

実証炉設計用統合炉定数の整備（その4）

〈「もんじゅ」炉物理試験データ解析〉

（動力炉・核燃料開発事業団 契約業務報告書）

1997年3月

高速炉エンジニアリング株式会社

複製又はこの資料の入手については、下記にお問い合わせください。

〒311-13 茨城県東茨城郡大洗町成田町4002

動力炉・核燃料開発事業団

大洗工学センター システム開発推進部・技術管理室

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動力炉・核燃料開発事業団 (Power Reactor and Nuclear Fuel Development Corporation)

PNC-TJ9263 97-001

1997年 3月

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坪井靖^{*}、亀井孝信^{*}

要　　旨

実証炉設計用統合炉定数作成の一環として、「もんじゅ」炉物理試験で得られた臨界性及び制御棒価値に関し、試験データ及びその解析結果をレビューし、測定誤差、解析誤差を評価した。また、これらの特性（臨界性及び制御棒価値）に対する種々の断面積の感度係数を一般化摂動コード SAGEP により求めた。

ここで得られた測定誤差、解析誤差、C/E 値、及び感度係数は、本研究シリーズの他の部分で JENDL 3.2 の断面積調整に活用される。

本報告書は、高速炉エンジニアリング株式会社が動力炉・核燃料開発事業団との契約により実施した業務の成果である。

契約番号 : 08-C-3364

事業団担当部課室及び担当者：大洗工学センター基盤技術開発部 炉心技術開発室 石川 真

* 高速炉エンジニアリング株式会社 技術部

PNC-TJ9263 97-001

MARCH, 1997

Preparation of Unified Cross Section Library
for Demonstration Fast Breeder Reactor (IV)

—Analysis of Reactor Physics Experiment in Monju System Startup Test—

Yasushi Tsuboi*, Takanobu Kamei*

Abstract

Along the line of work of preparing unified cross-section library for demonstration fast breeder reactors, Monju criticality and control rod worth experimental data and their analysis were reviewed to evaluate experimental and analysis errors to apply the data in the cross-section adjustment work.

The sensitivity coefficients of each cross-section for criticality and control rod worth were calculated by use of the generalized perturbation code SAGEP. The C/E values ,experimental and analysis errors, and sensitivity coefficients are utilized in the adjustment of JENDL 3.2 in the other part of this series of work.

Work performed by FBR Engineering Co., Ltd. under contract with Power Reactor and Nuclear Fuel Development Corporation

PNC Liaison : Makoto Ishikawa, Reactor Physics Research Section,
Advanced Technology Division, O-arai Engineering Center

* Engineering Department, FBR Engineering Co., Ltd.

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1. はじめに

近年、臨界実験解析などの炉物理研究の成果を大型炉炉心の核設計に反映する手法として、ベイスの定理を基礎とした炉定数調整法が採用されている。動力炉・核燃料事業団は、1989～1991年度に日本原子力発電株式会社との共同研究として、JENDL-2ベースの基本炉定数を用いて JUPITER 実験解析の結果を反映した修正炉定数を作成した。

この 1991 年度版の修正炉定数は、従来問題であった制御棒価値及び出力分布の C/E 値径方向依存性や Na ボイド反応度の過大評価などを大幅に是正して、かなりの程度で核設計精度を向上させることができ、これまで、日本原子力発電株式会社の実証炉最適化設計研究や動力炉・核燃料事業団の大型炉設計研究において有效地に利用されてきた。しかし、この 1991 年度版は、積分データとして JUPITER 実験のみを用いていること、燃焼核特性や温度核特性を扱っていないこと、基本ライブラリが 1980 年代前半に作成された JENDL-2 ベースであったこと、非弾性散乱マトリックスの調整を行っていないことなどの改良点が明らかになっています。こうした観点から、実証炉の基本設計のような、より高度な精度が要求される設計段階においては、最新の研究成果を反映して、炉定数に改良を施す必要があることが認識されている。

本研究は、上記の背景の基で、1994 年に公開された我が国最新のライブラリである JENDL-3.2 を対象とし、動力炉・核燃料事業団が所有している「もんじゅ」炉物理試験データや「常陽」性能試験・運転特性データ、及び JUPITER 以外にこれまでの炉物理研究で蓄積してきた MOZART や ZPPR-2, 3 の臨界実験データまで積分データを拡張し、さらに燃焼核特性・温度核特性までその評価対象を広げて、予測精度及び信頼性を向上させることにより、実証炉の基本設計から許認可まで一貫して使用できる統合炉定数を作成することを目的とする。

本件では、この実証炉設計用統合炉定数の整備の（その 4）として、臨界実験データを補完する実機データとして、「もんじゅ」炉物理試験データに着目し、その実測データ及び解析結果をレビューする。そして、臨界性や制御棒価値などの核特性に関し、炉定数調整計算に使うための測定誤差や解析誤差の評価を行うとともに、これら核特性に対する断面積の感度係数の計算を行い、炉定数調整用積分データとして整備する。

2. 「もんじゅ」炉物理試験データ解析

2.1 「もんじゅ」炉物理試験データの整理

JENDL-3.2 の調整に資すべきもんじゅの SST 試験データを選定するために、日本原子力学会の春、秋の大会で報告されたもんじゅ性能試験データをレビューし、JENDL-2 を使用して得られた C/E 値に関して調査を行った。

(1) 臨界性

初臨界炉心の臨界時制御棒位置、及び挿入制御棒の反応度価値測定データから制御棒全引抜き時の過剰反応度を測定。

参照データ 1994 年 秋の大会 G 9 初臨界炉心特性、 G 10 臨界性予測解析

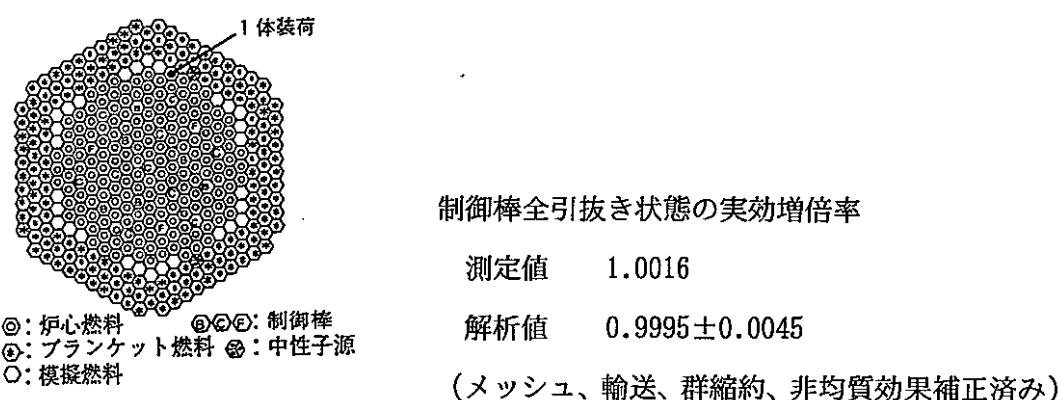


図 2.1-1 初臨界炉心 (168 体) C/E 値 0.998

尚、198 体初期炉心の臨界性の解析は、JENDL3.2 を用いて行われており、その結果は、1996 年秋の大会(A53)で報告されている。

(2) 燃料等価反応度

炉心燃料集合体を模擬燃料集合体と置換し、下記データが得られている。

参照データ 1995 年 春の年会 C 2 燃料等価反応度 (初期炉心)

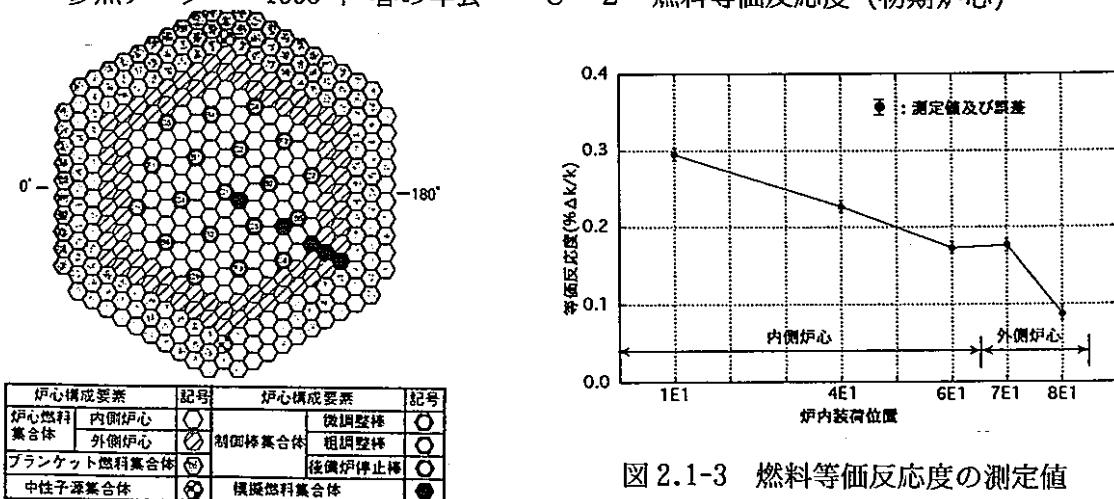


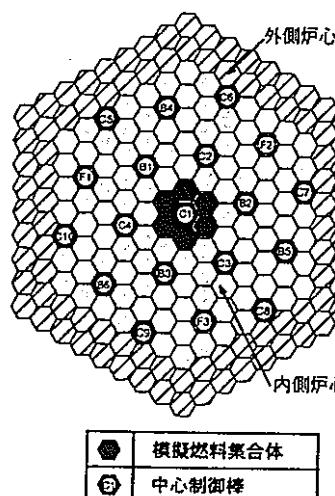
図 2.1-2 模擬燃料集合体の炉心装荷位置

図 2.1-3 燃料等価反応度の測定値

(3)冷却材反応度

炉心中心部で冷却材の占める割合が異なる模擬燃料集合体(Na流入型及びHe封入型)を装荷。炉心中心制御棒近傍に6体装荷し、下記結果を得ている。

参照データ 1995年 春の年会 C 3 冷却材反応度



参照データ

1995年 春の年会 C 5 制御棒価値

1996年 春の年会 A49 制御棒価値

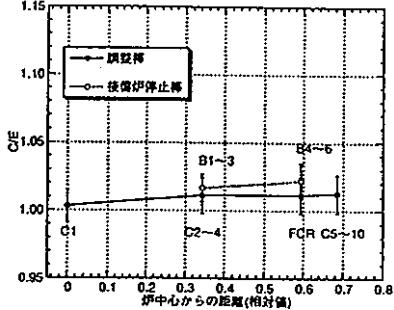
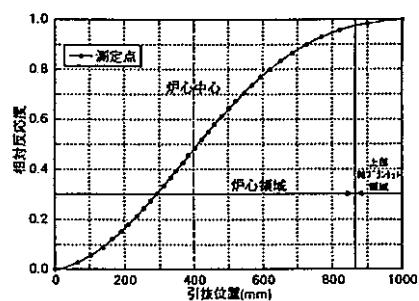
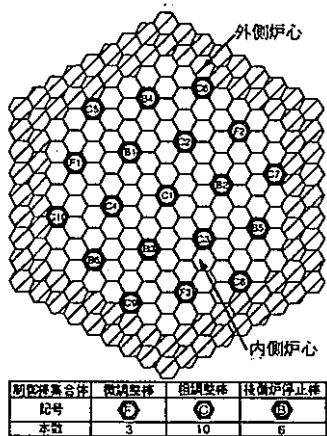


図 2.1-8 もんじゅの制御棒配置 図 2.1-9 中心制御棒の S 字カーブ 図 2.1-10 制御棒価値 C/E 値

(測定値と解析値は良く一致)

(6) 出力分布

中性子検出要素（箔を封入）を装荷した試験用集合体を内側炉心用3体、外側炉心用2体、プランケット用3体、しゃへい体用3体を炉内に装荷し、下記箔を用いた測定が行われている。

中性子検出箇所： ^{239}Pu , ^{235}U , ^{238}U , ^{237}Np (^{239}Pu は炉内約230箇所)

放射化箔： 高速中性子用 Ni, Ti (^{68}Ni (n,p)は炉内約230箇所)

中·低速中性子用……Fe, Na, Au, Sc, Co

参照データ 1995年 春の年会 C 7 出力分布

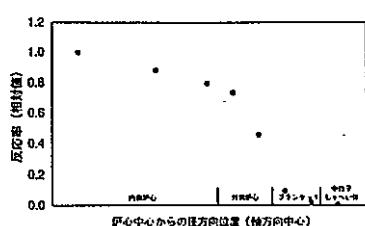
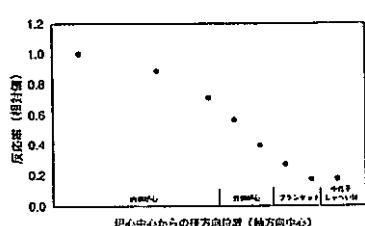
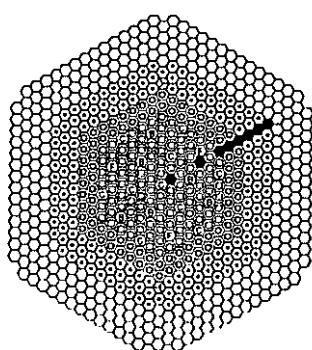


図 2.1-11 試験用集合体炉内蔵荷例 図 2.1-12 ^{113}Pu 核分裂率分布実測値 図 2.1-13 $^{64}\text{Ni}(n,p)$ 反応率分布実測値

(7) 等温温度係数

ポンプ入熱により、約 190°C～300°Cの範囲で等温温度係数を測定

参考データ 1995年秋の大会 A 5 等温温度係数

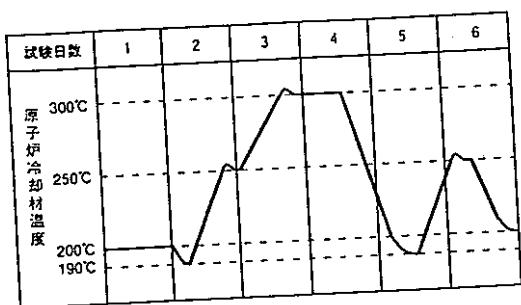


図 2.1-14 試験時の温度変化

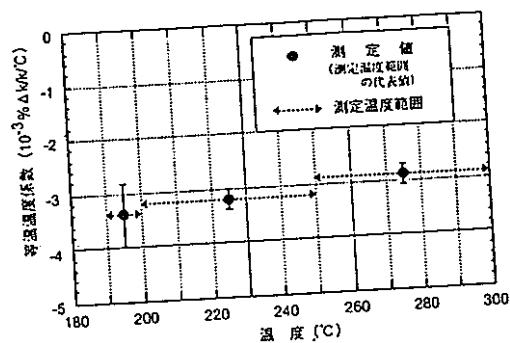


図 2.1-15 等温温度係数測定結果

(8) 出力係数

もんじゅの起動試験において、熱出力 0～45%における熱出力上昇に伴う反応度変化が測定されている。測定は複数回行われたが、測定誤差内ではほぼ一致し、測定値の再現性が良いことが報告されている。解析結果の報告はまだなされていない。

参考データ 1996年秋の大会 A 5 0 热出力上昇に伴う反応度変化の測定

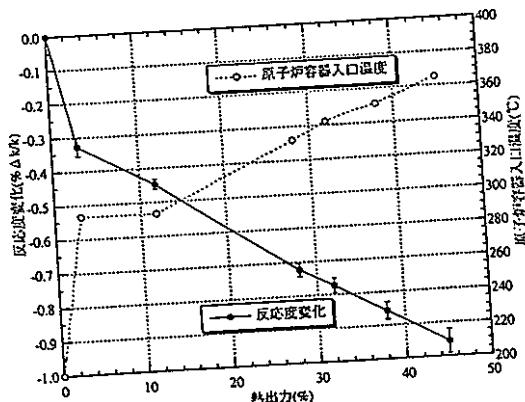


図 2.1-16 热出力上昇に伴う反応度変化

(9) 燃焼反応度

もんじゅの起動試験(40%出力試験等)において、燃焼による反応度変化を測定し、燃焼係数として評価した結果が報告されている。燃焼係数の測定値は、ほぼ、 $-1.8 \sim -2.1 \times 10^{-4}$ $\Delta k/k_0/\text{MWd}$ の範囲にあり、比較的安定した測定値になっている。このことから、本データは炉定数調整上有用なデータとなると思われる。なお、解析結果の報告はまだなされていない。

参考データ 1996年秋の大会 A 5.1 初期炉心における燃焼係数の測定

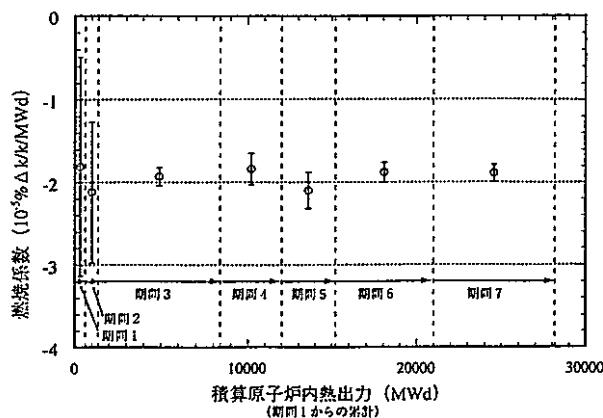


図 2.1-17 燃焼係数測定値

(10) まとめ

以上見てきたように、SSTに於いて、有用な測定結果が数多く出されており、それらの C/E 値も現状では、妥当な（1.0 とそれ程大きな乖離の無い）値であり、大部分は今回の炉定数の調整に採用出来るものと考える。

これらの内、今年度は、JENDL-3.2 を用いてもんじゅ技術課で計算することになっている初臨界炉心（168 体炉心）及び初期炉心（198 体炉心）の臨界性と制御棒価値（初期炉心）を炉定数調整の対象とする。

2.2 臨界性及び制御棒価値の C/E の整理

(1) 臨界性解析

もんじゅの臨界性については、JENDL3.2 を用いた詳細解析が実施され、日本原子力学会「1996 年秋の大会」の『A 5 3 JENDL3.2 によるもんじゅ臨界性解析』において、動燃 鈴木らにより報告されている。

解析対象炉心はもんじゅ初臨界炉心(168 体燃料) (図 2.2-1) 及び初期炉心(198 体炉心) (図 2.2-2) である。

解析においては、制御棒はすべてパーク位置（粗・微調整棒は 1000mm 引抜き、後備炉停止棒は 1100mm 引抜き）とし、測定値としての過剰反応度は挿入制御棒の測定データから算出したものを用いた。

解析手法としては、基準計算に 3 次元 6 角メッシュ体系、エネルギー 18 群を用い、これにメッシュ、輸送、群縮約、燃料非均質性、温度等の補正を施し、解析値を求めており。得られた解析結果を各補正值とともに、表 2.2-1 に示す。初臨界炉心の C/E 値は 0.993、初期炉心の C/E 値は 0.995 であり、計算値は 0.7~0.5% の過小評価になっている。

(2) 制御棒価値の解析

もんじゅ初期炉心の制御棒価値測定の内、1994 年 9 月の核加熱・出力試験開始前に行われた測定の詳細解析が JENDL3.2 を用いて行われ、Physo96 において、澤田らにより報告されている (ページ E-76~E-85)。

制御棒価値測定は、図 2.2-2 で示す炉心の各リングの代表的制御棒に対して行われており、測定法としては、中心制御棒は炉周期法、その他の制御棒は、置換法 (臨界法) が採用されている。

解析は基準計算には、JUPITER 実験解析手法に準じた手法が採用され、その解析値に群縮約補正、メッシュ補正、輸送補正、非均質化断面積補正などが施されている。結果の整理は、制御棒単体価値の形で整理されている。

得られた解析結果を各補正值とともに、表 2.2-2 に示す。補正後の制御棒価値の C/E 値は 0.98~0.99 であり、どの制御棒に対しても測定と解析の一一致はすこぶる良好である。

表 2.2-1 もんじゅ初臨界炉心及び初期炉心の実効増倍率の解析結果

| 体 系 | 初 臨 界 炉 心 | 初 期 炉 心 | |
|---------|---------------|---|--|
| 測 定 日 付 | 1994/4/5 | 1994/5/27 | |
| 項 目 | 測定値或いは解析値 | 測定値或いは解析値 | |
| 測 定 値 | 1.0015 | 1.0301 | |
| 解 析 値 | 基準計算 補 正 値 | 0.9925 −0.0056 0.0064 0.0002 0.0038 −0.0021 −0.0008 0.0002 0.0021 | 1.0229 −0.0057 0.0068 0.0001 0.0038 −0.0021 −0.0008 −0.0004 0.0017 |
| | 補正後 K_{eff} | 0.9946 | 1.0246 |
| | C/E 値 | 0.993 | 0.995 |

* 解析に使用した ^{241}Pu 原子数密度は 1994/4/25 のものであるので、測定日への組成の外挿を行ったもの。

測定値は、初臨界炉心：PNC ZN2410 95-071、初期炉心：PNC ZN2410 96-013 より引用、但し、初期炉心の

測定値は下記学会の OHP から引用。（ZN 2410 96-013 の表示値は 1.0305%）

解析値は原子力学会 1996 年秋の大会 A53(板垣他)の OHP より引用。

表 2.2-2 もんじゅ初期炉心の制御棒価値の解析結果（94/9 測定値の解析）

| | ノミナル値 | | | | | | |
|-------------------|-------|-------|-------|-------|-------|-------|-------|
| | CCR1 | CCR4 | CCR5 | CCR10 | BCR1 | BCR4 | FCR1 |
| 測定値 (E) (%△ k/kk) | 0.974 | 0.840 | 0.588 | 0.575 | 1.187 | 0.938 | 0.658 |
| 基準解析値(%△ k/kk) | 1.002 | 0.877 | 0.613 | 0.601 | 1.292 | 1.023 | 0.682 |
| 群縮約効果補正係数 | 0.983 | 0.982 | 0.972 | 0.967 | 0.968 | 0.963 | 0.972 |
| メッシュ効果補正係数 | 1.034 | 1.034 | 1.030 | 1.031 | 1.040 | 1.037 | 1.030 |
| 輸送効果補正係数 | 0.970 | 0.971 | 0.982 | 0.979 | 0.954 | 0.959 | 0.982 |
| 温度補正係数 | 1.004 | 1.004 | 1.004 | 1.004 | 1.005 | 1.005 | 1.004 |
| 均質化断面積補正係数 | 0.958 | 0.959 | 0.958 | 0.958 | 0.941 | 0.941 | 0.959 |
| 補正係数合計 | 0.948 | 0.949 | 0.946 | 0.938 | 0.909 | 0.905 | 0.947 |
| 補正後解析値 (C) | 0.951 | 0.832 | 0.580 | 0.564 | 1.174 | 0.926 | 0.646 |
| C / E | 0.976 | 0.991 | 0.987 | 0.980 | 0.989 | 0.987 | 0.981 |

測定値は、PNC ZN2410 96-013 より引用。

基準解析値及び補正值は動燃もんじゅ技術課よりの私信。

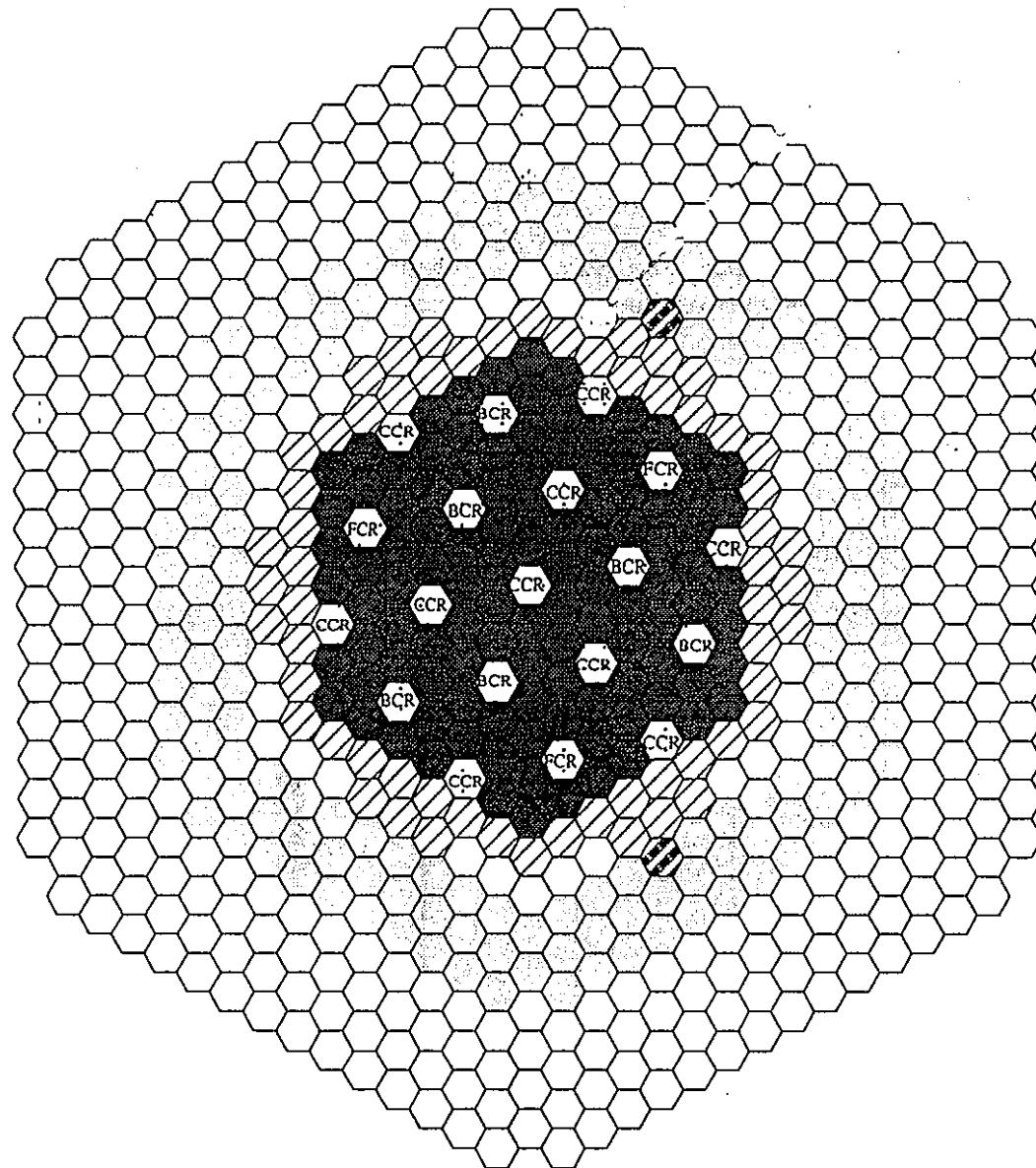


図 2.2-1 もんじゅ初臨界炉心

| 炉心構成要素 | 記号 | 数量 |
|-------------|--------|-----|
| 炉心燃料集合体 | 内側炉心 | 108 |
| | 外側炉心 | 60 |
| プランケット燃料集合体 | ○ | 172 |
| 制御棒集合体 | 微調整棒 | 3 |
| | 粗調整棒 | 10 |
| | 後備炉停止棒 | 6 |
| 中性子源集合体 | △ | 2 |
| 中性子しゃへい体 | ○ | 316 |
| サーベイランス集合体 | | 8 |
| 模擬燃料集合体 | ○ | 30 |

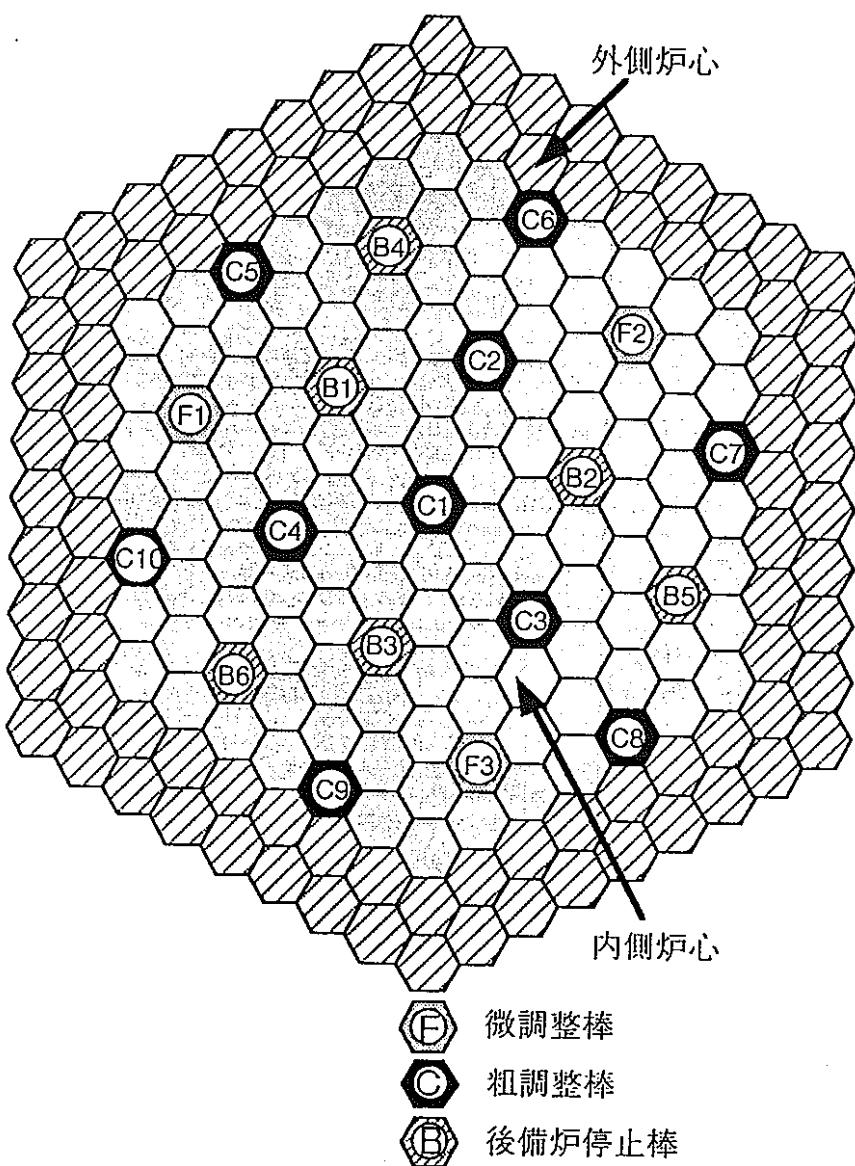


図 2.2-2 もんじゅ初期炉心

3. 「もんじゅ」炉物理試験データ及び解析結果の誤差評価

前項で得られた最確C/E値に対し、その不確かさ評価を行うため、測定誤差の評価及び解析誤差の評価を行う。

3.1 実験誤差の評価

(1) 実効増倍率の測定誤差

実効増倍率の測定誤差に関しては、初臨界炉心に関してはPNC ZN2410 95-071⁽¹⁾で、また初期炉心の過剰反応度の測定誤差に関しては、PNC ZN2410 96-013⁽²⁾で詳細に報告されている。以下に、これらの報告書をもとに実効増倍率の測定誤差を整理し、まとめる。

a. 臨界時の制御棒挿入状態

初臨界炉心及び初期炉心の臨界時の制御棒挿入状態は、以下に示すようになっている。

| 臨界時の制御棒挿入状態 | |
|---------------|----------------|
| 初臨界炉心 | 初期炉心 |
| (炉心燃料 168体) | (炉心燃料 198体) |
| 測定日 | 1994/4/5 |
| C1 : 731mm | C1 : 534mm |
| その他の制御棒：パーク位置 | C2～C4 : 533mm |
| | C5～C10 : 532mm |
| その他の制御棒：パーク位置 | |

解析では、制御棒はパーク位置の状態を模擬して行うので、測定誤差としては、臨界判定誤差、制御棒位置推定誤差、臨界時制御棒位置からパーク位置に制御棒を移動させることを想定し、測定値から組立てられた過剰反応度評価誤差等からなる。これら考えられる誤差要因を以下に示すように列挙し、過剰反応度の測定誤差を評価する。

b. 初臨界炉心の過剰反応度評価誤差

初臨界炉心の過剰反応度評価誤差は、臨界点制御棒位置確認誤差、及び臨界時に部分挿入されている炉中心制御棒をパーク位置に移動させた時の反応度評価誤差からなる。この反応度算出の際の誤差要因は下記のようである。

・統計誤差

制御棒位置 1.06E-03%△ k/k' 1mm相当

| | | |
|--------|------------------|-----------------------|
| 温度測定 | 4.50E-03%Δ k/kk' | T/C 計装系の誤差 (誤差 1.5°C) |
| 炉心平均温度 | 3.00E-03%Δ k/kk' | 3 ループ平均時 (誤差 1 °C) |
| 小 計 | 5.51E-03%Δ k/kk' | |

・系統誤差(I) (下記をステップ毎に考慮)

| | | |
|---------|------------------|----------------------------------|
| 外部中性子源 | 5.76E-05%Δ k/kk' | 6000cps では 0.1/6 φ 未臨界 |
| 臨界判定 | 2.65E-04%Δ k/kk' | CCR 最小駆動 0.25mm |
| 計測系 | 1.04E-04%Δ k/kk' | 実効チャンネル誤差 0.3% |
| 演算処理 | 1.29E-03%Δ k/kk' | 逆時間動特性方程式採用時の平均化誤差等 |
| β | 1.04E-03%Δ k/kk' | β の誤差として 3%を想定。10 φ 投入時 |
| 小 計 | 1.03E-02%Δ k/kk' | (β_{eff} の誤差を含めない) |
| | 1.65E-02%Δ k/kk' | (β_{eff} の誤差を含める) |

・系統誤差(II)

| | | |
|----------|------------------|----------------------------------|
| CRD の熱収縮 | 1.06E-03%Δ k/kk' | 半挿入状態から 2 時間以上で 1mm |
| 干渉効果 | 1.49E-04%Δ k/kk' | C1-バンクの干渉効果 (補正量の 30%) |
| 系統誤差の合計 | 1.15E-02%Δ k/kk' | (β_{eff} の誤差を含めない) |
| | 1.77E-02%Δ k/kk' | (β_{eff} の誤差を含める) |
| 合 計 | 1.28E-02%Δ k/kk' | (β_{eff} の誤差を含めない) |
| | 1.86E-02%Δ k/kk' | (β_{eff} の誤差を含める) |

c. 初期炉心(198 体)(1994/5/27)の過剰反応度評価誤差

初期炉心の過剰反応度評価誤差は、臨界点制御棒位置確認誤差、及び臨界時に部分挿入されている粗調整制御棒をパーク位置に移動させた時の反応度評価誤差からなる。この反応度算出の際の誤差要因は下記のようである。

・統計誤差

| | |
|-------------------|-------------------------------------|
| 制御棒値測定誤差における統計的誤差 | 4.1E-03%Δ k/kk' |
| 臨界点の位置表示誤差 | 1.9E-03%Δ k/kk' (各制御棒毎に ±0.5mm を想定) |
| C1 臨界判定誤差 | 7.0E-04%Δ k/kk' (±0.5mm を想定) |
| R/V 入り口温度誤差 | 7.8E-03%Δ k/kk' (誤差 2.3°C) |
| 小 計 | 9.1E-03%Δ k/kk' |

・系統誤差

| | |
|-----------------|-----------------|
| 制御棒値測定における系統的誤差 | 8.5E-03%Δ k/kk' |
|-----------------|-----------------|

| | | |
|------------------------|--------------------------|---------------------------|
| 制御棒干渉効果補正係数の誤差 | 3.1E-02% $\Delta k/kk'$ | |
| (干渉効果補正分として補正量の30%を想定) | | |
| β_{eff} の誤差 | 9.16E-02% $\Delta k/kk'$ | (β の誤差として3%を想定) |
| 小 計 | 0.0395% $\Delta k/kk'$ | (β_{eff} の誤差を含めない) |
| | 0.1311% $\Delta k/kk'$ | (β_{eff} の誤差を含める) |
| 合 計 | 0.0405% $\Delta k/kk'$ | (β_{eff} の誤差を含めない) |
| | 0.1314% $\Delta k/kk'$ | (β_{eff} の誤差を含める) |

d. 過剰反応度測定誤差のまとめ

前項までに、実際の測定において生じる過剰反応度の誤差について述べた。炉定数調整においては、遅発中性子割合 β のデータは、調整パラメータとして考慮はするが、 k_{eff} のC/Eに対する β の感度の評価が難しいので、 β_{eff} の誤差は測定誤差に含めるものとし、 k_{eff} のC/Eに対する β_{eff} の感度は0.0として扱うものとする。

もんじゅの特性解析において使用する燃料集合体の原子数密度は、製造データから算定されたものであるが、製造データ自体の不確かさは、現在入手していない。原子数密度の不確かさに起因して生じる誤差は、測定誤差として考慮するものとするが、ここでは、以下のような二通りのケースを考えた。すなわち、製造時の原子数密度及び装荷物質の重量の測定が精度良く行われれ、解析に使用した燃料データの不確かさは無視できるものと想定したケースと、燃料製作時のペレット径、密度、Pu富化度等が、ノミナル値の周りに、燃料製作スペックの許容公差内で正規分布していると想定したケース（その時の不確かさは±0.12% $\Delta k/kk'$ （設計書から参照した値））、の両者を考えるものとする。

以上より、 β_{eff} の誤差を含めた測定誤差と上記原子数密度の測定誤差を統計的に加えあわせ、過剰反応度の測定誤差としては、下記を得る。

| CR パーク位置過剰反応度 | 測定誤差 |
|--|--------------|
| 初臨界炉心 | 0.019%~0.12% |
| 初期炉心 | 0.13%~0.18% |
| (最小値は、製造データの不確かさを0と想定したケース、最大値は許容公差内で正規分布すると想定したケース) | |

(2) 制御棒価値の測定誤差（初期炉心）

制御棒価値の測定は、先にも述べたように、炉中心の制御棒に対してはペリオド

法を用い、その他の制御棒に対しては、炉中心の制御棒との置換法により行われている。また、制御棒価値の測定では、測定対象の制御棒と反応度調整用制御棒との干渉効果が入り込むことは避けられない。これら干渉効果は、解析により評価するが、測定値にも、基準制御棒の価値の、測定対象制御棒との干渉を受ける効果の補正や、他のバンク挿入制御棒との干渉状態が基準制御棒の価値を測定した時とは異なることに対する補正誤差等が入り込む。

なお、遅発中性子割合 β のデータは炉定数の調整パラメータとして考慮するので、 β_{eff} の誤差は以下の測定誤差の評価においては考慮から除外した。

以下に、制御棒価値測定の誤差要因毎に誤差評価を行った結果をまとめる。なお、対象とした測定は、核加熱・出力試験開始前(94/9)に行った制御棒価値測定とする。

a. 正のペリオド法の誤差要因

炉中心の制御棒(C1)の反応度価値は、正のペリオド法で求める。その際生じる誤差要因としては、制御棒ラッチ誤差、臨界点調整誤差、制御棒位置表示誤差、倍増時間測定誤差、CRD 駆動軸の熱収縮による誤差等がある。これら各要因毎に下記のように評価した結果が報告されている。

(a) 統計的誤差

- ・制御棒ラッチ誤差 : $0.1 \phi / \text{CR}$
- ・臨界点調整誤差 : $0.1 \phi / \text{step}$
- ・制御棒位置表示誤差 : $0.15 \phi / \text{CR}$
- ・倍増時間測定誤差 : $0.1 \phi / \text{step}$

(b) 系統的誤差

- ・外部中性子源効果 : $-0.1 \phi / \text{CR}$
- ・CRD 駆動軸の熱収縮 : $-0.1 \phi / \text{CR}$

統計的誤差要因と系統的誤差要因の合計は、両者に相関が無いとして統計処理する。

b. 置換法の誤差要因

炉中心以外の制御棒の価値は、炉中心制御棒(C1)との置換により測定されている。その際生じる誤差は、制御棒ラッチ誤差、臨界点調整誤差、測定対象位置表示誤差、反応度基準制御棒(C1)の位置表示誤差、CRD 駆動軸の熱収縮による誤差等からなる。これら各要因毎に誤差を評価し、下記のような誤差幅が提示されて

いる。

(a) 統計的誤差

- ・制御棒ラッチ誤差 : $0.1\phi/\text{CR}$
- ・臨界点調整誤差 : $0.1\phi/\text{step}$
- ・臨界点調整中の臨界点からのはずれ : $0.3\phi/\text{CR}$
- ・測定対象制御棒位置表示誤差 : $0.15\phi/\text{CR}$
- ・反応度基準制御棒位置表示誤差 : 調整棒 $0.5\phi/\text{CR}$ 、後備炉停止棒 $1\phi/\text{CR}$
- ・反応度基準制御棒価値の誤差 : $1.2\%/\text{CR}$ (核加熱・出力試験開始前)

(b) 系統的誤差

- ・CRD 駆動軸の熱収縮 :
 - 測定対象制御棒 : $-0.1\phi/\text{CR}$
 - 反応度基準制御棒 : 調整棒 $-0.5\phi/\text{CR}$ 、後備炉停止棒 $-2.0\phi/\text{CR}$

統計的誤差要因と系統的誤差要因の合計は、両者に相関が無いとして統計処理する。

c. 測定誤差のまとめ

測定値を解析値と比較する上では、干渉効果補正を施す必要がある。その補正により生じる誤差としては、C1については、単体価値の0.5%を、C1以外は測定時の干渉補正係数による補正量に対し、調整棒は50%、後備炉停止棒は25%を考慮する。

以上の誤差幅、及び誤差の処理方法に従って求めた单体制御棒価値の相対誤差を以下にまとめる。

| | 測定法 | 制御棒価値測定誤差 |
|--------|------|-----------|
| C1 | ペリド法 | 1.73% |
| C2～C4 | 置換法 | 1.93% |
| C5～C10 | 置換法 | 1.93% |
| F1～F3 | 置換法 | 1.83% |
| B1～B3 | 置換法 | 2.97% |
| B4～B6 | 置換法 | 2.57% |

注：上記誤差には β_{eff} の誤差を含めていない。

3.2 解析誤差の評価

(1) 臨界性評価における解析誤差の評価

実機の臨界性評価において、燃料ピンの非均質効果は無視出来ない効果を及ぼす。しかし、その評価は難しく、その効果の評価において誤差が入り込む余地が大きい。そこで、この非均質効果の誤差評価を行った。

評価の方法としては、燃料ピン非均質効果の解析モデルを変えて非均質効果がどの程度変動するかを調べ、不確かさ幅評価のデータとする。計算における使用ライブラリーは、JENDL-3.2とする。

非均質効果の評価は、実効断面積に関する効果とストリーミング効果に関する部分に分け、以下に示すモデルで検討を行う。なお、セル計算におけるバッククリングは臨界バッククリングとする。

a. 実効断面積に対する非均質効果の評価

2ステップモデルにより行う。ステップ1はピンセルモデルで、ステップ2は集合体セルモデルである。（図3.2-1参照）

(a) ステップ1セル計算

ステップ1のピンセルモデルの作り方を下記の2通りで計算する。

(i) ピンセルにラッパー管を入れないモデル

図3.2-1のモデル1。

(ii) ピンセルにラッパー管を考慮するモデル

図3.2-1のモデル2。

ピンセルにラッパー管を燃料集合体内の燃料ピン本数で割り振った分を考慮する。但し、ステップ2に渡す実効断面積の評価領域には、ラッパー管分は含めない。

(b) ステップ2セル計算

集合体平均の実効断面積の計算を図3.2-1の下側のモデルにより行う。但し、ステップ2の内側領域の実効断面積はステップ1で得られたものを使う。

(c) 炉心計算

上記計算を内側炉心、外側炉心、軸プランケット、径プランケットのすべてについて行い、得られた実効断面積を用いて炉心計算を行う。

併せて、完全な均質モデルでやはり炉心計算を行う。上記との差異がストリー

ミング効果を除いた非均質効果である。ここで拡散係数Dとしては、中性子束重みのDを用いる。

炉心計算は、もんじゅ初期炉心（198体炉心）を対象に、制御棒パターンとしては、初期炉心の代表的な制御棒挿入深度である、粗及び微調整制御棒は54.3cm挿入、後備制御棒はパーク位置、とした。

得られた結果を表3.2-1に示す。モデル1による非均質効果は0.69%であり、モデル2による非均質効果は0.45%という結果を得た。

b. ストリーミング効果の評価

ストリーミング効果の評価は燃料周辺のストリーミング効果とラッパー管周辺のストリーミング効果に分けて以下の手順で評価する。

(a) 燃料ピン周辺のストリーミング効果

(i) 均質モデル

集合体内の体積平均で完全に均質化した組成。但し、拡散係数Dとしては、中性子束重みのDを用いる。

(ii) ストリーミング効果評価モデル

前述のステップ1のモデル2で、Benoistの方法で計算した非等方のDを求める。その他の断面積は、上記(i)の均質モデルのものを使って炉心計算をする。(i)の炉心計算の k_{eff} との差が燃料ピン周りのストリーミング効果である。

(b) ラッパー管周りのNa領域のストリーミング効果

(i) 均質モデル

上記(a)(i)の均質モデルは、ここでも共通。

(ii) ストリーミングモデル

前述の非均質効果評価計算のステップ2モデルを対象に考える。ラッパー管内側の燃料ピン領域の原子数密度を体積平均で求め、その体積平均原子数密度を用いて、集合体セルの非均質計算を行う。そして、Benoistの方法で非等方のDを求める。その他の断面積は、上記(i)の均質モデルのものを使って炉心計算をする。(i)均質モデルの炉心計算の k_{eff} との差がラッパー管周りのストリーミング効果である。

炉心計算は、前記非均質効果の計算と同様に、もんじゅ初期炉心を対象

に行った。得られた結果を表 3.2-2 に示す。燃料ピン周りのストリーミング効果は -0.105%、ラッパー管周りのストリーミング効果は -0.087%、ストリーミング効果の合計は -0.192% という結果を得た。

- c. 断面積に対する非均質効果とストリーミング効果を合算した全非均質効果
断面積に対する非均質効果とストリーミング効果を合算すると、モデル 1 による結果は 0.50%、モデル 2 による結果は 0.26% となる。一方、動燃の評価値は 0.38% であり、モデル 1 と 2 の丁度中間の値になっている。

本検討結果より、もんじゅの実効増倍率に対する非均質効果効果を

0.38% ± 0.12%

と設定する。

- d. 実効増倍率に対する解析誤差のまとめ

上記非均質効果評価誤差の他に、基準計算結果に対する各種補正項に対する誤差を評価し、表 3.2-3 にまとめた。誤差要因としては、自己遮蔽因子のフィッティング誤差、 Σtr の評価誤差、輸送効果補正誤差等を考慮した。これら誤差の設定根拠は同表の注釈欄に記した。同表には、前項で記した測定誤差も併せて示した。臨界性に対する解析誤差は、初臨界炉心及び初期炉心とともに、0.25% である。

(2) 制御棒価値評価における解析誤差の評価

もんじゅ初期炉心出力試験開始前に行った制御棒価値の基準解析値及び各種補正值に対する誤差を評価し、表 3.2-4 にまとめた。解析誤差の設定根拠は同表の注釈欄に記した。同表には、前項で記した測定誤差も併せて示した。制御棒価値に対する解析誤差は、2 ~ 4 % の大きさである。

表 3.2-1 もんじゅ燃料ピン非均質効果（実効断面積に対する非均質効果）

| 計算モデル | Σ_{tr} 重み | k_{eff} | 相対誤差 (% $\Delta k/kk'$) | 備 考 |
|--------|------------------|-----------|-----------------------------|--|
| 均質（基準） | 中性子束 | 0.995109 | — | $D = 1/3 \Sigma_{tr}$ |
| 非均質(1) | 中性子束 | 1.001948 | 0.686 | ステップ1(モデル1)+ステップ2, $D = 1/3 \Sigma_{tr}$ |
| 非均質(2) | 中性子束 | 0.999625 | 0.454 | ステップ1(モデル2)+ステップ2, $D = 1/3 \Sigma_{tr}$ |

表 3.2-2 もんじゅ燃料ピン及び集合体におけるストリーミング効果の評価

| 計算モデル | Σ_{tr} 重み | K_{eff} | 相対誤差 (% $\Delta k/kk'$) | 備 考 |
|-----------------|------------------|-----------|-----------------------------|-----------------------------------|
| 均 質 | 中性子束 | 0.995109 | — | $D = 1/3 \Sigma_{tr}$ |
| 燃料ピン周 非 均 質 | 中性子束 | 0.994069 | -0.105 | ステップ1 モデル2 の非等方拡散 D, その他は均質炉定数 |
| ラッパー管周 非 均 質 | 中性子束 | 0.994250 | -0.087 | ステップ2 の非等方拡散 D, その他は均質炉定数 |

使用ライブラリー : J E N D L - 3.2

制御棒パターン : 粗及び微調整制御棒は 54.3cm 挿入、後備制御棒はバーク位置

炉心計算形状 : 2 次元 R Z 体系

計算群数 : 70 群

表 3.2-3 もんじゅ初臨界炉心及び初期炉心の実効増倍率の測定値、解析値、及びそれらの誤差

| 体 系 | | 初 臨 界 炉 心 | | 初 期 炉 心 | |
|----------------------|-----------------------|-----------|-------------------|-----------|-------------------|
| 測 定 日 付 | | 1994/4/5 | | 1994/5/27 | |
| 項 目 | | 測定値或いは解析値 | 誤 差 (1σ) | 測定値或いは解析値 | 誤 差 (1σ) |
| 測 定 値 | | 1.0015 | 0.019%~0.12%(注 1) | 1.0301 | 0.18%~0.18%(注 1) |
| 解 析 值 | 基準計算 | 0.9925 | 0.18%(注 2) | 1.0229 | 0.18%(注 2) |
| | メッシュ | -0.0056 | -(注 3) | -0.0057 | -(注 3) |
| | 輸 送 | 0.0064 | 0.04%(注 4) | 0.0068 | 0.06%(注 4) |
| | 群縮補正 | 0.0002 | 0.01%(注 5) | 0.0001 | 0.01%(注 5) |
| | 燃料非均質 | 0.0038 | 0.12%(注 6) | 0.0038 | 0.12%(注 6) |
| | 温度補正 | -0.0021 | 0.11%(注 7) | -0.0021 | 0.11%(注 7) |
| | SUS実組成 | -0.0008 | 0.04%(注 8) | -0.0008 | 0.04%(注 8) |
| | ^{241}Pu 崩壊* | 0.0002 | 0.01%(注 9) | -0.0004 | 0.01%(注 9) |
| | 合 計 | 0.0021 | - | 0.0017 | - |
| 補正後 K_{eff} | | 0.9946 | 0.25%(注 10) | 1.0246 | 0.25%(注 10) |
| C/E 値 | | 0.993 | 0.25%~0.28%(注 11) | 0.995 | 0.28%~0.31%(注 11) |

