18	2.32
0.5	3.32	4.01	4.09	2.42
0.6	3.41	3.77	4.12	2.47
0.7	3.29	3.90	4.21	2.42
1.0	3.19	4.00	4.05	2.47
1.5	3.16	3.79	4.15	2.39
2.0	3.42	3.86	4.26	2.47
2.5	3.34	3.93	3.86	2.43
3.0	3.50	3.95	4.00	2.49
3.5	3.32	3.91	3.88	2.49
4.0	3.24	3.93	3.88	2.41
4.5	3.35	3.85	3.94	2.46
5.0	3.31	3.86	3.97	2.42
7.0	3.18	3.86	3.96	2.48
7.5	3.26	3.72	3.94	2.38
9.0	3.39	3.88	4.15	2.42
10.0	3.25	3.85	4.19	2.46
15.0	3.31	3.98	4.18	2.43
20.0	3.47	3.76	4.01	2.46
21.0	3.34	3.99	4.09	2.49
25.0	3.46	3.89	4.16	2.51
35.0	3.42	4.13	4.19	2.44
45.0	3.47	4.08	4.22	2.47
50.0	3.48	3.96	4.14	2.51

Ref. (1) AMENDMENT VII Table 7.1-1A

第 2.3 - 4 3 表

SUMMARY OF POTENTIAL WHOLE BODY POPULATION DOSES FROM PLANT ACCIDENTS  
Whole Body Population Dose

<u>Accident Number</u>	<u>Minimum Estimate (Man-rem)</u>	<u>Maximum Estimate (Man-rem)</u>
2.1	$4.74 \times 10^{-1}$	$7.77 \times 10^0$
3.1	$2.51 \times 10^{-6}$	$4.10 \times 10^{-5}$
3.2	$1.00 \times 10^{-5}$	$1.64 \times 10^{-4}$
3.3	$4.08 \times 10^0$	$6.67 \times 10^{+1}$
3.4	$1.36 \times 10^{-1}$	$2.22 \times 10^0$
4.1	$3.90 \times 10^0$	$6.30 \times 10^{+1}$
4.2	$4.03 \times 10^0$	$6.58 \times 10^{+1}$
5.1	$9.11 \times 10^{-5}$	$1.49 \times 10^{-3}$
5.2	$5.67 \times 10^{-3}$	$9.26 \times 10^{-2}$
6.1	$4.13 \times 10^{-3}$	$6.76 \times 10^{-2}$
6.2	$4.13 \times 10^{-1}$	$6.76 \times 10^0$
6.3	$1.80 \times 10^{-2}$	$2.96 \times 10^{-1}$
7.1	$2.49 \times 10^{-3}$	$4.06 \times 10^{-2}$
8.1	$2.60 \times 10^{-1}$	$4.26 \times 10^0$
8.2	$2.23 \times 10^{-1}$	$3.64 \times 10^0$
8.3	$4.77 \times 10^{-1}$	$7.85 \times 10^0$
8.4	$5.63 \times 10^{-2}$	$9.21 \times 10^{-1}$
8.5	$5.09 \times 10^{-1}$	$8.34 \times 10^0$

Ref. (1) AMENDMENT VIII Table 7.1-13

第 2.3 - 4 4 表

ESTIMATED\* SODIUM HYDROXIDE RELEASES FOR REPRESENTATIVE POTENTIAL FIRE ACCIDENTS

<u>Accident No.**</u>	<u>Description</u>	<u>Duration</u>	<u>Average Concentration (mg/m<sup>3</sup>)</u>	<u>Peak Concentration (mg/m<sup>3</sup>)</u>
4.1	Failure of ex-containment primary sodium drain pipe during maintenance	2 minutes	1.73	2.54
5.2	Steam generator tube rupture	15 seconds	7.95	--
8.1	Primary sodium in-containment drain tank failure during maintenance	145 hours	$3 \times 10^{-7}$	$7.3 \times 10^{-5}$

\*Estimated sodium hydroxide levels at the closest Site boundary

\*\*Refer to accident numbering in Section 7.1

Ref.(1) AMENDMENT VIII Table 7.2-2

## 第 2.3 - 4 5 表

## AVERAGE ENERGY PER DISINTEGRATION

<u>Isotope</u>	<u>Beta (MeV)</u>	<u>Gamma (MeV)</u>
H-3	0.006	0
C-14	0.052	0
Na-22	0.182	2.195
Na-24	0.463	4.123
Ne-23	1.460	0.160
Ar-39	0.188	0
Ar-41	0.406	1.280
Mn-54	0.00021	0.835
Co-58	0.0237	0.977
Co-60	0.105	2.51
Kr-83m	0.036	0.00248
Kr-85m	0.277	0.158
Kr-85	0.230	0.002
Kr-87	1.324	0.793
Kr-88	0.376	1.950
Sr-89	0.488	0.000082
Sr-90	0.182	0.0
Y-90	0.930	0.0
Y-91	0.515	0.0036
Zr-95	0.130	0.725
Nb-95	0.0532	0.765
Ru-103	0.077	0.474
Ru-106	0.013	0.0
Sb-125	0.335	0.121
Te-129m	0.621	0.0414
Te-129	0.407	0.108
Te-132	0.10	0.216

(Continued)

第 2.3 - 4 5 表 (Continued)

<u>Isotope</u>	<u>Beta (MeV)</u>	<u>Gamma (MeV)</u>
I-131	0.197	0.371
I-132	0.448	2.40
Xe-131m	0.143	0.02
Xe-133m	0.189	0.042
Xe-133	0.135	0.045
Xe-135m	0.095	0.432
Xe-135	0.316	0.247
Xe-138	0.612	1.183
Cs-134	0.166	1.59
Cs-136	0.139	2.23
Cs-137	0.246	0.563
Ba-140	0.284	0.236
La-140	0.397	2.12
Ce-141	0.315	0.0695
Ce-144	0.101	0.0163
Pr-143	0.310	0.0
Nd-147	0.335	0.122
Pm-147	0.070	0.0

Ref. (1) AMENDMENT VIII Table 7.1-2



第 2.3 - 4 6 表

INHALATION DOSE CONVERSION FACTORS,  $F_i$   
rem/Ci Inhaled\*

<u>Isotope</u>	<u>Lung</u>	<u>Bone</u>	<u>Thyroid</u>	<u>Whole Body</u>
H-3	$1.34 \times 10^2$	--	$1.34 \times 10^2$	$1.34 \times 10^2$
Na-22	$1.30 \times 10^4$	$1.30 \times 10^4$	$1.30 \times 10^4$	$1.30 \times 10^4$
Na-24	$1.69 \times 10^3$	$1.69 \times 10^3$	$1.69 \times 10^3$	$1.69 \times 10^3$
Mn-54	$1.75 \times 10^5$	--	--	$7.87 \times 10^2$
Co-58	$1.16 \times 10^5$	--	--	$2.59 \times 10^2$
Co-60	$7.47 \times 10^5$	--	--	$1.85 \times 10^3$
Sr-89	$1.75 \times 10^5$	$3.80 \times 10^4$	--	$1.09 \times 10^3$
Sr-90	$1.20 \times 10^6$	$1.24 \times 10^7$	--	$7.62 \times 10^5$
Y-90	$2.12 \times 10^4$	$2.61 \times 10^2$	--	$7.01 \times 10^0$
Y-91	$2.13 \times 10^5$	$5.78 \times 10^4$	--	$1.55 \times 10^3$
Zr-95	$2.22 \times 10^5$	$1.34 \times 10^4$	--	$2.91 \times 10^3$
Nb-95	$6.32 \times 10^4$	$1.76 \times 10^3$	--	$5.26 \times 10^2$
Ru-103	$6.32 \times 10^4$	$1.91 \times 10^2$	--	$8.23 \times 10^1$
Ru-106	$1.18 \times 10^6$	$8.64 \times 10^3$	--	$1.09 \times 10^3$
Sb-125	$2.75 \times 10^5$	$8.26 \times 10^3$	$7.34 \times 10^0$	$1.66 \times 10^3$
Te-129M	$1.45 \times 10^5$	$1.22 \times 10^3$	$4.30 \times 10^2$	$1.98 \times 10^2$
Te-129	$2.42 \times 10^2$	$6.22 \times 10^{-3}$	$4.87 \times 10^{-3}$	$1.55 \times 10^{-3}$
Te-132	$3.60 \times 10^4$	$3.25 \times 10^2$	$2.37 \times 10^1$	$2.02 \times 10^1$
I-131	--	$3.15 \times 10^3$	$1.49 \times 10^6$	$2.56 \times 10^3$
I-132	--	$1.45 \times 10^2$	$5.48 \times 10^4$	$1.45 \times 10^2$
I-133	--	$1.08 \times 10^3$	$3.66 \times 10^5$	$5.67 \times 10^2$
I-134	--	$8.06 \times 10^1$	$2.87 \times 10^4$	$7.70 \times 10^1$
I-135	--	$3.36 \times 10^2$	$1.17 \times 10^5$	$3.22 \times 10^2$
Cs-134	$1.22 \times 10^4$	$4.67 \times 10^4$	--	$9.11 \times 10^4$
Cs-136	$1.50 \times 10^3$	$4.89 \times 10^3$	--	$1.39 \times 10^4$

(Continued)

第 2.3 - 4 6 表 (Continued)

<u>Isotope</u>	<u>Lung</u>	<u>Bone</u>	<u>Thyroid</u>	<u>Whole Body</u>
Cs-137	$9.41 \times 10^3$	$5.98 \times 10^4$	--	$5.36 \times 10^4$
Bu-140	$1.59 \times 10^5$	$4.88 \times 10^3$	--	$3.21 \times 10^2$
La-140	$1.70 \times 10^4$	$4.30 \times 10^1$	--	$5.73 \times 10^0$
Ce-141	$4.52 \times 10^4$	$2.49 \times 10^3$	--	$1.91 \times 10^2$
Ce-144	$9.73 \times 10^5$	$4.29 \times 10^5$	--	$2.30 \times 10^4$
Pr-143	$3.51 \times 10^4$	$1.17 \times 10^3$	--	$5.79 \times 10^1$
Pr-144	$1.27 \times 10^2$	$3.76 \times 10^{-3}$	--	$1.91 \times 10^{-4}$
Nd-147	$2.76 \times 10^4$	$6.59 \times 10^2$	--	$4.56 \times 10^1$
Pm-147	$6.61 \times 10^4$	$8.37 \times 10^4$	--	$3.18 \times 10^3$
Pu-238	$1.76 \times 10^8$	$2.69 \times 10^9$	--	$6.66 \times 10^7$
Pu-239	$1.67 \times 10^8$	$3.05 \times 10^9$	--	$7.53 \times 10^7$
Pu-240	$1.67 \times 10^8$	$3.04 \times 10^9$	--	$7.53 \times 10^7$
Pu-241	$1.52 \times 10^5$	$6.05 \times 10^7$	--	$1.29 \times 10^6$
Pu-242	$1.59 \times 10^8$	$2.89 \times 10^9$	--	$7.17 \times 10^7$

\* From Table C-1, Reg. Guide 1.109

Ref. (1) AMENDMENT VIII Table 7.1-3

第 2.3 - 4 7 表

POPULATION DISTRIBUTION AND WIND FREQUENCY FOR THE ENE AND NNW SECTORS\*

Radial Interval (miles)	Population Within Radial Interval	
	ENE $f_k = 0.104^{**}$	NNW $f_k = 0.0392^{**}$
0-1	5	0
1-2	5	0
2-3	0	0
3-4	0	0
4-5	0	75
5-10	224	1,539
10-20	27,890	3,035
20-30	189,115	990
30-40	45,135	4,235
40-50	14,180	2,230

\*Population distribution is the projected distribution for census year 2010

\*\*Refer following table

Ref. (1) AMENDMENT VII Table 7.1-4

ANNUAL JOINT FREQUENCY OF WIND DIRECTION AND WIND SPEED FOR  
ALL STABILITY CLASSES  
CRBRP METEOROLOGICAL TOWER, 33-FOOT LEVEL  
JULY 1, 1975 THROUGH JUNE 30, 1976

	WIND SPEED, KNOTS*								Total
	0.0-1.3	1.4-2.9	3.0-4.7	4.8-6.4	6.5-10.0	10.1-16.0	16.1-21.0	21.1-99.0	
N	0.01257	0.01116	0.00219	0.00046	0.00012	0.00000	0.00000	0.00000	0.02649
NNE	0.01089	0.01496	0.00288	0.00058	0.00023	0.00000	0.00000	0.00000	0.02953
NE	0.01939	0.01922	0.01105	0.00288	0.00046	0.00000	0.00000	0.00000	0.05299
ENE	0.03578	0.02106	0.01277	0.00598	0.00207	0.00000	0.00000	0.00000	0.07767
E	0.04536	0.01588	0.00794	0.00322	0.00000	0.00000	0.00000	0.00000	0.07240
ESE	0.05912	0.01208	0.00702	0.00115	0.00000	0.00000	0.00000	0.00000	0.07937
SE	0.05780	0.00806	0.00334	0.00058	0.00012	0.00000	0.00000	0.00000	0.06988
SSE	0.02513	0.01036	0.00311	0.00058	0.00000	0.00000	0.00000	0.00000	0.03917
S	0.01927	0.00967	0.00426	0.00092	0.00092	0.00000	0.00000	0.00000	0.03503
SSW	0.01580	0.01542	0.00990	0.00644	0.00449	0.00035	0.00000	0.00000	0.05239
SW	0.01699	0.03682	0.00337	0.02359	0.01876	0.00173	0.00000	0.00000	0.13126
WSW	0.01269	0.03452	0.03441	0.01369	0.00783	0.00115	0.00000	0.00000	0.10428
W	0.01280	0.01300	0.01289	0.00587	0.00288	0.00012	0.00000	0.00000	0.04756
WNW	0.01352	0.01254	0.01530	0.01692	0.01128	0.00046	0.00000	0.00000	0.07002
NW	0.01987	0.01577	0.00852	0.00426	0.00380	0.00000	0.00000	0.00000	0.05220
NNW	0.03040	0.02002	0.00610	0.00219	0.00104	0.00000	0.00000	0.00000	0.05974
TOTAL	0.40736	0.27054	0.17503	0.08930	0.05397	0.00380	0.00000	0.00000	1.00000

\* 1 knot = 0.515 m/sec, 1 knot = 1.16 mph

Note: The total frequency of calms for this stability is 0.01565. Calms are distributed proportionally in the 0.0-1.3 knot wind speed group above.

第 2.3 - 4 8 表

MAXIMUM PERMISSIBLE CONCENTRATION IN AIR (MPC<sub>a</sub>)\* FOR CONTINUOUS EXPOSURE TO RADIONUCLIDES RELEASED FROM THE CRBRP GASEOUS RADWASTE SYSTEM<sup>(50)</sup>++

Isotope	Whole Body ( $\mu\text{Ci/cc}$ )
H-3	$3 \times 10^{-6}$
Ne-23	$3 \times 10^{-7+}$
Ar-39	$1 \times 10^{-9+}$
Ar-41	$4 \times 10^{-7+}$
Kr-83m	$3 \times 10^{-7+}$
Kr-85	$3 \times 10^{-6**}$
Kr-85m	$1 \times 10^{-6**}$
Kr-87	$2 \times 10^{-7**}$
Kr-88	$2 \times 10^{-7+}$
Xe-131m	$4 \times 10^{-6**}$
Xe-133	$3 \times 10^{-6**}$
Xe-133m	$3 \times 10^{-6+}$
Xe-135	$1 \times 10^{-6**}$
Xe-135m	$1 \times 10^{-9+}$
Xe-138	$3 \times 10^{-7+}$

\*MPC<sub>a</sub> for soluble compounds

\*\*MPC<sub>a</sub> in 10CFR20, Table II, column 1 are based upon a maximum permissible dose of 1/10 of the occupational exposure levels reported in ICRP-2<sup>(50)</sup>

+MPC<sub>a</sub> is calculated from data presented in 10CFR20, Table II, column 1

++Used to calculate Table 5.3A-3 (第 2.3 - 4 9 表)

Ref.(1) AMENDMENT VIII Table 5.3A-2

第 2.3 - 4 9 表

DOSE CONVERSION FACTORS\* FOR EXPOSURE TO RADIOACTIVE MATERIALS RELEASED FROM THE CPBRP GASEOUS WASTE SYSTEM

<u>Isotope</u>	<u>Whole Body**</u> <u>(mrem/yr per <math>\mu</math>Ci/cc)</u>
H-3	$1.7 \times 10^9$
Ne-23	$1.7 \times 10^{10}$
Ar-39	$5.0 \times 10^{12}$
Ar-41	$1.7 \times 10^{10}$
Kr-83m	$1.7 \times 10^{10}$
Kr-81	$1.7 \times 10^9$
Kr-85m	$5.0 \times 10^9$
Kr-87	$2.5 \times 10^{10}$
Kr-88	$2.5 \times 10^{10}$
Xe-131m	$1.3 \times 10^9$
Xe-133	$1.7 \times 10^9$
Xe-133m	$1.7 \times 10^9$
Xe-135	$5.0 \times 10^9$
Xe-135m	$5.0 \times 10^{12}$
Xe-138	$1.7 \times 10^{10}$

\*Calculated from data tabulated in Table 5.3A-2, maximum permissible dose (as provided in reference 5)  $\div$  maximum permissible concentration in air,  $\frac{MPD}{MPC_a}$  (第 2.3 - 4 8 表)

\*\*Except for tritium, dose conversion factors for noble and inert gases are considered = 0. for inhalation pathway. The values given represent constants which would be used to calculate an external submersion dose.

