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Creep Test of Fuel Cladding Tubes for Fast Breeder Reactor (Part III)

February, 1974

POWER REACTOR AND NUCLEAR FUEL
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Creep Test of Fuel Cladding Tubes for Fast Breeder Reactor (Part III)*

Teruo Yukitoshi, ** Kunihiko Yoshikawa, **
and Kenichiro Ueno **

Abstract

This work, which involved high temperature tensile test, internal pressure creep rupture test and examination of the ruptured test pieces, was undertaken as the third program of a series of experiment by contract with Power Reactor and Nuclear Fuel Development Corporation (PNC) for the purpose of determining the high temperature performance of clad tubing for the Fast Experimental Reactor "JOYO".

The materials tested under this experiment were SUS 316 tubes of 6.3 mm diameter and 0.35 mm thickness supplied by two different manufacturers. These materials were classified and designated for convenience sake as B-material and A-material respectively according to their manufacturers.

As the result of this experiment, it was confirmed that both A and B materials demonstrated sufficient strength and elongation under 600°C - 700°C temperature range satisfying the specifications given by PNC, and that in respect of their creep rupture strength, A-material showed a higher strength over that of B-material while A's rupture elongation was lower than that of B under the applied stress at a temperature of 650°C.

* Work performed under contracts between Power Reactor and Nuclear Fuel Development Corporation and Sumitomo Metal Industries, Ltd.

** Central Research Laboratories,
Sumitomo Metal Industries, Ltd.

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I. Preface

This experiment was performed for the purpose of determining allowable tensile stresses for the fuel cladding tube of the Fast Experimental Breeder Reactor (FEBR) under high temperatures as the third program of the project undertaken by this Central Research Laboratory by contract with the Power Reactor & Nuclear Fuel Development Corporation (PNC).

II. Research Plan

1. Experiment Target

This work is the third program of a series of experiment project involving tests of strength and performance of FEBR'S cladding tube under high temperatures. The first one was undertaken in 1970 and the second one in 1972, and this one which is the third experiment is to conduct a series of internal pressure creep tests to study high temperature properties of the cladding tube, and will involve internal creep rupture tests, post-rupture metallographic tests, and high temperature tensile test.

2. Kinds of Test and Test Conditions

(1) High temperature tensile test

Test temperatures: 600, 650, 700 and 750°C.

(2) Internal pressure creep rupture test

Test temperature: 650°C

Rupture time target: 100, 300, 1000 and 3000 hrs.

(3) Examination of ruptured test pieces

Photographing of appearance of test pieces

Observation of microstructures

Hardness measurement

Dimensional measurement

III. Test Materials

1. Type of steel

SUS 316, austenitic stainless steel, was used for the materials used in this test.

2. Dimension of test materials

6.3^φ x 0.35^t mm. The gauge length was 50 mm and the gauge width was 10 mm.

3. Test Pieces

3-1. High temperature tensile test pieces

The following 24 pieces were used. Gauge length was 50 mm and total length was 1000 mm.

K2771	K2722	K2737	K2738
Specimen No. 1 to specimen No. 6 below will be shown first			
K2795	K2756	K2778	K2752
Specimen No. 7 to specimen No. 12 below will be shown second			
K2746	K2792	K2789	K2764
Specimen No. 13 to specimen No. 18 below will be shown third			
S0514	S0511	S0512	S0513
Specimen No. 19 to specimen No. 24 below will be shown fourth			
S0510	S0519	S0521	S0518
Specimen No. 25 to specimen No. 29 below will be shown fifth			
S0517	S0515	S0516	S0520

3-2. Internal creep rupture test pieces

The form and configuration of the internal creep

rupture test pieces are given in Fig. 1. Preparation of the test pieces was performed by PNC. The following nine pieces

were used for this test:

K2703-5	S0522-1
K2705-6	S0526-8
K2701-5	S0528-5
K2706-3	S0523-6

Specimen No. 1 to Specimen No. 6 will be shown first

Specimen No. 7 to Specimen No. 12 will be shown second

Specimen No. 13 to Specimen No. 18 will be shown third

Specimen No. 19 to Specimen No. 24 will be shown fourth

Specimen No. 25 to Specimen No. 29 will be shown fifth

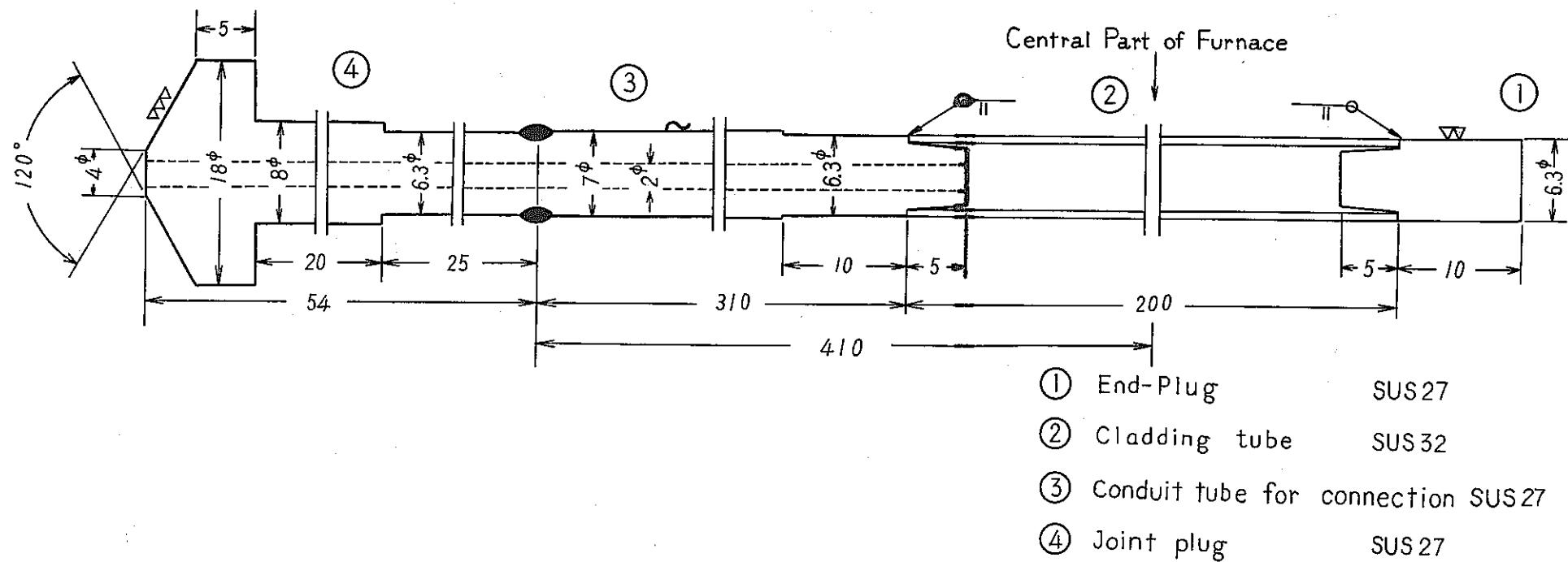


Fig. 1. Configuration of Internal Pressure Creep Test Piece

IV. Test Method

1. High Temperature Tensile Test

The equipment used for this high temperature tensile test was Electron Tube Self-balancing Universal Tester (10 tons) which is hydraulically loaded. The strain velocity is automatically controlled upto the proof stress, and thereafter, it is controlled manually by use of a strain-pacer.

The test pieces used for this test had a length of 1000mm, and were tested by JIS G0567-1966 under the following conditions:

Up to the proof stress: Strain measurement by D.T.F. at 50 mm G.L.; Strain rate of 0.3%/min.

After the proof stress: Strain rate of 7.5 mm/min was aimed at with assumed G.L. of 100 mm

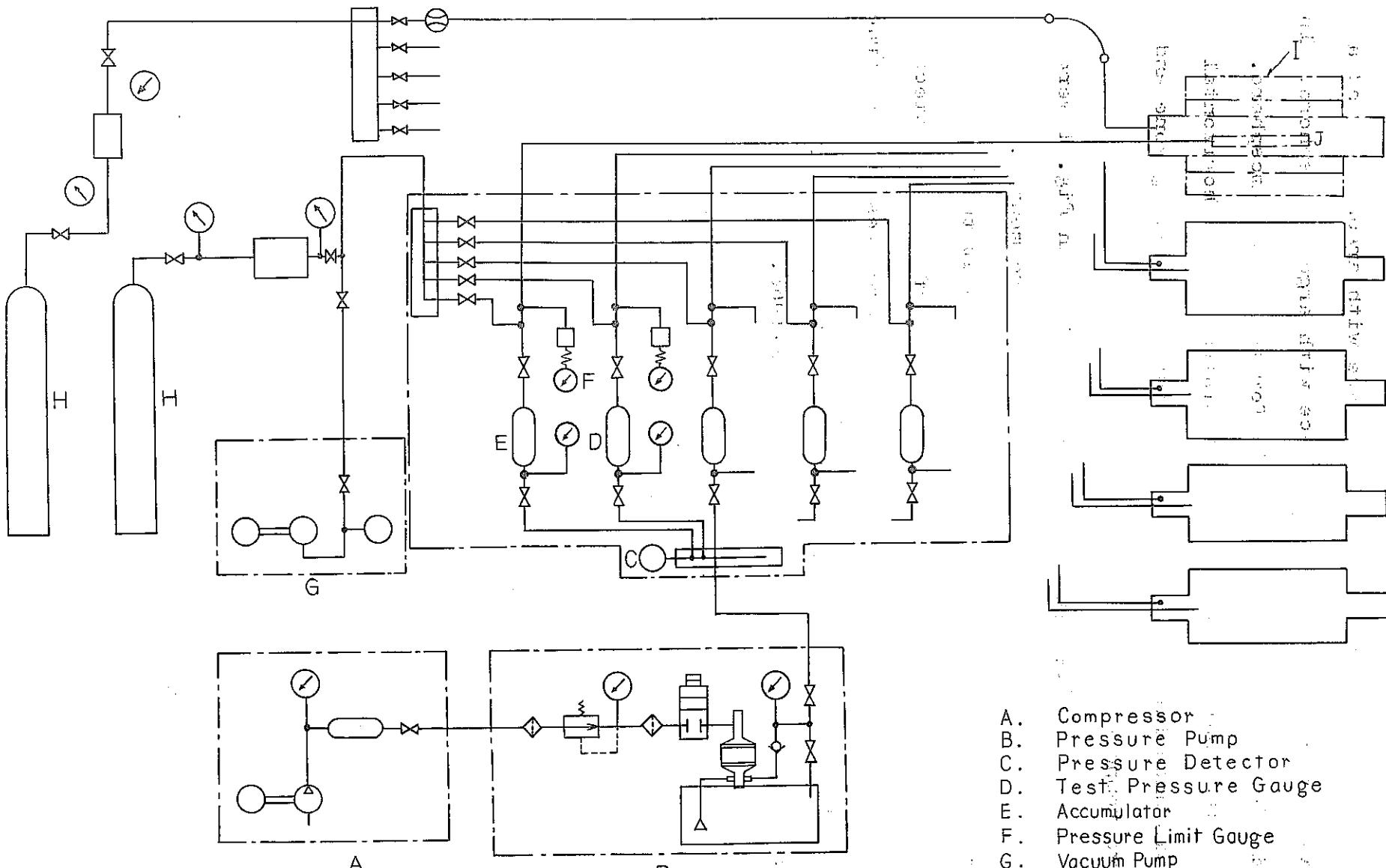
2. Internal Pressure Creep Rupture Test

Fig. 2 shows the piping system of the test equipment. Its working pressure range is 0 - 500 kg/cm², test temperature range 200 - 800°C. It is consisted of a pressurizer, a pressure regulator, an atmospheric apparatus and a temperature controller. The pressurizer, which operates a pressure pump by a compressor, uses water as the pressure medium to apply a load on the test pressure. In the course of this process, the pressure medium is converted from water to argon gas in the accumulator and applies load on the test piece in the heating furnace. Test pressure is adjusted through the control of the pressure pump by detecting the pressure using a strain gauge type detector. The atmospheric apparatus is provided with a vacuum pump to

replace the air inside the test piece with argon gas, and a device to fill the heating furnace with argon atmosphere. In this experiment, we used the air for the outer atmosphere.

The heating apparatus is consisted of five horizontal resistance furnaces with 5 temperature controlling zone and five temperature controllers.

In this test, the test pieces as shown in Fig. 1 were used, and argon gas was used as the pressure medium. The temperature of the test piece was measured at the three points by placing thermocouples at the end-plug of the test piece, the conduit tube and the center of the dummy test piece arranged in parallel to the real test piece. Other tests followed the creep rupture test method of JIS Z2272-1968.



- A. Compressor
- B. Pressure Pump
- C. Pressure Detector
- D. Test Pressure Gauge
- E. Accumulator
- F. Pressure Limit Gauge
- G. Vacuum Pump
- H. Argon Gas Container
- I. Heating Furnace
- J. Test Piece

Fig. 2. Internal Pressure Creep Testing equipment

V. Test Results

1. Results of High Temperature Tensile Test

Table 1-1, 1-2, and Fig. 3 show the results of the high temperature tensile test.

Both materials of A and B showed similar values as to their tensile strength and proof stress, showing an approximately linear decline as temperature going up from 600°C to 750°C. While their elongation showed an increase as temperature rising, and scatter range was comparatively small. Both the strength and elongation satisfied the requirements at 650°C of PNC (0.2% proof stress : above 20 kg/mm², tensile strength : above 30 kg/mm², elongation : above 15%).

2. Results of Internal Pressure Creep Rupture Test

Table 2 and Fig. 4 show the results of the internal pressure rupture test at 650°C.