* 解析に使用した ^{241}Pu 原子数密度は 1994/4/25 のものであるので、測定日への組成の外挿を行ったもの。

測定値及び測定誤差は、初臨界炉心：PNC ZN2410 95-071、初期炉心：PNC ZN2410 96-013 より引用。但し、初期炉心の測定値は下記学会の OHP から引用。(ZN 2410 96-013 の表示値は 1.0305%)

解析値は原子力学会 1996 年秋の大会 A53(板垣他)の OHP より引用、解析誤差は今回評価。

- 注 1 最小値は、製造データの不確かさを 0 と想定したケース、最大値は許容公差内で正規分布すると想定したケース。 β_{eff} の誤差を含む。
- 注 2 実効断面積を計算する上で生じる誤差として、自己遮蔽因子のフィッティング誤差、及び Σtr の評価誤差を考慮する。自己遮蔽因子の誤差としては、0.05%を想定。 Σtr の評価誤差としては、中性子束重みを用いた場合とカレント重みを用いた場合の実効増倍率の差異 0.34% の 50%、すなわち 0.17%を想定し、この 2つを統計的に加え合わせ、0.18%を基準計算の誤差とする。なお、 Σtr の基準評価法はカレント重みとする。
- 注 3 この補正による誤差は輸送効果の項で併せて考慮する。
- 注 4 輸送効果補正誤差としては、メッシュ補正効果と併せた補正量の 50%とする。
- 注 5 補正量の 50%を誤差と想定する。
- 注 6 2つの非均質効果評価モデルの差異より評価。別添資料参照。
- 注 7 補正量の 50%を誤差と想定する。
- 注 8 補正量の 50%を誤差と想定する。
- 注 9 ^{241}Pu の崩壊定数の誤差を ENSDF の評価に基づき 0.7%とする。製造時からの補正量として、1% Δk と暫定し、 ^{241}Pu の崩壊による補正誤差は 0.007% Δk となる。
- 注 1 0 解析値に関する各誤差を統計的に加え合った値。（2乗和の平方根）
- 注 1 1 解析値の誤差と測定値の誤差を統計的に加え合った値。

表 3.2-4 もんじゅ初期炉心の制御棒価値の測定値、解析値、解析補正值とそれらの誤差 (94/9 測定)

| | ノミナル値 | | | | | | | 相対誤差 (1σ) (単位 %) | | | | | | | |
|----------------------------|-------|-------|-------|-------|-------|-------|-------|---------------------------|------|------|-------|------|------|------|-----|
| | CCR1 | CCR4 | CCR5 | CCR10 | BCR1 | BCR4 | FCR1 | CCR1 | CCR4 | CCR5 | CCR10 | BCR1 | BCR4 | FCR1 | 備考 |
| 測定値 (E) (% $\Delta k/kk$) | 0.974 | 0.840 | 0.588 | 0.575 | 1.187 | 0.938 | 0.658 | 1.73 | 1.93 | 1.93 | 1.93 | 2.97 | 2.57 | 1.83 | 注 1 |
| 基準解析値(% $\Delta k/kk$) | 1.002 | 0.877 | 0.613 | 0.601 | 1.292 | 1.023 | 0.682 | — | — | — | — | — | — | — | 注 2 |
| 群縮約効果補正係数 | 0.983 | 0.982 | 0.972 | 0.967 | 0.968 | 0.963 | 0.972 | 0.7 | 0.9 | 1.4 | 1.7 | 1.6 | 1.9 | 1.4 | 注 3 |
| メッシュ効果補正係数 | 1.034 | 1.034 | 1.030 | 1.031 | 1.040 | 1.037 | 1.030 | — | — | — | — | — | — | — | 注 4 |
| 輸送効果補正係数 | 0.970 | 0.971 | 0.982 | 0.979 | 0.954 | 0.959 | 0.982 | 0.1 | 0.2 | 0.6 | 0.5 | 0.4 | 0.3 | 0.6 | 注 5 |
| 温度補正係数 | 1.004 | 1.004 | 1.004 | 1.004 | 1.005 | 1.005 | 1.004 | 0.2 | 0.2 | 0.2 | 0.2 | 0.3 | 0.3 | 0.2 | 注 6 |
| 均質化断面積補正係数 | 0.958 | 0.959 | 0.958 | 0.958 | 0.941 | 0.941 | 0.959 | 2.1 | 2.1 | 2.1 | 2.1 | 3.0 | 3.0 | 2.1 | 注 7 |
| 補正係数合計 | 0.948 | 0.949 | 0.946 | 0.938 | 0.909 | 0.905 | 0.947 | — | — | — | — | — | — | — | |
| 補正後解析値 (C) | 0.951 | 0.832 | 0.580 | 0.564 | 1.174 | 0.926 | 0.646 | 2.2 | 2.3 | 2.6 | 2.8 | 3.4 | 3.6 | 2.6 | 注 8 |
| C/E | 0.976 | 0.991 | 0.987 | 0.980 | 0.989 | 0.987 | 0.981 | 2.8 | 3.0 | 3.2 | 3.4 | 4.5 | 4.4 | 3.2 | 注 9 |

測定値及び測定誤差は、PNC ZN2410 96-013 より引用。基準解析値及び補正值は動燃もんじゅ技術課よりの私信。解析誤差は今回評価。

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注 1 測定値の誤差には、 β_{eff} の誤差を含めない。

注 2 実効断面積を計算する上での誤差等は均質化断面積補正係数の項で考慮する。

注 3 群縮約補正の誤差は補正量の 50% とする。

注 4 この補正による誤差は輸送効果の項で併せて考慮する。

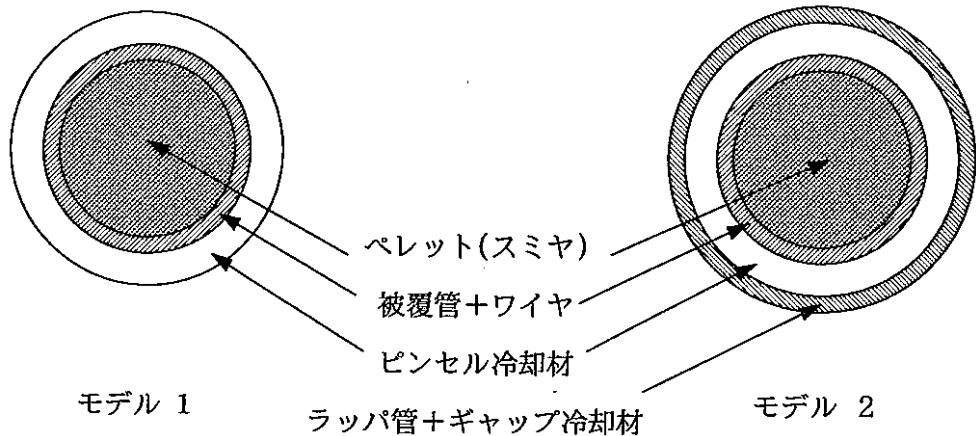
注 5 輸送効果補正誤差としては、メッシュ補正効果と併せた補正量の 50% とする。

注 6 温度補正係数の誤差は補正量の 50% とする。

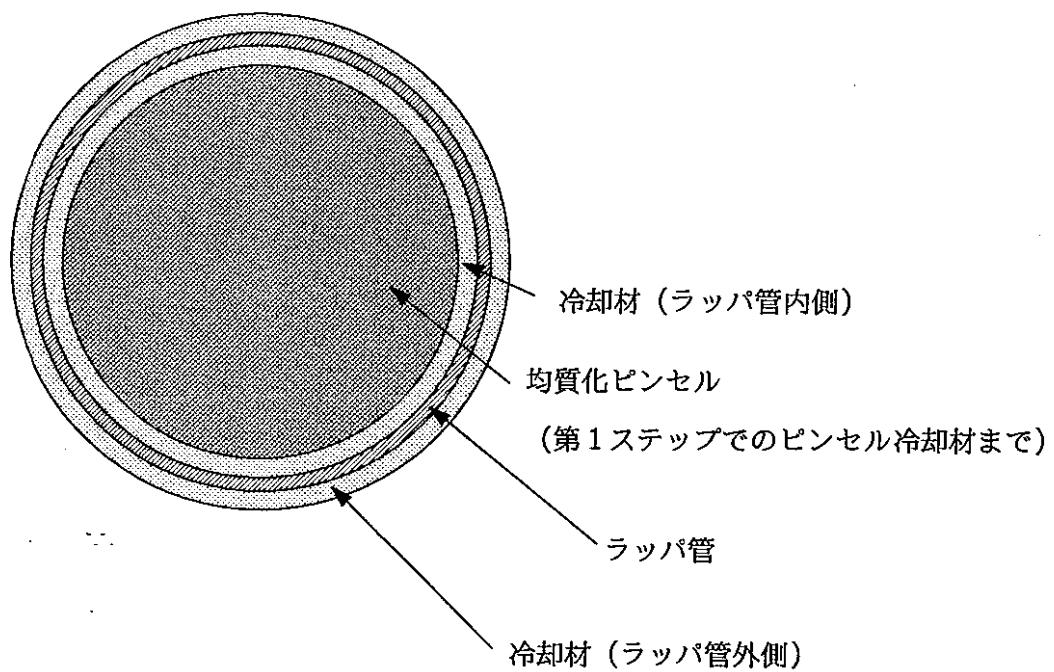
注 7 均質化断面積補正により生じる誤差には、実効断面積を計算する上で生じる誤差をすべて含めて考える。制御棒ピン非均質効果や、炉定数作成に関連して生じる誤差等も含めるものとする。これらの誤差として、均質化断面積補正量の 50% とする。

注 8 補正後解析値の誤差は各誤差を統計的に加え合わせた値。（2乗和の平方根）

注 9 C/E 値の不確かさは解析値の誤差と測定値の誤差を統計的に加え合わせた値。



(1) ステップ1 (燃料ピンセル非均質)



(2) 第2ステップ (ラッパ管非均質)

図 3.2-1 炉心燃料集合体均質化モデル（2ステップ非均質モデル）

3.3 相関係数の評価

上記の実験誤差及び解析誤差に対して、異なる炉心間、異なる核特性値間の共分散を以下のように評価した。

(1) 実効増倍率の測定値、解析値の共分散：

実効増倍率の測定誤差(V_e)：

実効増倍率の測定誤差は、それを構成する原子数密度に強く依存する。従って、初臨界炉心と初期炉心との測定誤差の相関係数は、原子数密度の誤差の設定に依存する。原子数密度の誤差として、製造データの不確かさは無視できるものと想定したケースでは、両体系の測定誤差の共通成分は β に起因する誤差のみとなる。 β に起因する誤差は、過剰反応度に比例するが、初臨界炉心の過剰反応度は $0.15\% \Delta k/kk'$ と小さいことから、両体系の誤差の相関は小さいと考えられ、相関係数は～0と設定する。

一方、製造データの不確かさとして、ノミナル値の周りに、燃料製作スペックの許容公差内で正規分布していると想定したケースでは、両体系の共通誤差は、3.1(1)で示したように、 $0.12\% \Delta k/kk'$ あり、それによる相関係数は0.7となる。

解析誤差(V_m)：

解析誤差の誤差要因のうち主要なものは、輸送補正、燃料ピン非均質効果、実効断面積評価上の誤差等であるが、これらの補正による誤差は初臨界炉心と初期炉心とで共通に生じるものであるので、両体系間の誤差の相関は非常に強く、初臨界炉心と初期炉心との相関係数は0.8とする。

測定誤差及び解析誤差の相関係数マトリックスを、後述する制御棒価値に対する結果とともに、表3.2-5及び表3.2-6にまとめる。

(2) 制御棒価値の測定値、解析値の共分散

C1 を除く各種制御棒価値の測定は、すべて C1 との置換法で求められている。これら各種制御棒の誤差は、3.1(2)で示したように、その大部分は C1 の誤差から構成されている。また、干渉効果の補正にともない生じる誤差も、干渉効果の評価手法が同一であり、制御棒パターンもほぼ類似であることから、相互の誤差には強い相関があると見なされる。以上より、制御棒相互の測定誤差の相関は0.8とする。

また、94年4月及び5月測定の臨界性と94年9月の制御棒価値との誤差の相関は、

0.0とする。これは、臨界性の過剰反応度の測定において使用した基準制御棒の価値測定と9月の制御棒価値測定における基準制御棒の価値測定とは、測定条件が異なっており、両者に相関が見られないと判断したことによる。

解析誤差の主要因は均質化断面積補正、輸送効果、群縮約補正である。これらの誤差の内、前2者は単一制御棒内の微視的な現象であり、炉内の位置に依存しないものである。このことから、異なった制御棒間の解析誤差の相関は非常に強いと考えられ、異なった制御棒間の相関係数はすべて一様に0.8とした。

実効増倍率及び制御棒価値に関する測定値及び解析値の共分散マトリックスを表3.2-5及び表3.2-6にまとめて示した。数値の入っていないところは0.0が入っているものとする。また、 V_e 及び V_m はいずれも対称マトリックスである。

表 3.2-5 実効増倍率及び制御棒価値の測定誤差と相関係数のまとめ

Ve

| | k(168) | k(198) | CCR1 | CCR4 | CCR5 | CR10 | BCR1 | BCR4 | FCR1 |
|--------|----------------|---------------|------|------|------|------|------|------|------|
| 誤差 (%) | 0.019 ～0.12 | 0.13～ 0.18 | 1.73 | 1.93 | 1.93 | 1.93 | 2.97 | 2.57 | 1.83 |
| k(168) | 1.00 | 0～0.7 | | | | | | | |
| k(198) | 0～0.7 | 1.00 | | | | | | | |
| CCR1 | | | 1.00 | 0.8 | 0.8 | 0.8 | 0.8 | 0.8 | 0.8 |
| CCR4 | | | 0.8 | 1.00 | 0.8 | 0.8 | 0.8 | 0.8 | 0.8 |
| CCR5 | | | 0.8 | 0.8 | 1.00 | 0.8 | 0.8 | 0.8 | 0.8 |
| CR10 | | | 0.8 | 0.8 | 0.8 | 1.00 | 0.8 | 0.8 | 0.8 |
| BCR1 | | | 0.8 | 0.8 | 0.8 | 0.8 | 1.00 | 0.8 | 0.8 |
| BCR4 | | | 0.8 | 0.8 | 0.8 | 0.8 | 0.8 | 1.00 | 0.8 |
| FCR1 | | | 0.8 | 0.8 | 0.8 | 0.8 | 0.8 | 0.8 | 1.00 |

(数字の入っていない所は 0.0)

表 3.2-6 実効増倍率及び制御棒価値の解析誤差と相関係数のまとめ

Vm

| | k(168) | k(198) | CCR1 | CCR4 | CCR5 | CR10 | BCR1 | BCR4 | FCR1 |
|--------|--------|--------|------|------|------|------|------|------|------|
| 誤差 (%) | 0.25 | 0.25 | 2.2 | 2.3 | 2.6 | 2.8 | 3.4 | 3.6 | 2.6 |
| k(168) | 1.00 | 0.8 | | | | | | | |
| k(198) | 0.8 | 1.00 | | | | | | | |
| CCR1 | | | 1.00 | 0.8 | 0.8 | 0.8 | 0.8 | 0.8 | 0.8 |
| CCR4 | | | 0.8 | 1.00 | 0.8 | 0.8 | 0.8 | 0.8 | 0.8 |
| CCR5 | | | 0.8 | 0.8 | 1.00 | 0.8 | 0.8 | 0.8 | 0.8 |
| CR10 | | | 0.8 | 0.8 | 0.8 | 1.00 | 0.8 | 0.8 | 0.8 |
| BCR1 | | | 0.8 | 0.8 | 0.8 | 0.8 | 1.00 | 0.8 | 0.8 |
| BCR4 | | | 0.8 | 0.8 | 0.8 | 0.8 | 0.8 | 1.00 | 0.8 |
| FCR1 | | | 0.8 | 0.8 | 0.8 | 0.8 | 0.8 | 0.8 | 1.00 |

(数字の入っていない所は 0.0)

4. 「もんじゅ」炉物理試験データの感度係数計算

4.1 実効増倍率に関する感度解析

(1) 目的

炉定数調整の為、もんじゅの 168 体臨界体系及び 198 体初期炉心での、臨界性に対する感度係数を算出する。

(2) 解析対象

初臨界炉心（168 体燃料装荷炉心）

燃料装荷状態 図 4.1-1 に示す。¹⁾

制御棒挿入状態 中心制御棒 吸収体下端が炉心上端より 13.4cm 挿入
その他 パーク位置

初期炉心（198 体燃料装荷）

燃料装荷状態 図 4.1-2 に示す。²⁾

制御棒挿入状態 調整棒 吸収体下端が炉心上端より 32.2cm 挿入
(出力試験直前状態)

後備炉停止棒 パーク位置

(3) 解析方法

・感度解析評価 SAGEP コードを用いる。

中性子束、共役中性子束は CITATION-FBR コードを用いて算出する。

・エネルギー群数 18 群

(群分割 70 群のエネルギーに分割に対し

2, 4, 6, 8, 10, 13, 16, 19, 22, 25, 28, 31, 34, 37, 40, 43, 46, 70)

・使用ライブラリ JENDL3.2

・実効断面積計算 均質モデルで求める。

なお非均質性が強い制御棒については以下の評価を行う。

a. 均質化因子の設定

制御棒の非均質効果を模擬するため SLAROM コードにより均質計算と非均質計算を行い反応度保存となるように、¹⁰B、¹¹B、C に対する均質化因子（希釈因子）を設定する。実効断面積評価には本均質化因子を用いて ¹⁰B、¹¹B、C を希釈して求める。

b. リング化に対する希釈因子の設定

SAGEP コードは 2 次元評価であるため中心以外の制御棒については 2 次元 R-Z 計算と 3 次元計算で制御棒価値が等しくなるように ^{10}B 、 ^{11}B 、C に対して乗じる因子（リング化希釈因子）を設定する。

(4) 解析条件

a. 制御棒の均質化因子評価条件

粗調整棒に対して図 4.1-3 に示す様に炉心燃料 6 体分を巻いたスーパセル計算により均質化計算と非均質計算の比較を行う。

b. リング化に対する因子

198 体の体系を対象に微調整棒で第 1 リングは 3 本の粗調整棒の挿入、第 2 リングは微調整棒 3 本、粗調整棒 6 本の挿入状態に対し希釈因子を設定する。

なお挿入深度は 288mm（初期炉心の制御棒価値実験の代表的な制御棒挿入深度）で評価する。

なお、168 体系は外側燃料 30 本を模擬集合体に置き換えた体系である。

c. 168 本体系の感度解析条件

R-Z の体系を表 4.1-1 に示す。

燃料の組成は H 6 年 4 月 25 日の組成とする。ⁱⁱ⁾

また、制御棒は全て $\pm\frac{1}{2}$ 位置とする。これは制御棒の C/E の評価が全引き抜き状態で評価していることにあわせるためである。

d. 198 本体系の感度解析条件

168 本体系で模擬燃料が外側炉心燃料になる以外の体系条件は 168 本体系と同じである。なお制御棒は挿入深度が 32.2cm となるが c 項と同じく制御棒は全て $\pm\frac{1}{2}$ 位置とする。

燃料組成は H 6 年 9 月 16 日の組成とする。ⁱⁱ⁾

(5) 解析結果

a. 制御棒の均質化因子

図 4.1-4 に示す様に ^{10}B 、 ^{11}B 、C に対する因子を 0.866 に設定する。

b. リング化因子

図 4.1-5、図 4.1-6 に示す結果から ^{10}B 、 ^{11}B 、C に対する因子を下記の様に設定する。

第1リング 0.50

第2リング 0.75

これをパーセント位置の係数として用いる。

c. 評価結果

(a) 2次元拡散計算の結果 (CITATION)

168 本体系 固有値 0.9915

198 本体系 固有値 1.0179

(b) 感度解析結果

得られた実効増倍率に対する感度係数を Appendix A にまとめる。（表 A-1 に 168 本体系での感度解析の評価結果を、また、表 A-2 に 198 本体系での感度係数の評価結果を示す。）実効増倍率に対する感度の大きい核種は ^{139}Pu の ν 、 σ_f 、 ^{238}U の σ_c 、 ^{241}Pu の ν 、 σ_f 等である。JENDL2 での評価結果³⁾と比較した結果を表 4.1-2、表 4.1-3 及び図 4.1-7、図 4.1-8 に示す。この比較結果から分かるように両者の差は小さく、「もんじゅ」の臨界体系及び初期炉心においての固有値に対する感度は JENDL3.2 と JENDL2 でほぼ等しいことが示された。

なお、198 本体系の中心制御棒引き抜き状態で直接 ^{139}Pu の σ_f と ^{238}U の σ_c を 10% 増加させた場合の計算結果を参考に示す。良い一致を示している。

| 基準 | $^{139}\text{Pu} \sigma_f$ | | $^{238}\text{U} \sigma_c$ |
|------------|----------------------------|-------|---------------------------|
| | | 10%増加 | 10%増加 |
| 実効増倍率 | 0.990 | 1.038 | 0.973 |
| Δk | | 0.048 | -0.017 |
| 感度係数よりの評価 | | 0.049 | -0.019 |

表 4.1-1 2 次元 R-Z モデル

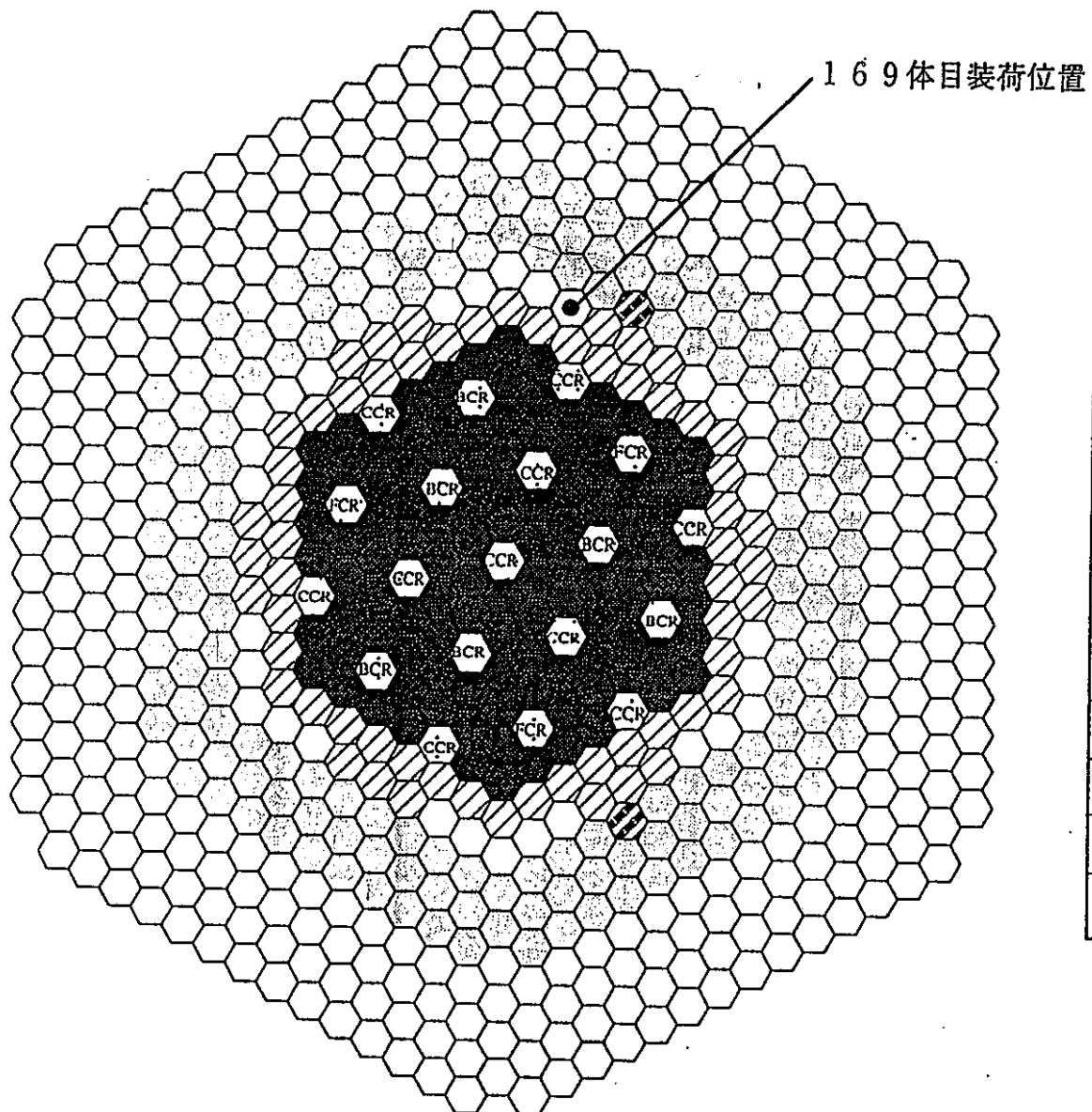
| region | ring幅 (cm) | 半径 (cm) | 面積 (cm ²) | 等価集合体本数 | 種類 | 積算燃料体数 | 備考 |
|--------|---------------|------------|--------------------------|---------|---------|--------|-------------------------|
| 1 | 6.06943 | 6.06943 | 115.7299 | 1.0 | CR | | |
| 2 | 9.98878 | 16.05821 | 694.3803 | 6.0 | INNER-F | 6.0 | |
| 3 | 10.39784 | 26.45605 | 1388.761 | 12.0 | INNER-F | 18.0 | |
| 4 | 2.32216 | 28.77821 | 402.9494 | 3.5 | INNER-F | 21.5 | |
| 5 | 3.61336 | 32.39157 | 694.3813 | 6.0 | CR | | |
| 6 | 4.52736 | 36.91893 | 985.8116 | 8.5 | INNER-F | 30.0 | |
| 7 | 10.48487 | 47.4038 | 2777.522 | 24.0 | INNER-F | 54.0 | |
| 8 | 7.73198 | 55.13578 | 2490.761 | 21.5 | INNER-F | 75.5 | |
| 9 | 3.87278 | 59.00856 | 1388.76 | 12.0 | CR | | |
| 10 | 9.39049 | 68.39905 | 3758.664 | 32.5 | INNER-F | 108.0 | |
| 11 | 10.5036 | 78.90265 | 4860.666 | 42.0 | OUTER-F | 150.0 | 外側炉心 60本 |
| 12 | 4.09588 | 82.99853 | 2083.277 | 18.0 | OUTER-F | 168.0 | |
| 13 | 6.41012 | 89.40865 | 3471.933 | 30.0 | DUMMY | | 198体では外側燃料 (中性子源を含む) |
| 14 | 10.50715 | 99.9158 | 6249.446 | 54.0 | R-BL | 54.0 | |
| 15 | 10.50818 | 110.424 | 6943.825 | 60.0 | R-BL | 114.0 | |
| 16 | 9.59162 | 120.0156 | 6943.827 | 60.0 | R-BL | 174.0 | |
| 17 | 30 | 150.0156 | 25449.84 | 219.9 | SHIELD | | |

表 4.1-2 感度係数の比較 (JENDL2 と JENDL3.2 の比較 168 本体系)

| 核種 | reaction | total | | (1E-4 $\Delta k/kk' / \Delta \sigma / \sigma$) | |
|--------|----------|----------|--------|---|--------|
| | | JENDL3.2 | JENDL2 | JENDL3.2 | JENDL2 |
| U-235 | CAPTURE | -8 | -1 | -214 | -200 |
| U-235 | NU | 86 | 83 | 349 | 328 |
| U-235 | FISSION | 60 | 53 | -167 | -163 |
| U-235 | ELASTIC | 0 | 0 | -100 | -103 |
| U-235 | INELASTC | 0 | 0 | (N, 2N) 0 | 0 |
| U-235 | MU-AVE | 0 | 0 | CR CAPTURE -60 | -56 |
| U-235 | (N, 2N) | 0 | 0 | CR ELASTIC 130 | 120 |
| U-238 | CAPTURE | -1853 | -1833 | CR INELASTC -37 | -33 |
| U-238 | NU | 993 | 999 | CR MU-AVE -28 | -27 |
| U-238 | FISSION | 621 | 626 | CR (N, 2N) 0 | 0 |
| U-238 | ELASTIC | 244 | 238 | NI CAPTURE -117 | -116 |
| U-238 | INELASTC | -285 | -325 | NI ELASTIC 127 | 111 |
| U-238 | MU-AVE | -120 | -117 | NI INELASTC -23 | -24 |
| U-238 | (N, 2N) | 1 | 1 | NI MU-AVE -22 | -103 |
| PU-239 | CAPTURE | -570 | -574 | NI (N, 2N) 0 | 0 |
| PU-239 | NU | 6990 | 7004 | NA CAPTURE -23 | -19 |
| PU-239 | FISSION | 4981 | 5004 | NA ELASTIC 211 | 278 |
| PU-239 | ELASTIC | 20 | 18 | NA INELASTC -77 | -95 |
| PU-239 | INELASTC | -22 | -16 | NA MU-AVE -67 | -65 |
| PU-239 | MU-AVE | -13 | -8 | NA (N, 2N) 0 | 0 |
| PU-239 | (N, 2N) | 0 | 0 | O CAPTURE -17 | -19 |
| PU-240 | CAPTURE | -246 | -226 | O ELASTIC 11 | 47 |
| PU-240 | NU | 584 | 571 | O INELASTC -1 | -1 |
| PU-240 | FISSION | 403 | 391 | O MU-AVE -41 | -22 |
| PU-240 | ELASTIC | 9 | 3 | O (N, 2N) 0 | 0 |
| PU-240 | INELASTC | -10 | -8 | C CAPTURE 0 | 0 |
| PU-240 | MU-AVE | -4 | -1 | C ELASTIC 0 | 0 |
| PU-240 | (N, 2N) | 0 | 0 | C INELASTC 0 | 0 |
| PU-240 | MU-AVE | 0 | 0 | C MU-AVE 0 | 0 |
| PU-240 | (N, 2N) | 0 | 0 | C (N, 2N) 0 | 0 |
| PU-241 | CAPTURE | -62 | -54 | | |
| PU-241 | NU | 1151 | 1116 | | |
| PU-241 | FISSION | 824 | 805 | | |
| PU-241 | ELASTIC | 1 | 0 | | |
| PU-241 | INELASTC | -2 | 0 | | |
| PU-241 | MU-AVE | 0 | 0 | | |
| PU-241 | (N, 2N) | 0 | 0 | | |
| PU-242 | CAPTURE | -33 | -26 | | |
| PU-242 | NU | 66 | 62 | | |
| PU-242 | FISSION | 46 | 42 | | |
| PU-242 | ELASTIC | 0 | 0 | | |
| PU-242 | INELASTC | -2 | 0 | | |
| PU-242 | (N, 2N) | 0 | 0 | | |
| PU-242 | MU-AVE | 0 | 0 | | |
| AM-241 | CAPTURE | -64 | -65 | | |
| AM-241 | NU | 43 | 45 | | |
| AM-241 | FISSION | 31 | 31 | | |
| AM-241 | ELASTIC | 0 | 0 | | |
| AM-241 | INELASTC | 0 | 0 | | |
| AM-241 | MU-AVE | 0 | 0 | | |
| AM-241 | (N, 2N) | 0 | 0 | | |

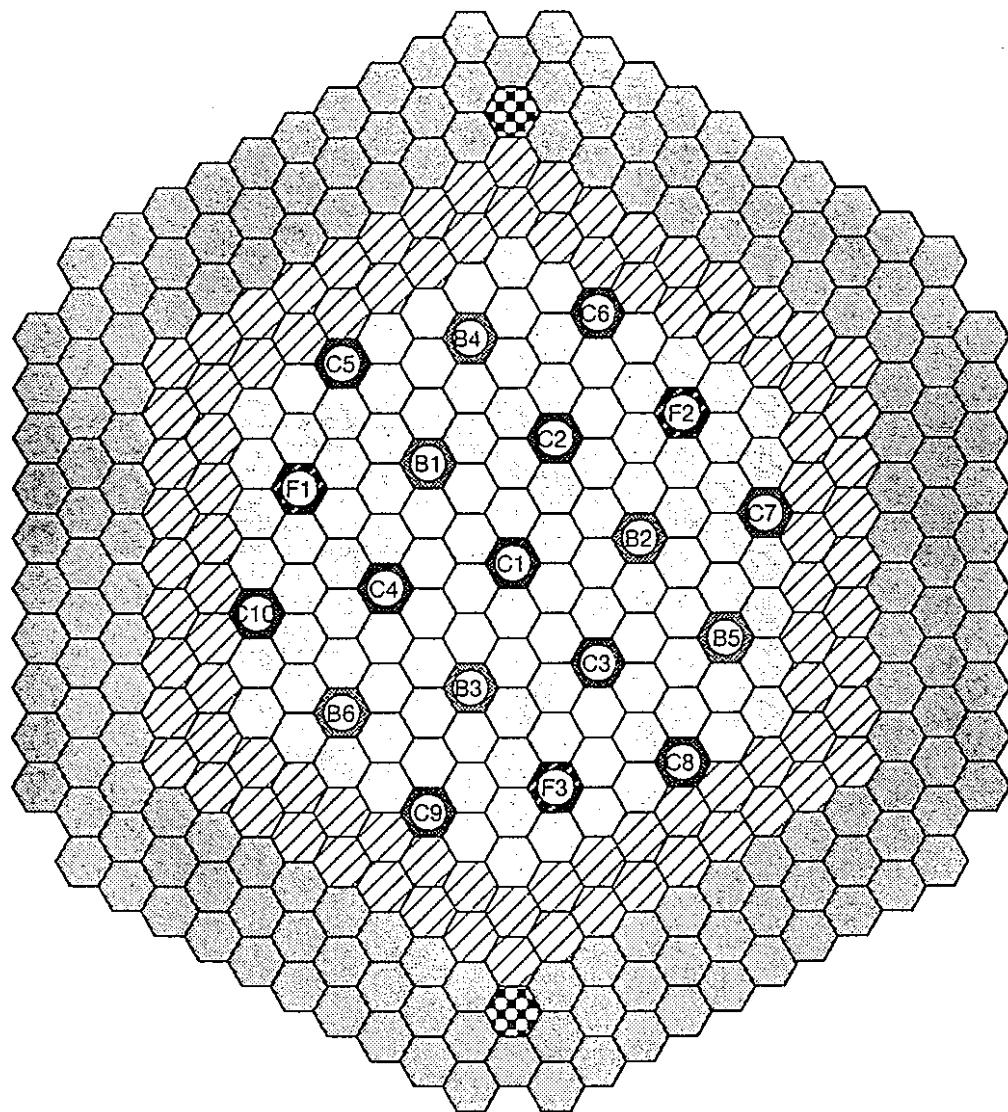
表 4.1-3 感度係数の比較 (JENDL2 と JENDL3.2 の比較 198 本体系)

| 核種 | reaction | total | | (1E-4 $\Delta k/kk' / \Delta \sigma/\sigma$) | | | |
|--------|----------|----------|--------|---|----------|------|------|
| | | JENDL3.2 | JENDL2 | JENDL3.2 | JENDL2 | | |
| U-235 | CAPTURE | -8 | -1 | FE | CAPTURE | -199 | -185 |
| U-235 | NU | 94 | 81 | FE | ELASTIC | 248 | 227 |
| U-235 | FISSION | 61 | 53 | FE | INELASTC | -181 | -170 |
| U-235 | ELASTIC | 0 | 0 | FE | MU-AVE | -80 | -79 |
| U-235 | INELASTC | 0 | 0 | FE | (N, 2N) | 0 | 0 |
| U-235 | MU-AVE | 0 | 0 | CR | CAPTURE | -51 | -52 |
| U-235 | (N, 2N) | 0 | 0 | CR | ELASTIC | 94 | 86 |
| U-238 | CAPTURE | -1925 | -1842 | CR | INELASTC | -41 | -35 |
| U-238 | NU | 1043 | 999 | CR | MU-AVE | -23 | -19 |
| U-238 | FISSION | 644 | 616 | CR | (N, 2N) | 0 | 0 |
| U-238 | ELASTIC | 262 | 261 | NI | CAPTURE | -115 | -113 |
| U-238 | INELASTC | -307 | -336 | NI | ELASTIC | 102 | 87 |
| U-238 | MU-AVE | -142 | -141 | NI | INELASTC | -23 | -24 |
| U-238 | (N, 2N) | 1 | 1 | NI | MU-AVE | -19 | -11 |
| PU-239 | CAPTURE | -559 | -570 | NI | (N, 2N) | 0 | 0 |
| PU-239 | NU | 6960 | 7008 | NA | CAPTURE | -22 | -19 |
| PU-239 | FISSION | 4927 | 4961 | NA | ELASTIC | 153 | 209 |
| PU-239 | ELASTIC | 20 | 17 | NA | INELASTC | -75 | -97 |
| PU-239 | INELASTC | -22 | -18 | NA | MU-AVE | -59 | -56 |
| PU-239 | MU-AVE | -14 | -8 | NA | (N, 2N) | 0 | 0 |
| PU-239 | (N, 2N) | 0 | 0 | O | CAPTURE | -18 | -19 |
| PU-240 | CAPTURE | -243 | -224 | O | ELASTIC | -7 | 47 |
| PU-240 | NU | 587 | 574 | O | INELASTC | -1 | -1 |
| PU-240 | FISSION | 400 | 385 | O | MU-AVE | -48 | -22 |
| PU-240 | ELASTIC | 10 | 4 | O | (N, 2N) | 0 | 0 |
| PU-240 | INELASTC | -11 | -8 | C | CAPTURE | 0 | 0 |
| PU-240 | MU-AVE | -4 | -1 | C | ELASTIC | 0 | 0 |
| PU-240 | (N, 2N) | 0 | 0 | C | INELASTC | 0 | 0 |
| PU-241 | CAPTURE | -58 | -53 | C | MU-AVE | 0 | 0 |
| PU-241 | NU | 1120 | 1115 | C | (N, 2N) | 0 | 0 |
| PU-241 | FISSION | 799 | 798 | | | | |
| PU-241 | ELASTIC | 1 | 0 | | | | |
| PU-241 | INELASTC | -2 | 0 | | | | |
| PU-241 | MU-AVE | 0 | 0 | | | | |
| PU-241 | (N, 2N) | 0 | 0 | | | | |
| PU-242 | CAPTURE | -32 | -25 | | | | |
| PU-242 | NU | 66 | 62 | | | | |
| PU-242 | FISSION | 46 | 41 | | | | |
| PU-242 | ELASTIC | 0 | 0 | | | | |
| PU-242 | INELASTC | -2 | 0 | | | | |
| PU-242 | MU-AVE | 0 | 0 | | | | |
| PU-242 | (N, 2N) | 0 | 0 | | | | |
| AM-241 | CAPTURE | -64 | -62 | | | | |
| AM-241 | NU | 43 | 42 | | | | |
| AM-241 | FISSION | 31 | 29 | | | | |
| AM-241 | ELASTIC | 0 | 0 | | | | |
| AM-241 | INELASTC | 0 | 0 | | | | |
| AM-241 | MU-AVE | 0 | 0 | | | | |
| AM-241 | (N, 2N) | 0 | 0 | | | | |



| 炉心構成要素 | | 記号 | 数量 |
|-------------|--------|----|-----|
| 炉心燃料集合体 | 内側炉心 | ◆ | 108 |
| | 外側炉心 | ◆ | 60 |
| プランケット燃料集合体 | | ◆ | 172 |
| 制御棒集合体 | 微調整棒 | ◆ | 3 |
| | 粗調整棒 | ◆ | 10 |
| | 後備炉停止棒 | ◆ | 6 |
| 中性子源集合体 | | ◆ | 2 |
| 中性子しゃへい体 | | ◆ | 316 |
| サーベイランス集合体 | | ◆ | 8 |
| 模擬燃料集合体 | | ◆ | 30 |

図 4.1-1 168体炉心



| 炉心構成要素 | | 記号 | 本数 |
|-------------|------|----|-----|
| 炉心燃料集合体 | 内側炉心 | ○ | 108 |
| | 外側炉心 | △ | 90 |
| ブランケット燃料集合体 | | □ | 172 |
| 中性子源集合体 | | ◆ | 2 |

| 炉心構成要素 | | 記号 | 本数 |
|--------|--------|----|----|
| 制御棒集合体 | 微調整棒 | ○ | 3 |
| | 粗調整棒 | △ | 10 |
| | 後端炉停止棒 | □ | 6 |

図 4.1-2 198 体炉心

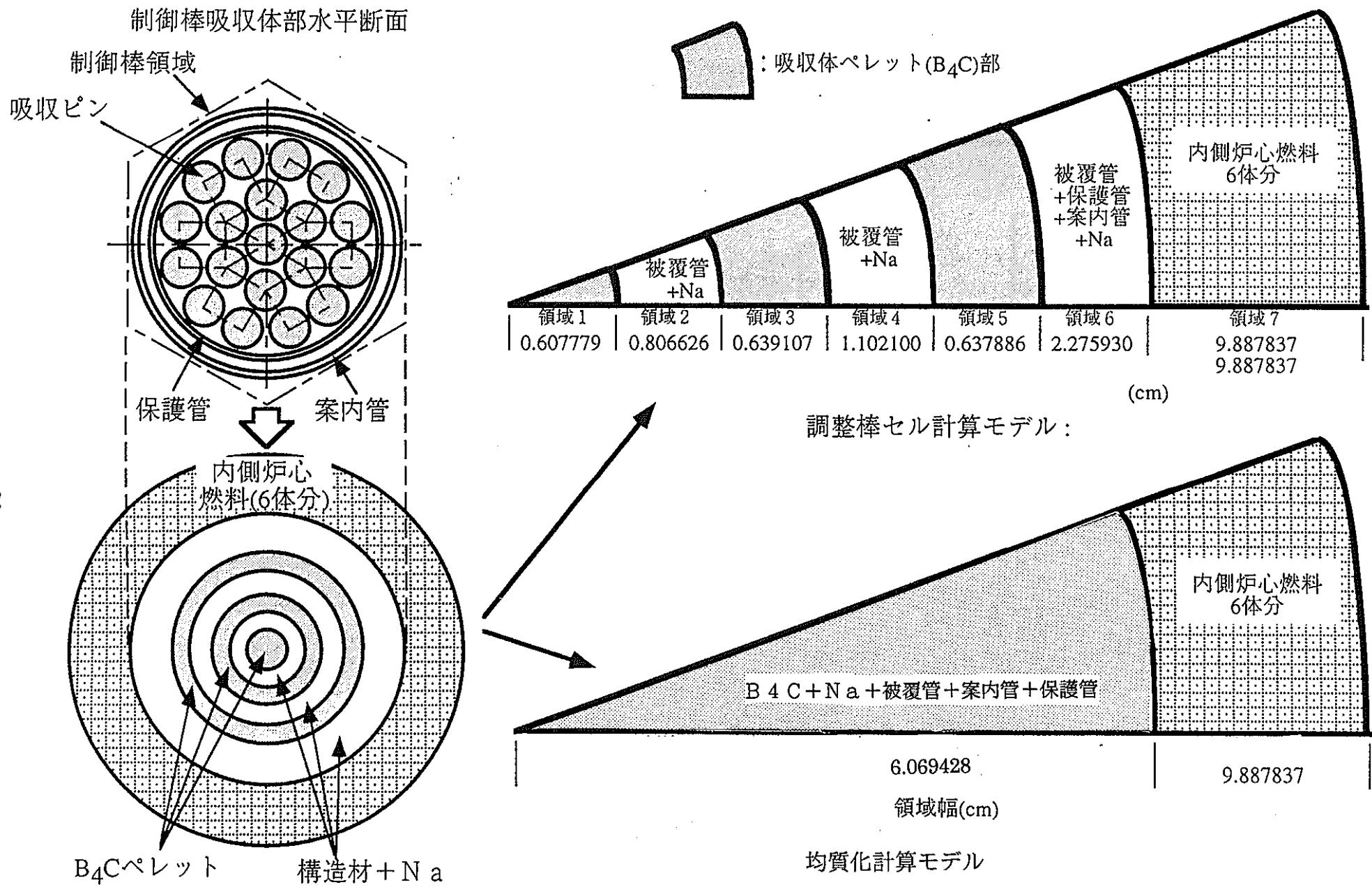


図 4.1-3 制御棒セル計算モデル

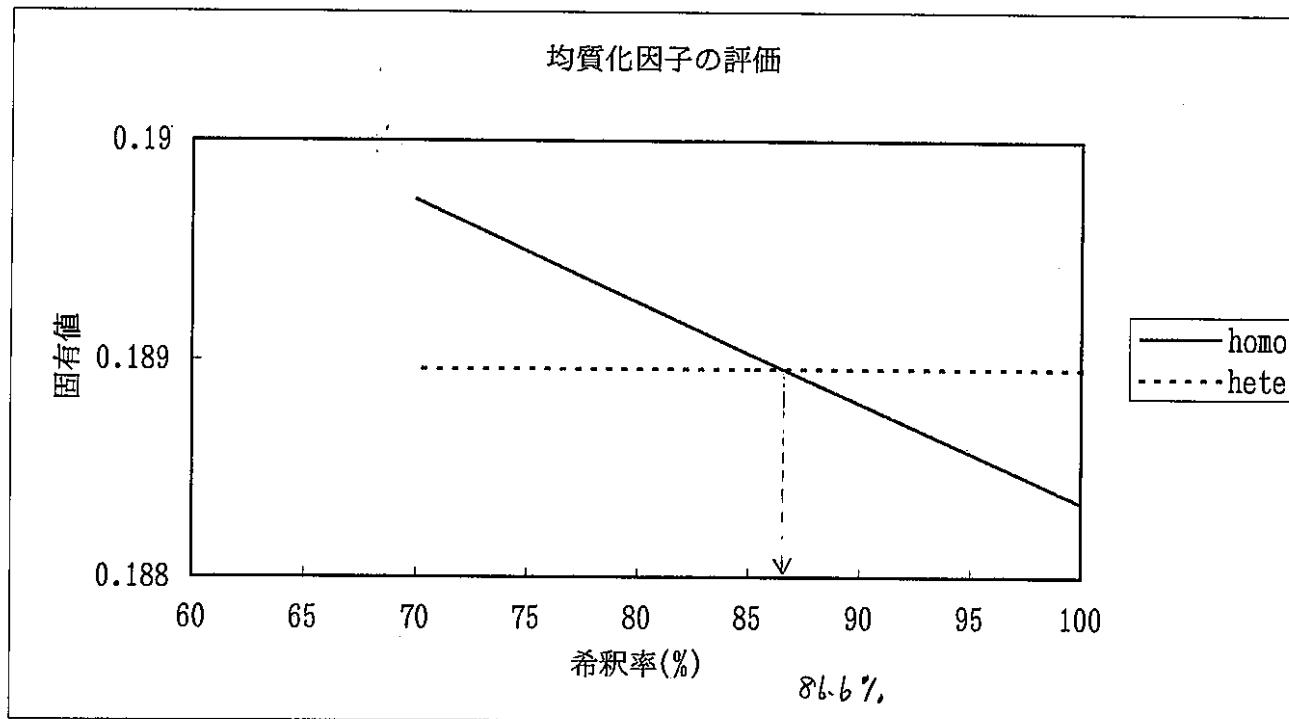


図 4.1-4 均質化因子の評価

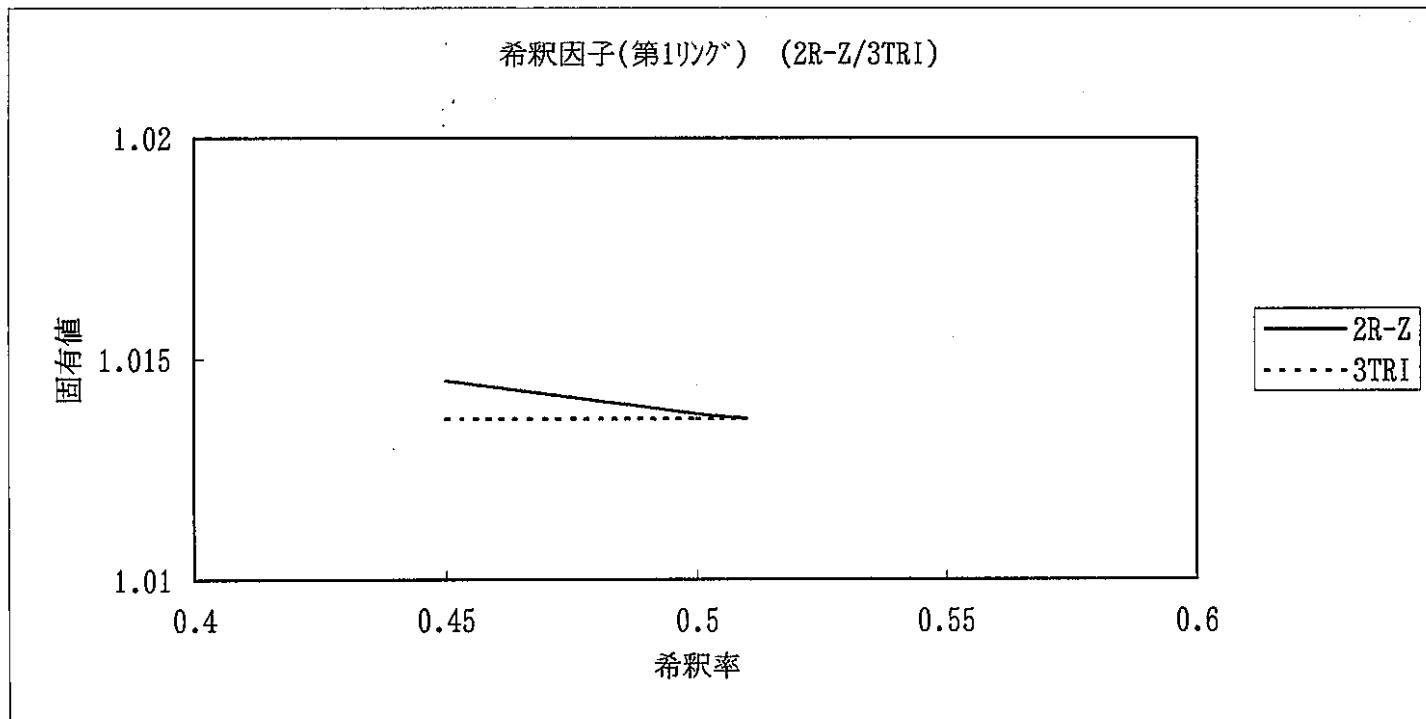


図 4.1-5 リング化因子の評価（第1リング）

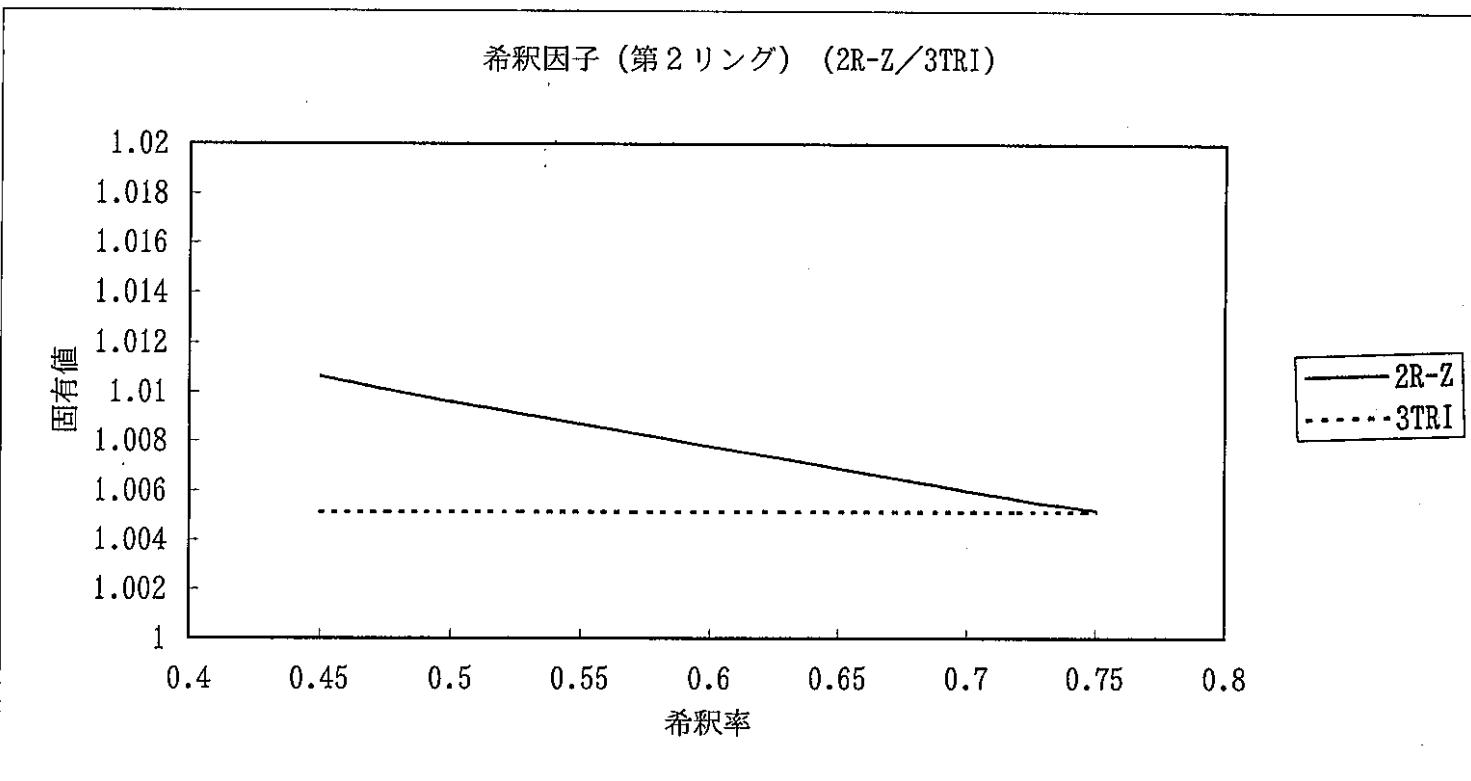


図 4.1-6 リング化因子の評価（第2 リング）

もんじゅ臨界体系のkeffへの感度 (168本)