Ref. (1) AMENDMENT VIII Table 5.2A-3

第 2.3 - 5 0 表

MAXIMUM PERMISSIBLE CONCENTRATION IN WATER, MPC<sub>w</sub>, FOR CONTINUOUS EXPOSURE  
TO RADIONUCLIDES RELEASED FROM THE CRBRP RADWASTE SYSTEMS<sup>(50)</sup>

μCi/cc

Isotope	Whole Body	Bone	GI Tract**	Thyroid (adult)	Kidney
H-3	$5 \times 10^{-2}$	--	--	--	--
Na-22	$4 \times 10^{-4+}$	--	$3 \times 10^{-3}$	--	--
Na-24	$4 \times 10^{-3}$	--	$2 \times 10^{-3+}$	--	--
Cr-51	$2 \times 10^{-1}$	--	$2 \times 10^{-2+}$	$1 \times 10^0$	$2 \times 10^0$
Mn-54	$8 \times 10^{-3}$	--	$1 \times 10^{-3+}$	--	--
Fe-59	$2 \times 10^{-3}$	$1 \times 10^{-2}$	$5 \times 10^{-4+}$	--	--
Co-58	$4 \times 10^{-3}$	--	$9 \times 10^{-4+}$	--	$7 \times 10^{-2}$
Co-60	$1 \times 10^{-3}$	--	$3 \times 10^{-4+}$	--	$3 \times 10^{-2}$
Sr-89	$7 \times 10^{-4}$	$1.8 \times 10^{-4++}$	$3 \times 10^{-4}$	--	--
Sr-90	$4 \times 10^{-6}$	$1.8 \times 10^{-5++}$	$4 \times 10^{-4}$	--	--
Y-90	$3 \times 10^1$	$4 \times 10^0$	$2 \times 10^{-4+}$	--	--
Y-91	$2 \times 10^0$	$3 \times 10^{-1}$	$3 \times 10^{-4+}$	--	--
Zr-95	$1 \times 10^0$	$2 \times 10^0$	$6 \times 10^{-4+}$	--	$2 \times 10^0$
Nb-95	$4 \times 10^0$	$7 \times 10^0$	$1 \times 10^{-3+}$	--	$6 \times 10^0$

(Continued)

第 2.3 - 5 0 表 (Continued)

μCi/cc

<u>Isotope</u>	<u>Whole Body</u>	<u>Bone</u>	<u>GI Tract**</u>	<u>Thyroid (adult)</u>	<u>Kidney</u>
Mo-99	$8 \times 10^{-3}$	--	$4 \times 10^{-4}^+$	--	$2 \times 10^{-3}^+$
Ru-103	$8 \times 10^{-2}$	$2 \times 10^{-1}$	$8 \times 10^{-4}^+$	--	$3 \times 10^{-2}$
Ru-106	$2 \times 10^{-2}$	$1 \times 10^{-2}$	$1 \times 10^{-4}^+$	--	$4 \times 10^{-3}$
Rh-106	NA	--	--	--	--
Ag-111	$x 10^{-1}$	$6 \times 10^{-1}$	$4 \times 10^{-4}^+$	--	$2 \times 10^{-1}$
Sb-125	$2 \times 10^{-2}$	$2 \times 10^{-2}$	$1 \times 10^{-3}^+$	$2 \times 10^1$	--
Te-129	$5 \times 10^{-1}$	$1 \times 10^0$	$8 \times 10^{-3}^+$	$1 \times 10^0$	$1 \times 10^{-1}$
Te-129m	$2 \times 10^{-3}$	$3 \times 10^{-3}$	$2 \times 10^{-4}^+$	$8 \times 10^{-3}$	$4 \times 10^{-4}$
Te-132	$5 \times 10^{-3}$	$2 \times 10^{-2}$	$2 \times 10^{-4}^+$	$2 \times 10^{-2}$	$2 \times 10^{-3}$
I-131	$2 \times 10^{-3}$	--	$1 \times 10^{-2}$	$2 \times 10^{-5}^{\nabla}$	--
I-132	$4 \times 10^{-2}$	--	$4 \times 10^{-3}$	$6 \times 10^{-4}^{\nabla}$	--
Cs-134	$9 \times 10^{-5}^+$	$7 \times 10^{-4}$	$5 \times 10^{-3}$	--	$4 \times 10^{-4}$
Cs-136	$9 \times 10^{-4}^+$	$1 \times 10^{-2}$	$8 \times 10^{-3}$	--	$3 \times 10^{-3}$
Cs-137	$2 \times 10^{-4}^+$	$5 \times 10^{-4}$	$8 \times 10^{-3}$	--	$5 \times 10^{-4}$
Ba-140	$5 \times 10^{-3}$	$2 \times 10^{-3}$	$2 \times 10^{-4}^+$	--	$3 \times 10^0$
La-140	$2 \times 10^1$	$2 \times 10^1$	$2 \times 10^{-4}^+$	--	--
Ce-141	$1 \times 10^1$	$5 \times 10^0$	$9 \times 10^{-4}^+$	--	$7 \times 10^0$
Ce-144	$3 \times 10^{-1}$	$8 \times 10^{-2}$	$1 \times 10^{-4}^+$	--	$2 \times 10^{-1}$

(Continued)



第 2.3 - 5 0 表 (Continued)

 $\mu\text{Ci/cc}$ 

Isotope	Whole Body	Bone	GI Tract**	Thyroid (adult)	Kidney
Pr-143	$1 \times 10^1$	$4 \times 10^0$	$5 \times 10^{-4}^+$	--	$9 \times 10^0$
Pr-144	NA	--	--	--	--
Nd-147	$1 \times 10^1$	$6 \times 10^0$	$6 \times 10^{-4}^+$	--	$5 \times 10^0$
Pm-147	$2 \times 10^0$	$5 \times 10^{-1}$	$2 \times 10^{-3}^+$	--	$2 \times 10^0$
Eu-155	$1 \times 10^0$	$8 \times 10^{-1}$	$2 \times 10^{-3}^+$	--	$7 \times 10^{-1}$
Ta-182	$7 \times 10^{-1}$	$2 \times 10^0$	$4 \times 10^{-4}^+$	--	$7 \times 10^{-1}$
Pu-238	$4 \times 10^{-4}$	$5 \times 10^{-5}^+$	$3 \times 10^{-4}$	--	$3 \times 10^{-4}$
Pu-239	$3 \times 10^{-4}$	$5 \times 10^{-5}^+$	$3 \times 10^{-4}$	--	$2 \times 10^{-4}$
Pu-240	$3 \times 10^{-4}$	$5 \times 10^{-5}^+$	$3 \times 10^{-4}$	--	$2 \times 10^{-4}$
Pu-241	$2 \times 10^{-2}$	$2 \times 10^{-3}^+$	$1 \times 10^{-2}$	--	$1 \times 10^{-2}$
Pu-242	$4 \times 10^{-4}$	$5 \times 10^{-5}^+$	$3 \times 10^{-4}$	--	$3 \times 10^{-4}$

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\*MPC<sub>w</sub> for soluble compounds

\*\*MPC for insoluble compounds used for all elements except I<sub>2</sub>, Cs and Na. CRBRP releases of I<sub>2</sub>, Cs and Na will be in soluble form only.

<sup>+</sup>MPC<sub>w</sub> in 10 CFR 20, Table II, column 2 is based upon a maximum permissible dose 1/10 of the occupational exposure levels reported in ICRP-2(50)

第 2.3 - 5 0 表 (Continued)

++Calculated from data presented in a report by Gamertsfelder, C. C., Statement on the Selection of as Low as Practicable Design Objectives and Technical Specifications for the Operation of Light Water Cooled Nuclear Power Reactors, U.S. AEC, Docket No. RM 50-2, Washington, D. C.

∇MPC<sub>w</sub> presented in 10 CFR 20, Table II, column 2 is based upon a maximum permissible dose of 1,500 mrem to a child thyroid. MPC<sub>w</sub> in above table is from ICRP-2.

NA - Not available.

Ref.(1) AMENDMENT IV Table 5.3A-4

第 2.3 - 5 1 表

WATER BODY WIDTH FACTORS FOR ESTIMATING GAMMA EXPOSURE  
FROM CONTAMINATED SEDIMENT<sup>(49)</sup>

<u>Width Factor</u>	<u>Exposure Situation</u>
0.1	Discharge canal bank
0.2	Riverbank
0.3	Lakeshore
0.5	Nominal ocean site
1.0	Tidal basin
2.0	Crustacea or shellfish

Ref. (1) Table 5.3A-11

第 2.3 - 5 2 表

ENVIRONMENTAL HALF-LIVES OF RADIOISOTOPES  
RELEASED FROM CRBRP RADWASTE SYSTEMS

<u>Isotope</u>	<u>Environmental Half-Life (Days)</u>
H-3	14.0
Na-22	13.4
Na-24	0.6
Ne-23	$4.4 \times 10^{-4}$
Ar-39	14.0
Ar-41	0.1
Cr-51	9.3
Mn-54	13.4
Fe-59	10.7
Co-58	11.7
Co-60	13.9
Kr-83m	0.1
Kr-85	14.0
Kr-85m	0.2
Kr-87	0.5
Kr-88	0.1
Sr-89	11.1
Sr-90	14.0
Y-90	2.2
Y-91	11.3
Zr-95	11.5
Nb-95	10.0
Mo-99	2.3
Ru-103	10.3
Ru-106	13.5

(Continued)

第 2.3 - 5 2 表 (Continued)

<u>Isotope</u>	<u>Environmental Half-Life (Days)</u>
Rh-106	$3.5 \times 10^{-4}$
Ag-111	4.9
Sb-125	13.3
Te-129	0.05
Te-129m	9.9
Te-132	2.6
I-131	5.1
I-132	0.1
Xe-131m	6.1
Xe-133	3.3
Xe-133m	1.9
Xe-135	5.6
Xe-135m	7.4
Xe-138	$1.0 \times 10^{-3}$
Cs-134	13.7
Cs-136	6.9
Cs-137	14.0
Ba-140	6.7
La-140	1.5
Ce-141	9.3
Ce-144	13.3
Pr-143	6.9
Pr-144	0.02
Nd-147	6.2
Pm-147	13.3
Eu-155	13.7
Ta-182	14.0

(Continued)

第 2.3 - 5 2 表 (Continued)

<u>Isotope</u>	<u>Environmental Half-Life (Days)</u>
Pu-238	14.0
Pu-239	14.0
Pu-240	14.0
Pu-241	14.0
Pu-242	14.0

Ref. (1) AMENDMENT IV Table 5.3A-6

第 2.3 - 5 3 表

DOSE CONVERSION FACTORS FOR TOTAL BODY AND SKIN EXPOSURE  
VIA IMMERSION IN WATER AND SHORELINE DEPOSITS<sup>(49)</sup>

Isotope	Immersion in Water		Shoreline Deposits	
	Total Body (mrem/hr per pCi/l)	Skin (mrem/hr per pCi/l)	Total Body (mrem/hr per pCi/m <sup>2</sup> )	Skin (mrem/hr per pCi/m <sup>2</sup> )
H-3	0	0	0	0
Na-22	$4.0 \times 10^{-6}$	$4.8 \times 10^{-6}$	$1.6 \times 10^{-8}$	$1.8 \times 10^{-8}$
Na-24	$7.8 \times 10^{-6}$	$9.3 \times 10^{-6}$	$2.5 \times 10^{-8}$	$2.9 \times 10^{-8}$
Ne-23	NA	NA	NA	NA
Ar-39	$6.2 \times 10^{-10}$	$1.3 \times 10^{-7}$	0	0
Ar-41	$2.4 \times 10^{-6}$	$3.2 \times 10^{-6}$	0	0
Cr-51	$5.2 \times 10^{-8}$	$6.4 \times 10^{-8}$	$2.2 \times 10^{-10}$	$2.6 \times 10^{-10}$
Mn-54	$1.5 \times 10^{-6}$	$1.8 \times 10^{-6}$	$5.8 \times 10^{-9}$	$6.8 \times 10^{-9}$
Fe-59	$2.2 \times 10^{-6}$	$2.9 \times 10^{-6}$	$8.0 \times 10^{-9}$	$9.4 \times 10^{-9}$
Co-58	$1.8 \times 10^{-6}$	$2.3 \times 10^{-6}$	$7.0 \times 10^{-9}$	$8.2 \times 10^{-9}$
Co-60	$4.6 \times 10^{-6}$	$5.4 \times 10^{-6}$	$1.7 \times 10^{-8}$	$2.0 \times 10^{-8}$
Kr-83m	$3.1 \times 10^{-9}$	$7.9 \times 10^{-9}$	0	0
Kr-85	$4.7 \times 10^{-9}$	$1.8 \times 10^{-7}$	0	0
Kr-85m	$2.8 \times 10^{-7}$	$5.1 \times 10^{-7}$	0	0
Kr-87	$2.7 \times 10^{-6}$	$4.6 \times 10^{-6}$	0	0
Kr-88	$3.3 \times 10^{-6}$	$4.1 \times 10^{-6}$	0	0
Sr-89	$4.6 \times 10^{-9}$	$5.4 \times 10^{-7}$	$5.6 \times 10^{-13}$	$6.5 \times 10^{-13}$
Sr-90	$5.4 \times 10^{-10}$	$1.5 \times 10^{-7}$	0	0
Y-90	$1.3 \times 10^{-8}$	$9.6 \times 10^{-7}$	$2.2 \times 10^{-12}$	$2.6 \times 10^{-12}$
Y-91	$9.1 \times 10^{-9}$	$5.6 \times 10^{-7}$	$2.4 \times 10^{-11}$	$2.7 \times 10^{-11}$
Zr-95	$1.5 \times 10^{-6}$	$1.8 \times 10^{-6}$	$5.0 \times 10^{-9}$	$5.8 \times 10^{-9}$
Nb-95	$1.4 \times 10^{-6}$	$1.6 \times 10^{-6}$	$5.1 \times 10^{-9}$	$6.0 \times 10^{-9}$
Mo-99*	$4.7 \times 10^{-7}$	$9.1 \times 10^{-7}$	$1.9 \times 10^{-9}$	$2.2 \times 10^{-9}$

(Continued)

第 2.3 - 5 3 表 (Continued)

Isotope	Immersion in Water		Shoreline Deposits	
	Total Body (mrem/hr per pCi/l)	Skin (mrem/hr per pCi/l)	Total Body (mrem/hr per pCi/m <sup>2</sup> )	Skin (mrem/hr per pCi/m <sup>2</sup> )
Ru-103*	$8.9 \times 10^{-7}$	$1.1 \times 10^{-6}$	$4.2 \times 10^{-9}$	$3.6 \times 10^{-9}$
Ru-106*	$3.8 \times 10^{-7}$	$1.9 \times 10^{-6}$	$1.8 \times 10^{-9}$	$1.5 \times 10^{-9}$
Rh-106	NA	NA	NA	NA
Ag-111	$4.8 \times 10^{-8}$	$3.8 \times 10^{-7}$	$2.1 \times 10^{-10}$	$1.8 \times 10^{-10}$
Sb-125	$7.8 \times 10^{-7}$	$9.5 \times 10^{-7}$	$3.1 \times 10^{-9}$	$3.5 \times 10^{-9}$
Te-129	$1.9 \times 10^{-7}$	$7.0 \times 10^{-7}$	$7.1 \times 10^{-10}$	$8.4 \times 10^{-10}$
Te-129m*	$2.1 \times 10^{-7}$	$7.4 \times 10^{-7}$	$7.7 \times 10^{-10}$	$9.0 \times 10^{-10}$
Te-132	$4.0 \times 10^{-7}$	$4.8 \times 10^{-7}$	$1.7 \times 10^{-9}$	$2.0 \times 10^{-9}$
I-131	$6.8 \times 10^{-7}$	$9.3 \times 10^{-7}$	$2.8 \times 10^{-9}$	$3.4 \times 10^{-9}$
I-132	$4.4 \times 10^{-6}$	$5.5 \times 10^{-6}$	$1.7 \times 10^{-8}$	$2.0 \times 10^{-8}$
Xe-131m	$6.2 \times 10^{-9}$	$5.6 \times 10^{-8}$	0	0
Xe-133	$5.7 \times 10^{-8}$	$1.1 \times 10^{-7}$	0	0
Xe-133m	$6.0 \times 10^{-8}$	$1.0 \times 10^{-7}$	0	0
Xe-135	$4.5 \times 10^{-7}$	$7.9 \times 10^{-7}$	0	0
Xe-135m	$7.6 \times 10^{-7}$	$1.0 \times 10^{-6}$	0	0
Xe-138	$2.6 \times 10^{-6}$	$3.4 \times 10^{-6}$	0	0
Cs-134	$2.9 \times 10^{-6}$	$3.5 \times 10^{-6}$	$1.2 \times 10^{-8}$	$1.4 \times 10^{-8}$
Cs-136	$5.6 \times 10^{-6}$	$4.9 \times 10^{-6}$	$1.5 \times 10^{-8}$	$1.7 \times 10^{-8}$
Cs-137	$1.0 \times 10^{-6}$	$1.4 \times 10^{-6}$	$4.2 \times 10^{-9}$	$4.9 \times 10^{-9}$
Ba-140	$4.9 \times 10^{-7}$	$7.6 \times 10^{-7}$	$2.1 \times 10^{-9}$	$2.4 \times 10^{-9}$
La-140	$4.1 \times 10^{-6}$	$5.3 \times 10^{-6}$	$1.5 \times 10^{-8}$	$1.7 \times 10^{-8}$
Ce-141	$1.3 \times 10^{-7}$	$2.4 \times 10^{-7}$	$5.5 \times 10^{-10}$	$6.2 \times 10^{-10}$
Ce-144*	$8.6 \times 10^{-8}$	$1.4 \times 10^{-6}$	$3.2 \times 10^{-10}$	$3.7 \times 10^{-10}$
Pr-143	$1.6 \times 10^{-9}$	$2.8 \times 10^{-7}$	0	0
Pr-144	$5.6 \times 10^{-7}$	$1.3 \times 10^{-6}$	$2.0 \times 10^{-10}$	$2.3 \times 10^{-10}$
Nd-147	$2.8 \times 10^{-7}$	$5.0 \times 10^{-7}$	$1.0 \times 10^{-9}$	$1.2 \times 10^{-9}$
Pm-147	$7.5 \times 10^{-11}$	$1.3 \times 10^{-8}$	0	0