Table 1-1. Results of High Temperature Tensile Test

A-material

Temperature °C	Test Pieces No.	0.2% Proof Stress, Kg/mm ²	Tensile Strength, Kg/mm ²	Elongation, %
600	K2771	42.9	51.6	16.8
	K2795	42.4	51.2	16.0
	K2746	41.7	50.8	18.0
650	K2722	35.6	43.2	20.0
	K2756	36.4	45.9	18.0
	K2792	36.5	44.3	17.8
700	K2737	30.3	35.8	26.4
	K2778	30.9	36.4	24.2
	K2789	30.4	36.4	24.8
750	K2738	24.2	29.1	27.8
	K2752	24.1	29.1	30.0
	K2764	-	-	-

Note 1: The proof stress and rupture elongation are measured as G.L = 50 mm

Note 2: The cross section area: 6.6 mm²

Table 1-2. Results of High Temperature Tensile Test

B-material

Temperature °C	Test Pieces No.	0.2% Proof Stress, Kg/mm ²	Tensile Strength, Kg/mm ²	Elongation, %
600	S0514	44.1	53.4	20.2
	S0510	44.1	52.3	15.6
	S0517	44.0	52.4	15.6
650	S0511	34.9	43.2	23.0
	S0519	37.0	45.0	18.6
	S0515	35.8	44.3	22.2
700	S0512	27.3	36.4	30.0
	S0521	27.6	36.5	29.6
	S0516	28.5	35.2	28.6
750	S0513	22.7	28.0	45.8
	S0518	22.0	28.3	35.6
	S0520	21.2	27.6	34.6

Note 1: The proof stress and rupture elongation are measured as G.L = 50 mm

Note 2: The cross section area: 6.6 mm²

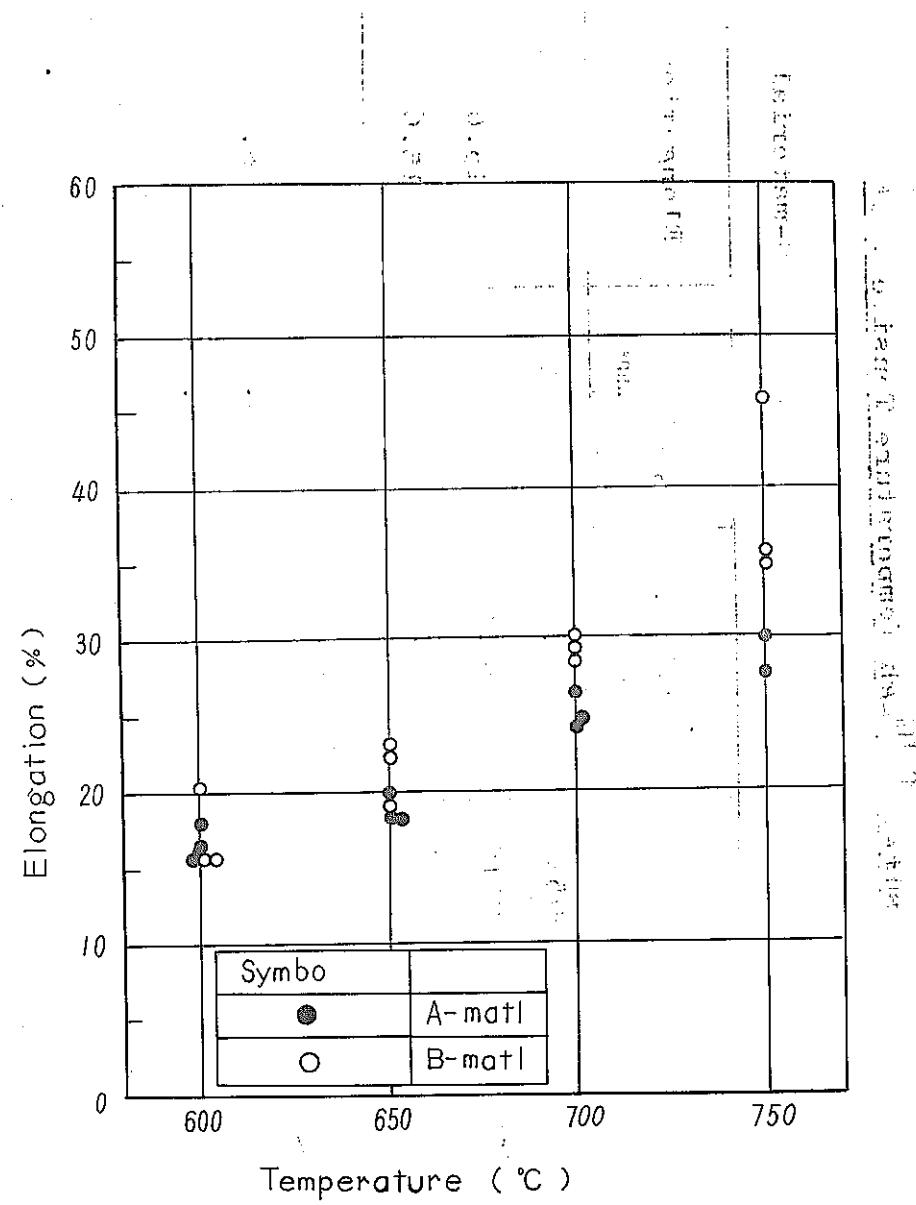
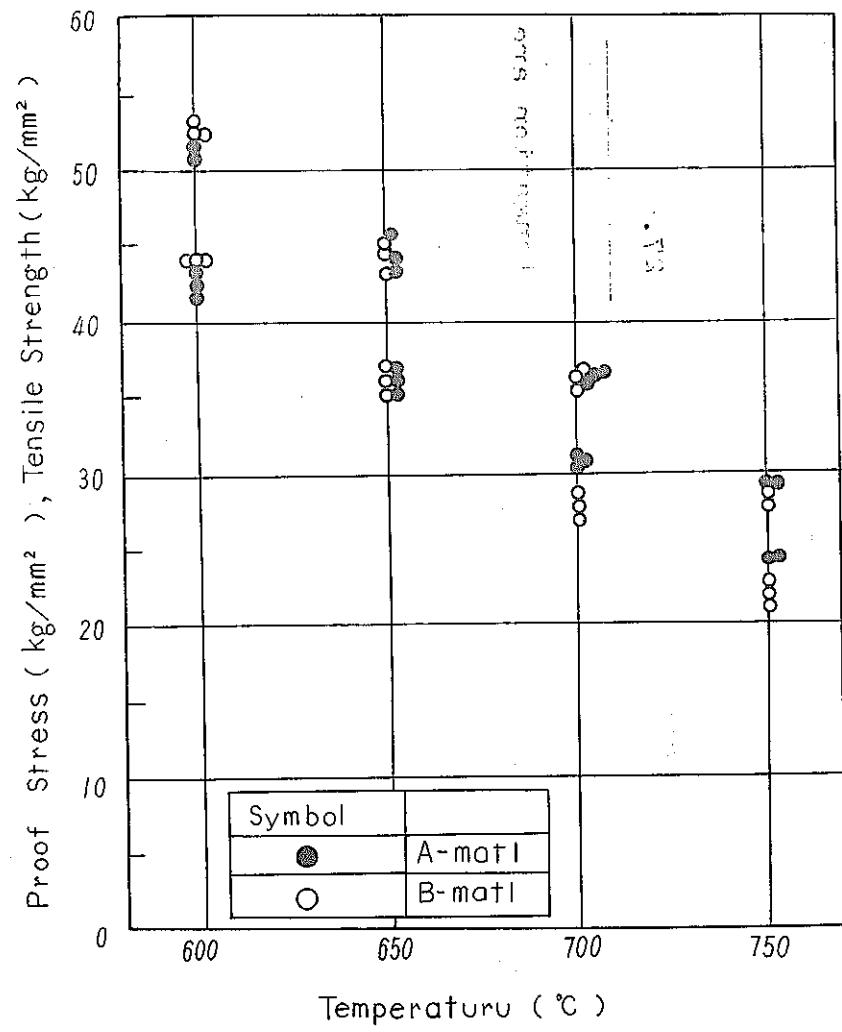


Fig. 3. Result of High Temperature Tensile Test

Table 2. Result of Internal Pressure Creep Rupture Test

Temperature, °C		Test Pieces No.	Test Pressure, Kg/cm ²	Rupture Time, hr.
650	A- material	K2703-5	300	171.2
		K2705-6	270	397.0
		K2701-5	240	1406.4
		K2706-3	210	3165.5
650	B- material	S0522-1	280	56.6
		S0526-8	210	364.8
		S0528-5	170	1161.0
		S0523-6	140	1851.0
		S0524-7	140	2005.2

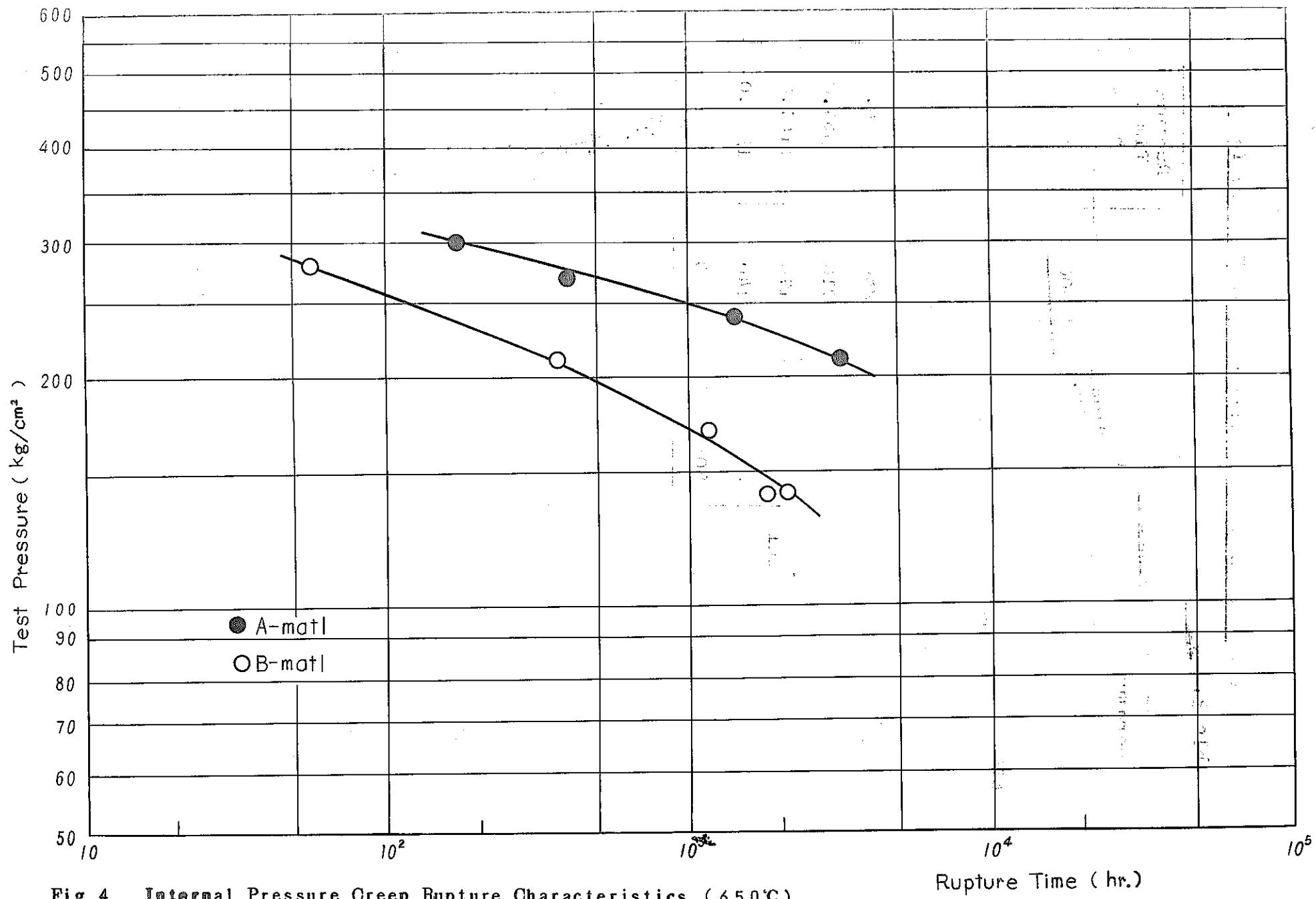


Fig. 4. Internal Pressure Creep Rupture Characteristics (650°C)

3. Examination of Ruptured Test Pieces

The result of the examination of test pieces after the creep rupture test is given as follows:

Test Piece No.	Temperature °C	Internal Pressure Kg/cm ²	Rupture Time h	Photographing of Appearance	Measurement of Dimension	Optical Microscopic Observation	Hardness Measurement
K2703-5	650	300	171.2	○			
K2705-6	"	270	397.0	○ ○			
K2701-5	"	240	1406.4	○ ○			
K2706-3	"	210	3165.5	○ ○			
S0522-1	"	280	56.6	○ ○			
S0526-8	"	210	364.8	○ ○			
S0528-5	"	170	1161.0	○ ○			
S0523-6	"	140	1851.0	○ ○			

Beside the above, the observation of optical microstructure and hardness measurement were carried out on the following two test pieces before the test:

A-material K2708-9

B-material S0532-8

The results are given as follows:

(1) Appearance of ruptured test pieces are shown in Photo-1. The arrows indicate the ruptured portions. The remarkable deformation at the ruptures was caused by the strike against the wall of the heating furnace at the time of rupture.

(2) The results of the after-test dimensional measurement of the test pieces are shown in Table 3-1 - 3-8 and Fig. 5-1 - 5-8. The measurement was performed on the outside diameters of test pieces by use of a micrometer. The measuring points were at 19 different positions at intervals of 10 mm from each other, and at 4 positions in each same cross section.

(3) The optical microstructures of the cross sections and the longitudinal sections of the test pieces prior to the tests are shown in Photo 2-1 and 2-2. Villella was used as the etching reagent.

The microstructures of the cross sections and the longitudinal sections of the test pieces after the tests are shown in Photo 3-1 - 3-4.

(4) The hardness measurement results of the cross sections and the longitudinal sections of the test pieces prior to tests are given by the following table:

Test Piece No.	Hardness, H_v , 500 g											
	Longitudinal Section						Cross Section					
	1	2	3	4	5	Aver- age	1	2	3	4	5	Aver- age
K2708-9	276	278	276	276	274	275	276	266	264	266	258	266
S0532-8	272	274	267	265	276	271	260	267	271	265	263	265

The hardness measurement results of ruptured test pieces which had the longest rupture time and of which hardness was measured at the reverse side of the rupture in the longitudinal direction at each 10 mm interval are given in Table 4-1 and 4-2 respectively.

VI. Conclusion

The third program of the experiment has undertaken the high temperature tensile test and the internal pressure creep rupture test of FBR's fuel cladding tube (SUS316), and has confirmed the high temperature strength characteristics of materials as well as examined the post-test structural change of the test pieces.