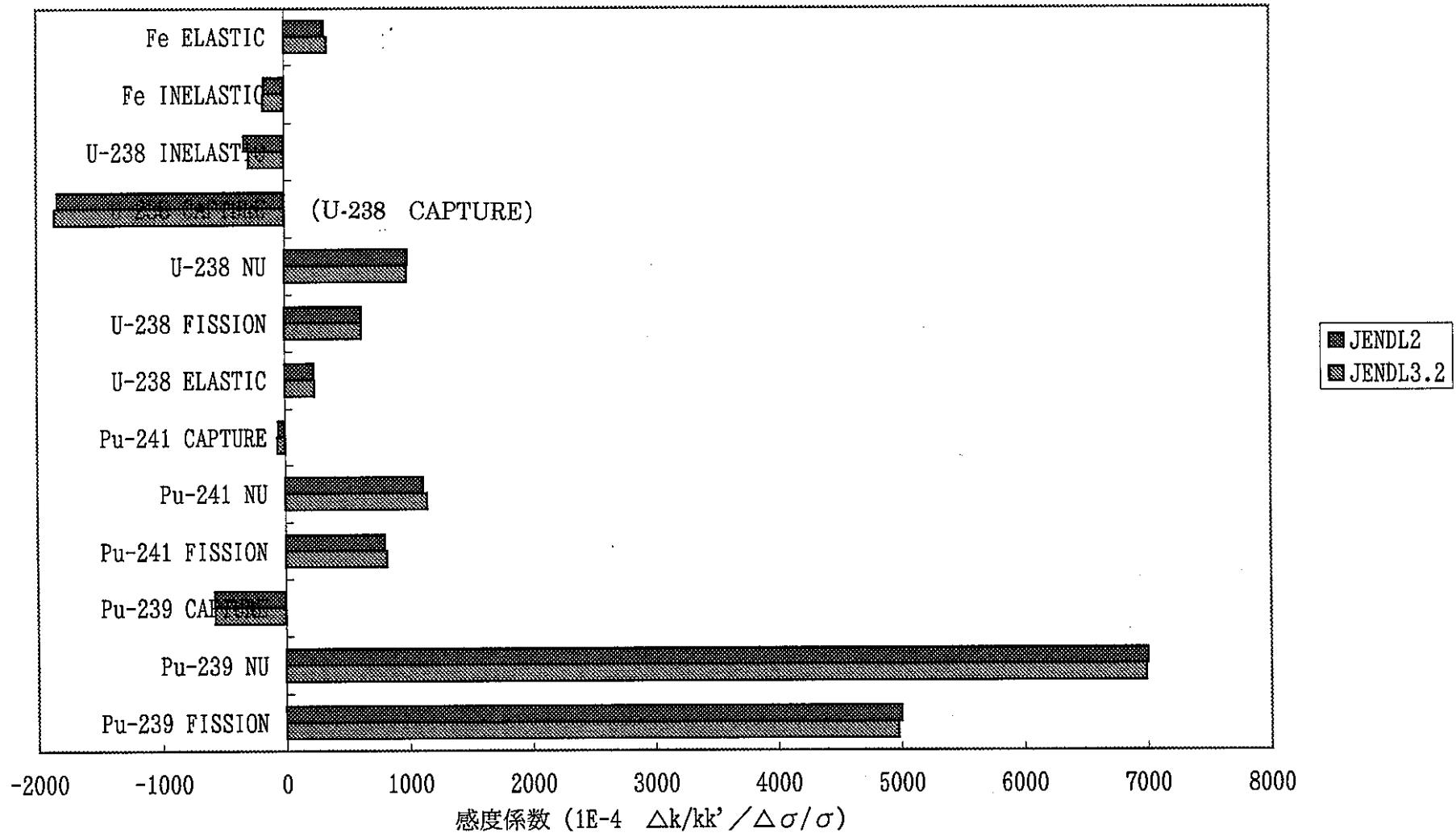


図 4.1-7 感度係数の比較 (JENDL2 と JENDL3.2 の比較 168 本体系)

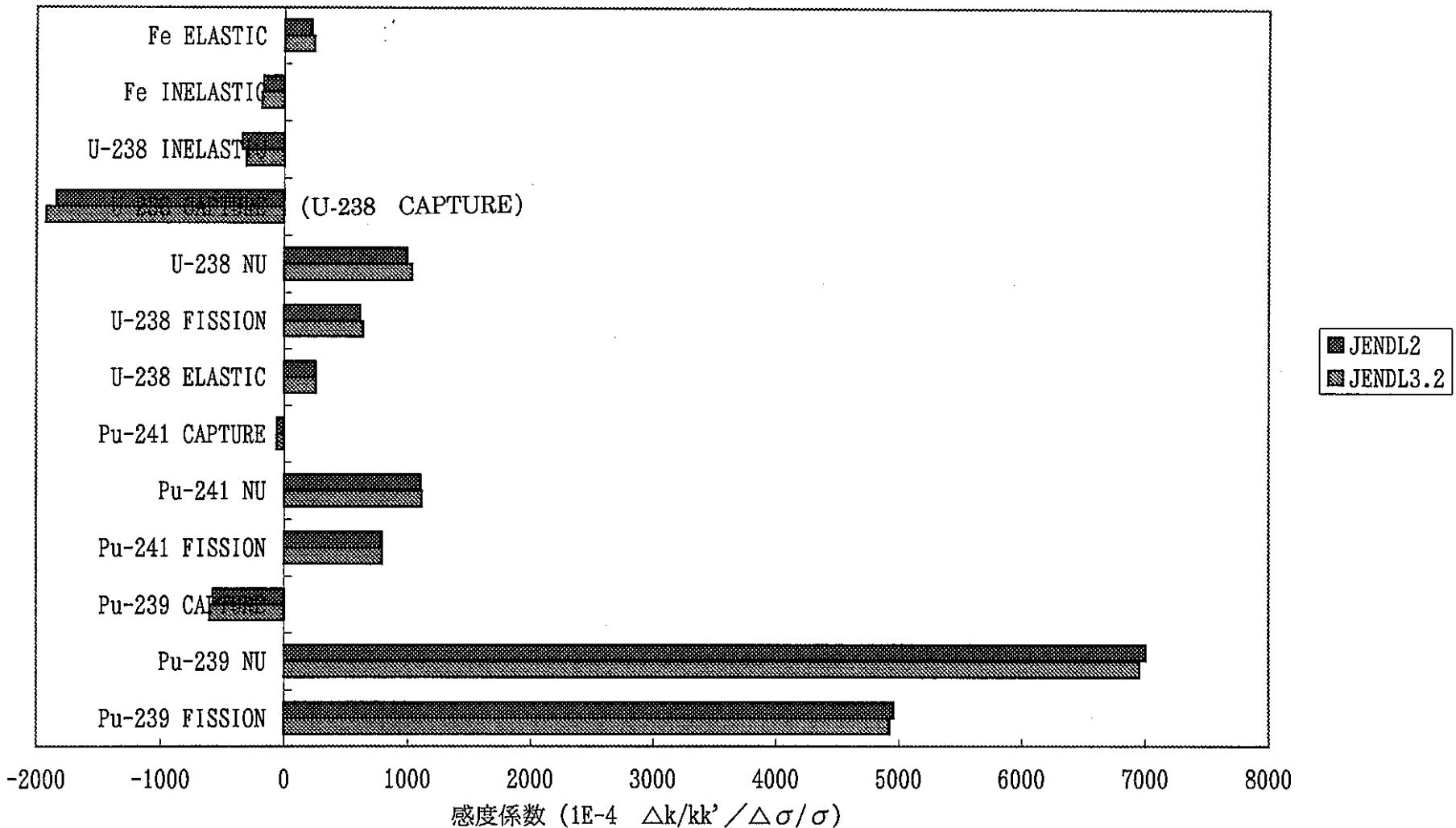
もんじゅ 198 体系 k_{eff} への感度係数

図 4.1-8 感度係数の比較 (JENDL2 と JENDL3.2 の比較 198 本体系)

4.2 制御棒価値に関する感度係数

(1) 目的

JENDL3.2 の調整に資する為、制御棒価値に対する感度係数を算出する。

(2) 制御棒の感度解析

評価対象炉心

- ・初臨界炉心（168 体燃料炉心）制御棒価値（参考）

表 4.2-1 に示す反応度価値が測定されている。¹⁾

炉心体系 図 4.2-1 に示す。

- ・初期炉心（198 体燃料炉心） 制御棒価値

表 4.2-2 に示す様に制御棒ワースが測定されている。¹⁾

炉心体系 図 4.2-2 に示す。

この中から各制御棒リングの代表として下記ケースの感度を評価する。

粗調整棒 CCR 1 挿入引き抜き

CCR 4 挿入引き抜き

CCR 10 挿入引き抜き

微調整棒 FCR 1 挿入引き抜き

後備炉停止棒 BCR 3 挿入引き抜き

BCR 6 挿入引き抜き

(3) 解析方法

- 感度解析評価 SAGEP コードを用いる。

中性子束、共役中性子束は CITATION-FBR コードを用いて算出する。

- エネルギー群数 18 群

（群分割 70 群のエネルギー分割に対し、

2, 4, 6, 8, 10, 13, 16, 19, 22, 25, 28, 31, 34, 37, 40, 43, 46, 70)

- 使用ライブラリ JENDL3.2

- 計算体系

中心制御棒（CCR 1） RZ 計算、XY 計算

その他の制御棒 XY 計算

- XY 計算に於ける制御棒部分挿入の取扱について

感度解析コードは2次元コードであるため、中心制御棒はR-Z計算で扱えるが、その他はX-Y計算を行うこととなる。この為制御棒部分挿入状態の扱いのために以下の評価を行い軸方向希釈率及び均質化因子を定める。

もんじゅ2次元R-Z体系の中心制御棒に対して以下の評価を行う。

(a) 軸方向希釈率の設定

制御棒挿入深度に対するそれと同じ固有値となる軸方向Naフオロアの実効断面積と吸収体部の断面積の混合比（軸方向希釈率）を設定する。

(b) 均質化因子の設定

均質計算を行う為に上記で設定した混合比でNaフオロアと吸収体部の組成を混合し、固有値が合うように均質モデルでの¹⁰B、¹¹B、Cに対する希釈率を求める。本希釈率は全てのリングで用いるものとする。

本評価の流れを図4.2-3に示す。

体系は198体炉心で評価した。評価結果を図4.2-4に示す。

これより

| 吸収体下端位置 (炉心下端より) | 軸方向希釈因子 (Naフオロアと吸収体の混合比) | 吸収体 | 均質化因子 |
|---------------------|-----------------------------|------|-------|
| 60.8cm | 0.81 | 0.19 | 0.74 |
| 64.2cm | 0.85 | 0.15 | 0.72 |

f. 後備炉停止棒の均質化因子の設定

後備炉停止棒の非均質効果を模擬する為、SLAROMコードにより均質計算と非均質計算を行い反応度保存になるように¹⁰B、¹¹B、Cに対する均質化因子を設定する。

なお後備炉停止棒は吸収体長は炉心長と同一の93cmあるのでe項で算出した軸方向希釈因子は設定しない。評価結果を図4.2-5に示す。これより

均質化因子 0.84

(4) 解析条件

a. 体系

図4.2-1と図4.2-2の集合体配置を模擬してR-Z計算体系とXY計算体系で計算する。

b. 制御棒挿入深度

- ・ RZ 計算 168 体 中心制御棒 炉心下端より 797mm ¹⁾
 - その他 ハーク位置
- 198 体 中心制御棒価値測定 ²⁾
 - 粗、微調整棒 炉心下端より 608mm ²⁾
 - 後備炉停止棒 ハーク位置
- その他の制御棒価値測定
 - 粗、微調整棒 炉心下端より 642mm
 - 後備炉停止棒 ハーク位置

c. 燃料組成

- 168 体 H 6 年 4 月 25 日の組成 ¹⁾
- 198 体 H 6 年 9 月 16 日の組成 ²⁾

(5) 解析結果

a. 168 本体系

- 2 次元 R-Z 計算による制御棒価値 (炉心下端より 797mm から 1065mm)
 - 0.16% $\Delta k/KK'$

得られた制御棒価値に対する感度係数を Appendix B-1 表に示す。(なお収束は 10^{-3} で行った。)

b. 198 本体系

中心制御棒計算 (CCR 1)

・ 制御棒価値 2 次元 R-Z 計算

- 拡散計算結果 0.95% $\Delta k/kk'$
- 感度解析結果 Appendix B-2 表

・ 制御棒価値 2 次元 XY 計算

- 拡散計算結果 0.91% $\Delta k/kk'$
- 感度解析結果 Appendix B-3 表

表 4.2-3 に上記結果を JENDL 2 による結果 ³⁾とともに対比して示す。

今回の制御棒部分挿入時の制御棒の取扱についての妥当性について検討する。

RZ 忠実モデルと軸方向均質モデルでの主要核種への感度はほぼ等しい。しかし

ながら RZ モデルでは忠実モデルと軸方向均質モデルで ^{238}U の σ_c で～25%程度の差がある。これは軸方向非均質化モデルでは上／下部ブランケット部にまで均質化した B4C が希釈されているため、上／下部ブランケットにおける ^{238}U の感度係数が異なってきたことによると推定される。 ^{238}U の σ_c 以外の感度係数は両モデルで殆ど一致している。但し、Na の σ_{el} で 30%弱の差異が生じているが感度も小さいことから問題は生じないと考える。

XY モデルについては収束判定因子に関しては 10^{-2} と 5×10^{-3} では殆ど差がない。このことから収束判定因子は 10^{-2} としても特に問題はないと考えられる。

RZ 忠実モデル計算と XY 計算との比較では主要核特性の感度係数はほぼ同等の値になっている。このことは制御棒が部分挿入された体系を XY モデルで近似する方法として本研究で採用している手法の妥当性を示している。但し、Na の σ_{el} が RZ 忠実モデルと異なっているが、この感度は上記でも述べたように小さいので問題ないと考える。

なお、JENDL2 による感度係数も JENDL3.2 の数値と殆ど変わらないことが分かる。

表 4.2-4 には RZ 計算で軸方向忠実モデルと均質化モデルで、表 4.2-5 に 7 群計算で 2 次元 X Y 計算と 3 次元 TRI-Z 計算で、 ^{239}Pu の σ_f と ^{238}U の σ_c を 10%増加させて制御棒反応度変化を検討した結果を示す。

この計算でも 2 次元 X Y 計算は忠実モデル（2 次元及び 3 次元 TRI-Z）の良い近似となっており、本 XY 近似手法の妥当性が確認できた。

CCR 4 制御棒

・制御棒価値 2 次元 X Y 計算

拡散計算結果 $0.81\%\Delta k/kk'$

感度計算結果 Appendix B-4 表

CCR 10 制御棒

・制御棒 2 次元 X Y 計算 $0.53\%\Delta k/kk'$

感度計算結果 Appendix B-5 表

表 4.2-5 に見られるように、CCR 4、CCR 10 の結果に対して感度係数を用いて制御棒価値の変化を計算した結果と直接計算の結果は良い一致を示している。

F C R 1 制御棒

- ・制御棒 2 次元 X Y 計算 $0.62\%\Delta k/kk'$
- 感度計算結果 Appendix B - 6 表

B C R 3 制御棒

- ・制御棒 2 次元 X Y 計算 $1.32\%\Delta k/kk'$
- 感度計算結果 Appendix B - 7 表

B C R 6 制御棒

- ・制御棒 2 次元 X Y 計算 $0.99\%\Delta k/kk'$
- 感度計算結果 Appendix B - 8 表

表 4.2-1 制御棒価値測定結果（初臨界炉心）

| 制御棒位置 | 炉心下端よりの制御棒位置 | 反応度 |
|-------|--------------|-------------|
| CCR1 | 797mm～1065mm | 0.15%△k/kk' |

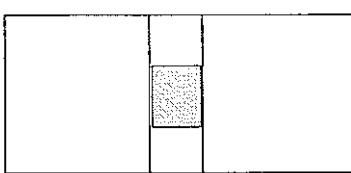
表 4.2-2 制御棒単体価値測定結果

| 制御棒種類 | 測定値 |
|-------------|-------|
| 調整棒 CCR1 | 0.974 |
| CCR4 | 0.840 |
| CCR10 | 0.575 |
| FCR1 | 0.658 |
| 後備炉停止棒 BCR1 | 1.187 |
| BCR6 | 0.938 |

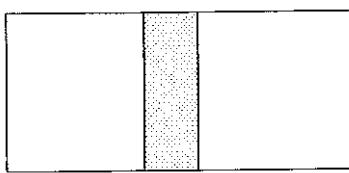
表 4.2-3 感度係数の比較

| 核種 | reaction | (1E-4 Δk/kk' / Δσ/σ) | | | | | (1E-4 Δk/kk' / Δσ/σ) | | | | |
|--------|----------|--------------------------|--------------------------|--------------------|--------------------|----------------------|--------------------------|--------------------------|--------------------|--------------------|----------------------|
| | | RZcal | | xycal | | | RZcal | | xycal | | |
| | | JENDL3.2 軸方向忠 実モデル | JENDL3.2 軸方向均 質モデル | JENDL3.2 収束1E-2 | JENDL3.2 収束5E-3 | JENDL2 PNC殿計 算 | JENDL3.2 軸方向忠 実モデル | JENDL3.2 軸方向均 質モデル | JENDL3.2 収束1E-2 | JENDL3.2 収束5E-3 | JENDL2 PNC殿計 算 |
| U-235 | CAPTURE | -7 | -9 | -8 | -8 | -2 | | | | | |
| U-235 | NU | -82 | -55 | -81 | -82 | -85 | | | | | |
| U-235 | FISSION | -101 | -75 | -96 | -97 | -95 | | | | | |
| U-235 | ELASTIC | 0 | 0 | 0 | 0 | 0 | | | | | |
| U-235 | INELASTC | 0 | 0 | 0 | 0 | 0 | | | | | |
| U-235 | (N,2N) | 0 | 0 | 0 | 0 | 0 | | | | | |
| U-235 | MU-AVE | 0 | 0 | 0 | 0 | 0 | | | | | |
| U-238 | CAPTURE | -1617 | -2021 | -1676 | -1678 | -1532 | | | | | |
| U-238 | NU | -1871 | -1847 | -1873 | -1873 | -1909 | | | | | |
| U-238 | FISSION | -1563 | -1548 | -1538 | -1538 | -1573 | | | | | |
| U-238 | ELASTIC | -853 | -945 | -753 | -758 | -982 | | | | | |
| U-238 | INELASTC | 462 | 426 | 699 | 697 | 717 | | | | | |
| U-238 | (N,2N) | -5 | -5 | -4 | -4 | -5 | | | | | |
| U-238 | MU-AVE | 561 | 581 | 451 | 455 | 527 | | | | | |
| PU-239 | CAPTURE | -682 | -720 | -792 | -795 | -765 | | | | | |
| PU-239 | NU | -5987 | -6021 | -6002 | -6000 | -5989 | | | | | |
| PU-239 | FISSION | -6322 | -6362 | -6560 | -6557 | -6464 | | | | | |
| PU-239 | ELASTIC | -36 | -47 | -24 | -23 | -35 | | | | | |
| PU-239 | INELASTC | 46 | 45 | 64 | 65 | 48 | | | | | |
| PU-239 | (N,2N) | 0 | 0 | 0 | 0 | 0 | | | | | |
| PU-239 | MU-AVE | 35 | 37 | 21 | 21 | 16 | | | | | |
| PU-240 | CAPTURE | -289 | -303 | -330 | -333 | -302 | | | | | |
| PU-240 | NU | -1127 | -1142 | -1110 | -1111 | -1089 | | | | | |
| PU-240 | FISSION | -972 | -986 | -963 | -964 | -946 | | | | | |
| PU-240 | ELASTIC | -14 | -18 | -11 | -10 | -14 | | | | | |
| PU-240 | INELASTC | 23 | 21 | 31 | 31 | 20 | | | | | |
| PU-240 | (N,2N) | 0 | 0 | 0 | 0 | 0 | | | | | |
| PU-240 | MU-AVE | 10 | 11 | 6 | 6 | 4 | | | | | |
| PU-241 | CAPTURE | -47 | -51 | -59 | -59 | -47 | | | | | |
| PU-241 | NU | -651 | -642 | -648 | -648 | -626 | | | | | |
| PU-241 | FISSION | -777 | -774 | -818 | -820 | -773 | | | | | |
| PU-241 | ELASTIC | -5 | -6 | 0 | 0 | 0 | | | | | |
| PU-241 | INELASTC | 7 | 7 | 9 | 9 | 5 | | | | | |
| PU-241 | (N,2N) | 0 | 0 | 0 | 0 | 0 | | | | | |
| PU-241 | MU-AVE | 4 | 5 | 2 | 2 | 0 | | | | | |
| PU-242 | CAPTURE | -38 | -40 | -44 | -44 | -37 | | | | | |
| PU-242 | NU | -144 | -146 | -143 | -143 | -137 | | | | | |
| PU-242 | FISSION | -122 | -124 | -122 | -122 | -117 | | | | | |
| PU-242 | ELASTIC | 0 | -3 | 0 | 0 | 0 | | | | | |
| PU-242 | INELASTC | 4 | 4 | 6 | 6 | 2 | | | | | |
| PU-242 | (N,2N) | 0 | 0 | 0 | 0 | 0 | | | | | |
| PU-242 | MU-AVE | 0 | 0 | 0 | 0 | 0 | | | | | |
| AM-241 | CAPTURE | -155 | -158 | -161 | -163 | -150 | | | | | |
| AM-241 | NU | -39 | -39 | -42 | -42 | -47 | | | | | |
| AM-241 | FISSION | -40 | -40 | -43 | -42 | -48 | | | | | |
| AM-241 | ELASTIC | 0 | 0 | 0 | 0 | 0 | | | | | |
| AM-241 | INELASTC | 1 | 1 | 4 | 4 | 0 | | | | | |
| AM-241 | (N,2N) | 0 | 0 | 0 | 0 | 0 | | | | | |
| AM-241 | MU-AVE | 0 | 0 | 0 | 0 | 0 | | | | | |

RZ計算については収束は1E-3で行った。
PNC殿計算値： PNC ZJ2270 95-001「もんじゅ」核特性感度解析



軸方向忠実モデル



軸方向均質モデル
(2次元XY計算用の組成を用いる)

表 4.2-4 直接計算による制御棒価値の感度係数の価値（中心制御棒）

| (Δk) | | | | |
|---------------|------------------------|------------------|-----------------------------|-----------------------------|
| | | 基準ケース* | 239Pu の σ_f 10%増加 | 238 U の σ_c 10%増加 |
| 直接計算 | 2 次元 RZ 計算 忠実モデル | (9.70E-3) | -0.57E-3 (9.13E-3) | -0.15E-3 (9.55E-3) |
| | 2 次元 RZ 計算 軸方向均質モデル | (9.78E-3) | -0.58E-3 (9.20E-3) | -0.18E-3 (9.60E-3) |
| 感度係数より算出された△k | 2 次元 RZ 忠実モデル | 基準を 9.70E-3 とする。 | -0.61 ₃ E-3 | -0.15 ₆ E-3 |
| | 2 次元 RZ 計算 軸方向均質モデル | 同上 | -0.61 ₇ E-3 | -0.19 ₆ E-3 |
| | 2 次元 XY 計算 | 同上 | -0.64 ₁ E-3 | -0.16 ₅ E-3 |

() 内は実効増倍率

*直接計算はメッシュ等を感度係数用と異なるものを用いている。

表 4.2-5 直接計算による制御棒価値の感度計算（7 群計算）

| (Δk) | | | | |
|---------------|-----------|------------------|-----------------------------|-----------------------------|
| | | 基準ケース | 239Pu の σ_f 10%増加 | 238 U の σ_c 10%増加 |
| 2 次元 X Y 計算 | CCR4 制御棒 | 8.67E-3 | -0.54E-3 (8.14E-3) | -0.1E-3 (8.57E-3) |
| | CCR10 制御棒 | 5.66E-3 | -0.35E-3 (5.31E-3) | -0.03E-3 (5.63E-3) |
| 3 次元 TRI-Z | CCR4 制御棒 | 9.13E-3 | -0.54E-3 (8.59E-3) | -0.09E-3 (9.04E-4) |
| | CCR10 制御棒 | 6.08E-3 | -0.37E-3 (5.71E-3) | -0.03E-3 (6.05E-3) |
| 感度係数より算出された△k | CCR4 制御棒 | 基準を 8.67E-3 とする | -0.57 ₈ E-3 | -0.13 ₆ E-3 |
| | CCR10 制御棒 | 基準を 5.66E-3 とする。 | -0.39E-3 | -0.06E-3 |

() 内は実効増倍率

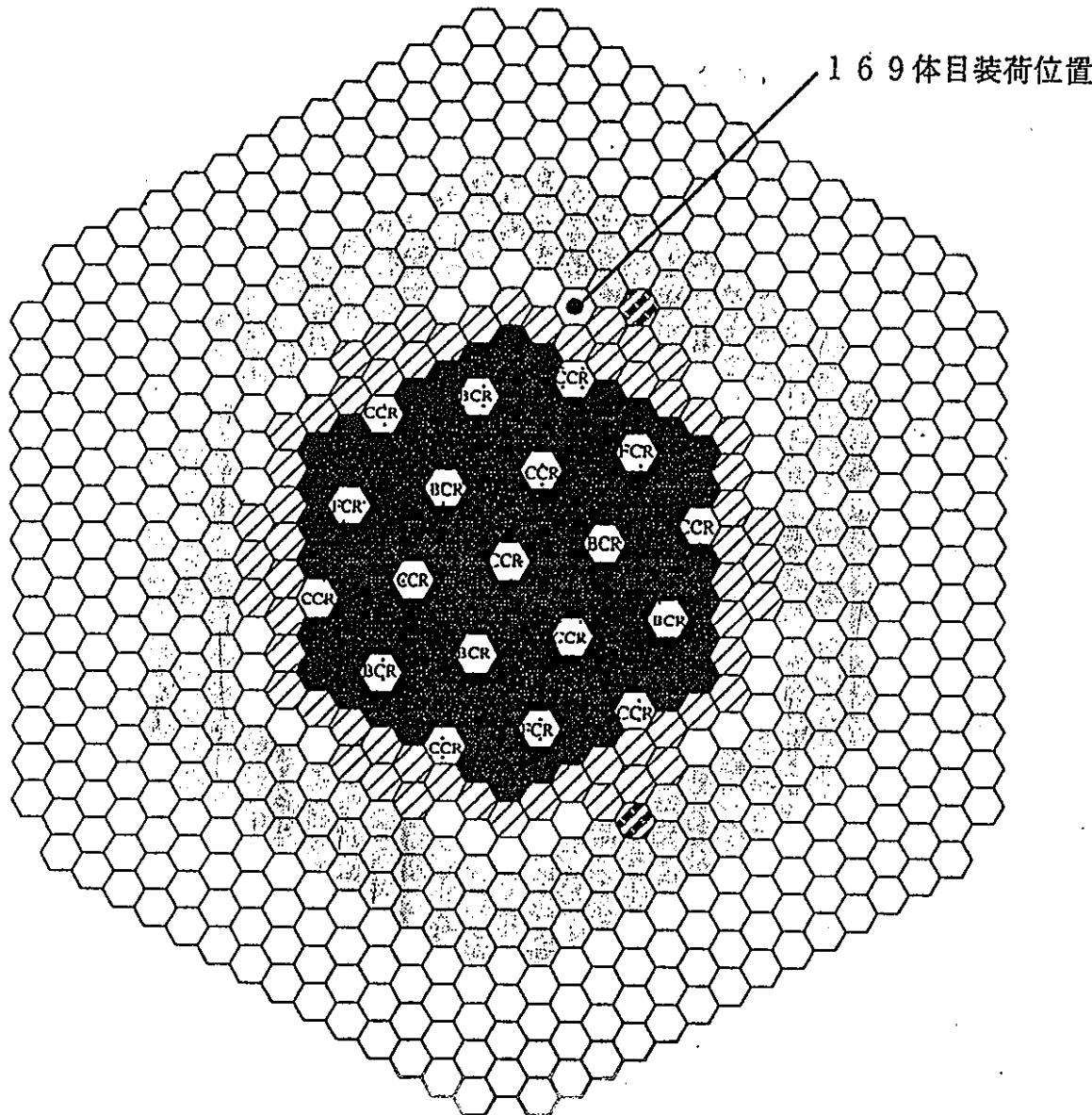
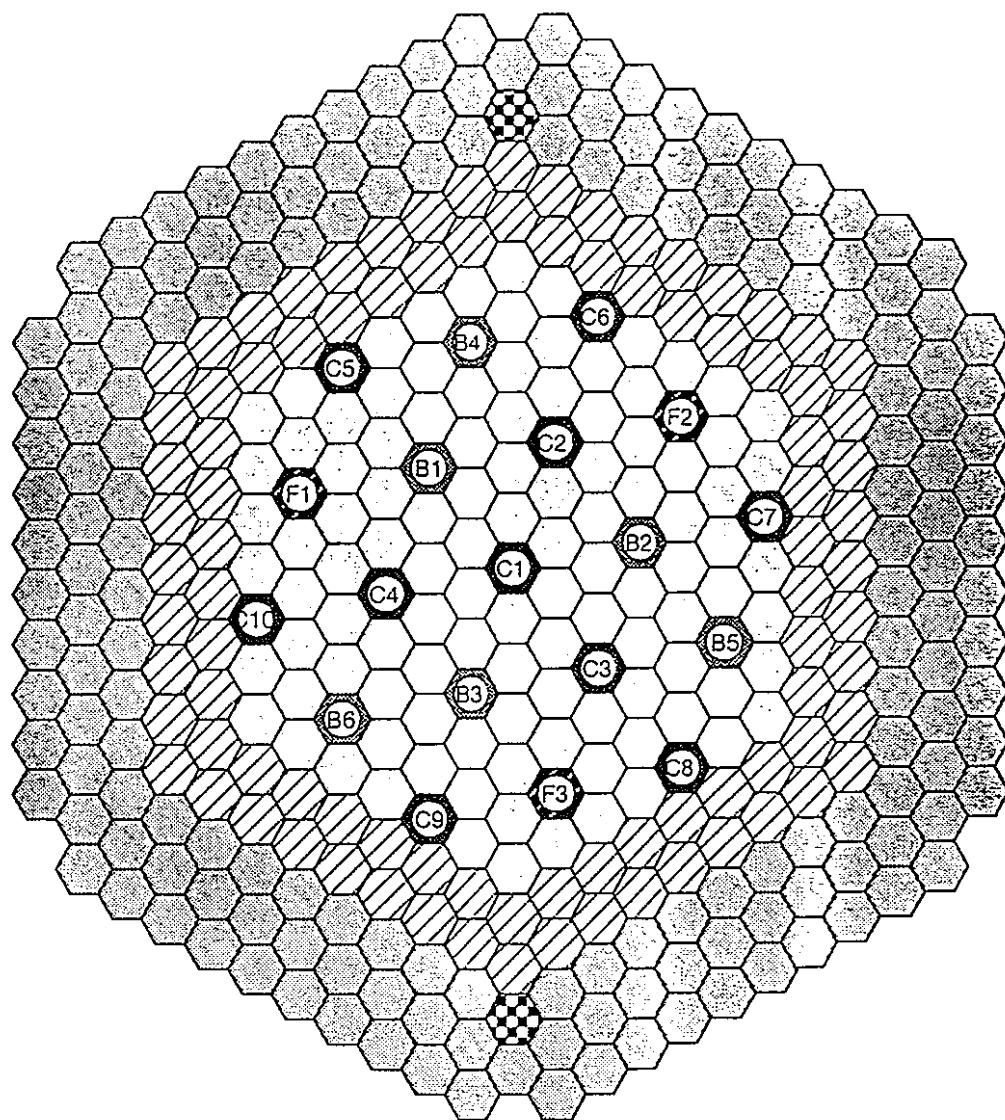


図 4.2-1 168 体炉心

| 炉心構成要素 | 記号 | 数量 |
|-------------|--------|-----|
| 炉心燃料集合体 | 内側炉心 | 108 |
| | 外側炉心 | 60 |
| プランケット燃料集合体 | | 172 |
| 制御棒集合体 | 微調整棒 | 3 |
| | 粗調整棒 | 10 |
| | 後備炉停止棒 | 6 |
| 中性子源集合体 | | 2 |
| 中性子しゃへい体 | | 316 |
| サーベイランス集合体 | | 8 |
| 模擬燃料集合体 | | 30 |



| 炉心構成要素 | 記号 | 本数 | 炉心構成要素 | 記号 | 本数 |
|-------------|------|-----|--------|-------|----|
| 炉心燃料集合体 | 内側炉心 | 108 | 制御棒集合体 | 数調整棒 | 3 |
| | 外側炉心 | 90 | | 粗調整棒 | 10 |
| ブランケット燃料集合体 | ○ | 172 | | 後端定位棒 | 6 |
| 中性子源集合体 | △ | 2 | | | |

図 4.2-2 198 体炉心

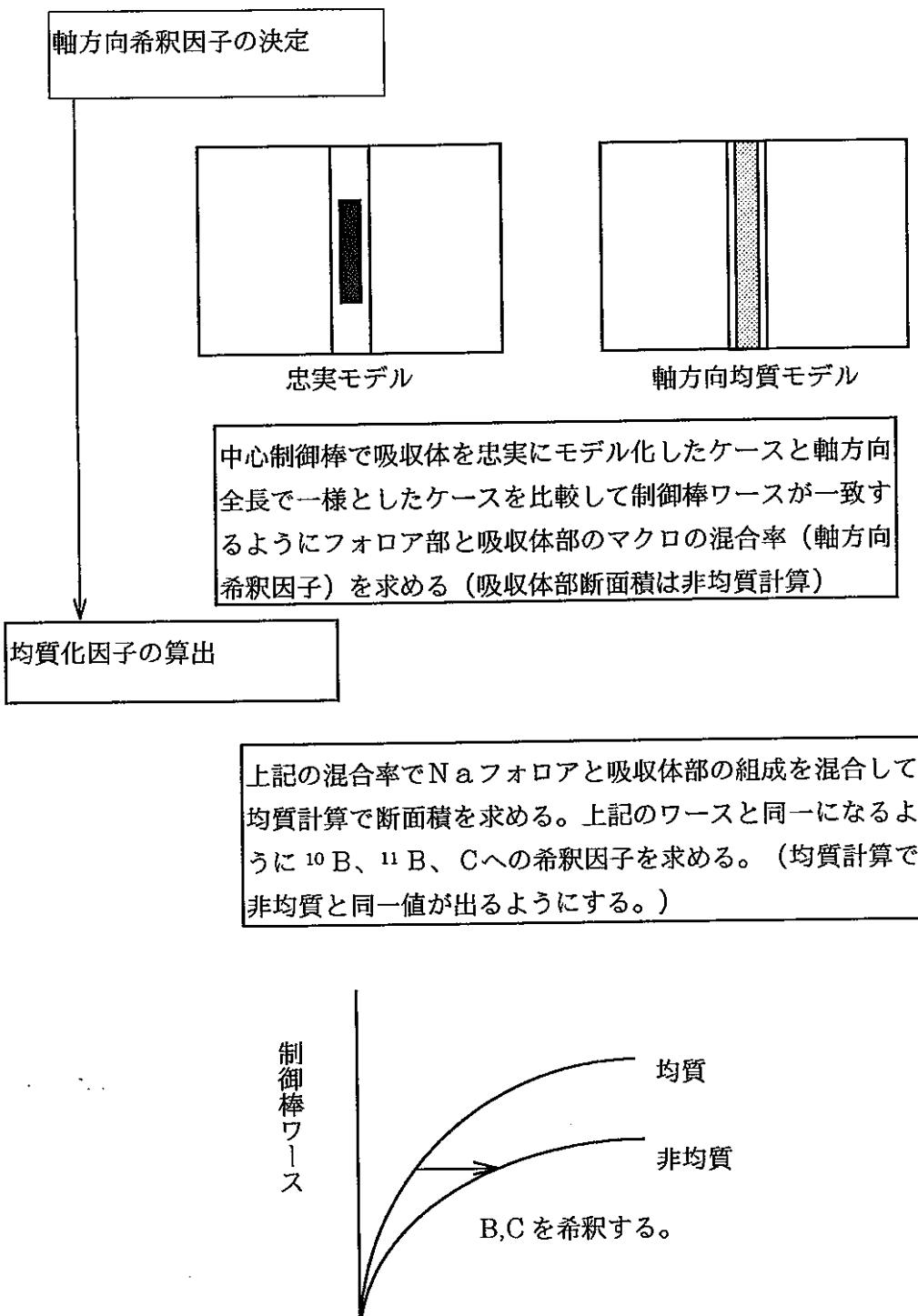


図 4.2-3 XY計算部分挿入用の希釈因子の設定の流れ

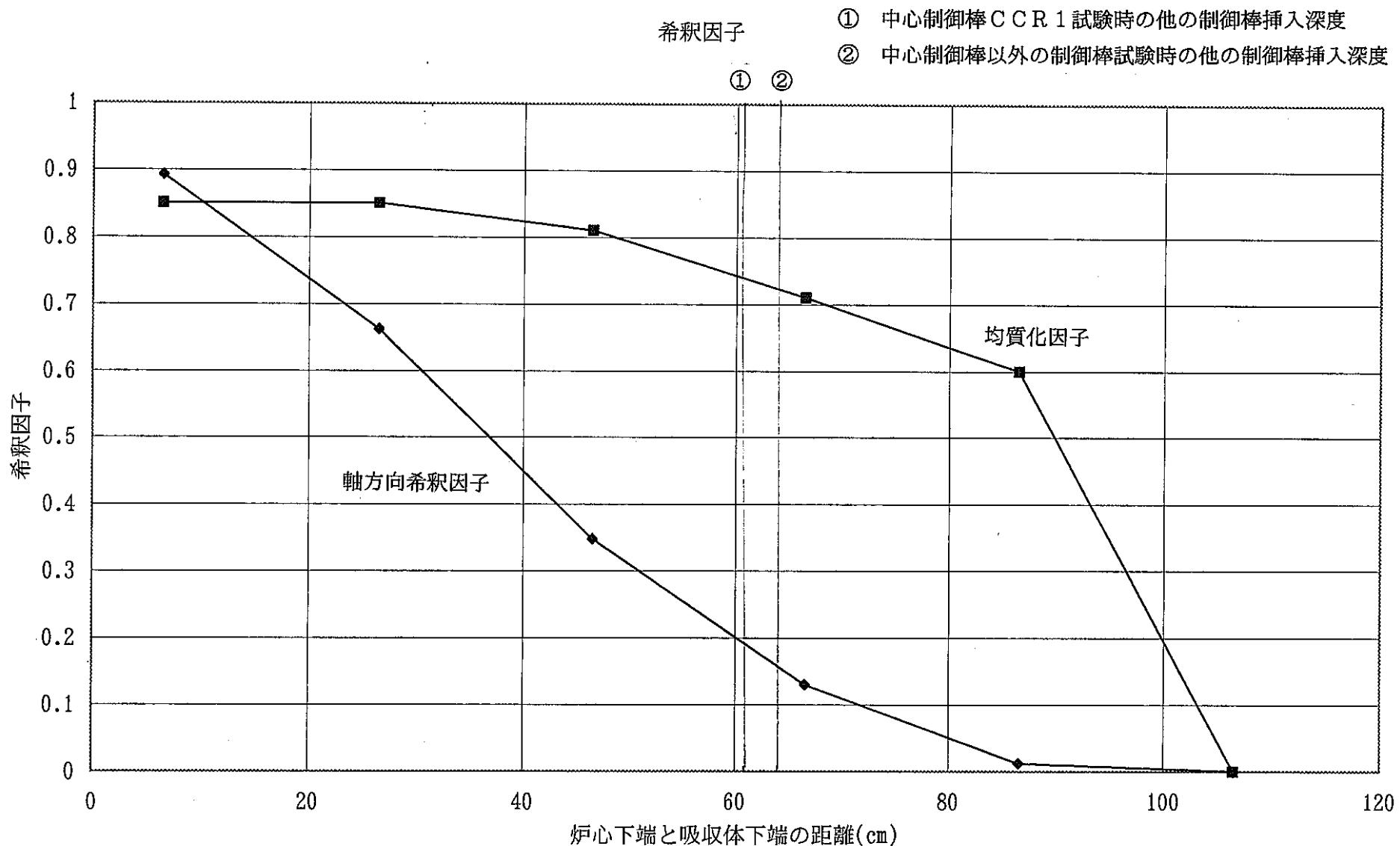


図 4.2-4 X Y 計算時制御棒部分挿入時用軸方向希釈因子と均質化因子

後備炉停止棒の希釈率

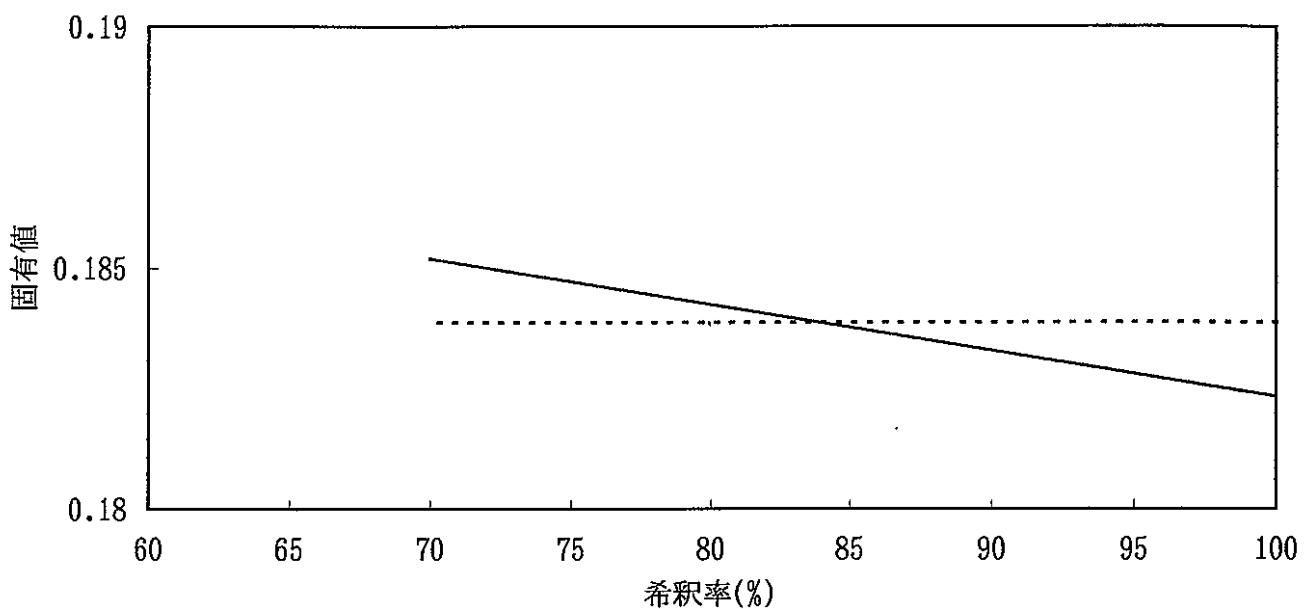


図 4.2-5 後備炉停止棒の均質化因子

5. おわりに

実証炉設計用統合炉定数作成の一環として、もんじゅ性能試験データをレビューし、臨界性と制御棒価値に関し、実験データ及び解析結果を整理し、その誤差評価を行った。また、これらの特性（臨界性及び制御棒価値）の各種断面積に対する感度係数を、一般化摂動コード SAGEP により、計算した。

ここで得られた測定誤差、解析誤差、C/E 値、及び感度係数は、本研究シリーズの他の部分で JENDL3.2 の断面積調整に活用される。

今後、更に統合炉定数の充実のために活用するべき積分データとしては、出力分布、燃焼反応度等が考えられる。特に、燃焼反応度に関しては、もんじゅの全出力換算運転日数は 40 日程度と少ないにもかかわらず、燃焼反応度の測定値が安定しており、臨界集合体では得られない有用な情報を含んでいることから、考慮の対象にする価値は十分にある。

冷却材ボイド反応度は、輸送計算による解析値と測定値の一致が悪いことから、このデータを炉定数調整に用いるのは、この不一致の原因を解明してからになる。

参考文献

- (1) 沖元豊、鈴木隆之、他、高速増殖原型炉「もんじゅ」性能試験報告書 最小臨界炉心特性確認：PNC ZN2410 95-071、1995年5月
- (2) 澤田周作、沖元豊、他、高速増殖原型炉「もんじゅ」性能試験報告書 制御棒価値確認（その1）(SST-R-2-11)：PNC ZN2410 96-013、1996年4月
- (3) 斎藤正幸、鰯坂洋史、「もんじゅ」核特性感度解析(I)：PNC ZJ2270 95-001、1995年3月

謝 辞

本研究を遂行するに当たり、貴重なコメントを頂き、また計算コードの提供や資料の開示の労取って頂いた石川真氏、杉野和輝氏、もんじゅの解析結果を開示して下さった鈴木隆之氏、検討会において貴重なコメントを頂いた統合炉定数検討会のメンバー諸氏に対し、深く感謝の意を表します。