(Continued)



第 2.3 - 5 3 表 (Continued)

Isotope	Immersion in Water		Shoreline Deposits	
	Total Body (mrem/hr per pCi/l)	Skin	Total Body (mrem/hr per pCi/m <sup>2</sup> )	Skin
Eu-155	NA	NA	NA	NA
Ta-182	NA	NA	NA	NA
Pu-238	$1.5 \times 10^{-10}$	$4.0 \times 10^{-9}$	$1.3 \times 10^{-12}$	$1.8 \times 10^{-11}$
Pu-239	$1.2 \times 10^{-10}$	$1.7 \times 10^{-9}$	$7.9 \times 10^{-13}$	$7.7 \times 10^{-12}$
Pu-240	$1.4 \times 10^{-10}$	$4.0 \times 10^{-9}$	$1.3 \times 10^{-12}$	$1.8 \times 10^{-11}$
Pu-241*	$6.1 \times 10^{-11}$	$9.5 \times 10^{-11}$	$4.6 \times 10^{-12}$	$6.8 \times 10^{-12}$
Pu-242	$1.1 \times 10^{-10}$	$3.6 \times 10^{-9}$	$1.1 \times 10^{-12}$	$1.6 \times 10^{-11}$

\*Includes contribution from daughter products

NA - Not available

Ref. (1) AMENDMENT IV Table 5.3A-7

第 2.3 - 5 4 表

EFFECTIVE HALF-LIVES<sup>(50)</sup> OF RADIOISOTOPES  
RELEASED FROM CRBRP RADWASTE SYSTEMS

<u>Isotope</u>	<u>Effective Half-Life (Days)</u>
H-3	12.0
Na-22	11.0
Na-24	NA
Ne-23	NA
Ar-39	NA
Ar-41	NA
Cr-51	26.6
Mn-54	5.6
Fe-59	42.7
Co-58	8.4
Co-60	$1.9 \times 10^3$
Kr-83m	NA
Kr-85	NA
Kr-85m	NA
Kr-87	NA
Kr-88	NA
Sr-89	50.3
Sr-90	$5.7 \times 10^3$
Y-90	2.7
Y-91	58.0
Zr-95	59.0
Nb-95	33.5
Mo-99	1.8

(Continued)

第 2.3 - 5 4 表 (Continued)

<u>Isotope</u>	<u>Effective Half-Life (Days)</u>
Ru-103	6.2
Ru-106	7.2
Rh-106	7.2
Ag-111	3.0
Sb-125	36.0
Te-129	$5.1 \times 10^{-2}$
Te-129m	10.0
Te-132	2.9
I-131	3.7
I-132	0.1
Xe-131m	NA
Xe-133	NA
Xe-133m	NA
Xe-135	NA
Xe-135m	NA
Xe-138	NA
Cs-134	65.0
Cs-136	11.0
Cs-137	70.0
Ba-140	4.2
La-140	1.7
Ce-141	30.0
Ce-144	$1.9 \times 10^2$
Pr-143	13.5
Pr-144	NA
Nd-147	11.1
Pm-147	$3.8 \times 10^2$
Eu-155	$3.1 \times 10^2$
Ta-182	76.0

(Continued)

第 2.3 - 5 4 表 (Continued)

<u>Isotope</u>	<u>Effective Half-Life (Days)</u>
Pu-238	$2.2 \times 10^4$
Pu-239	$6.4 \times 10^4$
Pu-240	$6.3 \times 10^4$
Pu-241	$4.5 \times 10^3$
Pu-242	$6.5 \times 10^4$

NA - Not available

Ref. (1) AMENDMENT VIII Table 5.3A-8

第 2.3 - 5 5 表

FRACTION OF INGESTED RADIOISOTOPE RETAINED IN THE WHOLE BODY  
OF AN ORGANISM FEEDING ON CONTAMINATED FOOD<sup>(50)</sup>

<u>Isotope</u>	<u>Fraction Retained</u>
H-3	1.0
Na-22	1.0
Na-24	1.0
Ne-23	1.0
Ar-39	1.0
Ar-41	1.0
Cr-51	0.005
Mn-54	0.1
Fe-59	0.013
Co-58	0.3
Co-60	0.3
Kr-83m	1.0
Kr-85	1.0
Kr-85m	1.0
Kr-87	1.0
Kr-88	1.0
Sr-89	0.3
Sr-90	0.3
Y-90	$1 \times 10^{-4}$
Y-91	$1 \times 10^{-4}$
Zr-95	$1 \times 10^{-4}$
Nb-95	$1 \times 10^{-4}$
Mo-99	0.8
Ru-103	0.03
Ru-106	0.03
Rh-106	0.2
Ag-111	0.01

(Continued)

第 2.3 - 5 5 表 (Continued)

<u>Isotope</u>	<u>Fraction Retained</u>
Sb-125	0.03
Te-129	0.25
Te-129m	0.25
Te-132	0.25
I-131	1.0
I-132	1.0
Xe-131m	1.0
Xe-133	1.0
Xe-133m	1.0
Xe-135	1.0
Xe-135m	1.0
Xe-138	1.0
Cs-134	1.0
Cs-136	1.0
Cs-137	1.0
Ba-140	0.05
La-140	$1 \times 10^{-4}$
Ce-141	$1 \times 10^{-4}$
Ce-144	$1 \times 10^{-4}$
Pr-143	$1 \times 10^{-4}$
Pr-144	$1 \times 10^{-4}$
Nd-147	$1 \times 10^{-4}$
Pm-147	$1 \times 10^{-4}$
Eu-155	$1 \times 10^{-4}$
Ta-182	$1 \times 10^{-4}$
Pu-238	$1 \times 10^{-5}$
Pu-239	$1 \times 10^{-5}$
Pu-240	$1 \times 10^{-5}$
Pu-241	$1 \times 10^{-5}$
Pu-242	$1 \times 10^{-5}$

Ref. (1) AMENDMENT IV Table 5.3A-9

第 2.3 - 5 6 表

EFFECTIVE ABSORBED BETA AND GAMMA ENERGIES IN FINITE VOLUMES OF MUSCLE TISSUE<sup>(49)</sup>  
MeV/dis

Effective Radius* (cm)	Effective Radius*							
	1.4	2.0	3.0	5.0	7.0	10.0	20.0	30.0
Isotope								
H-3	0.01	0.01	0.01	0.01	0.01	0.01	0.01	0.01
Na-22	0.286	0.325	0.387	0.507	0.619	0.775	1.20	1.51
Na-24	0.712	0.771	0.868	1.05	1.23	1.48	2.19	2.74
Ne-23	--	--	--	NA	--	--	--	--
Ar-39	0.194	0.194	0.194	0.194	0.194	0.194	0.194	0.194
Ar-41	0.519	0.541	0.576	0.642	0.705	0.793	1.04	1.22
Cr-51	0.00222	0.00276	0.00363	0.00529	0.00685	0.00901	0.0149	0.0191
Mn-54	0.0364	0.0514	0.0758	0.122	0.166	0.227	0.392	0.512
Fe-59	0.171	0.191	0.224	0.286	0.346	0.428	0.655	0.824
Co-58	0.0722	0.0905	0.119	0.174	0.226	0.297	0.492	0.633
Co-60	0.195	0.237	0.306	0.437	0.560	0.732	1.21	1.56
Kr-83m	0.0438	0.0438	0.0438	0.0438	0.0438	0.0438	0.0438	0.0438
Kr-85	0.224	0.224	0.224	0.224	0.224	0.225	0.225	0.225
Kr-85m	0.245	0.248	0.252	0.260	0.268	0.279	0.309	0.331
Kr-87	1.21	1.24	1.27	1.34	1.41	1.50	1.77	1.97
Kr-88	0.449	0.475	0.517	0.599	0.677	0.786	1.09	1.33
Sr-89	0.564	0.564	0.564	0.564	0.564	0.564	0.564	0.564

(Continued)

第 2.3 - 5 6 表 (Continued)

MeV/dis

Effective Radius* (cm)	1.4	2.0	3.0	5.0	7.0	10.0	20.0	30.0
Sr-90	1.14	1.14	1.14	1.14	1.14	1.14	1.14	1.14
Y-90	0.939	0.939	0.939	0.939	0.939	0.939	0.939	0.939
Y-91	0.590	0.590	0.591	0.591	0.591	0.591	0.592	0.592
Zr-95	0.227	0.254	0.297	0.380	0.458	0.565	0.857	1.07
Nb-95	0.0767	0.0906	0.113	0.156	0.197	0.253	0.405	0.515
Mo-99**	0.419	0.423	0.430	0.444	0.457	0.475	0.524	0.561
Ru-103**	0.116	0.125	0.140	0.168	0.194	0.230	0.328	0.399
Ru-106**	1.44	1.44	1.45	1.46	1.47	1.49	1.53	1.56
Rh-106	--	--	--	NA	--	--	--	--
Ag-111	0.361	0.362	0.362	0.364	0.365	0.367	0.372	0.376
Sb-125	0.105	0.113	0.126	0.156	0.173	0.205	0.291	0.353
Te-129	0.535	0.538	0.541	0.548	0.555	0.563	0.585	0.601
Te-129m**	0.599	0.601	0.605	0.612	0.619	0.627	0.651	0.667
Te-132	0.121	0.125	0.131	0.143	0.154	0.169	0.211	0.242
I-131	0.206	0.213	0.224	0.245	0.266	0.293	0.360	0.422
I-132	0.581	0.624	0.693	0.826	0.950	1.12	1.59	1.94
Xe-131m	0.136	0.136	0.136	0.137	0.137	0.137	0.138	0.139
Xe-133	0.137	0.137	0.138	0.140	0.141	0.143	0.148	0.152
Xe-133m	0.176	0.177	0.178	0.180	0.182	0.184	0.191	0.196
Xe-135	0.330	0.335	0.342	0.355	0.368	0.386	0.434	0.469
Xe-135m	0.118	0.126	0.139	0.163	0.186	0.217	0.302	0.363

(Continued)



第 2.3 - 5 6 表 (Continued)

MeV/dis

Effective Radius* (cm)	MeV/dis							
	1.4	2.0	3.0	5.0	7.0	10.0	20.0	30.0
Xe-138	0.505	0.527	0.562	0.630	0.694	0.784	1.04	1.23
Cs-134	0.230	0.259	0.306	0.396	0.480	0.596	0.913	1.14
Cs-136	0.233	0.273	0.337	0.458	0.573	0.732	1.17	1.49
Cs-137	0.257	0.267	0.284	0.316	0.346	0.388	0.509	0.582
Ba-140	0.315	0.320	0.328	0.343	0.357	0.376	0.428	0.465
La-140	0.698	0.734	0.793	0.907	1.01	1.16	1.58	1.89
Ce-141	0.173	0.174	0.175	0.179	0.182	0.187	0.199	0.209
Ce-144**	1.32	1.32	1.32	1.33	1.33	1.33	1.34	1.35
Pr-143	0.314	0.314	0.314	0.314	0.314	0.314	0.314	0.314
Pr-144	1.23	1.23	1.23	1.24	1.24	1.24	1.24	1.25
Nd-147	0.257	0.259	0.264	0.272	0.280	0.291	0.320	0.342
Pm-147	0.0620	0.0620	0.0620	0.0620	0.0620	0.0620	0.0620	0.0620
Eu-155	--	--	--	NA	--	--	--	--
Ta-182	--	--	--	NA	--	--	--	--
Pu-238	55.0	55.0	55.0	55.0	55.0	55.0	55.0	55.0
Pu-239	51.5	51.5	51.5	51.5	51.5	51.5	51.5	51.5
Pu-240	51.6	51.6	51.6	51.6	51.6	51.6	51.6	51.6
Pu-241**	0.00636	0.00636	0.00636	0.00636	0.00636	0.00636	0.00636	0.00636
Pu-242	48.9	48.9	48.9	48.9	48.9	48.9	48.9	48.9

\*Effective radius may be calculated from the mass of the organism using the following relationship:

$$ER = 10.0 M^{0.292516} \text{ where: } ER = \text{effective radius, cm}$$

$$M = \text{mass of the organism, kg}$$

\*\*Includes contribution from daughter products

NA - Not available

第 3.1 - 1 表 SNR-300 設計の主要目

• 原子炉型式	ループ型
• 電気出力 (送電端)	~ 280 MWe
• 熱出力	~ 700 MWt
• 炉心燃料	(Pu, U)O <sub>2</sub>
• 炉心高さ	950 mm
• 炉心燃料集合体本数 (内側/外側・炉心)	
1 サイクル	94~109/90
2 サイクル	97~112/90
3 サイクル	100~115/90
• ブランケット燃料集合体本数	96
• 炉心燃料集合体	
ペレット直径 (MK-1a/MK-II)	5.09 mm / (6.45 mm)
被覆材	SUS316 相当
被覆材外径 (MK-1a/MK-II)	6.0 mm / 7.6 mm
被覆材肉厚 (MK-1a/MK-II)	0.38 mm / 0.5 mm
スペーサ型式	グリッド (MK-1a) グリッド又はワイヤー (MK-II)
• 線出力 (ノミナル/ホットスポット)	370/455 W/cm (MK-1a) 440/540 W/cm (MK-II)
• 軸方向ブランケット厚さ (上/下)	400 mm
• 半径方向ブランケット層数	2
• ガスプレナム長さ	655 mm
• ガスプレナム位置	炉心下部
• 被覆材許容最高温度 (ノミナル/ホットスポット)	620°C / 670°C
• 炉心燃料集合体当りピン本数 (MK-1a/MK-II)	166 / 127
• 取出し燃料燃焼度 (最大)	90,000 MWD/T
• 制御棒	
吸収材	B <sub>4</sub> C
調整棒+安全棒	9本
後備炉停止棒	3本

• 原子炉容器寸法（高さ／直径）	16.15m／6.7m
• ループ数	3
• クランピング構造	外部クランピング・バイメタル方式
• ポンプ位置（1次系／2次系）	ホットレグ／コールドレグ
• 1次冷却系流量	4,300 ton／hr・ループ
• 2次冷却系流量	4,000 ton／hr・ループ
• 原子炉出入口温度（入口／出口）	377℃／546℃
• 2次系中間熱交換器出入口温度（入口／出口）	335℃／520℃
• 中間熱交換器型式	直管内部遊動ヘッド型
• 中間熱交換器基数	3
• 蒸気発生器	
蒸気発生器型式	モジュラー（直管及びヘリカルコイル型）
蒸気器基数（ループ当り）	3
過熱器基数（ループ当り）	3
• 主蒸気圧力	167 kg／cm <sup>2</sup>
• 主蒸気温度	500℃
• 非常用炉心冷却系	
型式	投込みクーラー方式
基数	6
除熱容量	合計 7.2 MWt
• 炉内燃料交換方式	3重回転ブラグ
• 燃料交換間隔	～1年
• 格納容器型式	角型

第3.2 - 1表

General view about the relevant parameters of thermal load and the resulting conditions for the cooling water inlet