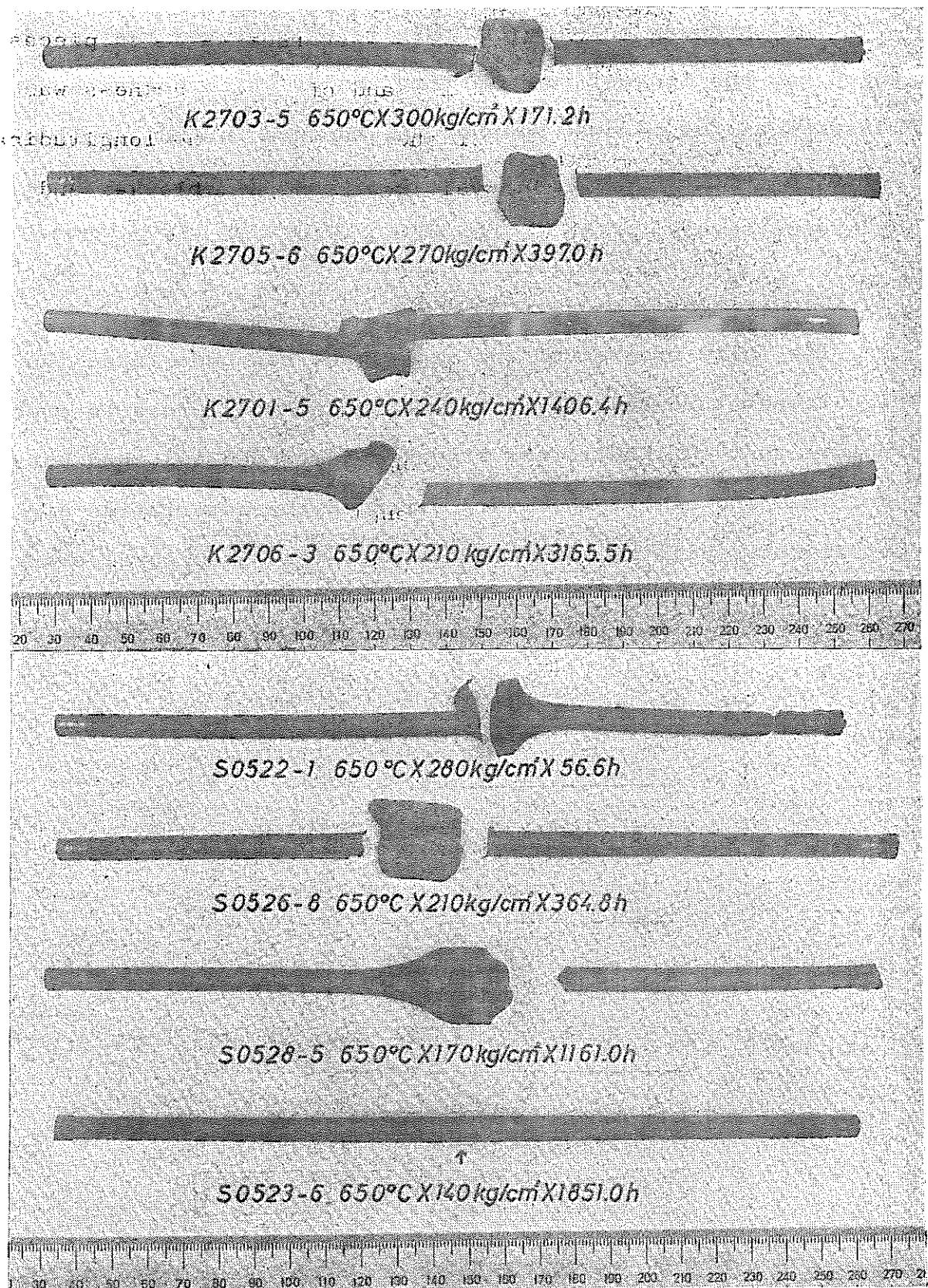


Photo 1. Appearance of Internal Pressure Creep Rupture
Test Pieces.

Table 3-1 Outside Diameters Measured after Internal Pressure Creep Rupture Test

Test Piece No. (Test Condition)	Position	Conduit tube side)										Outside Diameters, mm										(End plug side)			
		1	2	3	4	5	6	7	8	9	10	11	12	13	14	15	16	17	18	19					
K2703-5 Temp.: 650°C Prssr.: 300 kg/cm ² Puncture Time : 1712 h	A	6.46	6.50	6.55	6.56	6.61	6.60	6.72	—	—	6.71	6.70	6.62	6.59	6.55	6.53	6.50	6.48	6.45	6.43					
	B	6.46	6.50	6.55	6.56	6.62	6.67	6.72	—	—	6.73	6.73	6.61	6.57	6.55	6.52	6.50	6.48	6.45	6.43					
	C	6.46	6.50	6.55	6.56	6.61	6.66	6.73	—	—	6.75	6.73	6.61	6.58	6.55	6.52	6.50	6.48	6.45	6.43					
	D	6.46	6.50	6.55	6.56	6.61	6.65	6.77	—	—	6.74	6.73	6.62	6.59	6.56	6.52	6.50	6.48	6.45	6.43					
	Max.	6.46	6.50	6.55	6.56	6.62	6.67	6.77	—	—	6.75	6.73	6.62	6.59	6.56	6.53	6.50	6.48	6.45	6.43					
		(2.5)	(3.1)	(3.9)	(4.1)	(5.0)	(5.8)	(7.4)	—	—	(7.1)	(6.8)	(5.0)	(4.6)	(4.1)	(3.6)	(3.1)	(2.8)	(2.3)	(2.0)					
	Mean	6.46	6.50	6.55	6.56	6.61	6.66	6.74	—	—	6.73	6.72	6.62	6.58	6.55	6.52	6.50	6.48	6.45	6.43					
		(2.5)	(3.1)	(3.9)	(4.1)	(4.9)	(5.7)	(7.0)	—	—	(6.8)	(6.6)	(5.0)	(4.4)	(3.9)	(3.5)	(3.1)	(2.8)	(2.3)	(2.0)					
	Min.	6.46	6.50	6.55	6.56	6.61	6.65	6.72	—	—	6.71	6.70	6.61	6.57	6.55	6.52	6.50	6.48	6.45	6.43					
		(2.5)	(3.1)	(3.9)	(4.1)	(4.9)	(5.5)	(6.6)	—	—	(6.5)	(6.3)	(4.9)	(4.3)	(3.9)	(3.5)	(3.1)	(2.8)	(2.3)	(2.0)					

Note 1: Figures in () indicate calculated elongation(%). The pre-test outside diameter was 6.302 mm.

Note 2: * indicates the value at the weld-heat affected area.

Note 3: ——shows the ruptured area.

Table 3-2 Outside Diameters Measured after Internal Pressure Creep Rupture Test

Test Piece No. (Test Condition)	Position	Conduit tube side)										Outside Diameters, mm (End plug side)									
		1	2	3	4	5	6	7	8	9	10	11	12	13	14	15	16	17	18	19	
K2705-6	A	6.48	6.49	6.51	6.51	6.54	6.62	6.68	—	—	6.74	6.67	6.72	6.85	6.70	6.57	6.52	6.49	6.48	6.49	
	B	6.47	6.49	6.51	6.51	6.54	6.63	6.65	—	—	6.75	6.68	6.72	6.87	6.68	6.56	6.52	6.50	6.48	6.49	
	C	6.47	8.49	6.51	6.51	6.54	6.65	6.65	—	—	6.76	6.67	6.72	6.88	6.66	6.56	6.52	6.49	6.48	6.48	
	D	6.47	6.48	6.51	6.51	6.54	6.65	6.65	—	—	6.77	6.67	6.72	6.88	6.67	6.56	6.52	6.49	6.48	6.49	
	Max.	6.48	6.49	6.51	6.51	6.54	6.65	6.68	—	—	6.77	6.68	6.72	6.88	6.70	6.57	6.52	6.50	6.48	6.49	
		(2.8)	(3.0)	(3.3)	(3.3)	(3.8)	(5.5)	(6.0)	—	—	(7.4)	(6.0)	(6.6)	(9.2)	(6.3)	(4.3)	(3.5)	(3.1)	(2.8)	(3.0)	
	Mean	6.47	6.49	6.51	6.51	6.54	6.64	6.66	—	—	6.76	6.67	6.72	6.87	6.68	6.56	6.52	6.49	6.48	6.49	
		(2.7)	(3.0)	(3.3)	(3.3)	(3.8)	(5.4)	(5.7)	—	—	(7.3)	(5.8)	(6.6)	(9.0)	(6.0)	(4.1)	(3.5)	(3.0)	(2.8)	(3.0)	
	Min.	6.47	6.48	6.51	6.51	6.54	6.62	6.65	—	—	6.74	6.67	6.72	6.85	6.60	6.56	6.52	6.49	6.48	6.48	
		(2.7)	(2.8)	(3.3)	(3.3)	(3.8)	(5.0)	(5.5)	—	—	(7.0)	(5.8)	(6.6)	(8.7)	(5.7)	(4.1)	(3.5)	(3.0)	(2.8)	(2.8)	

Note 1 : Figures in () indicate calculated elongation(%). The pre-test outside diameter was 6.302 mm.

Note 2 : * indicates the value at the weld-heat affected area.

Note 3 : — shows the ruptured area.

Table 3-3 Outside Diameters Measured after Internal Pressure Creep Rupture Test

Test Piece No. (Test Condition)	Position	Outside Diameters, mm.												(End plug side)						
		1	2	3	4	5	6	7	8	9	10	11	12	13	14	15	16	17	18	19
K2701-5 Temp. : 650°C Prssr. : 240 kg/cm ² Rupture Time : 1406.4 h	A	6.41	6.42	6.46	6.47	6.50	6.54	6.61	6.68	6.76	6.85	—	—	6.67	6.55	6.48	6.45	6.44	6.44	6.40
	B	6.41	6.43	6.46	6.47	6.49	6.53	6.63	6.69	6.78	6.82	—	—	6.68	6.56	6.48	6.45	6.44	6.43	6.40
	C	6.41	6.43	6.46	6.48	6.50	6.54	6.62	6.69	6.79	6.85	—	—	6.71	6.54	6.49	6.45	6.43	6.43	6.40
	D	6.41	6.43	6.45	6.48	6.50	6.54	6.62	6.68	6.77	6.89	—	—	6.70	6.54	6.48	6.46	6.44	6.43	6.40
	Max.	6.41	6.43	6.46	6.48	6.50	6.54	6.63	6.69	6.79	6.89	—	—	6.71	6.56	6.49	6.46	6.44	6.44	6.40
		(1.7)	(2.0)	(2.5)	(2.8)	(3.2)	(3.8)	(5.2)	(6.2)	(7.8)	(9.3)	—	—	(6.5)	(4.1)	(3.0)	(2.5)	(2.2)	(2.2)	(1.6)
	Mean	6.41	6.43	6.46	6.48	6.50	6.54	6.62	6.69	6.78	6.85	—	—	6.69	6.55	6.48	6.45	6.44	6.43	6.40
		(1.7)	(2.0)	(2.5)	(2.8)	(3.2)	(3.8)	(5.1)	(6.2)	(7.6)	(8.7)	—	—	(6.2)	(4.0)	(2.8)	(2.4)	(2.2)	(2.0)	(1.6)
	Min.	6.41	6.42	6.45	6.47	6.49	6.53	6.61	6.68	6.76	6.82	—	—	6.68	6.54	6.48	6.45	6.43	6.43	6.46
		(1.7)	(1.9)	(2.4)	(2.7)	(3.0)	(3.6)	(4.9)	(6.0)	(7.3)	(8.2)	—	—	(6.0)	(3.8)	(2.8)	(2.4)	(2.0)	(2.0)	(1.6)

Note 1 : Figures in () indicate calculated elongation(%). The pre-test outside diameter was 6,301 mm.

Note 2 : * indicates the value at the weld-heat affected area.

Note 3 : — shows the ruptured area.

Table 3-4 Outside Diameters Measured after Internal Pressure Creep Rupture Test

Test Piece No. [Test Condition]	Position	Outside Diameters, mm.												(End plug side)						
		1	2	3	4	5	6	7	8	9	10	11	12	13	14	15	16	17	18	19
K2706-3 Temp. : 650°C Prssr. : 210 kg/cm ² Rupture Time : 3165.5 h	A	6.44	6.38	6.42	6.44	6.44	6.47	6.51	6.53	6.62	6.69	—	—	—	6.52	6.47	6.42	6.40	6.37	6.38
	B	6.34	6.42	6.42	6.43	6.46	6.48	6.51	6.53	6.63	6.59	—	—	—	6.48	6.45	6.43	6.41	6.38	6.34
	C	6.33	6.44	6.42	6.43	6.46	6.47	6.49	6.53	6.61	6.59	—	—	—	6.49	6.45	6.43	6.41	6.39	6.35
	D	6.37	6.43	6.43	6.44	6.47	6.47	6.51	6.54	6.61	6.60	—	—	—	6.51	6.45	6.43	6.41	6.38	6.37
	Max.	6.44	6.44	6.43	6.44	6.47	6.48	6.51	6.54	6.63	6.69	—	—	—	6.52	6.47	6.43	6.41	6.39	6.38
		(2.2)	(2.2)	(2.0)	(2.0)	(2.7)	(2.8)	(3.3)	(3.8)	(5.2)	(6.2)	—	—	—	(3.5)	(2.7)	(2.0)	(1.7)	(1.4)	(1.3)
	Mean	6.37	6.42	6.42	6.44	6.46	6.47	6.51	6.53	6.62	6.62	—	—	—	6.50	6.46	6.43	6.41	6.38	6.36
		(1.1)	(1.9)	(1.9)	(2.2)	(2.5)	(2.7)	(3.3)	(3.6)	(5.1)	(5.1)	—	—	—	(3.2)	(2.5)	(2.0)	(1.7)	(1.3)	(1.1)
	Min.	6.33	6.38	6.42	6.43	6.44	6.47	6.49	6.53	6.61	6.59	—	—	—	6.48	6.45	6.42	6.40	6.37	6.34
		(0.5)	(1.3)	(1.9)	(2.0)	(2.2)	(2.7)	(3.0)	(3.6)	(4.9)	(4.6)	—	—	—	(2.8)	(2.4)	(1.9)	(1.6)	(1.1)	(0.6)

Note 1 : Figures in () indicate calculated elongation(%). The pre-test outside diameter was 6.301mm.

Note 2 : * indicates the value at the weld-heat affected area.

Note 3 : — shows the ruptured area.