Appendix A

実効増倍率に対する感度係数

表A-1(1/4) 実効倍増率に対する感度係数 (168体炉心 keff rcal)

| 核種 | reaction | 群数 | | | | | | | | | | | | | | (1E-4Δk/kk' / Δσ/σ) | | | | | | | | | | | |
|--------|-----------|-------|----|-----|-----|------|------|-----|------|------|------|------|------|------|------|---------------------|-----|------|-----|-----|-----|-----|----|---|---|---|---|
| | | total | 18 | 17 | 16 | 15 | 14 | 13 | 12 | 11 | 10 | 9 | 8 | 7 | 6 | 5 | 4 | 3 | 2 | 1 | | | | | | | |
| U-235 | CAPTURE | -8 | 0 | 0 | 0 | -1 | -1 | 0 | -1 | -1 | -1 | -1 | -1 | -1 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| U-235 | NU | 86 | 1 | 1 | 3 | 6 | 9 | 3 | 5 | 7 | 9 | 10 | 10 | 8 | 6 | 3 | 2 | 2 | 1 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| U-235 | FISSION | 60 | 1 | 1 | 1 | 2 | 5 | 6 | 2 | 4 | 5 | 6 | 7 | 5 | 4 | 2 | 2 | 1 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| U-235 | ELASTIC | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| U-235 | INELASTIC | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| U-235 | MU-AVE | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| U-235 | (N,2N) | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| U-238 | CAPTURE | -1853 | -7 | -20 | -44 | -134 | -184 | -82 | -165 | -227 | -275 | -238 | -173 | -129 | -109 | -43 | -17 | -5 | -1 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| U-238 | NU | 993 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 3 | 33 | 398 | 343 | 156 | 60 | 0 | 0 | 0 | 0 | 0 |
| U-238 | FISSION | 621 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 2 | 21 | 246 | 210 | 102 | 40 | 0 | 0 | 0 | 0 |
| U-238 | ELASTIC | 244 | 0 | 0 | 0 | 0 | 1 | 5 | 1 | 4 | 10 | 22 | 38 | 50 | 46 | 40 | 11 | 9 | 5 | 2 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| U-238 | INELASTIC | -285 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | -6 | -14 | -7 | -1 | -37 | -103 | -90 | -23 | -4 | 0 | 0 | 0 | 0 | 0 | |
| U-238 | MU-AVE | -120 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | -1 | -3 | -9 | -18 | -27 | -12 | -17 | -19 | -11 | -3 | 0 | 0 | 0 | 0 | 0 |
| U-238 | (N,2N) | 1 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Pu-238 | CAPTURE | -14 | 0 | 0 | -1 | -2 | -2 | -1 | -1 | -1 | -2 | -2 | -1 | -1 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 1 |
| Pu-238 | NU | 86 | 0 | 0 | 1 | 2 | 2 | 1 | 3 | 4 | 6 | 6 | 8 | 11 | 16 | 9 | 8 | 6 | 2 | 1 | 0 | 0 | 0 | 0 | 0 | 0 | |
| Pu-238 | FISSION | 60 | 0 | 0 | 1 | 1 | 2 | 1 | 2 | 3 | 4 | 6 | 8 | 11 | 16 | 9 | 8 | 6 | 2 | 1 | 0 | 0 | 0 | 0 | 0 | 0 | |
| Pu-238 | ELASTIC | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | |
| Pu-238 | INELASTIC | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | |
| Pu-238 | MU-AVE | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | |
| Pu-238 | (N,2N) | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | |
| PU-239 | CAPTURE | -570 | -4 | -10 | -36 | -72 | -96 | -36 | -59 | -57 | -56 | -48 | -44 | -31 | -16 | -3 | -2 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | |
| PU-239 | NU | 6990 | 17 | 45 | 121 | 301 | 429 | 145 | 302 | 434 | 633 | 797 | 916 | 892 | 827 | 382 | 372 | 250 | 99 | 28 | 0 | 0 | 0 | 0 | 0 | 0 | |
| PU-239 | FISSION | 4981 | 9 | 28 | 81 | 208 | 308 | 105 | 221 | 320 | 467 | 583 | 659 | 634 | 580 | 266 | 252 | 170 | 70 | 20 | 0 | 0 | 0 | 0 | 0 | 0 | |
| PU-239 | ELASTIC | 20 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 1 | 2 | 3 | 4 | 4 | 3 | 1 | 1 | 1 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | |
| PU-239 | INELASTIC | -22 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | -1 | -1 | -3 | -7 | -6 | -2 | 0 | 0 | 0 | 0 | 0 | |
| PU-239 | MU-AVE | -13 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | -1 | -2 | -1 | -2 | -3 | -2 | 0 | 0 | 0 | 0 | 0 | |
| PU-239 | (N,2N) | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | |
| PU-240 | CAPTURE | -246 | -2 | -6 | -12 | -26 | -32 | -11 | -20 | -26 | -32 | -29 | -22 | -14 | -9 | -2 | -1 | -1 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | |
| PU-240 | NU | 584 | 0 | 0 | 0 | 5 | 7 | 1 | 4 | 8 | 14 | 17 | 17 | 25 | 121 | 119 | 118 | 84 | 34 | 10 | 0 | 0 | 0 | 0 | 0 | 0 | |
| PU-240 | FISSION | 403 | 0 | 0 | 0 | 4 | 5 | 1 | 3 | 6 | 10 | 12 | 12 | 18 | 84 | 82 | 79 | 56 | 24 | 7 | 0 | 0 | 0 | 0 | 0 | 0 | |
| PU-240 | ELASTIC | 9 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 1 | 1 | 2 | 2 | 2 | 1 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | | |
| PU-240 | INELASTIC | -10 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | -1 | 0 | 0 | -4 | -3 | -1 | 0 | 0 | 0 | 0 | 0 | 0 | |
| PU-240 | MU-AVE | -4 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | -1 | -1 | 0 | -1 | -1 | -1 | 0 | 0 | 0 | 0 | 0 | 0 | |
| PU-240 | (N,2N) | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | |
| PU-241 | CAPTURE | -62 | 0 | -1 | -3 | -6 | -8 | -2 | -5 | -6 | -7 | -6 | -5 | -4 | -1 | -1 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | |
| PU-241 | NU | 1151 | 3 | 9 | 30 | 61 | 100 | 36 | 72 | 94 | 123 | 138 | 148 | 124 | 94 | 41 | 40 | 25 | 10 | 3 | 0 | 0 | 0 | 0 | 0 | 0 | |
| PU-241 | FISSION | 824 | 1 | 6 | 20 | 42 | 72 | 26 | 52 | 70 | 91 | 101 | 107 | 88 | 66 | 29 | 27 | 17 | 7 | 2 | 0 | 0 | 0 | 0 | 0 | 0 | |
| PU-241 | ELASTIC | 1 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | |
| PU-241 | INELASTIC | -2 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | |
| PU-241 | MU-AVE | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | -1 | -1 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | |
| PU-241 | (N,2N) | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | |
| PU-242 | CAPTURE | -33 | 0 | -1 | -1 | -3 | -4 | -2 | -3 | -4 | -5 | -4 | -3 | -2 | -1 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | |
| PU-242 | NU | 66 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | |
| PU-242 | FISSION | 46 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | |
| PU-242 | ELASTIC | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | |
| PU-242 | INELASTIC | -2 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | |
| PU-242 | MU-AVE | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | |
| PU-242 | (N,2N) | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | |

表A-1(2/4) 実効倍増率に対する感度係数(168体炉心 keff rzcsl)

| 核種 | reaction | 群数 | | | | | | | | | | | | | | | | (1E-4△k/kk' / △σ/σ) | | |
|--------|----------|-------|----|----|----|----|-----|----|-----|-----|-----|-----|-----|-----|-----|-----|-----|---------------------|-----|----|
| | | total | 18 | 17 | 16 | 15 | 14 | 13 | 12 | 11 | 10 | 9 | 8 | 7 | 6 | 5 | 4 | 3 | 2 | 1 |
| AM-241 | CAPTURE | -64 | 0 | -1 | -3 | -7 | -9 | -3 | -5 | -6 | -8 | -3 | -7 | -4 | -2 | -1 | 0 | 0 | 0 | 0 |
| AM-241 | NU | 43 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 1 | 4 | 11 | 13 | 9 | 4 | 1 |
| AM-241 | FISSION | 31 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 1 | 3 | 8 | 9 | 6 | 3 | 1 |
| AM-241 | ELASTIC | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| AM-241 | INELASTC | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| AM-241 | MU-AVE | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| AM-241 | (N,2N) | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| B-10 | CAPTU | -3 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | -1 | -1 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| B-10 | ELASTI | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| B-10 | INELAST | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| B-10 | MU-AVE | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| B-10 | (N,2N) | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| B-11 | CAPTU | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| B-11 | ELASTI | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| B-11 | INELAST | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| B-11 | MU-AVE | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| B-11 | (N,2N) | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| C | CAPTU | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| C | ELASTI | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| C | INELAST | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| C | MU-AVE | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| C | (N,2N) | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| O | CAPTU | -17 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | -11 | -6 |
| O | ELASTI | 11 | 0 | 1 | 2 | 3 | 18 | 4 | 8 | 11 | 7 | -17 | -23 | 3 | -15 | 6 | -17 | 12 | 8 | 0 |
| O | INELAST | -1 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | -1 | -1 |
| O | MU-AVE | -41 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | -1 | -1 | 0 | 7 | -31 | -4 | -4 | -2 | -4 | -1 |
| O | (N,2N) | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| NA | CAPTU | -23 | 0 | 0 | 0 | -1 | -4 | -7 | -1 | 0 | -2 | -1 | -1 | -1 | 0 | 0 | 0 | 0 | -1 | -3 |
| NA | ELASTI | 211 | 0 | 0 | 1 | 2 | 15 | 17 | 17 | 14 | 14 | 12 | 9 | 24 | 54 | 13 | 4 | 10 | 5 | 0 |
| NA | INELAST | -77 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | -20 | -11 | -22 | -17 | -4 | -3 |
| NA | MU-AVE | -67 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | -1 | -1 | -2 | -5 | -15 | -11 | -14 | -12 | -5 | -1 |
| NA | (N,2N) | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| CR | CAPTU | -60 | 0 | 0 | -1 | -1 | -13 | -3 | -11 | -2 | -7 | -4 | -6 | -4 | -3 | -1 | -1 | -1 | -1 | -1 |
| CR | ELASTI | 130 | 0 | 0 | 0 | 0 | 0 | 1 | 1 | 8 | 4 | 11 | 33 | 16 | 24 | 11 | 9 | 6 | 2 | 0 |
| CR | INELAST | -37 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | -13 | -16 | -5 | -2 | -2 |
| CR | MU-AVE | -28 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | -1 | -1 | -2 | -2 | -6 | -9 | -5 |
| CR | (N,2N) | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| MN | CAPTU | -25 | 0 | 0 | -9 | -1 | -8 | -1 | -2 | -1 | -1 | -1 | -1 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| MN | ELASTI | 15 | 0 | 0 | -1 | 0 | 2 | 2 | 1 | 1 | 2 | 0 | 2 | 1 | 2 | 1 | 1 | 1 | 0 | 0 |
| MN | INELAST | -3 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | -1 | -1 | -1 | 0 | 0 |
| MN | MU-AVE | -2 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | -1 | -1 | 0 | 0 |
| MN | (N,2N) | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| FE | CAPTU | -214 | -1 | -1 | -2 | -3 | -56 | -1 | -10 | -13 | -26 | -20 | -24 | -19 | -15 | -4 | -3 | -6 | -4 | -4 |
| FE | ELASTI | 349 | -2 | -1 | 1 | 2 | 16 | 2 | 8 | 14 | 47 | 31 | 31 | 45 | 66 | 26 | 29 | 9 | 1 | 1 |
| FE | INELAST | -167 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | -2 | 0 | 0 | -1 | -26 | -65 | -43 | -21 | -9 | -9 |
| FE | MU-AVE | -100 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | -1 | -1 | -3 | -7 | -14 | -9 | -19 | -24 | -17 | -5 |
| FE | (N,2N) | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Ni | CAPTU | -117 | 0 | 0 | -1 | -1 | -2 | -2 | -3 | -18 | -11 | -10 | -8 | -5 | -3 | -5 | -16 | -16 | -6 | -6 |
| Ni | ELASTI | 127 | 0 | 0 | 0 | 1 | 5 | 1 | 4 | 17 | 13 | 14 | 14 | 21 | 17 | 7 | 6 | 2 | 0 | 0 |
| Ni | INELAST | -23 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | -8 | -11 | -3 | -1 | -1 |
| Ni | MU-AVE | -22 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | -1 | -1 | -3 | -2 | -4 | -4 | -3 | -3 | -1 | -1 |
| Ni | (N,2N) | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Mo | CAPTU | -57 | -1 | -1 | -3 | -6 | -7 | -3 | -6 | -6 | -7 | -5 | -4 | -3 | -3 | -1 | -1 | 0 | 0 | 0 |
| Mo | ELASTI | 12 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 1 | 1 | 2 | 3 | 3 | 1 | 1 | 0 | 0 | 0 |
| Mo | INELAST | -9 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | -1 | -1 | -3 | -3 | -1 | 0 | 0 |
| Mo | MU-AVE | -4 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | -1 | -1 | -1 | -1 | 0 | 0 | 0 | 0 |
| Mo | (N,2N) | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |

表A-1(3/4) 実効倍増率に対する感度係数(168体炉心 keff rzcals)

(1E-4 $\Delta k/kk' / \Delta \sigma/\sigma$)

| 項目 | level | 群数 | | | | | | | | | | | | | | | | | | |
|-----------------|-------|-------|----|----|----|----|----|----|----|----|----|----|-----|----|----|-----|------|-----|-----|----|
| | | total | 18 | 17 | 16 | 15 | 14 | 13 | 12 | 11 | 10 | 9 | 8 | 7 | 6 | 5 | 4 | 3 | 2 | 1 |
| U-238 INELASTIC | 1 | -11 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | -6 | -14 | -6 | 7 | 3 | 2 | 2 | 1 | 0 |
| U-238 | 2 | -1 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | -1 | 0 | 0 | -1 | 1 | 0 | 0 |
| U-238 | 3 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| U-238 | 4 | -15 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | -5 | -6 | -4 | 0 | 0 | 0 |
| U-238 | 5 | -9 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | -2 | -4 | -3 | 0 | 0 | 0 |
| U-238 | 6 | -1 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | -1 | 0 | 0 | 0 |
| U-238 | 7 | -4 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | -2 | -2 | 0 | 0 | 0 |
| U-238 | 8 | -7 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | -4 | -3 | 0 | 0 | 0 |
| U-238 | 9 | -6 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | -3 | -3 | 0 | 0 | 0 |
| U-238 | 10 | -8 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | -4 | -4 | 0 | 0 | 0 |
| U-238 | 11 | -4 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | -2 | -2 | 0 | 0 | 0 |
| U-238 | 12 | -5 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | -2 | -3 | 0 | 0 | 0 |
| U-238 | 13 | -6 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | -2 | -4 | 0 | 0 | 0 |
| U-238 | 14 | -3 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | -1 | -2 | 0 | 0 | 0 |
| U-238 | 15 | -4 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | -1 | -3 | 0 | 0 | 0 |
| U-238 | 16 | -8 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | -2 | -5 | -1 | 0 | 0 |
| U-238 | 17 | -4 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | -1 | -3 | 0 | 0 | 0 |
| U-238 | 18 | -3 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | -1 | -2 | 0 | 0 | 0 |
| U-238 | 19 | -3 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | -1 | -2 | 0 | 0 | 0 |
| U-238 | 20 | -4 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | -1 | -3 | 0 | 0 | 0 |
| U-238 | 21 | -2 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | -2 | 0 | 0 | 0 |
| U-238 | 22 | -3 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | -1 | -2 | 0 | 0 | 0 |
| U-238 | 23 | -4 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | -1 | -3 | 0 | 0 | 0 |
| U-238 | 24 | -1 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | -1 | 0 | 0 | 0 |
| U-238 | 25 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| U-238 | 26 | -3 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | -1 | -2 | 0 | 0 | 0 |
| U-238 | 27 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| U-238 | 28 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| U-238 | 29 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| U-238 | 30 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| U-238 | 31 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| U-238 | 32 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| U-238 | 33 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| U-238 | 34 | -163 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | -45 | -88 | -25 | -5 | -5 |
| | total | -282 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | -6 | -14 | -7 | 0 | -37 | -103 | -86 | -24 | -5 |

表A-1(4/4) 実効倍増率に対する感度係数(168体炉心 keff rzcalf)

(1E-4Δk/kk' / Δσ/σ)

| 項目 | サペイ | 群数 | | | | | | | | | | | | | | | | | | | | | | | |
|------------------|-------|-------|----|----|----|----|----|----|----|----|-----|-----|-----|------|------|------|-----|-----|-----|----|--|--|--|--|--|
| | | total | 18 | 17 | 16 | 15 | 14 | 13 | 12 | 11 | 10 | 9 | 8 | 7 | 6 | 5 | 4 | 3 | 2 | 1 | | | | | |
| FISSION SPECTRUM | -1 | 34 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | -1 | -5 | -13 | -33 | -82 | -172 | -145 | 88 | 232 | 111 | 54 | | | | | |
| FISSION | -0.9 | 28 | 0 | 0 | 0 | 0 | 0 | 0 | -1 | -5 | -13 | -33 | -82 | -170 | -142 | 85 | 226 | 109 | 54 | | | | | | |
| FISSION | -0.8 | 26 | 0 | 0 | 0 | 0 | 0 | 0 | -1 | -5 | -13 | -33 | -81 | -167 | -139 | 83 | 220 | 108 | 54 | | | | | | |
| FISSION | -0.7 | 21 | 0 | 0 | 0 | 0 | 0 | 0 | -1 | -5 | -13 | -33 | -81 | -164 | -136 | 80 | 214 | 106 | 54 | | | | | | |
| FISSION | -0.6 | 16 | 0 | 0 | 0 | 0 | 0 | 0 | -1 | -5 | -13 | -33 | -81 | -162 | -134 | 78 | 208 | 105 | 54 | | | | | | |
| FISSION | -0.5 | 15 | 0 | 0 | 0 | 0 | 0 | 0 | -1 | -5 | -13 | -33 | -80 | -159 | -131 | 76 | 203 | 104 | 54 | | | | | | |
| FISSION | -0.4 | 10 | 0 | 0 | 0 | 0 | 0 | 0 | -1 | -5 | -13 | -33 | -80 | -157 | -129 | 74 | 198 | 102 | 54 | | | | | | |
| FISSION | -0.3 | 8 | 0 | 0 | 0 | 0 | 0 | 0 | -1 | -5 | -13 | -33 | -79 | -155 | -126 | 72 | 194 | 101 | 53 | | | | | | |
| FISSION | -0.2 | 5 | 0 | 0 | 0 | 0 | 0 | 0 | -1 | -5 | -13 | -33 | -79 | -152 | -124 | 70 | 189 | 100 | 53 | | | | | | |
| FISSION | -0.1 | 4 | 0 | 0 | 0 | 0 | 0 | 0 | -1 | -5 | -13 | -33 | -78 | -150 | -122 | 69 | 185 | 99 | 53 | | | | | | |
| FISSION | -0.05 | 2 | 0 | 0 | 0 | 0 | 0 | 0 | -1 | -5 | -13 | -33 | -78 | -149 | -121 | 68 | 183 | 98 | 53 | | | | | | |
| FISSION | 0.05 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | -1 | -5 | -13 | -32 | -78 | -147 | -119 | 66 | 179 | 97 | 53 | | | | | | |
| FISSION | 0.1 | -1 | 0 | 0 | 0 | 0 | 0 | 0 | -1 | -5 | -13 | -32 | -78 | -146 | -118 | 66 | 177 | 96 | 53 | | | | | | |
| FISSION | 0.2 | -3 | 0 | 0 | 0 | 0 | 0 | 0 | -1 | -5 | -13 | -32 | -77 | -144 | -116 | 64 | 173 | 95 | 53 | | | | | | |
| FISSION | 0.3 | -6 | 0 | 0 | 0 | 0 | 0 | 0 | -1 | -5 | -13 | -32 | -77 | -142 | -114 | 63 | 169 | 94 | 52 | | | | | | |
| FISSION | 0.4 | -7 | 0 | 0 | 0 | 0 | 0 | 0 | -1 | -5 | -13 | -32 | -76 | -140 | -112 | 61 | 166 | 93 | 52 | | | | | | |
| FISSION | 0.5 | -8 | 0 | 0 | 0 | 0 | 0 | 0 | -1 | -5 | -13 | -32 | -76 | -138 | -110 | 60 | 163 | 92 | 52 | | | | | | |
| FISSION | 0.6 | -11 | 0 | 0 | 0 | 0 | 0 | 0 | -1 | -5 | -13 | -32 | -75 | -137 | -109 | 59 | 159 | 91 | 52 | | | | | | |
| FISSION | 0.7 | -12 | 0 | 0 | 0 | 0 | 0 | 0 | -1 | -5 | -13 | -32 | -75 | -135 | -107 | 58 | 156 | 90 | 52 | | | | | | |
| FISSION | 0.8 | -14 | 0 | 0 | 0 | 0 | 0 | 0 | -1 | -5 | -13 | -32 | -75 | -133 | -105 | 56 | 153 | 89 | 52 | | | | | | |
| FISSION | 0.9 | -16 | 0 | 0 | 0 | 0 | 0 | 0 | -1 | -5 | -13 | -32 | -74 | -132 | -104 | 55 | 150 | 88 | 52 | | | | | | |
| FISSION | 1 | -16 | 0 | 0 | 0 | 0 | 0 | 0 | -1 | -5 | -13 | -32 | -74 | -130 | -102 | 54 | 148 | 87 | 52 | | | | | | |

表A-2(1/4) 実効倍増率に対する感度係数(198体炉心 keff rzcal)

(1E-4Δk/kk' / Δσ/σ)

| 核種 | reaction | 群数 | | | | | | | | | | | | | | | | | | |
|--------|----------|-------|----|-----|-----|------|------|-----|------|------|------|------|------|------|------|-----|------|-----|-----|----|
| | | total | 18 | 17 | 16 | 15 | 14 | 13 | 12 | 11 | 10 | 9 | 8 | 7 | 6 | 5 | 4 | 3 | 2 | 1 |
| U-235 | CAPTURE | -8 | 0 | 0 | 0 | -1 | -1 | 0 | -1 | -1 | -1 | -1 | -1 | -1 | 0 | 0 | 0 | 0 | 0 | 0 |
| U-235 | NU | 94 | 1 | 1 | 3 | 6 | 9 | 3 | 6 | 8 | 10 | 11 | 11 | 9 | 7 | 3 | 3 | 2 | 1 | 0 |
| U-235 | FISSION | 61 | 1 | 1 | 2 | 4 | 6 | 2 | 4 | 5 | 7 | 7 | 7 | 6 | 4 | 2 | 2 | 1 | 0 | 0 |
| U-235 | ELASTIC | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| U-235 | INELASTC | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| U-235 | MU-AVE | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| U-235 | (N,2N) | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| U-238 | CAPTURE | -1925 | -5 | -17 | -40 | -129 | -186 | -84 | -171 | -238 | -291 | -253 | -185 | -139 | -117 | -46 | -18 | -5 | -1 | 0 |
| U-238 | NU | 1043 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 3 | 34 | 417 | 361 | 164 | 64 |
| U-238 | FISSION | 644 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 2 | 22 | 254 | 218 | 106 | 42 |
| U-238 | ELASTIC | 262 | 0 | -1 | 0 | 0 | 4 | 1 | 4 | 10 | 22 | 40 | 53 | 50 | 45 | 13 | 11 | 7 | 2 | 1 |
| U-238 | INELASTC | -307 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | -8 | -17 | -9 | -1 | -41 | -109 | -94 | -23 | -5 |
| U-238 | MU-AVE | -142 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | -1 | -3 | -10 | -19 | -31 | -14 | -21 | -25 | -14 | -4 |
| U-238 | (N,2N) | 1 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 1 |
| Pu-238 | CAPTURE | -14 | 0 | 0 | -1 | -2 | -2 | -1 | -1 | -1 | -2 | -2 | -1 | -1 | 0 | 0 | 0 | 0 | 0 | 0 |
| Pu-238 | NU | 86 | 0 | 0 | 1 | 2 | 2 | 1 | 3 | 4 | 6 | 6 | 8 | 11 | 16 | 9 | 8 | 6 | 2 | 1 |
| Pu-238 | FISSION | 59 | 0 | 0 | 1 | 1 | 2 | 1 | 2 | 3 | 4 | 4 | 5 | 8 | 11 | 6 | 5 | 4 | 2 | 0 |
| Pu-238 | ELASTIC | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Pu-238 | INELASTC | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Pu-238 | MU-AVE | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Pu-238 | (N,2N) | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| PU-239 | CAPTURE | -559 | -2 | -8 | -31 | -66 | -93 | -36 | -59 | -57 | -57 | -50 | -45 | -32 | -16 | -4 | -2 | -1 | 0 | 0 |
| PU-239 | NU | 6960 | 11 | 36 | 106 | 276 | 412 | 144 | 301 | 433 | 635 | 802 | 923 | 900 | 836 | 386 | 376 | 254 | 101 | 28 |
| PU-239 | FISSION | 4927 | 6 | 23 | 71 | 191 | 296 | 104 | 220 | 319 | 467 | 583 | 658 | 632 | 580 | 266 | 251 | 170 | 70 | 20 |
| PU-239 | ELASTIC | 20 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 1 | 2 | 3 | 4 | 4 | 3 | 1 | 1 | 0 | 0 | 0 |
| PU-239 | INELASTC | -22 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 1 | 0 | 0 | -1 | -1 | -3 | -3 | -7 | -6 | -2 | 0 |
| PU-239 | MU-AVE | -14 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | -1 | -2 | -3 | -1 | -2 | -3 | -2 | -2 | 0 |
| PU-239 | (N,2N) | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| PU-240 | CAPTURE | -243 | -1 | -5 | -11 | -23 | -31 | -11 | -20 | -26 | -33 | -30 | -22 | -14 | -10 | -3 | -2 | -1 | 0 | 0 |
| PU-240 | NU | 587 | 0 | 0 | 0 | 5 | 7 | 1 | 4 | 8 | 14 | 17 | 17 | 25 | 122 | 120 | 118 | 85 | 34 | 10 |
| PU-240 | FISSION | 400 | 0 | 0 | 0 | 3 | 5 | 1 | 3 | 6 | 10 | 12 | 12 | 18 | 84 | 82 | 78 | 56 | 23 | 7 |
| PU-240 | ELASTIC | 10 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 1 | 1 | 2 | 2 | 2 | 2 | 0 | 0 | 0 | 0 | 0 |
| PU-240 | INELASTC | -11 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | -1 | 0 | -1 | -1 | -4 | -3 | -1 | 0 |
| PU-240 | MU-AVE | -4 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | -1 | 0 | -1 | -1 | 0 | 0 |
| PU-240 | (N,2N) | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| PU-241 | CAPTURE | -58 | 0 | -1 | -2 | -5 | -7 | -2 | -5 | -5 | -7 | -7 | -6 | -5 | -4 | -1 | -1 | 0 | 0 | 0 |
| PU-241 | NU | 1120 | 2 | 7 | 26 | 55 | 95 | 35 | 70 | 93 | 121 | 136 | 146 | 123 | 93 | 41 | 39 | 25 | 10 | 3 |
| PU-241 | FISSION | 799 | 1 | 4 | 17 | 38 | 68 | 25 | 51 | 68 | 89 | 100 | 105 | 87 | 65 | 28 | 27 | 17 | 7 | 2 |
| PU-241 | ELASTIC | 1 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 1 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| PU-241 | INELASTC | -2 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | -1 | -1 | 0 | 0 |
| PU-241 | MU-AVE | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| PU-241 | (N,2N) | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| PU-242 | CAPTURE | -32 | 0 | 0 | -1 | -3 | -4 | -2 | -3 | -4 | -5 | -4 | -3 | -2 | -1 | 0 | 0 | 0 | 0 | 0 |
| PU-242 | NU | 66 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 1 | 2 | 13 | 18 | 16 | 11 | 4 | 1 |
| PU-242 | FISSION | 46 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 1 | 2 | 9 | 12 | 11 | 7 | 3 |
| PU-242 | ELASTIC | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| PU-242 | INELASTC | -2 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | -1 | -1 | 0 | 0 |
| PU-242 | MU-AVE | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| PU-242 | (N,2N) | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |

表A-2(2/4) 実効倍増率に対する感度係数(198体炉心 keff rzcsl)

| 核種 | reaction | 群数 | | | | | | | | | | | | | | | | (1E-4Δk/k' / Δσ/σ) | | | | | | | | | | | |
|--------|----------|-------|----|----|----|----|-----|----|-----|-----|-----|-----|-----|-----|-----|-----|-----|--------------------|-----|-----|--|--|--|--|--|--|--|--|--|
| | | total | 18 | 17 | 16 | 15 | 14 | 13 | 12 | 11 | 10 | 9 | 8 | 7 | 6 | 5 | 4 | 3 | 2 | 1 | | | | | | | | | |
| AM-241 | CAPTURE | -64 | 0 | -1 | -3 | -6 | -9 | -3 | -5 | -6 | -8 | -8 | -7 | -4 | -3 | -1 | 0 | 0 | 0 | 0 | | | | | | | | | |
| AM-241 | NU | 43 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 1 | 4 | 11 | 13 | 9 | 4 | 1 | | | | | | | | | |
| AM-241 | FISSION | 31 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 1 | 3 | 8 | 9 | 6 | 3 | 1 | | | | | | | | | |
| AM-241 | ELASTIC | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | | | | | | | | | |
| AM-241 | INELASTC | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | | | | | | | | | |
| AM-241 | MU-AVE | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | | | | | | | | | |
| AM-241 | (N,2N) | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | | | | | | | | | |
| B-10 | CAPTU | -18 | 0 | 0 | 0 | -1 | -1 | 0 | -1 | -2 | -3 | -4 | -3 | -2 | -1 | 0 | 0 | 0 | 0 | 0 | | | | | | | | | |
| B-10 | ELASTI | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | | | | | | | | | |
| B-10 | INELAST | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | | | | | | | | | |
| B-10 | MU-AVE | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | | | | | | | | | |
| B-10 | (N,2N) | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | | | | | | | | | |
| B-11 | CAPTU | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | | | | | | | | | |
| B-11 | ELASTI | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | | | | | | | | | |
| B-11 | INELAST | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | | | | | | | | | |
| B-11 | MU-AVE | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | | | | | | | | | |
| B-11 | (N,2N) | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | | | | | | | | | |
| C | CAPTU | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | | | | | | | | | |
| C | ELASTI | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | | | | | | | | | |
| C | INELAST | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | | | | | | | | | |
| C | MU-AVE | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | | | | | | | | | |
| C | (N,2N) | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | | | | | | | | | |
| O | CAPTU | -18 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | | | | | | | | | |
| O | ELASTI | -7 | 0 | 0 | 2 | 3 | 17 | 4 | 8 | 11 | 3 | -24 | -31 | -5 | -18 | 10 | -13 | 16 | 10 | -6 | | | | | | | | | |
| O | INELAST | -1 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | | | | | | | | | |
| O | MU-AVE | -48 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | | | | | | | | | |
| O | (N,2N) | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | | | | | | | | | |
| NA | CAPTU | -22 | 0 | 0 | 0 | -1 | -4 | -6 | -1 | 0 | -2 | -1 | -1 | -1 | -1 | 0 | 0 | 0 | 0 | 0 | | | | | | | | | |
| NA | ELASTI | 153 | 0 | 0 | 1 | 2 | 12 | 16 | 15 | 11 | 9 | 4 | 2 | 11 | 44 | 9 | 3 | 9 | 5 | 0 | | | | | | | | | |
| NA | INELAST | -75 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | -20 | -11 | -21 | -16 | -4 | | | | | | | | | |
| NA | MU-AVE | -59 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | -13 | -9 | -13 | -11 | -4 | | | | | | | | | |
| NA | (N,2N) | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | | | | | | | | | |
| CR | CAPTU | -51 | 0 | 0 | 0 | -1 | -12 | -2 | -10 | -1 | -6 | -3 | -6 | -3 | -2 | -1 | -1 | -1 | -1 | -1 | | | | | | | | | |
| CR | ELASTI | 94 | 0 | 0 | 0 | 0 | 1 | 1 | 7 | 3 | 3 | 8 | 25 | 9 | 17 | 7 | 6 | 5 | 2 | 0 | | | | | | | | | |
| CR | INELAST | -41 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | -1 | -14 | -17 | -6 | -3 | | | | | | | | | |
| CR | MU-AVE | -23 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | -1 | -2 | -5 | -7 | -4 | | | | | | | | | |
| CR | (N,2N) | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | | | | | | | | | |
| MN | CAPTU | -22 | 0 | 0 | -7 | -1 | -7 | -1 | -2 | -1 | -1 | -1 | -1 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | | | | | | | | | |
| MN | ELASTI | 10 | 0 | 0 | -1 | 0 | 2 | 2 | 0 | 1 | 2 | 0 | 1 | 1 | 1 | 1 | 0 | 0 | 0 | 0 | | | | | | | | | |
| MN | INELAST | -4 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | | | | | | | | | |
| MN | MU-AVE | -1 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | | | | | | | | | |
| MN | (N,2N) | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | | | | | | | | | |
| FE | CAPTU | -199 | 0 | -1 | -1 | -3 | -49 | -1 | -10 | -12 | -25 | -19 | -23 | -18 | -14 | -4 | -3 | -6 | -6 | -4 | | | | | | | | | |
| FE | ELASTI | 248 | -1 | -1 | 1 | 3 | 13 | 2 | 7 | 11 | 37 | 20 | 17 | 27 | 48 | 18 | 20 | 18 | 7 | 1 | | | | | | | | | |
| FE | INELAST | -181 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | -1 | -2 | 0 | 0 | -1 | -28 | -68 | -47 | -24 | -10 | | | | | | | | | |
| FE | MU-AVE | -80 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | -1 | -1 | -3 | -6 | -11 | -7 | -15 | -19 | -13 | -4 | | | | | | | | | |
| FE | (N,2N) | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | | | | | | | | | |
| Ni | CAPTU | -115 | 0 | 0 | 0 | -1 | -2 | -2 | -3 | -17 | -11 | -9 | -10 | -8 | -5 | -3 | -5 | -16 | -17 | -6 | | | | | | | | | |
| Ni | ELASTI | 102 | 0 | 0 | 0 | 1 | 5 | 1 | 4 | 15 | 9 | 11 | 10 | 16 | 14 | 6 | 5 | 4 | 1 | 0 | | | | | | | | | |
| Ni | INELAST | -23 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | -8 | -11 | -3 | | | | | | | | | |
| Ni | MU-AVE | -19 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | -1 | -2 | -3 | -2 | -4 | -3 | -1 | | | | | | | | | |
| Ni | (N,2N) | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | | | | | | | | | |
| Mo | CAPTU | -59 | -1 | -1 | -2 | -6 | -7 | -3 | -6 | -6 | -7 | -6 | -5 | -4 | -3 | -1 | -1 | 0 | 0 | 0 | | | | | | | | | |
| Mo | ELASTI | 11 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 1 | 1 | 2 | 2 | 3 | 1 | 1 | 0 | 0 | 0 | | | | | | | | | |
| Mo | INELAST | -10 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | -1 | -1 | -4 | -3 | -1 | | | | | | | | | |
| Mo | MU-AVE | -5 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | -1 | -1 | -1 | 0 | 0 | | | | | | | | | |
| Mo | (N,2N) | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | | | | | | | | | |

表A-2(3/4) 実効倍増率に対する感度係数(198体炉心 keff rzcal)

(1E-4 $\Delta k/kk' / \Delta \sigma/\sigma$)

| 項目 | level | 群数 | | | | | | | | | | | | | | | | | | |
|-----------------|-------|-------|----|----|----|----|----|----|----|----|----|----|-----|----|----|-----|-----|-----|----|---|
| | | total | 18 | 17 | 16 | 15 | 14 | 13 | 12 | 11 | 10 | 9 | 8 | 7 | 6 | 5 | 4 | 3 | 2 | 1 |
| U-238 INELASTIC | 1 | -14 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | -8 | -17 | -8 | 8 | 4 | 3 | 3 | 1 | 0 |
| U-238 | 2 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | -1 | 0 | 0 | 0 | 1 | 0 | 0 |
| U-238 | 3 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| U-238 | 4 | -17 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | -6 | -7 | -4 | 0 | 0 | 0 |
| U-238 | 5 | -9 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | -2 | -4 | -3 | 0 | 0 | 0 |
| U-238 | 6 | -1 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | -1 | 0 | 0 | 0 | 0 |
| U-238 | 7 | -4 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | -2 | 0 | 0 | 0 | 0 |
| U-238 | 8 | -8 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | -5 | -3 | 0 | 0 | 0 |
| U-238 | 9 | -7 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | -4 | -3 | 0 | 0 | 0 |
| U-238 | 10 | -8 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | -4 | -4 | 0 | 0 | 0 |
| U-238 | 11 | -4 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | -2 | -2 | 0 | 0 | 0 |
| U-238 | 12 | -5 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | -2 | -3 | 0 | 0 | 0 |
| U-238 | 13 | -6 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | -2 | -4 | 0 | 0 | 0 |
| U-238 | 14 | -3 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | -1 | -2 | 0 | 0 | 0 |
| U-238 | 15 | -4 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | -1 | -3 | 0 | 0 | 0 |
| U-238 | 16 | -8 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | -5 | -1 | 0 | 0 | 0 |
| U-238 | 17 | -4 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | -1 | -3 | 0 | 0 | 0 |
| U-238 | 18 | -4 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | -1 | -3 | 0 | 0 | 0 |
| U-238 | 19 | -3 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | -1 | -2 | 0 | 0 | 0 |
| U-238 | 20 | -4 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | -1 | -3 | 0 | 0 | 0 |
| U-238 | 21 | -3 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | -1 | -2 | 0 | 0 | 0 |
| U-238 | 22 | -3 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | -1 | -2 | 0 | 0 | 0 |
| U-238 | 23 | -4 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | -1 | -3 | 0 | 0 | 0 |
| U-238 | 24 | -1 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | -1 | -1 | 0 | 0 | 0 |
| U-238 | 25 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| U-238 | 26 | -3 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | -1 | -2 | 0 | 0 | 0 |
| U-238 | 27 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| U-238 | 28 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| U-238 | 29 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| U-238 | 30 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| U-238 | 31 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| U-238 | 32 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| U-238 | 33 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| U-238 | 34 | -174 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | -49 | -94 | -26 | -5 | |
| | total | -301 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |

表A-2(4/4) 実効倍増率に対する感度係数(198体炉心 keff rzcals)

(1E-4 $\Delta k/kk' / \Delta \sigma/\sigma$)

| 項目 | サベイ | 群数 | | | | | | | | | | | | | | | | | | |
|------------------|-------|-------|----|----|----|----|----|----|----|----|----|-----|-----|-----|------|------|----|-----|-----|----|
| | | total | 18 | 17 | 16 | 15 | 14 | 13 | 12 | 11 | 10 | 9 | 8 | 7 | 6 | 5 | 4 | 3 | 2 | |
| FISSION SPECTRUM | -1 | 33 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | -2 | -5 | -13 | -34 | -83 | -171 | -141 | 88 | 229 | 110 | 55 |
| FISSION | -0.9 | 31 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | -2 | -5 | -13 | -34 | -82 | -168 | -138 | 86 | 223 | 109 | 55 |
| FISSION | -0.8 | 23 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | -2 | -5 | -13 | -34 | -82 | -166 | -136 | 83 | 217 | 107 | 54 |
| FISSION | -0.7 | 20 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | -2 | -5 | -13 | -34 | -82 | -163 | -133 | 81 | 211 | 106 | 54 |
| FISSION | -0.6 | 17 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | -2 | -5 | -13 | -34 | -81 | -161 | -130 | 79 | 206 | 104 | 54 |
| FISSION | -0.5 | 14 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | -2 | -5 | -13 | -34 | -81 | -158 | -128 | 77 | 201 | 103 | 54 |
| FISSION | -0.4 | 11 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | -2 | -5 | -13 | -34 | -80 | -156 | -126 | 75 | 196 | 102 | 54 |
| FISSION | -0.3 | 9 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | -2 | -5 | -13 | -34 | -80 | -153 | -123 | 73 | 191 | 101 | 54 |
| FISSION | -0.2 | 5 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | -2 | -5 | -13 | -33 | -79 | -151 | -121 | 71 | 186 | 99 | 53 |
| FISSION | -0.1 | 2 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | -2 | -5 | -13 | -33 | -79 | -149 | -119 | 69 | 182 | 98 | 53 |
| FISSION | -0.05 | 2 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | -2 | -5 | -13 | -33 | -79 | -148 | -118 | 69 | 180 | 98 | 53 |
| FISSION | 0.05 | -1 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | -2 | -5 | -13 | -33 | -78 | -146 | -116 | 67 | 176 | 96 | 53 |
| FISSION | 0.1 | -2 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | -2 | -5 | -13 | -33 | -78 | -145 | -115 | 66 | 174 | 96 | 53 |
| FISSION | 0.2 | -3 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | -2 | -5 | -13 | -33 | -78 | -143 | -113 | 65 | 171 | 95 | 53 |
| FISSION | 0.3 | -5 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | -2 | -5 | -13 | -33 | -77 | -141 | -111 | 63 | 167 | 94 | 53 |
| FISSION | 0.4 | -6 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | -2 | -5 | -13 | -33 | -77 | -139 | -109 | 62 | 164 | 93 | 53 |
| FISSION | 0.5 | -10 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | -2 | -5 | -13 | -33 | -76 | -137 | -108 | 61 | 160 | 91 | 52 |
| FISSION | 0.6 | -13 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | -2 | -5 | -13 | -33 | -76 | -136 | -106 | 59 | 157 | 90 | 52 |
| FISSION | 0.7 | -14 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | -2 | -5 | -13 | -33 | -76 | -134 | -104 | 58 | 154 | 89 | 52 |
| FISSION | 0.8 | -15 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | -2 | -5 | -13 | -33 | -75 | -132 | -103 | 57 | 151 | 88 | 52 |
| FISSION | 0.9 | -16 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | -2 | -5 | -13 | -33 | -75 | -130 | -101 | 56 | 148 | 87 | 52 |
| FISSION | 1 | -16 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | -2 | -5 | -13 | -33 | -74 | -129 | -100 | 55 | 146 | 87 | 52 |

Appendix B

制御棒価値に対する感度係数

表B-1(1/4) 制御棒価値に対する感度係数 (168体炉心 中心C R 1E-3 RZcal)

(1E-4 Δk/kk' / Δσ/σ)

| 核種 | reaction | 群数 | | | | | | | | | | | | | | | | | | |
|--------|-----------|-------|-----|------|------|------|------|------|------|------|------|------|-------|-------|-------|------|------|------|------|------|
| | | total | 18 | 17 | 16 | 15 | 14 | 13 | 12 | 11 | 10 | 9 | 8 | 7 | 6 | 5 | 4 | 3 | 2 | 1 |
| U-235 | CAPTURE | -13 | 0 | -1 | -1 | -3 | -3 | 0 | -1 | -1 | -1 | -1 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| U-235 | NU | 18 | -1 | 3 | 9 | 18 | 17 | 3 | 4 | 3 | 1 | -3 | -7 | -9 | -8 | -4 | -4 | -3 | -1 | 0 |
| U-235 | FISSION | -17 | -1 | 2 | 5 | 11 | 10 | 1 | 1 | 0 | -3 | -7 | -9 | -9 | -8 | -4 | -3 | -2 | -1 | 0 |
| U-235 | ELASTIC | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| U-235 | INELASTIC | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| U-235 | (N,2N) | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| U-235 | MU-AVE | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| U-238 | CAPTURE | -2970 | -25 | -105 | -197 | -507 | -518 | -152 | -290 | -367 | -395 | -264 | -135 | -49 | -1 | 19 | 11 | 4 | 1 | 0 |
| U-238 | NU | -1666 | 0 | 0 | 0 | 1 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | -4 | -52 | -653 | -583 | -272 | -103 |
| U-238 | FISSION | -1395 | 0 | 0 | 0 | 1 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | -4 | -47 | -555 | -479 | -226 | -85 |
| U-238 | ELASTIC | -675 | -2 | -3 | -7 | -25 | -38 | -7 | -25 | -47 | -73 | -98 | -111 | -99 | -81 | -24 | -19 | -11 | -4 | -1 |
| U-238 | INELASTIC | 494 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | -30 | -38 | -16 | -11 | 82 | 230 | 206 | 61 | 10 |
| U-238 | (N,2N) | -2 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | -2 |
| U-238 | MU-AVE | 252 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 1 | 2 | 6 | 16 | 35 | 55 | 27 | 38 | 42 | 24 | 6 |
| PU-239 | CAPTURE | -663 | -14 | -45 | -124 | -195 | -165 | -29 | -45 | -38 | -29 | -11 | 2 | 12 | 11 | 4 | 2 | 1 | 0 | 0 |
| PU-239 | NU | -6226 | 72 | 198 | 397 | 692 | 510 | 34 | 23 | -103 | -361 | -784 | -1217 | -1491 | -1592 | -853 | -855 | -591 | -239 | -66 |
| PU-239 | FISSION | -6478 | 41 | 126 | 262 | 443 | 302 | 2 | -39 | -178 | -445 | -832 | -1204 | -1391 | -1415 | -724 | -699 | -477 | -196 | -54 |
| PU-239 | ELASTIC | -106 | 0 | 0 | -1 | -3 | -5 | -1 | -4 | -8 | -13 | -17 | -18 | -15 | -10 | -3 | -4 | -3 | -1 | 0 |
| PU-239 | INELASTIC | 33 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | -4 | -3 | -4 | -3 | -2 | 7 | 18 | 16 | 6 | 1 | 1 |
| PU-239 | (N,2N) | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| PU-239 | MU-AVE | 46 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 2 | 4 | 6 | 8 | 4 | 7 | 9 | 5 |
| PU-240 | CAPTURE | -269 | -10 | -28 | -44 | -71 | -59 | -9 | -17 | -19 | -19 | -9 | 0 | 4 | 6 | 3 | 2 | 1 | 0 | 0 |
| PU-240 | NU | -1104 | 0 | 0 | 1 | 13 | 9 | 0 | 1 | -1 | -15 | -21 | -41 | -227 | -259 | -262 | -193 | -79 | -23 | -23 |
| PU-240 | FISSION | -953 | 0 | 0 | 0 | 0 | 8 | 5 | 0 | 0 | -3 | -9 | -17 | -21 | -38 | -203 | -220 | -215 | -156 | -65 |
| PU-240 | ELASTIC | -49 | 0 | 0 | 0 | 0 | -2 | -3 | 0 | -2 | -4 | -6 | -8 | -7 | -5 | -1 | -1 | -1 | 0 | 0 |
| PU-240 | INELASTIC | 16 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | -2 | -2 | -1 | 0 | 3 | 9 | 7 | 2 | 0 |
| PU-240 | (N,2N) | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| PU-240 | MU-AVE | 14 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 1 | 1 | 2 | 3 | 1 | 2 | 2 | 2 | 0 |
| PU-241 | CAPTURE | -46 | -1 | -3 | -9 | -15 | -13 | -2 | -3 | -3 | -3 | -1 | 0 | 2 | 3 | 1 | 1 | 0 | 0 | 0 |
| PU-241 | NU | -701 | 9 | 38 | 96 | 137 | 114 | 7 | 3 | -25 | -73 | -139 | -200 | -209 | -183 | -93 | -92 | -60 | -24 | -7 |
| PU-241 | FISSION | -820 | 5 | 24 | 64 | 88 | 67 | 0 | -11 | -40 | -88 | -146 | -197 | -195 | -163 | -79 | -75 | -48 | -20 | -6 |
| PU-241 | ELASTIC | -12 | 0 | 0 | 0 | 0 | -1 | 0 | 0 | -1 | -1 | -2 | -2 | -1 | -1 | -1 | 0 | 0 | 0 | 0 |
| PU-241 | INELASTIC | 6 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 1 | 2 | 2 | 1 | 0 |
| PU-241 | (N,2N) | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| PU-241 | MU-AVE | 6 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 1 | 1 | 1 | 1 | 1 | 1 | 0 |
| PU-242 | CAPTURE | -36 | -1 | -2 | -5 | -9 | -8 | -2 | -3 | -3 | -3 | -1 | 0 | 0 | 1 | 0 | 0 | 0 | 0 | 0 |
| PU-242 | NU | -141 | 0 | 0 | 0 | 1 | 0 | 0 | 0 | 0 | 0 | 0 | -1 | -4 | -24 | -39 | -36 | -25 | -10 | -3 |
| PU-242 | FISSION | -119 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | -1 | -3 | -21 | -33 | -30 | -20 | -8 | -3 |
| PU-242 | ELASTIC | -6 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | -1 | -1 | -1 | -1 | -1 | 0 | 0 | 0 | 0 | 0 |
| PU-242 | INELASTIC | 3 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 1 | 1 | 0 | 0 |
| PU-242 | (N,2N) | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| PU-242 | MU-AVE | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| AM-241 | CAPTURE | -105 | -1 | -6 | -13 | -24 | -22 | -4 | -7 | -8 | -9 | -6 | -4 | -1 | 0 | 0 | 0 | 0 | 0 | 0 |
| AM-241 | NU | -72 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | -1 | -6 | -18 | -22 | -16 | -7 | -2 | -2 |
| AM-241 | FISSION | -64 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | -1 | -6 | -16 | -19 | -14 | -6 | -2 |
| AM-241 | ELASTIC | -2 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | -1 | -1 | 0 | 0 | 0 | 0 | 0 | 0 |
| AM-241 | INELASTIC | 2 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | -1 | -1 | 0 | 0 | 1 | 1 | 0 | 0 |
| AM-241 | (N,2N) | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| AM-241 | MU-AVE | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |

表B-1(2/4) 制御棒価値に対する感度係数 (168体炉心 中心CR 1E-3 RZcal)

| 核種 | reaction | 群数 | | | | | | | | | | | | | | | | | | (1E-4 Δk/kk' / Δσ/σ) | | | | | | | |
|------|----------|-------|----|-----|-----|-----|------|-----|-----|------|------|------|------|------|-----|-----|-----|-----|-----|----------------------|----|---|--|--|--|--|--|
| | | total | 18 | 17 | 16 | 15 | 14 | 13 | 12 | 11 | 10 | 9 | 8 | 7 | 6 | 5 | 4 | 3 | 2 | 1 | | | | | | | |
| B-10 | CAPTU | 5658 | -1 | 0 | 9 | 76 | 185 | 86 | 279 | 572 | 880 | 1086 | 1098 | 739 | 400 | 73 | 107 | 45 | 20 | 4 | | | | | | | |
| | ELASTI | 120 | 0 | 0 | -1 | -2 | -3 | -1 | 2 | 11 | 21 | 31 | 32 | 32 | 16 | -4 | -3 | -7 | -4 | 0 | | | | | | | |
| | INELAST | 5 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 2 | 2 | 1 | 0 | 0 | | | | | | |
| | MU-AVE | 28 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 1 | 1 | 2 | 3 | 7 | 3 | 4 | 3 | 3 | 1 | | | | | | |
| | (N,2N) | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | | | | | | |
| B-11 | CAPTU | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | | | | | | |
| | ELASTI | 225 | 0 | -1 | -2 | -6 | -11 | -3 | 6 | 30 | 55 | 73 | 61 | 41 | 27 | -16 | -8 | -12 | -8 | -1 | | | | | | | |
| | INELAST | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | | | | | | | |
| | MU-AVE | 44 | 0 | 0 | 0 | 0 | 1 | 0 | 0 | 1 | 2 | 3 | 4 | 3 | 13 | 4 | 5 | 5 | 5 | 2 | 1 | | | | | | |
| | (N,2N) | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | | | | | | |
| C | CAPTU | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | | | | | | |
| | ELASTI | 69 | 0 | 0 | -1 | -3 | -5 | -1 | 2 | 11 | 20 | 27 | 22 | 15 | 2 | -5 | -4 | -7 | -4 | 0 | 0 | | | | | | |
| | INELAST | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | | | | | | |
| | MU-AVE | 16 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 1 | 1 | 2 | 3 | 4 | 2 | 2 | 0 | 0 | 1 | | | | | | |
| | (N,2N) | 2 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | | | | | | |
| O | CAPTU | 17 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | | | | | | |
| | ELASTI | -972 | -1 | 2 | 5 | -26 | -6 | 3 | -38 | -125 | -196 | -244 | -227 | -148 | 25 | 21 | 29 | -29 | -17 | 0 | | | | | | | |
| | INELAST | 3 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | | | | | | |
| | MU-AVE | 95 | 0 | 0 | 0 | 0 | 1 | 1 | 0 | 1 | 1 | 2 | -1 | -16 | 68 | 9 | 9 | 6 | 10 | 2 | | | | | | | |
| | (N,2N) | 172 | 0 | 0 | 0 | -1 | 0 | 0 | 0 | 1 | 1 | 2 | -1 | -23 | 117 | 18 | 19 | 12 | 23 | 4 | | | | | | | |
| NA | CAPTU | -35 | 0 | -1 | -2 | -4 | -12 | -14 | -2 | 0 | -2 | -1 | -1 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 1 | 3 | | | | | |
| | ELASTI | -1017 | 0 | 0 | 2 | -27 | -52 | -20 | -54 | -98 | -142 | -184 | -172 | -109 | -85 | 0 | -25 | -33 | -16 | -2 | | | | | | | |
| | INELAST | 171 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 32 | 49 | 40 | 36 | 8 | 6 | | | | | | | |
| | MU-AVE | 171 | 0 | 0 | 0 | 1 | 2 | 2 | 1 | 1 | 2 | 3 | 5 | 9 | 28 | 24 | 39 | 36 | 15 | 3 | | | | | | | |
| | (N,2N) | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | | | | | | | |
| CR | CAPTU | -110 | 0 | -1 | -2 | -5 | -46 | -6 | -25 | -3 | -12 | -5 | -6 | -2 | 0 | 0 | 0 | 0 | 1 | 1 | 1 | | | | | | |
| | ELASTI | -279 | 0 | -1 | -1 | -7 | -10 | -6 | -47 | -27 | -19 | -20 | -42 | -15 | -26 | -13 | -22 | -16 | -6 | -1 | | | | | | | |
| | INELAST | 86 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 3 | 31 | 35 | 12 | 5 | | | | | | | |
| | MU-AVE | 65 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 1 | 1 | 3 | 4 | 14 | 23 | 14 | 4 | | | | | |
| | (N,2N) | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | | | | | | |
| FE | CAPTU | -357 | 0 | -4 | -10 | -14 | -185 | -3 | -24 | -27 | -46 | -25 | -23 | -10 | -2 | 2 | 2 | 4 | 5 | 3 | | | | | | | |
| | ELASTI | -1011 | -5 | -10 | -12 | -88 | -81 | -5 | -68 | -88 | -151 | -113 | -105 | -47 | -60 | -28 | -65 | -60 | -22 | -3 | | | | | | | |
| | INELAST | 348 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | -19 | -7 | -1 | 0 | 1 | 74 | 142 | 92 | 50 | 16 | | | | | | | |
| | MU-AVE | 190 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 1 | 1 | 2 | 7 | 20 | 15 | 37 | 56 | 38 | 13 | | | | | | |
| | (N,2N) | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | | | | | | | |

表B-1(3/4) 制御棒価値に対する感度係数 (168体炉心 中心CR 1E-3 RZcal)

(1E-4 $\Delta k/k' / \Delta \sigma/\sigma$)

| 項目 | level | 群数 | | | | | | | | | | | | | | | | | | |
|-----------------|-------|-------|----|----|----|----|----|----|----|----|----|-----|-----|-----|-----|-----|----|-----|-----|----|
| | | total | 18 | 17 | 16 | 15 | 14 | 13 | 12 | 11 | 10 | 9 | 8 | 7 | 6 | 5 | 4 | 3 | 2 | 1 |
| U-238 INELASTIC | 1 | -115 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | -30 | -38 | -15 | -13 | -5 | -6 | -5 | -2 | -1 |
| U-238 | 2 | 1 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | -1 | 1 | 2 | 1 | -1 | -1 | 0 |
| U-238 | 3 | 1 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 1 | 0 | 0 | 0 |
| U-238 | 4 | 28 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 2 | 18 | 8 | 0 | 0 | 0 |
| U-238 | 5 | 17 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 10 | 7 | 0 | 0 | 0 |
| U-238 | 6 | 3 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 1 | 2 | 0 | 0 | 0 |
| U-238 | 7 | 8 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 4 | 4 | 0 | 0 | 0 |
| U-238 | 8 | 15 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 8 | 7 | 0 | 0 | 0 |
| U-238 | 9 | 14 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 7 | 7 | 0 | 0 | 0 |
| U-238 | 10 | 19 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 8 | 10 | 1 | 0 | 0 |
| U-238 | 11 | 9 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 3 | 5 | 1 | 0 | 0 |
| U-238 | 12 | 10 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 4 | 6 | 0 | 0 | 0 |
| U-238 | 13 | 15 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 4 | 10 | 1 | 0 | 0 |
| U-238 | 14 | 6 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 1 | 5 | 0 | 0 | 0 |
| U-238 | 15 | 12 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 3 | 8 | 1 | 0 | 0 |
| U-238 | 16 | 16 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 4 | 11 | 1 | 0 | 0 |
| U-238 | 17 | 10 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 2 | 7 | 1 | 0 | 0 |
| U-238 | 18 | 8 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 2 | 6 | 0 | 0 | 0 |
| U-238 | 19 | 7 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 1 | 5 | 1 | 0 | 0 |
| U-238 | 20 | 8 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 2 | 6 | 0 | 0 | 0 |
| U-238 | 21 | 7 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 1 | 5 | 1 | 0 | 0 |
| U-238 | 22 | 7 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 1 | 5 | 1 | 0 | 0 |
| U-238 | 23 | 9 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 1 | 7 | 1 | 0 | 0 |
| U-238 | 24 | 3 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 3 | 0 | 0 | 0 |
| U-238 | 25 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| U-238 | 26 | 5 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 5 | 0 | 0 | 0 |
| U-238 | 27 | 1 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 1 | 0 | 0 | 0 |
| U-238 | 28 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| U-238 | 29 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| U-238 | 30 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| U-238 | 31 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| U-238 | 32 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| U-238 | 33 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| U-238 | 34 | 373 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | -30 | -38 | -16 | -10 | 82 | 232 | 205 | 62 |
| | total | 497 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | -30 | -38 | -16 | -10 | 82 | 232 | 205 | 10 |

表B-1(4/4) 制御棒価値に対する感度係数 (168 体炉心 中心CR 1E-3 RZcal)

(1E-4 $\Delta k/kk' / \Delta \sigma/\sigma$)

| 項目 | サペイ | 群数 | | | | | | | | | | | | | | | 4 | 3 | 2 | 1 |
|------------------|-------|-------|----|----|----|----|----|----|----|----|----|----|----|-----|-----|-----|------|------|------|------|
| | | total | 18 | 17 | 16 | 15 | 14 | 13 | 12 | 11 | 10 | 9 | 8 | 7 | 6 | 5 | | | | |
| FISSION SPECTRUM | -1 | -76 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 1 | 5 | 21 | 73 | 214 | 463 | 338 | -198 | -571 | -293 | -129 |
| FISSION | -0.9 | -66 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 1 | 5 | 21 | 73 | 213 | 455 | 331 | -192 | -555 | -289 | -129 |
| FISSION | -0.8 | -56 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 1 | 5 | 21 | 72 | 212 | 448 | 324 | -186 | -540 | -285 | -128 |
| FISSION | -0.7 | -47 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 1 | 5 | 21 | 72 | 211 | 441 | 318 | -181 | -526 | -281 | -128 |
| FISSION | -0.6 | -38 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 1 | 5 | 21 | 72 | 209 | 434 | 312 | -176 | -512 | -277 | -127 |
| FISSION | -0.5 | -32 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 1 | 5 | 21 | 72 | 208 | 428 | 306 | -172 | -500 | -274 | -127 |
| FISSION | -0.4 | -24 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 1 | 5 | 21 | 72 | 207 | 421 | 300 | -167 | -487 | -270 | -127 |
| FISSION | -0.3 | -17 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 1 | 5 | 21 | 72 | 206 | 415 | 295 | -163 | -476 | -267 | -126 |
| FISSION | -0.2 | -12 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 1 | 5 | 21 | 72 | 205 | 409 | 289 | -159 | -465 | -264 | -126 |
| FISSION | -0.1 | -7 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 1 | 5 | 21 | 71 | 204 | 403 | 284 | -155 | -454 | -261 | -126 |
| FISSION | -0.05 | -4 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 1 | 5 | 21 | 71 | 203 | 400 | 282 | -153 | -449 | -259 | -126 |
| FISSION | 0.05 | 2 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 1 | 5 | 21 | 71 | 202 | 395 | 277 | -150 | -439 | -256 | -125 |
| FISSION | 0.1 | 5 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 1 | 5 | 21 | 71 | 202 | 392 | 274 | -148 | -434 | -254 | -125 |
| FISSION | 0.2 | 10 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 1 | 5 | 21 | 71 | 201 | 387 | 270 | -145 | -425 | -251 | -125 |
| FISSION | 0.3 | 14 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 1 | 5 | 21 | 71 | 199 | 381 | 265 | -141 | -416 | -248 | -124 |
| FISSION | 0.4 | 17 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 1 | 5 | 21 | 71 | 198 | 376 | 261 | -138 | -408 | -246 | -124 |
| FISSION | 0.5 | 21 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 1 | 5 | 21 | 71 | 197 | 371 | 257 | -136 | -399 | -243 | -124 |
| FISSION | 0.6 | 26 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 1 | 5 | 21 | 71 | 196 | 367 | 253 | -133 | -392 | -240 | -123 |
| FISSION | 0.7 | 29 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 1 | 5 | 21 | 70 | 195 | 362 | 249 | -130 | -384 | -237 | -123 |
| FISSION | 0.8 | 31 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 1 | 5 | 21 | 70 | 194 | 357 | 245 | -127 | -377 | -235 | -123 |
| FISSION | 0.9 | 36 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 1 | 5 | 21 | 70 | 193 | 353 | 242 | -125 | -370 | -232 | -122 |
| FISSION | 1 | 38 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 1 | 5 | 21 | 70 | 192 | 349 | 238 | -123 | -363 | -230 | -122 |

表B-2(1/4) 制御棒価値に対する感度係数(198体炉心 中心CR 1E-3 RZcal)

(1E-4 Δk/kk' / Δσ/σ)

| 核種 | reaction | 群数 | | | | | | | | | | | | | | | | | | | |
|--------|----------|-------|----|-----|------|------|------|-----|------|------|------|------|-------|-------|-------|------|------|------|------|------|------|
| | | total | 18 | 17 | 16 | 15 | 14 | 13 | 12 | 11 | 10 | 9 | 8 | 7 | 6 | 5 | 4 | 3 | 2 | 1 | |
| U-235 | CAPTURE | -7 | 0 | 0 | -1 | -1 | -2 | 0 | -1 | -1 | -1 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | |
| U-235 | NU | -82 | -4 | -2 | -1 | 3 | 2 | -2 | -3 | -5 | -8 | -11 | -13 | -13 | -11 | -5 | -5 | -3 | -1 | 0 | |
| U-235 | FISSION | -101 | -4 | -3 | -3 | -1 | -2 | -3 | -5 | -7 | -10 | -13 | -14 | -13 | -10 | -5 | -4 | -3 | -1 | 0 | |
| U-235 | ELASTIC | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | |
| U-235 | INELASTC | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | |
| U-235 | (N,2N) | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | |
| U-235 | MU-AVE | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | |
| U-238 | CAPTURE | -1617 | 5 | -31 | -101 | -322 | -349 | -82 | -179 | -232 | -227 | -128 | -54 | 3 | 35 | 27 | 12 | 5 | 1 | 0 | |
| U-238 | NU | -1871 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | -1 | -5 | -61 | -721 | -660 | -306 | -117 |
| U-238 | FISSION | -1563 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | -1 | -5 | -54 | -610 | -541 | -255 | -97 |
| U-238 | ELASTIC | -853 | 5 | 13 | 13 | 21 | 9 | -6 | -19 | -36 | -71 | -125 | -172 | -171 | -165 | -54 | -49 | -32 | -11 | -3 | |
| U-238 | INELASTC | 462 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | -10 | -7 | -7 | -31 | 74 | 210 | 183 | 43 | 7 | |
| U-238 | (N,2N) | -5 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | -5 | |
| U-238 | MU-AVE | 561 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 1 | 2 | 9 | 28 | 62 | 112 | 58 | 91 | 115 | 67 | 16 | |
| PU-239 | CAPTURE | -682 | -8 | -32 | -108 | -186 | -176 | -30 | -53 | -50 | -40 | -20 | -6 | 9 | 11 | 4 | 2 | 1 | 0 | 0 | |
| PU-239 | NU | -5987 | 40 | 142 | 354 | 703 | 598 | 41 | 72 | -4 | -251 | -672 | -1100 | -1454 | -1638 | -926 | -907 | -647 | -265 | -73 | |
| PU-239 | FISSION | -6322 | 25 | 92 | 237 | 465 | 377 | 8 | -1 | -104 | -367 | -761 | -1133 | -1380 | -1465 | -782 | -739 | -519 | -216 | -59 | |
| PU-239 | ELASTIC | -36 | 1 | 1 | 2 | 3 | 1 | -1 | -2 | -3 | -4 | -5 | -6 | -7 | -6 | -3 | -3 | -1 | 0 | | |
| PU-239 | INELASTC | 46 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | -3 | -3 | -1 | 4 | 10 | 20 | 18 | 7 | 1 | | |
| PU-239 | (N,2N) | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | | |
| PU-239 | MU-AVE | 35 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 1 | 3 | 5 | 4 | 7 | 9 | 5 | | |
| PU-240 | CAPTURE | -289 | -5 | -20 | -38 | -69 | -64 | -10 | -21 | -26 | -27 | -16 | -6 | 2 | 5 | 3 | 2 | 1 | 0 | 0 | |
| PU-240 | NU | -1127 | 0 | 0 | 0 | 13 | 10 | 0 | 1 | 1 | -4 | -12 | -18 | -38 | -228 | -271 | -268 | -204 | -84 | -25 | |
| PU-240 | FISSION | -972 | 0 | 0 | 0 | 9 | 6 | 0 | 0 | -1 | -14 | -19 | -37 | -206 | -230 | -220 | -164 | -69 | -20 | | |
| PU-240 | ELASTIC | -14 | 0 | 1 | 1 | 2 | 1 | 0 | -1 | -2 | -2 | -2 | -3 | -3 | -1 | -1 | -1 | -1 | 0 | | |
| PU-240 | INELASTC | 23 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | -2 | -1 | 0 | 1 | 4 | 10 | 8 | 3 | | |
| PU-240 | (N,2N) | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | | |
| PU-240 | MU-AVE | 10 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 1 | 2 | 1 | 2 | 2 | 0 | | |
| PU-241 | CAPTURE | -47 | -1 | -2 | -8 | -14 | -13 | -2 | -4 | -4 | -4 | -2 | 0 | 2 | 3 | 1 | 1 | 0 | 0 | | |
| PU-241 | NU | -651 | 5 | 26 | 83 | 135 | 129 | 8 | 13 | -6 | -54 | -121 | -182 | -204 | -187 | -100 | -97 | -65 | -26 | -8 | |
| PU-241 | FISSION | -777 | 3 | 17 | 56 | 89 | 81 | 1 | -3 | -26 | -74 | -134 | -185 | -192 | -167 | -85 | -79 | -52 | -21 | -6 | |
| PU-241 | ELASTIC | -5 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | -1 | -1 | -1 | 0 | -1 | 0 | 0 | 0 | | |
| PU-241 | INELASTC | 7 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 1 | 2 | 3 | 1 | | |
| PU-241 | (N,2N) | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | | |
| PU-241 | MU-AVE | 4 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 1 | 0 | 1 | 1 | 0 | | |
| PU-242 | CAPTURE | -38 | 0 | -2 | -4 | -9 | -8 | -2 | -3 | -4 | -4 | -2 | -1 | 0 | 1 | 0 | 0 | 0 | 0 | | |
| PU-242 | NU | -144 | 0 | 0 | 0 | 0 | 1 | 0 | 0 | 0 | 0 | 0 | -1 | -3 | -24 | -40 | -37 | -26 | -11 | -3 | |
| PU-242 | FISSION | -122 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | -1 | -3 | -21 | -34 | -30 | -21 | -9 | -3 | |
| PU-242 | ELASTIC | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | | |
| PU-242 | INELASTC | 4 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 1 | 2 | 1 | 0 | | |
| PU-242 | (N,2N) | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | | |
| PU-242 | MU-AVE | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | | |
| AM-241 | CAPTURE | -155 | -1 | -5 | -12 | -26 | -29 | -7 | -12 | -15 | -17 | -14 | -10 | -5 | -2 | 0 | 0 | 0 | 0 | | |
| AM-241 | NU | -39 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | -3 | -10 | -12 | -9 | -4 | -1 | | |
| AM-241 | FISSION | -40 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | -3 | -11 | -12 | -9 | -4 | -1 | | |
| AM-241 | ELASTIC | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | | |
| AM-241 | INELASTC | 1 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | | |
| AM-241 | (N,2N) | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | | |
| AM-241 | MU-AVE | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | | |

表B-2(2/4) 制御棒価値に対する感度係数 (198体炉心 中心CR 1E-3 RZcal)

(1E-4 Δk/kk' / Δσ/σ)

| 核種 | reaction | 群数 | | | | | | | | | | | | | | | | | | | |
|------|----------|-------|----|----|-----|-----|------|-----|-----|-----|------|------|------|------|-----|-----|-----|-----|-----|----|---|
| | | total | 18 | 17 | 16 | 15 | 14 | 13 | 12 | 11 | 10 | 9 | 8 | 7 | 6 | 5 | 4 | 3 | 2 | 1 | |
| B-10 | CAPTU | 4654 | 0 | 1 | 4 | 36 | 97 | 54 | 191 | 424 | 691 | 900 | 947 | 667 | 382 | 76 | 111 | 48 | 21 | 4 | |
| B-10 | ELASTI | 250 | 0 | 0 | 0 | -1 | -2 | -1 | 2 | 9 | 20 | 33 | 45 | 58 | 56 | 17 | 11 | 4 | -1 | 0 | |
| B-10 | INELAST | 9 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 2 | 3 | 2 | 1 | 1 | |
| B-10 | MU-AVE | 4 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 1 | 1 | 0 | 1 | 1 | 0 | 0 | |
| B-10 | (N,2N) | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | |
| B-11 | CAPTU | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | |
| B-11 | ELASTI | 429 | 0 | 0 | 0 | -1 | -3 | -6 | -2 | 5 | 26 | 52 | 80 | 85 | 77 | 75 | 13 | 24 | 5 | -1 | 0 |
| B-11 | INELAST | 3 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 1 | 1 | 1 | |
| B-11 | MU-AVE | 9 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 1 | 1 | 1 | 1 | 2 | 1 | 1 | 0 | 0 | |
| B-11 | (N,2N) | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | |
| C | CAPTU | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | |
| C | ELASTI | 160 | 0 | 0 | 0 | -1 | -3 | -1 | 2 | 9 | 19 | 31 | 33 | 31 | 24 | 8 | 7 | 2 | -1 | 0 | |
| C | INELAST | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | |
| C | MU-AVE | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | |
| C | (N,2N) | 2 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 1 | 1 | 0 | 0 | 0 | 0 | 0 | |
| O | CAPTU | 19 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 12 | 7 | |
| O | ELASTI | -842 | 4 | 8 | 15 | 19 | 21 | -4 | -27 | -72 | -112 | -140 | -139 | -134 | -54 | -64 | -33 | -84 | -43 | -3 | |
| O | INELAST | 3 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 3 | |
| O | MU-AVE | 172 | 0 | 0 | 0 | -1 | 0 | 0 | 0 | 1 | 1 | 2 | -1 | -23 | 117 | 18 | 19 | 12 | 23 | 4 | |
| O | (N,2N) | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | |
| NA | CAPTU | -49 | 0 | -1 | -2 | -5 | -15 | -14 | -3 | 0 | -4 | -2 | -1 | -1 | -1 | 0 | 0 | 0 | 0 | 0 | |
| NA | ELASTI | 269 | -5 | -7 | -5 | -28 | -7 | 4 | 13 | -4 | 10 | 16 | 34 | 104 | 79 | 45 | 18 | 2 | -1 | 1 | |
| NA | INELAST | 159 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 34 | 44 | 30 | 30 | 15 | 6 | |
| NA | MU-AVE | -2 | 0 | 0 | 0 | 1 | 3 | 1 | 0 | 0 | -1 | -2 | -4 | -7 | -3 | 2 | 2 | 5 | 1 | 0 | |
| NA | (N,2N) | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | |
| CB | CAPTU | -65 | 0 | -1 | -1 | -3 | -30 | -3 | -16 | -2 | -8 | -3 | -3 | -1 | 1 | 1 | 1 | 1 | 1 | 1 | |
| CB | ELASTI | -175 | 0 | 1 | 1 | 0 | -1 | -4 | -27 | -14 | -8 | -10 | -27 | -10 | -26 | -13 | -17 | -14 | -5 | -1 | |
| CR | INELAST | 110 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 1 | 4 | 37 | 44 | 17 | 7 | |
| CB | MU-AVE | 58 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 1 | 1 | 3 | 4 | 12 | 21 | 12 | |
| CB | (N,2N) | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | |
| MN | CAPTU | -55 | 0 | -1 | -25 | -2 | -19 | -1 | -3 | -1 | -2 | -1 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | |
| MN | ELASTI | -25 | 0 | 0 | 3 | 0 | -3 | -3 | -3 | -3 | -4 | -2 | -1 | -2 | -1 | -1 | -1 | 0 | 0 | 0 | |
| MN | INELAST | 12 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 1 | 1 | 3 | 4 | 2 | 1 | 1 | |
| MN | MU-AVE | 6 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 1 | 1 | 1 | 1 | 2 | 1 | 0 | |
| MN | (N,2N) | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | |
| FE | CAPTU | -217 | 0 | -2 | -5 | -9 | -128 | -2 | -16 | -18 | -31 | -16 | -13 | -3 | 3 | 3 | 6 | 6 | 5 | | |
| FE | ELASTI | -477 | 3 | 7 | 10 | 0 | -3 | -5 | -38 | -43 | -63 | -53 | -46 | -29 | -59 | -29 | -54 | -54 | -19 | -2 | |
| FE | INELAST | 469 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | -9 | -2 | -1 | 0 | 2 | 91 | 176 | 119 | 69 | 24 | |
| FE | MU-AVE | 190 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 1 | 1 | 2 | 7 | 20 | 15 | 37 | 56 | 38 | 13 | |
| FE | (N,2N) | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | |

表B-2(3/4) 制御棒価値に対する感度係数 (198体炉心 中心C R 1E-3 RZcal)

(1E-4 Δk/kk' / Δσ/σ)

| 項目 | level | 群数 | | | | | | | | | | | | | | | | | (1E-4 Δk/kk' / Δσ/σ) | | | | | | | | | | | | | | | |
|-----------------|-------|-------|----|----|----|----|----|----|----|----|----|-----|----|----|-----|-----|-----|-----|----------------------|----|--|--|--|--|--|--|--|--|--|--|--|--|--|--|
| | | total | 18 | 17 | 16 | 15 | 14 | 13 | 12 | 11 | 10 | 9 | 8 | 7 | 6 | 5 | 4 | 3 | 2 | 1 | | | | | | | | | | | | | | |
| U-238 INELASTIC | 1 | -124 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | -10 | -7 | -7 | -39 | -18 | -19 | -16 | -6 | -2 | | | | | | | | | | | | | | |
| U-238 | 2 | -13 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 1 | -2 | -3 | -3 | -4 | -2 | 0 | | | | | | | | | | | | | | |
| U-238 | 3 | -1 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | -1 | 0 | 0 | | | | | | | | | | | | | | |
| U-238 | 4 | 30 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 8 | 17 | 7 | -1 | -1 | 0 | | | | | | | | | | | | | | |
| U-238 | 5 | 18 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 2 | 10 | 6 | 0 | 0 | 0 | | | | | | | | | | | | | | |
| U-238 | 6 | 3 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 1 | 2 | 0 | 0 | 0 | | | | | | | | | | | | | | |
| U-238 | 7 | 9 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 5 | 4 | 0 | 0 | | | | | | | | | | | | | | |
| U-238 | 8 | 16 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 10 | 6 | 0 | 0 | | | | | | | | | | | | | | |
| U-238 | 9 | 15 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 8 | 7 | 0 | 0 | | | | | | | | | | | | | | |
| U-238 | 10 | 18 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 9 | 9 | 0 | 0 | | | | | | | | | | | | | | |
| U-238 | 11 | 7 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 3 | 4 | 0 | 0 | | | | | | | | | | | | | | |
| U-238 | 12 | 10 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 5 | 6 | 0 | 0 | | | | | | | | | | | | | | |
| U-238 | 13 | 14 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 9 | 9 | 0 | 0 | | | | | | | | | | | | | | |
| U-238 | 14 | 7 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 2 | 5 | 0 | 0 | | | | | | | | | | | | | | |
| U-238 | 15 | 10 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 3 | 7 | 0 | 0 | | | | | | | | | | | | | | |
| U-238 | 16 | 13 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 4 | 10 | 0 | -1 | | | | | | | | | | | | | | |
| U-238 | 17 | 9 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 2 | 7 | 0 | 0 | | | | | | | | | | | | | | |
| U-238 | 18 | 9 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 3 | 6 | 0 | 0 | | | | | | | | | | | | | | |
| U-238 | 19 | 6 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 1 | 5 | 0 | 0 | | | | | | | | | | | | | | |
| U-238 | 20 | 8 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 2 | 6 | 0 | 0 | | | | | | | | | | | | | | |
| U-238 | 21 | 6 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 1 | 5 | 0 | 0 | | | | | | | | | | | | | | |
| U-238 | 22 | 7 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 2 | 5 | 0 | 0 | | | | | | | | | | | | | | |
| U-238 | 23 | 9 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 2 | 7 | 0 | 0 | | | | | | | | | | | | | | |
| U-238 | 24 | 4 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 1 | 3 | 0 | 0 | | | | | | | | | | | | | | |
| U-238 | 25 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | | | | | | | | | | | | | | |
| U-238 | 26 | 6 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 1 | 5 | 0 | 0 | | | | | | | | | | | | | | |
| U-238 | 27 | 1 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 1 | 0 | 0 | | | | | | | | | | | | | | |
| U-238 | 28 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | | | | | | | | | | | | | | |
| U-238 | 29 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | | | | | | | | | | | | | | |
| U-238 | 30 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | | | | | | | | | | | | | | |
| U-238 | 31 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | | | | | | | | | | | | | | |
| U-238 | 32 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | | | | | | | | | | | | | | |
| U-238 | 33 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | | | | | | | | | | | | | | |
| U-238 | 34 | 367 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 102 | 200 | 55 | 10 | | | | | | | | | | | | | | |
| | total | 464 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | -10 | -7 | -6 | -31 | 75 | 212 | 178 | 45 | 8 | | | | | | | | | | | | | | |

表B-2(4/4) 制御棒価値に対する感度係数(198体炉心 中心CR 1E-3 RZcal)

(1E-4 Δk/kk' / Δσ/σ)

| 項目 | サペイ | 群数 | | | | | | | | | | | | | | | | | 1 | |
|------------------|-------|-------|----|----|----|----|----|----|----|----|----|----|----|-----|-----|-----|------|------|------|------|
| | | total | 18 | 17 | 16 | 15 | 14 | 13 | 12 | 11 | 10 | 9 | 8 | 7 | 6 | 5 | 4 | 3 | | |
| FISSION SPECTRUM | -1 | -82 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 1 | 7 | 26 | 82 | 229 | 486 | 343 | -226 | -587 | -303 | -140 |
| FISSION | -0.9 | -71 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 1 | 7 | 26 | 81 | 227 | 479 | 336 | -219 | -571 | -299 | -139 |
| FISSION | -0.8 | -60 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 1 | 7 | 26 | 81 | 226 | 471 | 330 | -213 | -555 | -295 | -139 |
| FISSION | -0.7 | -50 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 1 | 7 | 26 | 81 | 225 | 464 | 323 | -207 | -541 | -291 | -138 |
| FISSION | -0.6 | -43 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 1 | 7 | 25 | 81 | 223 | 456 | 317 | -201 | -527 | -287 | -138 |
| FISSION | -0.5 | -35 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 1 | 7 | 25 | 81 | 222 | 450 | 311 | -196 | -514 | -284 | -138 |
| FISSION | -0.4 | -28 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 1 | 7 | 25 | 81 | 221 | 443 | 305 | -191 | -501 | -280 | -137 |
| FISSION | -0.3 | -20 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 1 | 7 | 25 | 81 | 220 | 436 | 299 | -186 | -489 | -277 | -137 |
| FISSION | -0.2 | -12 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 1 | 7 | 25 | 80 | 219 | 430 | 294 | -181 | -478 | -273 | -136 |
| FISSION | -0.1 | -7 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 1 | 7 | 25 | 80 | 217 | 424 | 289 | -177 | -467 | -270 | -136 |
| FISSION | -0.05 | -4 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 1 | 7 | 25 | 80 | 217 | 421 | 286 | -175 | -462 | -268 | -136 |
| FISSION | 0.05 | 2 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 1 | 7 | 25 | 80 | 216 | 415 | 281 | -171 | -451 | -265 | -136 |
| FISSION | 0.1 | 5 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 1 | 7 | 25 | 80 | 215 | 412 | 279 | -169 | -446 | -264 | -135 |
| FISSION | 0.2 | 10 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 1 | 7 | 25 | 80 | 214 | 406 | 274 | -165 | -437 | -260 | -135 |
| FISSION | 0.3 | 15 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 1 | 7 | 25 | 80 | 213 | 401 | 270 | -162 | -428 | -257 | -135 |
| FISSION | 0.4 | 22 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 1 | 7 | 25 | 80 | 212 | 396 | 266 | -158 | -419 | -254 | -134 |
| FISSION | 0.5 | 22 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 1 | 7 | 25 | 79 | 211 | 390 | 261 | -155 | -411 | -252 | -134 |
| FISSION | 0.6 | 27 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 1 | 7 | 25 | 79 | 210 | 385 | 257 | -152 | -403 | -249 | -133 |
| FISSION | 0.7 | 31 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 1 | 7 | 25 | 79 | 208 | 380 | 253 | -148 | -395 | -246 | -133 |
| FISSION | 0.8 | 35 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 1 | 7 | 25 | 79 | 207 | 376 | 249 | -146 | -387 | -243 | -133 |
| FISSION | 0.9 | 39 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 1 | 7 | 25 | 79 | 206 | 371 | 246 | -143 | -380 | -241 | -132 |
| FISSION | 1 | 42 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 1 | 7 | 25 | 79 | 205 | 366 | 242 | -140 | -373 | -238 | -132 |

表B-3(1/4) 制御棒価値に対する感度係数(198体炉心 中心CR 1E-2 xycal)

(1E-4Δk/kk' / Δσ/σ)

| 核種 | reaction | 群数 | | | | | | | | | | | | | | | | | | |
|--------|----------|-------|----|-----|------|------|------|-----|------|------|------|------|-------|-------|-------|------|------|------|------|------|
| | | total | 18 | 17 | 16 | 15 | 14 | 13 | 12 | 11 | 10 | 9 | 8 | 7 | 6 | 5 | 4 | 3 | 2 | 1 |
| U-235 | CAPTURE | -8 | 0 | 0 | -1 | -2 | -2 | 0 | -1 | -1 | -1 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| U-235 | NU | -81 | -4 | -2 | 0 | 4 | 3 | -2 | -3 | -5 | -8 | -12 | -14 | -13 | -11 | -5 | -5 | -3 | -1 | 0 |
| U-235 | FISSION | -96 | -3 | -2 | -2 | 0 | -2 | -3 | -5 | -7 | -10 | -13 | -14 | -13 | -10 | -4 | -4 | -3 | -1 | 0 |
| U-235 | ELASTIC | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| U-235 | INELASTC | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| U-235 | MU-AVE | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| U-235 | (N,2N) | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| U-238 | CAPTURE | -1676 | 6 | -31 | -105 | -344 | -372 | -84 | -189 | -246 | -235 | -127 | -50 | 9 | 43 | 29 | 14 | 5 | 1 | 0 |
| U-238 | NU | -1873 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | -1 | -5 | -61 | -725 | -659 | -305 | -117 |
| U-238 | FISSION | -1538 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | -1 | -5 | -53 | -603 | -531 | -250 | -95 |
| U-238 | ELASTIC | -753 | 4 | 12 | 12 | 16 | 4 | -6 | -19 | -39 | -73 | -120 | -154 | -143 | -133 | -42 | -37 | -24 | -9 | -2 |
| U-238 | INELASTC | 699 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | -7 | 6 | 11 | -3 | 115 | 270 | 235 | 62 | 10 |
| U-238 | MU-AVE | 451 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 1 | 2 | 9 | 26 | 53 | 91 | 46 | 71 | 88 | 52 | 12 |
| U-238 | (N,2N) | -4 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | -4 |
| Pu-238 | CAPTURE | -20 | 0 | -1 | -2 | -5 | -5 | -1 | -1 | -2 | -2 | -1 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Pu-238 | NU | -105 | 0 | 1 | 4 | 5 | 4 | 0 | 1 | 0 | -2 | -5 | -9 | -16 | -29 | -20 | -18 | -13 | -6 | -2 |
| Pu-238 | FISSION | -102 | 0 | 1 | 3 | 3 | 2 | 0 | 0 | -1 | -3 | -6 | -9 | -16 | -27 | -17 | -15 | -11 | -5 | -1 |
| Pu-238 | ELASTIC | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Pu-238 | INELASTC | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Pu-238 | MU-AVE | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Pu-238 | (N,2N) | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| PU-239 | CAPTURE | -792 | -8 | -35 | -118 | -210 | -202 | -36 | -64 | -61 | -48 | -25 | -9 | 7 | 10 | 4 | 2 | 1 | 0 | 0 |
| PU-239 | NU | -6002 | 39 | 145 | 369 | 740 | 624 | 34 | 63 | -23 | -280 | -725 | -1141 | -1467 | -1630 | -906 | -882 | -626 | -255 | -71 |
| PU-239 | FISSION | -6560 | 21 | 90 | 239 | 473 | 371 | -5 | -25 | -144 | -431 | -837 | -1195 | -1405 | -1461 | -766 | -720 | -501 | -207 | -57 |
| PU-239 | ELASTIC | -24 | 0 | 1 | 2 | 3 | 1 | 0 | -2 | -3 | -4 | -4 | -4 | -4 | -3 | -2 | -2 | -1 | 0 | 0 |
| PU-239 | INELASTC | 64 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | -4 | -3 | -3 | -2 | 1 | 9 | 12 | 24 | 21 | 8 | 1 |
| PU-239 | MU-AVE | 21 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 1 | 2 | 3 | 2 | 4 | 5 | 3 | 1 |
| PU-239 | (N,2N) | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| PU-240 | CAPTURE | -330 | -5 | -22 | -42 | -77 | -72 | -12 | -25 | -30 | -32 | -19 | -7 | 2 | 5 | 3 | 2 | 1 | 0 | 0 |
| PU-240 | NU | -1110 | 0 | 0 | 1 | 14 | 11 | 0 | 1 | 1 | -5 | -13 | -19 | -39 | -228 | -267 | -263 | -198 | -82 | -24 |
| PU-240 | FISSION | -963 | 0 | 0 | 0 | 9 | 6 | 0 | 0 | -2 | -9 | -16 | -20 | -38 | -206 | -227 | -215 | -159 | -67 | -19 |
| PU-240 | ELASTIC | -11 | 0 | 1 | 1 | 1 | 1 | 0 | -1 | -2 | -2 | -2 | -2 | -1 | -1 | -1 | -1 | 0 | 0 | 0 |
| PU-240 | INELASTC | 31 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | -2 | -1 | 2 | 5 | 12 | 10 | 3 | 1 | 1 |
| PU-240 | MU-AVE | 6 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 1 | 1 | 1 | 1 | 1 | 1 | 0 |
| PU-240 | (N,2N) | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| PU-241 | CAPTURE | -59 | -1 | -2 | -9 | -16 | -16 | -2 | -5 | -5 | -5 | -3 | -1 | 1 | 3 | 1 | 1 | 0 | 0 | 0 |
| PU-241 | NU | -648 | 5 | 27 | 87 | 143 | 136 | 7 | 11 | -9 | -61 | -129 | -187 | -205 | -186 | -98 | -94 | -63 | -25 | -7 |
| PU-241 | FISSION | -818 | 3 | 17 | 57 | 92 | 80 | -2 | -8 | -34 | -86 | -146 | -194 | -195 | -166 | -83 | -77 | -50 | -20 | -6 |
| PU-241 | ELASTIC | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| PU-241 | INELASTC | 9 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 1 | 1 | 3 | 3 | 1 | 0 |
| PU-241 | MU-AVE | 2 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 1 | 1 | 0 | 0 |
| PU-241 | (N,2N) | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| PU-242 | CAPTURE | -44 | 0 | -2 | -5 | -10 | -9 | -2 | -4 | -5 | -5 | -2 | -1 | 0 | 1 | 0 | 0 | 0 | 0 | 0 |
| PU-242 | NU | -143 | 0 | 0 | 0 | 1 | 0 | 0 | 0 | 0 | 0 | 0 | -1 | -3 | -24 | -40 | -36 | -26 | -11 | -3 |
| PU-242 | FISSION | -122 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | -1 | -3 | -21 | -34 | -30 | -21 | -9 | -3 |
| PU-242 | ELASTIC | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| PU-242 | INELASTC | 6 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 1 | 2 | 2 | 1 | 0 |
| PU-242 | MU-AVE | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| PU-242 | (N,2N) | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |

表B-3(2/4) 制御棒価値に対する感度係数 (198体炉心 中心CR 1E-2 xycal)

(1E-4Δk/k' / Δσ/σ)

| 核種 | reaction | total | 群数 | | | | | | | | | | | | | | | | | | 1 |
|--------|----------|-------|----|----|-----|-----|------|-----|-----|-----|------|------|------|-----|-----|-----|-----|-----|-----|----|----|
| | | | 18 | 17 | 16 | 15 | 14 | 13 | 12 | 11 | 10 | 9 | 8 | 7 | 6 | 5 | 4 | 3 | 2 | | |
| AM-241 | CAPTURE | -161 | -1 | -5 | -13 | -28 | -31 | -7 | -13 | -15 | -17 | -14 | -10 | -5 | -2 | 0 | 0 | 0 | 0 | 0 | 0 |
| AM-241 | NU | -42 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | -3 | -11 | -13 | -10 | -4 | -4 | -1 | -1 |
| AM-241 | FISSION | -43 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | -4 | -12 | -13 | -9 | -4 | -4 | -1 | -1 |
| AM-241 | ELASTIC | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| AM-241 | INELASTC | 4 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 1 | 1 | 1 | 1 | 0 | 0 | 0 | 0 |
| AM-241 | MU-AVE | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| AM-241 | (H, 2H) | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| B-10 | CAPTU | 5326 | 1 | 1 | 6 | 54 | 150 | 76 | 244 | 511 | 806 | 1019 | 1055 | 726 | 406 | 79 | 116 | 50 | 22 | 4 | |
| B-10 | ELASTI | 259 | 0 | 0 | 0 | -1 | -2 | -1 | 2 | 10 | 21 | 35 | 48 | 59 | 55 | 18 | 12 | 5 | 0 | 0 | 0 |
| B-10 | INELAST | 9 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 2 | 3 | 2 | 1 | 1 | 1 | 1 |
| B-10 | MU-AVE | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| B-10 | (H, 2H) | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| B-11 | CAPTU | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| B-11 | ELASTI | 442 | 0 | 0 | 0 | -1 | -4 | -7 | -3 | 5 | 28 | 56 | 84 | 89 | 77 | 73 | 14 | 26 | 6 | -1 | 0 |
| B-11 | INELAST | 3 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 1 | 1 | 1 | 1 |
| B-11 | MU-AVE | 7 | 0 | 0 | 0 | 0 | 0 | 1 | 0 | 0 | 1 | 1 | 1 | 1 | 0 | 0 | 0 | 0 | 1 | 0 | 0 |
| B-11 | (H, 2H) | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| C | CAPTU | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| C | ELASTI | 168 | 0 | 0 | 0 | -1 | -3 | -1 | 2 | 10 | 21 | 32 | 35 | 31 | 24 | 8 | 8 | 2 | 0 | 0 | 0 |
| C | INELAST | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| C | MU-AVE | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| C | (H, 2H) | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| O | CAPTU | 19 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 12 | 7 |
| O | ELASTI | -377 | 3 | 8 | 15 | 18 | 19 | -3 | -30 | -78 | -106 | -115 | -75 | -35 | 95 | -11 | 11 | -58 | -30 | -1 | |
| O | INELAST | 4 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 4 | |
| O | MU-AVE | 137 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 1 | 2 | 2 | -1 | -19 | 94 | 14 | 15 | 9 | 17 | 3 | 0 |
| O | (H, 2H) | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| NA | CAPTU | -52 | 0 | -1 | -2 | -5 | -17 | -15 | -3 | 0 | -4 | -2 | -1 | -1 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| NA | ELASTI | -198 | -3 | -3 | -2 | -30 | -27 | -3 | 1 | -33 | -43 | -71 | -55 | 33 | 20 | 30 | 0 | -8 | -4 | 0 | |
| NA | INELAST | 189 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 57 | 48 | 31 | 32 | 15 | 6 | |
| NA | MU-AVE | 74 | 0 | 0 | 0 | 0 | 2 | 3 | 1 | 1 | 1 | 1 | 1 | 1 | 10 | 15 | 14 | 5 | 1 | 1 | |
| NA | (H, 2H) | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| CB | CAPTU | -60 | 0 | 0 | -1 | -3 | -30 | -3 | -16 | -2 | -7 | -2 | -1 | 1 | 1 | 1 | 1 | 1 | 1 | 1 | 1 |
| CB | ELASTI | -191 | 0 | 1 | 1 | -1 | -3 | -5 | -33 | -16 | -11 | -18 | -43 | -7 | -22 | -9 | -11 | -10 | -4 | 0 | |
| CB | INELAST | 129 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 1 | 5 | 43 | 51 | 21 | 8 | | |
| CB | MU-AVE | 50 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 2 | 3 | 3 | 10 | 17 | 10 | 3 | |
| CB | (H, 2H) | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| MN | CAPTU | -53 | 0 | 0 | -25 | -2 | -19 | -1 | -3 | -1 | -1 | -1 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| MN | ELASTI | -30 | 0 | 0 | 2 | 0 | -6 | -4 | -4 | -3 | -5 | -3 | -2 | -1 | -1 | -1 | -1 | -1 | 0 | 0 | 0 |
| MN | INELAST | 16 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 1 | 2 | 1 | 4 | 5 | 2 | 1 | |
| MN | MU-AVE | 4 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 1 | 0 | 1 | 1 | 1 | 0 | 0 |
| MN | (H, 2H) | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| FE | CAPTU | -202 | 0 | -2 | -5 | -9 | -130 | -2 | -16 | -17 | -28 | -14 | -10 | 0 | 6 | 3 | 3 | 7 | 7 | 5 | |
| FE | ELASTI | -516 | 5 | 8 | 9 | -13 | -19 | -6 | -48 | -53 | -110 | -59 | -47 | -18 | -40 | -19 | -38 | -41 | -15 | -2 | |
| FE | INELAST | 567 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | -5 | -1 | 0 | 1 | 3 | 112 | 200 | 144 | 85 | 28 |
| FE | MU-AVE | 169 | 0 | 0 | 0 | 0 | 1 | 0 | 1 | 0 | 2 | 4 | 10 | 18 | 13 | 31 | 45 | 31 | 10 | 0 | |
| FE | (H, 2H) | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Ni | CAPTU | -13 | 0 | -1 | -1 | -3 | -5 | -2 | -5 | -25 | -12 | -7 | -4 | 0 | 2 | 2 | 5 | 17 | 19 | 7 | |
| Ni | ELASTI | -255 | 1 | 3 | 3 | -5 | -9 | -4 | -17 | -69 | -41 | -29 | -21 | -18 | -7 | -9 | -9 | -3 | 0 | | |
| Ni | INELAST | 76 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 27 | 33 | 12 | 4 | |
| Ni | MU-AVE | 39 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 1 | 2 | 3 | 4 | 3 | 7 | 9 | 6 | 2 | 2 | |
| Ni | (H, 2H) | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Mo | CAPTU | -81 | 0 | -2 | -8 | -20 | -18 | -4 | -9 | -9 | -8 | -4 | -2 | 0 | 1 | 1 | 1 | 0 | 0 | 0 | |
| Mo | ELASTI | -23 | 0 | 0 | 0 | 0 | -1 | 0 | -1 | -2 | -3 | -4 | -3 | -4 | -1 | -1 | -1 | 0 | 0 | 0 | |
| Mo | INELAST | 34 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 2 | 6 | 11 | 10 | 4 | 1 | 1 | |
| Mo | MU-AVE | 9 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 1 | 3 | 1 | 2 | 1 | 0 | 0 | |
| Mo | (H, 2H) | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |

表B-3(3/4) 制御棒価値に対する感度係数(198体炉心 中心CR 1E-2 xycal)

(1E-4 $\Delta k/k^*$ / $\Delta\sigma/\sigma$)

| 項目 | level | 群数 | | | | | | | | | | | | | | | | | | |
|-----------------|-------|-------|----|----|----|----|----|----|----|----|----|----|---|----|-----|-----|-----|-----|----|----|
| | | total | 18 | 17 | 16 | 15 | 14 | 13 | 12 | 11 | 10 | 9 | 8 | 7 | 6 | 5 | 4 | 3 | 2 | 1 |
| U-238 INELASTIC | 1 | -56 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | -7 | 6 | 10 | -21 | -13 | -13 | -12 | -5 | -1 |
| U-238 | 2 | -3 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 1 | 1 | 0 | -1 | -3 | -1 | 0 |
| U-238 | 3 | 1 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 1 | 0 | 0 | 0 |
| U-238 | 4 | 45 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 13 | 23 | 9 | 0 | 0 | 0 |
| U-238 | 5 | 24 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 4 | 13 | 7 | 0 | 0 | 0 |
| U-238 | 6 | 3 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 1 | 2 | 0 | 0 | 0 |
| U-238 | 7 | 10 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 6 | 4 | 0 | 0 |
| U-238 | 8 | 21 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 13 | 8 | 0 | 0 |
| U-238 | 9 | 19 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 11 | 8 | 0 | 0 |
| U-238 | 10 | 23 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 12 | 11 | 0 | 0 |
| U-238 | 11 | 10 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 5 | 5 | 0 | 0 |
| U-238 | 12 | 13 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 6 | 7 | 0 | 0 |
| U-238 | 13 | 18 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 6 | 11 | 1 | 0 |
| U-238 | 14 | 8 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 2 | 6 | 0 | 0 |
| U-238 | 15 | 13 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 4 | 9 | 0 | 0 |
| U-238 | 16 | 18 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 6 | 12 | 1 | -1 |
| U-238 | 17 | 13 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 3 | 9 | 1 | 0 |
| U-238 | 18 | 11 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 4 | 7 | 0 | 0 |
| U-238 | 19 | 9 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 2 | 6 | 1 | 0 |
| U-238 | 20 | 10 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 3 | 7 | 0 | 0 |
| U-238 | 21 | 8 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 1 | 6 | 1 | 0 |
| U-238 | 22 | 8 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 2 | 6 | 0 | 0 |
| U-238 | 23 | 12 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 2 | 9 | 1 | 0 |
| U-238 | 24 | 4 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 1 | 3 | 0 | 0 |
| U-238 | 25 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| U-238 | 26 | 7 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 1 | 6 | 0 | 0 |
| U-238 | 27 | 1 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 1 | 0 | 0 |
| U-238 | 28 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| U-238 | 29 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| U-238 | 30 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| U-238 | 31 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| U-238 | 32 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| U-238 | 33 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| U-238 | 34 | 451 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 126 | 242 | 71 | 12 |
| | total | 701 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | -7 | 6 | 11 | -3 | 114 | 272 | 233 | 64 | 11 |

表B-3(4/4) 制御棒価値に対する感度係数(198体炉心 中心CR 1E-2 xycal)

(1E-4Δk/kk' / Δσ/σ)

| 項目 | #ヘイ | 群数 | | | | | | | | | | | | | | | | | | |
|------------------|-------|-------|----|----|----|----|----|----|----|----|----|----|----|-----|-----|-----|------|------|------|------|
| | | total | 18 | 17 | 16 | 15 | 14 | 13 | 12 | 11 | 10 | 9 | 8 | 7 | 6 | 5 | 4 | 3 | 2 | 1 |
| FISSION SPECTRUM | -1 | -93 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 2 | 9 | 32 | 96 | 255 | 510 | 363 | -249 | -632 | -333 | -146 |
| FISSION | -0.9 | -82 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 2 | 9 | 32 | 96 | 254 | 501 | 355 | -242 | -614 | -329 | -146 |
| FISSION | -0.8 | -68 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 2 | 9 | 32 | 96 | 252 | 494 | 348 | -235 | -597 | -324 | -145 |
| FISSION | -0.7 | -59 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 2 | 9 | 32 | 95 | 251 | 486 | 341 | -228 | -582 | -320 | -145 |
| FISSION | -0.6 | -49 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 2 | 9 | 32 | 95 | 250 | 478 | 335 | -222 | -567 | -316 | -145 |
| FISSION | -0.5 | -39 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 2 | 9 | 32 | 95 | 248 | 471 | 328 | -216 | -552 | -312 | -144 |
| FISSION | -0.4 | -30 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 2 | 9 | 32 | 95 | 247 | 464 | 322 | -210 | -539 | -308 | -144 |
| FISSION | -0.3 | -21 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 2 | 9 | 32 | 95 | 246 | 457 | 316 | -205 | -526 | -304 | -143 |
| FISSION | -0.2 | -13 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 2 | 9 | 32 | 95 | 244 | 451 | 311 | -200 | -514 | -300 | -143 |
| FISSION | -0.1 | -8 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 2 | 9 | 32 | 94 | 243 | 444 | 305 | -195 | -502 | -297 | -143 |
| FISSION | -0.05 | -4 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 2 | 9 | 32 | 94 | 242 | 441 | 302 | -193 | -496 | -295 | -142 |
| FISSION | 0.05 | 4 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 2 | 9 | 32 | 94 | 241 | 435 | 297 | -188 | -485 | -291 | -142 |
| FISSION | 0.1 | 6 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 2 | 9 | 32 | 94 | 240 | 432 | 295 | -186 | -480 | -290 | -142 |
| FISSION | 0.2 | 12 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 2 | 9 | 32 | 94 | 239 | 426 | 290 | -182 | -470 | -286 | -142 |
| FISSION | 0.3 | 18 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 2 | 9 | 32 | 94 | 238 | 420 | 285 | -178 | -460 | -283 | -141 |
| FISSION | 0.4 | 23 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 2 | 9 | 32 | 94 | 237 | 415 | 280 | -174 | -451 | -280 | -141 |
| FISSION | 0.5 | 25 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 2 | 9 | 31 | 93 | 235 | 409 | 276 | -171 | -442 | -277 | -140 |
| FISSION | 0.6 | 32 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 2 | 9 | 31 | 93 | 234 | 404 | 272 | -167 | -433 | -273 | -140 |
| FISSION | 0.7 | 35 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 2 | 9 | 31 | 93 | 233 | 399 | 267 | -164 | -425 | -270 | -140 |
| FISSION | 0.8 | 41 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 2 | 9 | 31 | 93 | 232 | 394 | 263 | -160 | -417 | -267 | -139 |
| FISSION | 0.9 | 43 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 2 | 9 | 31 | 93 | 230 | 389 | 259 | -157 | -409 | -265 | -139 |
| FISSION | 1 | 49 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 2 | 9 | 31 | 93 | 229 | 384 | 256 | -154 | -401 | -262 | -138 |