Parameter	Conditions
max. summer temperature $T_{su \max}$ max. winter temperature $T_{wi \max}$	$T_{su \max} < 28^{\circ}\text{C}$  $T_{wi \max} < 5-6^{\circ}\text{C}$
temperature difference in the river $\Delta t$	$\Delta t < 3\text{K}$ , only in approved exceptions $< 5\text{K}$
max. temperature of the cooling water	no general regulations (spec. case studies neces- sary)
changes in the yearly temperature course	no general regulations (spec. case studies neces- sary)
Water losses	no general regulations (spec. case studies neces- sary)
concerned water type (fish region, pre-load of organic and toxic substances)	no general regulations (spec. case studies neces- sary)
Interference with the or- ganic pre-load of the water (influence of the $\text{O}_2$ -content)	substitution of the $\text{O}_2$ used by the heating of the water by artificial ventilation

Ref.(1) Table 6

第 3.2 - 2 表 Activity Inventory in Primary Sodium Coolant <sup>(65)</sup>

<u>Type</u>	<u>Nuclide</u>	<u>Activity (Ci)</u>
Activation Products	Na-22	$3.5 \times 10^2$
	Na-24	$2.0 \times 10^7$
Fission Products	I-131	$2.1 \times 10^5$
	I-133	$9.4 \times 10^4$
	Cs-134	$3.8 \times 10^3$
	Cs-137	$6.4 \times 10^3$
Corrosion Products	Mn-54	$1.9 \times 10^3$
	Co-58	$3.9 \times 10^3$
	Co-60	$3.0 \times 10^2$

Ref.(1) Table 1

第 3.2 - 3 表 Activity in Argon Cover Gas<sup>(65), (66)</sup>

<u>Type</u>	<u>Nuclide</u>	<u>Activity (Ci)</u>
Fission Products	Xe-133	$4.2 \times 10^5$
	Xe-135	$9.6 \times 10^4$
	I-131	$3.5 \times 10^{-2}$
	I-133	$1.6 \times 10^{-2}$
	Cs-134	$4.8 \times 10^{-2}$
	Cs-137	$8.0 \times 10^{-2}$
Activation Products	Na-22	$3.2 \times 10^{-3}$
	Na-24	$1.9 \times 10^1$
	Ar-41	$1.1 \times 10^2$

Ref. (11) Table 2

第 3.2 - 4 表 Activity Released to the Environment  
During Normal Operation - Airborne<sup>(65), (66)</sup>

Nuclide	Release (Ci/a)
Xe-133	$6.0 \times 10^4$
Xe-135	$2.1 \times 10^4$
Ar-41	$6.4 \times 10^3$
Kr-85	$3.9 \times 10^2$
I-131	$3.8 \times 10^{-3}$
I-133	$5.0 \times 10^{-4}$
Cs-134	$4.6 \times 10^{-5}$
Cs-137	$7.7 \times 10^{-5}$

Ref. (1) Table 3

第 3.2 - 5 表 Activity Released to the Environment  
During Normal Operation - Liquid Waste <sup>(65)</sup>

<u>Nuclide</u>	<u>Release (Ci/a)</u>
Co-58	0.1
Co-60	0.1
I-131	1.8
Cs-134	0.1
Cs-137	0.2
Other	0.2
Total	<hr/> 2.5

Ref. (11) Table 4



第3.2-6表 Total Activity of Noble-Gas and Iodine Isotopes  
During Operation of a 1000-MW(e) LMFBR

Isotope	Saturated activity, Ci	Half-Life	Accumulated yield (fast fission), %	
			$^{239}\text{Pu}$	$^{238}\text{Pu}^{**}$
$^{83\text{m}}\text{Kr}$	$7.016 \times 10^6$	1.86 hr	0.350	0.412
$^{85\text{m}}\text{Kr}$	$1.301 \times 10^7$	4.4 hr	0.642	0.811
$^{85}\text{Kr}$	$2.4 \times 10^5$	10.76 years	0.142	0.173
$^{87}\text{Kr}$	$2.250 \times 10^7$	76 min	1.108	1.416
$^{88}\text{Kr}$	$2.759 \times 10^7$	2.79 hr	1.368	1.677
$^{89}\text{Kr}$	$3.585 \times 10^7$	3.18 min	1.653	3.010
$^{131\text{m}}\text{Xe}$	$4.822 \times 10^5$	11.96 days	0.025	0.022
$^{133\text{m}}\text{Xe}$	$3.785 \times 10^6$	2.26 days	0.195	0.181
$^{133}\text{Xe}$	$1.328 \times 10^8$	5.27 days	6.824	6.471
$^{135\text{m}}\text{Xe}$	$3.459 \times 10^7$	15.7 min	1.902	0.852
$^{135}\text{Xe}$	$1.416 \times 10^8$	9.16 hr	7.447	5.748
$^{137}\text{Xe}$	$1.138 \times 10^8$	3.82 min	5.785	5.951
$^{138}\text{Xe}$	$7.828 \times 10^7$	14.2 min	3.709	5.908
$^{129}\text{I}$	1.7*	$1.6 \times 10^7$ years	0.922	0.653
$^{131}\text{I}$	$8.086 \times 10^7$	8.065 days	4.196	3.662
$^{132}\text{I}$	$1.050 \times 10^8$	2.284 hr	5.366	5.300
$^{133}\text{I}$	$1.327 \times 10^8$	20.8 hr	6.817	6.471
$^{134}\text{I}$	$1.392 \times 10^8$	52.3 min	7.186	6.553
$^{135}\text{I}$	$1.217 \times 10^8$	6.7 hr	6.290	5.673

\* Approximate values in the reactor [1000-MW(e) GE design]  
at shutdown for refueling.

\*\* 編者注； $^{238}\text{U}$ の誤植と思われる。

Ref.(4) Table 10

第3.2-7表 Estimates of Activated Corrosion Products in the Primary System of a  
1000-MW(e) LMFBR After 30 Years of Operation\*

Isotope	Formation reaction	$T_{1/2}$	Contribution to the primary system activity, Ci				Total Primary system activity
			Core	Axial blanket	Gas Plenum	Radial blanket	
$^{60}\text{Co}$	$n, \gamma$	5.24 years	1,400†	9,300†	6,600†	2,200†	20,000
	$n, p$		1,000				
$^{58}\text{Co}$	$n, p$	71 days	20,000	2,800	300	400	23,000
$^{54}\text{Mn}$	$n, p$	313 days	16,000	2,400		300	19,000
$^{55}\text{Fe}$	$n, \gamma$	45 days	26,000	‡	‡	‡	>26,000
$^{59}\text{Fe}$	$n, \gamma$	2.4 years	300	500	300		1,000
$^{51}\text{Cr}$	$n, \gamma$	28 days	2,500	2,800	1,800		7,000
	$n, \alpha$		200				
$^{182}\text{Ta}$	$n, \gamma$	115 days	800	3,200	2,400		6,000

\* All values are based on stoichiometric corrosion, assuming 316 stainless steel.

† Based on only 0.02 wt% cobalt in stainless steel.

‡ Cross sections were unavailable for the soft spectra in these regions. It is expected that the  $^{55}\text{Fe}$  generation from the  $(n, \gamma)$  reaction would be higher outside of the core than inside. The calculation was not pursued further, however, because  $^{55}\text{Fe}$  decays only by electron capture so that the  $^{55}\text{Fe}$  activity is of little importance.

第 3.2 - 8 表

Environmental aspects by producing 1 MW(e) annual<sup>(64)</sup>

		coal fired facility	oil fired facility	SNR 300	remarks
O <sub>2</sub> use	(3)T	8	8	-	
CO <sub>2</sub> -CO impact	(3)T	10	10	-	
SO <sub>x</sub> NO <sub>x</sub> impact	T	160	75	-	
dust impact	T	5	0,7	-	
krypton im- pact	Ci	-	-	1.3	
other noble gases	Ci	-	-	240	proposal values
combustion- air	(6)m <sup>3</sup>	29	29	-	
other waste gases	(6)m <sup>3</sup>	180 000	73 000	-	
SO <sub>2</sub> concen- tration	PPM	0,3	0,3	-	MAK:5 ppm
NO <sub>2</sub> concen- tration	PPM	2	2	-	MAK:5 ppm
Kr 85 con- centration	Ci/m <sup>3</sup>	-	-	3(-9)	MZK:9(-6)Ci/m <sup>3</sup> (40 H/W)
Xe 133 con- centration	Ci/m <sup>3</sup>	-	-	5(-7)	MZK:9(-6)Ci/m <sup>3</sup> (40 H/W)
waste heat (cooling water) (10)kcal		1,1	1,1	1,2	operation with fresh water and equal plant efficiency
cooling water requirement	(6)m <sup>3</sup>	1,3	1,3	1,4	
Ra 226/Ra 228	Ci	1(-4)	-	-	MZK:3(-11)Ci/m <sup>3</sup> (40 H/W)

Ref.(11) Table 8

第 3.2 - 9 表 Annual Amounts of Fuel Cycle Waste  
SNR-300 Class Fast Reactor\* (67)

Reprocessing Plant:

High-level solid waste:	(m <sup>3</sup> /a)	1.5
	(kg/a)	3,000.
Cladding hulls:	(m <sup>3</sup> /a)	4.
	(kg/a)	19,000.
Other solids:	(m <sup>3</sup> /a)	30. - 200.
	(kg/a)	50,000. - 100,000.

Fuel Fabrication Plant

Pu-contaminated waste	(m <sup>3</sup> /a)	200.
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Ref.(1) Table 5

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\* Assumed full-power operation after completion of demonstration period.

第3.3 - 1表

General view about the relevant parameters of thermal load and the resulting conditions for the cooling water inlet

Parameter	Conditions
max. summer temperature $T_{su \text{ max}}$ max. winter temperature $T_{wi \text{ max}}$	$T_{su \text{ max}} < 28^{\circ}\text{C}$  $T_{wi \text{ max}} < 5-6^{\circ}\text{C}$
temperature difference in the river $\Delta t$	$\Delta t < 3\text{K}$ , only in approved exceptions $< 5\text{K}$
max. temperature of the cooling water	no general regulations (spec. case studies neces- sary)
changes in the yearly temperature course	no general regulations (spec. case studies neces- sary)
Water losses	no general regulations (spec. case studies neces- sary)
concerned water type (fish region, pre-load of organic and toxic substances)	no general regulations (spec. case studies neces- sary)
Interference with the or- ganic pre-load of the water (influence of the $\text{O}_2$ -content)	substitution of the $\text{O}_2$ used by the heating of the water by artificial ventilation

Ref.(1) Table 6

第 3.3 - 2 表

Annual Costs for 1000 MW(e) Energy System, 1990

Item	Coal	PWR	LFMBR
Occupational health			
Occupational accident (MDL)	2400	490	65
Occupational health (MDL)	0	240	200
Occupational genetic (MDL)	unevaluated	920	900
Public health			
Public (routine releases) (MDL)	$(18-60) \times 10^3$	110	110
Public (accidental releases) (MDL)	unevaluated	unevaluated	unevaluated
Public (transportation accidents) (MDL)	$(6-18) \times 10^3$	30	35
Environment			
Thermal discharge damage ( $10^6$ \$)	0.7	1.0	0.8
Pollutant effect (vegetation)	$\$2 \times 10^6$	small	small
Social			
Perceived risk-terrorism	small	moderate	large
Perceived risk-waste disposal	small	large	large
Impact life style	unevaluated	unevaluated	unevaluated
National security	unevaluated	unevaluated	unevaluated

Ref.(1) Table 7

第 3.3 - 3 表

Environmental aspects by producing 1 MW(e) annual <sup>(64)</sup>

		coal fired facility	oil fired facility	SNR 300	remarks
O <sub>2</sub> use	(3)T	8	8	-	
CO <sub>2</sub> -CO impact	(3)T	10	10	-	
SO <sub>x</sub> NO <sub>x</sub> impact	T	160	75	-	
dust impact	T	5	0,7	-	
krypton im- pact	Ci	-	-	1.3	
other noble gases	Ci	-	-	240	proposal values
combustion- air	(6)m <sup>3</sup>	29	29	-	
other waste gases	(6)m <sup>3</sup>	180 000	73 000	-	
SO <sub>2</sub> concen- tration	PPM	0,3	0,3	-	MAK: 5 ppm
NO <sub>2</sub> concen- tration	PPM	2	2	-	MAK: 5 ppm
Kr 85 con- centration	Ci/m <sup>3</sup>	-	-	3(-9)	MZK: 9(-6)Ci/m <sup>3</sup> (40 H/W)
Xe 133 con- centration	Ci/m <sup>3</sup>	-	-	5(-7)	MZK: 9(-6)Ci/m <sup>3</sup> (40 H/W)
waste heat (cooling water) (10)kcal		1,1	1,1	1,2	operation with fresh water and equal plant efficiency
cooling water requirement	(6)m <sup>3</sup>	1,3	1,3	1,4	
Ra 226/Ra 228	Ci	1(-4)	-	-	MZK: 3(-11)Ci/m <sup>3</sup> (40 H/W)

Ref. (11) Table 8

第 3.3 - 4 表 Activity Released to the Environment  
During Normal Operation - Airborne <sup>(65)</sup> (66)

Nuclide	Release (Ci/a)
Xe-133	$6.0 \times 10^4$
Xe-135	$2.1 \times 10^4$
Ar-41	$6.4 \times 10^3$
Kr-85	$3.9 \times 10^2$
I-131	$3.8 \times 10^{-3}$
I-133	$5.0 \times 10^{-4}$
Cs-134	$4.6 \times 10^{-5}$
Cs-137	$7.7 \times 10^{-5}$

Ref. (1) Table 3



第 3.3 - 5 表 Annual Dose to Man from Airborne and Liquid Releases Due to Normal Operation of SNR-300<sup>(65)</sup> (stack height 100 m).

Critical Organ	Annual Dose (mrem/a)	Distance from Stack (m)
whole body	2.8	100
lens	0.6	800
thyroid (pasture-cow-milk path)	0.3	800
lung (inhalation)	$5.0 \times 10^{-6}$	800

Ref. (1) Table 9

第 3.3 - 6 表 Activity Released to the Environment  
During Normal Operation - Liquid Waste<sup>(65)</sup>

<u>Nuclide</u>	<u>Release (Ci/a)</u>
Co-58	0.1
Co-60	0.1
I-131	1.8
Cs-134	0.1
Cs-137	0.2
Other	0.2
	<hr/>
Total	2.5

Ref. (1) Table 4

第4.1-1表 CRBRP-ER ソース・ターム計算(まとめ)

1. 気体廃棄物中の放射性物質放出(BOPよりのH-3大気放出を除く)

(1) カバーガス中への流入率  $\dot{I}$

a) FP Xe及びKrの同位体のみ (cf. 第2.2-8表)

$$\dot{I} = K \cdot FF \cdot P \cdot EF \cdot YLD \cdot \lambda / 3.7 \times 10^{10}$$

ここで  $\dot{I}$  : FPのカバーガス中への流入率 (Ci/sec)

K : 核分裂率 ( $3.1 \times 10^{16}$  fission/MW.sec)

FF : ピンホールを持つ燃料ピンで発生する熱量の総発熱量に対する割合  
(0.01を設計値とする) 燃料欠陥率

P : 定格熱出力 (975 MWt)

EF : FPの燃料棒プレナム部への逃散率 [Kayser Model使用]

YLD : FPのPu-239高速核分裂による累積収率

$\lambda$  : FPの崩壊定数 (sec<sup>-1</sup>)

b) 冷却材放射化物 (Ar-39, Ar-41, Ne-23) 及びH-3

以下の式が予想される。

$$\dot{I} = \sum_r N_o \cdot \sigma \cdot \phi(r) \cdot V_o(r) \cdot \lambda / 3.7 \times 10^{10}$$

ここで  $\dot{I}$  : 冷却材放射化物のカバーガスへの流入率 (Ci/sec)

$N_o$  : 標的核の原子個数密度 (atm/cm<sup>3</sup>)

$\sigma$  : 放射化断面積 (1/cm<sup>2</sup>)

$\phi(r)$  : 中性子束 (n/cm<sup>2</sup>·sec), [DOT-IIIで計算]

$V_o(r)$  : 領域r内の容積 (cm<sup>3</sup>)

$\lambda$  : 冷却材放射化物崩壊定数 (sec<sup>-1</sup>)

r : 領域を表わす添字

(2) カバーガスのインベントリ及び濃度 (cf. 第2.2-18表)

$$I_g = \frac{\dot{I}}{\lambda + \epsilon F / V_g}$$

$$C_g = \frac{I_g}{V_g}$$

ここで  $I_g$  : FPのカバーガス中インベントリ ( $C_i$ )  
 $C_g$  : FPのカバーガス中濃度 ( $C_i/cm^3$ )  
 $\dot{I}$  : FPのカバーガス中への流入率 ( $C_i/sec$ )  
 $\lambda$  : FPの崩壊定数 ( $sec^{-1}$ )  
 $V_g$  : カバーガスの空間容積 ( $cm^3$ )  
 $F/V_g$  : カバーガスのバージ係数 ( $sec^{-1}$ )  
 $\epsilon$  : 処理効率係数