Table 3-5 Outside Diameters Measured after Internal Pressure Creep Rupture Test

Test Piece No. (Test Condition)	Position	Outside Diameters, mm													(End plug side)					
		1	2	3	4	5	6	7	8	9	10	11	12	13	14	15	16	17	18	19
S0522-1 Temp.: 650°C Prssr.: 280 kg/cm ² Rupture Time : 56.6 h	A	6.91	6.95	6.68	6.70	6.85	6.87	—	—	—	6.89	6.85	6.76	6.73	6.69	6.65	6.61	6.90	6.60	6.53
	B	6.92	6.78	6.71	6.74	6.80	6.82	—	—	—	6.88	6.85	6.76	6.73	6.69	6.65	6.61	6.80	6.60	6.53
	C	7.01	6.85	6.74	6.77	6.78	6.88	—	—	—	6.88	6.85	6.76	6.73	6.69	6.65	6.61	6.80	6.60	6.53
	D	6.90	6.85	6.74	6.77	6.79	6.87	—	—	—	6.92	6.83	6.75	6.73	6.69	6.65	6.63	6.80	6.60	6.53
	Max.	7.01	6.95	6.74	6.77	6.85	6.88	—	—	—	6.92	6.85	6.76	6.73	6.69	6.65	6.63	6.90	6.60	6.53
		(11.2)	(10.2)	(6.9)	(7.4)	(8.6)	(9.1)	—	—	—	(9.8)	(8.6)	(7.2)	(6.7)	(6.1)	(5.5)	(5.2)	(9.4)	(4.7)	(3.6)
	Mean	6.94	6.86	6.72	6.75	6.81	6.86	—	—	—	6.89	6.85	6.76	6.73	6.96	6.65	6.61	6.83	6.60	6.53
		(10.1)	(8.8)	(6.6)	(7.1)	(8.0)	(8.8)	—	—	—	(9.3)	(8.6)	(7.2)	(6.7)	(6.1)	(5.5)	(4.8)	(8.3)	(4.7)	(3.6)
	Min.	6.90	6.78	6.68	6.70	6.78	6.82	—	—	—	6.88	6.83	6.75	6.73	6.69	6.65	6.61	6.80	6.60	6.53
		(9.4)	(7.5)	(5.9)	(6.3)	(7.5)	(8.2)	—	—	—	(9.1)	(8.3)	(7.1)	(6.7)	(6.1)	(5.5)	(4.8)	(7.9)	(4.7)	(3.6)

Note 1 : Figures in () indicate calculated elongation(%). The pre-test outside diameter was 6.305mm.

Note 2 : * indicates the value at the weld-heat affected area.

Note 3 : — shows the ruptured area.

Table 3-6 Outside Diameters Measured after Internal Pressure Creep Rupture Test

Test Piece No. (Test Condition)	Position	Outside Diameters, mm												(End plug side)						
		1	2	3	4	5	6	7	8	9	10	11	12	13	14	15	16	17	18	19
S0526-8 Temp.: 650 °C Prssr.: 210 kg/cm² Rupture Time 36 48 h	A	6.63	6.67	6.72	6.80	6.90	7.01	7.18	7.18	7.23	—	—	—	7.05	7.00	6.90	6.80	6.75	6.68	6.60
	B	6.63	6.67	6.72	6.80	6.90	7.02	7.18	7.19	7.22	—	—	—	7.05	6.98	6.90	6.81	6.75	6.68	6.60
	C	6.63	6.67	6.71	6.80	6.90	7.03	7.18	7.20	7.20	—	—	—	7.14	6.97	6.90	6.81	6.75	6.68	6.60
	D	6.63	6.67	6.72	6.80	6.90	7.00	7.19	7.21	7.20	—	—	—	7.15	6.95	6.91	6.82	6.75	6.68	6.60
	Max.	6.63	6.67	6.72	6.80	6.90	7.03	7.19	7.21	7.23	—	—	—	7.15	7.00	6.91	6.82	6.75	6.68	6.60
		(5.0)	(5.6)	(6.4)	(7.7)	(9.3)	(11.3)	(13.9)	(14.2)	(14.5)	—	—	—	(13.2)	(10.8)	(9.4)	(8.0)	(6.9)	(5.8)	(4.5)
	Mean	6.63	6.67	6.72	6.80	6.90	7.02	7.18	7.20	7.21	—	—	—	7.10	6.98	6.90	6.81	6.75	6.68	6.60
		(5.0)	(5.6)	(6.4)	(7.7)	(9.3)	(11.2)	(13.7)	(14.0)	(14.2)	—	—	—	(12.4)	(10.5)	(9.3)	(7.8)	(6.9)	(5.8)	(4.5)
	Min.	6.63	6.67	6.71	6.80	6.90	7.00	7.18	7.18	7.20	—	—	—	7.05	6.95	6.90	6.80	6.75	6.68	6.60
		(5.0)	(5.6)	(6.3)	(7.7)	(9.3)	(10.8)	(13.7)	(13.7)	(14.0)	—	—	—	(11.6)	(10.1)	(9.3)	(7.7)	(6.9)	(5.8)	(4.5)

Note 1 : Figures in () indicate calculated elongation(%). The pre-test outside diameter was 6.315mm.

Note 2 : * indicates the value at the weld-heat affected area.

Note 3 : — shows the ruptured area.

Table 3-7 Outside Diameters Measured after Internal Pressure Creep Rupture Test

Test Piece No. [Test Condition]	Position	Conduit tube side										Outside Diameters, mm (End plug side)									
		1	2	3	4	5	6	7	8	9	10	11	12	13	14	15	16	17	18	19	
S0528-7 Temp. : 650 °C Prssr. : 170 kg/cm ² Rupture Time : 116.10 h	A	6.54	6.58	6.63	6.66	6.71	6.80	6.87	—	—	—	6.84	6.80	6.71	6.64	6.59	6.55	6.50	6.47		
	B	6.53	6.59	6.63	6.66	6.72	6.79	6.87	—	—	—	6.90	6.87	6.71	6.65	6.60	6.55	6.50	6.46		
	C	6.54	6.59	6.63	6.67	6.72	6.78	6.88	—	—	—	6.93	6.77	6.71	6.65	6.60	6.56	6.50	6.47		
	D	6.54	6.59	6.63	6.67	6.72	6.78	6.88	—	—	—	6.93	6.76	6.70	6.64	6.60	6.55	6.50	6.47		
	Max.	6.54	6.59	6.63	6.67	6.72	6.80	6.88	—	—	—	6.93	6.80	6.71	6.65	6.60	6.56	6.50	6.47		
		(3.6)	(4.4)	(5.0)	(5.6)	(6.4)	(7.7)	(9.0)	—	—	—	(9.8)	(7.7)	(6.3)	(5.3)	(4.5)	(3.9)	(2.9)	(2.5)		
	Mean	6.54	6.59	6.63	6.67	6.72	6.79	6.88	—	—	—	6.90	6.78	6.71	6.65	6.60	6.55	6.50	6.47		
		(3.6)	(4.4)	(5.0)	(5.6)	(6.4)	(7.5)	(9.0)	—	—	—	(9.3)	(7.4)	(6.3)	(5.3)	(4.5)	(3.7)	(2.9)	(2.5)		
	Min.	6.53	6.58	6.63	6.66	6.71	6.78	6.87	—	—	—	6.84	6.76	6.70	6.64	6.59	6.55	6.50	6.46		
		(3.6)	(4.2)	(5.0)	(5.5)	(6.3)	(7.4)	(8.8)	—	—	—	(8.3)	(7.1)	(6.1)	(5.2)	(4.4)	(3.7)	(2.9)	(2.6)		

Note 1 : Figures in () indicate calculated elongation(%). The pre-test outside diameter was 6,314mm.

Note 2 : * indicates the value at the weld-heat affected area.

Note 3 : _____ shows the ruptured.

Table 3-8 Outside Diameters Measured after Internal Pressure Creep Rupture Test

Test Piece No. (Test Condition)	Position	Outside Diameters, mm										(End plug side)								
		1	2	3	4	5	6	7	8	9	10	11	12	13	14	15	16	17	18	19
S0523-6 Temp. : 650 °C Prssr. : 140 kg/cm ² Rupture Time. 18510 h	A	6.49	6.54	6.58	6.66	6.75	6.85	6.98	7.15	7.24	—	7.28	7.18	7.02	6.91	6.79	6.68	6.63	6.58	6.54
	B	6.49	6.54	6.58	6.66	6.75	6.86	6.98	7.15	7.24	—	7.28	7.19	7.03	6.91	6.78	6.68	6.63	6.59	6.53
	C	6.49	6.54	6.59	6.66	6.75	6.85	6.98	7.15	7.24	—	7.28	7.18	7.02	6.91	6.79	6.68	6.63	6.58	6.53
	D	6.49	6.54	6.58	6.66	6.75	6.85	6.98	7.15	7.24	—	7.28	7.19	7.03	6.91	6.79	6.69	6.63	6.58	6.53
	Max.	6.49	6.54	6.59	6.66	6.75	6.86	6.98	7.15	7.24	—	7.28	7.19	7.03	6.91	6.79	6.69	6.63	6.59	6.54
		(2.9)	(3.7)	(4.5)	(5.6)	(7.0)	(8.7)	(10.6)	(13.3)	(14.8)	—	(15.4)	(14.0)	(11.4)	(9.5)	(7.6)	(6.0)	(5.1)	(4.5)	(3.7)
	Mean	6.49	6.54	6.58	6.66	6.75	6.85	6.98	7.15	7.24	—	7.28	7.19	7.03	6.91	6.79	6.68	6.63	6.58	6.53
		(2.9)	(3.7)	(4.3)	(5.6)	(7.0)	(8.6)	(10.6)	(13.3)	(14.8)	—	(15.4)	(14.0)	(11.4)	(9.5)	(7.6)	(5.9)	(5.1)	(4.3)	(3.5)
	Min.	6.49	6.54	6.58	6.66	6.75	6.85	6.98	7.15	7.24	—	7.28	7.18	7.02	6.91	6.78	6.68	6.63	6.58	6.53
		(2.9)	(3.7)	(4.3)	(5.6)	(7.0)	(8.6)	(10.6)	(13.3)	(14.8)	—	(15.4)	(13.8)	(11.3)	(9.5)	(7.5)	(5.9)	(5.1)	(4.3)	(3.5)

Note 1: Figures in () indicate calculated elongation(%). The pre-test outside diameter was 6.309mm.

2: * indicates the value at the weld-heat affected area.

3: — shows the ruptured area.