表B-4(1/4) 制御棒価値に対する感度係数 (198体炉心 CR-4 1E-2 xycal)

(1E-4△k/kk' / △σ/σ)

| 核種 | reaction | 群数 | | | | | | | | | | | | | | | | | | (1E-4△k/kk' / △σ/σ) |
|--------|----------|-------|----|-----|------|------|------|-----|------|------|------|------|-------|-------|-------|------|------|------|------|---------------------|
| | | total | 18 | 17 | 16 | 15 | 14 | 13 | 12 | 11 | 10 | 9 | 8 | 7 | 6 | 5 | 4 | 3 | 2 | |
| U-235 | CAPTURE | -8 | 0 | 0 | -1 | -2 | -2 | 0 | -1 | -1 | -1 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| U-235 | NU | -77 | -3 | -1 | 0 | 5 | 3 | -2 | -3 | -5 | -8 | -12 | -13 | -13 | -11 | -5 | -5 | -3 | -1 | 0 |
| U-235 | FISSION | -90 | -3 | -2 | -1 | 0 | -1 | -2 | -4 | -6 | -10 | -13 | -14 | -12 | -10 | -4 | -4 | -3 | -1 | 0 |
| U-235 | ELASTIC | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| U-235 | INELASTC | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| U-235 | MU-AVE | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| U-235 | (N,2N) | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| U-238 | CAPTURE | -1554 | 3 | -33 | -103 | -327 | -349 | -78 | -175 | -229 | -217 | -114 | -42 | 13 | 46 | 31 | 14 | 5 | 1 | 0 |
| U-238 | NU | -1867 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | -1 | -5 | -61 | -727 | -655 | -302 | -116 |
| U-238 | FISSION | -1526 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | -1 | -5 | -53 | -601 | -525 | -247 | -94 |
| U-238 | ELASTIC | -622 | 4 | 10 | 10 | 13 | 3 | -6 | -19 | -36 | -65 | -100 | -125 | -114 | -105 | -33 | -30 | -20 | -7 | -2 |
| U-238 | INELASTC | 762 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| U-238 | MU-AVE | 368 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| U-238 | (N,2N) | -3 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | -3 |
| Pu-238 | CAPTURE | -20 | 0 | -1 | -2 | -5 | -5 | -1 | -1 | -2 | -2 | -1 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Pu-238 | NU | -104 | 0 | 1 | 4 | 4 | 3 | 0 | 1 | 0 | -2 | -5 | -9 | -16 | -29 | -19 | -17 | -13 | -5 | -2 |
| Pu-238 | FISSION | -98 | 0 | 1 | 3 | 3 | 2 | 0 | 0 | -1 | -4 | -6 | -9 | -16 | -26 | -16 | -14 | -10 | -4 | -1 |
| Pu-238 | ELASTIC | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Pu-238 | INELASTC | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Pu-238 | MU-AVE | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Pu-238 | (N,2N) | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| PU-239 | CAPTURE | -762 | -8 | -33 | -112 | -200 | -193 | -35 | -62 | -59 | -47 | -25 | -10 | 6 | 9 | 4 | 2 | 1 | 0 | 0 |
| PU-239 | NU | -6031 | 39 | 138 | 342 | 677 | 552 | 20 | 34 | -59 | -327 | -748 | -1138 | -1431 | -1560 | -855 | -829 | -583 | -237 | -66 |
| PU-239 | FISSION | -6632 | 21 | 85 | 219 | 423 | 310 | -18 | -52 | -177 | -466 | -859 | -1197 | -1381 | -1410 | -730 | -682 | -471 | -194 | -53 |
| PU-239 | ELASTIC | -20 | 0 | 1 | 1 | 2 | 1 | -1 | -2 | -3 | -4 | -4 | -3 | -3 | -2 | -1 | -1 | 0 | 0 | 0 |
| PU-239 | INELASTC | 68 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | -4 | -2 | -2 | -1 | 1 | 10 | 12 | 24 | 21 | 8 |
| PU-239 | MU-AVE | 17 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 1 | 1 | 2 | 2 | 3 | 4 | 1 |
| PU-239 | (N,2N) | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| PU-240 | CAPTURE | -314 | -6 | -21 | -39 | -73 | -68 | -11 | -23 | -29 | -30 | -18 | -7 | 1 | 5 | 2 | 2 | 1 | 0 | 0 |
| PU-240 | NU | -1066 | 0 | 0 | 0 | 13 | 10 | 0 | 1 | 0 | -6 | -14 | -19 | -38 | -221 | -255 | -250 | -187 | -77 | -23 |
| PU-240 | FISSION | -934 | 0 | 0 | 0 | 8 | 5 | 0 | 0 | -3 | -10 | -17 | -21 | -38 | -201 | -219 | -206 | -151 | -63 | -18 |
| PU-240 | ELASTIC | -9 | 0 | 1 | 1 | 1 | 0 | 0 | -1 | -2 | -2 | -1 | -1 | -1 | 0 | -1 | -1 | 0 | 0 | 0 |
| PU-240 | INELASTC | 32 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | -1 | -1 | 1 | 2 | 5 | 12 | 10 | 3 | 1 |
| PU-240 | MU-AVE | 6 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 1 | 1 | 1 | 1 | 1 | 0 | 0 |
| PU-240 | (N,2N) | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| PU-241 | CAPTURE | -57 | -1 | -2 | -8 | -15 | -15 | -2 | -5 | -5 | -5 | -3 | -1 | 1 | 2 | 1 | 1 | 0 | 0 | 0 |
| PU-241 | NU | -669 | 5 | 26 | 81 | 132 | 121 | 4 | 5 | -16 | -66 | -132 | -185 | -199 | -177 | -92 | -88 | -58 | -23 | -7 |
| PU-241 | FISSION | -845 | 3 | 16 | 52 | 82 | 68 | -5 | -14 | -40 | -91 | -149 | -193 | -191 | -160 | -78 | -73 | -47 | -19 | -6 |
| PU-241 | ELASTIC | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| PU-241 | INELASTC | 9 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 1 | 1 | 3 | 3 | 1 | 0 |
| PU-241 | MU-AVE | 1 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 1 | 0 | 0 |
| PU-241 | (N,2N) | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| PU-242 | CAPTURE | -41 | 0 | -2 | -4 | -9 | -9 | -2 | -4 | -5 | -4 | -2 | -1 | 0 | 1 | 0 | 0 | 0 | 0 | 0 |
| PU-242 | NU | -135 | 0 | 0 | 0 | 1 | 0 | 0 | 0 | 0 | 0 | 0 | -1 | -3 | -23 | -38 | -34 | -24 | -10 | -3 |
| PU-242 | FISSION | -117 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | -1 | -3 | -21 | -33 | -28 | -20 | -8 | -3 |
| PU-242 | ELASTIC | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| PU-242 | INELASTC | 6 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 1 | 2 | 2 | 1 | 0 |
| PU-242 | MU-AVE | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| PU-242 | (N,2N) | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |

表B-4(2/4) 制御棒価値に対する感度係数(198体炉心 CR-4 1E-2 xycal)

(1E-4Δk/kk' / Δσ/σ)

| 核種 | reaction | total | 群数 | | | | | | | | | | | | | | | | | |
|--------|----------|-------|----|----|-----|-----|------|-----|-----|-----|------|------|------|-----|-----|-----|-----|-----|-----|----|
| | | | 18 | 17 | 16 | 15 | 14 | 13 | 12 | 11 | 10 | 9 | 8 | 7 | 6 | 5 | 4 | 3 | 2 | 1 |
| AM-241 | CAPTURE | -140 | -1 | -5 | -12 | -26 | -27 | -6 | -11 | -13 | -15 | -12 | -8 | -3 | -1 | 0 | 0 | 0 | 0 | 0 |
| AM-241 | NU | -44 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | -1 | -4 | -11 | -13 | -10 | -4 | -1 | -1 |
| AM-241 | FISSION | -44 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | -1 | -5 | -11 | -13 | -9 | -4 | -1 | -1 |
| AM-241 | ELASTIC | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| AM-241 | INELASTC | 4 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 1 | 1 | 1 | 0 | 0 | 0 |
| AM-241 | NU-AVE | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| AM-241 | (N,2N) | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| B-10 | CAPTU | 5434 | 1 | 3 | 11 | 71 | 177 | 81 | 256 | 524 | 818 | 1028 | 1061 | 727 | 405 | 79 | 116 | 50 | 22 | 4 |
| B-10 | ELASTI | 253 | 0 | 0 | 0 | -1 | -2 | -1 | 2 | 10 | 21 | 35 | 47 | 57 | 52 | 16 | 12 | 5 | 0 | 0 |
| B-10 | INELAST | 9 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 2 | 3 | 2 | 1 | 1 |
| B-10 | NU-AVE | 2 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 1 | 1 | 0 | 0 | 0 | 0 | 0 |
| B-10 | (N,2N) | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| B-11 | CAPTU | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| B-11 | ELASTI | 434 | 0 | 0 | -1 | -3 | -7 | -3 | 5 | 27 | 55 | 83 | 88 | 75 | 70 | 14 | 26 | 6 | -1 | 0 |
| B-11 | INELAST | 3 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 1 | 1 | 1 |
| B-11 | NU-AVE | 8 | 0 | 0 | 0 | 0 | 1 | 0 | 0 | 1 | 1 | 1 | 1 | 1 | 1 | 0 | 0 | 0 | 1 | 0 |
| B-11 | (N,2N) | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| C | CAPTU | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| C | ELASTI | 165 | 0 | 0 | 0 | 0 | -1 | -3 | -1 | 2 | 10 | 21 | 32 | 34 | 30 | 23 | 8 | 8 | 2 | 0 |
| C | INELAST | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| C | NU-AVE | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| C | (N,2N) | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| O | CAPTU | 19 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 12 | 7 |
| O | ELASTI | -268 | 3 | 7 | 14 | 12 | 15 | -2 | -31 | -79 | -104 | -100 | -55 | -3 | 149 | -13 | 10 | -59 | -31 | -1 |
| O | INELAST | 4 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 4 |
| O | NU-AVE | 121 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 1 | 1 | 1 | 1 | 1 | 16 | 76 | 14 | 15 | 9 | 17 |
| O | (N,2N) | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| NA | CAPTU | -50 | 0 | -1 | -2 | -5 | -16 | -14 | -3 | 0 | -4 | -2 | -1 | -1 | -1 | 0 | 0 | 0 | 0 | 0 |
| NA | ELASTI | -150 | -3 | -3 | -3 | -32 | -32 | -8 | -2 | -33 | -41 | -57 | -40 | 50 | 39 | 29 | -1 | -9 | -4 | 0 |
| NA | INELAST | 195 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 64 | 48 | 30 | 32 | 15 | 6 |
| NA | NU-AVE | 72 | 0 | 0 | 0 | 2 | 3 | 1 | 1 | 1 | 1 | 1 | 2 | 3 | 12 | 10 | 15 | 14 | 5 | 1 |
| NA | (N,2N) | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| CR | CAPTU | -55 | 0 | 0 | -1 | -3 | -28 | -3 | -14 | -2 | -6 | -2 | -2 | -2 | 0 | 1 | 1 | 1 | 1 | 1 |
| CR | ELASTI | -174 | 0 | 1 | 1 | -1 | -3 | -5 | -34 | -16 | -10 | -16 | -37 | -3 | -16 | -9 | -11 | -11 | -4 | 0 |
| CR | INELAST | 128 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 1 | 5 | 43 | 50 | 21 | 8 |
| CR | NU-AVE | 49 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 2 | 1 | 3 | 3 | 10 | 17 | 10 |
| CR | (N,2N) | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| MN | CAPTU | -50 | 0 | 0 | -24 | -2 | -18 | -1 | -2 | -1 | -1 | -1 | -1 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| MN | ELASTI | -32 | 0 | 0 | 0 | 0 | -1 | -6 | -4 | -4 | -3 | -5 | -3 | -2 | 0 | -1 | -1 | -1 | -1 | 0 |
| MN | INELAST | 16 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 1 | 2 | 1 | 4 | 5 | 2 |
| MN | NU-AVE | 3 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 1 | 1 | 1 | 0 |
| MN | (N,2N) | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| FE | CAPTU | -176 | 0 | -2 | -5 | -8 | -121 | -1 | -14 | -16 | -25 | -11 | -7 | 2 | 7 | 3 | 3 | 7 | 7 | 5 |
| FE | ELASTI | -474 | 4 | 6 | 7 | -18 | -23 | -7 | -49 | -53 | -106 | -69 | -35 | -3 | -21 | -19 | -39 | -42 | -15 | -2 |
| FE | INELAST | 568 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | -5 | 0 | 0 | 1 | 4 | 112 | 199 | 144 | 85 | 28 |
| FE | NU-AVE | 165 | 0 | 0 | 0 | 0 | 0 | 1 | 0 | 1 | 0 | 2 | 2 | 4 | 8 | 17 | 13 | 31 | 45 | 31 |
| FE | (N,2N) | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Ni | CAPTU | -3 | 0 | -1 | -1 | -3 | -5 | -2 | -4 | -22 | -11 | -5 | -3 | 1 | 3 | 2 | 5 | 17 | 19 | 7 |
| Ni | ELASTI | -240 | 1 | 2 | 2 | -7 | -11 | -4 | -17 | -68 | -39 | -25 | -17 | -16 | -13 | -7 | -9 | -3 | 0 | 0 |
| Ni | INELAST | 75 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 26 | 33 | 12 | 4 | 4 |
| Ni | NU-AVE | 38 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 1 | 1 | 1 | 3 | 4 | 3 | 7 | 9 | 6 | 2 | 2 |
| Ni | (N,2N) | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Mo | CAPTU | -73 | 0 | -2 | -8 | -19 | -17 | -4 | -8 | -8 | -7 | -3 | -1 | 0 | 2 | 1 | 1 | 0 | 0 | 0 |
| Mo | ELASTI | -21 | 0 | 0 | 0 | 0 | -1 | 0 | -1 | -2 | -2 | -3 | -3 | -3 | -1 | -1 | -1 | 0 | 0 | 0 |
| Mo | INELAST | 34 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 2 | 6 | 11 | 10 | 4 | 1 | 1 |
| Mo | NU-AVE | 7 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 1 | 2 | 1 | 1 | 0 | 0 | 0 |
| Mo | (N,2N) | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |

表B-4(3/4) 制御棒価値に対する感度係数 (198体炉心 CR-4 1E-2 xycal)

| 項目 | level | total | 群数 | | | | | | | | | | | | | | | | | | (1E-4Δk/kk' / Δσ/σ) | | | | | |
|-----------------|-------|-------|----|----|----|----|----|----|----|----|----|----|---|----|-----|----|-----|-----|-----|-----|---------------------|----|----|--|--|--|
| | | | 18 | 17 | 16 | 15 | 14 | 13 | 12 | 11 | 10 | 9 | 8 | 7 | 6 | 5 | 4 | 3 | 2 | 1 | | | | | | |
| U-238 INELASTIC | 1 | -31 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | -6 | 7 | 13 | -11 | -9 | -10 | -10 | -4 | -1 | | | | | | |
| U-238 | 2 | 3 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 2 | 3 | 1 | 0 | -2 | -1 | 0 | | | | | | |
| U-238 | 3 | 1 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 1 | 0 | 0 | 0 | | | | | | |
| U-238 | 4 | 47 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 13 | 24 | 10 | 0 | 0 | 0 | | | | | | |
| U-238 | 5 | 26 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 4 | 14 | 8 | 0 | 0 | 0 | | | | | | |
| U-238 | 6 | 3 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 2 | 0 | 0 | 0 | | | | | | |
| U-238 | 7 | 11 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 1 | 0 | 0 | 0 | | | | | | |
| U-238 | 8 | 21 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 7 | 4 | 0 | 0 | | | | | | |
| U-238 | 9 | 19 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 13 | 8 | 0 | 0 | | | | | | |
| U-238 | 10 | 24 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 11 | 8 | 0 | 0 | | | | | | |
| U-238 | 11 | 10 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 13 | 11 | 0 | 0 | | | | | | |
| U-238 | 12 | 13 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 5 | 5 | 0 | 0 | | | | | | |
| U-238 | 13 | 19 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 6 | 7 | 0 | 0 | | | | | | |
| U-238 | 14 | 8 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 2 | 6 | 0 | 0 | | | | | | |
| U-238 | 15 | 14 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 4 | 9 | 1 | 0 | | | | | | |
| U-238 | 16 | 20 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 6 | 13 | 1 | 0 | | | | | | |
| U-238 | 17 | 13 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 3 | 9 | 1 | 0 | | | | | | |
| U-238 | 18 | 11 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 4 | 7 | 0 | 0 | | | | | | |
| U-238 | 19 | 9 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 2 | 6 | 1 | 0 | | | | | | |
| U-238 | 20 | 11 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 3 | 7 | 1 | 0 | | | | | | |
| U-238 | 21 | 8 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 1 | 6 | 1 | 0 | | | | | | |
| U-238 | 22 | 9 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 2 | 6 | 1 | 0 | | | | | | |
| U-238 | 23 | 12 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 1 | 6 | 0 | | | | | | |
| U-238 | 24 | 4 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 2 | 9 | 1 | 0 | | | | | | |
| U-238 | 25 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 3 | 0 | 0 | | | | | | |
| U-238 | 26 | 7 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 1 | 6 | 0 | 0 | | | | | | |
| U-238 | 27 | 1 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 1 | 0 | 0 | | | | | | |
| U-238 | 28 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | | | | | | |
| U-238 | 29 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | | | | | | |
| U-238 | 30 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | | | | | | |
| U-238 | 31 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | | | | | | |
| U-238 | 32 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | | | | | | |
| U-238 | 33 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | | | | | | |
| U-238 | 34 | 466 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | -6 | 7 | 15 | 9 | 124 | 283 | 246 | 70 | 11 | | | |
| | total | 759 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | -6 | 7 | 15 | 9 | 124 | 283 | 246 | 70 | 11 | | | | |

表B-4(4/4) 制御棒価値に対する感度係数 (198体炉心 CR-4 1E-2 xycal)

(1E-4 $\Delta k/kk' / \Delta\sigma/\sigma$)

| 項目 | #ペイ | 群数 | | | | | | | | | | | | | | | | | | (1E-4 $\Delta k/kk' / \Delta\sigma/\sigma$) |
|------------------|-------|-------|----|----|----|----|----|----|----|----|----|----|----|-----|-----|-----|------|------|------|--|
| | | total | 18 | 17 | 16 | 15 | 14 | 13 | 12 | 11 | 10 | 9 | 8 | 7 | 6 | 5 | 4 | 3 | 2 | |
| FISSION SPECTRUM | -1 | -93 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 2 | 10 | 33 | 98 | 257 | 507 | 365 | -249 | -635 | -336 | -145 |
| FISSION | -0.9 | -82 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 2 | 10 | 33 | 97 | 256 | 498 | 357 | -242 | -618 | -331 | -144 |
| FISSION | -0.8 | -71 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 2 | 10 | 33 | 97 | 254 | 490 | 350 | -235 | -601 | -327 | -144 |
| FISSION | -0.7 | -58 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 2 | 10 | 33 | 97 | 253 | 483 | 343 | -228 | -585 | -322 | -144 |
| FISSION | -0.6 | -49 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 2 | 10 | 33 | 97 | 251 | 475 | 336 | -222 | -570 | -318 | -143 |
| FISSION | -0.5 | -39 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 2 | 10 | 33 | 97 | 250 | 468 | 330 | -216 | -556 | -314 | -143 |
| FISSION | -0.4 | -30 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 2 | 10 | 33 | 96 | 249 | 461 | 324 | -211 | -542 | -310 | -142 |
| FISSION | -0.3 | -22 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 2 | 10 | 33 | 96 | 247 | 454 | 318 | -205 | -529 | -306 | -142 |
| FISSION | -0.2 | -16 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 2 | 10 | 32 | 96 | 246 | 448 | 312 | -200 | -517 | -303 | -142 |
| FISSION | -0.1 | -7 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 2 | 10 | 32 | 96 | 245 | 441 | 307 | -195 | -505 | -299 | -141 |
| FISSION | -0.05 | -4 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 2 | 10 | 32 | 96 | 244 | 438 | 304 | -193 | -499 | -297 | -141 |
| FISSION | 0.05 | 2 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 2 | 10 | 32 | 96 | 243 | 432 | 299 | -189 | -488 | -294 | -141 |
| FISSION | 0.1 | 6 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 2 | 10 | 32 | 96 | 242 | 429 | 296 | -186 | -483 | -292 | -140 |
| FISSION | 0.2 | 11 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 2 | 10 | 32 | 95 | 241 | 423 | 291 | -182 | -473 | -288 | -140 |
| FISSION | 0.3 | 17 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 2 | 10 | 32 | 95 | 239 | 418 | 287 | -178 | -463 | -285 | -140 |
| FISSION | 0.4 | 23 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 2 | 10 | 32 | 95 | 238 | 412 | 282 | -174 | -453 | -282 | -139 |
| FISSION | 0.5 | 27 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 2 | 10 | 32 | 95 | 237 | 407 | 277 | -171 | -444 | -279 | -139 |
| FISSION | 0.6 | 32 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 2 | 10 | 32 | 95 | 236 | 401 | 273 | -167 | -436 | -275 | -139 |
| FISSION | 0.7 | 38 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 2 | 10 | 32 | 95 | 235 | 396 | 269 | -164 | -427 | -272 | -138 |
| FISSION | 0.8 | 40 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 2 | 10 | 32 | 94 | 233 | 391 | 265 | -161 | -419 | -269 | -138 |
| FISSION | 0.9 | 45 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 2 | 10 | 32 | 94 | 232 | 386 | 261 | -158 | -411 | -266 | -137 |
| FISSION | 1 | 48 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 2 | 10 | 32 | 94 | 231 | 382 | 257 | -155 | -404 | -264 | -137 |

表B-5(1/4) 制御棒価値に対する感度係数 (198体炉心 CR-10 1E-2 xycal)

(1E-4Δk/kk' / Δσ/σ)

| 核種 | reaction | 群数 | | | | | | | | | | | | | | | | (1E-4Δk/kk' / Δσ/σ) | | | | | | | | | |
|--------|----------|-------|----|-----|-----|------|------|-----|------|------|------|------|-------|-------|-------|------|------|---------------------|------|------|---|--|--|--|--|--|--|
| | | total | 18 | 17 | 16 | 15 | 14 | 13 | 12 | 11 | 10 | 9 | 8 | 7 | 6 | 5 | 4 | 3 | 2 | 1 | | | | | | | |
| U-235 | CAPTURE | -5 | 0 | 0 | -1 | -1 | -1 | 0 | 0 | -1 | -1 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | | | | | | | |
| | NU | -62 | 0 | 1 | 2 | 5 | 3 | -1 | -2 | -4 | -7 | -11 | -13 | -12 | -10 | -5 | -4 | -3 | -1 | 0 | | | | | | | |
| | FISSION | -71 | 0 | 0 | 1 | 2 | 0 | -1 | -3 | -5 | -8 | -12 | -13 | -12 | -9 | -4 | -4 | -2 | -1 | 0 | | | | | | | |
| | ELASTIC | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | | | | | | | |
| | INELASTC | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | | | | | | | |
| | MU-AVE | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | | | | | | | |
| | (N,2N) | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | | | | | | | |
| U-238 | CAPTURE | -1088 | -5 | -31 | -77 | -236 | -251 | -53 | -125 | -169 | -163 | -82 | -24 | 22 | 50 | 34 | 16 | 5 | 1 | 0 | | | | | | | |
| | NU | -1855 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | -1 | -5 | -62 | -736 | -642 | -296 | -113 | | | | | | | |
| | FISSION | -1493 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | -1 | -5 | -53 | -597 | -508 | -239 | -90 | | | | | | | |
| | ELASTIC | -168 | 1 | 5 | 6 | 9 | 4 | -5 | -16 | -25 | -34 | -35 | -25 | -21 | -15 | -5 | -5 | -2 | 0 | 0 | | | | | | | |
| | INELASTC | 963 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | -10 | 7 | 26 | 47 | 163 | 339 | 292 | 85 | 14 | | | | | | | |
| | MU-AVE | 88 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 1 | 2 | 4 | 10 | 14 | 8 | 14 | 20 | 12 | 3 | | | | | | |
| | (N,2N) | -1 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | -1 | | | | | | | |
| Pu-238 | CAPTURE | -16 | 0 | -1 | -2 | -4 | -4 | -1 | -1 | -1 | -1 | -1 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | | | | | | | |
| | NU | -98 | 0 | 1 | 3 | 3 | 2 | 0 | 0 | -1 | -4 | -6 | -9 | -16 | -26 | -16 | -14 | -10 | -4 | -1 | | | | | | | |
| | FISSION | -101 | 0 | 0 | 2 | 2 | 1 | 0 | -1 | -2 | -5 | -7 | -10 | -16 | -24 | -15 | -12 | -9 | -4 | -1 | | | | | | | |
| | ELASTIC | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | | | | | | | |
| | INELASTC | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | | | | | | | |
| | MU-AVE | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | | | | | | | |
| | (N,2N) | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | | | | | | | |
| PU-239 | CAPTURE | -697 | -7 | -25 | -85 | -163 | -172 | -35 | -64 | -61 | -50 | -29 | -15 | 1 | 5 | 2 | 1 | 0 | 0 | 0 | | | | | | | |
| | NU | -6120 | 32 | 97 | 233 | 462 | 348 | -17 | -40 | -150 | -423 | -811 | -1124 | -1327 | -1351 | -706 | -665 | -448 | -180 | -50 | | | | | | | |
| | FISSION | -6934 | 17 | 56 | 138 | 254 | 134 | -55 | -129 | -273 | -571 | -938 | -1212 | -1322 | -1266 | -627 | -568 | -377 | -153 | -42 | | | | | | | |
| | ELASTIC | -15 | 0 | 1 | 1 | 2 | 1 | -1 | -2 | -3 | -4 | -4 | -2 | -2 | -1 | 0 | -1 | 0 | 0 | 0 | | | | | | | |
| | INELASTC | 85 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | -3 | -2 | -1 | 1 | 3 | 16 | 15 | 25 | 21 | 9 | 1 | | | | | | | |
| | MU-AVE | 7 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 1 | 1 | 1 | 2 | 1 | 0 | 0 | | | | | | | |
| | (N,2N) | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | | | | | | | |
| PU-240 | CAPTURE | -264 | -4 | -15 | -29 | -57 | -57 | -10 | -22 | -27 | -28 | -17 | -7 | 1 | 3 | 2 | 2 | 1 | 0 | 0 | | | | | | | |
| | NU | -939 | 0 | 0 | 0 | 8 | 6 | 0 | -1 | -3 | -10 | -17 | -21 | -38 | -199 | -222 | -211 | -151 | -62 | -18 | | | | | | | |
| | FISSION | -848 | 0 | 0 | 0 | 4 | 2 | 0 | -2 | -5 | -13 | -20 | -22 | -38 | -186 | -196 | -179 | -126 | -52 | -15 | | | | | | | |
| | ELASTIC | -6 | 0 | 0 | 1 | 1 | 1 | 0 | -1 | -2 | -2 | -1 | -1 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | | | | | | | |
| | INELASTC | 38 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 1 | 2 | 4 | 6 | 12 | 10 | 3 | 1 | | | | | | | |
| | MU-AVE | 3 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 1 | 1 | 0 | 0 | 1 | 0 | 0 | | | | | | | |
| | (N,2N) | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | | | | | | | |
| PU-241 | CAPTURE | -59 | -1 | -2 | -7 | -13 | -14 | -2 | -5 | -6 | -6 | -4 | -2 | 0 | 1 | 1 | 1 | 0 | 0 | 0 | | | | | | | |
| | NU | -721 | 5 | 19 | 57 | 94 | 81 | -4 | -9 | -31 | -80 | -137 | -177 | -180 | -150 | -74 | -69 | -44 | -17 | -5 | | | | | | | |
| | FISSION | -927 | 2 | 11 | 35 | 52 | 32 | -13 | -29 | -58 | -108 | -159 | -191 | -179 | -141 | -66 | -59 | -37 | -15 | -4 | | | | | | | |
| | ELASTIC | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | | | | | | | |
| | INELASTC | 9 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 1 | 1 | 3 | 3 | 1 | 0 | | | | | | | |
| | MU-AVE | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | | | | | | | |
| | (N,2N) | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | | | | | | | |
| PU-242 | CAPTURE | -33 | 0 | -1 | -3 | -7 | -7 | -2 | -3 | -4 | -4 | -2 | -1 | 0 | 1 | 0 | 0 | 0 | 0 | 0 | | | | | | | |
| | NU | -119 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | -1 | -3 | -21 | -34 | -29 | -20 | -8 | -3 | | | | | | | |
| | FISSION | -105 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | -1 | -3 | -20 | -30 | -25 | -17 | -7 | -2 | | | | | | | |
| | ELASTIC | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | | | | | | | |
| | INELASTC | 7 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 1 | 1 | 2 | 2 | 1 | 0 | | | | | | | |
| | MU-AVE | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | | | | | | | |
| | (N,2N) | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | | | | | | | |

表B-5(2/4) 制御棒価値に対する感度係数(198体炉心 CR-10 1E-2 xycal)

(1E-4Δk/kk' / Δσ/σ)

| 核種 | reaction | 群数 | | | | | | | | | | | | | | | | | | | |
|--------|----------|-------|----|----|-----|-----|-----|-----|-----|-----|------|------|------|-----|-----|-----|-----|-----|-----|----|---|
| | | total | 18 | 17 | 16 | 15 | 14 | 13 | 12 | 11 | 10 | 9 | 8 | 7 | 6 | 5 | 4 | 3 | 2 | 1 | |
| AM-241 | CAPTURE | -56 | -1 | -3 | -6 | -14 | -14 | -2 | -4 | -5 | -5 | -3 | -1 | 1 | 1 | 0 | 0 | 0 | 0 | 0 | |
| AM-241 | NU | -84 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | -1 | -1 | -8 | -22 | -25 | -18 | -7 | -2 | |
| AM-241 | FISSION | -73 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | -1 | -1 | -7 | -19 | -22 | -15 | -6 | -2 | |
| AM-241 | ELASTIC | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | |
| AM-241 | INELASTC | 4 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | |
| AM-241 | MU-AVE | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 1 | 1 | 1 | 0 | 0 | 0 | |
| AM-241 | (N,2N) | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | |
| B-10 | CAPTU | 5883 | 2 | 6 | 24 | 110 | 246 | 96 | 292 | 571 | 866 | 1074 | 1111 | 764 | 430 | 84 | 124 | 54 | 24 | 5 | |
| B-10 | ELASTI | 230 | 0 | 0 | 0 | -1 | -2 | -1 | 2 | 10 | 20 | 32 | 42 | 51 | 48 | 15 | 11 | 4 | -1 | 0 | |
| B-10 | INELAST | 9 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 2 | 3 | 2 | 1 | 1 | |
| B-10 | MU-AVE | 4 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 1 | 1 | 0 | 0 | 0 | 0 | 0 | |
| B-10 | (N,2N) | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | |
| B-11 | CAPTU | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | |
| B-11 | ELASTI | 398 | 0 | 0 | 0 | -1 | -3 | -7 | -3 | 5 | 27 | 52 | 77 | 79 | 67 | 65 | 12 | 24 | 5 | -1 | 0 |
| B-11 | INELAST | 3 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 1 | 1 | 1 | |
| B-11 | MU-AVE | 9 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 1 | 1 | 1 | 1 | 1 | 2 | 0 | 0 | 1 | 0 | |
| B-11 | (N,2N) | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | |
| C | CAPTU | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | |
| C | ELASTI | 151 | 0 | 0 | 0 | 0 | -1 | -3 | -1 | 2 | 10 | 20 | 29 | 31 | 27 | 21 | 7 | 8 | 2 | -1 | 0 |
| C | INELAST | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | |
| C | MU-AVE | 3 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 1 | 1 | 0 | 0 | 0 | 0 | 0 | |
| C | (N,2N) | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | |
| O | CAPTU | 17 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 11 | 6 | |
| O | ELASTI | 375 | 1 | 4 | 8 | 2 | 2 | -1 | -35 | -86 | -101 | -71 | 16 | 108 | 325 | 110 | 97 | -1 | -5 | 2 | |
| O | INELAST | 4 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 4 | 0 | |
| O | MU-AVE | 27 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 1 | 1 | 1 | 1 | 16 | 3 | 3 | 2 | 4 | 1 | |
| O | (N,2N) | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | |
| NA | CAPTU | -30 | 0 | 0 | -1 | -4 | -11 | -9 | -2 | 0 | -2 | -1 | -1 | 0 | 0 | 0 | 0 | 0 | 0 | 1 | |
| NA | ELASTI | 92 | -3 | -5 | -6 | -37 | -46 | -24 | -10 | -28 | -23 | -14 | 10 | 100 | 90 | 54 | 29 | 6 | -2 | 1 | |
| NA | INELAST | 286 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 83 | 59 | 58 | 55 | 23 | 8 | |
| NA | MU-AVE | 44 | 0 | 0 | 0 | 2 | 3 | 1 | 1 | 1 | 1 | 1 | 1 | 2 | 7 | 5 | 8 | 7 | 3 | 1 | |
| NA | (N,2N) | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | |
| CR | CAPTU | -28 | 0 | 0 | -1 | -2 | -19 | -2 | -9 | -1 | -3 | -1 | 1 | 2 | 2 | 1 | 1 | 1 | 1 | 1 | |
| CR | ELASTI | -86 | 0 | 0 | 0 | -2 | -4 | -5 | -36 | -16 | -9 | -11 | -20 | 10 | 2 | 4 | 5 | -2 | -2 | 0 | |
| CR | INELAST | 154 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 2 | 6 | 50 | 60 | 27 | 9 | |
| CR | MU-AVE | 21 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 1 | 1 | 1 | 1 | 4 | 7 | 4 | 2 | |
| CR | (N,2N) | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | |
| MN | CAPTU | -34 | 0 | 0 | -17 | -1 | -12 | -1 | -1 | -1 | -1 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | |
| MN | ELASTI | -27 | 0 | 0 | -4 | -1 | -7 | -5 | -4 | -3 | -4 | -1 | 0 | 1 | 1 | 0 | 0 | 0 | 0 | 0 | |
| MN | INELAST | 19 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 1 | 2 | 1 | 5 | 6 | 3 | |
| MN | MU-AVE | 1 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 1 | 0 | 0 | |
| MN | (N,2N) | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | |
| FE | CAPTU | -76 | 0 | -1 | -3 | -6 | -83 | -1 | -9 | -9 | -13 | -3 | 2 | 8 | 12 | 4 | 4 | 8 | 8 | 6 | |
| FE | ELASTI | -201 | 0 | 1 | 0 | -25 | -30 | -7 | -50 | -51 | -90 | -35 | 5 | 40 | 39 | 14 | 5 | -11 | -6 | 0 | |
| FE | INELAST | 692 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | -4 | 1 | 0 | 1 | 4 | 134 | 235 | 184 | 106 | 31 | |
| FE | MU-AVE | 75 | 0 | 0 | 0 | 0 | 0 | 0 | 1 | 0 | 2 | 1 | 3 | 5 | 8 | 5 | 12 | 19 | 14 | 5 | |
| FE | (N,2N) | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | |
| Ni | CAPTU | 40 | 0 | 0 | -1 | -2 | -3 | -1 | -3 | -13 | -5 | -1 | 1 | 4 | 4 | 3 | 7 | 20 | 22 | 8 | |
| Ni | ELASTI | -163 | 0 | 0 | 0 | -9 | -13 | -5 | -19 | -64 | -33 | -17 | -4 | -2 | 0 | 3 | 3 | -2 | -1 | 0 | |
| Ni | INELAST | 90 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 1 | 31 | 39 | 15 | 4 | |
| Ni | MU-AVE | 20 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 1 | 1 | 1 | 2 | 2 | 1 | 3 | 4 | 3 | 1 | 0 | |
| Ni | (N,2N) | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | |
| Mo | CAPTU | -42 | -1 | -2 | -6 | -13 | -12 | -2 | -5 | -5 | -3 | -1 | 1 | 2 | 3 | 1 | 1 | 0 | 0 | 0 | |
| Mo | ELASTI | -13 | 0 | 0 | 0 | -1 | -1 | 0 | -1 | -2 | -2 | -2 | -1 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | |
| Mo | INELAST | 39 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 2 | 7 | 13 | 12 | 4 | 1 | |
| Mo | MU-AVE | 4 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 1 | 1 | 1 | 0 | 0 | 0 | 0 | |
| Mo | (N,2N) | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | |

表B-5(3/4) 制御棒価値に対する感度係数(198体炉心 CR-10 1E-2 xycal)

| 項目 | level | total | 群数 | | | | | | | | | | | | | | | | (1E-4Δk/kk ³ / Δσ/σ) | | | | |
|-----------------|-------|-------|----|----|----|----|----|----|----|----|----|-----|---|----|----|-----|-----|-----|---------------------------------|----|---|---|---|
| | | | 18 | 17 | 16 | 15 | 14 | 13 | 12 | 11 | 10 | 9 | 8 | 7 | 6 | 5 | 4 | 3 | 2 | 1 | | | |
| U-238 INELASTIC | 1 | 43 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | -10 | 7 | 24 | 20 | 4 | 1 | -2 | -1 | 0 | 0 | 0 | 0 |
| U-238 | 2 | 20 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 2 | 8 | 6 | 4 | 0 | 0 | 0 | 0 | 0 | 0 |
| U-238 | 3 | 3 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 1 | 2 | 0 | 0 | 0 | 0 | 0 | 0 |
| U-238 | 4 | 54 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 14 | 27 | 12 | 1 | 0 | 0 | 0 | 0 | 0 |
| U-238 | 5 | 30 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 4 | 16 | 9 | 1 | 0 | 0 | 0 | 0 | 0 |
| U-238 | 6 | 4 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 1 | 3 | 0 | 0 | 0 | 0 | 0 |
| U-238 | 7 | 13 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 8 | 5 | 0 | 0 | 0 | 0 | 0 |
| U-238 | 8 | 24 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 15 | 9 | 0 | 0 | 0 | 0 | 0 |
| U-238 | 9 | 22 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 13 | 9 | 0 | 0 | 0 | 0 | 0 |
| U-238 | 10 | 28 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 14 | 13 | 1 | 0 | 0 | 0 | 0 |
| U-238 | 11 | 12 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 5 | 6 | 1 | 0 | 0 | 0 | 0 |
| U-238 | 12 | 16 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 7 | 8 | 1 | 0 | 0 | 0 | 0 |
| U-238 | 13 | 22 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 8 | 13 | 1 | 0 | 0 | 0 | 0 |
| U-238 | 14 | 11 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 3 | 7 | 1 | 0 | 0 | 0 | 0 |
| U-238 | 15 | 16 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 5 | 10 | 1 | 0 | 0 | 0 | 0 |
| U-238 | 16 | 23 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 6 | 15 | 2 | 0 | 0 | 0 | 0 |
| U-238 | 17 | 15 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 4 | 10 | 1 | 0 | 0 | 0 | 0 |
| U-238 | 18 | 12 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 4 | 8 | 0 | 0 | 0 | 0 | 0 |
| U-238 | 19 | 10 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 2 | 7 | 1 | 0 | 0 | 0 | 0 |
| U-238 | 20 | 13 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 4 | 8 | 1 | 0 | 0 | 0 | 0 |
| U-238 | 21 | 10 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 2 | 7 | 1 | 0 | 0 | 0 | 0 |
| U-238 | 22 | 11 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 3 | 7 | 1 | 0 | 0 | 0 | 0 |
| U-238 | 23 | 14 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 3 | 10 | 1 | 0 | 0 | 0 | 0 |
| U-238 | 24 | 5 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 1 | 4 | 0 | 0 | 0 | 0 | 0 |
| U-238 | 25 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| U-238 | 26 | 9 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 2 | 6 | 1 | 0 | 0 | 0 | 0 |
| U-238 | 27 | 1 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 1 | 0 | 0 | 0 | 0 | 0 |
| U-238 | 28 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| U-238 | 29 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| U-238 | 30 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| U-238 | 31 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| U-238 | 32 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| U-238 | 33 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| U-238 | 34 | 523 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 145 | 277 | 87 | 14 | 0 | 0 | 0 |
| | total | 964 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | -10 | 7 | 26 | 46 | 164 | 339 | 292 | 86 | 14 | | | |

表B-5(4/4) 制御棒価値に対する感度係数(198体炉心 CR-10 1E-2 xycal)

(1E-4 $\Delta k/kk'$ / $\Delta \sigma/\sigma$)

| 項目 | サペイ | 群数 | | | | | | | | | | | | | | | | | | | |
|------------------|-------|-------|----|----|----|----|----|----|----|----|----|----|-----|-----|-----|-----|------|------|------|------|--|
| | | total | 18 | 17 | 16 | 15 | 14 | 13 | 12 | 11 | 10 | 9 | 8 | 7 | 6 | 5 | 4 | 3 | 2 | 1 | |
| FISSION SPECTRUM | -1 | -105 | 0 | 0 | 0 | 0 | 0 | 0 | 1 | 4 | 13 | 40 | 111 | 277 | 508 | 373 | -265 | -668 | -355 | -144 | |
| FISSION | -0.9 | -89 | 0 | 0 | 0 | 0 | 0 | 0 | 1 | 4 | 13 | 40 | 111 | 275 | 500 | 366 | -257 | -649 | -350 | -143 | |
| FISSION | -0.8 | -78 | 0 | 0 | 0 | 0 | 0 | 0 | 1 | 4 | 13 | 40 | 111 | 273 | 492 | 358 | -250 | -632 | -345 | -143 | |
| FISSION | -0.7 | -66 | 0 | 0 | 0 | 0 | 0 | 0 | 1 | 4 | 13 | 40 | 110 | 272 | 484 | 351 | -243 | -615 | -341 | -142 | |
| FISSION | -0.6 | -53 | 0 | 0 | 0 | 0 | 0 | 0 | 1 | 4 | 13 | 40 | 110 | 270 | 477 | 345 | -236 | -599 | -336 | -142 | |
| FISSION | -0.5 | -44 | 0 | 0 | 0 | 0 | 0 | 0 | 1 | 4 | 13 | 40 | 110 | 269 | 469 | 338 | -230 | -584 | -332 | -142 | |
| FISSION | -0.4 | -34 | 0 | 0 | 0 | 0 | 0 | 0 | 1 | 4 | 13 | 40 | 110 | 267 | 462 | 332 | -224 | -570 | -328 | -141 | |
| FISSION | -0.3 | -23 | 0 | 0 | 0 | 0 | 0 | 0 | 1 | 4 | 13 | 40 | 110 | 266 | 456 | 326 | -218 | -556 | -324 | -141 | |
| FISSION | -0.2 | -15 | 0 | 0 | 0 | 0 | 0 | 0 | 1 | 4 | 13 | 40 | 109 | 265 | 449 | 320 | -213 | -543 | -320 | -140 | |
| FISSION | -0.1 | -8 | 0 | 0 | 0 | 0 | 0 | 0 | 1 | 4 | 13 | 40 | 109 | 263 | 443 | 314 | -208 | -531 | -316 | -140 | |
| FISSION | -0.05 | -5 | 0 | 0 | 0 | 0 | 0 | 0 | 1 | 4 | 13 | 40 | 109 | 262 | 439 | 311 | -205 | -525 | -314 | -140 | |
| FISSION | 0.05 | 3 | 0 | 0 | 0 | 0 | 0 | 0 | 1 | 4 | 13 | 40 | 109 | 261 | 433 | 306 | -201 | -513 | -310 | -140 | |
| FISSION | 0.1 | 8 | 0 | 0 | 0 | 0 | 0 | 0 | 1 | 4 | 13 | 40 | 109 | 260 | 430 | 304 | -198 | -508 | -308 | -139 | |
| FISSION | 0.2 | 13 | 0 | 0 | 0 | 0 | 0 | 0 | 1 | 4 | 13 | 40 | 109 | 259 | 424 | 298 | -194 | -497 | -305 | -139 | |
| FISSION | 0.3 | 20 | 0 | 0 | 0 | 0 | 0 | 0 | 1 | 4 | 13 | 40 | 108 | 258 | 419 | 294 | -190 | -487 | -301 | -139 | |
| FISSION | 0.4 | 26 | 0 | 0 | 0 | 0 | 0 | 0 | 1 | 4 | 13 | 40 | 108 | 256 | 413 | 289 | -185 | -477 | -298 | -138 | |
| FISSION | 0.5 | 32 | 0 | 0 | 0 | 0 | 0 | 0 | 1 | 4 | 13 | 40 | 108 | 255 | 408 | 284 | -182 | -467 | -294 | -138 | |
| FISSION | 0.6 | 38 | 0 | 0 | 0 | 0 | 0 | 0 | 1 | 4 | 13 | 40 | 108 | 254 | 402 | 280 | -178 | -458 | -291 | -137 | |
| FISSION | 0.7 | 42 | 0 | 0 | 0 | 0 | 0 | 0 | 1 | 4 | 13 | 40 | 108 | 252 | 397 | 275 | -174 | -449 | -288 | -137 | |
| FISSION | 0.8 | 45 | 0 | 0 | 0 | 0 | 0 | 0 | 1 | 4 | 13 | 40 | 107 | 251 | 392 | 271 | -171 | -441 | -285 | -137 | |
| FISSION | 0.9 | 52 | 0 | 0 | 0 | 0 | 0 | 0 | 1 | 4 | 13 | 40 | 107 | 250 | 387 | 267 | -167 | -432 | -282 | -136 | |
| FISSION | 1 | 55 | 0 | 0 | 0 | 0 | 0 | 0 | 1 | 4 | 13 | 40 | 107 | 248 | 383 | 263 | -164 | -425 | -279 | -136 | |

表B-6(1/4) 制御棒価値に対する感度係数(198体炉心 FCR-1 1E-2 xycal)

$$(1E-4 \Delta k / k k' / \Delta \sigma / \sigma)$$

表B-6(2/4) 制御棒価値に対する感度係数(198体炉心 FCR-1 1E-2 xycal)

$$(1E-4 \Delta k / k k' / \Delta \sigma / \sigma)$$

表B-6(3/4) 制御棒価値に対する感度係数(198体炉心 FCR-1 1E-2 xycal)

(1E-4Δk/k' / Δσ/σ)

| 項目 | level | total | 群数 | | | | | | | | | | | | | | | | | |
|-----------------|-------|-------|----|----|----|----|----|----|----|----|----|----|---|----|----|-----|-----|-----|----|----|
| | | | 18 | 17 | 16 | 15 | 14 | 13 | 12 | 11 | 10 | 9 | 8 | 7 | 6 | 5 | 4 | 3 | 2 | 1 |
| U-238 INELASTIC | 1 | 15 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | -8 | 6 | 20 | 9 | -1 | -3 | -5 | -2 | -1 |
| U-238 | 2 | 13 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 2 | 6 | 4 | 3 | -1 | -1 | 0 |
| U-238 | 3 | 2 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 1 | 1 | 0 | 0 | 0 |
| U-238 | 4 | 52 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 14 | 26 | 11 | 1 | 0 | 0 |
| U-238 | 5 | 28 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 4 | 15 | 9 | 0 | 0 | 0 |
| U-238 | 6 | 4 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 1 | 3 | 0 | 0 | 0 |
| U-238 | 7 | 12 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 7 | 5 | 0 | 0 | 0 |
| U-238 | 8 | 23 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 14 | 9 | 0 | 0 | 0 |
| U-238 | 9 | 21 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 12 | 9 | 0 | 0 |
| U-238 | 10 | 27 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 14 | 12 | 1 | 0 |
| U-238 | 11 | 12 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 5 | 6 | 1 | 0 | 0 |
| U-238 | 12 | 16 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 7 | 8 | 1 | 0 | 0 |
| U-238 | 13 | 20 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 7 | 12 | 1 | 0 |
| U-238 | 14 | 10 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 2 | 7 | 1 | 0 | 0 |
| U-238 | 15 | 15 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 4 | 10 | 1 | 0 |
| U-238 | 16 | 22 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 6 | 14 | 2 | 0 | 0 |
| U-238 | 17 | 15 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 4 | 10 | 1 | 0 | 0 |
| U-238 | 18 | 12 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 4 | 8 | 0 | 0 | 0 |
| U-238 | 19 | 9 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 2 | 6 | 1 | 0 | 0 |
| U-238 | 20 | 13 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 4 | 8 | 1 | 0 | 0 |
| U-238 | 21 | 9 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 2 | 6 | 1 | 0 | 0 |
| U-238 | 22 | 11 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 3 | 7 | 1 | 0 | 0 |
| U-238 | 23 | 13 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 2 | 10 | 1 | 0 | 0 |
| U-238 | 24 | 5 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 1 | 4 | 0 | 0 | 0 |
| U-238 | 25 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| U-238 | 26 | 8 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 1 | 6 | 1 | 0 |
| U-238 | 27 | 1 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 1 | 0 | 0 | 0 |
| U-238 | 28 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| U-238 | 29 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| U-238 | 30 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| U-238 | 31 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| U-238 | 32 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| U-238 | 33 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| U-238 | 34 | 498 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 138 | 265 | 82 | 13 |
| | total | 886 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | -8 | 6 | 22 | 33 | 147 | 320 | 275 | 79 | 12 |

表B-6(4/4) 制御棒価値に対する感度係数(198体炉心 FCR-1 1E-2 xycal)