(3) 放射性物質の大気放出  $R_g$  (cf. 第 2.2 - 19, 20 表)

ヘッドシール部, RAPS 処理後のバッファード・シール部, 1 次系配管等の部分, 及び RAPS と CAPS 配管部の 4 個所の漏れを考慮。

$$R_g = C_g \times L_1 \cdot \lambda e^{-\lambda t_1} + \frac{C_g}{DF_{g1}} \times L_2 \times e^{-\lambda t_2} + C_g \times \frac{L_3}{DF_{g2}} + C_g \left( L_4 + \frac{L_5}{DF_{g1}} \right) \times \frac{1}{DF_{g2}}$$

ここで  $R_g$  : FPの放出率 ( $C_i/sec$ )  
 $C_g$  : FPのカバーガス中濃度 ( $C_i/cm^3$ )  
 $L_1$  : FPのヘッド・シール漏洩率 ( $C_i/sec$ )  
 $L_2$  : FPのバッファード・シール漏洩率 ( $C_i/sec$ )  
 $L_3$  : FPの1次系配管等, 漏洩率 ( $C_i/sec$ )  
 $L_4$  : FPのRAPS漏洩率 ( $C_i/sec$ )  
 $L_5$  : FPのCAPS漏洩率 ( $C_i/sec$ )  
 $DF_{g1}$  : FPに対するRAPSの除染係数  
 $DF_{g2}$  : FPに対するCAPSの除染係数  
 $t_1$  : ヘッド・シールにおけるホールド・アップ時間 ( $sec$ )  
 $t_2$  : バッファード・シールにおけるホールド・アップ時間 ( $sec$ )  
 $\lambda$  : FPの崩壊定数 ( $1/sec$ )

(4) データ

- 燃料欠陥率  $FR = 0.001$  (0.1%)
- 照射時間  $t = 1$ 年 (飽和)
- ガスの空間容積  $V_g = 1.15 \times 10^7 cm^3$
- バージ係数  $\epsilon F / V_g = 6.14$  1/day

○ 系統各部の漏洩率  $cm^3/min$

$$L_1 = 0.012, L_2 = 7, L_3 = 1, L_4 + L_5 = 1$$

○ 除染係数, 滞在時間: 核種毎に指定 (cf. 第2.2-17, 18表)

○ H-3は気液分配される

2. 液体廃棄物中の放射性物質放出 (BOPよりのH-3水中放出を除く)

(1) 1次冷却材中への流入率  $\dot{I}$

a) FP 希ガスを除くFP

$$\dot{I} = K \cdot FF \cdot P \cdot EF \cdot YLD \cdot \lambda / 3.7 \times 10^{10}$$

ここで  $\dot{I}$ : FPの1次冷却材中への流入率 (Ci/sec)

K, FF, P, EF, YLD,  $\lambda$  は1(1)記載のものと同じである。

b) Pu

$$\dot{I} = \phi_f \cdot n_f \cdot FF \cdot S_F \cdot \chi \cdot \lambda / 3.7 \times 10^{10}$$

c) 腐食生成物

$$\dot{I} = \sum_r N_o \cdot \sigma \cdot \phi(r) \cdot S(r) \cdot CR(r) / 3.7 \times 10^{10}$$

d) その他物質 (Na-22, 24, H-3)

$$\dot{I} = \sum_r N_o \cdot \sigma \cdot \phi(r) \cdot V_o(r) \cdot \lambda / 3.7 \times 10^{10}$$

} 予想される式

ここで  $\dot{I}$ : 放射性物質の1次冷却材中への流入率 (Ci/sec)

$\phi_f$ : Puの逃散係数 ( $atm/cm^2 \cdot sec$ )

$n_f$ : 炉心部の燃料棒総本数

FF: 燃料欠陥率

$S_F$ : 燃料棒被覆管の標準欠陥面積 ( $cm^2$ )

$\chi$ : Pu同位元素の存在比 (原子個数比)

r: 領域を表わす添字

$N_o$ : 標的核の原子個数密度 ( $atm/cm^3$ )

$\sigma$ : 放射化断面積 ( $1/cm^2$ )

$\phi(r)$ : 中性子束 ( $n/cm^2 \cdot sec$ ), [DOT-IIIで計算]

$S(r)$ : 領域rの接液面積 ( $cm^2$ )

CR(r): 腐食率 ( $cm/sec$ ), [Naの温度, 流速等の関数]

$V_0(r)$ : 領域  $r$  内の容積 ( $cm^3$ )

$\lambda$  : 放射性物質の崩壊定数 ( $sec^{-1}$ )

(注) H-3は気液分配する。

(2) 1次冷却材中のインベントリと濃度 (cf. 第2.2-23表)

$$I_w = \frac{\dot{I}}{\lambda} \cdot (1 - e^{-\lambda t}) \cdot \eta_n$$

(上式はH-3の場合には成立しない。)

$$C_w = I_w / W$$

ここで  $I_w$  : 放射性物質の1次冷却材中インベントリ ( $Ci$ )

$C_w$  : 放射性物質の1次冷却材中濃度 ( $Ci/g$ )

$W$  : 1次冷却材重量 ( $7.1 \times 10^8 g Na$ )

$\eta_n$  : 蓄積放射性物質の1次冷却材中に含まれる割合 (cf. 第2.2-22表)

$t$  : 原子炉運転時間 ( $sec$ )

$\dot{I}$  : 放射性物質の1次冷却材中への流入率 ( $Ci/sec$ )

$\lambda$  : 放射性物質の崩壊定数 ( $sec^{-1}$ )

(3) 1次冷却系機器内壁に付着するインベントリ

$$I_s = \frac{\dot{I}}{\lambda} (1 - e^{-\lambda t}) \cdot \eta_s$$

(上式はH-3の場合には成立しない。)

ここで  $I_s$  : 放射性物質の1次冷却系機器内壁に付着するインベントリ ( $Ci$ )

$\eta_s$  : 蓄積放射性物質の1次系機器に付着する割合 (cf. 第2.2-22表)

$t$  : 原子炉運転時間 ( $sec$ )

$\dot{I}$  : 放射性物質の1次冷却材中への流入率 ( $Ci/sec$ )

$\lambda$  : 放射性物質の崩壊定数 ( $sec^{-1}$ )

(4) 液体廃棄物処理系流入量と濃度 (cf. 第2.2-9表)

a) 低レベル廃棄物処理系

$$C_{w1} = C_w \times L_n / Q_1$$

ここで  $C_{w1}$  : 液体廃棄物処理系低レベル放射性物質の流入濃度 ( $Ci/cm^3$ )

$C_w$  : 放射性物質の1次冷却材中の濃度 ( $Ci/g$ )

$L_n$  :  $Na$ 漏洩率 ( $g(Na)/sec$ ) ←  $3.5 lb/yr$

$Q_1$  : 液体廃棄物処理系流入流量 ( $cm^3 / sec$ )  $\leftarrow 3.1 \times 10^5 gal / yr$

b) 中レベル廃棄物処理系

$$C_{w2} = I_s \cdot \beta / Q_2$$

ここで  $C_{w2}$  : 液体廃棄物処理系中レベル放射性物質の流入濃度 ( $ci/cm^3$ )

$I_s$  : 放射性物質の1次冷却系機器内壁に付着するインベントリ ( $ci$ )

$\beta$  : 洗浄率 ( $1 / sec$ )  $\leftarrow 0.4 / (365 \times 24 \times 3600)$

$Q_2$  : 洗浄水流量 ( $cm^3 / sec$ )  $\leftarrow 3.7 \times 10^4 gal / yr$

(5) 放射性物質の河川放出 (cf. 第2.2-26表)

a) 低レベル

$$R_{w1} = \frac{C_{w1}}{DF_w} \cdot \frac{Q_1}{Q_3}$$

ここで  $R_{w1}$  : 液体廃棄物処理系低レベル放射性物質の放出濃度 ( $ci/cm^3$ )

$C_{w1}$  : 液体廃棄物処理系低レベル放射性物質の流入濃度 ( $ci/cm^3$ )

$DF_w$  : 濃縮脱塩による除染係数

H-3は1, 他は  $10^5$

$Q_1$  : 液体廃棄物処理系流入流量 ( $cm^3 / sec$ )

$Q_3$  : 希釈水流量 ( $3 \times 10^{12} cm^3 / sec$ )

b) 中レベル

$$R_{w2} = \frac{C_{w2}}{DF_w} \cdot \frac{Q_4}{Q_3}$$

ここで  $R_{w2}$  : 液体廃棄物処理系中レベル放射性物質の放出濃度 ( $ci/cm^3$ )

$C_{w2}$  : 液体廃棄物処理系中レベル放射性物質の流入濃度 ( $ci/cm^3$ )

$DF_w$  : 濃縮脱塩による除染係数

$Q_3$  : 希釈水流量 ( $3 \times 10^{12} cm^3 / sec$ )

$Q_4$  : 放水貯蔵廃液流量 ( $cm^3 / sec$ )  $\leftarrow 4000 gal / yr$

(6) データ

- 燃料欠陥率  $FF = 0.001$  (0.1%)
- 照射時間  $t = 30$ 年 (Puは15年)
- Puの逃散係数  $\phi_f = 9.71 \times 10^{14} atm/cm^2 \cdot sec$

第 4.1 - 2 表 PWR の発生源の計算式

(B-1) 式  
1次冷却材中の希ガス及びヨウ素の濃度を求める計算式

$$A_{wt} = \frac{A_{ct} \cdot \nu_i}{W_m \cdot \alpha_i \cdot t} \left\{ t - \frac{1}{\alpha_i} (1 - e^{-\alpha_i t}) \right\}$$

$$\alpha_i = \lambda_i + \frac{W_p}{W_m} \left\{ t - \frac{(DF_i - 1)}{DF_i} + FS_i \right\} + \frac{W_n}{W_m}$$

$$A_{ct} = \frac{\lambda_i \cdot F \cdot Y_i / 100}{3.7 \times 10^4 (\lambda_i + \nu_i + \sigma_i \phi)}$$

$$F = 3.2 \times 10^{10} \cdot P \cdot \frac{f}{100} \text{ (fissions/s)}$$

$A_{wt}$  : 1次冷却材中の核種  $i$  の濃度 ( $\mu\text{Ci/g}$ )  
 $A_{ct}$  : 被覆管欠陥率に相当する燃料棒内の核種  $i$  の量 ( $\mu\text{Ci}$ )  
 $\nu_i$  : 核種  $i$  の逃散率係数 ( $\text{s}^{-1}$ )  
 $W_m$  : 1次冷却材保有量 ( $\text{g}$ )  
 $\alpha_i$  : 核種  $i$  の除去定数 ( $\text{s}^{-1}$ )  
 $t$  : 原子炉運転時間 ( $\text{s}$ )  
 $\lambda_i$  : 核種  $i$  の崩壊定数 ( $\text{s}^{-1}$ )  
 $W_p$  : 浄化系流量 ( $\text{g/s}$ )  
 $DF_i$  : 核種  $i$  の浄化系の除染係数  
 $FS_i$  : 核種  $i$  のストリップング係数  
 $W_n$  : ほう酸回収装置で処理される抽出冷却材の年間平均流量 ( $\text{g/s}$ )  
 $Y_i$  : 核種  $i$  の核分裂収率 (%)  
 $\sigma_i$  : 核種  $i$  の熱中性子断面積 ( $\text{cm}^2$ )  
 $\phi$  : 炉心平均熱中性子束 ( $\text{n/cm}^2 \cdot \text{s}$ )  
 $P$  : 原子炉熱出力 ( $\text{MWt}$ )  
 $f$  : 燃料被覆管欠陥率 (%)

《パラメータ》

$\nu_i$  : (Kr, Xe)  $6.5 \times 10^{-8} (\text{s}^{-1})$   
 (I)  $1.3 \times 10^{-8} (\text{s}^{-1})$

$DF_i$  : 冷却材混床式脱塩塔  
 (Kr, Xe) 1  
 (I) 10  
 冷却材陽イオン脱塩塔  
 (Kr, Xe) 1  
 (I) 1

$FS_i$  : 体積制御タンクの連続脱ガス 体積制御タンクの連続脱ガス 有\*

	(Kr-85) $2.3 \times 10^{-6}$ $2.0 \times 10^{-1}$
	(Kr-85m) $2.7 \times 10^{-1}$ $3.0 \times 10^{-1}$
	(Kr-87) $6.0 \times 10^{-1}$ $6.0 \times 10^{-1}$
	(Kr-88) $4.3 \times 10^{-1}$ $4.3 \times 10^{-1}$
	(Xe-131m) $1.0 \times 10^{-2}$ $2.2 \times 10^{-1}$
	(Xe-133) $1.6 \times 10^{-2}$ $2.3 \times 10^{-1}$
	(Xe-133m) $3.7 \times 10^{-2}$ $2.3 \times 10^{-1}$
	(Xe-135) $1.8 \times 10^{-1}$ $2.8 \times 10^{-1}$
	(Xe-135m) $8.0 \times 10^{-1}$ $8.0 \times 10^{-1}$
	(Xe-138) 1.0 1.0
	$\sigma_i$ : (Xe-135) $2.65 \times 10^{-18} \text{cm}^2$
	(他の核種) 無視する
	* 体積制御タンクパーシ流量 $330 \text{Ncm}^3/\text{s}$ , 脱ガス効率 40%

(B-2) 式  
ほう酸回収系等からガス減衰タンクに移行する希ガスの量を求める計算式

$$Q_i = A_{wt} (K \cdot W_e + W_d + n_d \cdot W_m)$$

$Q_i$  : ガス減衰タンクへの核種  $i$  の移行量 ( $\text{Ci/y}$ )  
 $A_{wt}$  : 1次冷却材中の核種  $i$  の濃度 ( $\mu\text{Ci/g}$ )  
 $K$  : 抽出操作に伴う1次冷却材濃度の平均希釈率  
 $W_e$  : ほう酸回収装置で処理される抽出冷却材量 ( $\text{t/y}$ )  
 $W_d$  : ほう酸回収装置で処理される1次系機器ドレン量 ( $\text{t/y}$ )  
 $n_d$  : 冷態停止時における1次冷却材の脱ガス回数 ( $\text{y}^{-1}$ )  
 $W_m$  : 1次冷却材保有量 ( $\text{t}$ )

(B-3) 式  
体積制御タンクから連続脱ガスによりガス減衰タンクに移行する希ガスの量を求める計算式

$$A_{wt} = \frac{A_{vt} \cdot W_p \cdot FS_i}{V_v \left( \lambda_i + \frac{q}{V_v} \right)}$$

$Q_i$  : ガス減衰タンクへの核種  $i$  の移行量 ( $\text{Ci/y}$ )  
 $A_{vt}$  : 体積制御タンク気相部の核種  $i$  の濃度 ( $\text{Ci/cm}^3$ )  
 $q$  : 体積制御タンクのパーシ流量 ( $\text{cm}^3/\text{s}$ )  
 $t$  : 連続脱ガス装置の年間運転時間 ( $\text{s/y}$ )  
 $A_{wt}$  : 1次冷却材中の核種  $i$  の濃度 ( $\mu\text{Ci/g}$ )  
 $W_p$  : 浄化系流量 ( $\text{t/s}$ )  
 $FS_i$  : 核種  $i$  のストリップング係数  
 $V_v$  : 体積制御タンク気相部体積 ( $\text{cm}^3$ )  
 $\lambda_i$  : 核種  $i$  の崩壊定数 ( $\text{s}^{-1}$ )