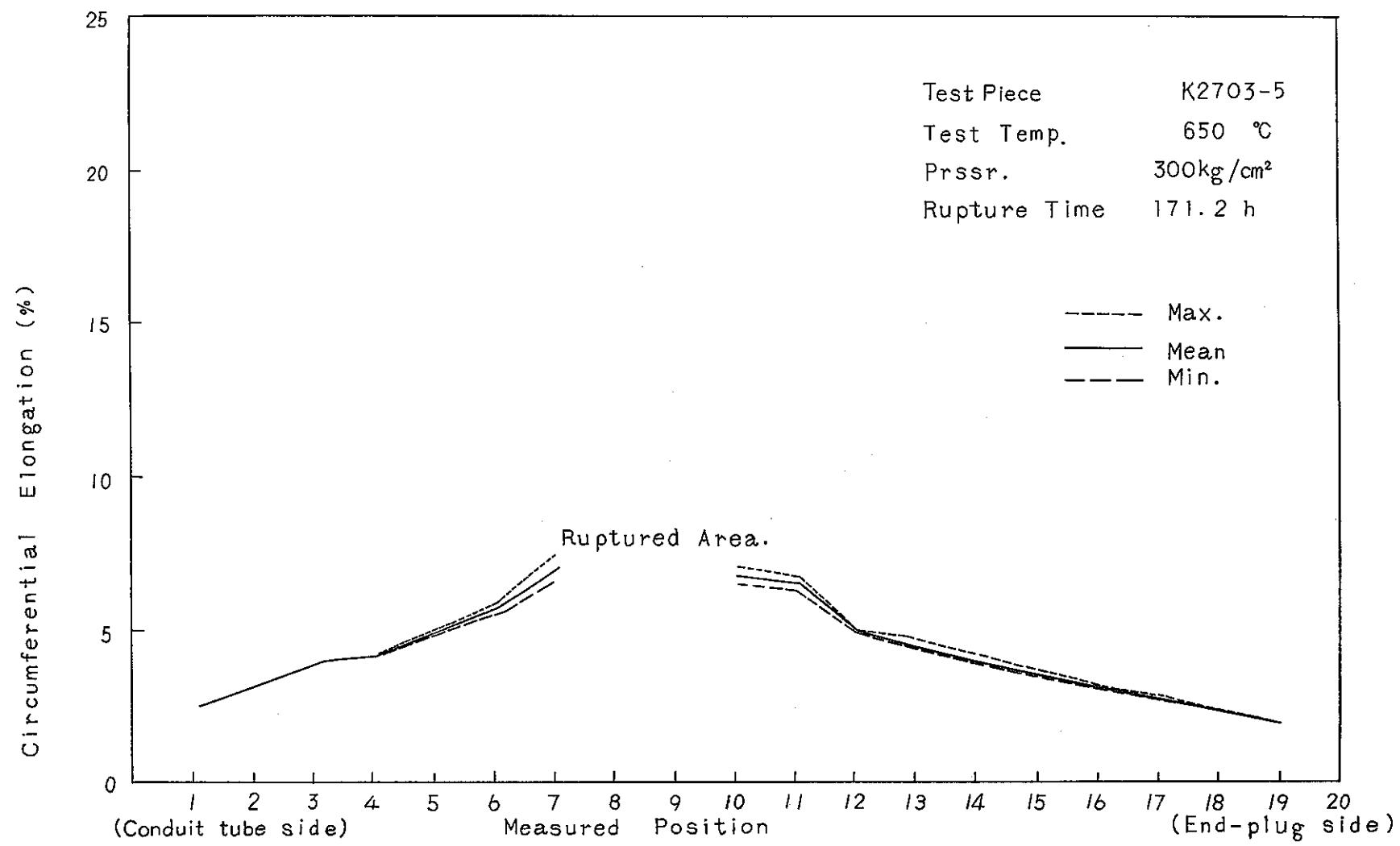


Fig. 5-1. Circumferential Elongation after Internal Pressure Creep Rupture Test

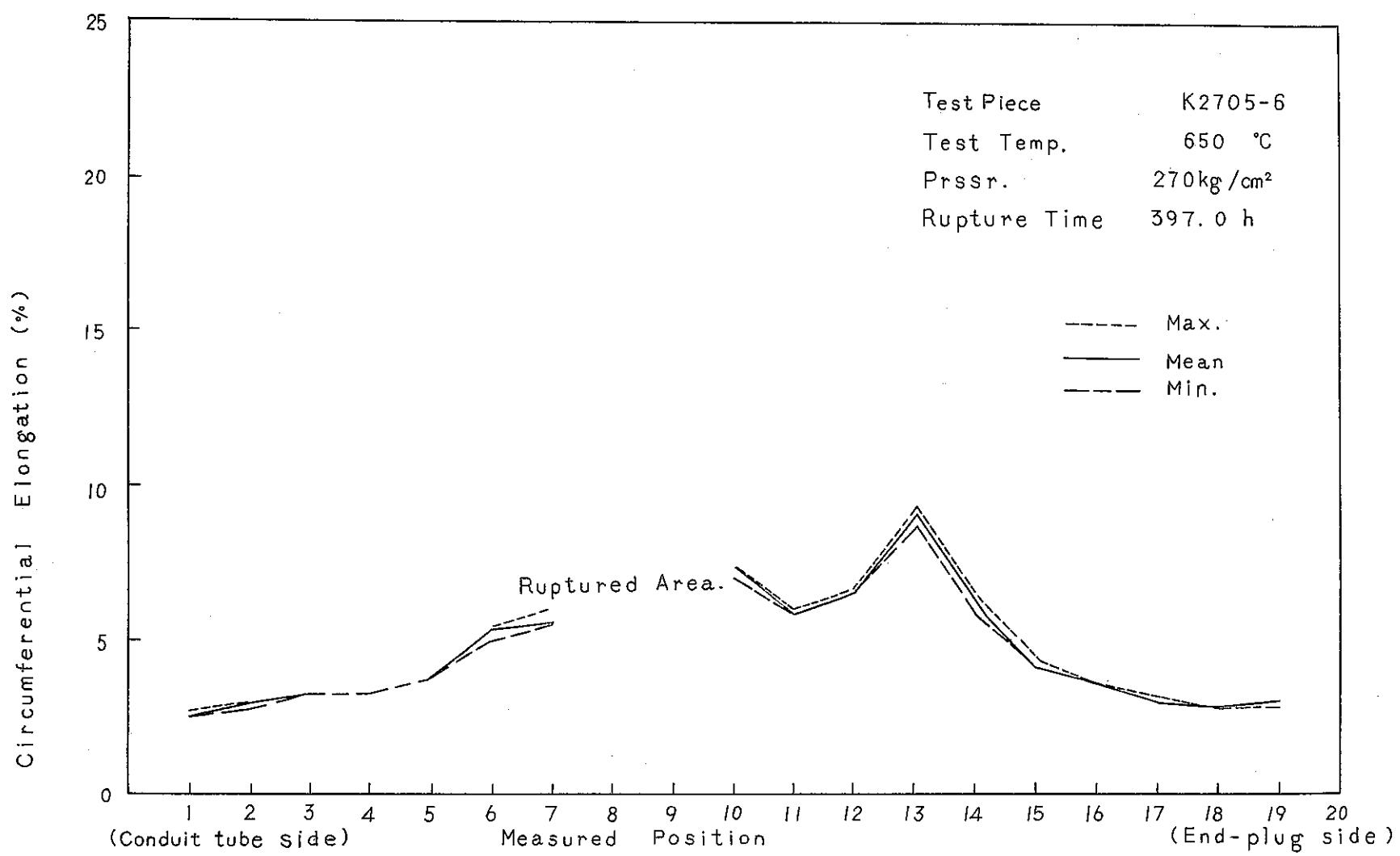


Fig. 5-2. Circumferential Elongation after Internal Pressure Creep Rupture Test

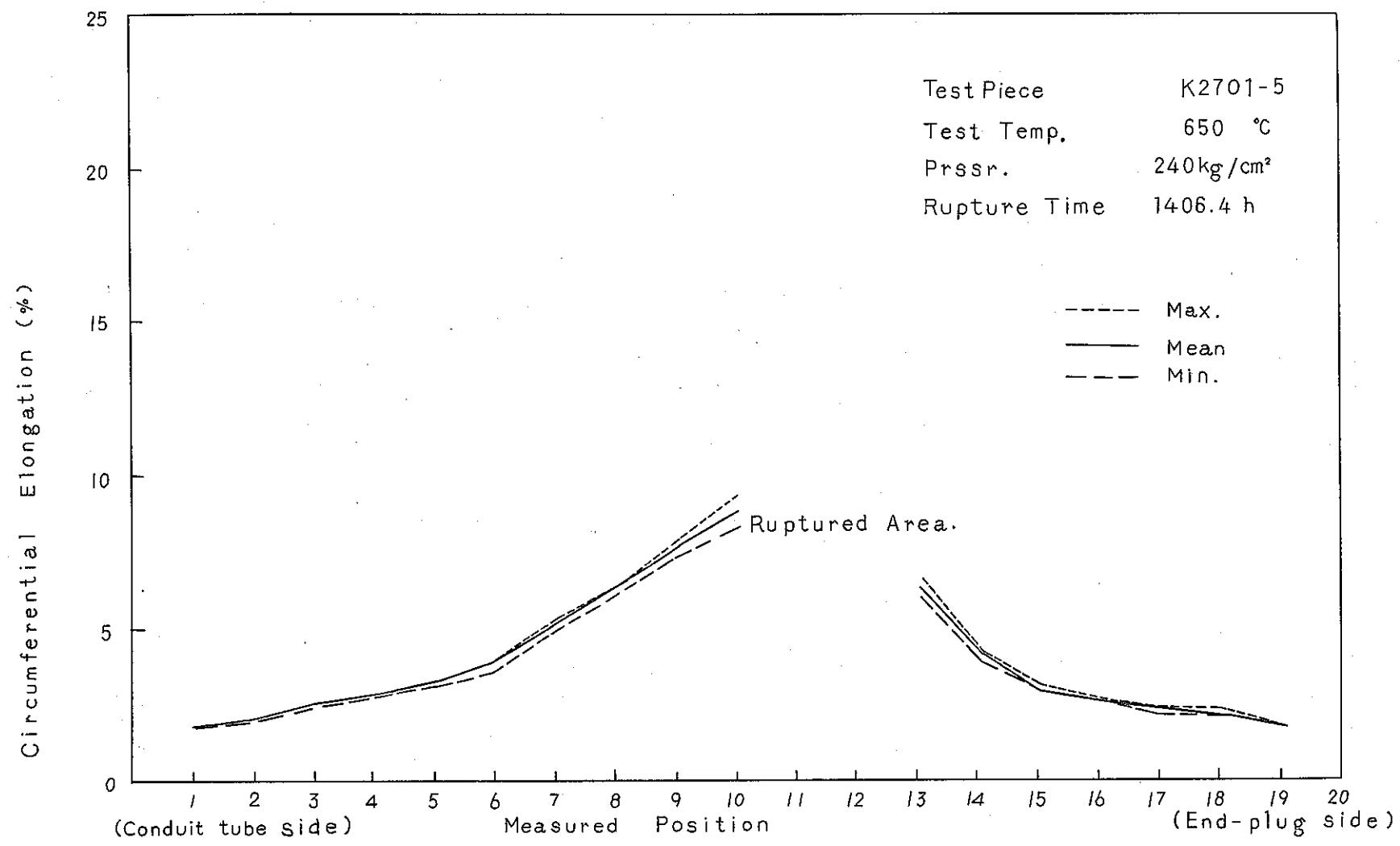


Fig. 5-3. Circumferential Elongation after Internal Pressure Creep Rupture Test

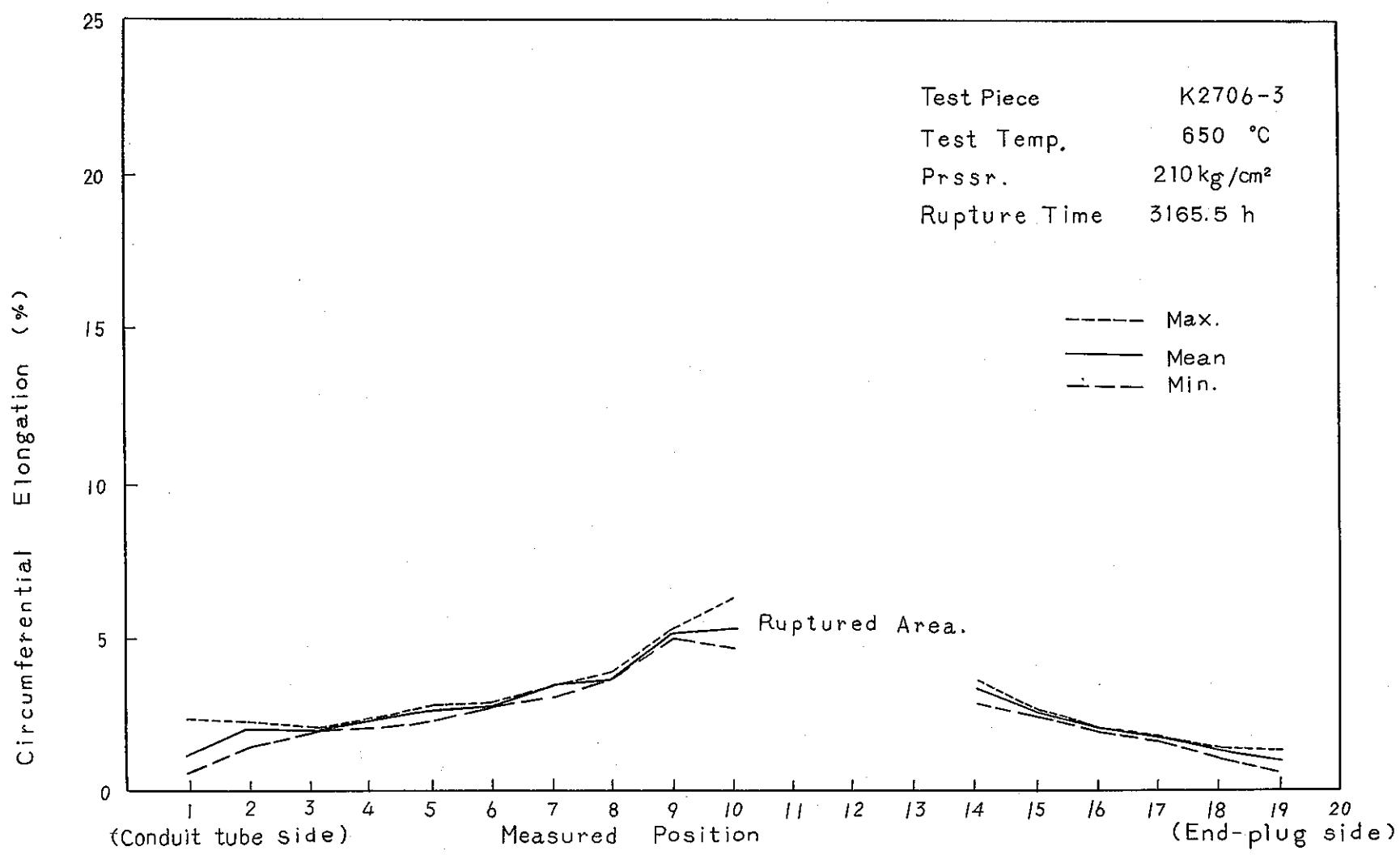


Fig. 5-4. Circumferential Elongation after Internal Pressure Creep Rupture Test