(1E-4Δk/kk' / Δσ/σ)

| 項目 | サベイ | 群数 | | | | | | | | | | | | | | | | | | (1E-4Δk/kk' / Δσ/σ) |
|------------------|-------|-------|----|----|----|----|----|----|----|----|----|----|-----|-----|-----|-----|------|------|------|---------------------|
| | | total | 18 | 17 | 16 | 15 | 14 | 13 | 12 | 11 | 10 | 9 | 8 | 7 | 6 | 5 | 4 | 3 | 2 | |
| FISSION SPECTRUM | -1 | -99 | 0 | 0 | 0 | 0 | 0 | 0 | 1 | 3 | 11 | 36 | 103 | 265 | 503 | 370 | -255 | -649 | -344 | -143 |
| FISSION | -0.9 | -85 | 0 | 0 | 0 | 0 | 0 | 0 | 1 | 3 | 11 | 36 | 103 | 264 | 495 | 362 | -247 | -631 | -339 | -143 |
| FISSION | -0.8 | -73 | 0 | 0 | 0 | 0 | 0 | 0 | 1 | 3 | 11 | 36 | 103 | 262 | 487 | 355 | -240 | -614 | -335 | -142 |
| FISSION | -0.7 | -60 | 0 | 0 | 0 | 0 | 0 | 0 | 1 | 3 | 11 | 36 | 103 | 261 | 480 | 348 | -233 | -598 | -330 | -142 |
| FISSION | -0.6 | -51 | 0 | 0 | 0 | 0 | 0 | 0 | 1 | 3 | 11 | 36 | 103 | 259 | 472 | 341 | -227 | -583 | -326 | -141 |
| FISSION | -0.5 | -40 | 0 | 0 | 0 | 0 | 0 | 0 | 1 | 3 | 11 | 36 | 103 | 258 | 465 | 335 | -221 | -568 | -322 | -141 |
| FISSION | -0.4 | -33 | 0 | 0 | 0 | 0 | 0 | 0 | 1 | 3 | 11 | 36 | 102 | 256 | 458 | 328 | -215 | -554 | -318 | -141 |
| FISSION | -0.3 | -23 | 0 | 0 | 0 | 0 | 0 | 0 | 1 | 3 | 11 | 36 | 102 | 255 | 452 | 322 | -210 | -541 | -314 | -140 |
| FISSION | -0.2 | -14 | 0 | 0 | 0 | 0 | 0 | 0 | 1 | 3 | 11 | 36 | 102 | 254 | 445 | 317 | -205 | -528 | -310 | -140 |
| FISSION | -0.1 | -6 | 0 | 0 | 0 | 0 | 0 | 0 | 1 | 3 | 11 | 36 | 102 | 252 | 439 | 311 | -200 | -516 | -306 | -139 |
| FISSION | -0.05 | -1 | 0 | 0 | 0 | 0 | 0 | 0 | 1 | 3 | 11 | 36 | 102 | 252 | 436 | 308 | -197 | -510 | -304 | -139 |
| FISSION | 0.05 | 2 | 0 | 0 | 0 | 0 | 0 | 0 | 1 | 3 | 11 | 36 | 101 | 250 | 429 | 303 | -193 | -499 | -301 | -139 |
| FISSION | 0.1 | 6 | 0 | 0 | 0 | 0 | 0 | 0 | 1 | 3 | 11 | 36 | 101 | 250 | 426 | 300 | -190 | -494 | -299 | -139 |
| FISSION | 0.2 | 13 | 0 | 0 | 0 | 0 | 0 | 0 | 1 | 3 | 11 | 36 | 101 | 248 | 421 | 295 | -186 | -483 | -296 | -138 |
| FISSION | 0.3 | 20 | 0 | 0 | 0 | 0 | 0 | 0 | 1 | 3 | 11 | 36 | 101 | 247 | 415 | 291 | -182 | -473 | -292 | -138 |
| FISSION | 0.4 | 26 | 0 | 0 | 0 | 0 | 0 | 0 | 1 | 3 | 11 | 36 | 101 | 246 | 409 | 286 | -178 | -463 | -289 | -137 |
| FISSION | 0.5 | 31 | 0 | 0 | 0 | 0 | 0 | 0 | 1 | 3 | 11 | 36 | 101 | 244 | 404 | 281 | -174 | -454 | -285 | -137 |
| FISSION | 0.6 | 35 | 0 | 0 | 0 | 0 | 0 | 0 | 1 | 3 | 11 | 36 | 100 | 243 | 399 | 277 | -171 | -445 | -282 | -137 |
| FISSION | 0.7 | 41 | 0 | 0 | 0 | 0 | 0 | 0 | 1 | 3 | 11 | 36 | 100 | 242 | 394 | 273 | -167 | -437 | -279 | -136 |
| FISSION | 0.8 | 45 | 0 | 0 | 0 | 0 | 0 | 0 | 1 | 3 | 11 | 36 | 100 | 241 | 389 | 268 | -164 | -428 | -276 | -136 |
| FISSION | 0.9 | 48 | 0 | 0 | 0 | 0 | 0 | 0 | 1 | 3 | 11 | 36 | 100 | 239 | 384 | 264 | -161 | -420 | -273 | -136 |
| FISSION | 1 | 53 | 0 | 0 | 0 | 0 | 0 | 0 | 1 | 3 | 11 | 36 | 100 | 238 | 379 | 261 | -158 | -413 | -270 | -135 |

表B-7(1/4) 制御棒価値に対する感度係数(198体炉心 B C R -3 1E-2 xycal)

(1E-4Δk/k' / Δσ/σ)

| 核種 | reaction | 群数 | | | | | | | | | | | | | | | | | | |
|--------|-----------|-------|----|-----|-----|------|------|-----|-----|------|------|------|-------|-------|-------|------|------|------|------|------|
| | | total | 18 | 17 | 16 | 15 | 14 | 13 | 12 | 11 | 10 | 9 | 8 | 7 | 6 | 5 | 4 | 3 | 2 | 1 |
| U-235 | CAPTURE | -2 | 0 | 0 | 0 | -1 | -1 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| | NU | -81 | -3 | -2 | -2 | 1 | 0 | -2 | -3 | -4 | -7 | -10 | -12 | -12 | -11 | -5 | -5 | -3 | -1 | 0 |
| | FISSION | -87 | -3 | -2 | -2 | -2 | -3 | -2 | -3 | -5 | -8 | -11 | -12 | -12 | -10 | -4 | -4 | -3 | -1 | 0 |
| | ELASTIC | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| | INELASTIC | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| | MU-AVE | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| | (N,2N) | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| U-238 | CAPTURE | -823 | 4 | -18 | -57 | -182 | -194 | -42 | -99 | -129 | -123 | -65 | -19 | 16 | 39 | 27 | 13 | 5 | 1 | 0 |
| | NU | -1870 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | -1 | -5 | -59 | -722 | -660 | -306 | -117 |
| | FISSION | -1542 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | -1 | -5 | -52 | -603 | -533 | -252 | -96 |
| | ELASTIC | -987 | 6 | 14 | 14 | 25 | 18 | -6 | -20 | -51 | -110 | -188 | -225 | -194 | -154 | -44 | -38 | -8 | -2 | 0 |
| | INELASTIC | 283 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | -23 | -39 | -40 | -56 | 25 | 186 | 173 | 48 | 9 |
| | MU-AVE | 491 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 1 | 4 | 13 | 35 | 67 | 102 | 48 | 72 | 87 | 50 | 12 |
| | (N,2N) | -4 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | -4 |
| Pu-238 | CAPTURE | -12 | 0 | -1 | -1 | -3 | -3 | 0 | -1 | -1 | -1 | -1 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| | NU | -101 | 0 | 1 | 3 | 3 | 2 | 0 | 1 | 0 | -2 | -4 | -8 | -15 | -27 | -18 | -17 | -13 | -5 | -2 |
| | FISSION | -94 | 0 | 0 | 2 | 2 | 1 | 0 | 0 | 0 | -2 | -5 | -8 | -14 | -25 | -16 | -14 | -10 | -4 | -1 |
| | ELASTIC | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| | INELASTIC | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| | MU-AVE | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| | (N,2N) | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| PU-239 | CAPTURE | -437 | -8 | -23 | -71 | -117 | -108 | -19 | -34 | -33 | -27 | -14 | -4 | 7 | 8 | 3 | 2 | 1 | 0 | 0 |
| | NU | -6018 | 35 | 92 | 218 | 433 | 367 | 25 | 44 | -17 | -227 | -599 | -1014 | -1329 | -1495 | -830 | -826 | -588 | -240 | -67 |
| | FISSION | -6120 | 17 | 55 | 141 | 285 | 232 | 5 | -3 | -83 | -306 | -662 | -1037 | -1273 | -1362 | -714 | -685 | -478 | -198 | -54 |
| | ELASTIC | -71 | 1 | 1 | 2 | 4 | 3 | -1 | -2 | -6 | -11 | -16 | -16 | -13 | -8 | -3 | -2 | -1 | 0 | 0 |
| | INELASTIC | 17 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | -3 | -3 | -4 | -7 | -6 | -4 | 5 | 16 | 16 | 6 | 1 |
| | MU-AVE | 36 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 1 | 3 | 5 | 6 | 3 | 6 | 7 | 4 | 1 |
| | (N,2N) | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| PU-240 | CAPTURE | -188 | -6 | -15 | -25 | -43 | -40 | -6 | -14 | -17 | -18 | -11 | -4 | 2 | 4 | 2 | 1 | 0 | 0 | 0 |
| | NU | -1048 | 0 | 0 | 0 | 8 | 6 | 0 | 1 | 0 | -4 | -11 | -17 | -35 | -211 | -247 | -249 | -188 | -78 | -23 |
| | FISSION | -913 | 0 | 0 | 0 | 5 | 4 | 0 | 0 | -1 | -6 | -13 | -18 | -34 | -193 | -214 | -207 | -153 | -64 | -19 |
| | ELASTIC | -31 | 1 | 1 | 1 | 2 | 2 | 0 | -1 | -3 | -5 | -8 | -8 | -6 | -4 | -1 | -1 | -1 | 0 | 0 |
| | INELASTIC | 9 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | -3 | -3 | -2 | -2 | 2 | 8 | 7 | 2 | 0 |
| | MU-AVE | 11 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 1 | 1 | 2 | 2 | 1 | 1 | 2 | 1 | 0 |
| | (N,2N) | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| PU-241 | CAPTURE | -31 | -1 | -2 | -5 | -9 | -8 | -1 | -2 | -3 | -3 | -2 | 0 | 1 | 2 | 1 | 1 | 0 | 0 | 0 |
| | NU | -701 | 5 | 17 | 51 | 83 | 79 | 5 | 8 | -7 | -48 | -106 | -166 | -185 | -170 | -89 | -88 | -59 | -24 | -7 |
| | FISSION | -772 | 2 | 10 | 33 | 55 | 49 | 0 | -3 | -20 | -61 | -116 | -168 | -176 | -154 | -77 | -73 | -48 | -19 | -6 |
| | ELASTIC | -9 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | -1 | -2 | -2 | -2 | -1 | 0 | 0 | 0 | 0 | 0 | 0 |
| | INELASTIC | 5 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 2 | 2 | 1 | 0 |
| | MU-AVE | 4 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 1 | 1 | 0 | 1 | 1 | 0 | 0 |
| | (N,2N) | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| PU-242 | CAPTURE | -25 | 0 | -1 | -3 | -5 | -5 | -1 | -2 | -3 | -3 | -2 | -1 | 0 | 1 | 0 | 0 | 0 | 0 | 0 |
| | NU | -134 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | -1 | -3 | -22 | -37 | -34 | -24 | -10 | -3 |
| | FISSION | -115 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | -1 | -3 | -20 | -32 | -28 | -20 | -8 |
| | ELASTIC | -5 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | -1 | -1 | -1 | 0 | 0 | 0 | 0 | 0 |
| | INELASTIC | 1 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 1 | 1 | 0 | 0 |
| | MU-AVE | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| | (N,2N) | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |

表B-7(2/4) 制御棒価値に対する感度係数(198体炉心 BCR-3 1E-2 xycal)

(1E-4Δk/kk' / Δσ/σ)

| 核種 | reaction | 群数 | | | | | | | | | | | | | | | | | | (1E-4Δk/kk' / Δσ/σ) | |
|--------|-----------|-------|----|----|-----|-----|-----|----|-----|------|------|------|------|------|------|-----|-----|-----|-----|---------------------|---|
| | | total | 18 | 17 | 16 | 15 | 14 | 13 | 12 | 11 | 10 | 9 | 8 | 7 | 6 | 5 | 4 | 3 | 2 | | |
| AM-241 | CAPTURE | -104 | -1 | -4 | -8 | -17 | -19 | -4 | -8 | -10 | -12 | -10 | -7 | -3 | -1 | 0 | 0 | 0 | 0 | 0 | |
| AM-241 | NU | -51 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | -4 | -13 | -16 | -12 | -5 | -1 | -1 | |
| AM-241 | FISSION | -50 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | -1 | -4 | -13 | -15 | -11 | -5 | -1 | |
| AM-241 | ELASTIC | -3 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | -1 | -1 | 0 | 0 | 0 | 0 | 0 | 0 | |
| AM-241 | INELASTIC | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | -1 | 0 | 0 | 0 | 0 | 0 | 0 | |
| AM-241 | MU-AVE | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 1 | 0 | 0 | 0 | |
| AM-241 | (N, 2N) | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | |
| B-10 | CAPTU | 2746 | 0 | -2 | -10 | -35 | -53 | -4 | 17 | 115 | 299 | 536 | 678 | 551 | 363 | 83 | 125 | 53 | 25 | 5 | |
| B-10 | ELASTI | 164 | 0 | 0 | -1 | -4 | -1 | -4 | -5 | -4 | 6 | 19 | 44 | 69 | 32 | 11 | 3 | -1 | 0 | 0 | |
| B-10 | INELAST | 13 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 4 | 4 | 3 | 1 | 1 | |
| B-10 | MU-AVE | 17 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 1 | 1 | 2 | 2 | 3 | 4 | 1 | 1 | 1 | 0 | 0 | |
| B-10 | (N, 2N) | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | |
| B-11 | CAPTU | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | |
| B-11 | ELASTI | 117 | 0 | 0 | 0 | 0 | -3 | -8 | -2 | -8 | -12 | -10 | 6 | 22 | 37 | 62 | 16 | 16 | 3 | -2 | 0 |
| B-11 | INELAST | 3 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 1 | 1 | |
| B-11 | MU-AVE | 22 | 0 | 0 | 0 | 0 | 0 | 1 | 0 | 1 | 1 | 2 | 3 | 3 | 2 | 5 | 1 | 1 | 1 | 0 | |
| B-11 | (N, 2N) | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | |
| C | CAPTU | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | |
| C | ELASTI | 21 | 0 | 0 | 0 | 0 | -1 | -2 | -1 | -2 | -4 | -4 | 0 | 4 | 9 | 13 | 7 | 3 | 0 | -1 | 0 |
| C | INELAST | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | |
| C | MU-AVE | 5 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 1 | 1 | 1 | 1 | 0 | 0 | 0 | 0 | 0 | |
| C | (N, 2N) | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | |
| O | CAPTU | 19 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 12 | |
| O | ELASTI | -1446 | 5 | 9 | 17 | 27 | 21 | -8 | -27 | -79 | -170 | -276 | -309 | -304 | -201 | -50 | -8 | -60 | -32 | -1 | |
| O | INELAST | 3 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 3 | |
| O | MU-AVE | 149 | 0 | 0 | 0 | -1 | 0 | 0 | 0 | 0 | 1 | 2 | 3 | -1 | -26 | 111 | 15 | 15 | 10 | 17 | |
| O | (N, 2N) | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | |
| NA | CAPTU | -31 | 0 | -1 | -1 | -3 | -10 | -9 | -2 | 0 | -3 | -1 | -1 | 0 | 0 | 0 | 0 | 0 | 0 | 1 | |
| NA | ELASTI | -1036 | -4 | -2 | 1 | -30 | -26 | -2 | -1 | -73 | -140 | -218 | -230 | -163 | -125 | 9 | -11 | -14 | -7 | 0 | |
| NA | INELAST | 120 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 41 | 28 | 32 | 13 | 6 | |
| NA | MU-AVE | 123 | 0 | 0 | 0 | 2 | 3 | 1 | 1 | 2 | 2 | 3 | 5 | 8 | 27 | 17 | 23 | 20 | 7 | 2 | |
| NA | (N, 2N) | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | |
| CR | CAPTU | -40 | 0 | 0 | -1 | -2 | -17 | -2 | -10 | -1 | -5 | -2 | -2 | -1 | 0 | 0 | 0 | 1 | 1 | 1 | |
| CR | ELASTI | -389 | 1 | 1 | 1 | 1 | 0 | -4 | -34 | -24 | -24 | -42 | -103 | -57 | -51 | -17 | -18 | -13 | -5 | -1 | |
| CR | INELAST | 89 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 2 | 28 | 38 | 15 | 6 | |
| CR | MU-AVE | 63 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 1 | 4 | 3 | 5 | 4 | 13 | 19 | 11 | 3 | |
| CR | (N, 2N) | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | |
| MN | CAPTU | -33 | 0 | 0 | -15 | -1 | -11 | -1 | -2 | -1 | -1 | -1 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | |
| MN | ELASTI | -53 | 0 | 0 | 6 | 1 | -1 | -5 | -4 | -5 | -11 | -13 | -9 | -5 | -4 | -1 | -1 | -1 | 0 | 0 | |
| MN | INELAST | 6 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | -1 | 0 | 0 | 2 | 3 | 1 | 1 | |
| MN | MU-AVE | 5 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 1 | 1 | 1 | 1 | 1 | 0 | |
| MN | (N, 2N) | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | |
| FE | CAPTU | -132 | 0 | -1 | -3 | -5 | -75 | -1 | -10 | -12 | -21 | -12 | -10 | -3 | 2 | 2 | 2 | 5 | 6 | 4 | |
| FE | ELASTI | -1226 | 8 | 11 | 15 | 11 | 5 | -7 | -48 | -79 | -213 | -206 | -218 | -183 | -154 | -40 | -59 | -50 | -17 | -2 | |
| FE | INELAST | 336 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | -1 | -19 | -8 | -3 | -1 | 0 | 42 | 147 | 98 | 60 | 21 | |
| FE | MU-AVE | 219 | 0 | 0 | 0 | 0 | 0 | 0 | 1 | 1 | 4 | 4 | 9 | 17 | 30 | 17 | 38 | 52 | 35 | 11 | |
| FE | (N, 2N) | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | |
| Ni | CAPTU | -9 | 0 | 0 | -1 | -2 | -3 | -1 | -3 | -17 | -9 | -6 | -5 | -1 | 1 | 3 | 13 | 15 | 6 | 6 | |
| Ni | ELASTI | -502 | 2 | 4 | 5 | 3 | 1 | -4 | -17 | -100 | -95 | -79 | -73 | -66 | -40 | -13 | -15 | -11 | -4 | 0 | |
| Ni | INELAST | 52 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 16 | 24 | 9 | 3 | |
| Ni | MU-AVE | 51 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 1 | 2 | 3 | 6 | 7 | 4 | 8 | 10 | 7 | 2 | 0 | |
| Ni | (N, 2N) | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | |
| Mo | CAPTU | -57 | 0 | -1 | -5 | -12 | -11 | -3 | -6 | -6 | -6 | -4 | -2 | -1 | 0 | 0 | 0 | 0 | 0 | 0 | |
| Mo | ELASTI | -49 | 0 | 0 | 0 | 0 | 0 | 0 | -1 | -3 | -5 | -8 | -10 | -9 | -8 | -2 | -2 | -1 | 0 | 0 | |
| Mo | INELAST | 20 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 3 | 7 | 7 | 2 | 1 | |
| Mo | MU-AVE | 13 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 1 | 2 | 4 | 2 | 2 | 1 | 1 | 0 | 0 | |
| Mo | (N, 2N) | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | |

表B-7(3/4) 制御棒価値に対する感度係数 (198体炉心 BCR-3 1E-2 xycal)

(1E-4 $\Delta k/kk'$ / $\Delta\sigma/\sigma$)

| 項目 | level | 群数 | (1E-4 $\Delta k/kk'$ / $\Delta\sigma/\sigma$) | | | | | | | | | | | | | | | | | | |
|-----------------|-------|------|--|----|----|----|----|----|----|----|----|-----|-----|-----|-----|-----|-----|-----|-----|----|----|
| | | | total | 18 | 17 | 16 | 15 | 14 | 13 | 12 | 11 | 10 | 9 | 8 | 7 | 6 | 5 | 4 | 3 | 2 | 1 |
| U-238 INELASTIC | 1 | -193 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | -23 | -39 | -38 | -46 | -15 | -14 | -12 | -5 | -1 | -1 |
| U-238 | 2 | -15 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | -1 | -6 | -2 | -2 | -3 | -1 | -1 | 0 | 0 |
| U-238 | 3 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| U-238 | 4 | 16 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| U-238 | 5 | 11 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | -1 | 6 | 6 | 0 | 0 | 0 |
| U-238 | 6 | 2 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 2 | 2 | 0 | 0 |
| U-238 | 7 | 6 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 4 | 6 | 0 | 0 |
| U-238 | 8 | 10 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| U-238 | 9 | 10 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| U-238 | 10 | 12 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| U-238 | 11 | 5 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 1 | 1 | 0 | 0 |
| U-238 | 12 | 6 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 1 | 1 | 0 | 0 |
| U-238 | 13 | 12 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 2 | 1 | 1 | 0 |
| U-238 | 14 | 6 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 1 | 1 | 0 | 0 |
| U-238 | 15 | 8 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 1 | 1 | 0 | 0 |
| U-238 | 16 | 12 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 2 | 1 | 1 | 0 |
| U-238 | 17 | 9 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 7 | 7 | 0 | 0 |
| U-238 | 18 | 6 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 5 | 5 | 0 | 0 |
| U-238 | 19 | 4 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 4 | 6 | 0 | 0 |
| U-238 | 20 | 7 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 1 | 1 | 0 | 0 |
| U-238 | 21 | 5 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 4 | 5 | 0 | 0 |
| U-238 | 22 | 5 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 6 | 6 | 0 | 0 |
| U-238 | 23 | 7 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 2 | 0 | 0 | 0 |
| U-238 | 24 | 2 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| U-238 | 25 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| U-238 | 26 | 4 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 4 | 0 | 0 | 0 |
| U-238 | 27 | 1 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 1 | 0 | 0 | 0 |
| U-238 | 28 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| U-238 | 29 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| U-238 | 30 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| U-238 | 31 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| U-238 | 32 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| U-238 | 33 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| U-238 | 34 | 325 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 77 | 181 | 57 | 10 |
| | total | 283 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |

表B-7(4/4) 制御棒価値に対する感度係数(198体炉心 BCR-3 1E-2 xycal)

(1E-4△k/kk' / △σ/σ)

| 項目 | サペイ | 群数 | | | | | | | | | | | | | | | | (1E-4△k/kk' / △σ/σ) | | | | | | | |
|------------------|-------|-------|----|----|----|----|----|----|----|----|----|----|----|-----|-----|-----|------|---------------------|------|------|--|--|--|--|--|
| | | total | 18 | 17 | 16 | 15 | 14 | 13 | 12 | 11 | 10 | 9 | 8 | 7 | 6 | 5 | 4 | 3 | 2 | 1 | | | | | |
| FISSION SPECTRUM | -1 | -61 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 2 | 13 | 53 | 183 | 468 | 360 | -174 | -552 | -282 | -132 | | | | | |
| FISSION | -0.9 | -52 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 2 | 12 | 53 | 182 | 461 | 353 | -168 | -537 | -278 | -132 | | | | | |
| FISSION | -0.8 | -45 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 2 | 12 | 53 | 181 | 453 | 346 | -164 | -522 | -275 | -131 | | | | | |
| FISSION | -0.7 | -37 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 2 | 12 | 53 | 180 | 446 | 339 | -159 | -508 | -271 | -131 | | | | | |
| FISSION | -0.6 | -32 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 2 | 12 | 53 | 179 | 439 | 332 | -155 | -495 | -268 | -131 | | | | | |
| FISSION | -0.5 | -24 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 2 | 12 | 53 | 178 | 433 | 326 | -151 | -483 | -264 | -130 | | | | | |
| FISSION | -0.4 | -19 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 2 | 12 | 53 | 177 | 426 | 320 | -147 | -471 | -261 | -130 | | | | | |
| FISSION | -0.3 | -13 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 2 | 12 | 53 | 176 | 420 | 314 | -143 | -460 | -258 | -129 | | | | | |
| FISSION | -0.2 | -6 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 2 | 12 | 53 | 175 | 414 | 309 | -139 | -449 | -254 | -129 | | | | | |
| FISSION | -0.1 | -3 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 2 | 12 | 53 | 174 | 408 | 303 | -136 | -439 | -251 | -129 | | | | | |
| FISSION | -0.05 | -2 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 2 | 12 | 52 | 173 | 405 | 301 | -134 | -434 | -250 | -129 | | | | | |
| FISSION | 0.05 | 3 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 2 | 12 | 52 | 172 | 400 | 295 | -131 | -424 | -247 | -128 | | | | | |
| FISSION | 0.1 | 5 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 2 | 12 | 52 | 172 | 397 | 293 | -130 | -420 | -245 | -128 | | | | | |
| FISSION | 0.2 | 8 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 2 | 12 | 52 | 171 | 391 | 288 | -127 | -411 | -242 | -128 | | | | | |
| FISSION | 0.3 | 12 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 2 | 12 | 52 | 170 | 386 | 283 | -124 | -402 | -240 | -127 | | | | | |
| FISSION | 0.4 | 16 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 2 | 12 | 52 | 169 | 381 | 279 | -121 | -394 | -237 | -127 | | | | | |
| FISSION | 0.5 | 18 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 2 | 12 | 52 | 168 | 376 | 274 | -119 | -386 | -234 | -127 | | | | | |
| FISSION | 0.6 | 22 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 2 | 12 | 52 | 168 | 371 | 270 | -116 | -379 | -232 | -126 | | | | | |
| FISSION | 0.7 | 25 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 2 | 12 | 52 | 167 | 366 | 266 | -114 | -371 | -229 | -126 | | | | | |
| FISSION | 0.8 | 28 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 2 | 12 | 52 | 166 | 362 | 262 | -112 | -364 | -226 | -126 | | | | | |
| FISSION | 0.9 | 29 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 2 | 12 | 52 | 165 | 357 | 258 | -110 | -358 | -224 | -125 | | | | | |
| FISSION | 1 | 30 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 2 | 12 | 51 | 164 | 353 | 254 | -108 | -351 | -222 | -125 | | | | | |

表B-8(1/4) 制御棒価値に対する感度係数(198体炉心 BCR-6 1E-2 xycal)

(1E-4Δk/kk' / Δσ/σ)

| 核種 | reaction | 群数 | | | | | | | | | | | | | | | | | (1E-4Δk/kk' / Δσ/σ) | |
|--------|----------|-------|----|-----|-----|------|------|-----|-----|------|------|------|-------|-------|-------|------|------|------|---------------------|------|
| | | total | 18 | 17 | 16 | 15 | 14 | 13 | 12 | 11 | 10 | 9 | 8 | 7 | 6 | 5 | 4 | 3 | 2 | |
| U-235 | CAPTURE | -2 | 0 | 0 | 0 | -1 | -1 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| | NU | -68 | -1 | -1 | 0 | 2 | 0 | -1 | -2 | -3 | -6 | -9 | -12 | -12 | -10 | -5 | -4 | -3 | -1 | 0 |
| | FISSION | -74 | -1 | -1 | -1 | 0 | -2 | -1 | -3 | -4 | -7 | -10 | -12 | -11 | -9 | -4 | -4 | -3 | -1 | 0 |
| | ELASTIC | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| | INELASTC | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| | MU-AVE | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| U-235 | (N,2N) | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| U-238 | CAPTURE | -596 | -3 | -21 | -50 | -144 | -147 | -31 | -73 | -97 | -92 | -44 | -7 | 22 | 42 | 29 | 14 | 5 | 1 | 0 |
| | NU | -1850 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | -1 | -5 | -59 | -723 | -648 | -300 | -114 |
| | FISSION | -1519 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | -1 | -5 | -52 | -599 | -522 | -247 | -93 |
| | ELASTIC | -729 | 4 | 10 | 10 | 20 | 16 | -6 | -19 | -44 | -90 | -148 | -165 | -140 | -102 | -28 | -24 | -16 | -6 | -1 |
| | INELASTC | 376 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | -24 | -37 | -33 | -34 | 43 | 189 | 208 | 54 | 10 |
| U-238 | MU-AVE | 332 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 1 | 3 | 10 | 25 | 48 | 68 | 31 | 47 | 57 | 34 | 8 |
| | (N,2N) | -2 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | -2 |
| Pu-238 | CAPTURE | -10 | 0 | -1 | -1 | -2 | -2 | 0 | -1 | -1 | -1 | -1 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| | NU | -101 | 0 | 1 | 2 | 2 | 1 | 0 | 0 | -1 | -3 | -5 | -8 | -15 | -26 | -17 | -15 | -11 | -5 | -1 |
| | FISSION | -95 | 0 | 0 | 1 | 1 | 1 | 0 | 0 | -1 | -3 | -5 | -9 | -14 | -24 | -15 | -13 | -9 | -4 | -1 |
| | ELASTIC | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| | INELASTC | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| | MU-AVE | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Pu-238 | (N,2N) | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| PU-239 | CAPTURE | -382 | -8 | -20 | -57 | -95 | -91 | -17 | -32 | -31 | -26 | -15 | -6 | 4 | 6 | 3 | 2 | 1 | 0 | 0 |
| | NU | -6085 | 34 | 74 | 161 | 303 | 226 | -1 | -10 | -85 | -297 | -641 | -1007 | -1259 | -1361 | -733 | -723 | -504 | -205 | -57 |
| | FISSION | -6283 | 16 | 42 | 98 | 182 | 113 | -20 | -55 | -147 | -374 | -707 | -1040 | -1226 | -1266 | -614 | -614 | -420 | -172 | -47 |
| | ELASTIC | -70 | 1 | 1 | 2 | 3 | 3 | -1 | -2 | -6 | -11 | -16 | -16 | -13 | -8 | -2 | -2 | -1 | 0 | 0 |
| | INELASTC | 19 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | -3 | -3 | -4 | -6 | -5 | -2 | 5 | 15 | 15 | 6 | 1 |
| PU-239 | MU-AVE | 33 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 1 | 3 | 5 | 6 | 3 | 5 | 6 | 3 | 1 |
| | (N,2N) | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| PU-240 | CAPTURE | -156 | -5 | -13 | -20 | -34 | -32 | -5 | -12 | -15 | -16 | -10 | -3 | 1 | 3 | 2 | 2 | 1 | 0 | 0 |
| | NU | -963 | 0 | 0 | 0 | 6 | 4 | 0 | 0 | -1 | -6 | -13 | -18 | -35 | -197 | -225 | -224 | -166 | -68 | -20 |
| | FISSION | -858 | 0 | 0 | 0 | 3 | 2 | 0 | -1 | -3 | -8 | -14 | -19 | -34 | -184 | -198 | -190 | -138 | -57 | -17 |
| | ELASTIC | -32 | 1 | 1 | 1 | 2 | 1 | 0 | -1 | -3 | -6 | -8 | -7 | -6 | -4 | -1 | -1 | 0 | 0 | 0 |
| | INELASTC | 11 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | -2 | -3 | -2 | -1 | 2 | 8 | 7 | 2 | 0 |
| | MU-AVE | 11 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 1 | 1 | 2 | 2 | 1 | 1 | 2 | 1 | 0 |
| PU-240 | (N,2N) | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| PU-241 | CAPTURE | -28 | -1 | -1 | -4 | -7 | -7 | -1 | -2 | -3 | -3 | -2 | -1 | 1 | 1 | 1 | 1 | 0 | 0 | 0 |
| | NU | -741 | 5 | 14 | 38 | 60 | 50 | -1 | -3 | -19 | -58 | -110 | -161 | -173 | -153 | -78 | -76 | -50 | -20 | -6 |
| | FISSION | -822 | 2 | 8 | 24 | 36 | 25 | -5 | -13 | -32 | -72 | -121 | -166 | -168 | -142 | -69 | -65 | -42 | -17 | -5 |
| | ELASTIC | -9 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | -1 | -1 | -2 | -2 | -1 | 0 | 0 | 0 | 0 | 0 | 0 |
| | INELASTC | 5 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 2 | 2 | 1 | 0 |
| PU-241 | MU-AVE | 4 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 1 | 1 | 1 | 1 | 0 | 0 |
| | (N,2N) | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| PU-242 | CAPTURE | -19 | 0 | -1 | -2 | -4 | -4 | -1 | -2 | -2 | -2 | -1 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| | NU | -124 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | -1 | -3 | -21 | -34 | -31 | -22 | -9 | -3 | -2 |
| | FISSION | -106 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | -1 | -3 | -19 | -30 | -26 | -18 | -7 | 0 | 0 |
| | ELASTIC | -5 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | -1 | -1 | -1 | 0 | 0 | 0 | 0 | 0 | 0 |
| | INELASTC | 2 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 1 | 1 | 0 | 0 |
| | MU-AVE | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| PU-242 | (N,2N) | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |

表B-8(2/4) 制御棒価値に対する感度係数(198体炉心 B C R -6 1E-2 xycal)

(1E-4Δk/kk' / Δσ/σ)

| 核種 | reaction | 群数 | | | | | | | | | | | | | | | | | | | | (1E-4Δk/kk' / Δσ/σ) |
|--------|-----------|-------|----|----|-----|-----|-----|-----|-----|-----|------|------|------|------|------|-----|-----|-----|-----|----|---|---------------------|
| | | total | 18 | 17 | 16 | 15 | 14 | 13 | 12 | 11 | 10 | 9 | 8 | 7 | 6 | 5 | 4 | 3 | 2 | 1 | | |
| AM-241 | CAPTURE | -60 | -1 | -3 | -6 | -11 | -11 | -2 | -5 | -6 | -5 | -3 | -1 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | |
| AM-241 | NU | -69 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | -1 | -6 | -18 | -21 | -15 | -6 | -2 | -2 | | |
| AM-241 | FISSION | -63 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | -1 | -1 | -6 | -16 | -19 | -13 | -6 | -2 | | |
| AM-241 | ELASTIC | -3 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | -1 | -1 | 0 | 0 | 0 | 0 | 0 | 0 | | |
| AM-241 | INELASTIC | 2 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 1 | 1 | 0 | 0 | | |
| AM-241 | MU-AVE | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 1 | 0 | 0 | | |
| AM-241 | (N,2N) | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | | |
| B-10 | CAPTU | 2976 | 1 | 1 | 1 | 1 | 6 | 9 | 47 | 152 | 332 | 554 | 685 | 548 | 356 | 81 | 121 | 52 | 24 | 5 | | |
| B-10 | ELASTI | 143 | 0 | 0 | 0 | -1 | -4 | -1 | -3 | -5 | -3 | 5 | 16 | 38 | 61 | 29 | 10 | 2 | -1 | 0 | | |
| B-10 | INELAST | 11 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 3 | 3 | 3 | 1 | 1 | | |
| B-10 | MU-AVE | 19 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 1 | 1 | 2 | 2 | 3 | 4 | 1 | 1 | 2 | 1 | 0 | | |
| B-10 | (N,2N) | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | | |
| B-11 | CAPTU | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | | |
| B-11 | ELASTI | 102 | 0 | 0 | 0 | 0 | -2 | -7 | -2 | -7 | -11 | -9 | 6 | 20 | 32 | 55 | 14 | 13 | 2 | -2 | 0 | |
| B-11 | INELAST | 3 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 1 | 1 | 1 | | |
| B-11 | MU-AVE | 23 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 1 | 1 | 2 | 3 | 3 | 2 | 6 | 1 | 1 | 2 | 1 | | |
| B-11 | (N,2N) | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | | |
| C | CAPTU | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | | |
| C | ELASTI | 20 | 0 | 0 | 0 | 0 | -1 | -2 | -1 | -2 | -3 | 0 | 4 | 8 | 11 | 7 | 3 | 0 | -1 | 0 | | |
| C | INELAST | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | | |
| C | MU-AVE | 5 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 1 | 1 | 1 | 1 | 1 | 0 | 0 | 0 | 0 | 0 | | |
| C | (N,2N) | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | | |
| O | CAPTU | 17 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 11 | 6 | |
| O | ELASTI | -1122 | 4 | 7 | 13 | 18 | 12 | -7 | -29 | -80 | -163 | -252 | -264 | -240 | -106 | -2 | 25 | -36 | -22 | 0 | | |
| O | INELAST | 3 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 3 | | |
| O | MU-AVE | 100 | 0 | 0 | 0 | -1 | 0 | 0 | 0 | 1 | 2 | 2 | -1 | -20 | 76 | 10 | 10 | 7 | 12 | 2 | | |
| O | (N,2N) | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | | |
| NA | CAPTU | -20 | 0 | 0 | -1 | -3 | -7 | -6 | -1 | 0 | -2 | -1 | -1 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | | |
| NA | ELASTI | -931 | -5 | -3 | -2 | -34 | -37 | -11 | -6 | -71 | -130 | -192 | -201 | -135 | -102 | 15 | -1 | -9 | -7 | 0 | | |
| NA | INELAST | 155 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 12 | 44 | 38 | 39 | 15 | 7 | | |
| NA | MU-AVE | 114 | 0 | 0 | 0 | 2 | 3 | 1 | 1 | 2 | 2 | 3 | 5 | 8 | 26 | 15 | 21 | 18 | 6 | 1 | | |
| NA | (N,2N) | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | | |
| CR | CAPTU | -23 | 0 | 0 | -1 | -1 | -13 | -1 | -7 | -1 | -3 | -1 | -1 | 0 | 1 | 1 | 1 | 1 | 1 | 1 | | |
| CR | ELASTI | -343 | 0 | 1 | 1 | 0 | -1 | -4 | -35 | -23 | -22 | -39 | -92 | -49 | -41 | -12 | -13 | -10 | -4 | 0 | | |
| CR | INELAST | 94 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 2 | 30 | 40 | 16 | 6 | | | |
| CR | MU-AVE | 52 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 1 | 3 | 3 | 4 | 3 | 10 | 16 | 9 | 3 | | |
| CR | (N,2N) | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | | |
| MN | CAPTU | -24 | 0 | 0 | -12 | -1 | -8 | 0 | -1 | -1 | -1 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | | |
| MN | ELASTI | -54 | 0 | 0 | 2 | 0 | -2 | -5 | -4 | -5 | -11 | -12 | -7 | -4 | -3 | -1 | -1 | -1 | 0 | 0 | | |
| MN | INELAST | 10 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 3 | 4 | 2 | 1 | | | |
| MN | MU-AVE | 4 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 1 | 1 | 1 | 1 | 0 | | | |
| MN | (N,2N) | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | | |
| FE | CAPTU | -75 | 0 | -1 | -3 | -4 | -54 | -1 | -7 | -8 | -13 | -7 | -4 | 1 | 4 | 3 | 3 | 6 | 4 | | | |
| FE | ELASTI | -1094 | 5 | 7 | 9 | 1 | -3 | -7 | -49 | -76 | -201 | -186 | -191 | -156 | -122 | -28 | -42 | -39 | -14 | -2 | | |
| FE | INELAST | 374 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | -1 | -17 | -7 | -2 | -1 | 0 | 49 | 157 | 109 | 65 | 22 | | |
| FE | MU-AVE | 181 | 0 | 0 | 0 | 0 | 0 | 0 | 1 | 1 | 3 | 4 | 8 | 15 | 25 | 14 | 31 | 42 | 28 | 9 | | |
| FE | (N,2N) | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | | |
| Ni | CAPTU | 16 | 0 | 0 | -1 | -1 | -2 | -1 | -2 | -11 | -6 | -3 | -2 | 1 | 2 | 2 | 4 | 14 | 16 | 6 | | |
| Ni | ELASTI | -459 | 2 | 2 | 3 | 0 | -2 | -4 | -18 | -97 | -89 | -72 | -64 | -57 | -33 | -9 | -10 | -8 | -3 | 0 | | |
| Ni | INELAST | 56 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 18 | 26 | 9 | 3 | | |
| Ni | MU-AVE | 44 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 1 | 1 | 2 | 3 | 5 | 6 | 3 | 7 | 8 | 6 | 2 | | |
| Ni | (N,2N) | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | | |
| Mo | CAPTU | -38 | -1 | -1 | -4 | -9 | -8 | -2 | -4 | -4 | -4 | -2 | -1 | 0 | 1 | 1 | 0 | 0 | 0 | 0 | | |
| Mo | ELASTI | -44 | 0 | 0 | 0 | 0 | 0 | 0 | -1 | -3 | -5 | -7 | -9 | -8 | -6 | -2 | -2 | -1 | 0 | 0 | | |
| Mo | INELAST | 23 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 3 | 8 | 8 | 3 | 1 | | |
| Mo | MU-AVE | 11 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 1 | 2 | 3 | 2 | 2 | 1 | 0 | | |
| Mo | (N,2N) | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | | |

表B-8(3/4) 制御棒価値に対する感度係数(198体炉心 B C R -6 1E-2 xycal)

(1E-4 $\Delta k/kk'$ / $\Delta\sigma/\sigma$)

| 項目 | level | 群数 | | | | | | | | | | | | | | | | | | |
|-----------------|-------|-------|----|----|----|----|----|----|----|----|-----|-----|-----|-----|----|----|----|-----|----|----|
| | | total | 18 | 17 | 16 | 15 | 14 | 13 | 12 | 11 | 10 | 9 | 8 | 7 | 6 | 5 | 4 | 3 | 2 | 1 |
| U-238 INELASTIC | 1 | -148 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | -24 | -37 | -31 | -28 | -8 | -8 | -8 | -3 | -1 | -1 |
| U-238 | 2 | -6 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | -1 | -3 | 1 | 0 | -2 | -1 | 0 | 0 |
| U-238 | 3 | 1 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 1 | 0 | 0 | 0 | 0 |
| U-238 | 4 | 18 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| U-238 | 5 | 13 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | -2 | 12 | 8 | 0 | 0 | 0 |
| U-238 | 6 | 3 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | -1 | 7 | 7 | 0 | 0 | 0 |
| U-238 | 7 | 6 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 2 | 4 | 0 | 0 | 0 |
| U-238 | 8 | 11 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 4 | 7 | 0 | 0 | 0 |
| U-238 | 9 | 11 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 4 | 7 | 0 | 0 | 0 |
| U-238 | 10 | 14 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 4 | 10 | 0 | 0 | 0 |
| U-238 | 11 | 7 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 2 | 5 | 0 | 0 | 0 |
| U-238 | 12 | 8 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 2 | 6 | 0 | 0 | 0 |
| U-238 | 13 | 12 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 2 | 9 | 1 | 0 | 0 |
| U-238 | 14 | 6 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 1 | 5 | 0 | 0 | 0 |
| U-238 | 15 | 10 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 2 | 7 | 1 | 0 | 0 |
| U-238 | 16 | 13 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 2 | 10 | 1 | 0 | 0 |
| U-238 | 17 | 9 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 1 | 7 | 1 | 0 | 0 |
| U-238 | 18 | 7 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 1 | 6 | 0 | 0 | 0 |
| U-238 | 19 | 7 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 1 | 5 | 1 | 0 | 0 |
| U-238 | 20 | 7 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 1 | 6 | 0 | 0 | 0 |
| U-238 | 21 | 6 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 5 | 1 | 0 | 0 |
| U-238 | 22 | 7 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 5 | 1 | 0 | 0 |
| U-238 | 23 | 8 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 7 | 1 | 0 | 0 |
| U-238 | 24 | 3 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 3 | 0 | 0 | 0 |
| U-238 | 25 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| U-238 | 26 | 4 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 4 | 0 | 0 | 0 |
| U-238 | 27 | 1 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 1 | 0 | 0 | 0 |
| U-238 | 28 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| U-238 | 29 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| U-238 | 30 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| U-238 | 31 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| U-238 | 32 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| U-238 | 33 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| U-238 | 34 | 341 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 82 | 188 | 60 | 11 |
| | total | 379 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |

表B-8(4/4) 制御棒価値に対する感度係数(198体炉心 BCR-6 1E-2 xycal)

(1E-4Δk/kk' / Δσ/σ)

| 項目 | サペイ | 群数 | | | | | | | | | | | | | | | | | | | |
|------------------|-------|-------|----|----|----|----|----|----|----|----|----|----|----|-----|-----|-----|------|------|------|------|--|
| | | total | 18 | 17 | 16 | 15 | 14 | 13 | 12 | 11 | 10 | 9 | 8 | 7 | 6 | 5 | 4 | 3 | 2 | 1 | |
| FISSION SPECTRUM | -1 | -66 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 3 | 15 | 58 | 186 | 455 | 357 | -178 | -554 | -281 | -127 | |
| FISSION | -0.9 | -57 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 3 | 15 | 58 | 185 | 448 | 350 | -173 | -538 | -278 | -127 | |
| FISSION | -0.8 | -49 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 3 | 15 | 58 | 184 | 441 | 343 | -168 | -524 | -274 | -127 | |
| FISSION | -0.7 | -40 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 3 | 15 | 58 | 183 | 434 | 336 | -163 | -510 | -270 | -126 | |
| FISSION | -0.6 | -34 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 3 | 15 | 58 | 182 | 427 | 330 | -159 | -497 | -267 | -126 | |
| FISSION | -0.5 | -27 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 3 | 15 | 57 | 181 | 421 | 324 | -155 | -484 | -263 | -126 | |
| FISSION | -0.4 | -21 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 3 | 15 | 57 | 180 | 414 | 318 | -151 | -472 | -260 | -125 | |
| FISSION | -0.3 | -16 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 3 | 15 | 57 | 179 | 408 | 312 | -147 | -461 | -257 | -125 | |
| FISSION | -0.2 | -11 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 3 | 15 | 57 | 178 | 402 | 306 | -143 | -450 | -254 | -125 | |
| FISSION | -0.1 | -5 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 3 | 15 | 57 | 177 | 397 | 301 | -140 | -440 | -251 | -124 | |
| FISSION | -0.05 | -2 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 3 | 15 | 57 | 177 | 394 | 298 | -138 | -435 | -249 | -124 | |
| FISSION | 0.05 | 1 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 3 | 15 | 57 | 176 | 388 | 293 | -135 | -426 | -246 | -124 | |
| FISSION | 0.1 | 4 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 3 | 15 | 57 | 175 | 386 | 291 | -133 | -421 | -245 | -124 | |
| FISSION | 0.2 | 8 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 3 | 15 | 57 | 174 | 380 | 286 | -130 | -412 | -242 | -123 | |
| FISSION | 0.3 | 12 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 3 | 15 | 57 | 173 | 375 | 281 | -127 | -403 | -239 | -123 | |
| FISSION | 0.4 | 14 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 3 | 15 | 56 | 173 | 370 | 276 | -125 | -395 | -236 | -123 | |
| FISSION | 0.5 | 18 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 3 | 15 | 56 | 172 | 365 | 272 | -122 | -387 | -234 | -122 | |
| FISSION | 0.6 | 21 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 3 | 15 | 56 | 171 | 361 | 268 | -120 | -380 | -231 | -122 | |
| FISSION | 0.7 | 25 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 3 | 15 | 56 | 170 | 356 | 264 | -117 | -372 | -228 | -122 | |
| FISSION | 0.8 | 27 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 3 | 15 | 56 | 169 | 351 | 260 | -115 | -365 | -226 | -121 | |
| FISSION | 0.9 | 30 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 3 | 15 | 56 | 168 | 347 | 256 | -113 | -358 | -223 | -121 | |
| FISSION | 1 | 32 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 3 | 15 | 56 | 167 | 343 | 252 | -110 | -352 | -221 | -121 | |

Appendix C

実効増倍率の感度係数に対する制御棒位置の影響について

実効増倍率の感度係数に対する制御棒の影響について

制御棒を試験体系通りに入れた場合とパーク位置に置いた場合の感度係数への影響について比較した結果を、表C-1と表C-2に示す。

- ・表C-1の168本体系では、制御棒は中心に 13.4cm 入っているのみなので影響は殆どない。
- ・表C-2の198本体系では、制御棒が 32cm 程度はいる。この場合、 ^{238}U の capture へ若干影響が現れる。

表C-1 制御棒の状態による感度係数への影響 (168本体系)

| 核種 | reaction | total | | |
|--------|----------|--------|-------|--------|
| | | cr-out | cr-in | JENDL2 |
| U-235 | CAPTURE | -8 | -8 | -1 |
| U-235 | NU | 86 | 86 | 83 |
| U-235 | FISSION | 60 | 59 | 53 |
| U-235 | ELASTIC | 0 | 0 | 0 |
| U-235 | INELASTC | 0 | 0 | 0 |
| U-235 | MU-AVE | 0 | 0 | 0 |
| U-235 | (N,2N) | 0 | 0 | 0 |
| U-238 | CAPTURE | -1853 | -1848 | -1833 |
| U-238 | NU | 993 | 996 | 999 |
| U-238 | FISSION | 621 | 624 | 626 |
| U-238 | ELASTIC | 244 | 244 | 238 |
| U-238 | INELASTC | -285 | -286 | -325 |
| U-238 | MU-AVE | -120 | -120 | -117 |
| U-238 | (N,2N) | 1 | 1 | 1 |
| PU-239 | CAPTURE | -570 | -569 | -574 |
| PU-239 | NU | 6990 | 6988 | 7004 |
| PU-239 | FISSION | 4981 | 4982 | 5004 |
| PU-239 | ELASTIC | 20 | 20 | 18 |
| PU-239 | INELASTC | -22 | -22 | -16 |
| PU-239 | MU-AVE | -13 | -13 | -8 |
| PU-239 | (N,2N) | 0 | 0 | 0 |
| PU-240 | CAPTURE | -246 | -245 | -226 |
| PU-240 | NU | 584 | 584 | 571 |
| PU-240 | FISSION | 403 | 404 | 391 |
| PU-240 | ELASTIC | 9 | 9 | 3 |
| PU-240 | INELASTC | -10 | -10 | -8 |
| PU-240 | MU-AVE | -4 | -4 | -1 |
| PU-240 | (N,2N) | 0 | 0 | 0 |
| PU-241 | CAPTURE | -62 | -62 | -54 |
| PU-241 | NU | 1151 | 1149 | 1116 |
| PU-241 | FISSION | 824 | 826 | 805 |
| PU-241 | ELASTIC | 1 | 1 | 0 |
| PU-241 | INELASTC | -2 | -2 | 0 |
| PU-241 | MU-AVE | 0 | 0 | 0 |
| PU-241 | (N,2N) | 0 | 0 | 0 |
| PU-242 | CAPTURE | -33 | -33 | -26 |
| PU-242 | NU | 66 | 66 | 62 |
| PU-242 | FISSION | 46 | 46 | 42 |
| PU-242 | ELASTIC | 0 | 0 | 0 |
| PU-242 | INELASTC | -2 | -2 | 0 |
| PU-242 | (N,2N) | 0 | 0 | 0 |
| PU-242 | MU-AVE | 0 | 0 | 0 |
| AM-241 | CAPTURE | -64 | -64 | -65 |
| AM-241 | NU | 43 | 43 | 45 |
| AM-241 | FISSION | 31 | 31 | 31 |
| AM-241 | ELASTIC | 0 | 0 | 0 |
| AM-241 | INELASTC | 0 | 0 | 0 |
| AM-241 | MU-AVE | 0 | 0 | 0 |
| AM-241 | (N,2N) | 0 | 0 | 0 |

| 核種 | reaction | (1E-4 $\Delta k/kk' / \Delta \sigma/\sigma$) | | |
|----|----------|---|--------|-------|
| | | total | cr-out | cr-in |
| | | JENDL2 | | |
| FE | CAPTURE | -214 | -213 | -200 |
| FE | ELASTIC | 349 | 349 | 328 |
| FE | INELASTC | -167 | -167 | -163 |
| FE | MU-AVE | -100 | -100 | -103 |
| FE | (N,2N) | 0 | 0 | 0 |
| CR | CAPTURE | -60 | -59 | -56 |
| CR | ELASTIC | 130 | 130 | 120 |
| CR | INELASTC | -37 | -37 | -33 |
| CR | MU-AVE | -28 | -28 | -27 |
| CR | (N,2N) | 0 | 0 | 0 |
| NI | CAPTURE | -117 | -117 | -116 |
| NI | ELASTIC | 127 | 127 | 111 |
| NI | INELASTC | -23 | -23 | -24 |
| NI | MU-AVE | -22 | -21 | -103 |
| NI | (N,2N) | 0 | 0 | 0 |
| NA | CAPTURE | -23 | -23 | -19 |
| NA | ELASTIC | 211 | 214 | 278 |
| NA | INELASTC | -77 | -78 | -95 |
| NA | MU-AVE | -67 | -69 | -65 |
| NA | (N,2N) | 0 | 0 | 0 |
| 0 | CAPTURE | -17 | -17 | -19 |
| 0 | ELASTIC | 11 | 12 | 47 |
| 0 | INELASTC | -1 | -1 | -1 |
| 0 | MU-AVE | -41 | -41 | -22 |
| 0 | (N,2N) | 0 | 0 | 0 |
| C | CAPTURE | 0 | 0 | 0 |
| C | ELASTIC | 0 | 0 | 0 |
| C | INELASTC | 0 | 0 | 0 |
| C | MU-AVE | 0 | 0 | 0 |
| C | (N,2N) | 0 | 0 | 0 |