<p>(B-4) 式 ガス減衰タンクから放出される希ガスの量を求める計算式</p>	$Q_{\text{out}t} = Q_i \cdot e^{-\lambda_i t}$ <p><math>Q_{\text{out}t}</math> : ガス減衰タンクから放出される核種 <math>i</math> の量 (<math>C_i/y</math>)  <math>Q_i</math> : 核種 <math>i</math> のガス減衰タンクへの移行量 (<math>C_i/y</math>)  <math>\lambda_i</math> : 核種 <math>i</math> の崩壊定数 (<math>s^{-1}</math>)  <math>t</math> : ガス減衰タンクの保持時間 (<math>s</math>)</p>
<p>(B-5) 式 原子炉格納容器換気系から放出される希ガス及びヨウ素の量を求める計算式</p>	<p>(a) 原子炉停止時の換気</p> $Q_{\text{out}} = \left[ \frac{\alpha_i}{\lambda_i + \beta_i} \left\{ 1 - e^{-(\lambda_i + \beta_i)t} \right\} + \frac{\alpha_i}{\lambda_i} \left\{ (1 - e^{-\lambda_i T}) \cdot e^{-(\lambda_i + \beta_i)t} \right\} \right] \times n$ $\alpha_i = A_{w1} \cdot L_1 \cdot P_{1i}$ $\beta_i = \frac{V_R}{V_{cv}} \cdot \eta_{ci} \cdot M$ <p>(b) 格納容器減圧時の換気</p> $Q_{\text{out}} = \frac{\alpha_i \cdot V_p}{\lambda_i \cdot T \cdot V_{cv}} (1 - \eta_{di}) \left\{ T - \frac{1}{\lambda_i} (1 - e^{-\lambda_i T}) \right\}$ $\alpha_i = A_{w1} \cdot L_1 \cdot P_{1i}$ <p><math>Q_{\text{out}}</math> : 核種 <math>i</math> の原子炉格納容器換気系からの放出量 (<math>C_i/y</math>)  <math>A_{w1}</math> : 1次冷却材中の核種 <math>i</math> の濃度 (<math>\mu C_i/g</math>)  <math>\lambda_i</math> : 核種 <math>i</math> の崩壊定数 (<math>d^{-1}</math>)  <math>t_f</math> : 格納容器内部空気浄化装置運転時間 (<math>d</math>)  <math>T</math> : 原子炉停止時換気の間隔 (<math>d</math>)  <math>n</math> : 原子炉停止に伴うバージ回数 (<math>y^{-1}</math>)  <math>L_1</math> : 原子炉格納容器内 1次冷却材漏洩率 (<math>t/d</math>)  <math>P_{1i}</math> : 原子炉格納容器内で漏洩冷却材中の核種 <math>i</math> が空気中に移行する割合  <math>V_R</math> : 格納容器内部空気浄化装置流量 (<math>m^3/d</math>)  <math>V_{cv}</math> : 原子炉格納容器自由体積 (<math>m^3</math>)  <math>\eta_{ci}</math> : 格納容器内部空気浄化装置の核種 <math>i</math> に対する活性炭フィルタの捕集効率  <math>\eta_{di}</math> : 格納容器減圧時換気ラインの核種 <math>i</math> に対する活性炭フィルタの捕集効率  <math>M</math> : 格納容器内部空気浄化装置の混合効率  <math>V_p</math> : 格納容器減圧時の換気量 (<math>m^3/y</math>)</p> <p>&lt;パラメータ&gt;  <math>L_1</math> : 0.1 t/d  <math>P_{1i}</math> : (Kr, Xe) 1.0 (I) 0.1  <math>M</math> : 0.7</p>

<p>(B-6) 式 原子炉補助建屋換気系から放出される希ガス及びヨウ素の量を求める計算式</p>	$Q_{\text{AB}i} = A_{w1} \cdot L_2 \cdot P_{2i} \cdot t$ <p><math>Q_{\text{AB}i}</math> : 核種 <math>i</math> の原子炉補助建屋換気系からの放出量 (<math>C_i/y</math>)  <math>A_{w1}</math> : 1次冷却材中の核種 <math>i</math> の濃度 (<math>\mu C_i/g</math>)  <math>L_2</math> : 原子炉補助建屋内 1次冷却材漏洩率 (<math>t/d</math>)  <math>P_{2i}</math> : 原子炉補助建屋内で漏洩冷却材中の核種 <math>i</math> が空気中に移行する割合  <math>t</math> : 原子炉年間運転時間 (<math>d/y</math>)</p> <p>&lt;パラメータ&gt;  <math>L_2</math> : 0.08 t/d  <math>P_{2i}</math> : (Kr, Xe) 1.0  (I) 0.005 [ただし抽出水クーラーが原子炉格納容器内にある場合等漏洩水の全てが低温とみなせる場合は0.001とする]</p>
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第 4.1 - 3 表 TYPICAL FISSION-PRODUCT INVENTORIES OF LWR AND LMFBR REACTORS (CURIES)

Isotope	1000-MWe LWR	1000-MWe LMFBR
Kr-85	$1.1 \times 10^5$	$5.7 \times 10^5$
Sr-90	$8.0 \times 10^5$	$3.2 \times 10^5$
Nb-95	$1.3 \times 10^8$	$1.0 \times 10^8$
I -129	0.5	0.25
I- 131	$8.0 \times 10^7$	$7.0 \times 10^7$
Xe-133	$1.6 \times 10^8$	$1.2 \times 10^8$
Cs-137	$1.1 \times 10^6$	$8.5 \times 10^5$
Ba-140	$1.5 \times 10^8$	$1.1 \times 10^8$

Ref. (14) TABLE 4.2-12

第 4.1 - 4 表 1,000MWe 軽水炉中の  
トリチウムの発生

トリチウム源	冷却材への流出 予想最大値 (Ci/yr)	
	PWR	BWR
三重核分裂 (0.1%が 冷却材に入ると仮定)	40	40
可溶性硼素	560	—
リチウム反応	17	—
重水素反応	10	10
計	627	50

Ref. (16) 第 4.6 表

第 4.1 - 5 表 Estimated Tritium Production Rates  
in a 1000-MW(e) LMFBR

Source	Production rate, Ci/year
Ternary fission	20,000
B <sub>4</sub> C control rods (shim and safety)	
<sup>10</sup> B(n, t)2α	7,000
<sup>7</sup> Li(n, nt)α	2,500
Lithium contamination [ <sup>6</sup> Li(n, t)α]	
In fuel (20 ppm Li in fuel)	4,000
In sodium (5 ppm Li in Na)	100
Total	~30,000

Ref. (4) TABLE 1 3

第 4.1 - 6 表. Gaseous Effluent Activities from LWRs and  
Phenix Fast Reactor

Gaseous Effluent Component	D i s c h a r g e s (Ci/GWe.y)		
	Current LWRs		Phenix
	Range	Mean	
Noble Gases	10 <sup>3</sup> - 10 <sup>4</sup>	6x10 <sup>3</sup>	1.6x10 <sup>3</sup>
Aerosols (Beta)	10 <sup>-4</sup> - 5x10 <sup>-2</sup>	2x10 <sup>-2</sup>	1.3x10 <sup>-4</sup>
(Alpha)	-	-	4 x10 <sup>-6</sup>
Iodine-131	10 <sup>-2</sup> - 6x10 <sup>-2</sup>	5x10 <sup>-2</sup>	2 x10 <sup>-3</sup>
Tritium	10 - 40	30	70

Ref. (5) TABLE C. 1.2

第 4.1 - 7 表

Comparison of FBR and LWR Radionuclide  
Gaseous Effluents (data as calculated)  
Release (Ci/GWe.yr)

Radionuclide	LMFBR	LWR(BWR)
Xe-131m	a	$1.6 \times 10^1$
Xe-133	$1.4 \times 10^1$	$2.5 \times 10^3$
Xe-135m	a	$5.7 \times 10^3$
Xe-135	$3.1 \times 10^1$	$8.5 \times 10^3$
Xe-138	a	$1.1 \times 10^3$
Kr-85m	$3.1 \times 10^1$	$1.2 \times 10^2$
Kr-85	$9.7 \times 10^2$	$2.4 \times 10^2$
Kr-87	a	$1.1 \times 10^2$
Kr-88	$1.7 \times 10^1$	$1.9 \times 10^2$
Ne-23	$5.7 \times 10^0$	b
Ar-39	$4.0 \times 10^1$	b
Ar-41	a	$1.9 \times 10^1$
H-3	$8.8 \times 10^0$	$6.1 \times 10^1$
C-14	c	$7.4 \times 10^0$

- a) Radionuclides released in amounts less than 1.0 Ci/GWe.year for noble gases are considered negligible and are not listed.
- b) Not applicable for LWR's.
- c) Not reported in "Radioactive Materials Released from Nuclear Power Plants" - NUREG-0139 (1976).

Ref. (15) TABLE C. 1.3

第4.1-8表 CRBRP-ERによる想定事故とソース・タームの概要

クラス*	事故区分	事故評価項目	照射期間 (年)	減衰時間	漏出物質	漏出量	漏洩率	酸素濃度 (%)	放出量	放出放射能	放射性物質の放出経路
1	軽微な故障	正常運転時に含まれる									
2	格納施設外の少量放出異常事象	1. 主復水器の機能喪失による蒸気ダンプ弁開放	30	-	SG系内の蒸気	-	-	-	45,000 lb	51 Ci	蒸気ダンプ弁→大気放出
		2. 復水貯蔵タンクの漏洩	30	-	復水貯蔵タンク水	-	10 gpm	-	$9.5 \times 10^{-8}$ Ci/min		復水貯蔵タンク→Clinch川
3	放射性廃棄物処理系の故障	1. 廃液貯蔵タンクの故障 (25%放出)	30**	-	中レベル廃液貯蔵水	5,000 gal (タンク容積の25%)	(蒸発)	-	** 37.5 gal	$2.7 \times 10^{-4}$ Ci	セル→RSB換気系→大気放出 (漏出液は正常なタンクに回収)
		2. 廃液貯蔵タンクの故障 (100%放出)	30**	-	中レベル廃液貯蔵水	20,000 gal (タンク容積の100%)	(蒸発)	-	** 150 gal	$1,008 \times 10^{-3}$ Ci	セル→RSB換気系→大気放出 (漏出液は正常なタンクに回収)
		3. RAPSサージタンクの破損	1**	0min	RAPSサージタンク内処理ガス	2,986 SCF	50 v/o/day at 10 psig	-	44 SCF 18 SCF	} 370 Ci	セル→RSB換気系→大気漏出
				20min							
				500min	カバーガス	?	-	-	2,000 SCF		34 Ci
4. カバーガス均圧配管の破損	1**	?	カバーガス	?	0.1 v/o/day at 10 psig	-	?	9.95 Ci	カバーガススペース→CAPS→大気放出		
4	保守作業中のナトリウム火災	1. 格納施設外1次ナトリウムドレン配管の破損	30	10 day	1次ナトリウム	130 lb	(火災)* 100 v/o/day at 10 psig	** 21	47 lb (Na <sub>2</sub> O)	0.04 Ci	セル→SGB換気系→大気放出
		2. EVSTナトリウム冷却系の故障	30	0min**	EVSTナトリウム	250 lb	(火災)** 100 v/o/day at 10 psig	** 21	95 lb (Na <sub>2</sub> O)	1.2 Ci	セル→RSB換気系→大気放出
5	1次及び2次冷却系へのFP放出	1. 設計以上の変動事象 (0.02%の希ガスとハロゲンの放出)	30	0min	平衡炉心燃料中の希ガスとハロゲン	インベントリの0.02%	?	-	?	$5.5 \times 10^{-3}$ Ci	正常運転時の大気放出と同一経路
		2. SG細管の破損事故 (1本)	30	-	SG系の水 2次ナトリウム SGの蒸気・水	-	-	-	138 lb 387 lb 5,040 lb	0.61 Ci	} SWRPS→大気放出 蒸気ダンプ弁→大気放出

クラス	事故区分	事故評価項目	照射期間 (年)	減衰時間	漏出物質	漏出量	漏洩率	酸素濃度 (%)	放出量	放出放射能	放射性物質の放出経路
6	燃料変換時の事故	1. EVTM内の照射済燃料被覆の破損(1%の希ガス, ハロゲン放出)	3**	87hr	SFの希ガスとハロゲン	インベントリの1% (燃料解体時)	? パーセント率は 0.97hr <sup>-1</sup>	-	-	1.1×10 <sup>-5</sup> Ci	燃料集合体→EVTM内部→RCB/RSB換気系→大気放出
		2. EVTM内の照射済燃料被覆の破損(100%の希ガス, ハロゲン放出)	3**	87hr	SFの希ガスとハロゲン	インベントリの100% (燃料解体時)	? パーセント率は 0.97hr <sup>-1</sup>	-	-	1.1×10 <sup>-3</sup> Ci	燃料集合体→EVTM内部→RCB/RSB換気系→大気放出
		3. ポートプラグ撤去時のフロア弁の誤開放操作	1**	30hr	炉上カバーガス	-	-	-	-	3.25Ci	カバースペース→RCB/RSB換気系→大気放出
7	照射済燃料取扱事故	1. 照射済燃料キャスクの落下事故	コア集合体3 ブランケット 集合体6	100day	SFの希ガス	インベントリの1%	-	-	-	38Ci**	キャスク→RSB換気系→大気放出
8	安全解析報告書の設計基準とした起因事象	1. 保守作業中の1次ナトリウム格納施設内ドレンタンクの故障	30	10day	1次ナトリウム	240,000ℓb (タンク容積の100%)	(火災) 0.1v/o/day at 10 psig	21**	1.6Kg (Na <sub>2</sub> O)	3.2×10 <sup>-3</sup> Ci	セル→RCB換気系→大気放出 (セルとRCB間は閉鎖されていない)
		2. 炉運転時の大量の1次ナトリウムの漏出事象	30	0min	1次ナトリウム	193,000ℓb	(火災) 0.1v/o/day at 10 psig	2	0.1Kg (Na <sub>2</sub> O)	9.5×10 <sup>-2</sup> Ci	HTSセル→BCB→アニュラス濾過系→大気放出(RCB換気系は停止)
		3. 格納施設外1次ナトリウム貯蔵タンクの大破損事故	30	10day	1次ナトリウム	600,000ℓb	(火災) 100v/o/day at 10 psig	2	3.0Kg (Na <sub>2</sub> O)	5.6×10 <sup>-3</sup> Ci	セル→SGB換気系→大気放出
		4. 炉運転時のEVSTナトリウム冷却系の破断事故	30	0min**	EVSTナトリウム	57,000ℓb	(火災) 100v/o/day at 10 psig	2	652g (Na <sub>2</sub> O)	1.9×10 <sup>-3</sup> Ci	セル→RSB換気系→大気放出
		5. 主蒸気管破断事故	30	-	SG系の蒸気・水	-	-	-	-	9,000ℓb 470,000ℓb	55Ci 配管 蒸気ダンプ弁 } →大気放出

注記) \* 区分はRegulatory Guide 4.2に従った。

\*\* CRBRP-ER本文中に記述なきため推測した数値。

? CRBRD-ER本文中に記述なきため推測不明なもの。

第 4.2 - 1 表

MAXIMUM INTERNAL WHOLE BODY DOSE RECEIVED BY AN INDIVIDUAL  
VIA EXPOSURE TO CRBRP GASEOUS EFFLUENTS

<u>Pathway</u>	<u>Location of Exposure</u>	<u>x/Q (sec/m<sup>3</sup>)</u>	<u>Dose (mrem/yr)</u>
Inhalation	Near side of river 2,500 feet NW of the Plant	$5.0 \times 10^{-5}$	$8.4 \times 10^{-3}$
Ingestion of milk	Closest dairy cow, 2 miles, WNW	$4.67 \times 10^{-6}$	$4.4 \times 10^{-1}$
Ingestion of leafy vegetables	Closest home garden, 0.6 mile, SSW	$9.69 \times 10^{-6}$	$3.5 \times 10^{-2}$
Ingestion of beef	Closest forage area 0.3 mile, S	$1.88 \times 10^{-5}$	$7.4 \times 10^{-2}$
Total			$5.6 \times 10^{-1}$

Ref. (1) AMENDMENT VIII TABLE 5.3-1

第 4.2 - 2 表

SUMMARY OF VARIABLES USED IN RADIOLOGICAL DOSE EVALUATIONS  
WHICH ARE NOT SPECIFIC TO THE CRBRP

<u>Variable</u>	<u>Description</u>	<u>Measurement</u>
<u>Ingestion of Leafy Vegetables</u>		
VDW	Deposition velocity of isotope over water	Noble gases, $0.5 \times 10^{-7}$ cm/sec <sup>(52)</sup> H-3, 5 cm/sec (53,54)
YC	Yield per unit of cultivated land area for leafy vegetables	1.5 kg/m <sup>2</sup> (55)
	Total acreage of leafy vegetable crops under cultivation within a 50-mile radius of the CRBRP	434 acres
TGS	Growing season of leafy vegetables	3 months <sup>(49)</sup>
VDL	Deposition velocity of isotope over land	Noble gases, $0.5 \times 10^{-7}$ cm/sec <sup>(52)</sup> H-3, 1.4 cm/sec(51)
TLV	Total daily intake of leafy vegetables	0.2 kg/day <sup>(49)</sup> for an individual or an average population
TDL	Elapsed time between harvest and ingestion	7 days <sup>(56)</sup>
T <sub>b</sub>	Weathering half-life of isotopes on leafy vegetables	14 days <sup>(55,57)</sup>
FLI	Fractional retention of isotope on vegetation leaves	0.1 <sup>(56)</sup>
FA	Average fraction of the ground surface covered by leafy vegetables	0.25 <sup>(49)</sup>

(Continued)