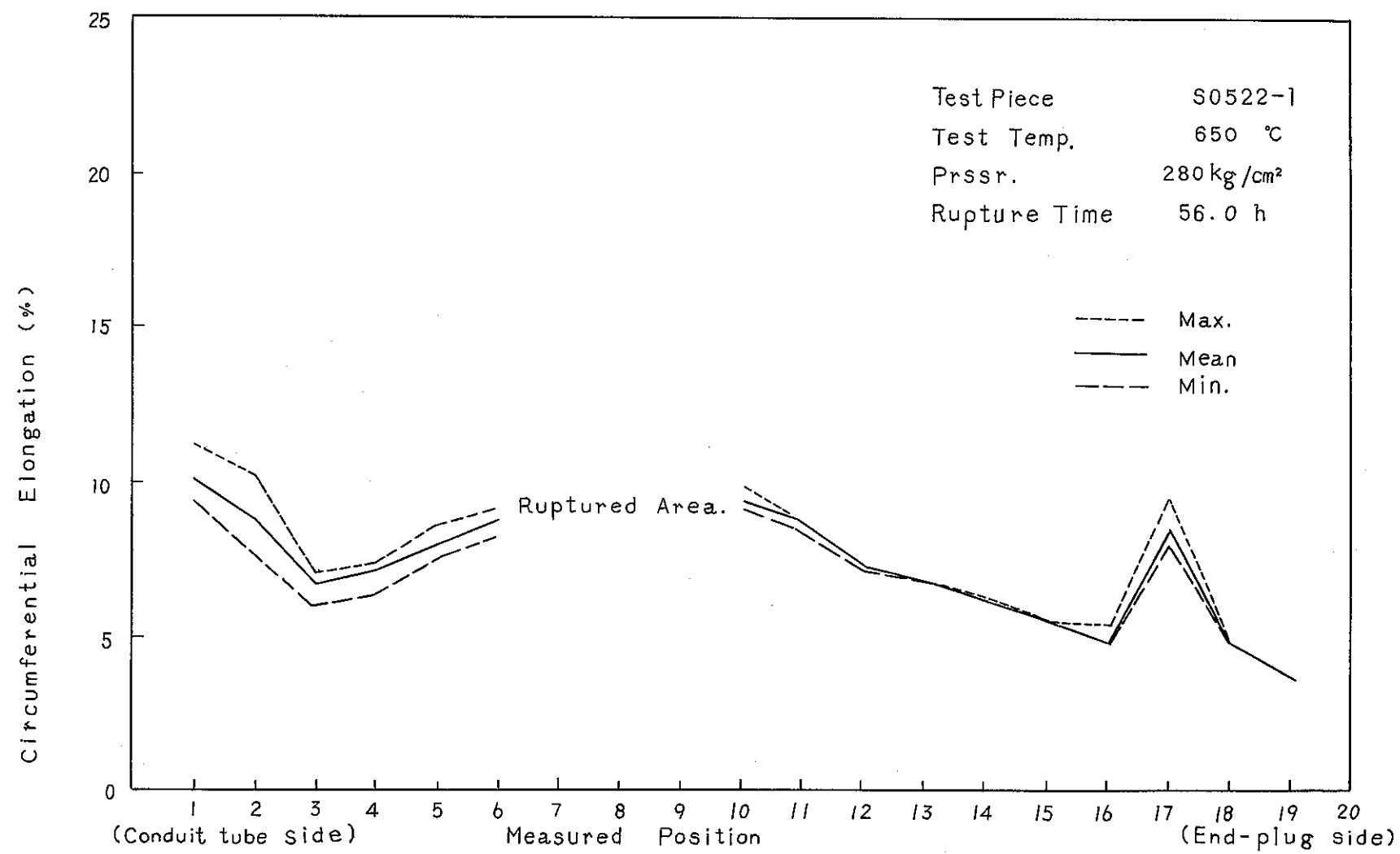


Fig. 5-5. Circumferential Elongation after Internal Pressure Creep Rupture Test

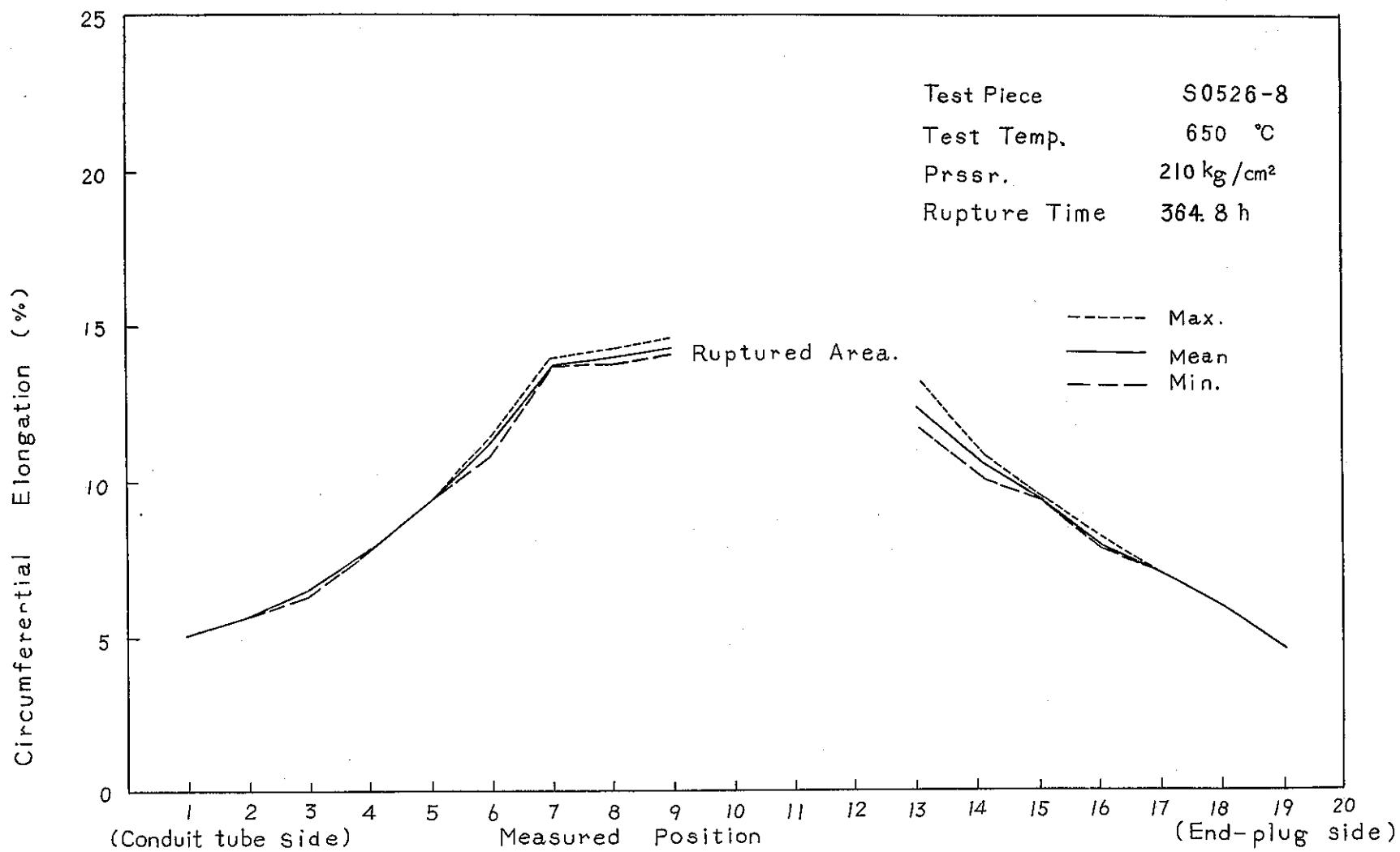


Fig. 5-6. Circumferential Elongation after Internal Pressure Creep Rupture Test

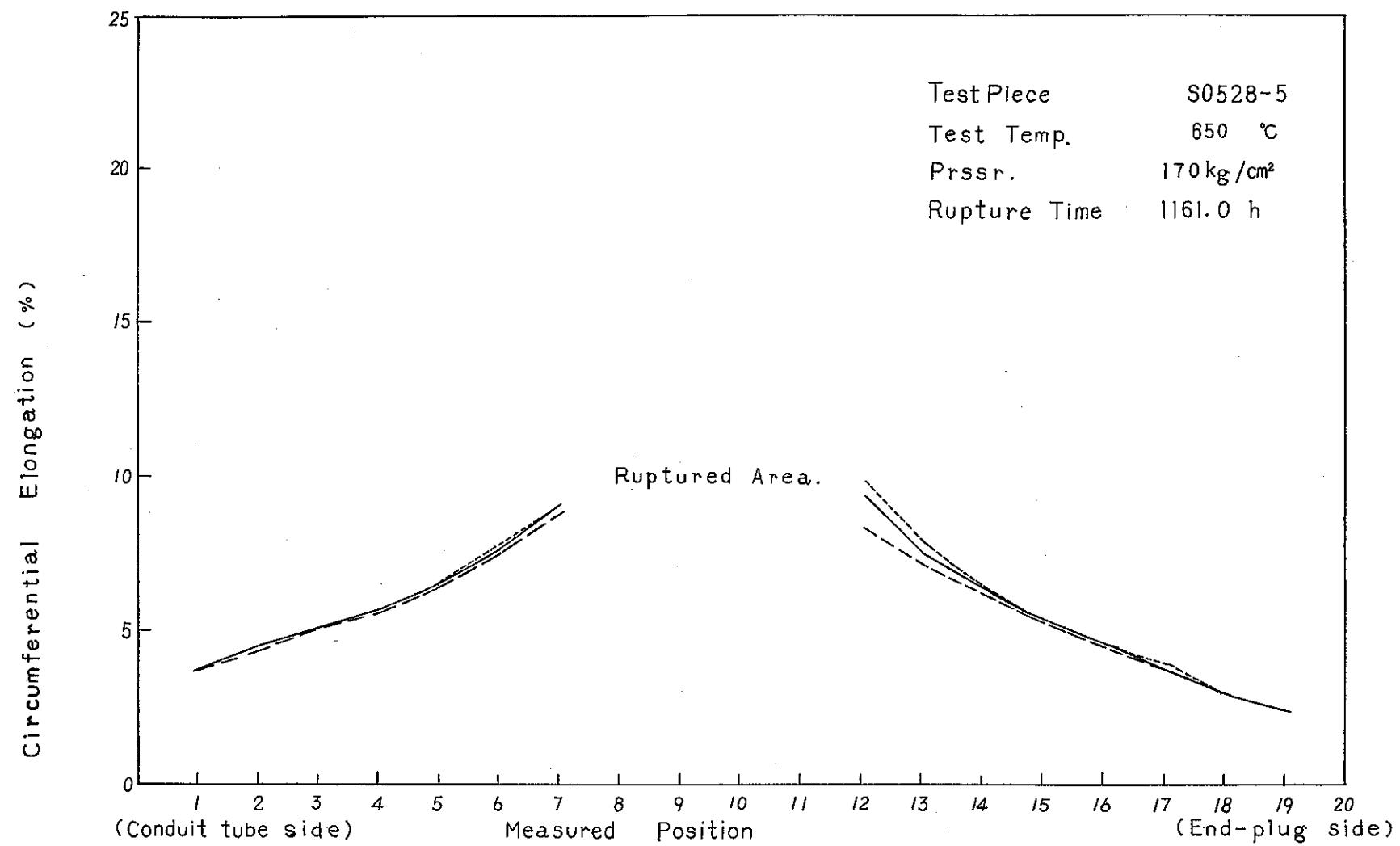


Fig. 5-7. Circumferential Elongation after Internal Pressure Creep Rupture Test

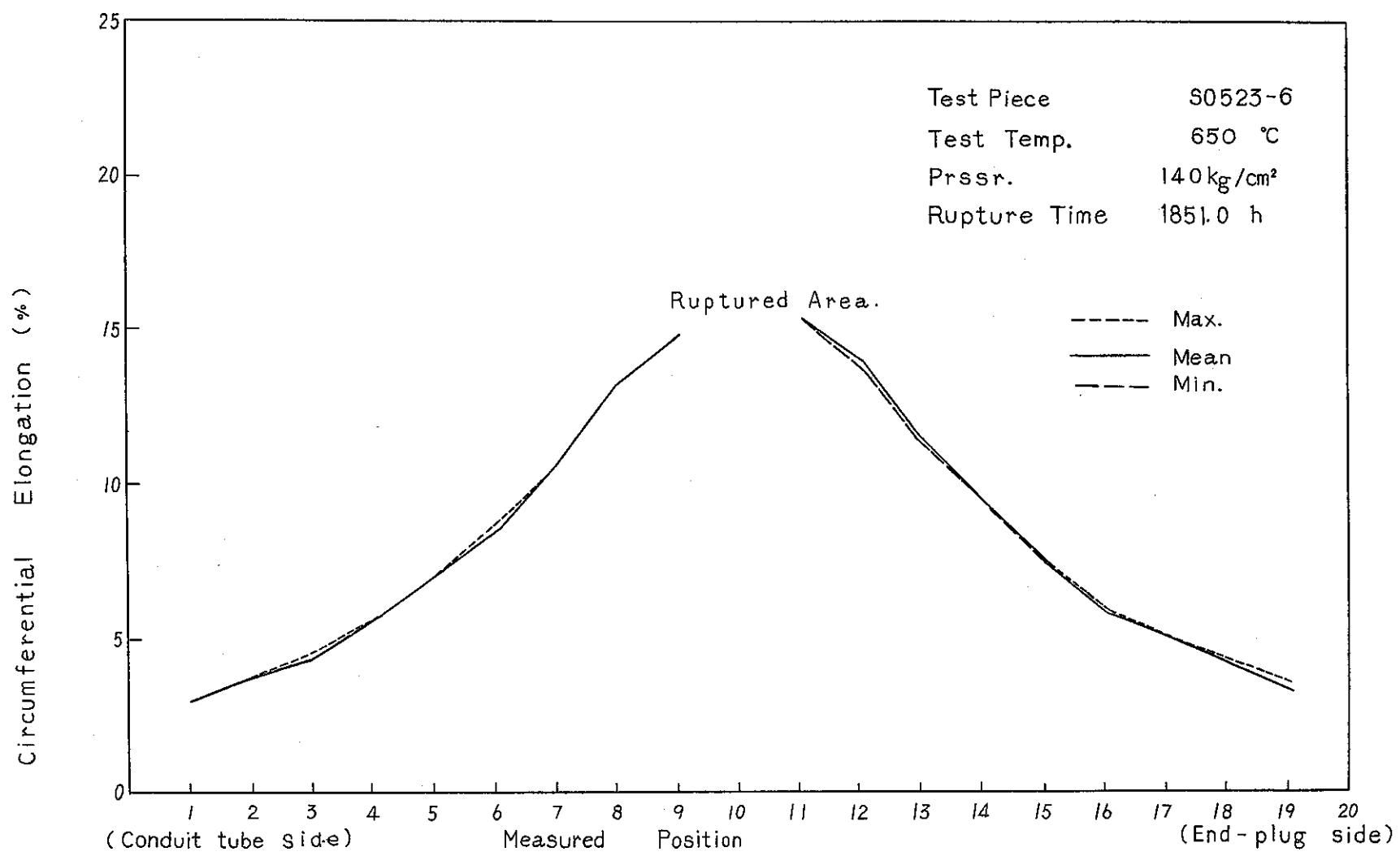
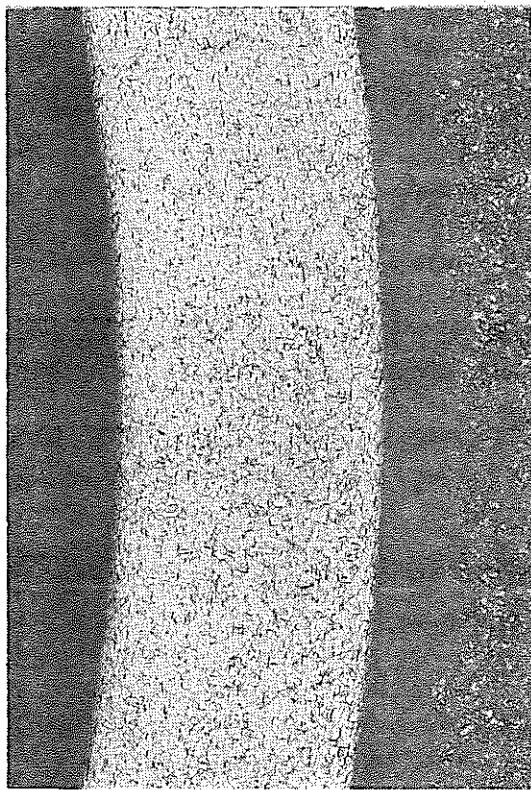
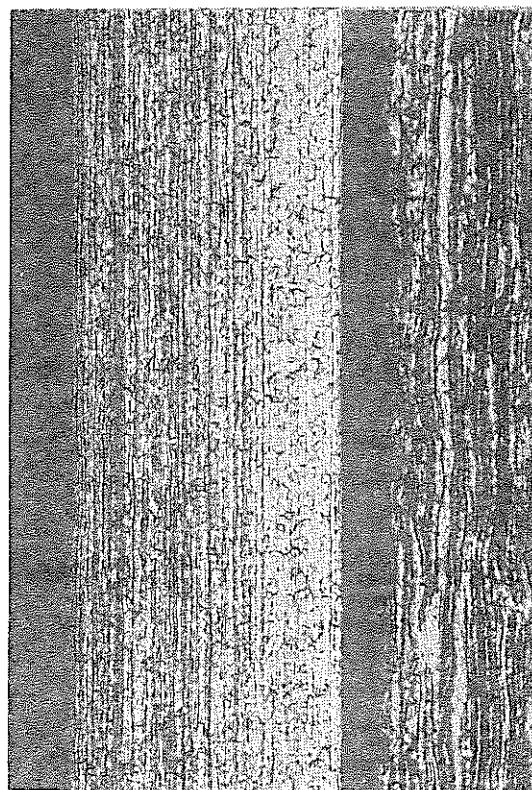