CR-OUT 制御棒パーク位置

CR-IN 中心制御棒 13.4cm 挿入 他はパーク位置

表C-2 制御棒の状態による感度係数への影響 (198本体系)

| 核種 | reaction | total | | |
|--------|----------|--------|-------|---------|
| | | cr-out | cr-in | jendl-2 |
| U-235 | CAPTURE | -8 | -8 | -1 |
| U-235 | NU | 94 | 86 | 81 |
| U-235 | FISSION | 61 | 61 | 53 |
| U-235 | ELASTIC | 0 | 0 | 0 |
| U-235 | INELASTC | 0 | 0 | 0 |
| U-235 | MU-AVE | 0 | 0 | 0 |
| U-235 | (N, 2N) | 0 | 0 | 0 |
| U-238 | CAPTURE | -1925 | -1739 | -1842 |
| U-238 | NU | 1043 | 1017 | 999 |
| U-238 | FISSION | 644 | 641 | 616 |
| U-238 | ELASTIC | 262 | 266 | 261 |
| U-238 | INELASTC | -307 | -303 | -336 |
| U-238 | MU-AVE | -142 | -148 | -141 |
| U-238 | (N, 2N) | 1 | 1 | 1 |
| PU-239 | CAPTURE | -559 | -523 | -570 |
| PU-239 | NU | 6960 | 6977 | 7008 |
| PU-239 | FISSION | 4927 | 5018 | 4961 |
| PU-239 | ELASTIC | 20 | 20 | 17 |
| PU-239 | INELASTC | -22 | -24 | -18 |
| PU-239 | MU-AVE | -14 | -14 | -8 |
| PU-239 | (N, 2N) | 0 | 0 | 0 |
| PU-240 | CAPTURE | -243 | -229 | -224 |
| PU-240 | NU | 587 | 601 | 574 |
| PU-240 | FISSION | 400 | 417 | 385 |
| PU-240 | ELASTIC | 10 | 10 | 4 |
| PU-240 | INELASTC | -11 | -11 | -8 |
| PU-240 | MU-AVE | -4 | -4 | -1 |
| PU-240 | (N, 2N) | 0 | 0 | 0 |
| PU-241 | CAPTURE | -58 | -56 | -53 |
| PU-241 | NU | 1120 | 1115 | 1115 |
| PU-241 | FISSION | 799 | 810 | 798 |
| PU-241 | ELASTIC | 1 | 1 | 0 |
| PU-241 | INELASTC | -2 | -2 | 0 |
| PU-241 | MU-AVE | 0 | 0 | 0 |
| PU-241 | (N, 2N) | 0 | 0 | 0 |
| PU-242 | CAPTURE | -32 | -30 | -25 |
| PU-242 | NU | 66 | 69 | 62 |
| PU-242 | FISSION | 46 | 48 | 41 |
| PU-242 | ELASTIC | 0 | 0 | 0 |
| PU-242 | INELASTC | -2 | -2 | 0 |
| PU-242 | MU-AVE | 0 | 0 | 0 |
| PU-242 | (N, 2N) | 0 | 0 | 0 |
| AM-241 | CAPTURE | -64 | -59 | -62 |
| AM-241 | NU | 43 | 43 | 42 |
| AM-241 | FISSION | 31 | 31 | 29 |
| AM-241 | ELASTIC | 0 | 0 | 0 |
| AM-241 | INELASTC | 0 | 0 | 0 |
| AM-241 | MU-AVE | 0 | 0 | 0 |
| AM-241 | (N, 2N) | 0 | 0 | 0 |

| 核種 | reaction | (1E-4 $\Delta k/kk' / \Delta \sigma / \sigma$) | | |
|----|----------|---|--------|-------|
| | | total | cr-out | cr-in |
| FE | CAPTURE | -199 | -192 | -185 |
| FE | ELASTIC | 248 | 242 | 227 |
| FE | INELASTC | -181 | -194 | -170 |
| FE | MU-AVE | -80 | -81 | -79 |
| FE | (N, 2N) | 0 | 0 | 0 |
| CR | CAPTURE | -51 | -50 | -52 |
| CR | ELASTIC | 94 | 92 | 86 |
| CR | INELASTC | -41 | -45 | -35 |
| CR | MU-AVE | -23 | -23 | -19 |
| CR | (N, 2N) | 0 | 0 | 0 |
| NI | CAPTURE | -115 | -114 | -113 |
| NI | ELASTIC | 102 | 99 | 87 |
| NI | INELASTC | -23 | -26 | -24 |
| NI | MU-AVE | -19 | -19 | -11 |
| NI | (N, 2N) | 0 | 0 | 0 |
| NA | CAPTURE | -22 | -21 | -19 |
| NA | ELASTIC | 153 | 151 | 209 |
| NA | INELASTC | -75 | -78 | -97 |
| NA | MU-AVE | -59 | -60 | -56 |
| NA | (N, 2N) | 0 | 0 | 0 |
| O | CAPTURE | -18 | -17 | -19 |
| O | ELASTIC | -7 | 1 | 47 |
| O | INELASTC | -1 | -1 | -1 |
| O | MU-AVE | -48 | -49 | -22 |
| O | (N, 2N) | 0 | 0 | 0 |
| C | CAPTURE | 0 | 0 | 0 |
| C | ELASTIC | 0 | -2 | 0 |
| C | INELASTC | 0 | 0 | 0 |
| C | MU-AVE | 0 | 0 | 0 |
| C | (N, 2N) | 0 | 0 | 0 |

CR-OUT 制御棒パーク位置

CR-IN 調整棒挿入深度 32.3cm 後備炉停止棒 パーク位置

Appendix D

感度係数補足計算結果

表D-1 198体 2次元XY計算 収束判定 5E-3

表D-2 198本 2次元RZ計算 収束判定 1E-3 軸方向均質体系

表D-1(1/4) 制御棒価値に対する感度係数(198体炉心 中心CR 5E-3 xycal)

(1E-4Δk/kk' / Δσ/σ)

| 核種 | reaction | 群数 | | | | | | | | | | | | | | | | | | |
|--------|----------|-------|----|-----|------|------|------|-----|------|------|------|------|-------|-------|-------|------|------|------|------|------|
| | | total | 18 | 17 | 16 | 15 | 14 | 13 | 12 | 11 | 10 | 9 | 8 | 7 | 6 | 5 | 4 | 3 | 2 | 1 |
| U-235 | CAPTURE | -8 | 0 | 0 | -1 | -2 | -2 | 0 | -1 | -1 | -1 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| U-235 | NU | -82 | -4 | -2 | -1 | 4 | 3 | -2 | -3 | -5 | -8 | -12 | -14 | -13 | -11 | -5 | -5 | -3 | -1 | 0 |
| U-235 | FISSION | -97 | -3 | -2 | -2 | 0 | -2 | -3 | -5 | -7 | -10 | -13 | -14 | -13 | -10 | -5 | -4 | -3 | -1 | 0 |
| U-235 | ELASTIC | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| U-235 | INELASTC | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| U-235 | MU-AVE | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| U-235 | (N,2N) | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| U-238 | CAPTURE | -1678 | 6 | -31 | -105 | -345 | -373 | -84 | -189 | -247 | -235 | -127 | -49 | 9 | 43 | 29 | 14 | 5 | 1 | 0 |
| U-238 | NU | -1873 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | -1 | -5 | -61 | -725 | -659 | -305 | -117 |
| U-238 | FISSION | -1538 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | -1 | -5 | -53 | -603 | -531 | -250 | -95 |
| U-238 | ELASTIC | -758 | 4 | 12 | 12 | 16 | 4 | -6 | -19 | -39 | -73 | -120 | -155 | -144 | -134 | -42 | -38 | -25 | -9 | -2 |
| U-238 | INELASTC | 697 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | -6 | 6 | 11 | -4 | 115 | 269 | 234 | 62 | 10 |
| U-238 | MU-AVE | 455 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 1 | 2 | 9 | 26 | 54 | 92 | 46 | 72 | 89 | 52 | 12 |
| U-238 | (N,2N) | -4 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | -4 |
| Pu-238 | CAPTURE | -20 | 0 | -1 | -2 | -5 | -5 | -1 | -1 | -2 | -2 | -1 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Pu-238 | NU | -105 | 0 | 1 | 4 | 5 | 4 | 0 | 1 | 0 | -2 | -5 | -9 | -16 | -29 | -20 | -18 | -13 | -6 | -2 |
| Pu-238 | FISSION | -102 | 0 | 1 | 3 | 3 | 2 | 0 | 0 | -1 | -3 | -6 | -9 | -16 | -27 | -17 | -15 | -11 | -5 | -1 |
| Pu-238 | ELASTIC | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Pu-238 | INELASTC | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Pu-238 | MU-AVE | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Pu-238 | (N,2N) | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| PU-239 | CAPTURE | -795 | -8 | -35 | -119 | -211 | -203 | -36 | -64 | -61 | -48 | -25 | -9 | 7 | 10 | 4 | 2 | 1 | 0 | 0 |
| PU-239 | NU | -6000 | 39 | 145 | 370 | 743 | 627 | 35 | 64 | -21 | -289 | -724 | -1141 | -1468 | -1633 | -907 | -885 | -628 | -256 | -71 |
| PU-239 | FISSION | -6557 | 21 | 90 | 240 | 474 | 373 | -4 | -24 | -143 | -430 | -835 | -1194 | -1405 | -1463 | -768 | -721 | -503 | -208 | -57 |
| PU-239 | ELASTIC | -23 | 1 | 1 | 2 | 3 | 1 | 0 | -2 | -3 | -4 | -4 | -4 | -4 | -3 | -2 | -2 | -1 | 0 | 0 |
| PU-239 | INELASTC | 65 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | -4 | -3 | -2 | -2 | 1 | 9 | 12 | 24 | 21 | 8 | 1 |
| PU-239 | MU-AVE | 21 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 1 | 2 | 3 | 4 | 5 | 3 | 1 |
| PU-239 | (N,2N) | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| PU-240 | CAPTURE | -333 | -5 | -22 | -42 | -78 | -73 | -12 | -25 | -31 | -32 | -19 | -7 | 2 | 5 | 3 | 2 | 1 | 0 | 0 |
| PU-240 | NU | -1111 | 0 | 0 | 1 | 14 | 11 | 0 | 1 | 1 | -5 | -13 | -19 | -39 | -228 | -267 | -263 | -199 | -82 | -24 |
| PU-240 | FISSION | -964 | 0 | 0 | 0 | 9 | 6 | 0 | 0 | -2 | -9 | -16 | -20 | -38 | -206 | -227 | -215 | -160 | -67 | -19 |
| PU-240 | ELASTIC | -10 | 0 | 1 | 1 | 1 | 1 | 0 | -1 | -2 | -2 | -2 | -2 | -1 | -1 | -1 | -1 | 0 | 0 | 0 |
| PU-240 | INELASTC | 31 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | -2 | -1 | 1 | 2 | 5 | 12 | 10 | 3 | 1 |
| PU-240 | MU-AVE | 6 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 1 | 1 | 1 | 1 | 1 | 0 | 0 |
| PU-240 | (N,2N) | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| PU-241 | CAPTURE | -59 | -1 | -2 | -9 | -16 | -16 | -2 | -5 | -5 | -5 | -3 | -1 | 1 | 3 | 1 | 1 | 0 | 0 | 0 |
| PU-241 | NU | -648 | 5 | 27 | 87 | 144 | 136 | 7 | 11 | -9 | -61 | -129 | -187 | -206 | -186 | -98 | -94 | -63 | -25 | -7 |
| PU-241 | FISSION | -820 | 3 | 17 | 57 | 92 | 81 | -2 | -8 | -34 | -86 | -146 | -194 | -196 | -167 | -83 | -77 | -50 | -21 | -6 |
| PU-241 | ELASTIC | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| PU-241 | INELASTC | 9 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 1 | 1 | 3 | 3 | 1 | 0 | 0 |
| PU-241 | MU-AVE | 2 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 1 | 1 | 0 | 0 | 0 |
| PU-241 | (N,2N) | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| PU-242 | CAPTURE | -44 | 0 | -2 | -5 | -10 | -9 | -2 | -4 | -5 | -5 | -2 | -1 | 0 | 1 | 0 | 0 | 0 | 0 | 0 |
| PU-242 | NU | -143 | 0 | 0 | 0 | 1 | 0 | 0 | 0 | 0 | 0 | 0 | -1 | -3 | -24 | -40 | -36 | -26 | -11 | -3 |
| PU-242 | FISSION | -122 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | -1 | -3 | -21 | -34 | -30 | -21 | -9 | -3 |
| PU-242 | ELASTIC | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| PU-242 | INELASTC | 6 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 1 | 2 | 2 | 1 | 0 |
| PU-242 | MU-AVE | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| PU-242 | (N,2N) | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |

表D-1(2/4) 制御棒価値に対する感度係数 (198体炉心 中心CR 5E-3 xycal)

| 核種 | reaction | 群数 | (1E-4Δk/k' / Δσ/σ) | | | | | | | | | | | | | | | | | | |
|--------|-----------|------|--------------------|----|-----|-----|------|-----|-----|-----|------|------|------|-----|-----|-----|-----|-----|-----|----|----|
| | | | Total | 18 | 17 | 16 | 15 | 14 | 13 | 12 | 11 | 10 | 9 | 8 | 7 | 6 | 5 | 4 | 3 | 2 | 1 |
| AN-241 | CAPTURE | -163 | -1 | -5 | -13 | -28 | -31 | -7 | -13 | -16 | -17 | -15 | -10 | -5 | -2 | 0 | 0 | 0 | 0 | 0 | 0 |
| AM-241 | NU | -42 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | -3 | -11 | -13 | -10 | -4 | -1 | -1 |
| AM-241 | FISSION | -42 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | -4 | -11 | -13 | -9 | -4 | -1 | -1 |
| AM-241 | ELASTIC | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| AM-241 | INELASTIC | 4 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 1 | 1 | 1 | 0 | 0 | 0 | 0 |
| AM-241 | MU-AVE | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| AM-241 | (N, 2N) | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| B-10 | CAPTU | 5318 | 1 | 1 | 6 | 53 | 149 | 75 | 244 | 510 | 805 | 1018 | 1054 | 725 | 406 | 79 | 115 | 50 | 22 | 4 | |
| B-10 | ELASTI | 259 | 0 | 0 | 0 | -1 | -2 | -1 | 2 | 10 | 21 | 35 | 48 | 59 | 55 | 16 | 12 | 5 | 0 | 0 | |
| B-10 | INELAST | 9 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 2 | 3 | 2 | 1 | 1 | |
| B-10 | MU-AVE | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| B-10 | (N, 2N) | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| B-11 | CAPTU | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| B-11 | ELASTI | 443 | 0 | 0 | 0 | -1 | -3 | -7 | -3 | 5 | 28 | 56 | 84 | 89 | 77 | 73 | 14 | 26 | 6 | -1 | 0 |
| B-11 | INELAST | 3 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 1 | 1 | 1 | 0 |
| B-11 | MU-AVE | 7 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 1 | 1 | 1 | 1 | 0 | 0 | 0 | 1 | 0 | 0 | 0 |
| B-11 | (N, 2N) | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| C | CAPTU | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| C | ELASTI | 168 | 0 | 0 | 0 | 0 | -1 | -3 | -1 | 2 | 10 | 21 | 32 | 35 | 31 | 24 | 8 | 8 | 2 | 0 | 0 |
| C | INELAST | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| C | MU-AVE | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| C | (N, 2N) | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| O | CAPTU | 19 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 12 | ? |
| O | ELASTI | -380 | 3 | 8 | 16 | 18 | 20 | -3 | -30 | -78 | -105 | -110 | -77 | -38 | 82 | -13 | 10 | -59 | -31 | -1 | |
| O | INELAST | 4 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 4 | |
| O | MU-AVE | 138 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 1 | 2 | 2 | -1 | -19 | 95 | 14 | 15 | 9 | 17 | 3 |
| O | (N, 2N) | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| HA | CAPTU | -52 | 0 | -1 | -2 | -5 | -17 | -15 | -3 | 0 | -4 | -2 | -1 | -1 | -1 | 0 | 0 | 0 | 0 | 0 | 0 |
| HA | ELASTI | -197 | -3 | -3 | -2 | -30 | -27 | -3 | 1 | -32 | -43 | -67 | -55 | 33 | 19 | 29 | -1 | -9 | -4 | 0 | |
| HA | INELAST | 188 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 57 | 48 | 30 | 32 | 15 | 6 | |
| HA | MU-AVE | 74 | 0 | 0 | 0 | 0 | 2 | 3 | 1 | 1 | 1 | 1 | 2 | 3 | 14 | 10 | 15 | 14 | 5 | 1 | |
| HA | (N, 2N) | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| CB | CAPTU | -50 | 0 | 0 | -1 | -3 | -30 | -3 | -3 | -16 | -2 | -7 | -2 | -2 | 0 | 1 | 1 | 1 | 1 | 1 | 1 |
| CB | ELASTI | -191 | 0 | 1 | 1 | -1 | -3 | -5 | -33 | -16 | -11 | -17 | -43 | -7 | -22 | -9 | -11 | -11 | -4 | 0 | |
| CB | INELAST | 128 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 1 | 5 | 43 | 50 | 21 | 8 | |
| CB | MU-AVE | 50 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 2 | 3 | 3 | 10 | 17 | 10 | 3 | 0 | |
| CB | (N, 2N) | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| MN | CAPTU | -53 | 0 | 0 | -25 | -2 | -19 | -1 | -3 | -1 | -1 | -1 | -1 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| MN | ELASTI | -30 | 0 | 0 | 2 | 0 | -6 | -4 | -4 | -3 | -5 | -3 | -2 | -1 | -1 | -1 | -1 | -1 | 0 | 0 | 0 |
| MN | INELAST | 15 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 1 | 2 | 1 | 4 | 5 | 2 | 1 |
| MN | MU-AVE | 4 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 1 | 1 | 1 | 0 | 0 | 0 |
| MN | (N, 2N) | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| FE | CAPTU | -205 | 0 | -2 | -5 | -9 | -131 | -2 | -16 | -18 | -23 | -14 | -10 | 0 | 6 | 3 | 3 | 7 | 7 | 5 | |
| FE | ELASTI | -514 | 5 | 8 | 10 | -12 | -19 | -5 | -48 | -52 | -109 | -67 | -48 | -18 | -41 | -19 | -39 | -42 | -15 | -2 | |
| FE | INELAST | 567 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | -5 | 0 | 1 | 3 | 112 | 199 | 144 | 85 | 28 | | |
| FE | MU-AVE | 170 | 0 | 0 | 0 | 0 | 1 | 0 | 1 | 0 | 2 | 2 | 4 | 10 | 20 | 13 | 31 | 45 | 31 | 10 | |
| FE | (N, 2N) | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Hi | CAPTU | -14 | 0 | -1 | -1 | -3 | -5 | -2 | -5 | -25 | -13 | -7 | -4 | 0 | 2 | 2 | 5 | 17 | 19 | ? | |
| Hi | ELASTI | -258 | 1 | 3 | 3 | -5 | -9 | -4 | -16 | -68 | -41 | -28 | -21 | -18 | -7 | -9 | -9 | -3 | 0 | | |
| Hi | INELAST | 75 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 28 | 33 | 12 | 4 | | |
| Hi | MU-AVE | 39 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 1 | 1 | 2 | 3 | 4 | 3 | 7 | 9 | 6 | 2 | |
| Hi | (N, 2N) | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Mo | CAPTU | -82 | 0 | -2 | -6 | -20 | -19 | -4 | -9 | -9 | -8 | -4 | -2 | -2 | 0 | 1 | 1 | 1 | 0 | 0 | 0 |
| Mo | ELASTI | -23 | 0 | 0 | 0 | 0 | -1 | 0 | -1 | -2 | -2 | -3 | -4 | -3 | -4 | -1 | -1 | -1 | 0 | 0 | |
| Mo | INELAST | 34 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 2 | 6 | 11 | 10 | 4 | 1 | |
| Mo | MU-AVE | 9 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 1 | 1 | 3 | 1 | 2 | 1 | 0 | 0 | 0 |
| Mo | (N, 2N) | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |

表D-1(3/4) 制御棒価値に対する感度係数 (198体炉心 中心CR 5E-3 xycal)

(1E-4 $\Delta k/kk' / \Delta\sigma/\sigma$)

| 項目 | level | 群数 | | | | | | | | | | | | | | | | | | |
|-----------------|-------|-------|----|----|----|----|----|----|----|----|----|----|---|----|-----|-----|-----|-----|----|----|
| | | total | 18 | 17 | 16 | 15 | 14 | 13 | 12 | 11 | 10 | 9 | 8 | 7 | 6 | 5 | 4 | 3 | 2 | 1 |
| U-238 INELASTIC | 1 | -57 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | -6 | 6 | 9 | -22 | -13 | -13 | -12 | -5 | -1 |
| U-238 | 2 | -3 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 1 | 1 | 0 | -1 | -3 | -1 | 0 |
| U-238 | 3 | 1 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 1 | 0 | 0 | 0 |
| U-238 | 4 | 44 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 13 | 22 | 9 | 0 | 0 | 0 |
| U-238 | 5 | 24 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 4 | 13 | 7 | 0 | 0 | 0 |
| U-238 | 6 | 3 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 1 | 2 | 0 | 0 | 0 |
| U-238 | 7 | 10 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 6 | 4 | 0 | 0 | 0 |
| U-238 | 8 | 21 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 13 | 8 | 0 | 0 |
| U-238 | 9 | 19 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 11 | 8 | 0 | 0 |
| U-238 | 10 | 23 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 12 | 11 | 0 | 0 |
| U-238 | 11 | 10 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 5 | 5 | 0 | 0 |
| U-238 | 12 | 13 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 6 | 7 | 0 | 0 |
| U-238 | 13 | 18 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 6 | 11 | 1 | 0 |
| U-238 | 14 | 8 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 2 | 6 | 0 | 0 |
| U-238 | 15 | 13 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 4 | 9 | 0 | 0 |
| U-238 | 16 | 18 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 6 | 12 | 1 | -1 |
| U-238 | 17 | 13 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 3 | 9 | 1 | 0 |
| U-238 | 18 | 11 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 4 | 7 | 0 | 0 |
| U-238 | 19 | 9 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 2 | 6 | 1 | 0 |
| U-238 | 20 | 10 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 3 | 7 | 0 | 0 |
| U-238 | 21 | 8 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 1 | 6 | 1 | 0 |
| U-238 | 22 | 8 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 2 | 6 | 0 | 0 |
| U-238 | 23 | 12 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 2 | 9 | 1 | 0 |
| U-238 | 24 | 4 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 1 | 3 | 0 | 0 |
| U-238 | 25 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| U-238 | 26 | 7 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 1 | 6 | 0 | 0 |
| U-238 | 27 | 1 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 1 | 0 | 0 |
| U-238 | 28 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| U-238 | 29 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| U-238 | 30 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| U-238 | 31 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| U-238 | 32 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| U-238 | 33 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| U-238 | 34 | 450 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 126 | 241 | 71 | 12 |
| | total | 698 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | -6 | 6 | 10 | -4 | 113 | 272 | 232 | 64 | 11 |

表D-1(4/4) 制御棒価値に対する感度係数(198体炉心 中心C R 5E-3 xycal)

(1E-4 $\Delta k/kk'$ / $\Delta\sigma/\sigma$)

| 項目 | サペイ | 群数 | | | | | | | | | | | | | | | | | | |
|------------------|-------|-------|----|----|----|----|----|----|----|----|----|----|----|-----|-----|-----|------|------|------|------|
| | | total | 18 | 17 | 16 | 15 | 14 | 13 | 12 | 11 | 10 | 9 | 8 | 7 | 6 | 5 | 4 | 3 | 2 | 1 |
| FISSION SPECTRUM | -1 | -94 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 2 | 9 | 32 | 96 | 255 | 509 | 362 | -249 | -631 | -333 | -146 |
| FISSION | -0.9 | -80 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 2 | 9 | 32 | 96 | 253 | 501 | 355 | -241 | -613 | -328 | -146 |
| FISSION | -0.8 | -68 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 2 | 9 | 32 | 95 | 252 | 493 | 348 | -234 | -596 | -324 | -145 |
| FISSION | -0.7 | -59 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 2 | 9 | 32 | 95 | 251 | 485 | 341 | -228 | -581 | -320 | -145 |
| FISSION | -0.6 | -49 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 2 | 9 | 32 | 95 | 249 | 478 | 334 | -221 | -566 | -316 | -145 |
| FISSION | -0.5 | -38 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 2 | 9 | 32 | 95 | 248 | 471 | 328 | -215 | -552 | -312 | -144 |
| FISSION | -0.4 | -31 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 2 | 9 | 31 | 95 | 246 | 464 | 322 | -210 | -538 | -308 | -144 |
| FISSION | -0.3 | -23 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 2 | 9 | 31 | 94 | 245 | 457 | 316 | -205 | -525 | -304 | -143 |
| FISSION | -0.2 | -16 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 2 | 9 | 31 | 94 | 244 | 450 | 310 | -200 | -513 | -300 | -143 |
| FISSION | -0.1 | -8 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 2 | 9 | 31 | 94 | 242 | 444 | 305 | -195 | -501 | -296 | -143 |
| FISSION | -0.05 | -4 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 2 | 9 | 31 | 94 | 242 | 441 | 302 | -192 | -496 | -295 | -142 |
| FISSION | 0.05 | 3 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 2 | 9 | 31 | 94 | 241 | 435 | 297 | -188 | -485 | -291 | -142 |
| FISSION | 0.1 | 6 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 2 | 9 | 31 | 94 | 240 | 432 | 294 | -186 | -479 | -289 | -142 |
| FISSION | 0.2 | 12 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 2 | 9 | 31 | 94 | 239 | 426 | 289 | -182 | -469 | -286 | -141 |
| FISSION | 0.3 | 16 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 2 | 9 | 31 | 93 | 237 | 420 | 285 | -178 | -459 | -283 | -141 |
| FISSION | 0.4 | 21 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 2 | 9 | 31 | 93 | 236 | 414 | 280 | -174 | -450 | -279 | -141 |
| FISSION | 0.5 | 28 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 2 | 9 | 31 | 93 | 235 | 409 | 276 | -170 | -441 | -276 | -140 |
| FISSION | 0.6 | 32 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 2 | 9 | 31 | 93 | 234 | 404 | 271 | -167 | -432 | -273 | -140 |
| FISSION | 0.7 | 35 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 2 | 9 | 31 | 93 | 232 | 398 | 267 | -163 | -424 | -270 | -140 |
| FISSION | 0.8 | 40 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 2 | 9 | 31 | 93 | 231 | 393 | 263 | -160 | -416 | -267 | -139 |
| FISSION | 0.9 | 43 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 2 | 9 | 31 | 92 | 230 | 388 | 259 | -157 | -408 | -264 | -139 |
| FISSION | 1 | 48 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 2 | 9 | 31 | 92 | 229 | 384 | 255 | -154 | -401 | -261 | -138 |

表D-2(1/4) 制御棒価値に対する感度係数(198体炉心 中心CR 1E-3 Rzcal用マクロ使用)

| 核種 | reaction | 群数 | | | | | | | | | | | | | | | | | | (1E-4 Δk/k' / Δσ/σ) | | | | | | | |
|--------|----------|-------|-----|-----|------|------|------|------|------|------|------|------|-------|-------|-------|------|------|------|------|---------------------|------|----|---|---|---|---|---|
| | | total | 18 | 17 | 16 | 15 | 14 | 13 | 12 | 11 | 10 | 9 | 8 | 7 | 6 | 5 | 4 | 3 | 2 | 1 | | | | | | | |
| U-235 | CAPTURE | -9 | 0 | 0 | -1 | -2 | -2 | 0 | -1 | -1 | -1 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | |
| | NU | -55 | -1 | 0 | 3 | 8 | 6 | -1 | -2 | -3 | -6 | -10 | -12 | -12 | -11 | -5 | -5 | -3 | -1 | 0 | 0 | 0 | 0 | 0 | 0 | | |
| | FISSION | -75 | -1 | 0 | 1 | 3 | 1 | -2 | -3 | -5 | -9 | -12 | -13 | -12 | -10 | -5 | -4 | -3 | -1 | 0 | 0 | 0 | 0 | 0 | 0 | | |
| | ELASTIC | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | | |
| | INELASTC | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | | |
| | (N,2N) | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | | |
| | MU-AVE | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | | |
| U-238 | CAPTURE | -2021 | -13 | -58 | -135 | -391 | -412 | -100 | -214 | -275 | -269 | -155 | -68 | -5 | 31 | 26 | 12 | 4 | 1 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | |
| | NU | -1847 | 0 | 0 | 0 | 1 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | -1 | -5 | -60 | -712 | -652 | -302 | -116 | | | | | | |
| | FISSION | -1548 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | -1 | -5 | -53 | -604 | -536 | -253 | -96 | | | | | | |
| | ELASTIC | -945 | 3 | 10 | 10 | 13 | -1 | -7 | -22 | -42 | -80 | -137 | -186 | -181 | -173 | -55 | -50 | -33 | -11 | -3 | | | | | | | |
| | INELASTC | 426 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | -11 | -11 | -10 | -35 | 71 | 201 | 175 | 40 | 6 | | | | | | |
| | (N,2N) | -5 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | | |
| | MU-AVE | 581 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 1 | 3 | 10 | 30 | 65 | 116 | 59 | 94 | 117 | 69 | 17 | | | | | | | |
| PU-239 | CAPTURE | -720 | -11 | -37 | -118 | -199 | -185 | -31 | -55 | -51 | -39 | -18 | -4 | 10 | 11 | 4 | 2 | 1 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | |
| | NU | -6021 | 60 | 167 | 390 | 757 | 633 | 43 | 76 | -6 | -268 | -707 | -1145 | -1496 | -1675 | -938 | -918 | -653 | -267 | -74 | | | | | | | |
| | FISSION | -6362 | 36 | 109 | 262 | 503 | 401 | 9 | 0 | -108 | -382 | -788 | -1166 | -1409 | -1490 | -790 | -748 | -524 | -217 | -60 | | | | | | | |
| | ELASTIC | -47 | 0 | 1 | 1 | 2 | 0 | -1 | -2 | -4 | -5 | -6 | -7 | -8 | -7 | -3 | -4 | -3 | -1 | 0 | | | | | | | |
| | INELASTC | 45 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | -4 | -3 | -3 | -3 | -1 | 4 | 9 | 20 | 18 | 7 | 1 | | | | | | | |
| | (N,2N) | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | |
| | MU-AVE | 37 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 1 | 3 | 6 | 4 | 7 | 9 | 6 | 1 | | | | | |
| PU-240 | CAPTURE | -303 | -8 | -23 | -41 | -74 | -67 | -10 | -22 | -26 | -27 | -15 | -5 | 3 | 6 | 3 | 2 | 1 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | |
| | NU | -1142 | 0 | 0 | 1 | 14 | 11 | 0 | 2 | 1 | -4 | -13 | -19 | -39 | -233 | -275 | -272 | -206 | -85 | -25 | | | | | | | |
| | FISSION | -986 | 0 | 0 | 0 | 9 | 7 | 0 | 0 | -1 | -7 | -15 | -20 | -38 | -209 | -233 | -223 | -166 | -70 | -20 | | | | | | | |
| | ELASTIC | -18 | 0 | 1 | 1 | 1 | 0 | 0 | -1 | -2 | -3 | -3 | -3 | -3 | -1 | -1 | -1 | -1 | -1 | 0 | | | | | | | |
| | INELASTC | 21 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | -2 | -1 | 0 | 0 | 4 | 10 | 8 | 2 | 0 | | | | | | | |
| | (N,2N) | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | | | | | | | |
| | MU-AVE | 11 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 1 | 2 | 1 | 2 | 3 | 2 | 0 | | | | | | |
| PU-241 | CAPTURE | -51 | -1 | -3 | -9 | -15 | -14 | -2 | -4 | -5 | -4 | -2 | 0 | 2 | 3 | 2 | 1 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | |
| | NU | -642 | 8 | 31 | 92 | 146 | 137 | 9 | 14 | -6 | -57 | -127 | -189 | -210 | -192 | -101 | -98 | -65 | -26 | -8 | | | | | | | |
| | FISSION | -774 | 5 | 20 | 62 | 97 | 87 | 1 | -3 | -26 | -77 | -139 | -190 | -196 | -170 | -85 | -80 | -53 | -21 | -6 | | | | | | | |
| | ELASTIC | -6 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | -1 | -1 | -1 | -1 | -1 | -1 | 0 | -1 | 0 | 0 | 0 | | | | | | | |
| | INELASTC | 7 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 1 | 2 | 3 | 1 | 0 | | | | | | |
| | (N,2N) | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | | | | | | | |
| | MU-AVE | 5 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 1 | 1 | 1 | 1 | 1 | 0 | | | | | | |
| PU-242 | CAPTURE | -40 | -1 | -2 | -4 | -9 | -9 | -2 | -3 | -4 | -4 | -2 | -1 | 0 | 1 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | |
| | NU | -146 | 0 | 0 | 0 | 1 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | -1 | -3 | -24 | -41 | -37 | -27 | -11 | -3 | | | | | |
| | FISSION | -124 | 0 | 0 | 0 | 1 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | -1 | -3 | -22 | -35 | -31 | -21 | -9 | -3 | | | | | |
| | ELASTIC | -3 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | -1 | -1 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | |
| | INELASTC | 4 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 1 | 2 | 1 | 0 | 0 | 0 | 0 | 0 | 0 | |
| | (N,2N) | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | |
| | MU-AVE | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | |
| AM-241 | CAPTURE | -158 | -1 | -5 | -13 | -28 | -30 | -7 | -12 | -15 | -16 | -14 | -10 | -5 | -2 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| | NU | -39 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | -3 | -10 | -12 | -9 | -4 | -1 | | | | | | | |
| | FISSION | -40 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | -3 | -11 | -12 | -9 | -4 | -1 | | | | | | | |
| | ELASTIC | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | |
| | INELASTC | 1 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | |
| | (N,2N) | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | |
| | MU-AVE | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | |

表D-2(2/4) 制御棒価値に対する感度係数(198体炉心 中心CR 1E-3 Rzcal用マクロ使用)

(1E-4 Δk/kk' / Δσ/σ)

| 核種 | reaction | 群数 | | | | | | | | | | | | | | | | | | |
|------|----------|-------|----|----|-----|-----|------|-----|-----|-----|------|------|------|------|-----|-----|-----|-----|-----|----|
| | | total | 18 | 17 | 16 | 15 | 14 | 13 | 12 | 11 | 10 | 9 | 8 | 7 | 6 | 5 | 4 | 3 | 2 | 1 |
| B-10 | CAPTU | 4893 | 1 | 1 | 6 | 46 | 124 | 63 | 214 | 461 | 736 | 941 | 980 | 680 | 384 | 74 | 110 | 47 | 21 | 4 |
| B-10 | ELASTI | 229 | 0 | 0 | 0 | -1 | -2 | -1 | 2 | 10 | 20 | 32 | 43 | 53 | 49 | 13 | 10 | 2 | -1 | 0 |
| B-10 | INELAST | 8 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 2 | 2 | 1 | 1 | 1 |
| B-10 | MU-AVE | 8 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 1 | 1 | 2 | 1 | 1 | 1 | 0 |
| B-10 | (N,2N) | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| B-11 | CAPTU | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| B-11 | ELASTI | 394 | 0 | 0 | -1 | -3 | -6 | -2 | 5 | 27 | 52 | 77 | 80 | 70 | 66 | 8 | 20 | 3 | -2 | 0 |
| B-11 | INELAST | 3 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 1 | 1 | 1 |
| B-11 | MU-AVE | 11 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 1 | 1 | 1 | 1 | 3 | 1 | 1 | 1 | 0 |
| B-11 | (N,2N) | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| C | CAPTU | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| C | ELASTI | 148 | 0 | 0 | 0 | -1 | -2 | -1 | 2 | 10 | 20 | 29 | 31 | 28 | 20 | 6 | 6 | 1 | -1 | 0 |
| C | INELAST | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| C | MU-AVE | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| C | (N,2N) | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| O | CAPTU | 18 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 12 | 6 |
| O | ELASTI | -973 | 3 | 7 | 14 | 11 | 19 | -3 | -30 | -80 | -122 | -156 | -180 | -154 | -75 | -73 | -40 | -87 | -44 | -3 |
| O | INELAST | 3 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 3 |
| O | MU-AVE | 182 | 0 | 0 | 0 | 0 | 0 | 0 | 1 | 1 | 2 | 2 | -1 | -24 | 123 | 18 | 20 | 13 | 23 | 4 |
| O | (N,2N) | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| NA | CAPTU | -54 | 0 | -1 | -2 | -6 | -17 | -16 | -3 | 0 | -4 | -2 | -1 | -1 | -1 | 0 | 0 | 0 | 0 | 0 |
| NA | ELASTI | 343 | -8 | -9 | -6 | -33 | -12 | 2 | 11 | -4 | 11 | 19 | 49 | 125 | 105 | 56 | 28 | 7 | 1 | 1 |
| NA | INELAST | 171 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 34 | 47 | 34 | 33 | 16 | 7 |
| NA | MU-AVE | -23 | 0 | 0 | 1 | 1 | 3 | 1 | 0 | 0 | -1 | -2 | -5 | -9 | -7 | -1 | -4 | 1 | -1 | 0 |
| NA | (N,2N) | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| CB | CAPTU | -72 | 0 | -1 | -2 | -3 | -33 | -4 | -18 | -2 | -8 | -3 | -3 | -1 | 1 | 1 | 1 | 1 | 1 | 1 |
| CB | ELASTI | -206 | 0 | 0 | 0 | -1 | -2 | -4 | -30 | -15 | -9 | -13 | -33 | -14 | -30 | -15 | -19 | -15 | -5 | -1 |
| CB | INELAST | 107 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 1 | 4 | 37 | 42 | 17 | 6 |
| CB | MU-AVE | 62 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 1 | 1 | 4 | 4 | 13 | 22 | 13 |
| CB | (N,2N) | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| MN | CAPTU | -63 | 0 | -1 | -31 | -2 | -21 | -1 | -3 | -1 | -2 | -1 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| MN | ELASTI | -34 | 0 | 0 | -2 | -1 | -5 | -3 | -3 | -4 | -4 | -4 | -2 | -1 | -2 | -1 | -1 | 0 | 0 | 0 |
| MN | INELAST | 12 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 1 | 1 | 3 | 4 | 2 | 1 |
| MN | MU-AVE | 6 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 1 | 1 | 1 | 2 | 1 | 0 |
| MN | (N,2N) | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| FE | CAPTU | -245 | -1 | -3 | -6 | -10 | -144 | -2 | -17 | -20 | -33 | -18 | -14 | -3 | 3 | 3 | 3 | 6 | 6 | 5 |
| FE | ELASTI | -606 | -2 | 2 | 5 | -15 | -11 | -5 | -42 | -48 | -75 | -64 | -58 | -41 | -75 | -36 | -60 | -58 | -20 | -3 |
| FE | INELAST | 452 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | -10 | -3 | -1 | 0 | 2 | 89 | 172 | 114 | 66 | 23 |
| FE | MU-AVE | 204 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 1 | 1 | 3 | 8 | 22 | 17 | 40 | 59 | 13 |
| FE | (N,2N) | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |

表D-2(3/4) 制御棒価値に対する感度係数 (198体炉心 中心CR 1E-3 Rzcal用マウス使用)

(1E-4 $\Delta k/kk' / \Delta \sigma/\sigma$)

| 項目 | level | 群数 | | | | | | | | | | | | | | | | | 1 | |
|-----------------|-------|-------|----|----|----|----|----|----|----|----|----|-----|-----|-----|-----|-----|-----|-----|----|----|
| | | total | 18 | 17 | 16 | 15 | 14 | 13 | 12 | 11 | 10 | 9 | 8 | 7 | 6 | 5 | 4 | 3 | 2 | |
| U-238 INELASTIC | 1 | -137 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | -11 | -11 | -10 | -42 | -19 | -19 | -16 | -7 | -2 |
| U-238 | 2 | -16 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | -3 | -3 | -4 | -4 | -2 | 0 |
| U-238 | 3 | -1 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | -1 | 0 | 0 | 0 |
| U-238 | 4 | 30 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 2 | 17 | 7 | -1 | -1 | 0 |
| U-238 | 5 | 18 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 10 | 6 | 0 | 0 | 0 |
| U-238 | 6 | 3 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 2 | 0 | 0 | 0 | 0 |
| U-238 | 7 | 8 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 5 | 3 | 0 | 0 | 0 |
| U-238 | 8 | 15 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 9 | 6 | 0 | 0 | 0 |
| U-238 | 9 | 14 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 8 | 6 | 0 | 0 | 0 |
| U-238 | 10 | 18 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 3 | 4 | 0 | 0 | 0 |
| U-238 | 11 | 7 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 4 | 5 | 0 | 0 | 0 |
| U-238 | 12 | 9 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 5 | 9 | 0 | 0 | 0 |
| U-238 | 13 | 14 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 5 | 0 | 0 | 0 |
| U-238 | 14 | 7 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 2 | 3 | 0 | 0 | 0 |
| U-238 | 15 | 10 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 4 | 10 | 0 | -1 | 0 |
| U-238 | 16 | 13 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 2 | 7 | 0 | 0 | 0 |
| U-238 | 17 | 9 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 3 | 5 | 0 | 0 | 0 |
| U-238 | 18 | 8 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 1 | 5 | 0 | 0 | 0 |
| U-238 | 19 | 6 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 2 | 6 | 0 | 0 | 0 |
| U-238 | 20 | 8 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 4 | 0 | 0 | 0 |
| U-238 | 21 | 5 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 1 | 5 | 0 | 0 | 0 |
| U-238 | 22 | 7 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 2 | 7 | 0 | 0 | 0 |
| U-238 | 23 | 8 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 1 | 3 | 0 | 0 | 0 |
| U-238 | 24 | 4 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| U-238 | 25 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| U-238 | 26 | 5 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 1 | 4 | 0 | 0 |
| U-238 | 27 | 1 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 1 | 0 | 0 | 0 |
| U-238 | 28 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| U-238 | 29 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| U-238 | 30 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| U-238 | 31 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| U-238 | 32 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| U-238 | 33 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 99 | 193 | 53 | 9 |
| U-238 | 34 | 354 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | -35 | 72 | 202 | 171 | 42 | 7 |
| | total | 427 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | -11 | -11 | -10 | -35 | 72 | 202 | 171 | 42 | 7 |

表D-2(4/4) 制御棒価値に対する感度係数(198体炉心 中心CR 1E-3 Rzcal用マウス)

(1E-4 Δk/k^{*} / Δσ/σ)

| 項目 | サペイ | 群数 | | | | | | | | | | | | | | | | (1E-4 Δk/k [*] / Δσ/σ) | | | | | | | | | | | | | | | | |
|------------------|-------|-------|----|----|----|----|----|----|----|----|----|----|----|-----|-----|-----|------|---------------------------------|------|------|------|------|------|------|------|------|------|------|------|------|------|------|------|------|
| | | total | 18 | 17 | 16 | 15 | 14 | 13 | 12 | 11 | 10 | 9 | 8 | 7 | 6 | 5 | 4 | 3 | 2 | 1 | -225 | -580 | -298 | -138 | -218 | -564 | -294 | -138 | -212 | -549 | -290 | -137 | -206 | -534 |
| FISSION SPECTRUM | -1 | -81 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 1 | 7 | 25 | 81 | 226 | 481 | 339 | -225 | -580 | -298 | -138 | -218 | -564 | -294 | -138 | -212 | -549 | -290 | -137 | -206 | -534 | -287 | -137 | | |
| FISSION | -0.9 | -71 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 1 | 7 | 25 | 81 | 224 | 473 | 332 | -218 | -564 | -294 | -138 | -212 | -549 | -290 | -137 | -206 | -534 | -287 | -137 | -200 | -521 | -283 | -136 | | |
| FISSION | -0.8 | -61 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 1 | 7 | 25 | 81 | 223 | 465 | 325 | -212 | -549 | -290 | -137 | -200 | -521 | -283 | -136 | -195 | -508 | -279 | -136 | -190 | -495 | -276 | -136 | | |
| FISSION | -0.7 | -52 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 1 | 7 | 25 | 80 | 222 | 458 | 319 | -206 | -534 | -287 | -137 | -195 | -508 | -279 | -136 | -190 | -495 | -276 | -136 | -185 | -483 | -272 | -135 | | |
| FISSION | -0.6 | -42 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 1 | 7 | 25 | 80 | 221 | 451 | 313 | -200 | -521 | -283 | -136 | -185 | -483 | -272 | -135 | -181 | -472 | -269 | -135 | -176 | -461 | -266 | -135 | | |
| FISSION | -0.5 | -34 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 1 | 7 | 25 | 80 | 220 | 444 | 307 | -195 | -508 | -279 | -136 | -181 | -472 | -269 | -135 | -176 | -461 | -266 | -135 | -170 | -446 | -261 | -134 | | |
| FISSION | -0.4 | -27 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 1 | 7 | 25 | 80 | 218 | 438 | 301 | -190 | -495 | -276 | -136 | -170 | -446 | -261 | -134 | -168 | -441 | -259 | -134 | -163 | -432 | -256 | -133 | | |
| FISSION | -0.3 | -18 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 1 | 7 | 25 | 80 | 217 | 431 | 296 | -185 | -483 | -272 | -135 | -163 | -432 | -256 | -133 | -161 | -423 | -253 | -133 | -157 | -414 | -250 | -133 | | |
| FISSION | -0.2 | -13 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 1 | 7 | 25 | 80 | 216 | 425 | 290 | -181 | -472 | -269 | -135 | -161 | -423 | -253 | -133 | -157 | -414 | -250 | -133 | -154 | -406 | -248 | -132 | | |
| FISSION | -0.1 | -7 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 1 | 7 | 25 | 79 | 215 | 419 | 285 | -176 | -461 | -266 | -135 | -161 | -423 | -253 | -133 | -154 | -406 | -248 | -132 | -150 | -400 | -244 | -132 | | |
| FISSION | -0.05 | -3 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 1 | 7 | 25 | 79 | 214 | 416 | 283 | -174 | -456 | -264 | -134 | -150 | -400 | -244 | -132 | -150 | -398 | -245 | -132 | -148 | -390 | -242 | -132 | | |
| FISSION | 0.05 | 2 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 1 | 7 | 25 | 79 | 213 | 410 | 278 | -170 | -446 | -261 | -134 | -148 | -390 | -242 | -132 | -146 | -383 | -239 | -131 | -142 | -376 | -237 | -131 | | |
| FISSION | 0.1 | 6 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 1 | 7 | 25 | 79 | 213 | 407 | 276 | -168 | -441 | -259 | -134 | -142 | -383 | -239 | -131 | -140 | -376 | -237 | -131 | -138 | -367 | -234 | -131 | | |
| FISSION | 0.2 | 11 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 1 | 7 | 25 | 79 | 211 | 402 | 271 | -164 | -432 | -256 | -133 | -140 | -376 | -234 | -131 | -138 | -367 | -234 | -131 | -136 | -354 | -232 | -131 | | |
| FISSION | 0.3 | 15 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 1 | 7 | 25 | 79 | 210 | 396 | 267 | -161 | -423 | -253 | -133 | -138 | -367 | -234 | -131 | -136 | -354 | -232 | -131 | -134 | -342 | -230 | -131 | | |
| FISSION | 0.4 | 20 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 1 | 7 | 25 | 79 | 209 | 391 | 262 | -157 | -414 | -250 | -133 | -134 | -354 | -230 | -131 | -132 | -342 | -230 | -131 | -130 | -337 | -228 | -131 | | |
| FISSION | 0.5 | 24 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 1 | 7 | 25 | 79 | 208 | 386 | 258 | -154 | -406 | -248 | -132 | -130 | -342 | -228 | -131 | -130 | -337 | -228 | -131 | -128 | -334 | -226 | -131 | | |
| FISSION | 0.6 | 27 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 1 | 7 | 25 | 78 | 207 | 381 | 254 | -151 | -398 | -245 | -132 | -128 | -334 | -226 | -131 | -130 | -331 | -226 | -131 | -128 | -328 | -223 | -131 | | |
| FISSION | 0.7 | 31 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 1 | 7 | 25 | 78 | 206 | 376 | 250 | -148 | -390 | -242 | -132 | -128 | -328 | -223 | -131 | -130 | -325 | -221 | -131 | -128 | -322 | -218 | -131 | | |
| FISSION | 0.8 | 35 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 1 | 7 | 25 | 78 | 205 | 371 | 246 | -145 | -383 | -239 | -131 | -128 | -322 | -218 | -131 | -130 | -319 | -215 | -131 | -128 | -316 | -212 | -131 | | |
| FISSION | 0.9 | 39 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 1 | 7 | 25 | 78 | 204 | 367 | 243 | -142 | -376 | -237 | -131 | -128 | -316 | -212 | -131 | -130 | -313 | -209 | -131 | -128 | -310 | -206 | -131 | | |
| FISSION | 1 | 42 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 1 | 7 | 25 | 78 | 203 | 362 | 239 | -139 | -369 | -234 | -131 | -128 | -310 | -206 | -131 | -130 | -307 | -203 | -131 | -128 | -304 | -200 | -131 | | |