第 4.2 - 2 表

<u>Variable</u>	<u>Description</u>	<u>Measurement</u>	
		<u>Element</u>	<u>Coefficient</u> <sup>(55,58)</sup>
FRI	Transfer coefficient for soil to plant via roots	Fe	$1.5 \times 10^{-4}$
		Sr	$3.2 \times 10^{-1}$
		Ru	$3.8 \times 10^{-3}$
		Cs	$1.9 \times 10^{-2}$
		Ce	$7.5 \times 10^{-4}$
		Pu	$1.0 \times 10^{-4}$
FSI	Fraction of isotope which reaches soil	0.75 <sup>(49)</sup>	
R	Rate of ingestion of vegetation	Rabbit, 100 g/day <sup>(55)</sup>	
<u>Ingestion of Beef</u>			
G	Effective grazing area of cattle	20-80 m <sup>2</sup> /day <sup>(59)</sup> (45 m <sup>2</sup> /day used <sup>(62)</sup> )	
SUMFT <sub>B</sub>	Total cumulative fraction of isotope transferred per kg of beef	$2 \times 10^{-3}$ /kg for H-3 <sup>(55)</sup> 0.2/kg for Cs <sup>(60)</sup> 0.05/kg for Sr <sup>(60)</sup>	
TB	Total daily human intake of beef	0.04 kg/day for an individual <sup>(55)</sup> 0.14 kg/day for an average population <sup>(63)</sup>	
TDB	Elapsed time between butchering and ingestion	20 days <sup>(55)</sup>	
<u>Ingestion of Aquatic Foods</u>			
G <sub>F</sub>	Rate of ingestion of aquatic food for man	50 g/day - freshwater fish (max. for adult) <sup>(49)</sup>	
P	Rate of ingestion of aquatic foods for biota other than man	Ducks, surface feeding - 100 g/day of plants <sup>(61)</sup>	
		Ducks, diving - 100 g/day of fish <sup>(61)</sup>	

第 4.2 - 2 表

<u>Variable</u>	<u>Description</u>	<u>Measurement</u>
		Mink - 50 g/day of fish and 50 g/day if invertebrates <sup>(61)</sup>
MS	Average mass of organism feeding on aquatic food	Ducks - 1 kg <sup>(49,61)</sup> Mink - 1 kg <sup>(61)</sup> Muskrat - 1 kg <sup>(49)</sup> Raccoon - 12 kg <sup>(49)</sup> Heron - 4.6 kg <sup>(49)</sup>
TIM	Elapsed time between release and ingestion	0.5 days
	Average effective radius of organisms feeding on aquatic food	Ducks - 5 cm <sup>(49)</sup> Mink - 10 cm <sup>(61)</sup> Rabbit - 10 cm <sup>(61)</sup> Muskrat - 6 cm <sup>(49)</sup> Raccoon - 14 cm <sup>(49)</sup> Heron - 11 cm <sup>(49)</sup>
M	Average mass of aquatic organism	Fish - 1 kg <sup>(61)</sup> Invertebrates - 0.005 kg <sup>(61)</sup> Plant - 0.005 kg <sup>(61)</sup>
	Average effective radius of aquatic organism	Fish - 10 cm <sup>(61)</sup> Invertebrates - 2 cm <sup>(61)</sup> Plant - 2 cm <sup>(61)</sup>
<u>Exposure Via Above-Water Activities</u>		
TI	Time spent immersed in effluent water	100 hr/yr <sup>(49)</sup>
TAW	Time spent in above water activities	Boating - 100 hr/yr <sup>(49)</sup> Shoreline activities - 500 hr/yr <sup>(49)</sup>

第 4.2 - 2 表

<u>Variable</u>	<u>Description</u>	<u>Measurement</u>
SUMFT	Accumulative fractional intake if isotope per liter which is transferred to the milk each day	$2.0 \times 10^{-2}/1$ for H-3 <sup>(55)</sup>

Ref. (1) AMENDMENT VIII TABLE 5.3A-13

第 4.2 - 3 表

DOSE RATES RECEIVED BY AN INDIVIDUAL VIA  
EXPOSURE TO CRBRP LIQUID EFFLUENTS

mrem/yr

	<u>Pathway</u>			
	<u>Contaminated River Sediment</u>	<u>Immersion</u>	<u>Above-Water Activities</u>	<u>Ingestion of Aquatic Food</u>
Total Body Gamma	$7.20 \times 10^{-8}$	$1.62 \times 10^{-7}$	$4.87 \times 10^{-7}$	--
Total Skin	$8.48 \times 10^{-8}$	$2.01 \times 10^{-7}$	$6.04 \times 10^{-7}$	--
Whole Body Internal	--	--	--	$1.69 \times 10^{-2}$
Bone	--	--	--	$2.89 \times 10^{-5}$
GI Tract	--	--	--	$2.00 \times 10^{-4}$
Thyroid (Adult)	--	--	--	$6.51 \times 10^{-7}$
Kidney	--	--	--	$3.41 \times 10^{-5}$

Ref. (1) AMENDMENT VIII TABLE 5.3-2

第 4.2 - 4 表 気体状化学物質に関する環境基準の例

	日 本		茨城県公 害防止条令	福井県公 害防止条令	ソビエト		アメリカ	備 考
	大気汚染防止法 瞬 間	大気汚染防止法 平 均			瞬 間	日 平均	年 平均	
HF	-	-	0.25 mg/m <sup>3</sup> (*)	日平均 1 μg/m <sup>3</sup> 週平均 0.5 μg/m <sup>3</sup>	30 μg/m <sup>3</sup> (**)	10 μg/m <sup>3</sup> (**)	0.5 μg/m <sup>3</sup>	(*) 敷地境界 (**) フッ素として
SO <sub>2</sub>	0.1 ppm	年平均 0.05 ppm	-	-	500	150	80	
NO <sub>x</sub>	-	日平均 0.02 ppm (*)	-	-	300 (**)	100 (**)	100	(*) NO <sub>2</sub> として (**) N <sub>2</sub> O <sub>5</sub> として
粒子	0.2 mg/m <sup>3</sup> (*)	日平均 0.10 mg/m <sup>3</sup> (*)	1.5 mg/m <sup>3</sup> (**)	-	500	150	75	(*) 10 μm以下の粒子 (**) 一般粉じん
C <sub>2</sub> H <sub>5</sub> OH	-	-	-	-	-	-	1.9 × 10 <sup>6</sup>	
CO	-	日 10 ppm 8-hr 20 ppm	-	-	6 × 10 <sup>3</sup>	1 × 10 <sup>3</sup>	1 × 10 <sup>4</sup>	
炭化水素	-	-	-	-	-	-	1.6 × 10 <sup>2</sup>	
塩素	-	-	-	-	100	50	-	

第 4.2 - 5 表 茨城県における気体状汚染物の排出基準  
(茨城県公害防止条例施行規則)

(a) ばい煙に係る有害物質の排出基準

ばい煙に係る有害物質の排出基準は、温度が零度であって圧力が1気圧の状態に換算した排出ガス1立方メートルにつき、次の表の第2欄に掲げる有害物質の種類及び同表の第3欄に掲げる施設の種類の種類ごとに同表の第4欄に掲げる有害物質の量とする。

項	有害物質の種類	ばい煙に係る特定施設	有害物質の量
1	アンモニア	尿素の製造の用に供する施設	270ミリグラム
2	シアン化水素	1. コークス炉及びこれに付属する施設 2. シアン化合物を用いる電気メッキ施設 3. シアン化合物を用いる金属の熱処理施設	10ミリグラム
3	ホスゲン	1. ホスゲンを用いる医薬品製造施設 2. トリレン・ジ・インシアネート製造施設	4ミリグラム
4	ホルムアルデヒド	1. ホルマリン製造施設 2. フェノール樹脂製造施設	30ミリグラム

備考 1 測定点は、ばい煙に係る特定施設の排出口(ばい煙に係る特定施設において発生するばい煙を大気中に排出するために設けられた煙突その他の施設の開口部をいう。)とする。

(b) 粉じんの排出基準

粉じんの排出基準は、1立方メートルにつき、次の表の第2欄に掲げる粉じんの種類及び同表の第3欄に掲げる施設の種類の種類ごとに同表の第4欄に掲げる粉じんの量とする。

項	粉じんの種類	粉じんに係る施設	粉じんの量	
			排出口	敷地境界線上
1	シアン化物 (シアンとして)	条例第2条第4項の特定施設の うち粉じんに係るもの及び大気 汚染防止法(昭和43年法律第 97号)第2条第5項の粉じん 発生施設	5ミリグラム	0.5ミリグラム
2	ふっ 弗化物 (弗素として)		2.5ミリグラム	0.25ミリグラム
3	マンガン		5ミリグラム	0.5ミリグラム
4	一般粉じん		15ミリグラム	1.5ミリグラム

第4.2-6表 わが国の環境水中基準  
(昭和50年環境庁告示3)

(a) 人の健康に係る環境基準(最高値)

項目	シアン	アルキル水銀	有機リン	カドミウム	鉛	クロム(6価)	ヒ素	総水銀
基準値	検出されないこと	検出されないこと	検出されないこと	0.01PPm以下	0.1PPm以下	0.05PPm以下	0.05PPm以下	0.0005PPm以下

(b) 生活環境の保全に関する環境基準(海域)

日平均値

項目 類型	利用目的の 適応性	基準値					該当水域
		水素イオン濃度(PH)	化学的酸素要求量(COD)	溶存酸素量(DO)	大腸菌群数	n-ヘキサン抽生物質(油分等)	
A	水産1級 水浴 およびB以下の欄に掲げるもの	7.8以上 8.3以下	2ppm以下	7.5ppm以上	1,000 MPN/100 ml以下	検出されないこと。	第1の2の(2)により水域類型ごとに指定する水域
B	水産2級 工業用水 およびCの欄に掲げるもの	7.8以上 8.3以下	3ppm以下	5ppm以上		検出されないこと。	
C	環境保全	7.0以上 8.3以下	8ppm以下	2ppm以上	-	-	

(注) 1 水産1級: マダイ, ブリ, ワカメ等の水産生物用および

水産2級の水産生物用

// 2級: ポラ, ノリ等の水産生物用

2 環境保全: 国民の日常生活(沿岸の遊歩等を含む。)に

おいて不快感を生じない限度

第 4.2 - 7 表 那珂川水域（那珂川，早戸川，大井川，中丸川，大川，本郷川及び新川並びに那珂川以外のこれらの河川に流入することとなる公共用水域）における汚水の排水基準

区 分			水素イオン濃度 (水素指数)	生 活 環 境 項 目											
				生物化学的酸素要求量 (単位1リットルにつきミリグラム)		化学的酸素要求量 (単位1リットルにつきミリグラム)		浮遊物質 (単位1リットルにつきミリグラム)		ノルマルヘキサン抽出物質含有量 (鉱油類含有量) (単位1リットルにつきミリグラム)	ノルマルヘキサン抽出物質含有量 (動植物油脂類含有量) (単位1リットルにつきミリグラム)	フェノール類含有量 (単位1リットルにつきミリグラム)	銅含有量 (単位1リットルにつきミリグラム)	亜鉛含有量 (単位1リットルにつきミリグラム)	
				日間平均	最 大	日間平均	最 大	日間平均	最 大	最 大	最 大	最 大	最 大	最 大	
工場 又は 事業場	第一種水域	新設のもの	5.8以上 8.6以下	10	15	10	15	20	25	5	5	0.5	3	5	
		既設のもの	5.8以上 8.6以下	25	30	25	30	40	50	5	10	1	3	5	
	第二種水域	新設のもの	1日当たりの平均的な排水の量が1,000立方メートル未満のもの	5.8以上 8.6以下	20	25	20	25	30	40	5	10	1	3	5
			1日当たりの平均的な排水の量が1,000立方メートル以上のもの	5.8以上 8.6以下	10	15	10	15	20	25	5	5	0.5	3	5
		既設のもの	1日当たりの平均的な排水の量が1,000立方メートル未満のもの	5.8以上 8.6以下	30	40	30	40	50	65	5	10	1	3	5
			1日当たりの平均的な排水の量が1,000立方メートル以上のもの	5.8以上 8.6以下	20	25	20	25	30	40	5	5	1	3	5
生 活 環 境 項 目					健 康 項 目										
溶解性鉄含有量 (単位1リットルにつきミリグラム)	溶解性マンガ含有量 (単位1リットルにつきミリグラム)	クロム含有量 (単位1リットルにつきミリグラム)	弗素含有量 (単位1リットルにつきミリグラム)	大腸菌群数 (単位1立方センチメートルにつき個)	カドミウム及びその化合物 (単位1リットルにつきミリグラム)	シアン化合物 (単位1リットルにつきミリグラム)	有機磷化合物 (パラチオン，メチルパラチオン，メチルジメトン及びEPNに限る) (単位1リットルにつきミリグラム)	鉛及びその化合物 (単位1リットルにつきミリグラム)	六価クロム化合物 (単位1リットルにつきミリグラム)	砒素及びその化合物 (単位1リットルにつきミリグラム)	水銀及びアルキル水銀その他の水銀化合物 (単位1リットルにつきミリグラム)	アルキル水銀化合物 (単位1リットルにつきミリグラム)			
最 大	最 大	最 大	最 大	日間平均	最 大	最 大	最 大	最 大	最 大	最 大	最 大	最 大			
10	1	1	8	3,000	0.1	検出されないこと。	1	1	0.5	0.5	水銀につき検出されないこと。	検出されないこと。			
10	1	1	8	3,000	0.1	検出されないこと。	1	1	0.5	0.5	水銀につき検出されないこと。	検出されないこと。			
10	1	1	8	3,000	0.1	0.5	1	1	0.5	0.5	水銀につき検出されないこと。	検出されないこと。			
10	1	1	8	3,000	0.1	0.5	1	1	0.5	0.5	水銀につき検出されないこと。	検出されないこと。			
10	1	1	8	3,000	0.1	0.5	1	1	0.5	0.5	水銀につき検出されないこと。	検出されないこと。			
10	1	1	8	3,000	0.1	0.5	1	1	0.5	0.5	水銀につき検出されないこと。	検出されないこと。			



第 4.2 - 8 表

一般騒音に関する基準（昭和 46 年 5 月閣議決定）

地 域	昼 間	朝 ・ 夕	夜 間
特に静穏を要する 地域	< 45 ホン(A)	< 40 ホン(A)	< 35 ホン(A)
主として居住を目的とする地域	50 //	< 45 //	< 40 //
相当数の住居と商、 工業もある地域	< 60 //	< 55 //	< 50 //

第4.2-9表 茨城県における騒音に係る特定施設

を設置する工場等に関する規制基準

区域の区分	時間の区分	昼 間	朝 ・ 夕	夜 間
第1種区域		50ホン	45ホン	40ホン
第2種区域		55ホン	50ホン	45ホン
第3種区域		65ホン	60ホン	50ホン
第4種区域		70ホン	65ホン	55ホン
第5種区域		75ホン	75ホン	65ホン

備考

- 1 昼間とは午前8時から午後6時まで、朝・夕とは午前6時から午前8時まで、及び午後6時から午後10時まで、夜間とは午後10時から翌日午前6時までをいう。
- 2 ホンとは、計量法（昭和26年法律第207号）第5条第44号に定める騒音の大きさの計量単位をいう。
- 3 第1種区域、第2種区域、第3種区域、第4種区域及び第5種区域とは、それぞれ次の各号に掲げる区域とする。
  - (1) 第1種区域 都市計画法第8条第1項第1号に規定する第1種住居専用地域
  - (2) 第2種区域 都市計画法第8条第1項第1号に規定する第2種住居専用地域及び住居地域
  - (3) 第3種区域 都市計画法第8条第1項第1号に規定する近隣商業地域、準工業地域及び都市計画法による用途地域の指定のない地域
  - (4) 第4種区域 都市計画法第8条第1項第1号に規定する工業地域
  - (5) 第5種区域 都市計画法第8条第1項第1号に規定する工業専用地域
- 4 第5種区域についての規制基準は、第5種区域から他の区域に排出される場合のみ適用されるものとする。
- 5 第2種区域、第3種区域又は第4種区域の区域内に所在する学校教育法第1条に規定する学校、児童福祉法第7条に規定する保育所、医療法第1項に規定する病院及び同条第2項に規定する診療所のうち患者の収容施設を有するもの、図書館法第2条第1項に規定する図書館並びに老人福祉法第14条第1項第2号に規定する特別養護老人ホームの敷地の周囲おおむね50メートルの区域内における基準値は、当該欄に定める値から5ホンを減じた値とする。

第5-1表 「NUJEEP」コード開発の進展<sup>(34)</sup>

開 発 段 階	主 要 な 特 徴
<p>Phase I (昭和52年8月)</p>	<ol style="list-style-type: none"> <li>1. 「HERMES」コードを参考に、日本独自の状況が取扱えるような放射性物質の拡散・輸送モデルの開発</li> <li>2. ATR を含めた原子力発電経済モデルの作成とLP（線型計画法）による最適炉型戦略の決定</li> <li>3. 食物の生産，流通，消費データの収集と評価</li> <li>4. ボックスモデルによる放射性物質海洋拡散のシミュレーション</li> </ol>
<p>Phase II (昭和53年8月)</p>	<ol style="list-style-type: none"> <li>1. 原子力発電経済モデルで、軽水炉特性評価の詳細化，プルトニウムバランス式評価精度の向上，評価関数の多様化を実施</li> <li>2. ATR の放出モデルの追加</li> <li>3. 生活様式モデルのデータの整備と拡張</li> <li>4. 大気中濃度計算の精度の向上</li> <li>5. 潮流拡散及び地表水拡散モデルの開発</li> </ol>
<p>Phase III (昭和54年3月)</p>	<ol style="list-style-type: none"> <li>1. 原子力発電経済モデルでのCANDU炉の追加感度分析モデルの開発</li> <li>2. 混合酸化物燃料加工施設からの放出モデルの開発</li> <li>3. 再処理施設からの放射性物質放出量の低減化シミュレーション</li> <li>4. 大気拡散における地形の影響についての検討</li> <li>5. 海洋拡散モデルの整備</li> </ol>