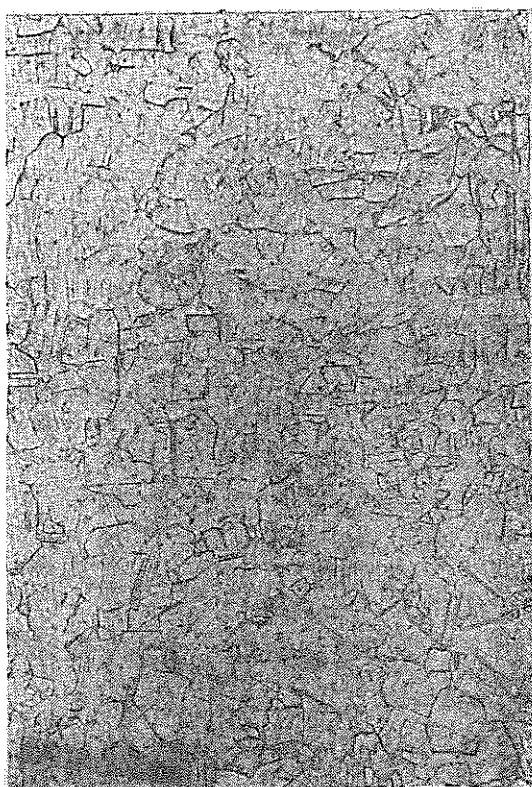
Fig. 5-8. Circumferential Elongation after Internal Pressure Creep Rupture Test



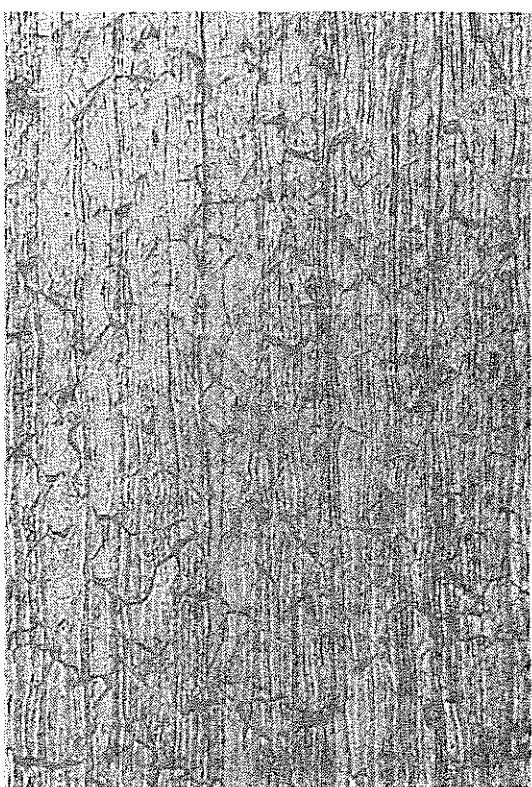
Cross section $\times 100$



Longitudinal section $\times 100$



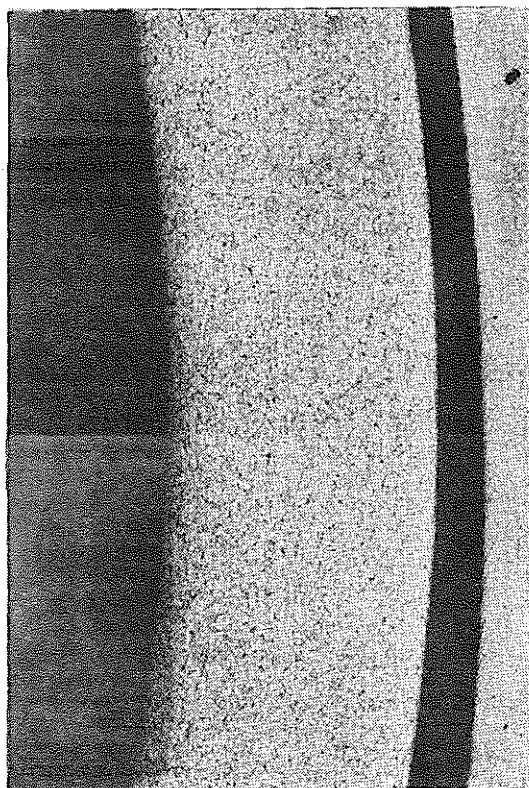
Cross section $\times 500$



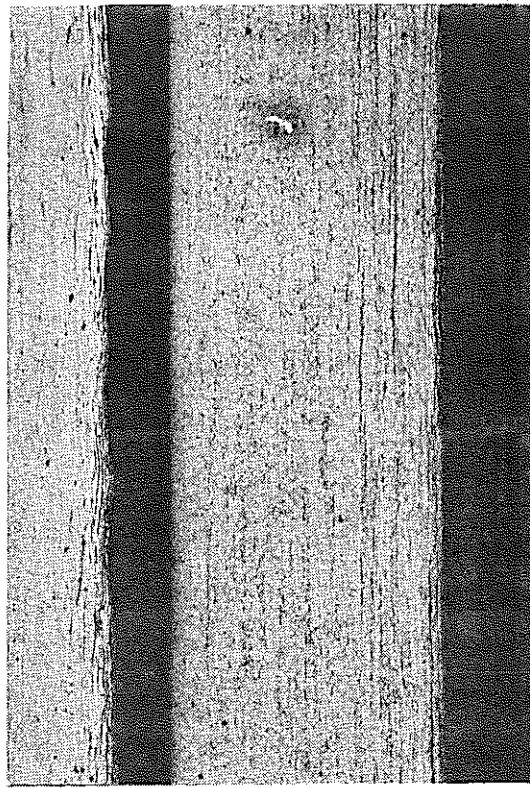
Longitudinal section $\times 500$

Etchant: Villela reagent

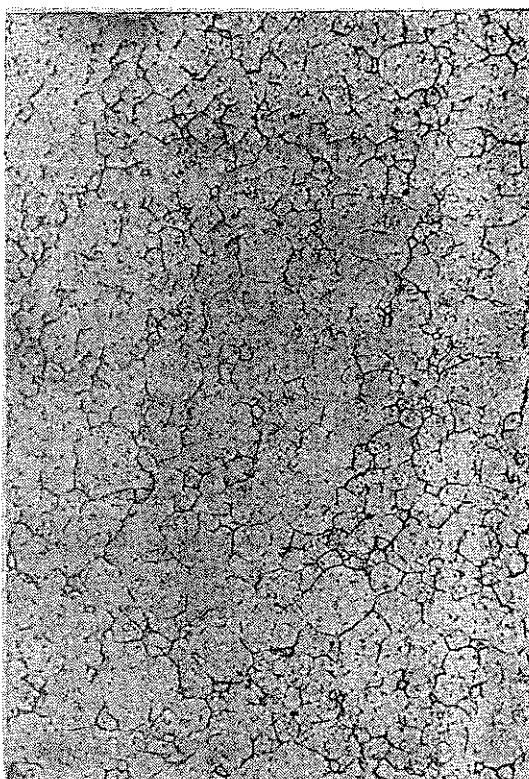
Photo. 2-1. Pre-Test Microstructure (K2708 - 9)



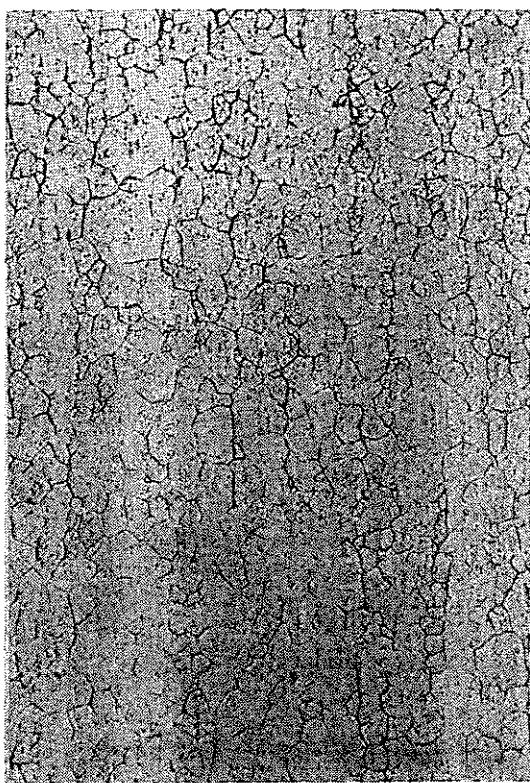
Cross section $\times 100$



Longitudinal section $\times 100$



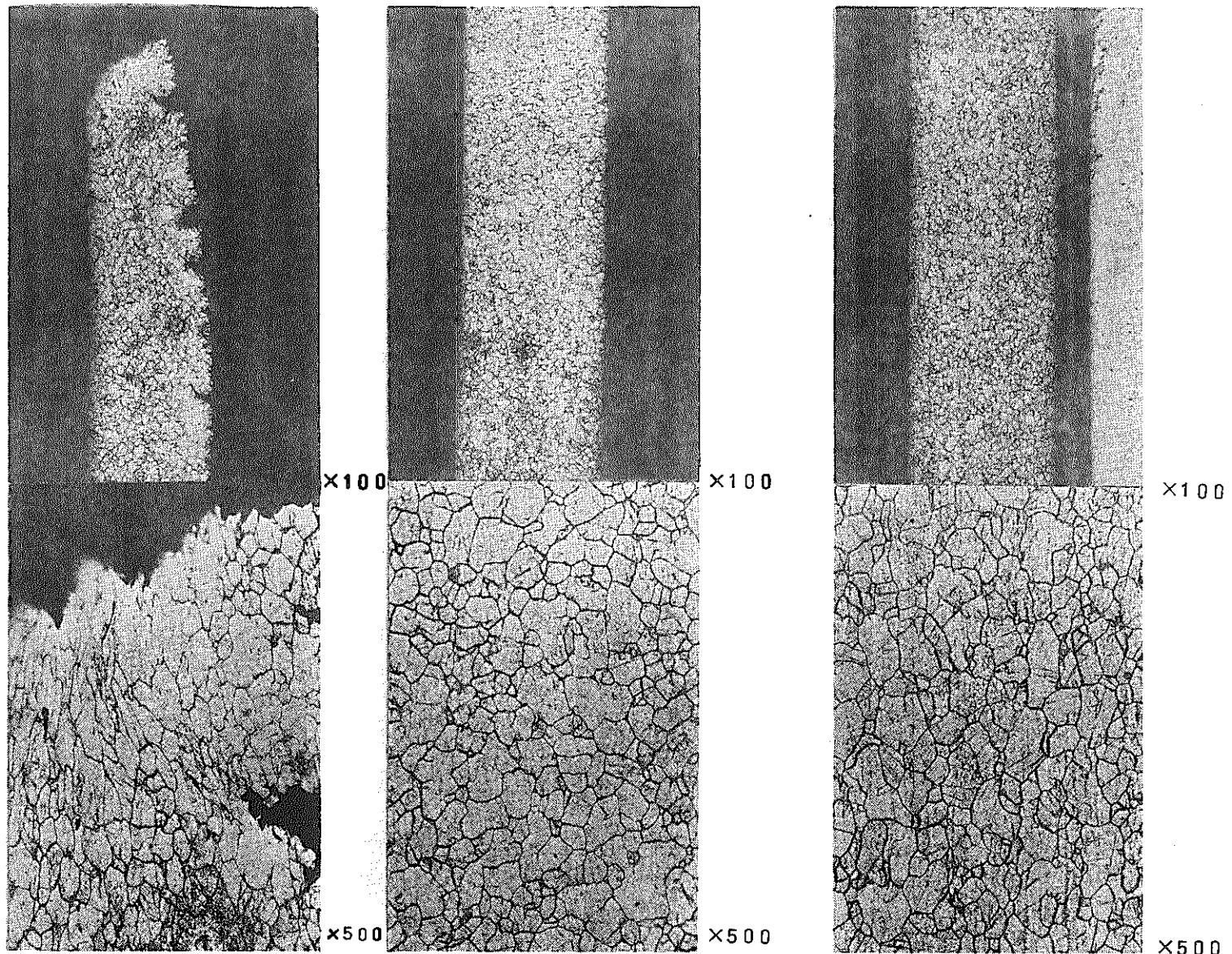
Cross section $\times 500$



Longitudinal section $\times 500$

Etchant: Villela reagent

Photo. 2-2. Pre-Test Microstructure (S0532 - 8)

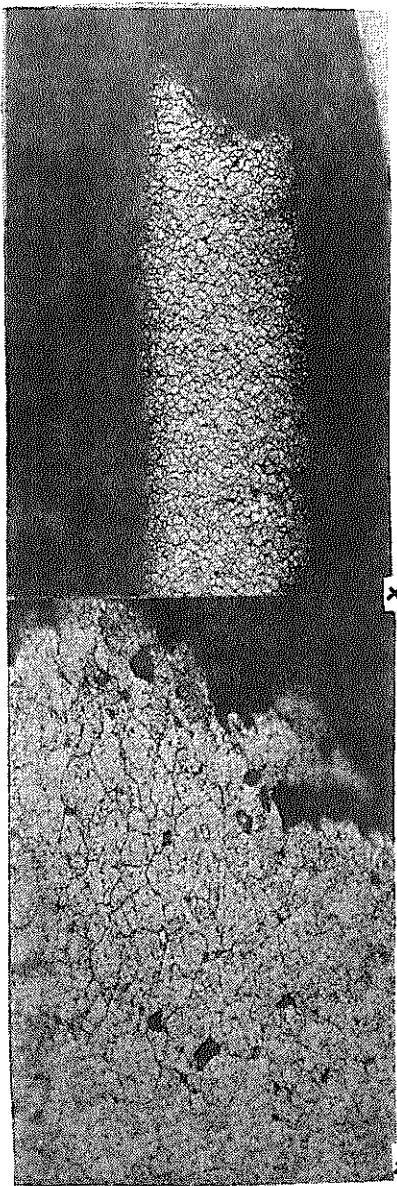


Cross section of ruptured area

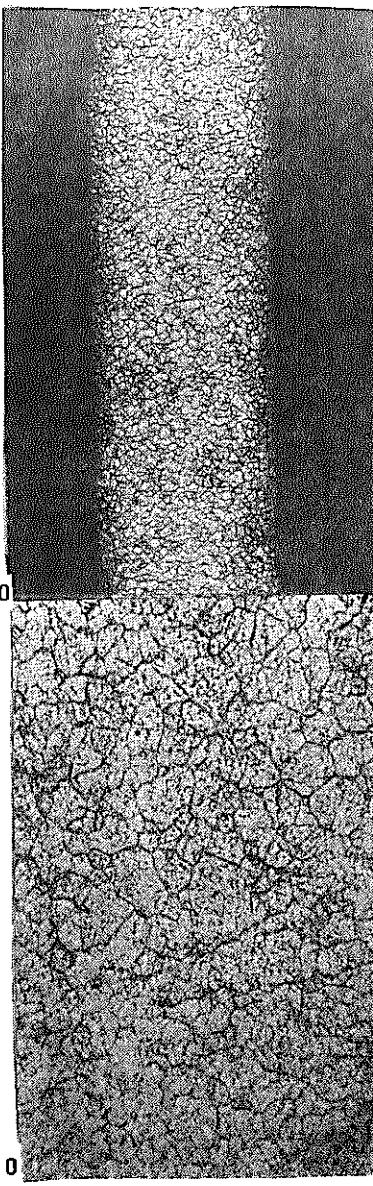
Cross section on the reverse side of ruptured area