第5-2表 「DOSIS」で取扱われている核種とその性質<sup>(33)</sup>

	核 種	半 減 期	空 気 中 放 出	水 中 放 出
1	H - 3	12.26 y	○	○
2	N - 13	9.96m	○	
3	C - 14	5730.0 y	○	○
4	Na - 22	2.6 y	○	○
5	Na - 24	15.0 h	○	○
6	Ar - 39	270.0 y	○	
7	Ar - 41	1.83h	○	
8	Cr - 51	27.8 d		○
9	Mn - 54	312.0 d		○
10	Fe - 55	2.4 y		○
11	Fe - 59	45.0 d		○
12	Co - 58	71.0 d		○
13	Co - 60	5.24y		○
14	Ni - 63	92.0 y		○
15	Cu - 64	12.9 h		○
16	Zn - 65	243.0 d		○
17	Kr - 85m	4.4 h	○	
18	Kr - 85	10.76y	○	
19	Kr - 87	76 m	○	
20	Kr - 88	2.8 h	○	
21	Sr - 89	50.6 d	○	○
22	Sr - 90	28.8 y	○	○
23	Zr - 95	65.0 d	○	○
24	Nb - 95	35.0 d	○	○
25	Mo - 99	67.0 h		○
26	Ru - 103	40.0 d	○	○
27	Ru - 106	1.0 y	○	○
28	Te - 132	78.0 h	○	○
29	I - 129	1.6×10 <sup>7</sup> y	○	○
30	I - 131	8.05d	○	○
31	I - 132	2.3 h	○	○
32	I - 133	21.0 h	○	○
33	I - 135	6.7 h	○	○
34	Xe - 131m	12.0 d	○	
35	Xe - 133m	2.3 d	○	
36	Xe - 133	5.27d	○	
37	Xe - 135m	16.0 m	○	
38	Xe - 135	9.2 h	○	
39	Xe - 138	17.0 m	○	
40	Os - 134	2.1 y	○	○
41	Cs - 137	30.0 y	○	○
42	Ba - 140	12.8 d	○	○
43	La - 140	40.2 h	○	○
44	Ce - 141	32.5 d	○	○
45	Ce - 144	285.0 d	○	○

○ ; 考慮する

第5-3表 累積核分裂収率と放射化物の生成関連係数<sup>(33)</sup>

核種名	累積核分裂収率 Yf atm/fiss			放射化物の生成関連係数 KI		
	U-235	U-238	Pu-239	構造材	被覆材	冷却材
H - 3	0.013-2*	0.020-2	0.025-2			
N - 13						
C - 14				1.63+3	4.08+2	
Na - 22						6.0 -3
Na - 24						7.5 +8
Ar - 39						4.75+6
Ar - 41						6.75+8
Cr - 51				7.90+9	1.98+9	
Mn - 54				-	6.90+9	
Fe - 55				6.60+9	1.66+9	
Fe - 59				1.57+8	1.87+7	
Co - 58				-	1.12+10	
Co - 60				1.66+9	4.58+8	
Ni - 63				3.70+9	9.28+8	
Cu - 64				-	-	
Zn - 65				-	-	
Kr - 85m	1.243-2	0.737-2	0.515-2			
Kr - 85	0.343-2	0.170-2	0.142-2			
Kr - 87	2.49 -2	1.72 -2	0.92 -2			
Kr - 88	3.57 -2	2.12 -2	1.42 -2			
Sr - 89	4.79 -2	3.33 -2	1.72 -2			
Sr - 90	5.77 -2	3.23 -2	2.21 -2			
Zr - 95	6.2 -2	5.85 -2	4.97 -2			
Nb - 95	6.2 -2	5.85 -2	4.97 -2			
Mo - 99	6.06 -2	6.62 -2	6.10 -2	1.04+8	2.60+7	
Ru -103	3.0 -2	5.86 -2	5.67 -2			
Ru -106	0.38 -2	2.83 -2	4.57 -2			
Te -132	4.24 -2	4.44 -2	5.10 -2			
I -129	1.0 -2	0.888-2	1.70 -2			
I -131	2.93 -2	3.23 -2	3.78 -2			
I -132	4.36 -2	4.74 -2	5.26 -2			
I -133	6.61 -2	5.55 -2	6.53 -2			
I -135	6.09 -2	4.51 -2	5.70 -2			
Xe -131m	0.023-2	0.025-2	0.030-2			
Xe -133m	0.159-2	0.133-2	0.158-2			
Xe -133	6.61 -2	5.55 -2	6.53 -2			
Xe -135m	1.83 -2	1.53 -2	1.71 -2			
Xe -135	6.41 -2	4.61 -2	7.17 -2			
Xe -138	5.78 -2	5.56 -2	6.31 -2			
Cs -134	6.61 -2**	5.55 -2**	6.53 -2**			
Cs -137	6.15 -2	6.36 -2	6.63 -2			
Ba -140	6.35 -2	6.06 -2	5.56 -2			
La -140	6.35 -2	6.06 -2	5.56 -2			
Ce -141	6.4 -2	5.54 -2	5.09 -2			
Ce -144	5.62 -2	4.34 -2	3.93 -2			

注記) \*  $0.013 \times 10^{-2}$  を意味する。

\*\* Xe-133 の値。

第5-4表 気/液分離係数 除染係数及び冷却材中への核種漏出補正係数<sup>(33)</sup>

核種名	気/液分離係数	除 染 係 数			冷却材中への核種漏出補正係数Kd
	K <sub>sp</sub>	DF <sub>C</sub>	DF <sub>G</sub>	DF <sub>F</sub>	
H - 3	1.01 <sup>-6</sup> *	10	1	1	1.0
N - 13	1.0	1	1	1	1.0
C - 14	1.0 <sup>-5</sup>	10	1	1	1.0
Na - 22	1.0 <sup>-4</sup>	1	1	1	1.0
Na - 24	1.0 <sup>-4</sup>	1	1	1	1.0
Ar - 39	1.0	1	1	1	1.0
Ar - 41	1.0	1	1	1	1.0
Cr - 51	0	10	1	2	1.0
Mn - 54	0	10	1	2	1.0
Fe - 55	0	10	1	2	1.0
Fe - 59	0	10	1	2	1.0
Co - 58	0	10	1	2	1.0
Co - 60	0	10	1	2	1.0
Ni - 63	0	10	1	2	1.0
Cu - 64	0	10	1	2	1.0
Zn - 65	0	10	1	2	1.0
Kr - 85 <sup>m</sup>	1.0	1	300	1	1.0
Kr - 85	1.0	1	300	1	1.0
Kr - 87	1.0	1	300	1	1.0
Kr - 88	1.0	1	300	1	1.0
Sr - 89	5.0 <sup>-6</sup>	10	1	2	1.09 <sup>-5</sup>
Sr - 90	5.0 <sup>-6</sup>	10	1	2	2.70 <sup>-7</sup>
Zr - 95	5.0 <sup>-6</sup>	10	1	2	1.54 <sup>-7</sup>
Nb - 95	5.0 <sup>-6</sup>	10	1	2	6.32 <sup>-8</sup>
Mo - 99	5.0 <sup>-6</sup>	10	1	2	3.50 <sup>+1</sup>
Ru - 103	5.0 <sup>-8</sup>	10	1	2	1.0
Ru - 106	5.0 <sup>-8</sup>	10	1	2	1.0
Te - 132	2.0 <sup>-5</sup>	10	1	2	1.32
I - 129	2.0 <sup>-5</sup>	10	1	1	86.1
I - 131	2.0 <sup>-5</sup>	10	1	1	86.1
I - 132	2.0 <sup>-5</sup>	10	1	1	262.0
I - 133	2.0 <sup>-5</sup>	10	1	1	262.0
I - 135	2.0 <sup>-5</sup>	10	1	1	932.0
Xe - 131 <sup>m</sup>	1.0	1	300	1	1.0
Xe - 133 <sup>m</sup>	1.0	1	300	1	1.0
Xe - 133	1.0	1	300	1	1.0
Xe - 135 <sup>m</sup>	1.0	1	300	1	1.0
Xe - 135	1.0	1	300	1	1.0
Xe - 138	1.0	1	300	1	1.0
Cs - 134	2.0 <sup>-5</sup>	10	1	2	0.224
Cs - 137	2.0 <sup>-5</sup>	10	1	2	0.92
Ba - 140	0	10	1	2	3.24 <sup>-5</sup>
La - 140	0	10	1	2	0.90 <sup>-5</sup>
Ce - 141	0	10	1	2	0.92 <sup>-8</sup>
Ce - 144	0	10	1	2	0.92 <sup>-8</sup>

注記) \* 1.01×10<sup>-6</sup>を意味する。

第 5 - 5 表 出力分布と燃料比率の関係 <sup>(33), (35)</sup>

X	出力分布関数値	燃 料 比 率	
	$\phi(X)$	$W_R(X)$	$W_Z(X)^*$
1	1.00	0.01	0.02
2	0.95	0.03	0.16
3	0.90	0.06	0.07
4	0.85	0.08	0.06
5	0.80	0.11	0.05
6	0.75	0.15	0.05
7	0.70	0.17	0.07
8	0.65	0.13	0.19
9	0.60	0.11	0.18
10	0.55	0.15	0.15

注記) \* HERMES より。

第5-6表 使用核種と半減期, 崩壊定数<sup>(32), (35)</sup>

核種名	半減期 (sec)	崩壊定数* (sec <sup>-1</sup> )	備考	
H - 3	3.8660+8**	1.793-9	FP	
N - 13	5.9760+2	1.160-3	冷却材放射化物	
C - 14	1.8070+11	3.836-12		
Na - 22	8.1990+7	8.454-9	冷却材放射化物	
Na - 24	5.4000+4	1.284-5		
Ar - 39	8.5150+9	8.141-11		
Ar - 41	6.5830+3	1.052-4		
Cr - 51	2.4020+6	2.886-7		
Mn - 54	2.6960+7	2.571-8	腐食放射化物	
Fe - 55	7.5690+7	9.158-9		
Fe - 59	3.8880+6	1.783-7		
Co - 58	6.1340+6	1.130-7		
Co - 60	1.6520+8	4.196-9		
Ni - 63	2.9010+9	2.389-10		
Cu - 64	4.6440+4	1.493-5		
Zn - 65	2.0990+7	3.302-8		
Kr - 85m	1.5840+4	4.376-5		
Kr - 85	3.3930+8	2.043-9		
Kr - 87	4.5600+3	1.520-4	腐食放射化物を含む。	
Kr - 88	1.0080+4	6.876-5		
Sr - 89	4.3720+6	1.585-7		
Sr - 90	9.0820+8	7.632-10		
Zr - 95	5.6160+6	1.234-7		
Nb - 95	3.0240+6	2.292-7		
Mo - 99	2.4120+5	2.874-6		
Ru - 103	3.4560+6	2.006-7		
Ru - 106	3.1540+7	2.198-8		
Te - 132	2.8080+5	2.468-6		
I - 129	5.0460+14	1.374-15		FP
I - 131	6.9550+5	9.966-7		
I - 132	8.2800+3	8.371-5		
I - 133	7.5600+4	9.169-6		
I - 135	2.4120+4	2.874-5		
Xe - 131m	1.0370+6	6.684-7		
Xe - 133m	1.9870+5	3.488-6		
Xe - 133	4.5530+5	1.522-6		
Xe - 135m	9.6000+2	7.220-4		
Xe - 135	3.3120+4	2.093-5		
Xe - 138	1.0200+3	6.796-4		
Cs - 134	6.6230+7	1.047-9		
Cs - 137	9.4610+8	7.327-10		
Ba - 140	1.1060+6	6.267-7		
La - 140	1.4470+5	4.790-6		
Ce - 141	2.8060+6	2.470-7		
Ce - 144	2.4620+7	2.815-8		

注記) \* HERMESより。  
\*\* 3.8660×10<sup>8</sup>を意味する。



第5-7表 1000MWe LMFBRからの放射性廃棄物放出率(稼働率100%の場合)<sup>(32)</sup>

ISOTOPE	TYPICAL LMFBR LOGG MWE HALF LIFF (SEC)	PLANT RELEASES DURING OPERATION AT 1.000 PLANT FACTOR		GASEOUS RELEASES		
		COOLANT CONCENTRATION (PICOCURIES/LITER)	LIQUID RELEASES (PICOCURIES/SEC)	(PICOCURIES/SEC)	(FRACTION)	
H3	3.8660E 08	2.4674E 06	0.0	0.0	1.1053E 01	1.2206E-06
N13	5.9760E 02	0.0	0.0	0.0	0.0	0.0
C14	1.8070E 11	7.6883E-05	0.0	0.0	3.4597E-09	3.8206E-10
NA22	8.1950E 07	5.9488E 07	0.0	0.0	1.4762E 01	1.6302E-06
NA24	5.4000E 04	5.2617E 09	0.0	0.0	7.1283E-09	7.8719E-10
AR39	8.5150E 09	0.0	0.0	0.0	3.2533E 06	3.5926E-01
AR41	6.5830E 03	0.0	0.0	0.0	7.2525E-21	8.0090E-26
CR51	2.4020E 06	5.1841E 05	0.0	0.0	0.0	0.0
MN54	2.6960E 07	3.6983E 05	0.0	0.0	0.0	0.0
FE55	7.5650E 07	2.6827E 05	0.0	0.0	0.0	0.0
FE59	3.8880E 06	1.0231E 04	0.0	0.0	0.0	0.0
CO58	6.1340E 06	1.2365E 06	0.0	0.0	0.0	0.0
CC60	1.6520E 08	4.9898E 04	0.0	0.0	0.0	0.0
NI63	2.9010E 09	1.0498E 04	0.0	0.0	0.0	0.0
CU64	4.6440E 04	0.0	0.0	0.0	0.0	0.0
ZN65	2.0950E 07	0.0	0.0	0.0	0.0	0.0
KR5M	1.5840E 04	0.0	0.0	0.0	1.1512E-24	1.2713E-31
KR85	3.3930E 08	0.0	0.0	0.0	6.6377E 05	7.3301E-02
KR87	4.5600E 03	0.0	0.0	0.0	1.0205E-24	1.1270E-31
KR88	1.0080E 04	0.0	0.0	0.0	1.8634E-24	2.0578E-31
SR89	4.3720E 06	2.7339E 07	0.0	0.0	2.0610E 02	2.2700E-05
SR90	9.0820E 08	2.9010E 05	0.0	0.0	3.2573E 00	3.5971E-07
ZR95	5.6160E 06	1.0869E 07	0.0	0.0	8.9532E 01	9.8072E-06
NB95	3.0240E 06	1.0213E 07	0.0	0.0	1.1092E 02	1.2249E-05
MO99	2.4120E 05	3.1870E 10	0.0	0.0	2.4856E 02	2.7449E-05
RU03	3.4560E 06	2.3054E 10	0.0	0.0	1.6168E 03	1.7855E-04
RU06	3.1540E 07	9.7648E 09	0.0	0.0	1.0392E 03	1.1476E-04
TE32	2.8080E 05	4.0681E 09	0.0	0.0	3.5527E 02	3.9233E-05
I129	5.0460E 14	4.1419E 02	0.0	0.0	3.7278E-02	4.1166E-09
I131	6.9550E 05	5.4845E 10	0.0	0.0	3.9762E 05	4.3909E-02
I132	8.2800E 03	5.3207E 09	0.0	0.0	7.3212E 02	8.0849E-05
I133	7.5600E 04	6.6011E 10	0.0	0.0	4.5664E-04	5.0428E-11
I135	2.4120E 04	4.4691E 10	0.0	0.0	4.6628E-24	5.1492E-31
X131	1.0370E 06	0.0	0.0	0.0	1.8497E 05	2.0427E-02
X33M	1.9870E 05	0.0	0.0	0.0	9.1080E 02	1.0058E-04
X133	4.5530E 05	0.0	0.0	0.0	4.4935E 06	4.9622E-01
X35M	9.6000E 02	0.0	0.0	0.0	3.8492E-21	4.2507E-26
X135	3.3120E 04	0.0	0.0	0.0	2.7090E-15	2.9916E-22
X138	1.0200E 03	0.0	0.0	0.0	2.1169E-24	2.3377E-31
CS34	6.6230E 07	6.2313E 08	0.0	0.0	2.7310E 04	3.0159E-03
CS37	9.4610E 08	6.5926E 08	0.0	0.0	2.9612E 04	3.2701E-03
BA40	1.1060E 06	6.5144E 07	0.0	0.0	0.0	0.0
LA40	1.4470E 05	2.5585E 07	0.0	0.0	0.0	0.0
CE41	2.8060E 06	1.4935E 06	0.0	0.0	0.0	0.0
CE44	2.4620E 07	2.0256E 06	0.0	0.0	0.0	0.0
TOTAL	RELEASES (PICOCURIES/SEC)				9.0554E 06	