Longitudinal section of the reverse side of ruptured area

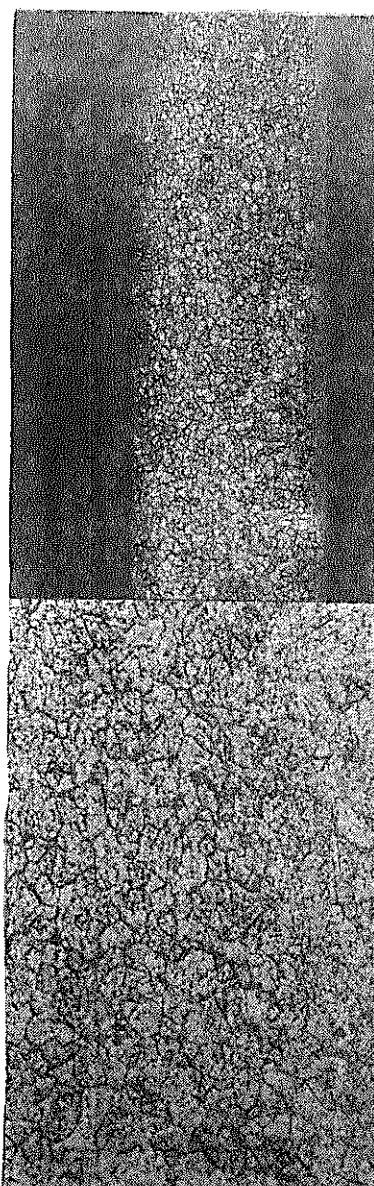
Photo 3-1. Microstructure after Internal Creep Rupture Test (K2701-5 650°C 240kg/cm² 1406.4h)



Cross section of ruptured area

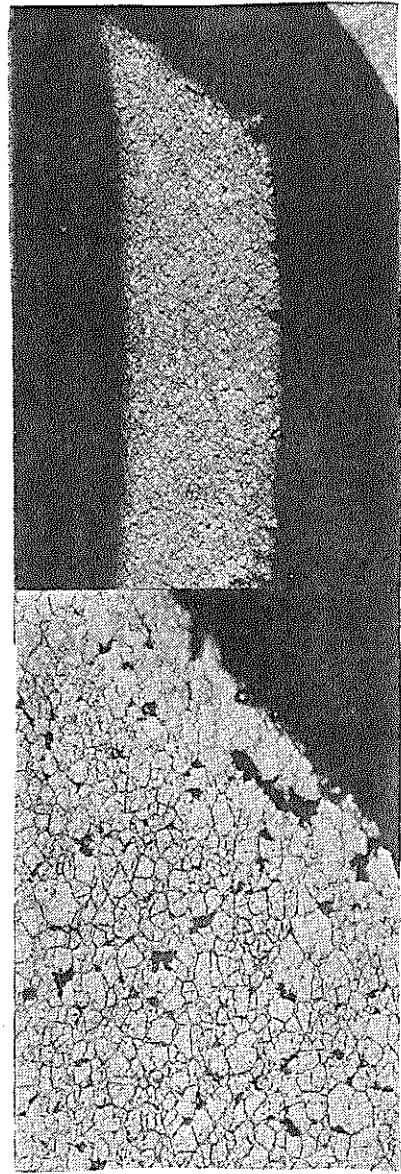


Cross section on the reverse
side of ruptured area



Longitudinal section of the
reverse side of ruptured area

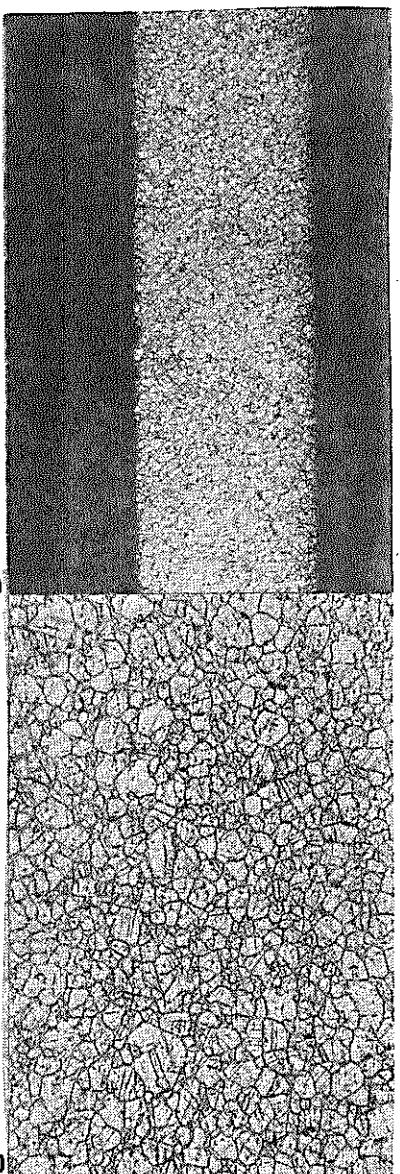
Photo 3-2. Microstructure after Internal Creep Rupture Test (K2706-3 650°C 210kg/cm² 3165.5 h)



×100

×500

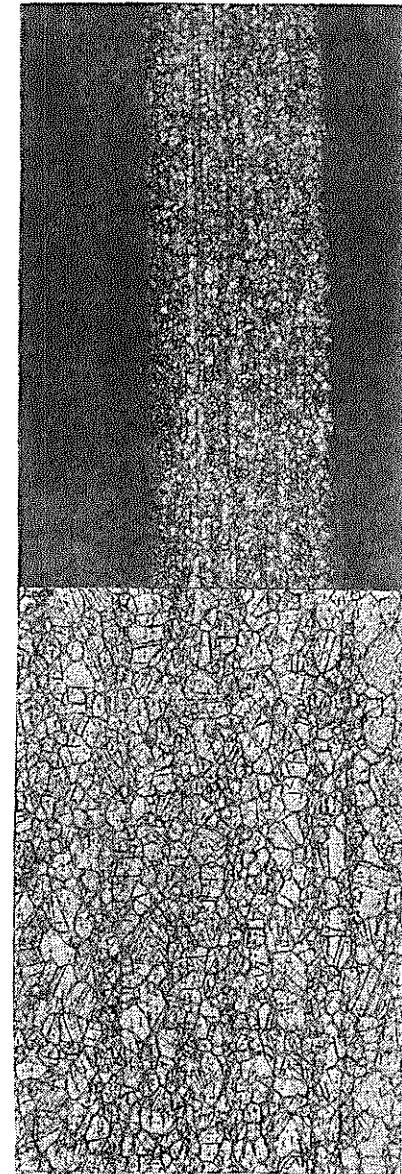
Cross section of ruptured area



×100

×500

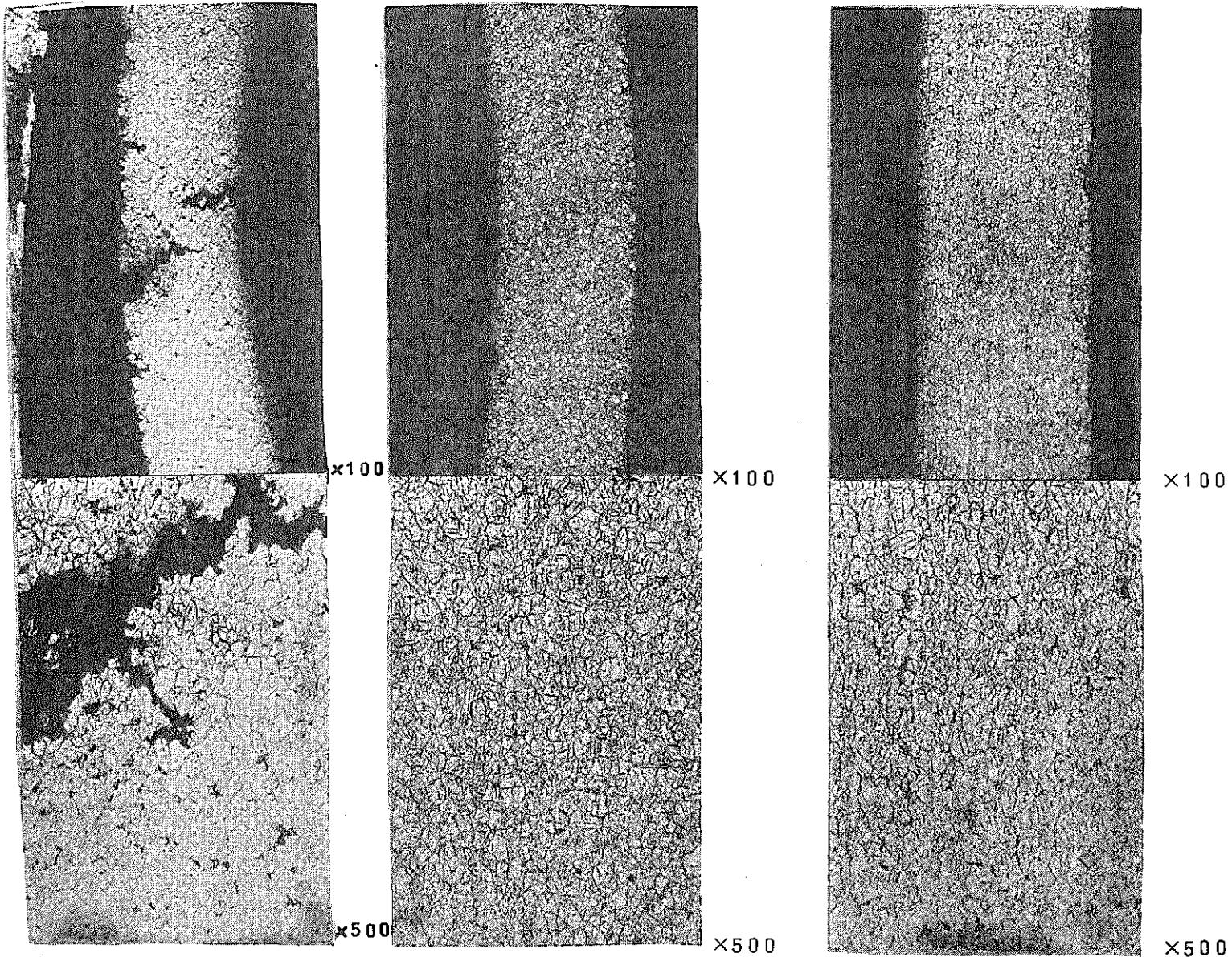
Cross section on the reverse
side of ruptured area



×100

×500

Longitudinal section of the
reverse side of ruptured area



Cross section of ruptured area

Cross section on the reverse
side of ruptured area

Longitudinal section of the
reverse side of ruptured area

Photo 3-4. Microstructure after Internal Creep Rupture Test (S0523-6 650°C 140Kg/cm² 1851.0 h)

Table 4-11 Results of Hardness Measurement after Internal Pressure

Creep Rupture Test.

K2706-3

Position	Hardness, Hv, 500g											
	Longitudinal section						Transverse section					
	1	2	3	4	5	Average	1	2	3	4	5	Average
- 1	256	256	256	256	253	255	258	249	250	249	256	252
- 2	243	247	253	247	227	243	251	247	249	245	247	248
- 3	245	249	243	243	243	245	241	241	249	243	251	245
- 4	251	247	241	243	243	245	247	249	239	241	243	244
- 5	238	245	247	251	254	247	241	252	247	243	241	245
- 6	243	240	247	243	245	244	239	249	227	230	237	236
- 7	227	247	239	227	241	236	242	223	241	239	243	238
- 8	236	226	234	234	234	233	239	239	227	239	210	231
- 9	234	236	243	228	232	235	241	241	242	237	241	240
- 10	240	243	236	236	236	238	229	234	232	232	243	234
- 11	271	269	266	269	271	269	264	252	256	256	247	255
- 12	236	241	243	244	241	241	240	219	245	239	247	238
- 13	245	245	247	251	245	247	251	238	241	245	243	244
- 14	252	256	249	249	251	251	249	249	245	251	253	249
- 15	256	247	247	247	247	249	243	251	247	249	251	248
- 16	256	258	249	247	253	253	249	273	283	281	254	268
- 17	254	256	267	256	260	259	270	269	264	266	271	268

Note : Hardness measurement was performed on both longitudinal and transverse sections on the reverse side of the ruptured area at intervals of 10mm in the longitudinal direction.

Table 4-2 Results of Hardness Measurement after Internal Pressure
Creep Rupture Test.
S0523-6-1~18

Position	Hardness, Hv, 500g											
	Longitudinal section						Transverse section					
	1	2	3	4	5	Average	1	2	3	4	5	Average
- 1	278	247	236	238	238	247	237	236	239	236	234	236
- 2	238	243	241	236	239	239	237	243	234	239	234	237
- 3	239	236	230	232	236	235	236	239	234	239	234	236
- 4	269	254	253	245	240	252	230	227	230	225	227	228
- 5	215	234	234	228	228	228	227	220	241	236	236	232
- 6	212	228	232	226	225	225	230	234	216	216	225	224
- 7	232	225	223	218	225	225	206	223	220	213	212	215
- 8	238	234	234	227	226	232	230	229	230	228	230	229
- 9	218	221	227	221	218	221	221	226	228	232	228	227
- 10	232	234	230	234	236	233	239	240	241	234	230	237
- 11	228	223	225	220	225	224	228	225	228	207	215	221
- 12	227	220	228	229	230	227	228	225	230	227	232	228
- 13	228	227	230	232	230	229	225	221	232	230	227	227
- 14	254	238	237	232	234	239	225	236	236	220	237	231
- 15	258	239	239	230	236	240	232	239	234	210	234	230
- 16	232	230	232	228	236	232	241	232	236	228	232	234
- 17	230	232	231	236	234	233	234	234	236	240	234	236
- 18	239	239	240	240	210	234	236	238	247	240	241	240
- 19	240	239	241	249	243	242	247	241	241	237	234	240

Note : Hardness measurement was performed on both longitudinal and transverse sections on the reverse side of the ruptured area at intervals of 10mm in the longitudinal direction.